

March 11, 1997

Madhulla,

Please review over the Risk Assessment and Risk Assessment addendum for the site at 2425 Encinal Ave. I have gone through and checked all the parameters they have used and have done the calculations to see whether they were done correctly, so you don't need to grind through them again. However, I do have some other questions:

o On Table 4-12 and 4-14, ACC has assumed an ED of 1 year and a EF of 12 days out of the year for a construction worker exposed to inhalation of outdoor air. Do these parameters seem too low? There are planter areas on site. Would it be fair to assess exposure to any potential gardener? 3 months →

o Do you think that the determined excess cancer risk of  $6.7E-05$  is too high? (Refer to Table 6-5 in addendum)? → 8 hr?

o It seems that ACC's overall approach was in conducting the risk assessment was acceptable. Can you skim the reports and see whether you agree?

Let me know whether you have any questions.

Thanks,  
Juliet

$6.5 \times 10^{-3}$  ✓

days / year →  
hours / day →



ENVIRONMENTAL  
PROTECTION  
97 FEB 14 PM 2:04

February 12, 1997

Ms. Juliet Shin  
Alameda County Health Care Services Agency  
1131 Harbor Bay Parkway, Suite 250  
Alameda, California 94502-6577

RE: Tier 1 Risk Assessment Addendum  
2425 Encinal Avenue, Alameda, California  
ACC Project No. 96-6039-2.5

Dear Ms. Shin:

ACC Environmental Consultants, Inc., (ACC) incorporated your comments into the Tier 1 Risk Assessment dated December 31, 1996, for the site at 2425 Encinal Avenue, Alameda, California. The revised Figure 5 and tables are attached, and should amend those in the report. ACC still believes that the risk to human health from constituents on site is minimal.

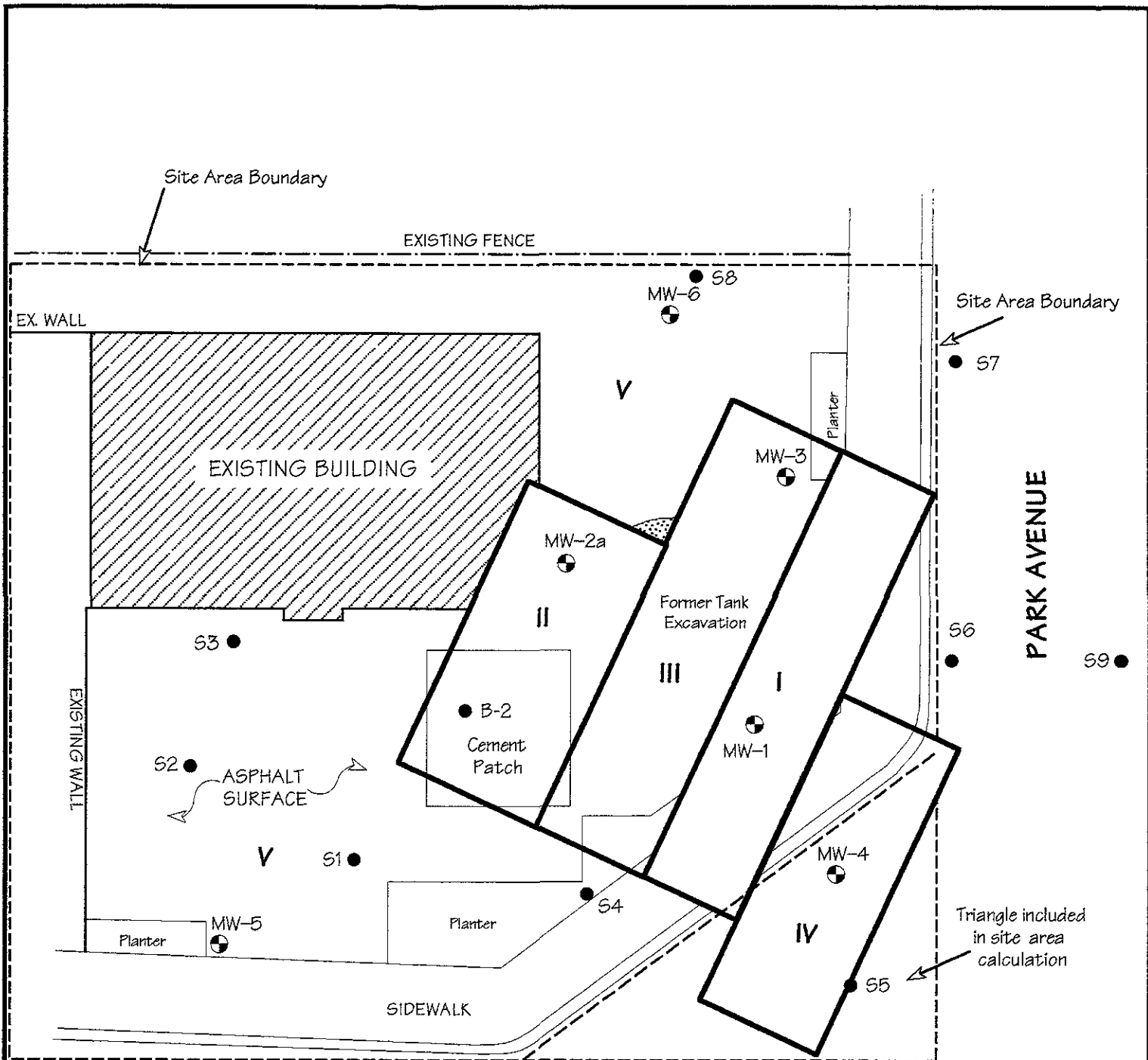
Please contact me if you have any questions regarding this addendum.

Sincerely,

Misty C. Kaltreider  
Senior Project Geologist

/mcr:mck




cc: Mr. Steve Chrissanthos, Alameda Cellars

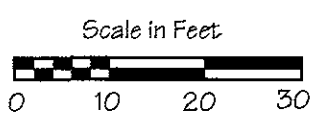


ENCINAL AVENUE

Site Area Boundary

**Legend**

- MW-5  - Groundwater Monitoring Well
- II - Polygon Designation
-  - Polygon Boundary
- S1  - Soil Sampling Location



Title: <b>Area of Polygon Determination</b> <b>2425 Encinal Avenue</b> <b>Alameda, California</b>	
Figure Number: <b>5</b>	Scale: <b>1" = 20'</b>
Drawn By: <b>JVC/DRD</b>	Date: <b>12/31/96</b>
Project Number: <b>6039-2.5</b>	
<b>ACC Environmental Consultants</b> 7977 Capwell Drive, Suite 100 Oakland, CA 94621 (510) 638-8400 Fax: (510) 638-8404	

*Should be 4.31 because soil concentrations from 16' bgs in Well MW-1 should be used because below water table.*

**TABLE 3-1**  
**THIESSEN POLYGON METHOD FOR SOIL**  
 Alameda Cellars  
 2425 Encinal Avenue, Alameda, California

Polygonal Element	Location of Corresponding Concentration in Boring/Well No.*	Mean Benzene Concentration in Soil - C (mg/kg)	Area of the Element A** (m <sup>2</sup> )	A * C (m <sup>2</sup> - mg/kg)	Area Weighted Average Concentration (mg/kg)
I	MW-1	2.15 <del>4.3</del>	81.9 ✓	176.1 <del>352.17</del>	
II	MW-2a, B-2	9.85 ✓	81.27 ✓	800.5	
III	MW-3, S4	0.2 <del>0.3</del>	93.6 ✓	18.72 <del>28.1</del>	
IV	MW-4, S5	0.04 <del>0.05</del>	74.52 ✓	2.98 <del>3.73</del>	
V	MW-5, MW-6, S1, S2, S3, S8	0	906.21	0	
TOTALS			1,237.5	998.3	
Area-Weighted Average Concentration = (Σ A * C)/A <sub>Total</sub>				1183.75	0.81 .96

\* Benzene concentrations from borings S6, S7, and S9 were evaluated to be off the subject property and were not used in the Polygon calculation for the site.

\*\*Areas were calculated by multiplying the area calculated in square feet by the conversion factor of 0.09.

**TABLE 3-2**  
**THIESSEN POLYGON METHOD FOR GROUNDWATER**  
 Alameda Cellars  
 2425 Encinal Avenue, Alameda, California

Polygonal Element	Location of Corresponding Concentration Well No.	Mean Benzene Concentration in Water - C (µg/L)	Area of the Element A* (m <sup>2</sup> )	A * C (m <sup>2</sup> - µg/L)	Area-Weighted Average Concentration µg/L
I	MW-1	395	81.9 ✓	32,350.5 ✓	
II	MW-2a	375	81.27 ✓	30,476.25 ✓	
III	MW-3	38	93.6 ✓	3,556.8 ✓	
IV	MW-4	127	74.52 ✓	9,464.04	
V	MW-5 and MW-6	0	906.21	0	
TOTALS			1,237.5	75,847.59 ✓	
Area-Weighted Average Concentration = (Σ A * C)/A <sub>Total</sub>					61.3 ✓

\*Areas were calculated by multiplying the area calculated in square feet by the conversion factor of 0.09.

**Table 3-3  
Benzene Concentrations in Soil Versus Tier 1 RBSLs**

Route of Exposure	Subsurface Soil (mg/kg)					
	Maximum Detected Concentration	Area Weighted Average Concentration	ASTM RBCA Tier 1 RBSL [1]	USEPA Soil Screening Levels (SSLs)	Average Concentration Exceeds RBSL?	Average Concentration Exceeds SSL?[2]
Indoor Inhalation of Vapor	18.9 mg/kg 1.89E+01	0.81 mg/kg <i>96</i> <del>8.1E-01</del> <i>9.6E-01</i>	3.16E-02	N/A	YES	N/A
Outdoor Inhalation of Vapor	18.9 mg/kg 1.89E+01	0.81 mg/kg <i>96</i> <del>8.1E-01</del> <i>9.6E-01</i>	1.33E00	2.5E+01	no	no
Ingestion of Soil	18.9 mg/kg 1.89E+01	0.81 mg/kg <i>96</i> <del>8.1E-01</del> <i>9.6E-01</i>	1.68E-01	2.2E+02	YES	no

[1] CalEPA. January 5, 1996. *Interim Guidelines*.

[2] USEPA. March 1994. *Technical Background Document for Draft Soil Screening Level Guidance*.

*Soil leachate to protect g.w. ingestion target rate 1/8*

**Table 3-4  
Benzene Concentrations in Groundwater Versus Tier 1 RBSLs**

Route of Exposure	Groundwater (mg/L)			
	Maximum Detected Concentration	Area Weighted Average Concentration	ASTM RBCA Tier 1 RBSL [1]	Average Concentration Exceeds RBSL?
Indoor Inhalation of Vapor	470 µg/L 4.7E+00 mg/L	61.3 µg/L <i>ok</i> 6.13E-02 mg/L	2.14E-01 <i>ok</i> 214 ppb	no
Outdoor Inhalation of Vapor	470 µg/L 4.7E+00 mg/L	61.3 µg/L <i>✓</i> 6.13E-02 mg/L	5.34E+01 <i>ok</i> 53,400 ppb	no
Ingestion of Groundwater	470 µg/L 4.7E+00 mg/L	61.3 µg/L <i>✓</i> 6.13E-02 mg/L	2.86E-02 <i>ok</i> 29 ppb	YES

[1] CalEPA. January 5, 1996. *Interim Guidelines*

**Table 4-1**  
**Effective Diffusion Coefficient in Soil Based on Vapor-Phase Concentration**  
 Alameda Cellars  
 2425 Encinal Avenue, Alameda, California

$$D_s^{eff} (cm^2 / s) = \left[ D_{air} \times \left( \frac{\theta_{as}^{3.33}}{\theta_T^2} \right) \right] + \left[ \frac{D_{wat}}{H} \times \left( \frac{\theta_{ws}^{3.33}}{\theta_T^2} \right) \right] \checkmark$$

Parameter	Value
$D_{air}$	0.093 cm <sup>2</sup> /s ✓
$\theta_{as}$	0.26 cm <sup>3</sup> -air/cm <sup>3</sup> -soil ✓
$\theta_T$	0.38 cm <sup>3</sup> /cm <sup>3</sup> -soil ✓
$D_{wat}$	1.1E-05 cm <sup>2</sup> /s ✓
H	0.22 cm <sup>3</sup> H <sub>2</sub> O/cm <sup>3</sup> -air ✓
$\theta_{ws}$	0.12 cm <sup>3</sup> H <sub>2</sub> O/cm <sup>3</sup> -soil ✓

Therefore,  $D_s^{eff} = 7.26E-03 \text{ cm}^2/\text{s}$  *dk*

**Table 4-2**  
**Effective Diffusion Coefficient Through Foundation**  
 Alameda Cellars  
 2425 Encinal Avenue, Alameda, California

$$D_{crack}^{eff} (cm^2 / s) = \left[ D_{air} \times \left( \frac{\theta_{acrack}^{3.33}}{\theta_T^2} \right) \right] + \left[ \frac{D_{wat}}{H} \times \left( \frac{\theta_{wcrack}^{3.33}}{\theta_T^2} \right) \right] \checkmark$$

Parameter	Value
$D_{air}$	0.093 cm <sup>2</sup> /s ✓
$\theta_{acrack}$	0.26 cm <sup>3</sup> -air/cm <sup>3</sup> -soil ✓
$\theta_T$	0.38 cm <sup>3</sup> /cm <sup>3</sup> -soil ✓
$D_{wat}$	1.1E-05 cm <sup>2</sup> /s ✓
H	0.22 cm <sup>3</sup> H <sub>2</sub> O/cm <sup>3</sup> -air ✓
$\theta_{wcrack}$	0.12 cm <sup>3</sup> H <sub>2</sub> O/cm <sup>3</sup> -soil ✓

Therefore,  $D_{cracks}^{eff} = 7.26E-03 \text{ cm}^2/\text{s}$  *dk*

**Table 4-3**  
**Effective Diffusion Coefficient Through Capillary Fringe**  
 Alameda Cellars  
 2425 Encinal Avenue, Alameda, California

$$D_{cap}^{eff} (cm^2 / s) = \left[ D_{air} \times \left( \frac{\theta_{acap}^{3.33}}{\theta_T^2} \right) \right] + \left[ \frac{D_{wat}}{H} \times \left( \frac{\theta_{wcap}^{3.33}}{\theta_T^2} \right) \right] \checkmark$$

Parameter	Value
$D_{air}$	0.093 cm <sup>2</sup> /s ✓
$\theta_{acap}$	0.38 cm <sup>3</sup> -air/cm <sup>3</sup> -soil ✓
$\theta_T$	0.38 cm <sup>3</sup> /cm <sup>3</sup> -soil ✓
$D_{wat}$	1.1E-05 cm <sup>2</sup> /s ✓
H	0.22 cm <sup>3</sup> H <sub>2</sub> O/cm <sup>3</sup> -air ✓
$\theta_{wcap}$	0.342 cm <sup>3</sup> H <sub>2</sub> O/cm <sup>3</sup> -soil ✓

Therefore,  $D_{cap}^{eff} = 2.6E-02 \text{ cm}^2/\text{s}$  ✓ ok

**Table 4-4**  
**Effective Diffusion Coefficient between Groundwater and Subsurface Soil**  
 Alameda Cellars  
 2425 Encinal Avenue, Alameda, California

$$D_{ws}^{eff} (cm^2 / s) = (h_{cap} + h_v) \times \left[ \left( \frac{h_{cap}}{D_{cap}^{eff}} \right) + \left( \frac{h_v}{D_s^{eff}} \right) \right]^{-1} \checkmark$$

Parameter	Value
$h_{cap}$	5 cm ✓
$h_v$	100 cm ✓
$D_{cap}^{eff}$	2.6E-02 cm <sup>2</sup> /s ✓
$D_s^{eff}$	7.26-03 cm <sup>2</sup> /s ✓

Therefore,  $D_{ws}^{eff} = 7.52E-03 \text{ cm}^2/\text{s}$  ✓ ok

**Table 4-5**  
**Volatilization Factor: Groundwater to Enclosed Space Air**  
 Alameda Cellars  
 2425 Encinal Avenue, Alameda, California

$$VF_{wesp} \left[ \frac{(mg / m^3 - air)}{mg / L - H_2O} \right] = \frac{H \times \left[ \frac{D_{ws}^{eff} / L_{GW}}{ER \times L_B} \right]}{1 + \left[ \frac{D_{ws}^{eff} / L_{GW}}{ER \times L_B} \right] + \left[ \frac{D_{ws}^{eff} / L_{GW}}{(D_{cracks}^{eff} / L_{crack})^n} \right]} \times 10^3 \frac{L}{m^3} \checkmark$$

Parameter	Value
H	0.22 cm <sup>3</sup> H <sub>2</sub> O/cm <sup>3</sup> -air ✓
D <sub>ws</sub> <sup>eff</sup>	7.52E-03 cm <sup>2</sup> /s ✓
L <sub>GW</sub>	105 cm = 3.44' ✓
ER	2.3E-04 s <sup>-1</sup> ✓ (from ASTM)
L <sub>B</sub>	300 cm ✓ ( " )
D <sub>cracks</sub> <sup>eff</sup>	7.26E-03 cm <sup>2</sup> /s ✓
L <sub>crack</sub>	1.5E+01 cm ✓ (from ASTM)
n	1.0E-02 cm <sup>2</sup> -cracks/cm <sup>2</sup> -total area ✓

From ASTM

Therefore, VF<sub>wesp</sub> = 1.45E-01 (mg/m<sup>3</sup>-air)/(mg/L-H<sub>2</sub>O) 1.45 × 10<sup>-2</sup>

**Table 4-6**  
**Volatilization Factor: Groundwater to Ambient Air**  
 Alameda Cellars  
 2425 Encinal Avenue, Alameda, California

$$VF_{wamb} \left[ \frac{(mg / m^3 - air)}{mg / L - H_2O} \right] = \frac{H}{1 + \left[ \frac{U_{air} \times \delta_{air} \times L_{GW}}{W \times D_{ws}^{eff}} \right]} \times 10^3 \frac{L}{m^3} \checkmark$$

Parameter	Value
H	0.22 cm <sup>3</sup> H <sub>2</sub> O/cm <sup>3</sup> -air ✓
U <sub>air</sub>	225 cm ✓ (From ASTM)
δ <sub>air</sub>	200 cm ✓ ( " )
L <sub>GW</sub>	105 cm ✓
W	1,500 cm ✓ (From ASTM)
D <sub>ws</sub> <sup>eff</sup>	7.52E-03 cm <sup>2</sup> /s ✓

also, seems to fit site

Therefore, VF<sub>wamb</sub> = 5.24E-03 (mg/m<sup>3</sup>-air)/(mg/L-H<sub>2</sub>O)  
↑ 5.25 × 10<sup>-4</sup>



**Table 4-7**  
**Volatilization Factor: Soil to Enclosed Space Air**  
 Alameda Cellars  
 2425 Encinal Avenue, Alameda, California

$$VF_{\text{seep}} \left[ \frac{\text{mg} / \text{m}^3 - \text{air}}{\text{mg} / \text{kg} - \text{soil}} \right] = \frac{H \rho_s \left[ \frac{D_s^{\text{eff}} / L_s}{ERL_B} \right]}{\left[ \theta_{ws} + k_s \rho_s + H \theta_{as} \right] \left[ \frac{D_s^{\text{eff}} / L_s}{ERL_B} \right] + \left[ \frac{D_s^{\text{eff}} / L_s}{(D_{\text{crack}}^{\text{eff}} / L_{\text{crack}}) \eta} \right]} \times 10^3 \frac{\text{cm}^3 - \text{kg}}{\text{m}^3 - \text{g}} \checkmark$$

Parameter	Value
H	0.22 cm <sup>3</sup> H <sub>2</sub> O/cm <sup>3</sup> -air ✓
ρ <sub>s</sub>	1.7 g/cm <sup>3</sup> ✓ (From ASTM)
θ <sub>ws</sub>	0.12g/cm <sup>3</sup> ✓ ( " )
k <sub>s</sub>	0.38 cm <sup>3</sup> -H <sub>2</sub> O/g -soil
θ <sub>as</sub>	0.26 cm <sup>3</sup> -air/cm <sup>3</sup> ✓ (From ASTM)
D <sub>s</sub> <sup>eff</sup>	7.26-03 cm <sup>2</sup> /s
ER	2.3E-04 s <sup>-1</sup> ✓ (From ASTM)
L <sub>s</sub>	100 cm ✓ ( " )
L <sub>B</sub>	300 cm ✓ (From ASTM)
D <sub>cracks</sub> <sup>eff</sup>	7.26E-03 cm <sup>2</sup> /s
L <sub>crack</sub>	1.5E+01 cm ✓ (From ASTM)
η	1.0E-02 cm <sup>2</sup> -cracks/cm <sup>2</sup> -total area ✓ (From ASTM)

*K<sub>oc</sub> = 1.58*

*Conservative for site*

Therefore, VF<sub>seep</sub> = 3.3E-04 (mg/m<sup>3</sup>-air)/(mg/kg-soil)

*↑ 2.9 × 10<sup>-2</sup>*

**Table 4-8**  
**Volatilization Factor: Soil to Ambient Air**  
 Alameda Cellars  
 2425 Encinal Avenue, Alameda, California

$$VF_{samb} \left[ \frac{(mg / m^3 - air)}{mg / kg - soil} \right] = \frac{H\rho_s}{[\theta_{ws} + k_s\rho_s + H\theta_{as}] \left( 1 + \frac{U_{air}\delta_{air}L_s}{D_s^{eff}W} \right)} \times 10^3 \frac{cm^3 - kg}{m^3 - g} \checkmark$$

Parameter	Value
H	0.22 cm <sup>3</sup> H <sub>2</sub> O/cm <sup>3</sup> -air ✓
θ <sub>ws</sub>	0.12 cm <sup>3</sup> -air/cm <sup>3</sup> -soil ✓
k <sub>s</sub>	0.38 cm <sup>3</sup> H <sub>2</sub> O/g-soil
θ <sub>as</sub>	0.26 cm <sup>3</sup> -air/cm <sup>3</sup> -soil ✓
U <sub>air</sub>	225 cm ✓ (From A Stu)
δ <sub>air</sub>	200 cm ✓ "
L <sub>s</sub>	100 cm ✓ "
W	1,500 cm ✓ "
D <sub>s</sub> <sup>eff</sup>	7.26E-03 cm <sup>2</sup> /s ✓

ρ<sub>s</sub> = 1.7

Therefore, VF<sub>samb</sub> = 1.1E-02 (mg/m<sup>3</sup>-air)/(mg/kg-soil)

↑  
1.1 x 10<sup>-3</sup>

**Table 4-9**  
**Exposure Point Concentrations for Groundwater COPCs**  
 Alameda Cellars  
 2425 Encinal Avenue, Alameda, California

Chemical	Direct <del>Soil</del> Groundwater Contact (mg/L)	VF <sub>wesp</sub> (mg/m <sup>3</sup> -air)/ (mg/L-H <sub>2</sub> O)	Enclosed Air Concentration (mg/m <sup>3</sup> ) [1]	VF <sub>wamb</sub> (mg/m <sup>3</sup> -air)/ (mg/L-H <sub>2</sub> O)	Ambient Air Concentration (mg/m <sup>3</sup> ) [2]
Benzene	6.13E-02	<del>1.45E-01</del> 1.45 x 10 <sup>-2</sup>	<del>8.9E-03</del> 8.9 x 10 <sup>-4</sup>	<del>5.24E-03</del> 5.24 x 10 <sup>-4</sup>	<del>3.2E-04</del> 3.2 x 10 <sup>-5</sup>

[1] Enclosed space air concentration calculated by multiplying groundwater concentration by appropriate volatilization factor (VF<sub>wesp</sub>).

[2] Ambient air concentration calculated by multiplying groundwater concentration by appropriate volatilization factor (VF<sub>wamb</sub>).

**Table 4-10**  
**Exposure Point Concentrations for Soil COPCs**  
 Alameda Cellars  
 2425 Encinal Avenue, Alameda, California

Chemical	Direct Soil Contact (mg/kg)	VF <sub>seps</sub> (mg/m <sup>3</sup> -air)/ (mg/kg-soil)	Enclosed Air Concentration (mg/m <sup>3</sup> ) [1]	VF <sub>samb</sub> (mg/m <sup>3</sup> -air)/ (mg/kg-soil)	Ambient Air Concentration (mg/m <sup>3</sup> ) [2]
Benzene	<del>8.1E-01</del> 9.6 x 10 <sup>-1</sup>	<del>3.3E-04</del> 2.9 x 10 <sup>-2</sup>	<del>2.7E-04</del> 2.8 x 10 <sup>-2</sup>	<del>1.1E-02</del> 1.1 x 10 <sup>-3</sup>	<del>8.9E-03</del> 1.1 x 10 <sup>-3</sup>

[1] Enclosed space air concentration calculated by multiplying groundwater concentration by appropriate volatilization factor (VF<sub>seps</sub>).

[2] Ambient air concentration calculated by multiplying groundwater concentration by appropriate volatilization factor (VF<sub>samb</sub>).

**Table 4-11**  
**Chemical Intake Exposure Assumptions Onsite Commercial Worker - Groundwater**  
**Inhalation of Indoor Air**  
 Alameda Cellars  
 2425 Encinal Avenue, Alameda, California

$$Intake(mg / kg - day) = \frac{C_A \times IR \times ET \times EF \times ED}{BW \times AT} = \frac{.914}{178500} = 5.1 \times 10^{-7}$$

Parameter	Onsite Commercial Worker Value
CA = Chemical concentration in air (mg/m <sup>3</sup> )	<del>8.9E-03</del> 8.9 x 10 <sup>-4</sup> (see Table 4-9)
IR = Inhalation rate (m <sup>3</sup> /hour)	0.83 ✓
ET = Exposure time (hour/day)	8 ✓ (35)
EF = Exposure frequency (days/year)	250 ✓
ED = Exposure duration (years)	→ 25 ✓ 15 <span style="border: 1px solid black; padding: 2px;">15 yrs!</span>
BW = Body weight (kg)	70 ✓
AT = Averaging time (days)	25,550 ✓

Therefore, Intake for the onsite commercial worker = 2.07E-04 mg/kg-day  
 $\times 10^{-5}$

**Table 4-12**  
**Chemical Intake Exposure Assumptions Onsite Construction Worker - Groundwater**  
**Inhalation of Outdoor Air**  
 Alameda Cellars  
 2425 Encinal Avenue, Alameda, California

$$Intake(mg / kg - day) = \frac{C_A \times IR \times ET \times EF \times ED}{BW \times AT} = \frac{.00079}{188500} = 4.4 \times 10^{-10}$$

Parameter	Onsite Construction Worker Value
CA = Chemical concentration in air (mg/m <sup>3</sup> )	3.2E-04 5 (see Table 4-9)
IR = Inhalation rate (m <sup>3</sup> /hour)	0.83 ✓
ET = Exposure time (hour/day)	8 ✓ (35)
EF = Exposure frequency (days/year)	12 ✓ ? 90 days
ED = Exposure duration (years)	1 ?
BW = Body weight (kg)	70 ✓
AT = Averaging time (days)	25,550 ✓

Therefore, Intake for the onsite construction worker = 1.4E-08 mg/kg-day  
 $1.0 \times 10^{-9}$

**Table 4-13**  
**Chemical Intake Exposure Assumptions Onsite Commercial Worker - Soil**  
**Inhalation of Indoor Air**  
 Alameda Cellars  
 2425 Encinal Avenue, Alameda, California

$$Intake(mg / kg - day) = \frac{C_A \times IR \times ET \times EF \times ED}{BW \times AT} = \frac{2.8 \times 10^{-2} \times 0.83 \times 8 \times 250 \times 15}{70 \times 25,550} = 1.6 \times 10^{-5}$$

Parameter	Onsite Commercial Worker Value
CA = Chemical concentration in air (mg/m <sup>3</sup> )	<del>2.7E-04</del> $2.8 \times 10^{-2}$ (see Table 4-10)
IR = Inhalation rate (m <sup>3</sup> /hour)	0.83 ✓
ET = Exposure time (hour/day)	8 ✓ (133)
EF = Exposure frequency (days/year)	250 ✓
ED = Exposure duration (years)	<del>25</del> 15 ✓ (15)
BW = Body weight (kg)	70 ✓
AT = Averaging time (days)	25,550 ✓ (365 × 70)

Therefore, Intake for the onsite commercial worker =  $6.3E-06$  mg/kg-day  
 $6.5 \times 10^{-4}$   $2.8 \times 10^{-2}$

**Table 4-14**  
**Chemical Intake Exposure Assumptions Onsite Construction Worker- Soil**  
**Inhalation of Outdoor Air**  
 Alameda Cellars  
 2425 Encinal Avenue, Alameda, California

$$Intake(mg / kg - day) = \frac{C_A \times IR \times ET \times EF \times ED}{BW \times AT} = \frac{1.1 \times 10^{-3} \times 0.83 \times 8 \times 12 \times 90}{70 \times 25,550} = 1.5 \times 10^{-8}$$

Parameter	Onsite Construction Worker Value
CA = Chemical concentration in air (mg/m <sup>3</sup> )	<del>8.9E-03</del> $1.1 \times 10^{-3}$ (see Table 4-10)
IR = Inhalation rate (m <sup>3</sup> /hour)	0.83 ✓
ET = Exposure time (hour/day)	8 ✓ (133)
EF = Exposure frequency (days/year)	12 ? 90 days
ED = Exposure duration (years)	1 ?
BW = Body weight (kg)	70 ✓
AT = Averaging time (days)	25,550 ✓

Therefore, Intake for the onsite construction worker =  $3.97E-07$  mg/kg-day  
 $4.8 \times 10^{-8}$

**Table 5-1**  
**Toxicity Values for Benzene**  
Alameda Cellars  
2425 Encinal Avenue, Alameda, California

Chemical	Carcinogenic Weight of Evidence	Inhalation Slope Factor (SF) (mg/kg-day) <sup>-1</sup>	
		Value	Source
Benzene	A	1.0E-01	CalEPA

*rk*

**Table 6-1**  
**Excess Cancer Risk Summary for Onsite Commercial Worker - Groundwater**  
 Alameda Cellars  
 2425 Encinal Avenue, Alameda, California

R = SF x LDCI

Parameter			Onsite, Indoor Commercial Worker Value
R	=	Excess lifetime cancer risk (probability)	2.07E-05
SF	=	Slope factor (mg/kg/day) <sup>-1</sup> for benzene from linearized model	1.0E-01 (see Table 5-1)
LDCI	=	Lifetime daily chemical intake (mg/kg/day)	<del>2.07E-04</del> × 10 <sup>-5</sup> (see Table 4-11)

Therefore, the excess lifetime cancer risk for the onsite, indoor commercial worker = ~~2.07E-05~~ × 10<sup>-6</sup>

**Table 6-2**  
**Excess Cancer Risk Summary for Onsite Construction Worker - Groundwater**  
 Alameda Cellars  
 2425 Encinal Avenue, Alameda, California

R = SF x LDCI

Parameter			Onsite Construction Worker Value
R	=	Excess lifetime cancer risk (probability)	1.4E-09
SF	=	Slope factor (mg/kg/day) <sup>-1</sup> from linearized model	1.0E-01 (see Table 5-1)
LDCI	=	Lifetime daily chemical intake (mg/kg/day)	<del>1.4E-08</del> × 10 <sup>-9</sup> (see Table 4-12)

Therefore, the excess lifetime cancer risk for the onsite, outdoor construction worker = ~~1.4E-09~~ × 10<sup>-10</sup>

**Table 6-3**  
**Excess Cancer Risk Summary for Onsite Commercial Worker - Soil**  
 Alameda Cellars  
 2425 Encinal Avenue, Alameda, California

$R = SF \times LDCI = 1.6 \times 10^{-6}$

Parameter			Onsite, Indoor Commercial Worker Value
R	=	Excess lifetime cancer risk (probability)	6.3E-07
SF	=	Slope factor (mg/kg/day) <sup>-1</sup> for benzene from linearized model	1.0E-01 (see Table 5-1)
LDCI	=	Lifetime daily chemical intake (mg/kg/day)	<del>6.3E-06</del> 6.5 x 10 <sup>-4</sup> (see Table 4-13) 1.6 x 10 <sup>-5</sup>

Therefore, the excess lifetime cancer risk for the onsite, indoor commercial worker = ~~6.3E-07~~  
 $6.5 \times 10^{-5}$

**Table 6-4**  
**Excess Cancer Risk Summary for Onsite Construction Worker - Soil**  
 Alameda Cellars  
 2425 Encinal Avenue, Alameda, California

$R = SF \times LDCI = 10^{-10}$

Parameter			Onsite Construction Worker Value
R	=	Excess lifetime cancer risk (probability)	3.97E-08
SF	=	Slope factor (mg/kg/day) <sup>-1</sup> from linearized model	1.0E-01 (see Table 5-1)
LDCI	=	Lifetime daily chemical intake (mg/kg/day)	<del>3.97E-07</del> 4.8 x 10 <sup>-8</sup> (see Table 4-14)

Therefore, the excess lifetime cancer risk for the onsite, outdoor construction worker = ~~3.97E-08~~  
 $4.8 \times 10^{-9}$

10<sup>-10</sup>



**Table 6-5**  
**Total Excess Cancer Risk Summary for Onsite Commercial Worker**  
 Alameda Cellars  
 2425 Encinal Avenue, Alameda, California

Worker/Pathway	Excess Lifetime Cancer Risk
Onsite Commercial Worker/groundwater ✓	✓ $2.07E-05 \times 10^{-6}$
Onsite Commercial Worker/soil	<del>6.3E-07</del> $6.5 \times 10^{-5}$
Total	<del>2.13E-05</del> $6.7 \times 10^{-5}$

**Table 6-6**  
**Total Excess Cancer Risk Summary for Onsite Construction Worker**  
 Alameda Cellars  
 2425 Encinal Avenue, Alameda, California

Worker/Pathway	Excess Lifetime Cancer Risk
Onsite Construction Worker/groundwater	<del>1.4E-09</del> $1.0 \times 10^{-9}$
Onsite Construction Worker/soil	<del>3.97E-08</del> $4.8 \times 10^{-8}$
Total	<del>4.1E-08</del> $4.9 \times 10^{-8}$