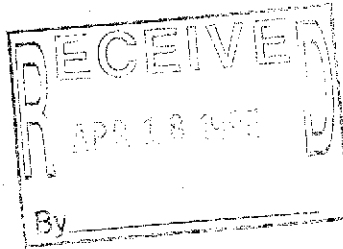


April 17, 1995

**Mr. Lynn Walker**  
*Shell Oil Company*  
 P.O. Box 4023  
 Concord, California 94524



**RE: Corrective Action Plan**  
 Former Shell Service Station  
 15275 Washington Avenue  
 San Leandro, California  
 WIC #204-6852-1108

Dear Mr. Walker:

Enviros, Inc. (Enviros) has prepared this Corrective Action Plan (CAP) to describe a remedial approach for the referenced site (Plates 1 and 2). The approach described in this CAP has been developed to address the Alameda County Health Care Services Agency (ACHCSA) correspondence dated February 16, 1995

**1.0 SITE HISTORY**

In August 1985, Emcon Associates (Emcon) installed four groundwater monitoring wells (designated S-1 through S-4). **Lithology encountered in the borings was primarily clay (CL), with interbedded discreet stringers of sand (SM and SP), and silt (ML).** Groundwater was encountered at 6 to 7 feet below grade (fbg). Petroleum hydrocarbons calculated as Gasoline (TPH-G) were identified in soil samples ranging from 3,100 to 3,900 parts per million (ppm). Dissolved TPH-G was detected in groundwater in Wells S-1, S-2, and S-4 ranging from 520 parts per billion (ppb) to 32,000 ppb. **Floating product (0.5 ft.) was measured in Well S-3.**

*Handwritten note:*  
 "Gall"  
 of various types  
 may also allow  
 to migrate  
 through soil

In August 1986, Emcon drilled four exploratory soil borings (designated S-A through S-D). This investigation was described in the Emcon report dated September 12, 1986. Boring S-A was drilled adjacent to the waste oil tank. Borings S-B through S-D were drilled adjacent to the fuel underground storage tanks (USTs). Boring S-A soils contained 330 ppm TPH, and no waste oil. Borings S-B and S-C contained TPH concentrations ranging from no detection (ND) to 1,700 ppm. Boring S-D was ND at all sample depths. Boring S-B was completed as a monitoring point by installing 3-inch diameter PVC well casing in the borehole. **Floating product was discovered in S-B in August 1986. Product thickness was reported on August 28, 1986 to be 0.40 ft.** Subsequently, this well was measured and floating product was bailed on a weekly basis.

In December 1986, Well [redacted] was installed. TPH-G was detected in well S-5 at a concentration of 7,800 ppb. Benzene was detected at a concentration of 380 ppb. This well installation was described in the Emcon report dated January 28, 1987.

In February 1987, Emcon performed a 1-mile radius water well survey. Based on this survey and calculated groundwater flow direction, southwest-southeast, only three wells were located within a 1/4-mile of the subject property in the downgradient direction. All three wells were former irrigation wells. The closest well was perforated from 100-120 fbg (Well #43). Well #56 was abandoned. Well #41 was drilled to a total depth of 130 feet. No information was available on the perforated zone of this well. Well #41 was located approximately 1/8-mile south of the subject property.

In May 1987, Wells S-B, [redacted] were destroyed during on-site construction activities.

wells reportedly still present during 10/87 trenching activities!

On June 6, 1987, the waste oil tank was replaced with a double-wall tank. This tank removal was documented in the Blaine Tech Services, Inc. (Blaine) report dated June 22, 1987. Soil samples collected beneath the removed tank contained 280 ppm TPH-G and 14 ppm benzene. Analysis for Total Petroleum Hydrocarbons as Diesel (TPH-D) was ND. STLC lead was detected at a concentration of 0.027 mg/L and TTLC lead was detected at a concentration of 22 mg/kg. Organic lead was identified at a concentration of 0.020 mg/kg. Aside from benzene, no VOCs were detected in soil samples from beneath the waste oil tank. As a result, soils were overexcavated to a depth of 13 fbg and approximately 2 to 4 feet beyond the dimensions of the waste oil tank. [redacted]

coups?

On June 9, 1987, four fuel USTs were removed; 2-5,000 gallon tanks, 1-8,000 gallon tank, and 1-7,500 gallon tank. These tank removals are described in the Kaprealian Engineering, Inc. (KEI) report dated June 24, 1987. A total of four soil samples were collected from the tank pit walls (Samples A through D). Groundwater was encountered at 10.5 fbg. Soil sample analyses indicated TPH-G levels of less than 100 ppm in all samples except Sample D (910 ppm). However, due to exposed underground utilities (i.e. sewer line), overexcavation could not be performed. A total of approximately [redacted] in July 1987, KEI sampled the stockpiled soils on site. TPH-G concentrations ranged from 11 to 64 ppm and benzene concentrations ranged from ND to 1.3 ppm. These soils were subsequently transported and disposed of at an appropriate Class III facility.

samples? lack of!

In December 1987, KEI performed a subsurface investigation at the subject property. Three trenches were excavated away from the former tank pit area. The trenches were dug down to a depth of approximately 8.5 fbg. TPH-G was identified in soil at concentrations ranging from 100 to 730 ppm and benzene was identified from at concentrations ranging from 3.9 to 10 ppm. [redacted] On December 22, 1987, the stockpiled soils (approximately [redacted]) were sampled. TPH-G was detected in these soils at a concentration of 3.5 ppm. Benzene was ND. [redacted] The results of this investigation are presented in the KEI report dated December 7, 1987.

200 vbs<sup>3</sup>

Quarterly groundwater monitoring of existing wells began in September 1988.

In November 1988, Woodward-Clyde installed monitoring wells S-6 through S-12. Additionally, a soil gas survey was performed. Soil gas from soil samples ranged from 0.63 to 5,800 ppm for TPH-G and 0.070 to 1,000 ppm for benzene. Groundwater samples collected from Wells S-1 through S-12 contained detectable concentrations of

TPH-G ranging from 50 ppb to 70,000 ppb (Well S-3). Benzene was detected at concentrations up to 4,600 ppb (Well S-3). These activities are described in the Woodward-Clyde report dated April 14, 1989.

In April 1989, GeoStrategies, Inc. (GSI) installed Wells S-13 through S-17. Field procedures for these well installations are described in the GSI report dated October 12, 1989. Additionally, the installation of recovery well SR-1 is also described in this GSI report.

In March 1990, GSI performed a variable discharge pump test in Well SR-1, and slug tests in Wells S-1, S-3, S-5, S-7, S-9, S-10, S-13, S-14, and S-16. The variable test lasted 52 minutes at a pumping rate of 2 gallons per minute. The results of these tests indicated that the aquifer beneath the subject property demonstrated very low yield. Transmissivity values ranged from 408 to 11,000 gallons per day per foot. Hydraulic conductivity values ranged from 7.3 to 100 feet per day. These data were derived from the slug tests. Based on actual yield during pumping, these values appear to be inflated and are probably more representative of the surrounding sandpack material than actual formation material. Based on the very low yield of the aquifer and the distribution of petroleum hydrocarbons in the subsurface, GSI recommended that the Benzene Transport Model developed by Shell Oil Company be used to track plume attenuation. Quarterly reporting continued throughout 1990.

In 1991, GSI prepared and submitted four quarterly reports to the appropriate regulatory agencies. Additionally, Well S-18 was installed. This well installation is described in the GSI June 24, 1991 Site Update/Well Installation Report.

In 1993, Wells S-11 through S-15 were paved over by the City of San Leandro. These wells were relocated, vault boxes raised to new grade and elevations were resurveyed.

## 2.0 SITE CONDITIONS

### 2.1 Previous Investigations

Previous investigations at the subject property have been performed to delineate the extent of petroleum hydrocarbons in soil and groundwater. Additionally, investigations have been performed to characterize hydraulic properties of the shallow aquifer. These investigations have been presented chronologically in section 1.0 and are described in detail in the following sections of this document.

### 2.2 Site Geology

A total of nineteen monitoring wells have been installed and four exploratory soil borings have been drilled to characterize subsurface conditions beneath the subject site. Based on data collected from these investigations, the subsurface geology consists primarily of a low permeability clay (CL and CH) with interbedded discrete stringers of sand (SM and SP) and silt (ML). Well SR-1 is the only well that encountered a sandy aquifer (28 to 40.5 fbg). The upper water-bearing zone appears to extend from a depth of approximately 6 feet to 20 fbg. Water in this upper zone is most likely yielded from the discrete sandy interbeds and possibly from silty horizons in the predominantly clay (CL and CH) matrix. A

geologic cross-section prepared by Woodward-Clyde Consultants depicting subsurface lithology is presented in Appendix A. Exploratory boring logs for soil borings and well borings are also presented in Appendix A.

**2.3 Site Hydrogeology**

First encountered groundwater occurs at depths ranging from approximately 6 to 20 fbg based on review of exploratory boring logs. Stabilized depths to groundwater have ranged from approximately 6 to 9 fbg. Historically, groundwater flow has been predominantly southwest to southeast. Based on a review of historical groundwater elevation data, water level fluctuations appear to be approximately 2 to 4 feet seasonally. Groundwater gradient calculated from the Emcon 4th Quarter 1994 report was 0.004 ft./ft. This gradient is consistent with historical groundwater flow gradient.

The groundwater contour map from the Emcon January 5, 1995 report is included in Appendix B. A summary of Historical Groundwater Elevation Data prepared by Emcon is presented in Table 1.

**2.4 Soil Chemistry**

Sampling data from the underground storage tank removals indicated the presence of TPH-G and benzene in soils from the pit walls and pit bottoms. As a result, over-excavation was performed, when possible, and stockpiled soils were aerated on site and were then properly disposed. Soil samples from the waste oil tank excavation were also analyzed for TPH-D, volatile organic compounds (VOCs), TTLC and STLC lead. **No TPH-D or VOCs (except benzene), were present in the soil.** TTLC and STLC lead values were low (refer to section 1.0). Waste oil was not detected in soil samples taken from the boring (S-A) adjacent to the waste oil tank.

*no evidence for any source removal other than bank fill media*

Soil samples taken from UST complex borings (S-B through S-D) and monitoring well borings S-1 through S-18 were analyzed for Total Petroleum Hydrocarbons calculated as gasoline (TPH-G), and benzene, toluene, ethylbenzene, and xylenes (BTEX). Due to shallow groundwater conditions, **most of the soil samples analyzed were collected from the capillary fringe or saturated zones and may be representative of groundwater conditions.** The distribution of TPH-G and benzene in soils is presented on Plate 3.

*No soil from 4-4.5' depths in borings S-6 thru S-12 do not appear to be representative of GW conditions*

**2.5 Groundwater Chemistry**

Currently, a total of seventeen monitoring wells exist at the subject site. Of these, there are seven on-site wells (S-1, S-3, S-5, S-6, S-7, S-8 and SR-1), and ten off-site wells (S-9 through S-18). The locations of these wells are shown on Plate 2. Quarterly monitoring at the site began in September 1988. Historical Groundwater Analytical Data are presented in Table 2 prepared by Emcon. The most recent TPH-G and BTEX concentration map prepared by Emcon is presented on Plate 4.

Historically, low levels of TPH-G and benzene have been present in Wells S-1, S-6, S-7, S-10, S-11, S-12, S-13, S-15, S-16, S-17 and S-18. Several sampling events indicate levels below method detection limit concentrations in these wells (Table 2). Wells S-1, S-6

**2.7 Previous Source Removal and Remediation Activities**

In 1987, the underground storage tanks were removed from the site as previously described. During the tank removal, approximately [redacted] of soil were excavated. This soil was aerated prior to disposal offsite.

**3.0 GROUNDWATER USE EVALUATION**

**3.1 Beneficial Uses**

The residences and commercial properties in the vicinity of the subject site receive water from the San Leandro and Pardee Reservoirs through the East Bay Municipal Utility District. Drinking water is not supplied from local groundwater. Therefore, groundwater contamination beneath the subject property does not pose a threat to human health since it is not a source of drinking water.

**3.2 Well Survey**

A well survey was performed by Emcon in 1987 and updated by EnviroS in April 1995. The Alameda County Public Works agency was contacted for a list of wells within a 0.5-mile radius of the subject property. The well survey data are presented in Appendix C. Data for downgradient wells identified during this survey are consistent with the 1987 Emcon survey and are presented below.

Address	Owner	Installation Date	Depth (ft.)	Use
15325 Washington	Gualco	1920	130	Irrigation
915 Lewelling	Pianetta	1925	120	Irrigation
15547 Sedgemoor	Raele	—	—	Abandoned

*Dist. from source*

*0.3 mi / 1554 ft*

*0.4 mi / 2112 ft*

*983 Lewelling*  
Based on the size of the groundwater plume as it is presently delineated, these wells are at least 1/8-mile from the distal edge of the groundwater plume (i.e. ND perimeter monitoring wells). *600 ft.*

**3.3 Ecological Considerations**

No recreational waterways exist in close proximity to the subject property. San Lorenzo Creek is located approximately 3/16 of a mile due south of the subject property. This surface waterway is not threatened based on current plume delineation.

**4.0 REMEDIAL ALTERNATIVES EVALUATION**

An evaluation of available remediation alternatives was made based on cost effective capability in protecting groundwater beneficial uses and receptors.

**4.1 Soil Remediation Alternatives**

*Ex-situ* alternatives include either excavation and disposal or excavation and treatment. Previous excavation activities removed the majority of contamination in shallow soils.

Remaining contamination is present within capillary fringe and saturated zones. Based on the extent and depth of this soil contamination beneath the subject property, cost of construction activities and disposal of soils to a landfill, and required backfilling activities, this remedial approach is not technically feasible, nor is it cost-effective.

*In-situ* soil remediation alternatives include soil flushing, solidification/fixation, bioventing, or soil vapor extraction (SVE). Soil flushing is typically used in conjunction with groundwater extraction and requires the injection of a designated "washing" solution which extracts petroleum hydrocarbons from the soil matrix and flushes them down to groundwater for extraction and surface treatment. Soil flushing is technically unfeasible due to low permeability conditions.

Solidification/Fixation involves permanently bonding petroleum hydrocarbons within the soil matrix. Several technologies have been developed for petroleum hydrocarbons such as Portland cement, flyash, and pozzolanic material. However, inherent problems are associated with this technology. The fixing agents must come into intimate contact with the petroleum hydrocarbons to be effective. Since the subsurface lithology is comprised predominantly of clay, this technology is not feasible.

Bioventing is accomplished by supplying oxygen to the soils to enhance and accelerate the natural biodegradation of petroleum hydrocarbons by indigenous microbes. Since the subsurface lithology is comprised of low-permeability clays, this technology is not feasible.

Soil Vapor Extraction (SVE) is a well documented and proven technology to remediate petroleum hydrocarbons in soil and on the groundwater table. A vacuum is applied on extraction wells and the subsequent soil vapors are abated at the ground surface using appropriate abatement equipment. Air flow through the capillary fringe causes volatilization of petroleum hydrocarbons on the groundwater surface. Additionally, as air is pulled through the soil matrix, natural biodegradation is enhanced and accelerated due to the increase in soil oxygen content. Because of the low permeability of subsurface materials and shallow groundwater conditions, SVE is not practical for this site.

**Natural Attenuation Modeling and Monitoring** involves the implementation of modeling to predict the fate and transport of petroleum hydrocarbons identified in soils, and institutional controls such as groundwater monitoring to demonstrate that the hydrocarbons in soils are not leaching to groundwater in a manner which will impact receptors and beneficial uses of groundwater. The low permeability of subsurface materials (i.e. clays) and aquifer testing indicate that migration of contaminants at this site is very slow.

**Therefore it is technically feasible that natural attenuation factors will degrade hydrocarbons in the subsurface prior to their migration to potential receptors.**

## 4.2 Groundwater Remediation Alternatives

The *Ex-situ* alternative is groundwater extraction and treatment. This alternative includes the installation of extraction wells to capture and transport petroleum hydrocarbons to a surface treatment area. Conventional pump and treat systems have proven to be effective in providing hydrodynamic control to preclude plume migration, however, these types of systems have also been shown to be very costly in operations are not effective in removing

petroleum hydrocarbons from soil surfaces (i.e. residual concentrations are not effectively removed for treatment). Based on aquifer test data for the subject site, pumping of groundwater for remediation purposes will be ineffective. Furthermore, pumping would likely promote migration of contaminants from the adjacent service station site onto the subject site.

*In-situ* groundwater remedial alternatives include air sparging, groundwater oxygenation and soil vapor extraction (SVE).

Air sparging involves the injection of air under pressure into the groundwater. This alternative combines two specific methods of groundwater remediation. First, air injected into groundwater strips the volatile components of petroleum hydrocarbons from groundwater. Secondly, air sparging increases the oxygen content of groundwater which enhances and accelerates natural biodegradation processes by indigenous microbes. While air sparging can be effective for groundwater remediation within a limited area surrounding an air sparging well, it has not been demonstrated that any significant radius around the well is benefited. Furthermore, the increased pressure zones created within the aquifer by air injection may promote plume migration and no standard method exists for measuring air sparging's areal influence. Additionally, this technology is not feasible due to low permeability conditions beneath the subject site.

Groundwater oxygenation is similar to air sparging. It involves the injection of low flowrates of air into groundwater in order to increase dissolved oxygen concentrations in groundwater and enhance biodegradation rates by the indigenous microbes. While this technology has feasibility to address groundwater, it is probably not feasible at this site due to low permeability conditions in the subsurface. As a result, this technology was not considered as an alternative for this site.

Soil vapor extraction (SVE), as previously mentioned, has been proven to aid in the remediation of groundwater simultaneously with overlying soils and the capillary fringe. Air flow through the capillary zone causes petroleum hydrocarbons to volatilize from this zone and the groundwater surface and migrate into the overlying soils for capture and surface treatment with appropriate equipment. However, because of low permeability conditions in soils and shallow groundwater conditions beneath the subject site, this technology is not feasible.

**Natural Attenuation Modeling and Monitoring** involves the implementation of modeling to predict the fate and transport of petroleum hydrocarbons identified in groundwater, and institutional controls such as groundwater monitoring to demonstrate that the hydrocarbons are not impacting receptors and beneficial uses of groundwater. The low permeability of subsurface materials (i.e. clays) and aquifer testing indicate that migration of contaminants at this site is very slow. Therefore it is technically feasible that natural attenuation factors will degrade hydrocarbons in the subsurface prior to their migration to potential receptors.

**4.3 Evaluation of Remediation Alternatives**

Enviros has evaluated the screened remediation technologies. Based on this screening, the technologies have been evaluated for three specific criteria:

- Implementability
- Effectiveness in protecting beneficial uses and groundwater receptors
- Cost

Enviros has prepared a Ranking Matrix which summarizes our evaluations of remedial alternatives:

**REMEDIAL ALTERNATIVES  
RANKING MATRIX**

<b>REMEDIAL ALTERNATIVE</b>	<b>IMPLEMENTABILITY</b>	<b>EFFECTIVENESS IN PROTECTING BENEFICIAL USES</b>	<b>COST</b>
<b>SOIL</b>			
ATTENUATION MONITORING	HIGH	HIGH	LOW
<i>EX-SITU</i>	LOW	HIGH	HIGH
<i>IN-SITU</i>	LOW	HIGH	HIGH
<b>GROUNDWATER</b>			
ATTENUATION MONITORING	HIGH	HIGH	LOW
<i>EX-SITU</i>	LOW	HIGH	HIGH
<i>IN-SITU</i>	LOW	HIGH	HIGH

Due to the limited use of groundwater in the vicinity of the subject site, and the location of potential receptors, any of the alternatives would be effective in protecting groundwater beneficial uses. However, natural attenuation is the most cost-effective alternative.

Therefore, natural attenuation modeling and monitoring has been selected to remediate petroleum hydrocarbons present in soil and groundwater.



## 5.0 NATURAL ATTENUATION MODELING

### 5.1 Natural Attenuation Process Description

The fate and transport of petroleum hydrocarbons beneath the subject site are determined primarily by physical and chemical processes. The fate of petroleum hydrocarbons in soil and groundwater beneath the subject property are dictated by the processes of adsorption, absorption, advection, dispersion, diffusion, volatilization, bioaccumulation and biodegradation. **For aromatic hydrocarbons, biodegradation is likely to be the most significant natural attenuation factor.**

Petroleum hydrocarbons released from the subject property have migrated down through the unsaturated zone primarily via advection and dispersion processes in the vicinity of the former USTs. Retardation of petroleum hydrocarbons occurs in unsaturated soils through the processes of adsorption, absorption, volatilization, bioaccumulation and biodegradation.

Petroleum hydrocarbons have been released to groundwater from the unsaturated zone. However, because of the very low permeability of the saturated lithology (primarily clays), migration has been slow. As a result, natural attenuation of petroleum hydrocarbons is suspected to have assisted in impeding migration.

A review of historical groundwater data indicate a general stabilization of concentrations in perimeter wells which define the groundwater plume (i.e. S-10, S-11, S-12, S-13, S-15, S-16, S-17 and S-18). These wells have contained at or near ND levels of petroleum hydrocarbons (Table 2).

### 5.2 Target Receptors

As previously discussed, groundwater is not used as a drinking water source in the vicinity of the subject property. However, the well survey identified three irrigation wells located within a 1/4-mile radius of the subject property in the downgradient direction. These wells are screened in the 100 to 120 fbg range, and are therefore unlikely to be affected by shallow groundwater contamination at the subject site. Furthermore, they are presently located approximately 1/8-mile from the distal edge of the hydrocarbon plume based on monitoring well data. However, they were considered to be receptors in order to maintain a conservative model.

San Leandro Creek was also identified approximately 3/16-mile south of the subject site. This was considered to be an ecological receptor, although it is not threatened based on plume delineation and is located greater than 1/8-mile from the subject site.

### 5.3 Fate and Transport Modeling

#### 5.3.1 FATE2 Model Description

FATE2 is the fate and transport model chosen to predict the migration of petroleum hydrocarbon contaminants and determine whether migration to target receptors will occur.

FATE2 is a modified version of the three-dimensional analytical transient groundwater contaminant model developed by Domenico (1987). Model assumptions include the following:

- uniform and constant aquifer properties
- one dimensional groundwater flow
- first-order contaminant decay, degradation, or transformation, and
- constant contaminant source of rectangular cross-section in the plane perpendicular to groundwater flow.

This original model was issued as FATE in 1992.

Modifications to Domenico's model have resulted in the implementation of the FATE2 model. These modifications have included:

- automation of model calibration to site specific contaminant plume data
- warning messages which flag input and output parameters which exceed nominal ranges,
- automated calculation of plume attenuation factors, and
- graphical output showing the site specific plume data, receptor location, and the modeled plume attenuation.

Domenico's model is based an equation which calculates the maximum centerline (of plume) concentration (of dissolved contaminant) at steady state. This equation is presented in Appendix D.

### 5.3.2 FATE2 Model Parameter Inputs and Outputs

Groundwater contamination sources (i.e. USTs and contaminated soil) were removed from the site in 1987. Review of groundwater analytical data from source area wells shows stabilized levels of hydrocarbons. Therefore, application of FATE2 is appropriate for this site.

FATE2 was applied to the subject site by utilizing the following input data in the model:

Soil Porosity,  $n$  (ft.<sup>3</sup>/ft.<sup>3</sup>): Porosity is percent void space in the soil. Typical values range from 20% to 50%. A soil porosity of 35% was used in this model as it is a common clay porosity value.

Hydraulic Conductivity,  $K$  (ft./day): Hydraulic Conductivity is a measure of the capacity of the aquifer to transmit water. Typical values range from 1.00E-04 to 1.00E+02 (ft./day). Based on site geology and prior aquifer testing, a Hydraulic Conductivity of 3 ft./day was used in this model.

*aquifer tests presented K values of between 2.3 and 100 ft/day*

Hydraulic Gradient,  $i$  (ft./ft.): Hydraulic Gradient is the change in hydraulic head per unit of horizontal distance measured in the downgradient direction. Typical values range from 0.001 to 0.1 ft./ft. 0.005 ft./ft. was used in this model based upon past quarterly groundwater monitoring data.

Source Concentration, Cs (mg/l): The source concentration is the concentration of the contaminants of concern (in this case benzene and TPH-G) in groundwater at the downgradient edge of the source. For use in this model, it has been estimated by calculating the effective solubility of benzene in groundwater by the following equation:

$$C_s = S_i * X_i$$

where  $S_i$  is the solubility limit of the pure compound in water and  $X_i$  is the mole fraction of the compound in a hydrocarbon mixture (as it is applied to the groundwater). In this case,  $S_i = 1780$  mg/l and  $X_i = 0.0205$ . Thus 36.5 mg/l was used in this model as  $C_s$  for benzene. It should be noted that this represents a worst case source concentration as  $S_i$  represents the solubility limit. Furthermore, the highest current benzene concentration in any of the groundwater monitoring wells is 0.467 mg/l, which is 78 times less than the parameter used in the model.

*benzene conc. of  
1000 ppb as  
of 4/95*

The  $C_s$  for TPH-G used in this model was 140 mg/l, which represents the high end of the range of solubility for TPH-G in water and is more than five times greater than any currently measured value.

Source Width, Y (ft.): The source width is the maximum distance in feet perpendicular to the direction of groundwater flow in the saturated zone impacted by the source area. In this case, the width of the former UST area perpendicular the direction of groundwater flow was approximately 40 feet.

Source Thickness, Z (ft.): Source thickness reflects the height of the groundwater column in the source area that contains solubilized petroleum hydrocarbons. Groundwater depths fluctuate from approximately 6 to 9 fbg seasonally. Assuming the total depth of the tank excavation (source area) was 13 fbg, it is estimated that the maximum height of the groundwater column in contact with the former tank excavation is 7 feet, which was thus selected as the source thickness for this model.

Monitoring Point Data: FATE2 is designed for input of data for up to three monitoring point locations. These monitoring points should be located as close to the centerline of the dissolved plume as possible and should span the full length of the dissolved phase plume if possible. The monitoring point data input to FATE2 is the concentration of the contaminants (benzene and TPH-G) and the distance from the source. In this case wells SR-1, S-8, and S-10 were input as monitoring points. Concentrations input into the model are based on worst case conditions, since the highest values which have been detected historically were used for each well. Wells S-12, S-13, and S-14 were not considered as monitoring points as concentration gradients indicate their chemistry may be influenced by the service station located across Lewelling Boulevard to the south of the subject site.

Receptor Distance, R (ft.): The receptor distance is the distance in feet from the downgradient edge of the source to the selected receptor location. As mentioned in the text above, three irrigation wells are listed within a 1/4-mile radius of the subject property in the downgradient direction. Based on the size of the groundwater plume as it is presently delineated, these wells are at least 1/8-mile from the distal edge of the groundwater plume (i.e. ND perimeter monitoring wells). Although the wells are

located an even greater distance from the downgradient edge of the source, the more conservative 1/8 mile (660-feet) distance (the distance from current ND monitoring wells) was used in this model as the receptor distance.

**Target Concentration,  $C^*$  (mg/l):** The target concentration is the selected target exposure point concentration which must be met at the receptor location. In this case the California Department of Health Services Primary MCL of 0.001 mg/l was selected as the target concentration for benzene. No MCL has been established for TPH-G. The analytical method detection limit of 0.050 mg/l was selected as the target concentration for TPH-G.

**Attenuation Coefficient,  $\lambda$  (1/day):** The attenuation coefficient is a measure of the rate at which a compound is lost from a solute plume due to the combined mechanisms of biodegradation, volatilization, and chemical transformation. For aromatic hydrocarbons, such as benzene, aerobic biodegradation is often the dominant mechanism and attenuation rates of 0.001 to 0.01/day are reported for sites where dissolved oxygen concentrations are sufficient to support aerobic biodegradation. In this case 0.0025/day for benzene and 0.0015/day for TPH-G, near the lower end of the attenuation coefficient range, were selected based on existing monitoring well data

**Dispersivity Coefficients, x, y, and z directions ( $\alpha_x, \alpha_y, \alpha_z$ ):** Dispersivity is a measure of the plumes tendency to spread horizontally in the direction of groundwater flow (x direction), horizontally perpendicular to the direction of groundwater flow (y direction), and vertically (z direction). The values used for these input variables (dispersivity multipliers) are those provided by the USEPA Office of Solid Waste *Background Document for the Groundwater Screening Procedure to support 40 CFR Part 268 Land Disposal Restrictions*, 1985. These values are  $\alpha_x = 0.1x$  (where x is the downgradient distance from the source),  $\alpha_y = \alpha_x/3$ , and  $\alpha_z = 0.05 * \alpha_x$ .

Parameters returned by FATE2 based on input data are as follows:

**Attenuation Factor AF:** The attenuation factor, AF, is equal the groundwater concentration at a given distance divided by the source concentration and ranges in value from zero to unity. Since the AF varies with distance from the source, the AF output is provided in the form of a plot where AF is plotted versus distance from the source area. This plot also includes the site monitoring input data, receptor distance, and location of plume attenuation length (see below). Therefore, model output can be compared with site monitoring data from selected well points to support model results.

**Receptor Attenuation Factor AFR:** The receptor attenuation factor, AFR, is equal the groundwater concentration at the receptor distance divided by the source concentration.

**Plume Attenuation Length, PAL (ft.):** The plume attenuation length or PAL is the distance away from the source in the direction of groundwater flow at which the groundwater concentration equals the target concentration,  $C^*$ .

Max Source Concentration,  $C_s^*$ : The maximum source concentration that is protective of a receptor is returned based upon the target concentration and the receptor attenuation factor.

5.3.3 FATE2 Model Results

The FATE2 input parameters, output data, and plot are presented in Appendix D. Results of the modeling are as follows:

Plume Attenuation Length: The PAL returned by FATE2 for benzene is 284 feet, and for TPH-G is 289 feet which indicates that at the given source concentrations, the groundwater concentration of benzene will reach the target concentrations for benzene and TPH-G 284 and 289 feet respectively in the downgradient direction. These PAL's represent less than half the distance to the nearest receptor.

Max Source Concentration,  $C_s^*$ : The maximum source concentration is returned as >S for both benzene and TPH-G, which indicates that the calculated maximum source concentration exceeds the solubility limit for benzene. This agrees with our input data as we had input the solubility limit as the source concentration.

Receptor Attenuation Factor  $A_{fr}$ : Because the calculated maximum source concentration exceeds the solubility limits for benzene and TPH-G,  $A_{fr}$  values are extremely low; 3.27E-12 for benzene and 5.8E-11 for TPH-G.

5.3.4 FATE2 Model Results Discussion

In entering FATE2 model input parameters, conservative values were used, including source concentrations which greatly exceed current measured concentrations since the highest historical value was used for each well. Based on these inputs, model results indicate that natural attenuation will degrade hydrocarbons to target levels at distances from the source considerably less than the distance to the nearest receptor (660 feet). The following table summarizes predicted and actual concentrations for TPH-G and benzene for downgradient wells SR-1, S-8, S-9, S-10, S-17, and S-18. 1/8 mi

Well ID	Distance from Source (ft.)	Predicted TPH-G (ppm)	Predicted Benzene (ppm)	Actual TPH-G (ppm)	Actual Benzene (ppm)
S-8	90	11.2	0.86	0.733	0.076
S-9	75	12.6	1.80	0.979	0.080
S-10	155	1.4	0.072	<0.050	0.002
S-17	185	0.84	0.027	<0.050	<0.0003
S-18	193	0.73	0.024	<0.050	<0.0003

This table demonstrates that measured concentrations in groundwater are within those values predicted by the model.

## 6.0 GROUNDWATER MONITORING PROGRAM

A groundwater monitoring program is proposed to evaluate conformance of the site to predicted model values and to ensure that no migration of the plume to potential receptors occurs.

### 6.1 Proposed Monitoring Program and Rationale

Proposed monitoring frequencies for each well along with rationale for each are listed as follows:

#### Wells S-1, S-6, S-15

These wells are located upgradient from the former USTs. Wells S-6 and S-15 have been ND for TPH-G and BTEX since their installation, with the exception of isolated anomalous detections. Well S-1 has contained only low-level detections of these compounds. **We propose elimination of S-6 and S-15 from the sampling program, and decreasing the sampling frequency of S-1 from quarterly to annual.**

*Do  
measurements  
needed  
upgradient*

#### Wells S-11 and S-16

Well S-11 has been ND for TPH-G and benzene since its installation. Well S-16 has periodically contained low levels of TPH-G and benzene. **We propose elimination of S-11 from the sampling program, and decreasing the sampling frequency of S-16 from quarterly to annual.**

*OK*

#### Wells SR-1, S-3, S-5, S-7

These wells represent source area wells. S-7 has contained low levels of TPH-G and benzene. Wells SR-1, S-3, and S-5 have contained the highest levels of TPH-G and BTEX, but concentrations in these wells are stable and free product is not present. **We propose that these wells be sampled on an annual basis**, provided that concentrations in downgradient wells remain within values predicted by the model. These wells will continue to be gauged on a quarterly basis.

*OK*

#### Wells S-8 and S-9

These wells are located downgradient of the source area wells. Concentrations in these wells will be used to evaluate the site's conformance with model predictions. **These wells will continue to be sampled on a quarterly basis.**

#### Wells S-10, S-17, and S-18

These wells represent a second tier of monitoring downgradient of the source area. Well S-10 has contained low-level concentrations of TPH-G and benzene. Wells S-17 and S-18 have been ND for these compounds since their installation, with the exception of isolated anomalous detections. **We propose continued sampling of S-17 on a quarterly basis**, in order to provide an immediate downgradient indicator should the site fail to conform to model predictions. **Wells S-18 and S-10 are proposed to be sampled on an annual basis.**

Wells S-12, S-13, and S-14

These wells are located in a downgradient/crossgradient direction from the subject site. Concentration gradient data suggest that concentrations in these wells are being influenced by the presence of the service station site located across Lewelling Boulevard to the south of the Shell site. **Continued quarterly monitoring of Well S-13 and elimination of Wells S-12 and S-14 from Shell's monitoring program are proposed.**

Summary

A summary of proposed sampling frequencies is as follows:

S-1	Annual (gauge quarterly)
S-3	Annual
S-5	Annual (gauge quarterly)
S-6	Eliminate from program
S-7	Annual
S-8	Quarterly
S-9	Quarterly
S-10	Annual
S-11	Eliminate from program
S-12	Eliminate from program
S-13	Quarterly
S-14	Eliminate from program
S-15	Eliminate from program
S-16	Annual
S-17	Quarterly
S-18	Annual
SR-1	Annual (gauge quarterly)

**7.0 SUMMARY**

Modeling using the FATE2 modeling program demonstrates that natural attenuation will be effective in remediating petroleum hydrocarbons identified in groundwater prior to their migration to potential receptors.

Data collected during the proposed sampling program will be compared to predicted model values to ensure continued conformance with model output parameters. Any discrepancies will be noted in quarterly monitoring reports, along with explanations and corrective action.

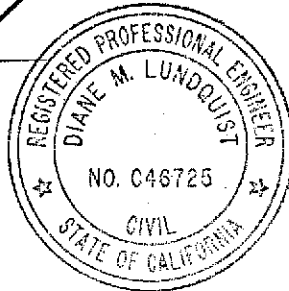
If you have any questions regarding the contents of this document, please call.

Sincerely,

Enviros, Inc.

*Jeffrey L. Peterson*  
Jeffrey L. Peterson  
Hydrogeologist

*Diane M. Lundquist*  
Diane M. Lundquist, P.E.  
Senior Engineer  
C46725





## **Attachments**

Table 1: Summary of Historical Groundwater Elevation Data

Table 2: Summary of Historical Groundwater Analytical Data

Plate 1: Vicinity Map

Plate 2: Site Plan

Plate 3: Soil Quality Map

Plate 4: Groundwater Quality Map

Appendix A: Exploratory Boring Logs & Geologic Cross-Section

Appendix B: Fourth Quarter 1994 - Groundwater Contour Map

Appendix C: Well Survey Data

Appendix D: FATE2 Model Parameters

cc: Mr. Scott Seery, Alameda County Health Care Services, Environmental Protection  
Division

Mr. Rich Hiatt, Regional Water Quality Control Board, San Francisco Bay Region

Mr. Mike Bakaldin, San Leandro Fire Department

Table 1  
Summary of Historical Groundwater Elevation Data

well	Date	Reference Elevation (ft.-MSL)	Depth to Groudwater (feet)	Depth to Floating Product (feet)	Floating Product Thickness (feet)	Groundwater Elevation (Ft.-MSL)
S-1	11/22/88	21.55	8.01	NA	0.00	13.54
	08/10/89	21.55	7.93	NA	0.00	13.62
	10/10/89	21.55	8.09	NA	0.00	13.46
	01/25/90	21.55	7.73	NA	0.00	13.82
	04/18/90	21.55	7.91	NA	0.00	13.64
	07/23/90	21.55	7.72	NA	0.00	13.83
	10/18/90	21.55	8.55	NA	0.00	13.00
	01/28/91	21.55	8.52	NA	0.00	13.03
	04/25/91	21.55	7.18	NA	0.00	14.37
	07/09/91	21.55	8.22	NA	0.00	13.33
	10/08/91	21.55	8.70	NA	0.00	12.85
	02/05/91	21.55	8.14	NA	0.00	13.41
	04/28/92	21.55	7.52	NA	0.00	14.03
	07/27/92	21.55	8.28	NA	0.00	13.27
	10/26/92	21.55	8.74	NA	0.00	12.81
	01/13/93	21.55	5.91	NA	0.00	15.64
	04/16/93	21.55	6.66	NA	0.00	14.89
	07/23/93	21.55	7.53	NA	0.00	14.02
	10/27/93	21.55	8.20	NA	0.00	13.35
	01/27/94	21.55	7.26	NA	0.00	14.29
05/05/94	21.27*	7.38	NA	0.00	13.89	
07/26/94	21.27	7.86	NA	0.00	13.41	
10/28/94	21.27	7.86	NA	0.00	13.41	
S-3	11/22/88	21.14	7.76	NA	0.00	13.38
	08/10/89	21.14	7.92	NA	0.00	13.22
	10/10/89	21.14	8.00	NA	0.00	13.14
	01/25/90	21.14	7.54	NA	0.00	13.60
	04/18/90	21.14	7.74	NA	0.00	13.40
	07/23/90	21.14	7.55	NA	0.00	13.59
	10/18/90	21.14	8.47	NA	0.00	12.67
	01/28/91	21.14	8.38	NA	0.00	12.76
	04/25/91	21.14	6.91	NA	0.00	14.23
	07/09/91	21.14	8.07	NA	0.00	13.07
	10/08/91	21.14	8.61	NA	0.00	12.53
	02/05/91	21.14	7.80	NA	0.00	13.34
	04/28/92	21.14	7.27	NA	0.00	13.87
	07/27/92	21.14	8.10	NA	0.00	13.04
	10/26/92	21.14	8.62	NA	0.00	12.52
	01/13/93	21.14	5.16	NA	0.00	15.98
	04/16/93	21.14	7.18	NA	0.00	13.96
	07/23/93	21.14	7.34	NA	0.00	13.80
	10/27/93	21.14	8.03	NA	0.00	13.11
	01/27/94	21.14	6.79	NA	0.00	14.35
05/05/94	20.48*	6.75	NA	0.00	13.73	
07/26/94	20.48	7.30	NA	0.00	13.18	
10/28/94	20.48	8.36	NA	0.00	12.12	

Table 1  
Summary of Historical Groundwater Elevation Data

well	Date	Reference Elevation (ft.-MSL)	Depth to Groudwater (feet)	Depth to Floating Product (feet)	Floating Product Thickness (feet)	Groundwater Elevation (Ft.-MSL)
S-5	08/10/89	21.41	8.28	NA	0.00	13.13
	10/10/89	21.41	8.32	NA	0.00	13.09
	01/25/90	21.41	8.20	NA	0.00	13.21
	04/18/90	21.41	8.32	NA	0.00	13.09
	07/23/90	21.41	8.03	NA	0.00	13.38
	10/18/90	21.41	9.03	NA	0.00	12.38
	01/28/91	21.41	8.80	NA	0.00	12.61
	04/25/91	21.41	7.40	NA	0.00	14.01
	07/09/91	21.41	8.52	NA	0.00	12.89
	10/08/91	21.41	9.00	NA	0.00	12.41
	02/05/92	21.41	8.11	NA	0.00	13.30
	04/28/92	21.41	7.70	NA	0.00	13.71
	07/27/92	21.41	8.52	NA	0.00	12.89
	10/26/92	21.41	9.02	NA	0.00	12.39
	01/13/93	21.41	5.22	NA	0.00	16.19
	04/16/93	21.41	7.04	NA	0.00	14.37
	07/23/93	21.41	7.75	NA	0.00	13.66
	10/27/93	21.41	8.49	NA	0.00	12.92
	01/27/94	21.41	7.04	NA	0.00	14.37
	05/05/94	21.03*	7.20	NA	0.00	13.83
07/27/94	21.03	7.72	NA	0.00	13.31	
10/28/94	21.03	7.82	NA	0.00	13.21	
S-6	11/22/88	22.02	8.58	NA	0.00	13.44
	08/10/89	22.02	8.54	NA	0.00	13.48
	10/10/89	22.02	8.58	NA	0.00	13.44
	01/25/90	22.02	8.31	NA	0.00	13.71
	04/18/90	22.02	8.43	NA	0.00	13.59
	07/23/90	22.02	8.24	NA	0.00	13.78
	10/18/90	22.02	9.20	NA	0.00	12.82
	01/28/91	22.02	9.10	NA	0.00	12.92
	04/25/91	22.02	7.74	NA	0.00	14.28
	07/09/91	22.02	8.81	NA	0.00	13.21
	10/08/91	22.02	9.26	NA	0.00	12.76
	02/05/92	22.02	8.47	NA	0.00	13.55
	04/28/92	22.02	7.91	NA	0.00	14.11
	07/27/92	22.02	8.83	NA	0.00	13.19
	10/26/92	22.02	9.29	NA	0.00	12.73
	01/13/93	22.02	9.43	NA	0.00	15.59
	04/16/93	22.02	7.12	NA	0.00	14.90
	07/23/93	22.02	8.14	NA	0.00	13.88
	10/27/93	22.02	8.75	NA	0.00	13.27
	01/27/94	22.02	7.87	NA	0.00	14.15
05/05/94	21.40*	7.71	NA	0.00	13.69	
07/26/94	21.40	8.10	NA	0.00	13.30	
10/28/94	21.40	8.04	NA	0.00	13.36	

Table 1  
Summary of Historical Groundwater Elevation Data

well	Date	Reference Elevation (ft.-MSL)	Depth to Groudwater (feet)	Depth to Floating Product (feet)	Floating Product Thickness (feet)	Groundwater Elevation (Ft.-MSL)
S-7	11/22/88	21.47	8.24	NA	0.00	13.23
	08/10/89	21.47	8.18	NA	0.00	13.29
	10/10/89	21.47	8.35	NA	0.00	13.12
	01/25/90	21.47	7.95	NA	0.00	13.52
	04/18/90	21.47	8.06	NA	0.00	13.41
	07/23/90	21.47	7.89	NA	0.00	13.58
	10/18/90	21.47	8.83	NA	0.00	12.64
	01/28/91	21.47	8.77	NA	0.00	12.70
	04/25/91	21.47	7.25	NA	0.00	14.22
	07/09/91	21.47	8.41	NA	0.00	13.06
	10/08/91	21.47	8.95	NA	0.00	12.52
	02/05/92	21.47	8.04	NA	0.00	13.43
	04/28/92	21.47	7.45	NA	0.00	14.02
	07/27/92	21.47	8.48	NA	0.00	12.99
	10/26/92	21.47	9.95	NA	0.00	11.52
	01/13/93	21.47	5.84	NA	0.00	15.63
	04/16/93	21.47	6.38	NA	0.00	15.09
	07/23/93	21.47	7.72	NA	0.00	13.75
	10/27/93	21.47	7.79	NA	0.00	13.68
	01/27/94	21.47	7.85	NA	0.00	13.62
05/05/94	20.85*	9.45	NA	0.00	11.40	
07/26/94	20.85	7.64	NA	0.00	13.21	
10/28/94	20.85	7.68	NA	0.00	13.17	
S-8	11/22/88	20.72	7.76	NA	0.00	12.96
	08/10/89	20.72	7.79	NA	0.00	12.93
	10/10/89	20.72	7.84	NA	0.00	12.88
	01/25/90	20.72	7.47	NA	0.00	13.25
	04/18/90	20.72	7.59	NA	0.00	13.13
	07/23/90	20.72	7.49	NA	0.00	13.23
	10/18/90	20.72	8.44	NA	0.00	12.28
	01/28/91	20.72	8.28	NA	0.00	12.44
	04/25/91	20.72	6.72	NA	0.00	14.00
	07/09/91	20.72	7.98	NA	0.00	12.74
	10/08/91	20.72	8.55	NA	0.00	12.17
	02/05/91	20.72	7.50	NA	0.00	13.22
	04/28/92	20.72	7.14	NA	0.00	13.58
	07/27/92	20.72	8.06	NA	0.00	12.66
	10/26/92	20.72	8.58	NA	0.00	12.14
	01/13/93	20.72	5.32	NA	0.00	15.40
	04/16/93	20.72	5.76	NA	0.00	14.96
	07/23/93	20.72	7.29	NA	0.00	13.43
	10/27/93	20.72	7.93	NA	0.00	12.79
	01/27/94	20.72	6.31	NA	0.00	14.41
05/05/94	20.32*	6.84	NA	0.00	13.48	
07/26/94	20.32	7.42	NA	0.00	12.90	
10/28/94	20.32	7.56	NA	0.00	12.76	

Table 1  
Summary of Historical Groundwater Elevation Data

well	Date	Reference Elevation (ft.-MSL)	Depth to Groudwater (feet)	Depth to Floating Product (feet)	Floating Product Thickness (feet)	Groundwater Elevation (Ft.-MSL)
S-9	11/22/88	20.96	7.78	NA	0.00	13.18
	08/10/89	20.96	7.82	NA	0.00	13.14
	10/10/89	20.96	7.87	NA	0.00	13.09
	01/25/90	20.96	7.41	NA	0.00	13.55
	04/18/90	20.96	7.65	NA	0.00	13.31
	07/23/90	20.96	7.58	NA	0.00	13.38
	10/18/90	20.96	8.46	NA	0.00	12.50
	01/28/91	20.96	8.29	NA	0.00	12.67
	04/25/91	20.96	6.09	NA	0.00	14.87
	07/09/91	20.96	7.82	NA	0.00	13.14
	10/08/91	20.96	8.55	NA	0.00	12.41
	02/05/91	20.96	6.96	NA	0.00	14.00
	04/28/92	20.96	6.76	NA	0.00	14.20
	07/27/92	20.96	8.10	NA	0.00	12.86
	10/26/92	20.96	8.53	NA	0.00	12.43
	01/13/93	20.96	6.80	NA	0.00	14.16
	04/16/93	20.96	6.28	NA	0.00	14.68
	07/23/93	20.96	7.26	NA	0.00	13.70
	10/27/93	20.96	8.00	NA	0.00	12.96
	01/27/94	20.96	5.96	NA	0.00	15.00
05/05/94	20.68*	6.99	NA	0.00	13.69	
07/26/94	20.68	7.56	NA	0.00	13.12	
10/28/94	20.68	7.78	NA	0.00	12.90	
S-10	11/22/88	20.69	7.91	NA	0.00	12.78
	08/10/89	20.69	7.94	NA	0.00	12.75
	10/10/89	20.69	7.99	NA	0.00	12.70
	01/25/90	20.69	7.56	NA	0.00	13.13
	04/18/90	20.69	7.71	NA	0.00	12.98
	07/23/90	20.69	7.64	NA	0.00	13.05
	10/18/90	20.69	8.58	NA	0.00	12.11
	01/28/91	20.69	8.35	NA	0.00	12.34
	04/25/91	20.69	6.91	NA	0.00	13.78
	07/09/91	20.69	8.14	NA	0.00	12.55
	10/08/91	20.69	8.70	NA	0.00	11.99
	02/05/91	20.69	7.57	NA	0.00	13.12
	04/28/92	20.69	7.20	NA	0.00	13.49
	07/27/92	20.69	8.17	NA	0.00	12.52
	10/26/92	20.69	8.68	NA	0.00	12.01
	01/13/93	20.69	3.78	NA	0.00	16.91
	04/16/93	20.69	6.46	NA	0.00	14.23
	07/23/93	20.69	7.38	NA	0.00	13.31
	10/27/93	20.69	8.09	NA	0.00	12.60
	01/27/94	20.69	5.81	NA	0.00	14.88
05/05/94	20.15*	6.82	NA	0.00	13.33	
07/26/94	20.15	7.40	NA	0.00	12.75	
10/28/94	20.15	7.62	NA	0.00	12.53	

Table 1  
Summary of Historical Groundwater Elevation Data

well	Date	Reference Elevation (ft.-MSL)	Depth to Groudwater (feet)	Depth to Floating Product (feet)	Floating Product Thickness (feet)	Groundwater Elevation (Ft.-MSL)
S-11	11/22/88	21.26	8.62	NA	0.00	12.64
	08/10/89	21.26	8.65	NA	0.00	12.61
	10/10/89	21.26	8.64	NA	0.00	12.62
	01/25/90	21.26	8.43	NA	0.00	12.83
	04/18/90	21.26	8.42	NA	0.00	12.84
	07/23/90	21.26	8.23	NA	0.00	13.03
	10/18/90	21.26	9.20	NA	0.00	12.06
	01/28/91	21.26	9.13	NA	0.00	12.13
	04/25/91	21.26	7.53	NA	0.00	13.73
	07/09/91	21.26	8.85	NA	0.00	12.41
	10/08/91	21.26	9.34	NA	0.00	11.92
	02/05/91	21.26	8.50	NA	0.00	12.76
	04/28/92	21.26	7.80	NA	0.00	13.46
	07/27/92	21.26	8.80	NA	0.00	12.46
	10/26/92	21.26	9.42	NA	0.00	11.84
	01/13/93	21.26	6.52	NA	0.00	14.74
	04/16/93	21.26	6.86	NA	0.00	14.40
	07/23/93	21.26	8.07	NA	0.00	13.19
	10/27/93	21.26	NM	NM	NM	NM
	01/27/94	21.26	NM	NM	NM	NM
05/05/94	21.24*	7.73	NA	0.00	13.51	
07/26/94	21.24	8.30	NA	0.00	12.94	
10/28/94	21.24	8.30	NA	0.00	12.94	
S-12	08/10/89	21.05	8.32	NA	0.00	12.73
	10/10/89	21.05	8.32	NA	0.00	12.73
	01/25/90	21.05	8.18	NA	0.00	12.87
	04/18/90	21.05	8.05	NA	0.00	13.00
	07/23/90	21.05	7.92	NA	0.00	13.13
	10/18/90	21.05	8.90	NA	0.00	12.15
	01/28/91	21.05	8.54	NA	0.00	12.51
	04/25/91	21.05	7.08	NA	0.00	13.97
	07/09/91	21.05	8.42	NA	0.00	12.63
	10/08/91	21.05	8.80	NA	0.00	12.25
	02/05/92	21.05	8.07	NA	0.00	12.98
	04/28/92	21.05	8.33	NA	0.00	12.72
	07/27/92	21.05	8.55	NA	0.00	12.50
	10/26/92	21.05	9.03	NA	0.00	12.02
	01/13/93	21.05	6.38	NA	0.00	14.67
	04/16/93	21.05	6.56	NA	0.00	14.49
	07/23/93	21.05	7.76	NA	0.00	13.29
	10/27/93	21.05	NM	NM	NM	NM
	01/27/94	21.05	NM	NM	NM	NM
	05/05/94	20.71*	7.49	NA	0.00	13.22
07/26/94	20.71	7.92	NA	0.00	12.79	
10/28/94	20.71	7.78	NA	0.00	12.93	

Table 1  
Summary of Historical Groundwater Elevation Data

well	Date	Reference Elevation (ft.-MSL)	Depth to Groudwater (feet)	Depth to Floating Product (feet)	Floating Product Thickness (feet)	Groundwater Elevation (Ft.-MSL)
S-13	08/10/89	20.57	8.00	NA	0.00	12.57
	10/10/89	20.57	7.95	NA	0.00	12.62
	01/25/90	20.57	7.79	NA	0.00	12.78
	04/18/90	20.57	7.73	NA	0.00	12.84
	07/23/90	20.57	7.63	NA	0.00	12.94
	10/18/90	20.57	8.58	NA	0.00	11.99
	01/28/91	20.57	8.39	NA	0.00	12.18
	04/25/91	20.57	7.00	NA	0.00	13.57
	07/09/91	20.57	8.12	NA	0.00	12.45
	10/08/91	20.57	8.69	NA	0.00	11.88
	02/05/92	20.57	7.62	NA	0.00	12.95
	04/28/92	20.57	7.15	NA	0.00	13.42
	07/27/92	20.57	8.20	NA	0.00	12.37
	10/26/92	20.57	8.73	NA	0.00	11.84
	01/13/93	20.57	5.06	NA	0.00	15.51
	04/16/93	20.57	6.38	NA	0.00	14.19
	07/23/93	20.57	7.45	NA	0.00	13.12
	10/27/93	20.57	NM	NM	NM	NM
	01/27/94	20.57	NM	NM	NM	NM
	05/05/94	20.16*	6.91	NA	0.00	13.25
07/26/94	20.16	7.52	NA	0.00	12.64	
10/28/94	20.16	7.68	NA	0.00	12.48	
S-14	08/10/89	20.44	7.58	NA	0.00	12.86
	10/10/89	20.44	7.62	NA	0.00	12.82
	01/25/90	20.44	7.82	NA	0.00	12.62
	04/18/90	20.44	7.37	NA	0.00	13.07
	07/23/90	20.44	7.28	NA	0.00	13.16
	10/18/90	20.44	8.10	NA	0.00	12.34
	01/28/91	20.44	8.04	NA	0.00	12.40
	04/25/91	20.44	6.40	NA	0.00	14.04
	07/09/91	20.44	7.69	NA	0.00	12.75
	10/08/91	20.44	8.24	NA	0.00	12.20
	02/05/92	20.44	7.20	NA	0.00	13.24
	04/28/92	20.44	9.75	NA	0.00	10.69
	07/27/92	20.44	7.64	NA	0.00	12.80
	10/26/92	20.44	8.32	NA	0.00	12.12
	01/13/93	20.44	5.07	NA	0.00	15.37
	04/16/93	20.44	5.86	NA	0.00	14.58
	07/23/93	20.44	7.06	NA	0.00	13.38
	10/27/93	20.44	NM	NM	NM	NM
	01/27/94	20.44	NM	NM	NM	NM
	05/05/94	19.99*	6.48	NA	0.00	13.51
07/26/94	19.99	7.04	NA	0.00	12.95	
10/28/94	19.99	7.07	NA	0.00	12.92	

Table 1  
Summary of Historical Groundwater Elevation Data

well	Date	Reference Elevation (ft.-MSL)	Depth to Groudwater (feet)	Depth to Floating Product (feet)	Floating Product Thickness (feet)	Groundwater Elevation (Ft.-MSL)
S-15	08/10/89	22.22	8.48	NA	0.00	13.74
	10/10/89	22.22	8.46	NA	0.00	13.76
	01/25/90	22.22	8.34	NA	0.00	13.88
	04/18/90	22.22	8.45	NA	0.00	13.77
	07/23/90	22.22	8.22	NA	0.00	14.00
	10/18/90	22.22	9.11	NA	0.00	13.11
	01/28/91	22.22	9.13	NA	0.00	13.09
	04/25/91	22.22	7.83	NA	0.00	14.39
	07/09/91	22.22	8.93	NA	0.00	13.29
	10/08/91	22.22	9.26	NA	0.00	12.96
	02/05/92	22.22	8.60	NA	0.00	13.62
	04/28/92	22.22	8.09	NA	0.00	14.13
	07/27/92	22.22	8.83	NA	0.00	13.39
	10/26/92	22.22	9.31	NA	0.00	12.91
	01/13/93	22.22	6.64	NA	0.00	15.58
	04/16/93	22.22	7.14	NA	0.00	15.08
	07/23/93	22.22	8.23	NA	0.00	13.99
	10/27/93	22.22	NM	NM	NM	NM
	01/27/94	22.22	NM	NM	NM	NM
	05/05/94	21.42*	7.57	NA	0.00	13.85
07/26/94	21.42	8.16	NA	0.00	13.26	
10/28/94	21.42	7.87	NA	0.00	13.55	
S-16	08/10/89	21.82	8.36	NA	0.00	13.46
	10/10/89	21.82	8.23	NA	0.00	13.59
	01/25/90	21.82	7.88	NA	0.00	13.94
	04/18/90	21.82	8.19	NA	0.00	13.63
	07/23/90	21.82	8.09	NA	0.00	13.73
	10/18/90	21.82	8.90	NA	0.00	12.92
	01/28/91	21.82	8.55	NA	0.00	13.27
	04/25/91	21.82	7.48	NA	0.00	14.34
	07/09/91	21.82	8.48	NA	0.00	13.34
	10/08/91	21.82	8.95	NA	0.00	12.87
	02/05/92	21.82	8.20	NA	0.00	13.62
	04/28/92	21.82	7.80	NA	0.00	14.02
	07/27/92	21.82	8.29	NA	0.00	13.53
	10/26/92	21.82	9.02	NA	0.00	12.80
	01/13/93	21.82	5.78	NA	0.00	16.04
	04/16/93	21.82	6.80	NA	0.00	15.02
	07/23/93	21.82	7.67	NA	0.00	14.15
	10/27/93	21.82	8.52	NM	NM	13.30
	01/27/94	21.82	7.20	NM	NM	14.62
	05/05/94	21.24*	7.76	NA	0.00	13.48
07/26/94	21.24	7.84	NA	0.00	13.40	
10/28/94	21.24	7.97	NA	0.00	13.27	



Table 1  
Summary of Historical Groundwater Elevation Data

well	Date	Reference Elevation (ft.-MSL)	Depth to Groudwater (feet)	Depth to Floating Product (feet)	Floating Product Thickness (feet)	Groundwater Elevation (Ft.-MSL)
S-17	08/10/89	20.95	8.13	NA	0.00	12.82
	10/10/89	20.95	8.18	NA	0.00	12.77
	01/25/90	20.95	7.60	NA	0.00	13.35
	04/18/90	20.95	7.95	NA	0.00	13.00
	07/23/90	20.95	7.87	NA	0.00	13.08
	10/18/90	20.95	8.71	NA	0.00	12.24
	01/28/91	20.95	8.54	NA	0.00	12.41
	04/25/91	20.95	7.15	NA	0.00	13.80
	07/09/91	20.95	8.24	NA	0.00	12.71
	10/08/91	20.95	8.86	NA	0.00	12.09
	02/05/92	20.95	7.74	NA	0.00	13.21
	04/28/92	20.95	7.41	NA	0.00	13.54
	07/27/92	20.95	8.34	NA	0.00	12.61
	10/26/92	20.95	8.87	NA	0.00	12.08
	01/13/93	20.95	3.43	NA	0.00	17.52
	04/16/93	20.95	6.70	NA	0.00	14.25
	07/23/93	20.95	7.53	NA	0.00	13.42
	10/27/93	20.95	8.29	NA	0.00	12.66
	01/27/94	20.95	5.78	NA	0.00	15.17
	05/05/94	20.45*	6.99	NA	0.00	13.46
07/26/94	20.45	7.62	NA	0.00	12.83	
10/28/94	20.45	7.91	NA	0.00	12.54	
S-18	04/25/91	21.03	NM	NM	NM	NM
	07/09/91	21.03	8.23	NA	0.00	12.80
	10/08/91	21.03	8.84	NA	0.00	12.19
	02/05/92	21.03	7.67	NA	0.00	13.36
	04/28/92	21.03	7.40	NA	0.00	13.63
	07/27/92	21.03	8.38	NA	0.00	12.69
	10/26/92	21.03	8.83	NA	0.00	12.20
	01/13/93	21.03	5.86	NA	0.00	15.17
	04/16/93	21.03	4.88	NA	0.00	16.15
	07/23/93	21.03	7.56	NA	0.00	13.47
	10/27/93	21.03	8.30	NA	0.00	12.73
	01/27/94	21.03	6.84	NA	0.00	14.19
	05/05/94	20.57*	7.05	NA	0.00	13.52
	07/26/94	20.57	7.62	NA	0.00	12.95
10/28/94	20.57	8.01	NA	0.00	12.56	
SR-1	01/25/90	21.45	7.53	NA	0.00	13.92
	04/18/90	21.45	8.17	NA	0.00	13.28
	07/23/90	21.45	7.58	NA	0.00	13.87
	10/18/90	21.45	8.81	NA	0.00	12.64
	01/28/91	21.45	8.37	NA	0.00	13.08
	04/25/91	21.45	6.91	NA	0.00	14.54
	07/09/91	21.45	8.11	NA	0.00	13.34
	10/08/91	21.45	8.63	NA	0.00	12.82
	02/05/92	21.45	7.68	NA	0.00	13.77
	04/28/92	21.45	7.27	NA	0.00	14.18

Table 1  
Summary of Historical Groundwater Elevation Data

well	Date	Reference Elevation (ft.-MSL)	Depth to Groudwater (feet)	Depth to Floating Product (feet)	Floating Product Thickness (feet)	Groundwater Elevation (Ft.-MSL)
SR-1 (cont.)	07/27/92	21.45	8.11	8.10	0.01	13.34
	10/26/92	21.45	8.63	NA	0.00	12.82
	01/13/93	21.45	5.46	NA	0.00	15.99
	04/16/93	21.45	6.28	NA	0.00	15.17
	07/23/93	21.45	7.34	NA	0.00	14.11
	10/27/93	21.45	8.04	NA	0.00	13.41
	01/27/94	21.45	6.68	NA	0.00	14.77
	05/05/94	20.57*	6.81	NA	0.00	13.76
	07/26/94	20.57	7.38	NA	0.00	13.19
	10/28/94	20.57	7.48	NA	0.00	13.09

FT.-MSL = feet above mean sea level

NM.= not measured

\* Top of casing elevation surveyed by L. Wade Hammond on 5/31/94

Table 2

Summary of Historical Groundwater Analytical Results  
(milligrams per liter)

Well Number	Sampling Date	TPHG	Benzene	Toluene	Ethylbenzene	Total Xylenes
S-1	07/08/85	0.52	NA	NA	NA	NA
	09/06/88	<0.050	<0.0005	<0.001	<0.001	<0.003
	11/16/88	<0.050	<0.0005	<0.001	<0.001	<0.003
	02/27/89	<0.050	0.0005	<0.001	<0.001	<0.003
	05/04/89	<0.050	0.001	<0.001	<0.001	<0.003
	08/10/89	<0.050	0.0007	<0.001	<0.001	<0.003
	10/10/89	<0.050	<0.0005	<0.001	<0.001	<0.003
	01/25/90	<0.050	<0.0005	<0.0005	<0.0005	<0.001
	04/18/90	<0.050	<0.0005	<0.0005	<0.0005	<0.001
	07/23/90	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	10/18/90	0.08	0.005	<0.0005	<0.0005	0.003
	01/28/91	<0.050	0.0045	<0.0005	<0.0005	0.002
	04/25/91	0.080*	0.0037	<0.0005	0.0007	0.002
	07/09/91	0.20	0.016	<0.0005	0.0013	0.0058
	10/08/91	<0.050	0.0023	<0.0005	<0.0005	<0.0005
	02/05/92	0.16	0.0089	<0.0005	0.0021	0.006
	04/28/92	<0.050	0.0024	<0.0005	<0.0005	0.0009
	07/27/92	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	10/26/92	0.057	0.003	0.0016	0.0014	0.0017
	01/14/93	0.49	0.053	0.0012	0.020	0.033
	04/16/93	0.24	0.020	<0.0005	0.015	0.24
	07/23/93	<0.050	0.0005	<0.0005	<0.0005	<0.0005
	10/27/93	0.060	0.0059	<0.0005	0.0025	0.0017
	01/27/94	<0.050	0.0021	<0.0005	<0.0005	0.00063
	05/05/94	0.057	0.0039	<0.0005	0.0019	0.0019
	07/26/94	<0.05	0.0022	<0.0003	<0.0003	<0.0006
10/28/94	<0.05	0.0008	<0.0003	<0.0003	0.0008	
S-3	09/06/88	96	3.4 3400	9.5	2.7	17
	11/16/88	70	4.6 4600	8.4	2.5	13
	02/27/89	32	2.4 2400	3.1	1.5	6.4
	05/04/89	47	4.4 4400	0.30	2.4	15
	08/10/89	110	5.7 5700	5.7	3.2	19
	10/10/89	52	4.6 4600	3.3	2.6	15
	01/25/90	420	5.2 5200	4.1	6.7	34
	04/18/90	58	3.8 3800	1.4	2.4	12
	07/23/90	49	3.4 3400	1.8	2.3	12
	10/18/90	44	3.5 3500	0.65	2.4	11
	01/28/91	64	40.9 40,900	0.57	1.94	8.09
	04/25/91	120	3.9 3900	3.6	2.4	8.9
	07/09/91	50	3.6 3600	2.3	1.8	10
	10/08/91	130	3.6 3600	1.0	2.8	8.4
	02/05/92	150	2.5 2500	0.67	2.7	10
	04/28/92	120	2.2 2200	1.2	2	5.8
	07/27/92	190	1.4 1400	<1.25	<1.25	3.4
	10/26/92	950	2.0 2000	8.4	16	36
	01/14/93	41	2.7 2700	2.5	1.8	6.9
	04/16/93	40	0.93 930	2.8	1.9	14
07/23/93	87	1.6 1600	<0.0050	1.3	4.0	

Table 2

Summary of Historical Groundwater Analytical Results  
(milligrams per liter)

Well Number	Sampling Date	TPHG	Benzene	Toluene	Ethylbenzene	Total Xylenes
S-3 (cont.)	10/27/93	36	2.2 2200	<0.5	1.5	3.2
	01/27/94	190	3.2 3200	3.1	4.1	15
	05/05/94	36	1.1 1100	0.49	1.6	4.7
	07/26/94	18.0	1.039 1030	0.1705	0.8454	0.9675
	10/28/94	25.869	0.4679 468	0.2940	0.5462	0.3433
S-5	01/08/87	7.8	0.38	0.51	NR	1.0
	09/06/88	7.0	2.6	0.060	0.40	0.7
	11/16/88	3.0	0.66	0.060	0.12	0.22
	02/27/89	5.7	2.0	0.22	0.26	0.32
	05/04/89	9.0	3.0	0.6	0.63	1.7
	08/10/89	5.1	1.1	<0.050	0.27	0.40
	10/10/89	15	3.3	0.16	0.83	2.2
	01/25/90	12	2.4	0.36	0.57	1.4
	04/18/90	5.2	1.1	0.040	0.30	0.46
	07/23/90	5.5	1.3	0.14	0.32	0.73
	10/18/90	12	3.2	0.040	0.72	0.9
	01/28/91	2.55	0.41	0.015	0.11	0.060
	04/25/91	67	5.1	3.1	2.8	11
	07/09/91	4.9	0.48	0.036	0.36	1.0
	10/08/91	6.6	0.37	0.007	0.19	0.38
	02/05/92	44	4.8	0.85	2.7	8.4
	04/28/92	33	1.4	0.32	1.6	5.2
	07/27/92	20	2.4	<0.025	1.8	2.3
	10/26/92	21	1.6	0.14	1.5	2.8
	01/14/93	54	1.9	1.0	2.7	16
04/16/93	42	2.0	1.3	4.3	18	
07/23/93	46	2.5	2.2	3.4	11	
10/27/93	6.5	0.99	0.031	1.1	1.0	
01/27/94	34	1.8	0.58	2.9	9.7	
05/05/94	24	0.67	0.070	1.4	2.7	
07/27/94	4.7	0.1936	0.0331	0.3323	0.2812	
10/28/94	3.2	0.1673	0.0180	0.2387	0.1045	
S-6	11/16/88	0.050	0.0007	<0.001	<0.001	<0.003
	02/27/89	<0.050	<0.0005	<0.001	<0.001	<0.003
	05/04/89	<0.050	<0.0005	<0.001	<0.001	<0.003
	08/10/89	<0.050	<0.0005	<0.001	<0.001	<0.003
	10/10/89	<0.050	<0.0005	<0.001	<0.001	<0.003
	01/25/90	<0.050	<0.0005	<0.0005	<0.0005	<0.001
	04/18/90	<0.050	<0.0005	0.0006	<0.0005	0.001
	07/23/90	<0.050	<0.0005	0.0009	<0.0005	0.0018
	10/18/90	<0.050	<0.0005	0.0007	<0.0005	0.0008
	01/28/91	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	04/25/91	<0.050	<0.0005	<0.0005	<0.0005	0.0007
	07/09/91	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	10/08/91	<0.050	0.0007	<0.0005	<0.0005	<0.0005
	04/28/92	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
10/26/92	<0.050	<0.0005	<0.0005	<0.0005	<0.0005	

Table 2

Summary of Historical Groundwater Analytical Results  
(milligrams per liter)

Well Number	Sampling Date	TPHG	Benzene	Toluene	Ethylbenzene	Total Xylenes	
S-6 (cont.)	01/13/94	NR	NR	NR	NR	NR	
	04/16/93	<0.050	<0.0005	<0.0005	<0.0005	<0.0005	
	07/23/93	NR	NR	NR	NR	NR	
	10/27/93	<0.050	<0.0005	<0.0005	<0.0005	<0.0005	
	01/27/94	NR	NR	NR	NR	NR	
	05/05/94	<0.050	<0.0005	<0.0005	<0.0005	<0.0005	
	07/26/94	NR	NR	NR	NR	NR	
	10/28/94	<0.05	<0.0003	<0.0003	<0.0003	<0.0006	
S-7	11/16/88	0.10	0.0051	0.015	0.002	0.013	
	02/27/89	0.050	0.0005	0.003	0.001	0.011	
	05/04/89	<0.050	<0.0005	<0.001	<0.001	<0.003	
	08/10/89	<0.050	<0.0005	<0.001	<0.001	<0.003	
	10/10/89	<0.050	<0.0005	<0.001	<0.001	<0.003	
	01/25/90	<0.050	<0.0005	<0.0005	<0.0005	<0.001	
	04/18/90	<0.050	<0.0005	<0.0005	<0.0005	<0.001	
	07/23/90	<0.050	<0.0005	<0.0005	<0.0005	<0.0005	
	10/18/90	<0.050	<0.0005	0.0005	0.0005	0.0041	
	01/28/91	<0.050	<0.0005	<0.0005	<0.0005	<0.0005	
	04/25/91	0.060	<0.0005	<0.0005	<0.0005	<0.0005	
	07/09/91	<0.050	<0.0005	<0.0005	<0.0005	<0.0005	
	02/05/92	<0.050	<0.0005	<0.0005	<0.0005	<0.0005	
	10/08/91	<0.050	<0.0005	<0.0005	<0.0005	<0.0005	
	04/28/92	<0.050	<0.0005	<0.0005	<0.0005	<0.0005	
	07/27/92	<0.050	<0.0005	<0.0005	<0.0005	<0.0005	
	10/26/92	0.57^	<0.0005	<0.0005	<0.0005	<0.0005	
	01/14/93	0.056^	<0.0005	<0.0005	<0.0005	<0.0005	
	04/16/93	0.11	0.028 <sup>28</sup>	<0.0005	<0.0005	<0.0005	0.0018
	07/23/93	0.080	0.00048 <sup>0.45</sup>	<0.0005	<0.0005	<0.0005	0.0008
10/27/93	<0.050	<0.0005	<0.0005	<0.0005	<0.0005	<0.0005	
01/27/94	0.070**	<0.0005	<0.0005	<0.0005	<0.0005	<0.0005	
05/05/94	0.092	0.0021 <sup>2.1</sup>	<0.0005	<0.0005	<0.0005	<0.0005	
07/26/94	0.088	<0.0003	<0.0003	<0.0003	<0.0003	<0.0006	
10/28/94	0.06	<0.0003	0.0005	<0.0003	<0.0003	<0.0006	
S-8	11/16/88	0.21	0.005	<0.001	0.001	0.005	
	02/27/89	<0.050	0.0024	<0.001	<0.001	<0.003	
	05/04/89	<0.050	0.0075	<0.001	0.002	<0.003	
	08/10/89	<0.050	0.0006	<0.001	<0.001	<0.003	
	10/10/89	<0.050	<0.0005	<0.001	<0.001	<0.003	
	01/25/90	<0.050	<0.0005	<0.0005	<0.0005	<0.001	
	04/18/90	<0.050	<0.0005	<0.0005	<0.0005	<0.001	
	07/23/90	<0.050	<0.0005	<0.0005	<0.0005	<0.0005	
	10/18/90	<0.050	<0.0005	<0.0005	<0.0005	<0.0005	
	01/28/91	<0.050	0.055 <sup>55</sup>	0.0005	<0.0005	0.0014	
	04/25/91	0.13*	0.019	<0.0005	0.0013	0.0011	
	07/09/91	0.20	0.033	<0.0005	0.0018	0.0028	
	10/08/91	0.58	0.095 <sup>95</sup>	0.0022	0.0049	0.0065	
	02/05/92	0.090*	0.018	<0.0005	0.0062	0.0018	

Table 2

Summary of Historical Groundwater Analytical Results  
(milligrams per liter)

Well Number	Sampling Date	TPHG	Benzene	Toluene	Ethylbenzene	Total Xylenes
S-8 (cont.)	04/28/92	<0.050	0.0059	<0.0005	0.0025	<0.0005
	07/27/92	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	10/26/92	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	01/14/93	0.27	0.074	0.0009	0.025	0.0055
	04/16/93	1.1	0.42 <i>420</i>	<0.0005	0.20	0.020
	07/23/93	0.16	0.023	<0.0005	0.0012	0.0015
	10/27/93	0.42	<i>0.065-0.65-650</i>	0.0007	0.011	0.0017
	01/27/94	0.29	0.065	<0.0010	0.0069	0.0024
	05/05/94	0.12	0.013	<0.0005	<0.0005	<0.0005
	07/26/94	0.115	0.0122	0.0013	<0.0003	0.0027
	10/28/94	0.733	0.0759	0.0032	0.0049	0.0042
S-9	11/16/88	1.4	0.069 <i>69</i>	0.003	0.052	0.18
	02/27/89	1.6	0.24 <i>240</i>	0.004	0.13	0.18
	05/04/89	2.6	0.47 <i>470</i>	0.010	0.24	0.48
	08/10/89	0.52	0.073 <i>73</i>	<0.01	0.040	<0.030
	10/10/89	0.38	0.082 <i>82</i>	<0.001	0.046	0.013
	01/25/90	0.75	0.14 <i>140</i>	0.0012	0.069	0.075
	04/18/90	0.68	0.15 <i>150</i>	0.0017	0.050	0.037
	07/23/90	0.49	0.094 <i>94</i>	0.0012	0.032	0.024
	10/18/90	0.39	0.14 <i>140</i>	0.0007	0.0033	0.024
	01/28/91	1.04	0.45 <i>450</i>	0.0046	0.085	0.097
	04/25/91	5.8	0.88 <i>880</i>	0.009	0.36	0.50
	07/09/91	1.4	0.22 <i>220</i>	0.0028	0.082	0.10
	10/08/91	0.89	0.96 <i>960</i>	<0.0025	0.016	0.029
	02/05/92	0.95	0.24 <i>240</i>	<0.0025	0.028	0.055
	04/28/92	1.4*	0.29 <i>290</i>	0.003	0.10	0.081
	07/27/92	0.89	0.19 <i>190</i>	<0.0025	0.066	0.068
	10/26/92	0.65	0.16 <i>160</i>	<0.0025	0.063	0.089
	01/13/93	19	2.4 <i>2400</i>	0.038	1.7	2.2
	04/16/93	10	1.5 <i>1500</i>	<0.005	1.1	0.99
	07/23/93	1.1	0.40 <i>400</i>	<0.0050	0.26	0.16
10/27/93	2.5	0.40 <i>400</i>	<0.005	0.19	0.11	
01/27/94	4.8	0.99 <i>990</i>	0.016	0.63	0.49	
05/05/94	3.7	0.48 <i>480</i>	<0.005	0.021	0.12	
07/26/94	1.0	0.1246 <i>124.6</i>	<0.0003	0.0358	0.0286	
10/28/94	0.979	0.0803 <i>80.3</i>	0.0070	0.0217	0.0292	
S-10	11/16/88	0.33	0.0005 <i>540</i>	<0.001	0.001	0.011
	02/27/89	0.14	<0.0005 <i>1000</i>	<0.003	0.002	0.006
	05/03/89	0.22	<0.0005	0.001	0.002	0.007
	08/10/89	<0.050	<0.0005	<0.001	<0.001	<0.003
	10/09/89	0.17	<0.0005	<0.001	<0.001	<0.003
	01/25/90	<0.050	<0.0005	<0.0005	0.0011	0.004
	04/18/90	<0.050	<0.0005	0.0009	<0.0005	0.002
	07/23/90	0.59	<0.0005	<0.0005	0.0019	0.019
	10/18/90	0.14	<0.0005	0.0007	<0.0005	0.007
	01/28/91	<0.050	<0.0005	<0.0005	<0.0005	0.0005
	04/25/91	<0.050	<0.0005	<0.0005	0.0011	0.0008

Table 2

Summary of Historical Groundwater Analytical Results  
(milligrams per liter)

Well Number	Sampling Date	TPHG	Benzene	Toluene	Ethylbenzene	Total Xylenes
S-10 (cont.)	07/09/91	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	10/08/91	0.14	<0.0005	<0.0005	<0.0005	<0.0005
	02/05/92	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	04/28/92	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	07/27/92	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	10/26/92	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	01/13/93	0.088	<0.0005	0.0006	0.0006	<0.0005
	04/16/93	0.080	<0.0005	<0.0005	<0.0005	<0.0005
	07/23/93	<0.050	0.0015	<0.0005	0.0007	0.0027
	10/27/93	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	01/27/94	0.27	0.0011	0.0013	0.0020	0.0074
	05/05/94	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	07/26/94	<0.05	<0.0003	<0.0003	<0.0003	<0.0006
	10/28/94	<0.05	0.0024	<0.0003	0.0005	0.0008
S-11	11/16/88	<0.050	<0.0005	<0.001	<0.001	<0.003
	02/27/89	<0.050	<0.0005	<0.001	<0.001	<0.003
	05/03/89	<0.050	<0.0005	<0.001	<0.001	<0.003
	08/10/89	<0.050	<0.0005	<0.001	<0.001	<0.003
	10/09/89	<0.050	<0.0005	<0.001	<0.001	<0.003
	01/25/90	<0.050	<0.0005	<0.0005	<0.0005	<0.001
	04/18/90	<0.050	<0.0005	<0.0005	<0.0005	<0.001
	07/23/90	<0.050	<0.0005	0.0006	<0.0005	0.0011
	10/18/90	<0.050	<0.0005	<0.0005	<0.0005	0.0005
	01/28/91	0.063	<0.0005	0.0033	0.0009	0.007
	04/25/91	<0.050	<0.0005	<0.0005	0.0008	<0.0005
	07/09/91	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	10/08/91	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	04/28/92	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	07/27/92	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	10/26/92	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	01/13/93	NR	NR	NR	NR	NR
	04/16/93	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	07/23/93	NR	NR	NR	NR	NR
	10/27/93	NA	NA	NA	NA	NA
01/27/94	NR	NR	NR	NR	NR	
05/05/94	<0.050	<0.0005	<0.0005	<0.0005	<0.0005	
07/26/94	NR	NR	NR	NR	NR	
10/28/94	<0.05	<0.0003	<0.0003	<0.0003	<0.0006	
S-12	11/16/88	0.050	0.0035	<0.001	<0.001	<0.003
	02/27/89	<0.050	0.0008	<0.001	<0.001	<0.003
	05/03/89	<0.050	<0.0005	<0.001	<0.001	<0.003
	08/10/89	<0.050	<0.0005	<0.001	<0.001	<0.003
	10/09/89	<0.050	<0.0005	<0.001	<0.001	<0.001
	01/25/90	<0.050	<0.0005	<0.0005	<0.0005	<0.001
	04/18/90	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	07/23/90	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	10/18/90	<0.050	<0.0005	<0.0005	<0.0005	<0.0005

Table 2

Summary of Historical Groundwater Analytical Results  
(milligrams per liter)

Well Number	Sampling Date	TPHG	Benzene	Toluene	Ethylbenzene	Total Xylenes
S-12 (cont.)	01/28/91	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	04/25/91	0.090	0.0054	<0.0005	0.0011	0.0007
	07/09/91	<0.050	0.0029	<0.0005	<0.0005	<0.0005
	10/08/91	0.050	<0.0005	<0.0005	<0.0005	<0.0005
	02/05/92	0.050*	<0.0005	<0.0005	<0.0005	<0.0005
	04/28/92	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	07/27/92	0.094^	<0.0005	<0.0005	<0.0005	<0.0005
	10/26/92	0.086^	<0.0005	<0.0005	<0.0005	<0.0005
	01/14/93	0.12	0.002	<0.0005	<0.0005	<0.0005
	04/16/93	0.060	<0.0005	<0.0005	<0.0005	<0.0005
	07/23/93	0.090	<0.0005	<0.0005	<0.0005	<0.0005
	10/27/93	NA	NA	NA	NA	NA
	01/27/94	NA	NA	NA	NA	NA
	05/05/94	<0.050	0.0020	<0.0005	<0.0005	<0.0005
	07/26/94	0.128	<0.0003	<0.0003	<0.0003	<0.0006
	10/28/94	0.167	<0.0003	<0.0003	<0.0003	<0.0006
S-13	05/03/89	0.15	0.0049	0.004	0.002	0.014
	08/10/89	0.11	0.0029	<0.001	<0.001	<0.003
	10/09/89	0.077	0.0014	<0.001	<0.001	<0.003
	01/25/90	0.051	0.0005	<0.0005	<0.0005	<0.001
	04/18/90	0.085	0.0087	<0.0005	<0.0005	<0.001
	07/23/90	0.080	0.0008	<0.0005	<0.0005	<0.0005
	10/18/90	0.13	<0.0005	<0.0005	<0.0005	<0.005
	01/28/91	<0.050	<0.0005	0.0009	0.0012	0.001
	04/25/91	0.44*	0.0038	<0.0005	<0.0005	0.0006
	07/09/91	0.32*	0.0006	<0.0005	<0.0005	<0.0005
	10/08/91	0.31	<0.0005	<0.0005	<0.0005	<0.0005
	04/28/92	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	10/26/92	0.18^	<0.0005	<0.0005	<0.0005	<0.0005
	01/13/93	NR	NR	NR	NR	NR
	04/16/93	0.24	0.0048	<0.0005	0.0013	<0.0005
	07/23/93	NR	NR	NR	NR	NR
	10/27/93	NA	NA	NA	NA	NA
	01/27/94	NR	NR	NR	NR	NR
	05/05/94	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	07/26/94	NR	NR	NR	NR	NR
10/28/94	0.368	<0.0003	<0.0003	<0.0003	<0.0006	
S-14	05/03/89	5.3	0.75	0.40	0.2	0.80
	08/10/89	1.8	0.54	0.14	0.042	0.05
	10/09/89	1.0	0.36	0.060	0.02	0.030
	01/25/90	0.64	0.16	0.077	0.017	0.039
	04/18/90	1.2	0.20	0.11	0.03	0.096
	07/23/90	5.0	0.43	0.34	0.14	0.66
	10/18/90	1.8	0.77	0.013	0.017	0.12
	01/28/91	0.72	0.20	0.036	0.021	0.078
	04/25/91	14	0.93	0.43	0.25	0.97
	07/09/91	0.16	0.030	0.0053	0.005	0.016



Table 2

Summary of Historical Groundwater Analytical Results  
(milligrams per liter)

Well Number	Sampling Date	TPHG	Benzene	Toluene	Ethylbenzene	Total Xylenes
S-14 (cont.)	10/08/91	5.4	0.081	0.057	0.095	0.38
	04/28/92	2.0	0.27	0.14	0.048	0.17
	10/26/92	0.92	0.033	0.012	0.025	0.088
	01/13/93	NR	NR	NR	NR	NR
	04/16/93	4.5	1.1	0.029	0.091	0.17
	07/23/93	NR	NR	NR	NR	NR
	10/27/93	NA	NA	NA	NA	NA
	01/27/94	NR	NR	NR	NR	NR
	05/05/94	0.81	0.25	<0.0025	0.0094	0.019
	07/26/94	NR	NR	NR	NR	NR
	10/28/94	5.385	0.2906	0.0858	0.0497	0.1862
S-15	05/03/89	<0.050	<0.0005	<0.001	<0.001	<0.003
	08/10/89	<0.050	<0.0005	<0.001	<0.001	<0.003
	10/09/89	<0.050	<0.0005	<0.001	<0.001	<0.003
	01/25/90	<0.050	<0.0005	<0.001	<0.001	<0.001
	04/18/90	<0.050	<0.0005	<0.0005	<0.0005	<0.001
	07/23/90	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	10/18/90	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	01/28/91	<0.050	<0.0005	0.0006	<0.0005	0.0008
	04/25/91	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	07/09/91	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	10/08/91	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	02/05/92	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	04/28/92	0.050	0.0008	0.0009	<0.0005	0.0014
	07/27/92	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	10/26/92	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	01/14/93	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	04/16/93	<0.050	0.0006	0.001	<0.0005	0.0007
	07/23/93	<0.050	0.0012	<0.0005	<0.0005	0.0016
	10/27/93	NA	NA	NA	NA	NA
	01/27/94	NA	NA	NA	NA	NA
05/05/94	<0.050	<0.0005	<0.0005	<0.0005	<0.0005	
07/26/94	<0.05	<0.0003	<0.0003	<0.0003	<0.0006	
10/28/94	<0.05	0.0003	<0.0003	<0.0003	<0.0006	
S-16	05/04/94	0.38	0.044	0.003	0.002	<0.003
	08/10/89	<0.050	0.0006	<0.001	<0.001	<0.003
	10/10/89	<0.005	<0.0005	<0.001	<0.001	<0.003
	01/25/90	0.24	0.16	0.0033	0.0008	0.011
	04/18/90	<0.050	0.001	<0.0005	<0.0005	<0.001
	07/23/90	<0.050	0.0011	<0.0005	<0.0005	<0.0005
	10/18/90	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	01/28/91	<0.050	<0.0005	0.0006	<0.0005	0.0009
	04/25/91	0.060^	0.021	0.0005	0.0032	0.0048
	07/09/91	<0.050	0.001	<0.0005	<0.0005	<0.0005
	10/08/91	0.050	0.017	0.0014	0.0012	0.0055
	02/05/92	0.15	0.065	0.0007	<0.0005	0.0084
	04/28/92	<0.050	0.013	<0.0005	<0.0005	<0.0005

Table 2

Summary of Historical Groundwater Analytical Results  
(milligrams per liter)

Well Number	Sampling Date	TPHG	Benzene	Toluene	Ethylbenzene	Total Xylenes
S-16 (cont.)	07/27/92	0.51	0.13	<0.0025	<0.0005	0.021
	10/26/92	<0.050	<0.0005	<0.0005	<0.0025	<0.0005
	01/13/93	0.10	0.025	0.0019	<0.0005	0.0084
	04/16/93	0.15	0.056	0.0018	0.0046	0.012
	07/23/93	<0.050	0.0009	<0.0005	<0.0005	<0.0005
	10/27/93	<0.050	0.0015	<0.0005	<0.0005	<0.0005
	01/27/94	0.14	0.085	<0.0010	<0.0010	0.013
	05/05/94	0.071	0.025	<0.0005	<0.0005	0.0042
	07/26/94	<0.05	<0.0003	<0.0003	<0.0003	<0.0006
	10/28/94	<0.05	0.0115	<0.0003	<0.0003	0.0018
S-17	05/03/89	<0.050	<0.0005	<0.001	<0.001	<0.003
	08/10/89	<0.050	<0.0005	<0.001	<0.001	<0.003
	10/09/89	<0.050	<0.0005	<0.001	<0.001	<0.003
	01/25/90	<0.050	<0.0005	<0.0005	<0.0005	<0.001
	04/18/90	<0.050	<0.0005	<0.0005	<0.0005	<0.001
	07/23/90	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	10/18/90	0.39	0.010	0.062	0.022	0.11
	01/28/91	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	04/25/91	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	07/09/91	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	10/08/91	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	04/28/92	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	10/26/92	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	01/13/93	NR	NR	NR	NR	NR
	04/16/93	0.13	<0.0005	<0.0005	<0.0005	<0.0005
	07/23/93	NR	NR	NR	NR	NR
	10/27/93	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	01/27/94	NR	NR	NR	NR	NR
	05/05/94	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	07/26/94	NR	NR	NR	NR	NR
10/28/94	<0.05	<0.0003	<0.0003	<0.0003	<0.0006	
S-18	05/31/91	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	07/09/91	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	10/08/91	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	02/05/92	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	04/28/92	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	07/27/92	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	10/26/92	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	01/13/93	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	04/16/93	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	07/23/93	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	10/27/93	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	01/27/94	<0.050	0.0019	<0.0005	<0.0005	<0.0005
	05/05/94	<0.050	<0.0005	<0.0005	<0.0005	<0.0005
	07/26/94	<0.5	<0.003	0.0011	<0.0003	0.0018
	10/28/94	<0.05	<0.0003	<0.0003	<0.0003	<0.0006

Table 2

Summary of Historical Groundwater Analytical Results  
(milligrams per liter)

Well Number	Sampling Date	TPHG	Benzene	Toluene	Ethylbenzene	Total Xylenes
SR-1	03/22/89	5.4	1.1 <sup>1100</sup>	0.23	0.35	1.3
	01/25/90	2.2	0.47 <sup>470</sup>	0.12	0.11	0.51
	04/18/90	1.0	0.13 <sup>130</sup>	0.047	0.047	0.22
	07/23/90	3.2	0.47 <sup>470</sup>	0.32	0.17	0.87
	10/18/90	1.3	0.28 <sup>280</sup>	0.0066	0.11	0.13
	01/28/91	0.11	0.12 <sup>120</sup>	0.012	0.051	0.11
	07/09/91	1.4	0.20 <sup>200</sup>	0.027	0.13	0.34
	10/08/91	0.98	0.079 <sup>79</sup>	0.0015	0.044	0.052
	02/05/91	3.8	0.58 <sup>580</sup>	0.036	0.32	0.40
	04/28/92	38	1.8 <sup>1800</sup>	0.46	1.9	0.75
	07/27/92	FP	FP	FP	FP	FP
	10/26/92	1.8	0.37 <sup>370</sup>	0.010	0.13	0.13
	1/13/93	47	1.0 <sup>1000</sup>	1.1	1.7	13
	4/16/93	25	1.7 <sup>1700</sup>	0.43	2.4	8.3
	7/23/93	33	2.4 <sup>2400</sup>	2.0	3.8	14
	10/27/93	2.3	0.34 <sup>3400</sup>	<0.0125	0.27	0.44
	1/27/94	36	2 <sup>2000</sup>	1.7	3.0	11
	5/5/94	43	1.5 <sup>1500</sup>	0.13	2.9	12
	7/26/94	13.6	0.6827 <sup>682</sup>	0.0392	0.9966	2.516
	10/28/94	8.462	0.3015 <sup>301</sup>	0.0293	0.3847	2.019

TPHG = Total petroleum hydrocarbons as gasoline by EPA Method 8015 (modified).

BTEX = Benzene, toluene, ethylbenzene and total xylenes by EPA Method 8020.

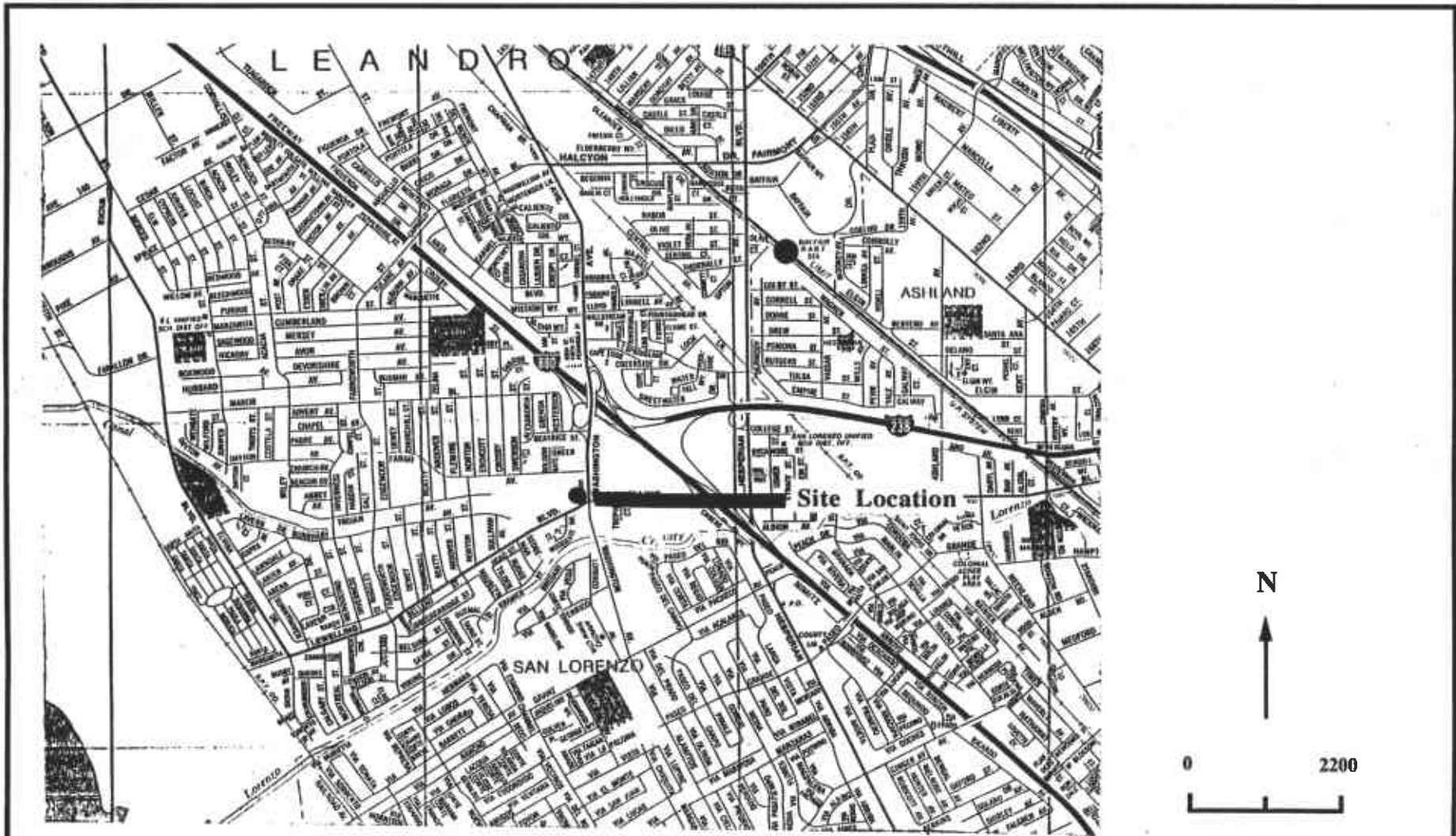
NA = Not analyzed; well inaccessible.

NR = Not required.

\* = Compounds detected within the chromatographic range of gasoline but not characteristic of the standard gasoline pattern.

\*\* = The concentration reported as gasoline is primarily due to the presence of a discrete peak not indicative of gasoline.

^ = Compounds detected are volatile aromatics (BTEX) present in sample.



Note: Vicinity Map taken from California State Automobile Association Map.

**PLATE**  
**1**

**SITE VICINITY MAP**  
Shell Oil Company  
15275 Washington Avenue  
San Leandro, California

**enviros**<sup>®</sup>  
95276.01

Drawn By: JLP                      Date: 3-23-95

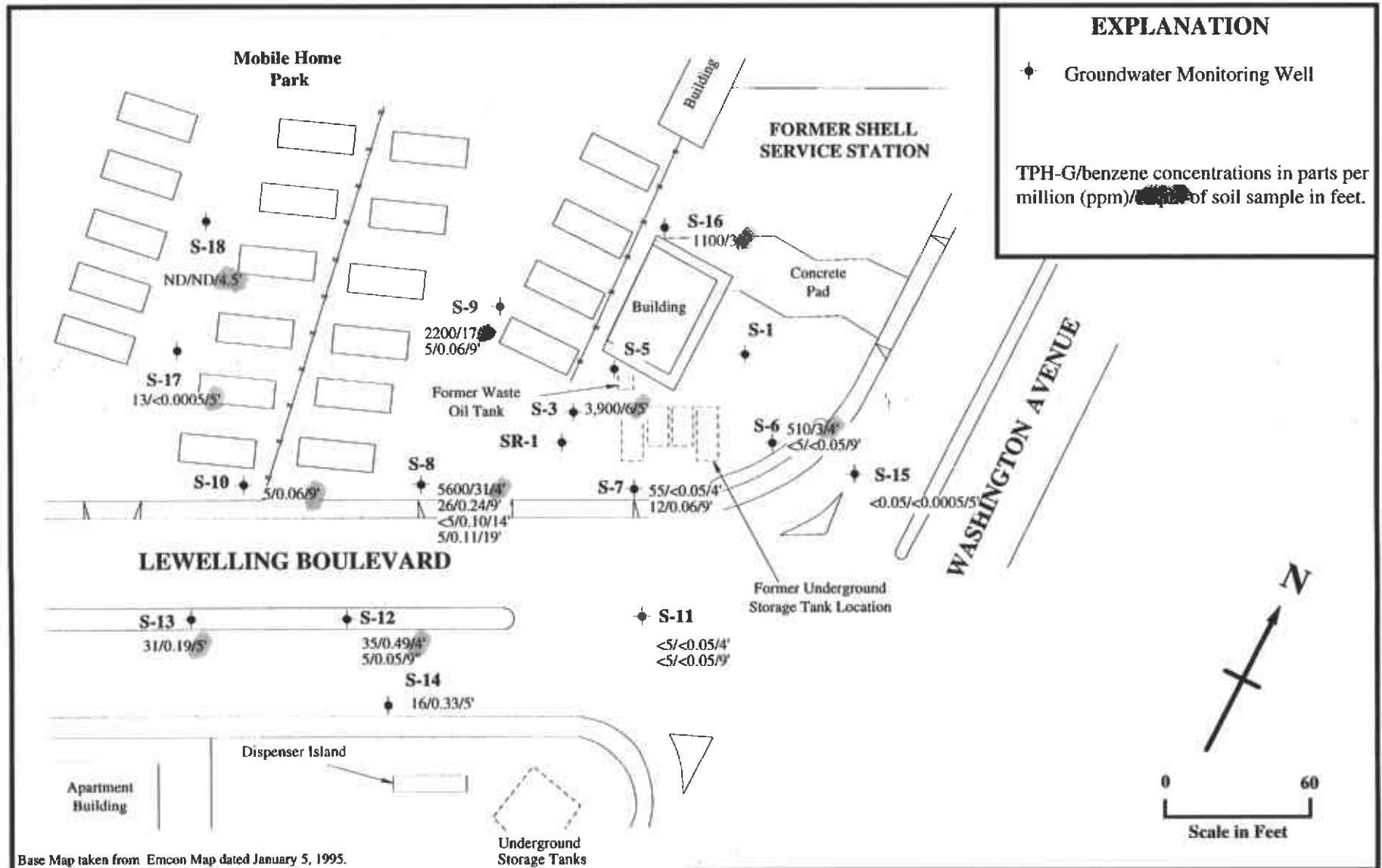
Approved By: *[Signature]*                      Date: *4-17-95*



### EXPLANATION

◆ Groundwater Monitoring Well

TPH-G/benzene concentrations in parts per million (ppm)/depth of soil sample in feet.



Base Map taken from Emcon Map dated January 5, 1995.

**PLATE 3** SOIL QUALITY MAP  
 Shell Oil Company  
 15275 Washington Avenue  
 San Leandro, California

**enviros**<sup>®</sup>  
 95276.01

Drawn By: JLP Date: 4-3-95

Approved By: *[Signature]* Date: 4-17-95



**APPENDIX A**

**Exploratory Boring Logs  
and  
Geologic Cross-Section**



# LOG OF EXPLORATORY BORING

PROJECT NUMBER 738-08.01

BORING NO. S-1

PROJECT NAME Gettler-Ryan, Shell @ Washington & Lewelling , PAGE 1 OF 2

BY JB DATE 6/18/85

San Leandro

SURFACE ELEV.

TORVANE (TSF)	POCKET PENETRO- METER (TSF)	PENETRA- TION (Blows/ FL)	GROUND WATER LEVELS	DEPTH IN FT.	SAMPLES	LITHO- GRAPHIC COLUMN	DESCRIPTION
				0		ASPHALT	
				1		GC FILL	CLAYEY GRAVEL; Fill; dark olive gray (5Y, 3/2); fine to coarse gravel; 30-35% fines; damp; no product odor.
				2		CL	CLAY; dark gray (5Y, 4/1); trace fine sand; slightly silty; moist; no product odor.
			▽	5			
				8.5			@8.5': black (2.5Y, 3/0); no product odor.
	1.25	28		10			@10': grayish brown (2.5Y, 5/2); stiff; wet; slight product odor.
				15			
	3.0	25		20			@20': light olive brown (2.5Y, 5/4); very silty; firm; wet; no product odor.
	1.5	12		20			

REMARKS Drilled using 8-inch continuous flight hollow-stem auger.  
Converted to a 3-inch monitoring well, detailed on Plate C.



# LOG OF EXPLORATORY BORING

PROJECT NUMBER 738-08.01

BORING NO. S-1

PROJECT NAME Gettler-Ryan, Shell @ Washington & Lewelling,


PAGE 2 OF 2

BY JB

DATE 6/18/85

San Leandro

SURFACE ELEV.

TORVANE (TSF)	POCKET PENETRO- METER (TSF)	PENETRA- TION (Blows/ Ft.)	GROUND WATER LEVELS	DEPTH IN FT.	SAMPLES	LITHO- GRAPHIC COLUMN	DESCRIPTION
				20			HOLE TERMINATED AT 21½ FEET.
				25			

REMARKS



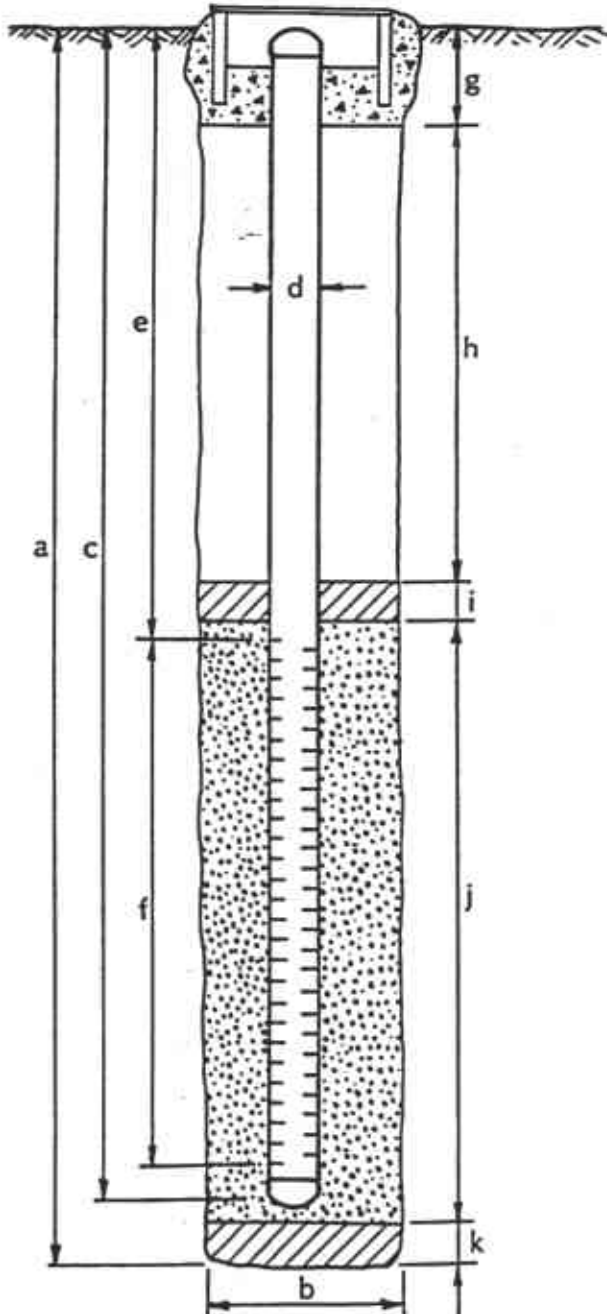
# WELL DETAILS



PROJECT NUMBER 738-08.01  
 PROJECT NAME Gettler-Ryan, Shell @ Washington & Lewelling  
 COUNTY Alameda  
 WELL PERMIT NO. \_\_\_\_\_

BORING / WELL NO. S-1  
 TOP OF CASING ELEV. \_\_\_\_\_  
 GROUND SURFACE ELEV. \_\_\_\_\_  
 DATUM \_\_\_\_\_

G-5 vault box (Std.)



## EXPLORATORY BORING

a. Total depth 21½ ft.  
 b. Diameter 8 in.  
 Drilling method Hollow-Stem Auger

## WELL CONSTRUCTION

c. Casing length 19 ft.  
 Material Schedule 40 PVC  
 d. Diameter 3 in.  
 e. Depth to top perforations 4 ft.  
 f. Perforated length 15 ft.  
 Perforated interval from 4 to 19 ft.  
 Perforation type Machined Slot  
 Perforation size 0.020 inch  
 g. Surface seal 1 ft.  
 Seal material Cement  
 h. Backfill 2 ft.  
 Backfill material Cement  
 i. Seal ½ ft.  
 Seal material Bentonite  
 j. Gravel pack (3½ to 19') 15½ ft.  
 Pack material 6 x 12 Monterey Sand  
 k. Bottom seal 2½ ft.  
 Seal material Bentonite 20-21½  
Compacted Clay 19-20

# LOG OF EXPLORATORY BORING

PROJECT NUMBER 738-08.01

BORING NO. S-2

PROJECT NAME Gettler-Ryan, Shell @ Washington & Lewelling,  
San Leandro

PAGE 1 OF 1

BY JB DATE 6/18/85

SURFACE ELEV.

TORVANE (TSF)	POCKET PENETRO- METER (TSF)	PENETRA- TION (Blows/ Ft)	GROUND WATER LEVELS	DEPTH IN FT.	SAMPLES	LITHO- GRAPHIC COLUMN	DESCRIPTION
				0		GC FILL CL	ASPHALT GRAVEL; Fill; 30% fines
				1		CL	CLAY; dark gray (5Y, 3/1); trace fine sand; slightly silty; moist; slight product odor.
			▽	5		SM	
	2.0	32		6		CL	SILTY SAND; very dark gray (5Y, 3/1); 50% fine sand; 50% silt; loose; wet; strong product odor.
				10			CLAY; black (2.5Y, 2/0); slightly silty ; very stiff; very moist; slight product odor.
	3.0	28		15			@13.5': grayish brown (2.5Y, 5/2); stiff; wet; no product odor.
	1.75	15		20			@18.5': light brownish gray (2.5Y, 6/2); 40% silt; trace fine sand; stiff; wet; no product odor.
HOLE TERMINATED AT 20 FEET.							

REMARKS Drilled using 8-inch continuous flight hollow-stem auger.  
Converted to 3-inch monitoring well, detailed on Plate E.



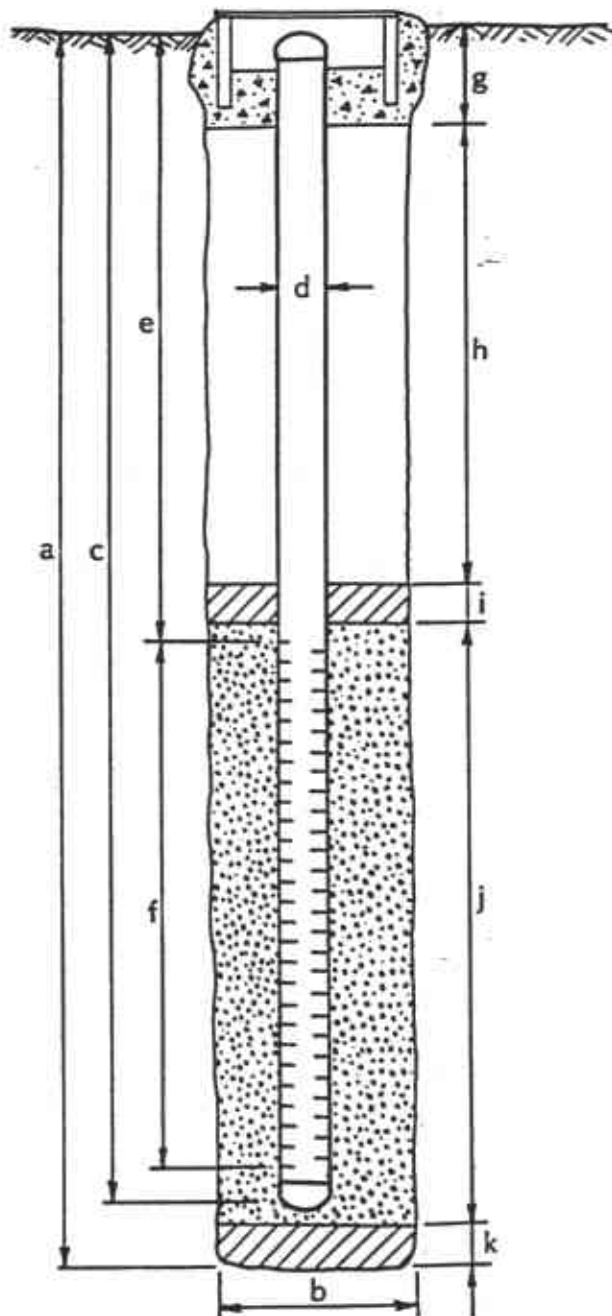
# WELL DETAILS



PROJECT NUMBER 738-08.01  
 PROJECT NAME Gettler-Ryan, Shell @ Washington & Lewelling  
 COUNTY Alameda  
 WELL PERMIT NO. \_\_\_\_\_

BORING / WELL NO. S-2  
 TOP OF CASING ELEV. \_\_\_\_\_  
 GROUND SURFACE ELEV. \_\_\_\_\_  
 DATUM \_\_\_\_\_

G-5 vault box (Std.)



## EXPLORATORY BORING

a. Total depth 20 ft.  
 b. Diameter 8 in.  
 Drilling method Hollow-Stem Auger

## WELL CONSTRUCTION

c. Casing length 18½ ft.  
 Material Schedule 40 PVC  
 d. Diameter 3 in.  
 e. Depth to top perforations 4 ft.  
 f. Perforated length 14½ ft.  
 Perforated interval from 4 to 18½ ft.  
 Perforation type Machined Slot  
 Perforation size 0.020 inch  
 g. Surface seal 1 ft.  
 Seal material Cement  
 h. Backfill 2 ft.  
 Backfill material Cement  
 i. Seal ½ ft.  
 Seal material Bentonite  
 j. Gravel pack (3½ to 18½') 15 ft.  
 Pack material 6 x 12 Monterey Sand  
 k. Bottom seal 1½ ft.  
 Seal material Compacted clay

# LOG OF EXPLORATORY BORING

PROJECT NUMBER 738-08.01

BORING NO. S-3

PROJECT NAME Gettler-Ryan, Shell @ Washington & Lewelling,  
San Leandro

PAGE 1 OF 1

BY JB DATE 6/18/85

SURFACE ELEV.

TORVANE (TSF)	POCKET PENETRO- METER (TSF)	PENETRA- TION (Blows/ Ft.)	GROUND WATER LEVELS	DEPTH IN FT.	SAMPLES	LITHO- GRAPHIC COLUMN	DESCRIPTION
				0		GP	ASPHALT GRAVEL; Fill
				5		CL	CLAY; dark gray (5Y, 3/1); slightly silty; trace fine sand; moist; slight product odor.
		12	▽	5	SM- ML	CL	SILTY SAND TO SANDY SILT; very dark gray (5Y, 3/1); 50% fine sand; 50% silt; loose wet; strong product odor; saturated with product
	1.25	11		10			CLAY; dark gray (5Y, 4/1); silty; firm; very moist; slight product odor.  @ 10': no product odor.
	3.0	24		15			@ 15': stiff; wet; no product odor.
				20			HOLE TERMINATED AT 16½ FEET.

REMARKS Drilled using 8-inch continuous flight hollow-stem auger.  
Converted to 3-inch monitoring well, detailed on Plate G.



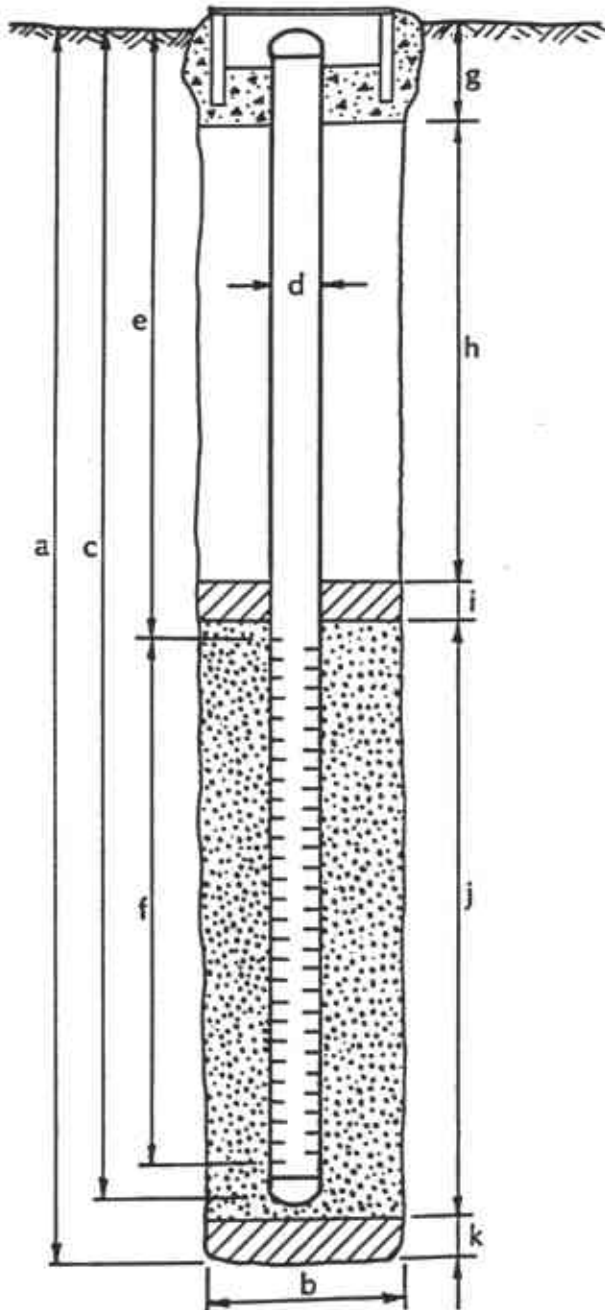
# WELL DETAILS



PROJECT NUMBER 738-08.01  
 PROJECT NAME Gettler-Ryan, Shell @ Washington & Lewelling  
 COUNTY Alameda  
 WELL PERMIT NO. \_\_\_\_\_

BORING / WELL NO. S-3  
 TOP OF CASING ELEV. \_\_\_\_\_  
 GROUND SURFACE ELEV. \_\_\_\_\_  
 DATUM \_\_\_\_\_

G-5 vault box (Std.)



## EXPLORATORY BORING

- a. Total depth 16 1/2 ft.
- b. Diameter 8 in.
- Drilling method Hollow-Stem Auger

## WELL CONSTRUCTION

- c. Casing length 16 1/2 ft.  
Material Schedule 40 PVC
- d. Diameter 3 in.
- e. Depth to top perforations 4 ft.
- f. Perforated length 12 1/2 ft.  
Perforated interval from 4 to 16 1/2 ft.  
Perforation type Machined Slot  
Perforation size 0.020 inch
- g. Surface seal 1 ft.  
Seal material Cement
- h. Backfill 1 ft.  
Backfill material Cement
- i. Seal 1 ft.  
Seal material Bentonite
- j. Gravel pack (3 to 16 1/2') 13 1/2 ft.  
Pack material 6x12 Monterey Sand
- k. Bottom seal - ft.  
Seal material -

# LOG OF EXPLORATORY BORING

PROJECT NUMBER 738-08.01 BORING NO. S-4  
 PROJECT NAME Gettler-Ryan, Shell @ Washington & Lewelling, PAGE 1 OF 1  
 BY JDB DATE 6/18/85 San Leandro SURFACE ELEV.

TORVANE (TSF)	POCKET PENETROMETER (TSF)	PENETRATION (Blows/Ft.)	GROUND WATER LEVELS	DEPTH IN FT.	SAMPLES	LITHO-GRAPHIC COLUMN	DESCRIPTION
				0		GW CL	CONCRETE. GRAVEL FILL.
						CL	CLAY; dark gray (2.5Y, 3/2); slightly silty; moist; slight product odor.
		11	▽	5	SP- ML	CL	SILTY SAND to SANDY SILT; very dark gray (5Y, 3/1); loose; wet; strong product odor; saturated with product.
	2.0	9		10		CL	CLAY; dark gray (5Y, 4/1); very silty; firm; wet; moderate product odor.
				15			@ 15': less silt; stiff; no product odor.
	2.75	24		18			HOLE TERMINATED AT 18 FEET.
				20			

REMARKS Drilled using 8-inch continuous flight hollow-stem auger. converted to 3-inch monitoring well as detailed on Plate I.





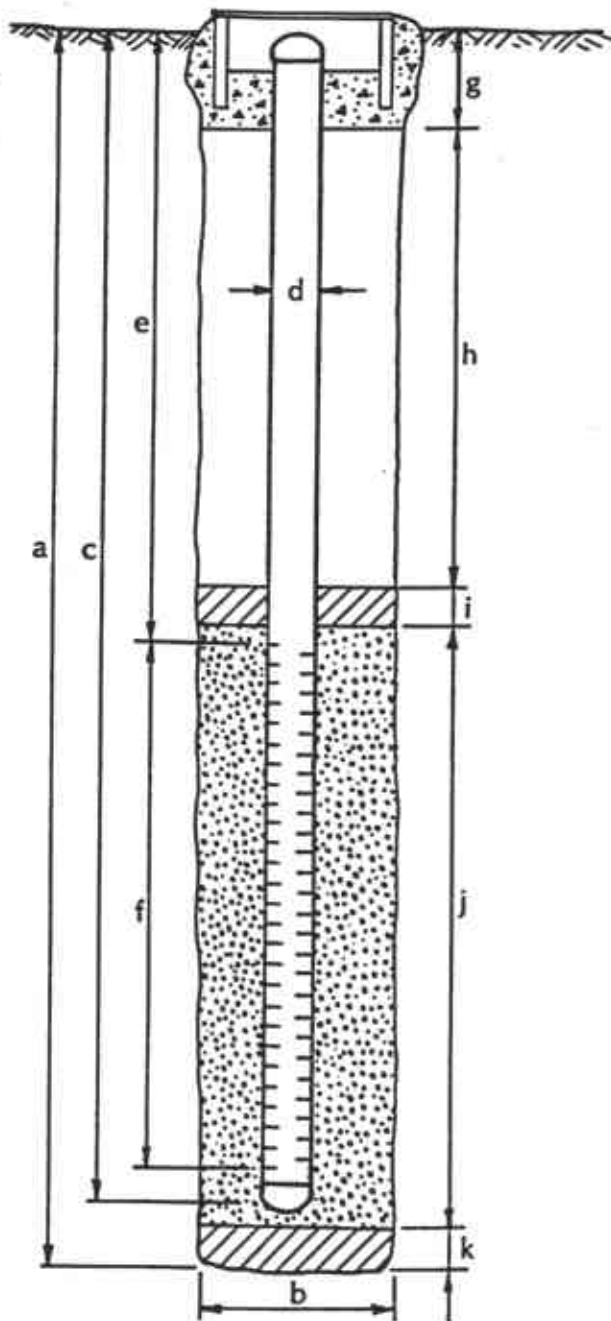
# WELL DETAILS



PROJECT NUMBER 738-08.01  
 PROJECT NAME Gettler-Ryan, Shell @ Washington & Lewelling  
 COUNTY Alameda  
 WELL PERMIT NO. \_\_\_\_\_

BORING / WELL NO. S-4  
 TOP OF CASING ELEV. \_\_\_\_\_  
 GROUND SURFACE ELEV. \_\_\_\_\_  
 DATUM \_\_\_\_\_

G-5 vault box (Std.)



## EXPLORATORY BORING

a. Total depth 18 ft.  
 b. Diameter 8 in.  
 Drilling method Hollow-Stem Auger

## WELL CONSTRUCTION

c. Casing length 18 ft.  
 Material Schedule 40 PVC  
 d. Diameter 3 in.  
 e. Depth to top perforations 4 ft.  
 f. Perforated length 14 ft.  
 Perforated interval from 4 to 18 ft.  
 Perforation type Machined Slot  
 Perforation size 0.020 inch  
 g. Surface seal 1 ft.  
 Seal material Cement  
 h. Backfill 1 ft.  
 Backfill material Cement  
 i. Seal 1 ft.  
 Seal material Bentonite  
 j. Gravel pack (3 to 18') 15 ft.  
 Pack material 6x12 Monterey Sand  
 k. Bottom seal - ft.  
 Seal material -

# LOG OF EXPLORATORY BORING

PROJECT NUMBER 738-08.02

BORING NO. S-A

PROJECT NAME Gettler-Ryan, Shell, Lewelling Bl. & Washington Av. PAGE 1 OF 1

BY EBL DATE 8/15/86

San Leandro

SURFACE ELEV. 22'±

TORVANE (TSF)	POCKET PENETRO- METER (TSF)	PENETRA- TION (Blows/ Fl.)	GROUND WATER LEVELS	DEPTH IN FT.	SAMPLES	LITHO- GRAPHIC COLUMN	DESCRIPTION
	2.0	10	▽	5	1	ML CH	<p>ASPHALT, SAND, AND GRAVEL-FILL.</p> <p>SANDY SILT; very dark gray (10YR, 3/1); 30-40% fine sand; soft; wet; strong product odor.</p> <p>CLAY; black (10YR, 2/1); 10-20% fine sand; stiff; wet; strong product odor.</p> <p>BOTTOM OF BORING AT 8 FEET.</p>
				10			
				15			
				20			
				25			
				30			
				35			
				40			

**REMARKS**

Drilled by 8-inch continuous-flight, hollow-stem auger; samples collected with 2-inch California modified split-spoon sampler. Boring backfilled with cuttings to 1 foot; concrete to surface.

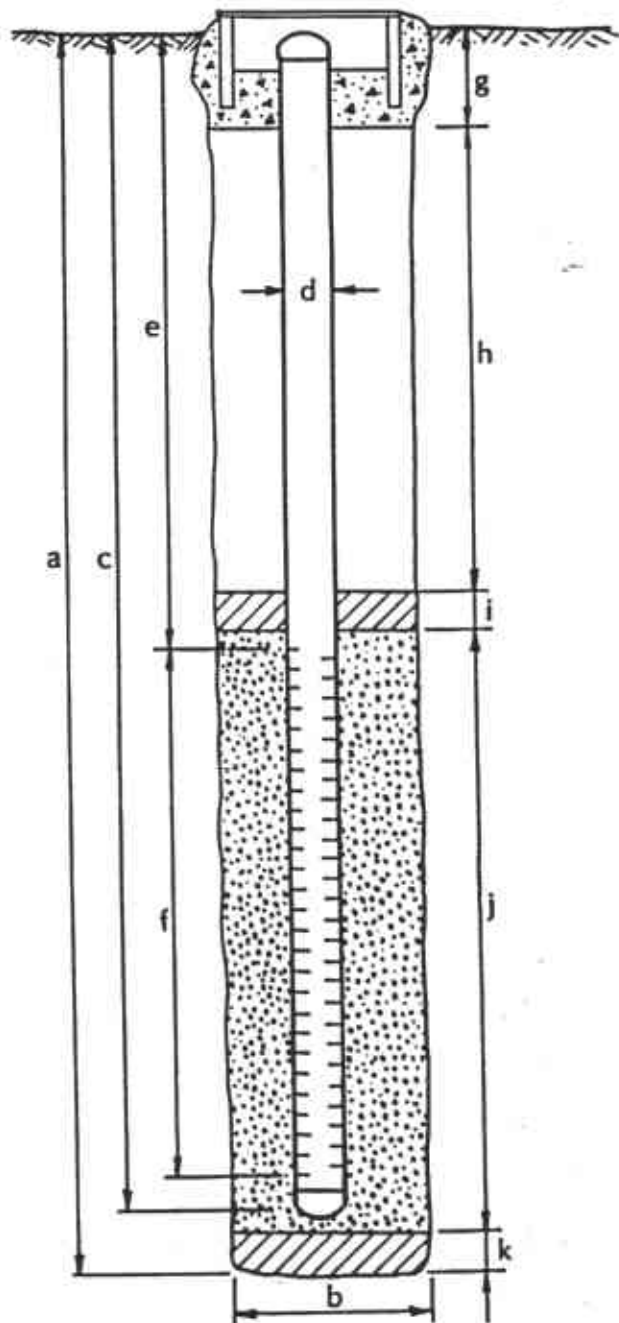
# WELL DETAILS



PROJECT NUMBER 738-08.02  
 PROJECT NAME G-R Shell, San Leandro  
 COUNTY Alameda  
 WELL PERMIT NO. \_\_\_\_\_

BORING / WELL NO. S-B  
 TOP OF CASING ELEV. \_\_\_\_\_  
 GROUND SURFACE ELEV. 22' MSL  
 DATUM USGS

G-5 vault box (Std.)



## EXPLORATORY BORING

- a. Total depth 15.5 ft.
- b. Diameter 8 in.
- Drilling method Hollow-Stem Auger

## WELL CONSTRUCTION

- c. Casing length 15.5 ft.  
Material Schedule 40 PVC
- d. Diameter 3 in.
- e. Depth to top perforations 1 ft.
- f. Perforated length 14.5 ft.  
Perforated interval from 14.5 to 1 ft.  
Perforation type Machined Slot  
Perforation size .020 inch
- g. Surface seal 0.3 ft.  
Seal material Bentonite
- h. Backfill 0 ft.  
Backfill material \_\_\_\_\_
- i. Seal 0.7 ft.  
Seal material Concrete
- j. Gravel pack (13.9 to 1 Ft.) 12.9 ft.  
Pack material Coarse Aquarium Sand
- k. Bottom seal 0 ft.  
Seal material \_\_\_\_\_

Note: Borehole caved to 13.9 feet.

# LOG OF EXPLORATORY BORING

PROJECT NUMBER 738-08.02 BORING NO. S-C  
 PROJECT NAME Gettler-Ryan, Shell, Lewelling Bl. & Washington Av. PAGE 1 OF 1  
 BY EBL DATE 8/15/86 San Leandro SURFACE ELEV. 22' ± MSL

TORVANE (TSF)	POCKET PENETRO- METER (TSF)	PENETRA- TION (Blows/ Ft.)	GROUND WATER LEVELS	DEPTH IN FT.	SAMPLES	LITHO- GRAPHIC COLUMN	DESCRIPTION
			▽	4	1	SW	CONCRETE, SAND, and GRAVEL- FILL.
				5	1	CL	SAND-FILL; dark gray (10YR, 4/1); < 10% fines; fine to coarse sand; loose; damp; strong product odor.
				10	2	SW	CLAY-FILL; very dark gray (2.5Y, N3); 10-20% fine sand; soft; moist; strong product odor.
1.5		13		15	3	CH	SAND-FILL; dark gray (10YR, 4/1); < 10% fines; fine to coarse sand; loose; wet; strong product odor.
3.0		21		15	4		CLAY; very dark grayish brown (2.5Y, 3/2); 15-25% fine sand; stiff; wet; faint product odor.
2.5				15-1/2	5		@ 14': very stiff; faint product odor. @ 15-1/2': stiff; moist; no product odor.
				20			BOTTOM OF BORING AT 17 FEET.
				25			
				30			
				35			
				40			

**REMARKS**

Drilled by 8-inch continous-flight, hollow-stem auger; samples collected with 2-inch California modified split-spoon sampler. Boring backfilled with Bentonite to 12 feet, cuttings to 1 foot, and concrete to surface.

# LOG OF EXPLORATORY BORING

PROJECT NUMBER 738-08.02

BORING NO. S-D

PROJECT NAME Gettler-Ryan, Shell, Lewelling Bl. & Washington Av. PAGE 1 OF 1

BY EBL DATE 8/15/86

San Leandro

SURFACE ELEV. 22' ± MSL

TORVANE (TSF)	POCKET PENETRO- METER (TSF)	PENETRA- TION (Blows/ Fl.)	GROUND WATER LEVELS	DEPTH IN FT.	SAMPLES	LITHO- GRAPHIC COLUMN	DESCRIPTION
			▽	2		SP	CONCRETE, SAND, and GRAVEL-FILL.
				5	1		SAND; very dark gray (10YR, 3/1); < 10% fines; fine sand; loose; moist; strong product odor.
				7	2		@ 7': moderate product odor.
				10	3		@ 11': wet; strong product odor; product sheen on sampler.
				12		CL	CLAY; very dark grayish brown; (2.5Y, 3/2); 10-20% fine sand; very stiff; moist; no product odor.
	3.0	26		15	4		BOTTOM OF BORING AT 15-1/2 FEET.
				20			
				25			
				30			
				35			
				40			

**REMARKS**

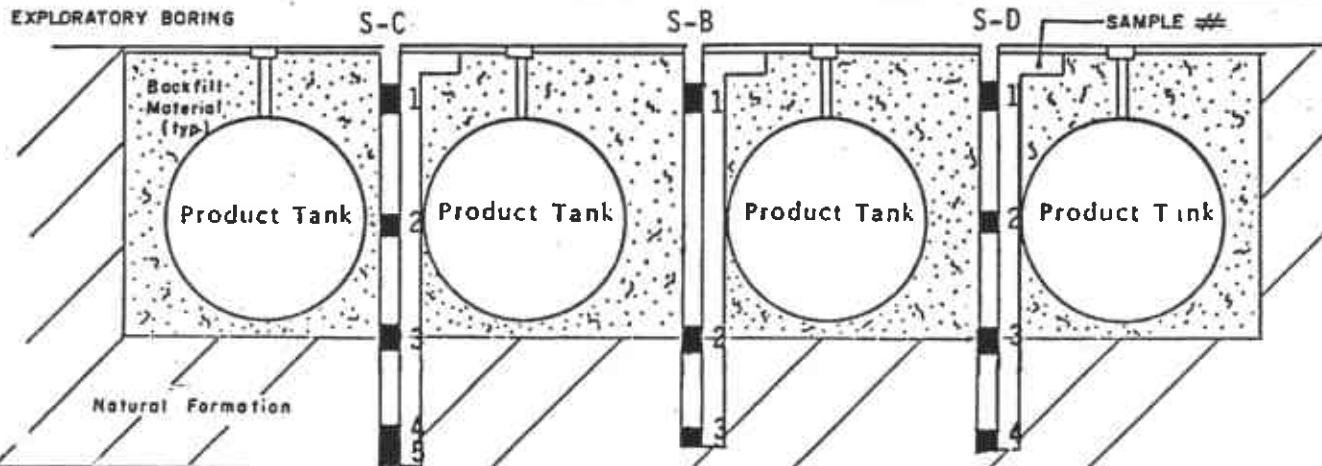
Drilled by continous-flight, hollow-stem auger; samples collected with 2-inch California modified split-spoon sampler. Boring backfilled with Bentonite to 12 feet, cuttings to 1 foot, and concrete to surface.



GETTLER-RYAN, INC.

GENERALIZED PROFILE OF SUBSURFACE TANK COMPLEX  
AND GASOLINE CONCENTRATIONS WITHIN BACKFILL MATERIAL

PROJECT NUMBER 738-08.02 MAPVIEW DIMENSIONS 27' x 42'  
 PROJECT NAME G-R Shell, San Leandro APPROXIMATE DEPTH 12 feet  
 NUMBER OF TANKS IN COMPLEX 4



SAMPLE #	BORING	DEPTH INTERVAL	GASOLINE CONCENTRATION (parts per million)
1	S-B	3-1/2 to 5	1,700
2	S-B	11 to 12-1/2	1,500
3	S-B	14 to 15-1/2	nd*
1	S-C	3-1/2 to 5	310
2	S-C	7-1/2 to 9	nd <sup>1</sup>
3	S-C	11-1/2 to 13	nd*
4	S-C	14 to 15-1/2	300
5	S-C	15-1/2 to 17	nd*
1	S-D	3-1/2 to 5	nd <sup>2</sup>
2	S-D	7 to 8-1/2	nd*
3	S-D	11 to 12-1/2	nd*
4	S-D	14 to 15-1/2	nd*

nd = no detection.

\* Detection limit = 5 parts per million.

1 Detection limit = 200 ppm due to matrix interferences.

2 Detection limit = 100 ppm due to matrix interferences.

# LOG OF EXPLORATORY BORING

PROJECT NUMBER 738-08.03

BORING NO. S-5

PROJECT NAME Gettler-Ryan, Shell, Washington & Lewelling

PAGE 1 OF 2

BY JDB DATE 12/24/86

SURFACE ELEV. 21.71'

TORVANE (TSF)	POCKET PENETRO- METER (TSF)	PENETRA- TION (Blows/ Fl.)	GROUND WATER LEVELS	DEPTH IN FT.	SAMPLES	LITHO- GRAPHIC COLUMN	DESCRIPTION
			▽	0		GP	ASPHALT GRAVEL-FILL; coarse baserock.
				5		CL	CLAY; dark gray (5Y, 4/1); 98-100% low- to moderate-plasticity fines; <2% fine sand; stiff; damp; no gasoline odor. @4': slight gasoline odor.
	1.25	9		6	1	SC	CLAYEY SAND; dark gray (5Y, 4/1); 20-40% low-plasticity fines; 60-80% fine sand; loose; moist; slight to mod- erate gasoline odor.
				10	2	ML CH- CL	SANDY SILT; dark gray (5Y, 4/1); 70-90% non-plastic fines; 10-30% fine sand; stiff; moderate gasoline odor.
	1.5	17		15	3	CH	CLAY; black (5Y, 2.5/1); 100% moderate- to high-plasticity fines; occasion- ally calcareous; stiff to very stiff; wet in voids; slight gasoline odor to 10 feet.
	2.25	22		19			@14': gray (5Y, 5/1); 100% high-plas- ticity fines; very stiff; very moist; no gasoline odor. @19': abundant caliche disseminated; no gasoline odor.
	2.0	29		20	4		

**REMARKS**

Drilled with 8- and 12-inch continuous-flight, hollow-stem auger drilling equipment. Converted to a 4-inch monitoring well as detailed on Plate B.

# LOG OF EXPLORATORY BORING

PROJECT NUMBER 738-08.03


BORING NO. S-5

PROJECT NAME Gettler-Ryan, Shell, Washington & Lewelling

PAGE 2 OF 2

BY JDB DATE 12/24/86

SURFACE ELEV. 21.71'

TORVANE (TSF)	POCKET PENETRO- METER (TSF)	PENETRA- TION (Blows/ Ft.)	GROUND WATER LEVELS	DEPTH IN FT.	SAMPLES	LITHO- GRAPHIC COLUMN	DESCRIPTION
				20			<p>BOTTOM OF BORING AT 20.5 FEET</p>
				25			
				30			
				35			
				40			

REMARKS

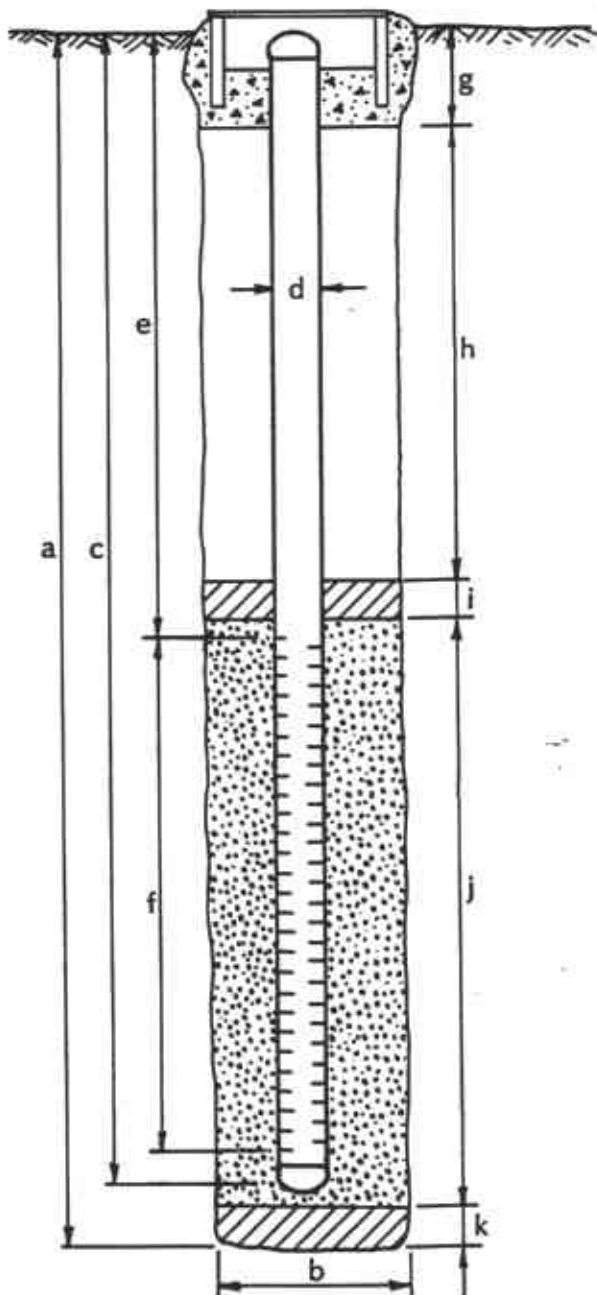


# WELL DETAILS



PROJECT NUMBER 738-08.03 BORING / WELL NO. S-5  
 PROJECT NAME Shell, Washington & Lewelling TOP OF CASING ELEV. 21.24'  
 COUNTY Alameda San Leandro GROUND SURFACE ELEV. 21.71'  
 WELL PERMIT NO. \_\_\_\_\_ DATUM Project

G-5 vault box (Std.)



## EXPLORATORY BORING

- a. Total depth 20 1/2 ft.  
 b. Diameter 12 in.  
 Drilling method Hollow-stem auger

## WELL CONSTRUCTION

- c. Casing length 18 1/2 ft.  
 Material schedule 40 PVC  
 d. Diameter 4 in.  
 e. Depth to top perforations 3 1/2 ft.  
 f. Perforated length 15 ft.  
 Perforated interval from 18 1/2 to 3 1/2 ft.  
 Perforation type machined slot  
 Perforation size 0.020 inch  
 g. Surface seal (1 - 0') 1 ft.  
 Seal material concrete  
 h. Backfill (1 1/2 - 1') 1 1/2 ft.  
 Backfill material concrete  
 i. Seal (2 1/2 - 1 1/2') 1 ft.  
 Seal material bentonite  
 j. Gravel pack (18 1/2 - 2 1/2') 16 ft.  
 Pack material 6x12 Monterey Sand  
 k. Bottom seal (20 1/2 - 18 1/2') 2 ft.  
 Seal material compacted clay

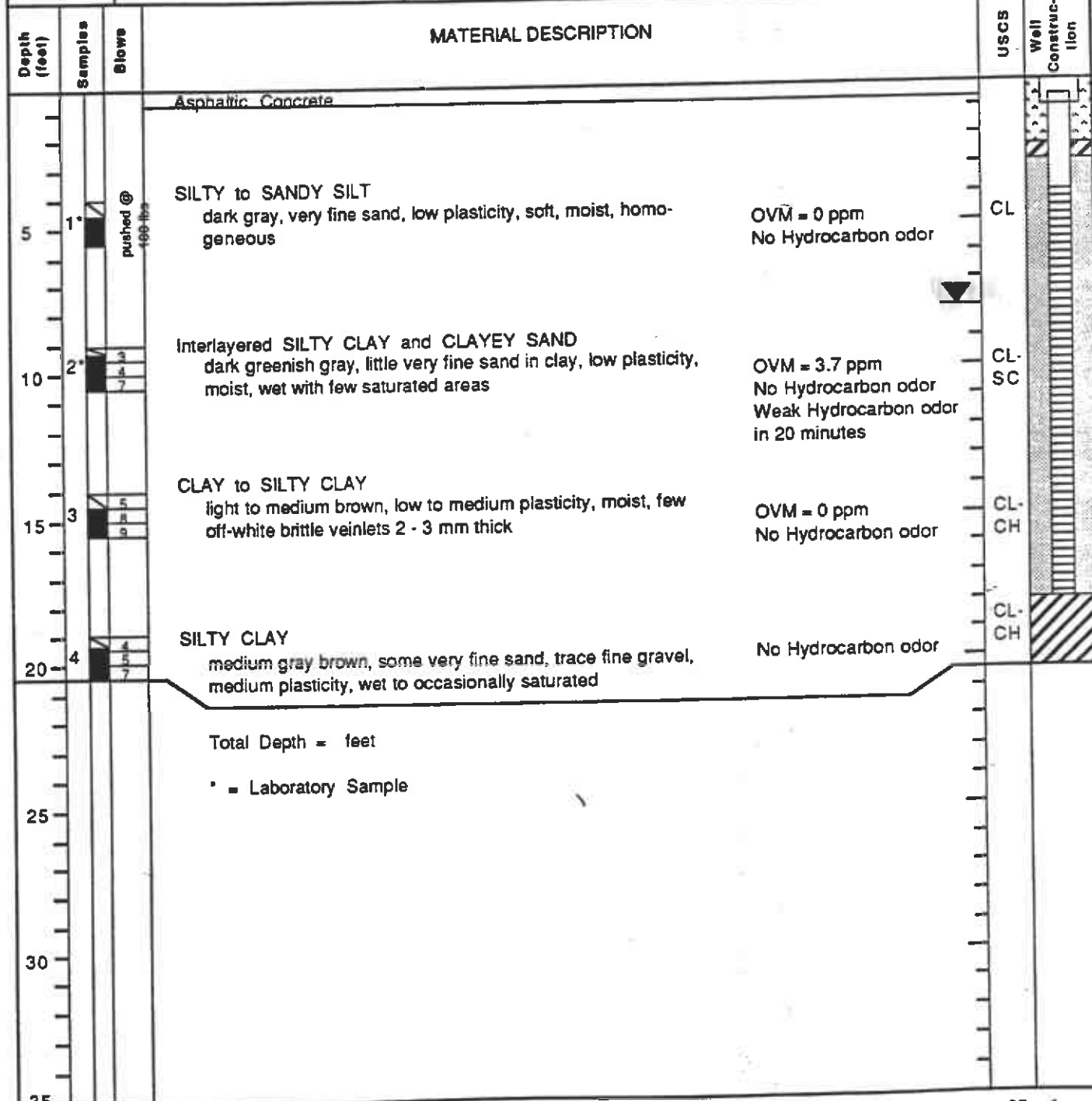
MONITORING WELL LOCATION 15275 Washington Ave., San Leandro, CA		ELEVATION AND DATUM	
DRILLING AGENCY Bay Land Drilling	DRILLER Tom/Mack	DATE STARTED 11/4 / 88 DATE FINISHED	
DRILLING EQUIPMENT CME - 55		COMPLETION DEPTH 24.5'	SAMPLER Modified California
DRILLING METHOD 8" Hollow stem auger	DRILL BIT CME Carbide	NO. OF SAMPLES	DIST. 5 UNDIST. 5
SIZE AND TYPE OF CASING Sch 40 3" PVC	FROM 24.0 TO 0.5 FT.	WATER LEVEL	FIRST 6' COMPL. 24 HRS.
TYPE OF PERFORATION 0.02"	FROM 23.5 TO 3.5 FT.	LOGGED BY: G. Hayman	
SIZE AND TYPE OF PACK 2 1/2 Monterey Sand	FROM 24.0 TO 3.0 FT.	CHECKED BY: M. Bonkowski	
TYPE OF SEAL	NO. 1 1/2" Bentonite Pellets	FROM 3 TO 2.5 FT.	
	NO. 2 Cement grout	FROM 2.5 TO surface FT.	

Depth (feet)	Samples	Blows	MATERIAL DESCRIPTION	USCS	Well Construction
			Asphaltic Concrete		
5	1	pushed @ 200 lbs	CLAYEY SAND to SANDY CLAY grading down to SILTY CLAY TO CLAYEY SILT greenish gray at top with gray mottling in middle and bottom of sample, very fine sand, low plasticity, moist, generally homogeneous	CL	
10	2	4 5 7	SILTY CLAY dark brownish gray, some very fine sand, low plasticity, firm, moist to wet, few beds of clay, sand to 1/4" thick	CL	
15	3	5 8 11	CLAY to SILTY CLAY medium grayish brown, some silt grading to silty clay, medium plasticity, wet homogeneous Driller indicates drilling through a series of 2 - 4" gravel layers from 16 - 19'	CL	
20	4	3 4 5	CLAY to SANDY CLAY medium grayish brown, little to some very fine sand occasionally grading to sandy clay, low to medium plasticity, firm, saturated	CL	
			CLAYEY SAND to SANDY CLAY medium yellow brown, very fine sand, saturated	CL	
	5	4 5 7	SILTY CLAY to CLAYEY SILT medium yellow brown, up to some very fine sand, low to medium plasticity, saturated	CL	
25			Total Depth = 24.5 feet * = Laboratory Sample		

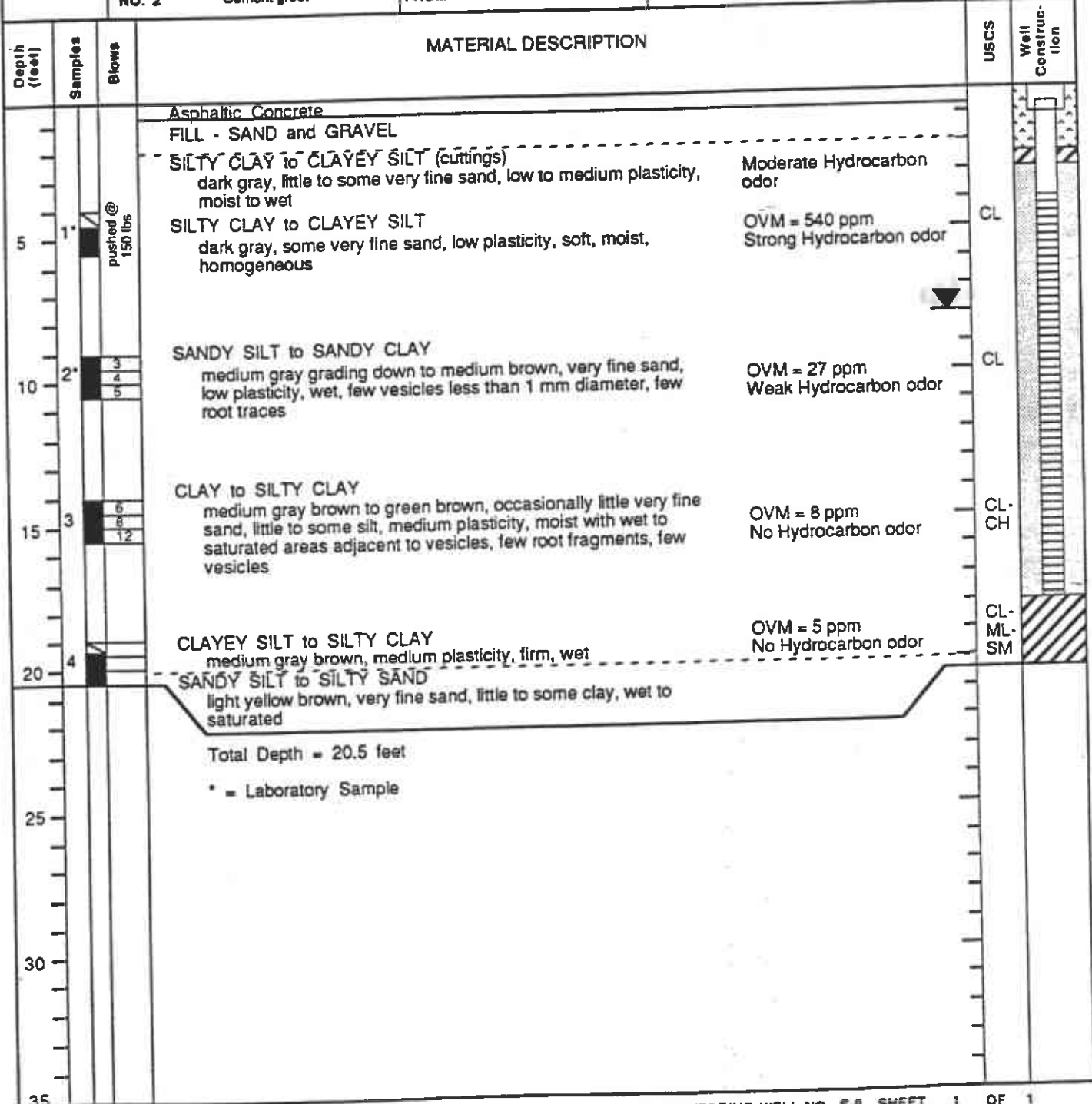
MONITORING WELL LOCATION 15275 Washington Ave., San Leandro, CA			ELEVATION AND DATUM				
DRILLING AGENCY Bay Land Drilling		DRILLER Tom/Mack		DATE STARTED 11/4/88			
DRILLING EQUIPMENT CME - 55			COMPLETION DEPTH 24.5'		SAMPLER Modified California		
DRILLING METHOD 8" Hollow stem auger		DRILL BIT CME Carbide		NO. OF SAMPLES 5	UNDIST. 5		
SIZE AND TYPE OF CASING Sch 40 3" PVC		FROM 24.5 TO 0.5 FT.		WATER LEVEL FIRST 8'	COMPL. 7.8' 24 HRS.		
TYPE OF PERFORATION 0.02"		FROM 24.0 TO 4.0 FT.		LOGGED BY:  G. Heyman			
SIZE AND TYPE OF PACK 2/12 Monterey Sand		FROM 24.5 TO 3.5 FT.				CHECKED BY:  M. Bonkowski	
TYPE OF SEAL	NO. 1 1/2" Bentonite Pellets	FROM 3.5 TO 3.0 FT.	NO. 2 Cement grout				

Depth (feet)	Samples	Blows	MATERIAL DESCRIPTION	USCS	Well Construction
0 - 2.5			Asphaltic Concrete and base rock		
2.5 - 5.0	1	pushed @ 175 lbs	SILTY to SANDY CLAY greenish gray, silt and very fine grained sand, content varies vertically, low plasticity, firm, moist, numerous vesicles less than 1 mm diameter	CL	
5.0 - 10.0	2	4 7 9	SILTY CLAY to CLAYEY SILT dark brown, little to some very fine sand, low plasticity, moist to wet, few vesicles	CL-ML	
10.0 - 15.0	3	5 10 11	SILTY CLAY greenish brown, little to some very fine sand, medium plasticity, wet with saturated areas, gravel layers 1 - 2" thick from 15 - 18' (driller)	CL	
15.0 - 20.0	4*	3 4 4	SILTY CLAY with Interbedded CLAYEY SAND to SANDY CLAY Clay is grayish brown, medium plasticity, wet with saturated areas, sand is light yellow brown, very fine grained, loose, wet to saturated, up to 3" thick	CL-SC	
20.0 - 25.0	5	4 7 8	SANDY CLAY to CLAYEY SAND layers are up to 5" thick, as above	CL	
25.0 - 35.0			Total Depth = 24.5 feet  * = Laboratory Sample		

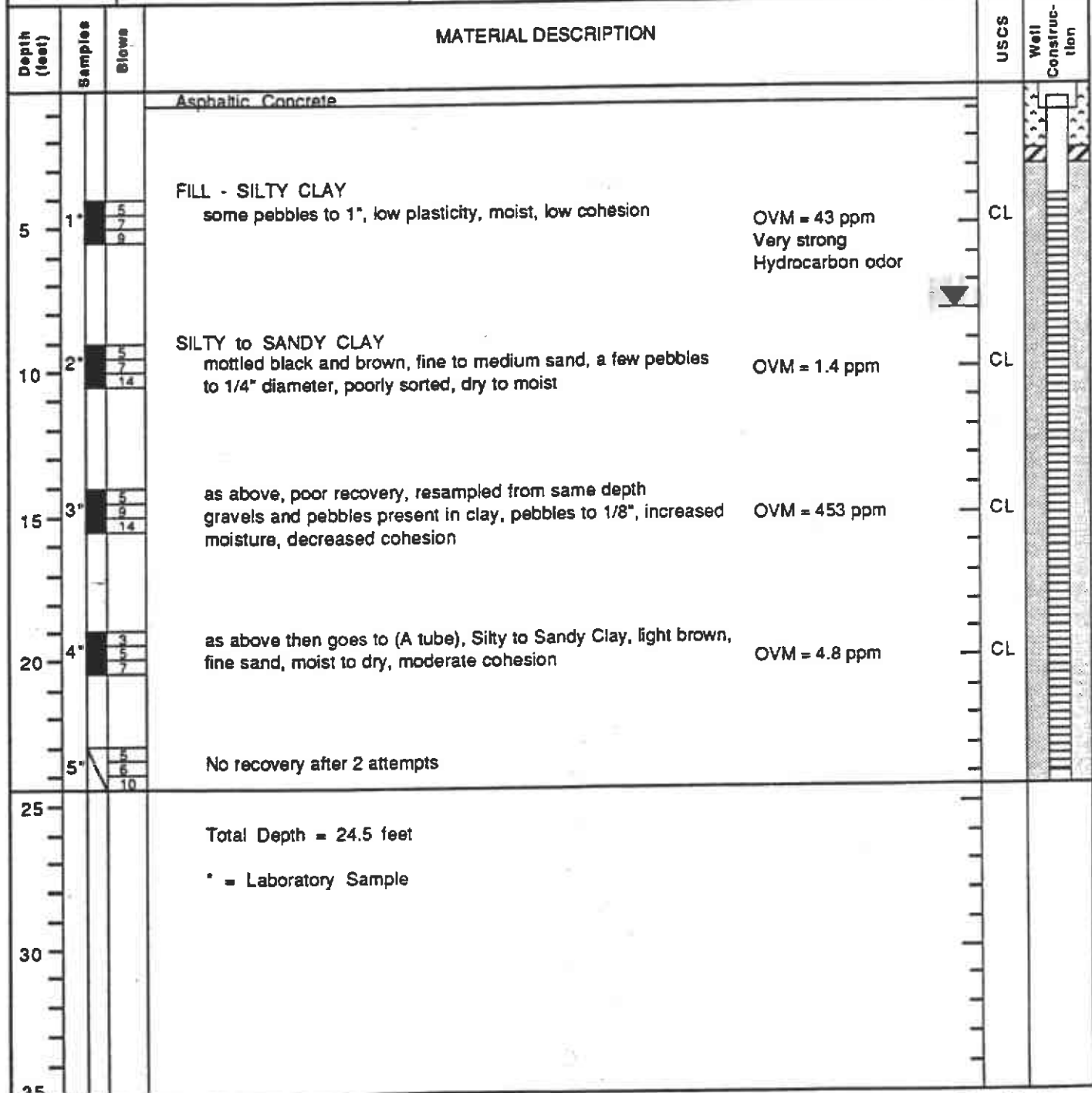
MONITORING WELL LOCATION 15275 Washington Ave., San Leandro, CA			ELEVATION AND DATUM		
DRILLING AGENCY Bay Land Drilling		DRILLER Tom/Mack	DATE STARTED 11/4/88		DATE FINISHED
DRILLING EQUIPMENT CME - 55			COMPLETION DEPTH 18'	SAMPLER Modified California	
DRILLING METHOD 8" Hollow stem auger		DRILL BIT CME Carbide	NO. OF SAMPLES 4	DIST. 4	
SIZE AND TYPE OF CASING Sch 40 3" PVC		FROM 18.0 TO 0.5 FT.	WATER LEVEL FIRST 8' +/-	UNDIST. ---	
TYPE OF PERFORATION 0.02"		FROM 17.5 TO 4.0 FT.	LOGGED BY: G. Heyman		CHECKED BY: M. Bonkowski
SIZE AND TYPE OF PACK 2/12 Monterey Sand		FROM 18 TO 3.0 FT.			
TYPE OF SEAL	NO. 1 1/2" Bentonite Pellets	FROM 3 TO 2.5 FT.			
	NO. 2 Cement grout	FROM 2.5 TO surface FT.			



MONITORING WELL LOCATION 15275 Washington Ave., San Leandro, CA			ELEVATION AND DATUM		
DRILLING AGENCY Bay Land Drilling		DRILLER Tom/Mack		DATE STARTED 11/4/88 DATE FINISHED	
DRILLING EQUIPMENT CME - 55				COMPLETION DEPTH 18'	SAMPLER Modified California
DRILLING METHOD 8" Hollow stem auger		DRILL BIT CME Carbide		NO. OF SAMPLES 4	DIST. 4
SIZE AND TYPE OF CASING Sch 40 3" PVC		FROM 18.0 TO 0.5 FT.		WATER LEVEL	FIRST 8' +/-
TYPE OF PERFORATION 0.02"		FROM 17.5 TO 4.0 FT.		LOGGED BY: G. Heyman	
SIZE AND TYPE OF PACK 2/12 Monterey Sand		FROM 18 TO 3.0 FT.		CHECKED BY: M. Bonkowski	
TYPE OF SEAL	NO. 1 1/2" Bentonite Pellets	FROM 3 TO 2.5 FT.			
	NO. 2 Cement grout	FROM 2.5 TO surface FT.			



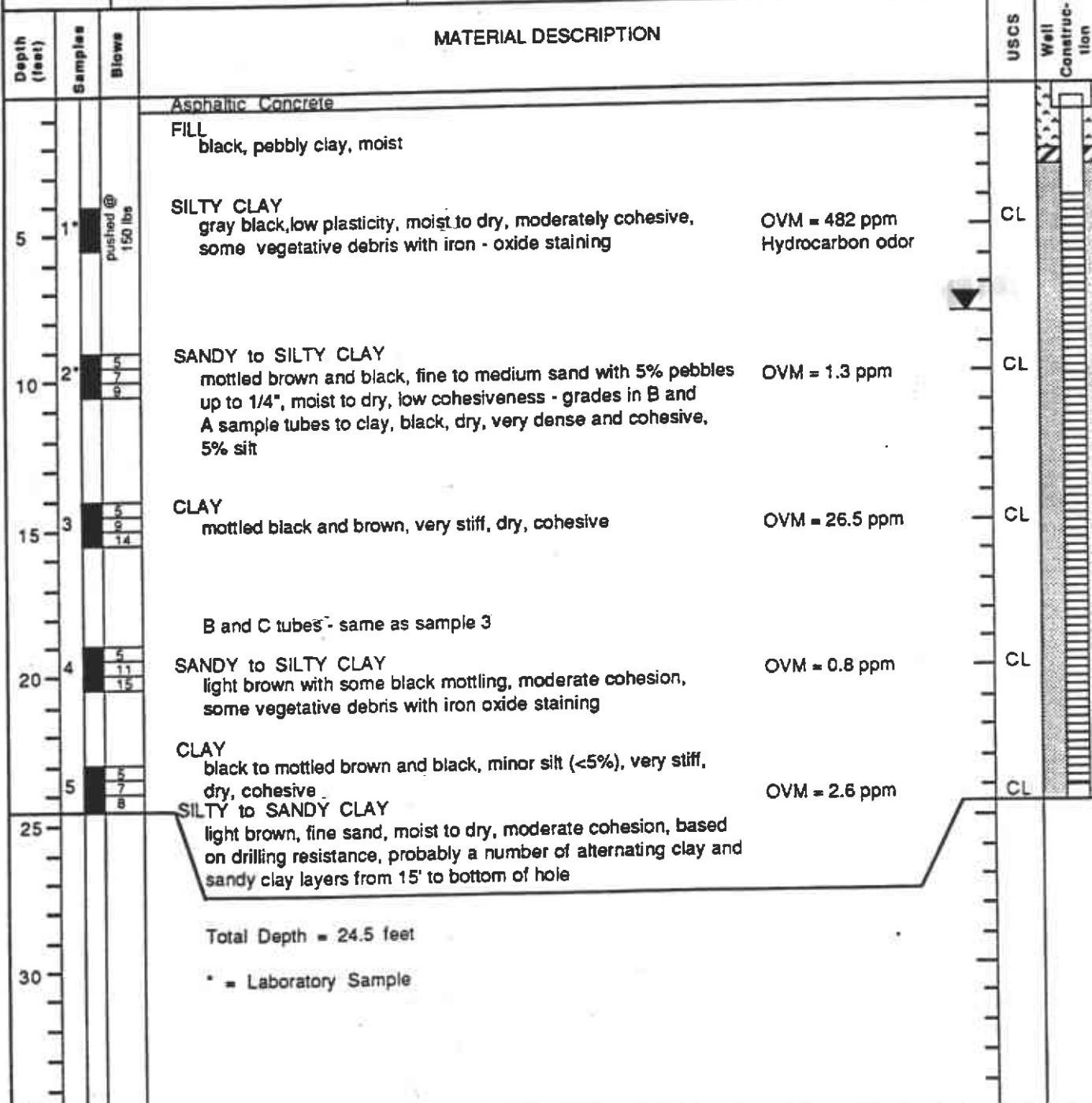
<b>MONITORING WELL LOCATION</b> 15275 Washington Ave., San Leandro, CA (S-8)			<b>ELEVATION AND DATUM</b>		
<b>DRILLING AGENCY</b> Bay Land Drilling		<b>DRILLER</b> Tom/Mack	<b>DATE STARTED</b> 11/3/88		<b>DATE FINISHED</b>
<b>DRILLING EQUIPMENT</b> CME - 55			<b>COMPLETION DEPTH</b> 24.5'	<b>SAMPLER</b> Modified California	
<b>DRILLING METHOD</b> 8" Hollow stem auger		<b>DRILL BIT</b> CME Carbide	<b>NO. OF SAMPLES</b>	<b>DIST.</b> 5	<b>UNDIST.</b> 5
<b>SIZE AND TYPE OF CASING</b> Sch 40 3" PVC		<b>FROM</b> 24.0 <b>TO</b> 0.5 FT.	<b>WATER LEVEL</b>	<b>FIRST</b> -8'	<b>COMPL.</b> 24 HRS.
<b>TYPE OF PERFORATION</b> 0.02"		<b>FROM</b> 24.0 <b>TO</b> 4.0 FT.	<b>LOGGED BY:</b>  R. Siegel		<b>CHECKED BY:</b>  M. Bonkowski
<b>SIZE AND TYPE OF PACK</b> 2/12 Monterey Sand		<b>FROM</b> 24.5 <b>TO</b> 3.0 FT.			
<b>TYPE OF SEAL</b>	<b>NO. 1</b> 1/2" Bentonite Pellets	<b>FROM</b> 3 <b>TO</b> 2.5 FT.			
	<b>NO. 2</b> Cement grout	<b>FROM</b> 2.5 <b>TO</b> 0.5 FT.			



MONITORING WELL LOCATION		15275 Washington Ave., San Leandro, CA (S-7)		ELEVATION AND DATUM	
DRILLING AGENCY		Bay Land Drilling		DRILLER	
				TomMack	
DRILLING EQUIPMENT		CME - 55		DATE STARTED	
				11/3/88	
DRILLING METHOD		8" Hollow stem auger		COMPLETION DEPTH	
				24.5'	
DRILL BIT		CME Carbide		SAMPLER	
				Modified California	
SIZE AND TYPE OF CASING		Sch 40 3" PVC		NO. OF SAMPLES	
				DIST. 5	
TYPE OF PERFORATION		0.02"		UNDIST. 5	
SIZE AND TYPE OF PACK		2/12 Monterey Sand		WATER LEVEL	
				FIRST -8'	
TYPE OF SEAL		NO. 1 Bentonite		COMPL. 24 HRS.	
		NO. 2 Cement grout		LOGGED BY:	
				R. Siegel	
				CHECKED BY:	
				M. Bonkowski	

Depth (feet)	Samples	Blows	MATERIAL DESCRIPTION	USCS	Well Construction
			Asphaltic Concrete		
5	1	pushed @ 200 lbs	FILL - CLAY silty sandy clay with large pebbles to 2" diameter, plastic, moist to wet, cohesive, Note: pipe encountered at -5', moved auger over slightly	OVM = 9.0 ppm	CL
10	2	5 8 10	CLAY black mottled with green, low plasticity, stiff, dry, moderate cohesion	OVM = 32 ppm	CL
15	3	6 9 12	SILTY CLAY mottled black and brown, gravelly clay present in top, stiff, dry, moderate cohesion	OVM = 2.2 ppm	CL
20	4	7 7 9	same as Silty Clay above	OVM = 1.8 ppm	CL
25	5	5 5 4	same as Silty Clay above but some fine sands present	OVM = 0.6 ppm	CL
25			Total Depth = 24.5 feet		
			* = Laboratory Sample		

MONITORING WELL LOCATION 15275 Washington Ave., San Leandro, CA (S-6)			ELEVATION AND DATUM		
DRILLING AGENCY Bay Land Drilling		DRILLER TomMack		DATE STARTED 11/3/88	
DRILLING EQUIPMENT CME - 55			COMPLETION DEPTH 24.5'		SAMPLER Modified California
DRILLING METHOD 8" Hollow stem auger		DRILL BIT CME Carbide		NO. OF SAMPLES: DIST. 5 UNDIST. 5	
SIZE AND TYPE OF CASING Sch 40 3" PVC		FROM 24.0 TO 0.5 FT.		WATER LEVEL: FIRST 8' COMPL. 24 HRS.	
TYPE OF PERFORATION 0.02"		FROM 24.0 TO 4.0 FT.		LOGGED BY: R. Siegel CHECKED BY: M. Bonkowski	
SIZE AND TYPE OF PACK 2/12 Monterey Sand		FROM 24.5 TO 3.0 FT.			
TYPE OF SEAL		FROM 3 TO 2.5 FT.			
NO. 1 1/2" Bentonite Pellets		FROM 2.5 TO 0.5 FT.			
NO. 2 Cement grout					





Field location of boring:	Project No.: 7615	Date: 4/26/89	Boring No:
	Client: Shell		S-13
	Location: 15275 Washington Ave/Lewelling		Sheet 1
	City: San Leandro		of 2
	Logged by: DAF	Driller: Bayland	
Casing installation data:			

Drilling method: Hollow Stem Auger  
 Hole diameter: 8 inch

Top of Box Elevation:	Datum:
Water Level 8.4'	7.3'
Time 11:50am	
Date 4/26	5/10

PID (ppm)	Blows/L. or Pressure (psf)	Type of Sample	Sample Number	Depth (ft.)	Sample	Well Detail	Soil Group Symbol (USCS)	Description
				1				PAVEMENT SECTION - 2 feet.
				2				
				3				CLAY (CL)- dark gray (10YR 4/1); soft; damp; low plasticity; trace gravel; no chemical odor.
350	150	S&H push	S-13-5'	4				color change to dark olive gray (5Y 3/2); no chemical odor.
				5				
				6				
				7				
				8				
50	2	S&H	S-13-10'	9				
	3			10				SILTY SAND (SM)- light olive brown (2.5Y 5/4); loose; damp; 20-30% silt; mottled brown; no chemical odor.
	6			11				
				12				CLAY (CL)- dark olive gray (5Y 3/2), medium stiff; damp; low plasticity; trace gravel; rootholes; no chemical odor.
				13				
40	3	S&H	S-13-15'	14				color change to very dark gray (5Y 3/1) mottled; organics present; no chemical odor.
	5			15				
	7			16				
				17				becoming saturated at 17.5 feet.
				18				
				19				
0	2	S&H	S-13-20'	20				SANDY SILT (ML)- light yellowish brown (2.5Y 6/4); medium stiff; saturated;
	3							

Remarks:

Field location of boring:	Project No.: 7615	Date: 4/26/89	Boring No.:
	Client: Shell		S-13
	Location: 15275 Washington Ave/Lewelling		Sheet 2
	City: San Leandro		of 2
	Logged by: DAF	Driller: Bayland	
Casing installation data:			

Drilling method: **Hollow Stem Auger**

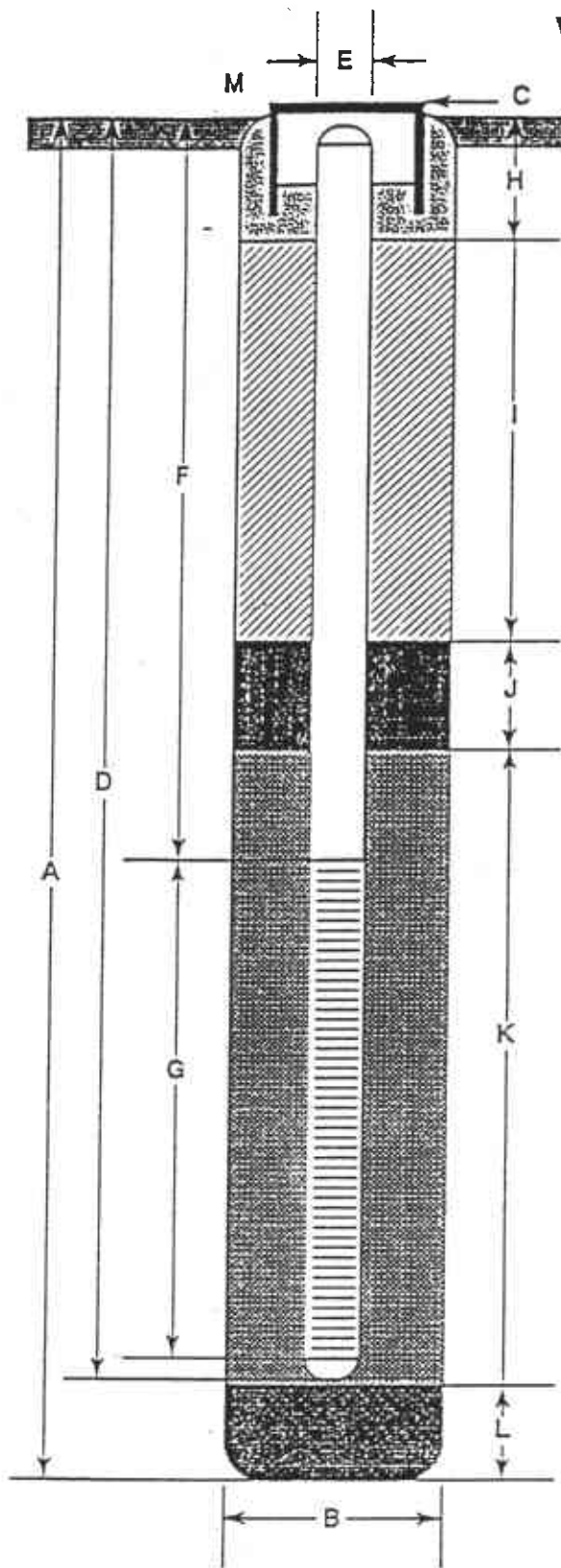
Hole diameter: **8 inch**

Top of Box Elevation: \_\_\_\_\_ Datum: \_\_\_\_\_

PID (ppm)	Blows ft. or Pressure (psf)	Type of Sample	Sample Number	Depth (ft.)	Sample	Well Detail	Soil Group Symbol (USCS)	Water Level				
								Time				
								Date				
Description												
	4			21								15% very fine to fine sand; 10% clay; trace organics; rootholes; mottled brown & black; no chemical odor.
				22								
				23								
25	2	S&H	S-13-	24								SILTY CLAY (CL-ML)- light olive brown (2.5Y 5/4); medium stiff; moist; trace organics; mottled brown & black; no chemical odor.
	3		25	25								
	4											
Bottom of boring 24.0 feet, Sampled to 25.5 feet 4/26/89												

Remarks:

# WELL CONSTRUCTION DETAIL



- A Total Depth of Boring 24 ft.
- B Diameter of Boring 8 in.  
Drilling Method HOLLOW STEM AUGER
- C Top of Box Elevation 20.57 ft.  
 Referenced to Mean Sea Level  
 Referenced to Project Datum
- D Casing Length 23.5 ft.  
Material SCH 40 PVC
- E Casing Diameter 3 in.
- F Depth to Top Perforations 4 ft.
- G Perforated Length 20 ft.  
Perforated Interval from 4 to 24 ft.  
Perforation Type FACTORY SLOTTED  
Perforation Size 0.020
- H Surface Seal 2.5 ft.  
Seal Material CONCRETE
- I Backfill \_\_\_\_\_ ft.  
Backfill Material \_\_\_\_\_
- J Seal 0.5 ft.  
Seal Material BENTONITE
- K Gravel Pack 21 ft.  
Pack Material LONESTAR 2/12 & #3
- L Bottom Seal \_\_\_\_\_ ft.  
Seal Material \_\_\_\_\_
- M CHRISTY BOX



GeoStrategies Inc.

Well Construction Detail  
Former Shell Service Station  
15275 Washington Ave.  
San Leandro

WELL NO

S-13

JOB NUMBER  
7615

REVIEWED BY RG/CEG  
Camp rev 1262

DATE  
5/89

REVISED DATE

REVISED DATE

Field location of boring:

Project No.: 7615 Date: 4/26/89 Boring No:  
 Client: Shell S-14  
 Location: 15275 Washington Ave/Lewelling  
 City: San Leandro Sheet 1  
 Logged by: DAF Driller: Bayland of 2  
 Casing installation data:

Drilling method: Hollow Stem Auger

Hole diameter: 8 inch

Top of Box Elevation: Datum:

PID (ppm)	Blows/ft. or Pressure (psf)	Type of Sample	Sample Number	Depth (ft.)	Sample	Well Detail	Soil Group Symbol (USCS)	Water Level		Description
								9'		
				1						PAVEMENT SECTION - 2 feet.
				2						
				3						
500	150	S&H push	S-14-5'	4						SILTY CLAY (CL-ML)- dark gray (2.5Y N4); soft; damp. becoming firm at 5 feet; with slight odor.
				5						
				6						
				7						
				8						SILTY SAND (SM)- olive (5Y 4/3); loose; damp; 30% medium sand; 20% very fine to fine sand; trace clay; no chemical odor, comment: drill cuttings.
50	2	S&H	S-14-	9						▼ CLAY (CL)- dark gray (2.5Y N4); stiff; damp; low plasticity; no chemical odor.
	3		10'	10						
	4			11						
				12						
				13						
0	2	S&H	S-14-	14						CLAY WITH SAND (CL)- light yellowish brown (2.5Y 6/4); medium stiff; damp; 10% very fine to fine sand; 5-10% silt; trace caliche nodules; mottled; no chemical odor.
	6		15'	15						
	7			16						
				17						
				18						
				19						
50	2	S&H	S-14-	19						▼ becoming saturated at 19 feet.
	6		20'	20						

Remarks:



GeoStrategies Inc.

BORING NO

S-14

JOB NUMBER  
7615

REVIEWED BY RG/CEG  
CWP CEG 1262

DATE  
5/89

REVISED DATE

REVISED DATE

Field location of boring:

Project No.: 7615

Date: 4/26/89

Boring No.:

Client: Shell

S-14

Location: 15275 Washington Ave/Lewelling

City: San Leandro

Sheet 2  
of 2

Logged by: DAF

Driller: Bayland

Casing installation data:

Drilling method: Hollow Stem Auger

Hole diameter: 8 inch

Top of Box Elevation:

Datum:

PID (ppm)	Blows/ft. or Pressure (psf)	Type of Sample	Sample Number	Depth (ft.)	Sample	Well Detail	Soil Group Symbol (USCS)
	7			21			
				22			
				23			
				24			
	2	SPT		25			
	2						
	4						

Water Level

Time

Date

Description

SANDY SILT (ML)- light yellowish brown (2.5Y 6/4); medium stiff; saturated; 30% very fine to fine sand; 5-10% clay; trace caliche nodules; mottled brown & black; no chemical odor.

CLAY (CL)- grayish brown (2.5Y 5/2); medium stiff; damp; low plasticity; trace caliche nodules; no chemical odor

Bottom of boring 24.0 feet, sampled to 25.5 feet  
4/26/89

Remarks:



GeoStrategies Inc.

BORING NO.

S-14

JOB NUMBER  
7615

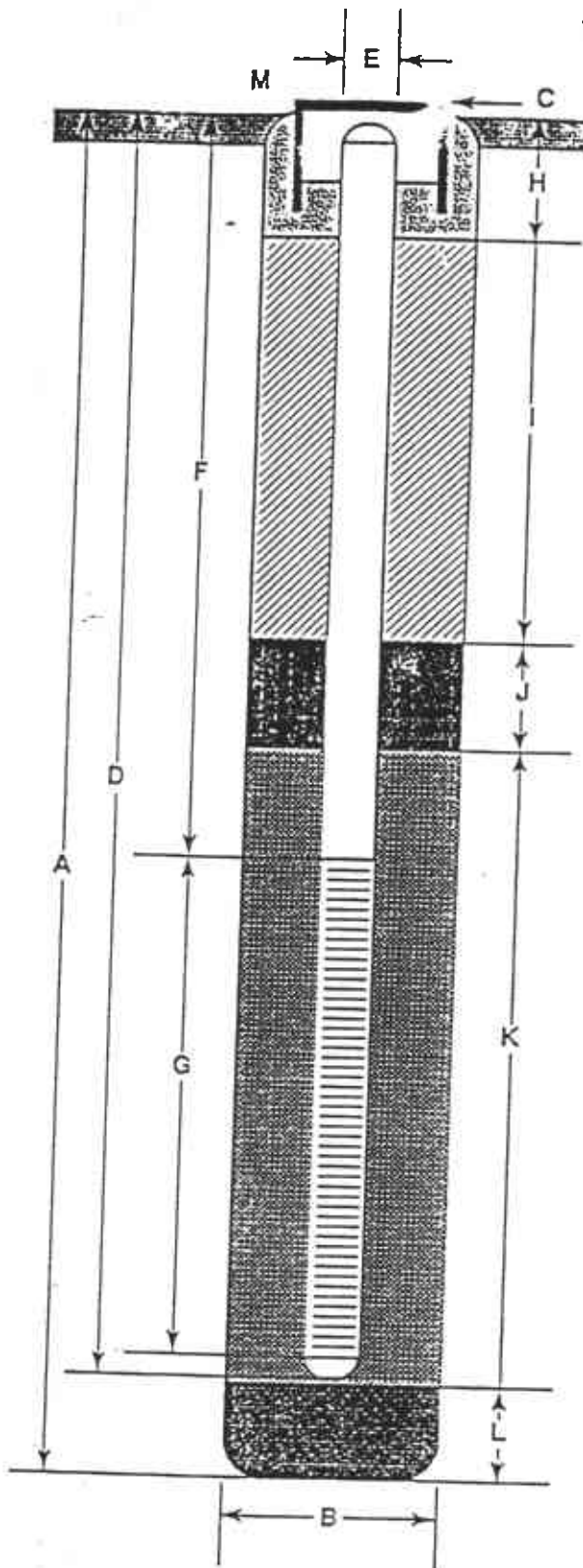
REVIEWED BY RG/CEG

DATE  
5/89

REVISED DATE

REVISED DATE

# WELL CONSTRUCTION DETAIL



- A Total Depth of Boring \_\_\_\_\_ 24 ft.
- B Diameter of Boring \_\_\_\_\_ 8 in.  
Drilling Method HOLLOW STEM AUGER
- C Top of Box Elevation \_\_\_\_\_ 20.44 ft.  
 Referenced to Mean Sea Level  
 Referenced to Project Datum
- D Casing Length \_\_\_\_\_ 23.5 ft.  
Material \_\_\_\_\_ SCH 40 PVC
- E Casing Diameter \_\_\_\_\_ 3 in.
- F Depth to Top Perforations \_\_\_\_\_ 4 ft.
- G Perforated Length \_\_\_\_\_ 20 ft.  
Perforated Interval from 4 to 24 ft.  
Perforation Type FACTORY SLOTTED  
Perforation Size \_\_\_\_\_ 0.020
- H Surface Seal \_\_\_\_\_ 2.5 ft.  
Seal Material \_\_\_\_\_ CONCRETE
- I Backfill \_\_\_\_\_ ft.  
Backfill Material \_\_\_\_\_
- J Seal \_\_\_\_\_ 0.5 ft.  
Seal Material \_\_\_\_\_ BENTONITE
- K Gravel Pack \_\_\_\_\_ 21 ft.  
Pack Material \_\_\_\_\_ LONESTAR 2/12 & #3
- L Bottom Seal \_\_\_\_\_ ft.  
Seal Material \_\_\_\_\_
- M \_\_\_\_\_ CHRISTY BOX



GeoStrategies Inc.

Well Construction Detail  
Former Shell Service Station  
15275 Washington Ave.  
San Leandro

WELL NO.

**S-14**

JOB NUMBER  
7615

REVIEWED BY RG/CEG  
*Chp ce41262*

DATE  
5/89

REVISED DATE

REVISED DATE

Field location of boring:	Project No.: 7615	Date: 4/26/89	Boring No:
	Client: Shell		S-15
	Location: 15275 Washington Ave/Lewelling		Sheet 1
	City: San Leandro		of 2
	Logged by: DAF	Driller: Bayland	
Casing installation data:			

Drilling method: **Hollow Stem Auger**  
Hole diameter: **8 inch**

Top of Box Elevation:	Datum:
Water Level: 8.3'	
Time: 2:25pm	
Date: 4/26/89	

PID (ppm)	Blows/ft. or Pressure (psf)	Type of Sample	Sample Number	Depth (ft.)	Sample	Well Detail	Soil Group Symbol (USCS)	Description
				1				PAVEMENT SECTION - 2.5 feet.
				2				
				3				CLAY (CL)- very dark grayish brown (2.5Y 3/2); medium stiff; damp; low plasticity; trace gravel.
55	150	S&H push	S-15-5'	4				
				5				SILTY CLAY (CL-ML) -olive (5Y 4/3); soft; damp; low plasticity; mottled brown.
				6				
				7				SILTY SAND (SM) -olive brown (2.5Y 4/4); loose; moist; poorly graded; trace clay.
				8				
				9				
35	2	S&H	S-15-10'	10				CLAY (CL) -very dark gray (5Y 3/1); stiff; damp; low plasticity; trace gravel; mottled brown; rootholes.
	4			11				
				12				
				13				
55	1	S&H	S-15-15'	14				becoming soft; 5% silt; trace caliche nodules at 14 feet.
	4			15				
	8			16				CLAY (CL) -olive gray (5Y 4/2); stiff; damp; low plasticity; mottled; trace caliche nodules.
				17				
				18				becoming saturated at 18.5 feet.
				19				
NM	3	SPT		20				SILTY CLAY (CL-ML) -light olive brown (2.5Y 5/4); medium stiff; saturated; trace organics; trace caliche nodules.
	2							

Remarks:



GeoStrategies Inc.

BOHRING 110

S-15

JOB NUMBER  
7615

REVIEWED BY RG/CEG  
*CEG* 262

DATE  
5/89

REVISED DATE

REVISED DATE

Field location of boring:	Project No.: 7615	Date: 4/26/89	Boring No:
	Client: Shell		S-15
	Location: 15275 Washington Ave/Lewelling		Sheet 2
	City: San Leandro		of 2
	Logged by: DAF	Driller: Bayland	
Casing installation date:			

Drilling method: Hollow Stem Auger

Hole diameter: 8 inch

Top of Box Elevation: Datum:

PID (ppm)	Blowsft. or Pressure (psf)	Type of Sample	Sample Number	Depth (ft.)	Sample	Well Detail	Soil Group Symbol (USCS)	Water Level				Description	
								Time	Date				
	4			21									
				22									
				23									
				24									
NM	1	SPT		25									
	3												
	5												
								CLAY (CL) -very dark gray (5Y 3/1); medium stiff; damp; low plasticity.					
								SILTY CLAY (CL-ML) - light olive brown (2.5Y 5/4); medium stiff; damp; some sandy lenses.					
								Bottom of boring 24.0 feet, Sampled to 25.5 feet 4/26/89					

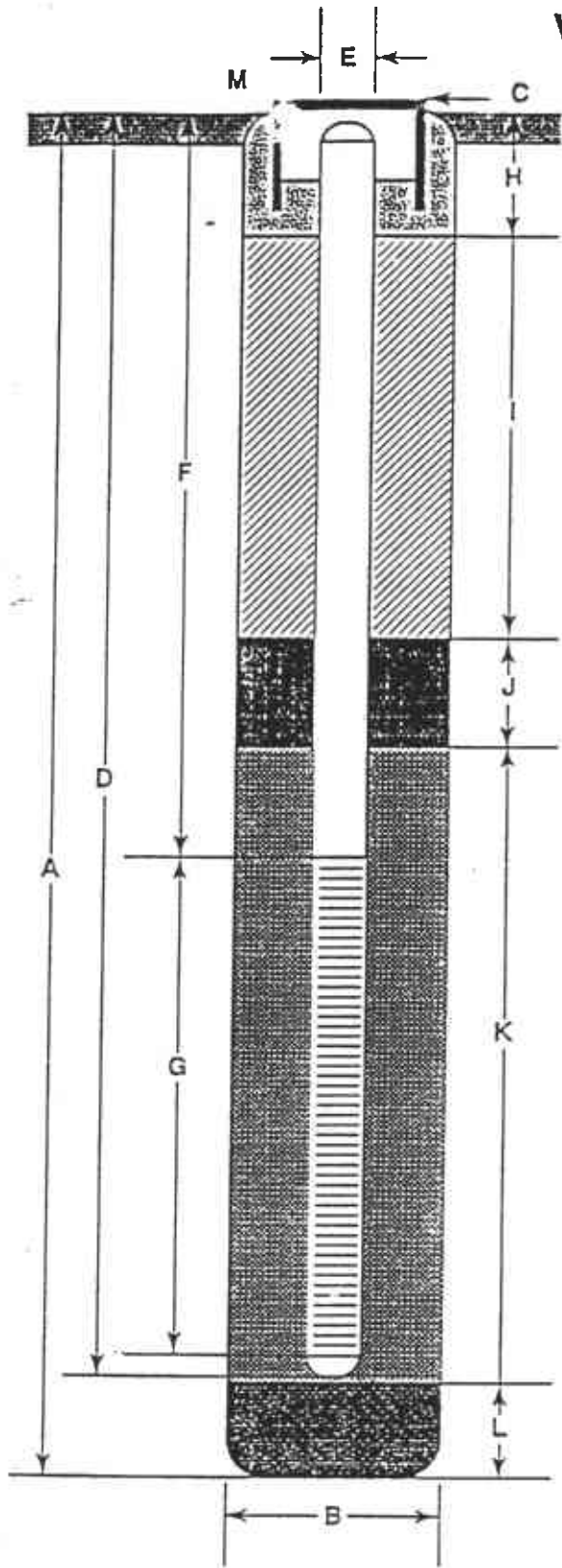
Remarks:



BORING NO. S-15



# WELL CONSTRUCTION DETAIL



- A Total Depth of Boring 24 ft.
- B Diameter of Boring 8 in.  
Drilling Method HOLLOW STEM AUGER
- C Top of Box Elevation 22.22 ft.  
 Referenced to Mean Sea Level  
 Referenced to Project Datum
- D Casing Length 23.5 ft.  
Material SCH 40 PVC
- E Casing Diameter 3 in.
- F Depth to Top Perforations 4 ft.
- G Perforated Length 20 ft.  
Perforated Interval from 4 to 24 ft.  
Perforation Type FACTORY SLOTTED  
Perforation Size 0.020
- H Surface Seal 2.5 ft.  
Seal Material CONCRETE
- I Backfill \_\_\_\_\_ ft.  
Backfill Material \_\_\_\_\_
- J Seal 0.5 ft.  
Seal Material BENTONITE
- K Gravel Pack 21 ft.  
Pack Material LONESTAR 2/12 & #3
- L Bottom Seal \_\_\_\_\_ ft.  
Seal Material \_\_\_\_\_
- M CHRISTY BOX



GeoStrategies Inc.

Well Construction Detail  
Former Shell Service Station  
15275 Washington Ave.  
San Leandro

WELL NO.

**S-15**

JOB NUMBER  
7615

REVIEWED BY RG/CEG  
CLP 06/12/62

DATE  
5/89

REVISED DATE

REVISED DATE

Field location of boring: \_\_\_\_\_

Project No.: 7615      Date: 4/25/89      Boring No: S-16

Client: Shell

Location: 15275 Washington Ave/Lewelling

City: San Leandro

Logged by: DAF      Driller: Bayland

Casing installation date: \_\_\_\_\_

Sheet 2 of 2

Drilling method: **Hollow Stem Auger**

Hole diameter: **8 inch**

Top of Box Elevation: \_\_\_\_\_ Datum: \_\_\_\_\_

PIU (ft)	Flow rate or Pressure (psi)	Type of Sample	Sample Number	Depth (ft.)	Sample	Well Detail	Soil Group Symbol (USCS)	Water Level		Description
								Time	Date	
	5			21			SC			CLAYEY SAND (SC) -pale brown (10 YR 6/3); loose; saturated.
				22						
				23						
0	1	S&H	S-16-	24			CL			SILTY CLAY (CL-ML) -brown (10YR 5/3); soft; damp; 10% silt; <10% fine sand; trace organics; mottled gray & orange.
	1		25'	25						
										Bottom of boring 24.0 feet, sampled to 25.5 feet.
										4/25/89

Remarks: \_\_\_\_\_

Field location of boring:

Project No.: 7615 Date: 4/25/89 Boring No: S-16  
 Client: Shell  
 Location: 15275 Washington Ave/Lewelling  
 City: San Leandro  
 Logged by: DAF Driller: Bayland  
 Casing installation data:

Drilling method: Hollow Stem Auger  
 Hole diameter: 8 inch

Top of Box Elevation: Datum.

PID (ppm)	Blowbl. or Pressure (psf)	Type of Sample	Sample Number	Depth (ft.)	Sample	Well Detail	Soil Group Symbol (USCS)	Water Level		Description
								Time	Date	
	5			21						
				22						CLAYEY SAND (SC) -pale brown (10 YR 6/3); loose; saturated.
				23						
0	1	S&H	S-16-	24						
	1		25'	25						SILTY CLAY (CL-ML) -brown (10YR 5/3); soft; damp; 10% silt; <10% fine sand; trace organics; mottled gray & orange.
	1									Bottom of boring 24.0 feet, sampled to 25.5 feet. 4/25/89

Remarks:



GeoStrategies Inc.

BORING NO.

S-16

JOB NUMBER  
7615

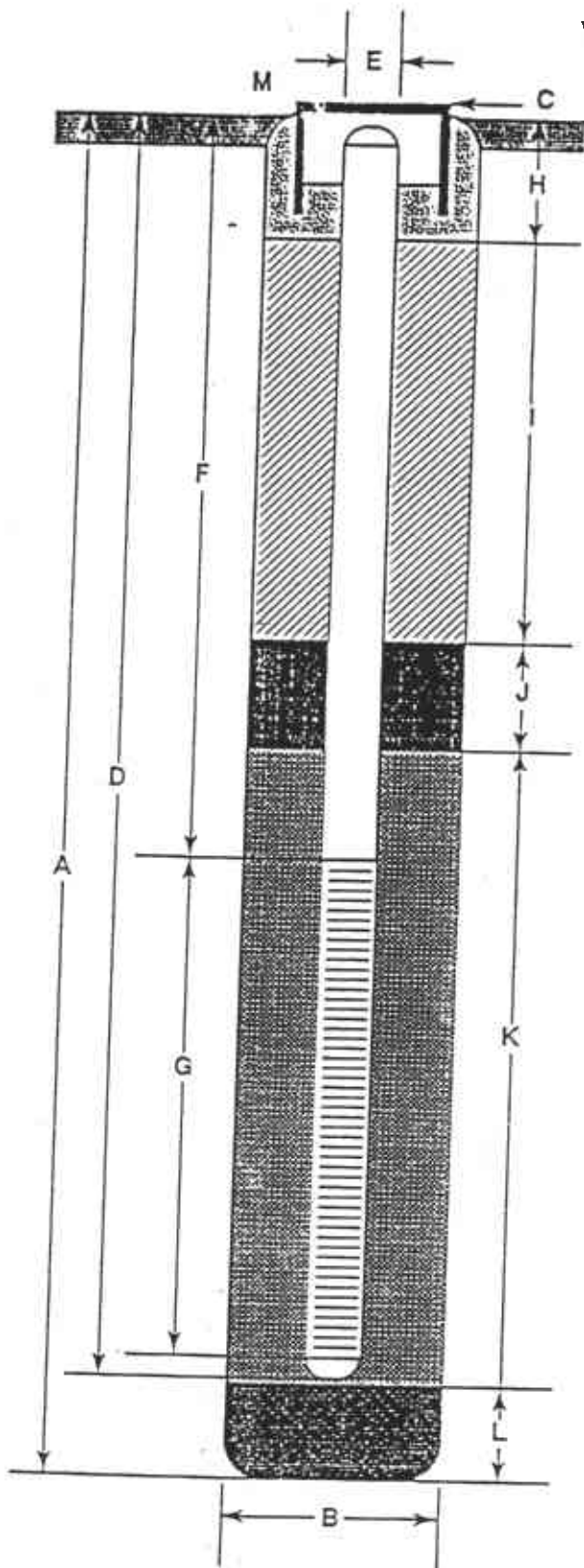
REVIEWED BY RG/CEG

DATE  
5/89

REVISED DATE

REVISED DATE

# WELL CONSTRUCTION DETAIL



- A Total Depth of Boring \_\_\_\_\_ 24 ft.
- B Diameter of Boring \_\_\_\_\_ 8 in.  
Drilling Method HOLLOW STEM AUGER
- C Top of Box Elevation \_\_\_\_\_ 21.82 ft.  
 Referenced to Mean Sea Level  
 Referenced to Project Datum
- D Casing Length \_\_\_\_\_ 23.5 ft.  
Material \_\_\_\_\_ SCH 40 PVC
- E Casing Diameter \_\_\_\_\_ 3 in.
- F Depth to Top Perforations \_\_\_\_\_ 4 ft.
- G Perforated Length \_\_\_\_\_ 20 ft.  
Perforated Interval from 4 to 24 ft.  
Perforation Type FACTORY SLOTTED  
Perforation Size \_\_\_\_\_ 0.020
- H Surface Seal \_\_\_\_\_ 2.5 ft.  
Seal Material \_\_\_\_\_ CONCRETE
- I Backfill \_\_\_\_\_ ft.  
Backfill Material \_\_\_\_\_
- J Seal \_\_\_\_\_ 0.5 ft.  
Seal Material \_\_\_\_\_ BENTONITE
- K Gravel Pack \_\_\_\_\_ 21 ft.  
Pack Material \_\_\_\_\_ LONESTAR 2/12 & #3
- L Bottom Seal \_\_\_\_\_ ft.  
Seal Material \_\_\_\_\_
- M \_\_\_\_\_ CHRISTY BOX



GeoStrategies Inc.

Well Construction Detail  
Former Shell Service Station  
15275 Washington Ave.  
San Leandro

WELL NO.

**S-16**

JOB NUMBER  
7615

REVIEWED BY RG/CEG  
CWP 641262

DATE  
5/89

REVISED DATE

REVISED DATE

Field location of boring: Project No.: 7615 Date: 4/25/89 Boring No: S-17  
 Client: Shell Location: 15275 Washington Ave/Lewelling City: San Leandro Sheet 1 of 2  
 Logged by: DAF Driller: Bayland Casing installation date:

Drilling method: Hollow Stem Auger Hole diameter: 8 inch Top of Box Elevation: Datum:

Water Level | 7.5' Time | 12.50 pm Date | 4/25/89 Description

PID (ppm)	Blow No. or Pressure (psf)	Type of Sample	Sample Number	Depth (ft.)	Sample	Well Detail	Soil Group Symbol (USCS)	Description
				1				PAVEMENT SECTION - 2 feet.
				2				
				3				SILTY SAND (SM) -very dark gray (5Y 3/1); loose; dry; >50% very fine to fine sand; trace clay.
12.5	150	S&H push	S-17-5'	4				
				5				SILTY CLAY (CL-ML) -dark greenish gray (5GY 4/1); medium stiff; damp; 5% very fine to fine sand; slight mottling - olive green & gray; moderate chemical odor.
				6				
				7				
				8				SANDY SILT (ML) -dark greenish gray (5GY 4/1); loose; saturated; 40% fine to very fine sand; 10% clay; weak chemical odor.
0	3	S&H	S-17-10'	9				
	4			10				
	7			11				SILTY CLAY WITH SAND (CL-ML) -dark gray (5Y 4/1), stiff; damp; 15-20% very fine to fine sand; trace caliche nodules; trace organics; mottled; rootholes.
				12				
				13				
NM	2	SPT		14				gravels up to 1 cm at 14 feet.
	4			15				CLAY (CL) -grayish brown (5Y 5/2); stiff; damp; trace caliche nodules up to 1 cm; mottled; occasional sand lens.
	7			16				
				17				
				18				SANDY SILT (ML) -light yellowish brown (10 YR 6/4); loose; saturated; 30% very fine to fine sand; trace clay; trace
NM	2	SPT		19				caliche nodules; trace medium grain sized sand.
	2			20				

Remarks:

Field location of boring:

Project No.: 7615

Date: 4/25/89

Boring No:

Client: Shell

S-17

Location: 15275 Washington Ave/Lewelling

City: San Leandro

Sheet 2  
of 2

Logged by: DAF

Driller: Bayland

Casing installation data:

Drilling method: Hollow Stem Auger

Hole diameter: 8 inch

Top of Box Elevation:

Datum:

PID (ppm)	Blows/ft. or Pressure (psf)	Type of Sample	Sample Number	Depth (ft.)	Sample	Well Detail	Soil Group Symbol (USCS)	Water Level		Description
								Time	Date	
	4			21						increasing clay at 20.5 feet.
				22						
				23						
NM	NM	SPT		24						SILTY CLAY (CL-ML) -olive (5Y 5/3); firm; damp; 10% very fine to fine sand; trace caliche nodules; trace medium to coarse grain sized sand; trace organics; trace saturated silt pockets.
				25						Bottom of boring 24.0 feet. Sampled to 25.5 feet. 4/25/89

Remarks:



GeoStrategies Inc.

BORING NO.

S-17

JOB NUMBER  
7615

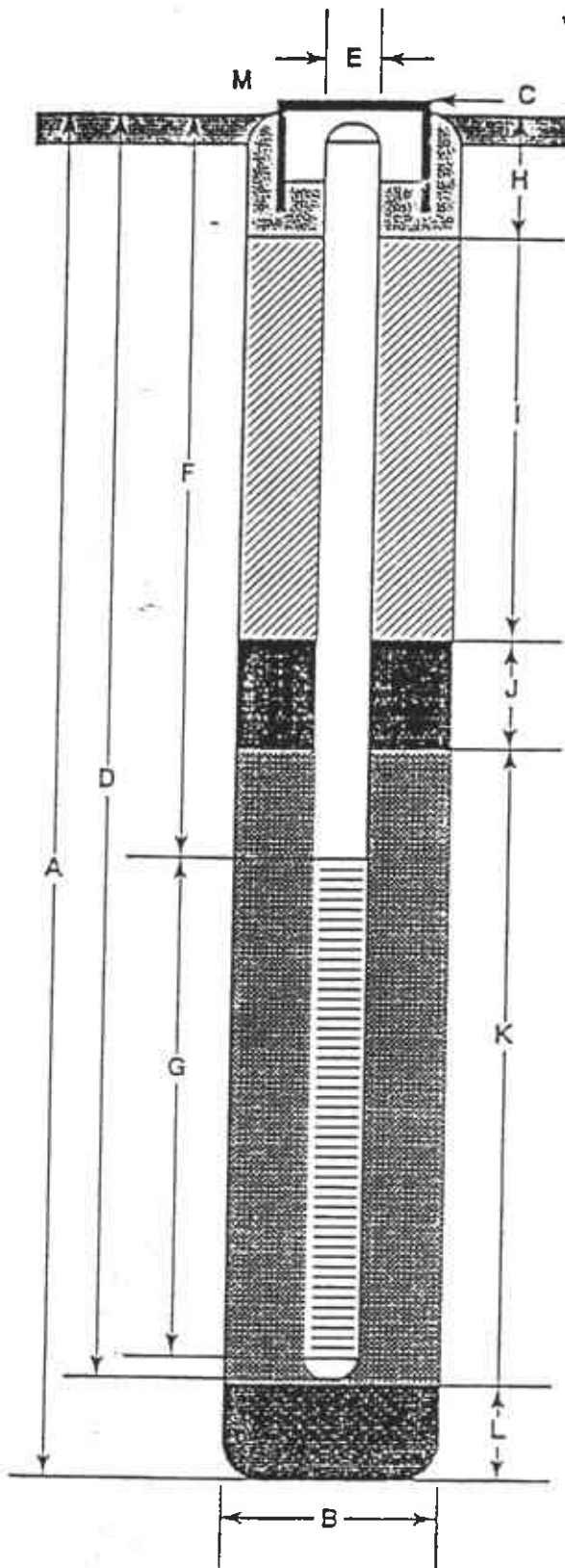
REVIEWED BY RQ/CEG

DATE  
5/89

REVISED DATE

REVISED DATE

# WELL CONSTRUCTION DETAIL



- A Total Depth of Boring \_\_\_\_\_ 24 ft.
- B Diameter of Boring \_\_\_\_\_ 8 in.  
Drilling Method HOLLOW STEM AUGER
- C Top of Box Elevation \_\_\_\_\_ 20.95 ft.  
 Referenced to Mean Sea Level  
 Referenced to Project Datum
- D Casing Length \_\_\_\_\_ 23.5 ft.  
Material SCH 40 PVC
- E Casing Diameter \_\_\_\_\_ 3 in.
- F Depth to Top Perforations \_\_\_\_\_ 4 ft.
- G Perforated Length \_\_\_\_\_ 20 ft.  
Perforated Interval from 4 to 24 ft.  
Perforation Type FACTORY SLOTTED  
Perforation Size \_\_\_\_\_ 0.020
- H Surface Seal \_\_\_\_\_ 2.5 ft.  
Seal Material CONCRETE
- I Backfill \_\_\_\_\_ ft.  
Backfill Material \_\_\_\_\_
- J Seal \_\_\_\_\_ 0.5 ft.  
Seal Material BENTONITE
- K Gravel Pack \_\_\_\_\_ 21 ft.  
Pack Material LONESTAR 2/12 & #3
- L Bottom Seal \_\_\_\_\_ ft.  
Seal Material \_\_\_\_\_
- M \_\_\_\_\_ CHRISTY BOX



GeoStrategies Inc.

Well Construction Detail  
Former Shell Service Station  
15275 Washington Ave.  
San Leandro

WELL NO.

**S-17**

JOB NUMBER  
7615

REVIEWED BY RG/CEG  
*Chp 0641262*

DATE  
5/89

REVISED DATE

REVISED DATE

Field location of boring: (See Plate 2)

Project No.: 7615 Date: 10/27/89 Boring No: SR-1

Client: Shell Oil Company

Location: 15275 Washington Avenue

City: San Leandro, California Sheet 1 of 3

Logged by: M.J.J. Driller: Bayland

Casing installation data: Pilot Boring

Drilling method: Hollow-Stem Auger

Hole diameter: 8-inches

Top of Box Elevation: Datum:

Water Level	12.5	10.9		
Time				
Date	10/27/89	10/27/89		

FD (ppm)	Blows/ft. or Pressure (psf)	Type of Sample	Sample Number	Depth (ft.)	Sample	Well Detail	Soil Group Symbol (USCS)	Description
				1				PAVEMENT SECTION - 4 inches
				2				FILL - Gravel (GW) - dark brown (10YR 3/3), damp, very loose.
				3				FILL - Clay with Silt (CL) - black (5Y 2.5/1), damp, soft, high plasticity; < 5% coarse sand; strong chemical odor.
				4				
231	2			5				
	3	S&H	SR1-5	5				
	4			6				CLAY (CL) - black (2.5Y N3/2), damp, soft, medium plasticity; interbeds of clayey sand (SP-SC); sand is very fine to fine; interbeds occur as discrete units 3 to 5 inches thick; contain 10-20% fines; strong chemical odor.
	3			6				
243	4	S&H	SR1-6.5	7				
	5			7				
	1			8				
296	2	S&H	SR1-8	8				
	3			9				
	2			9				moderate chemical odor.
	4			10				
373	6	S&H	SR1-10	10				COLOR CHANGE to black (10YR 3.3) at 10.5 feet.
	2			11				SILTY SAND (SM) - moist, loose, interbedded with clayey silt (ML-CL), medium plasticity; no chemical odor.
108	4	S&H		11				
	6		SR1-11.5	12				
				13				CLAY (CL) - very dark grayish brown (10YR 3/2), damp, stiff, high plasticity; fractured texture; no chemical odor.
				14				
	2			15				
4.3	4	S&H	SR1-15	15				first encountered water at 16.0 feet. Increasing sand at 16 feet. Interbedded clay with sand and clayey sand (observed during drilling with bucket auger, 11/16/89)
	8			16				
				17				
				18				
				19				

Remarks:



Field location of boring:  (See Plate 2)				Project No.: 7615		Date: 10/27/89		Boring No:	
				Client: Shell Oil Company		Location: 15275 Washington Avenue		City: San Leandro, California	
				Logged by: M.J.J.		Driller: Bayland		Sheet 2 of 3	
Drilling method: Hollow-Stem Auger				Casing installation data: Pilot Boring					
Hole diameter: 8-inches				Top of Box Elevation:				Datum:	
PCD (ppm)	Blow/L or Pressure (psf)	Type of Sample	Sample Number	Depth (ft.)	Sample	Well Detail	Soil Group Symbol (USCS)	Water Level	
								Time	Date
								Description	
80	2 4 6	S&H	SR1-20	20					
				21					CLAYEY SILT (ML-CL) - light olive brown (2.5Y 5/4), saturated, medium plasticity; 30% clay; 5% fine to medium sand; no chemical odor.
				22					
				23					
				24					CLAY with SAND (CL) - olive gray (5Y 4/2), saturated, stiff, high plasticity; 20% very fine to fine sand; no chemical odor.
66	3 3 6	S&H	SR1-30	25					
				26					SILT with SAND (ML) - light olive brown (2.5Y 5/4), saturated, stiff; 15% fine to medium sand; 20-30% clay; no chemical odor.
				27					
				28					
				29					SAND with SILT (SP-SM) - light olive brown (5Y 4/2), fine sand, saturated, medium dense; well sorted; 10% silt; trace clay; laminae of silt 0.25 inches thick in shoe; iron oxide staining; no chemical odor.
10	3 8 10	S&H	SR1-30	30					
				31					
				32					
				33					
				34					SILTY SAND (SM) - light olive brown (5Y 4/2), saturated, dense; very fine to medium sand; 15% silt; trace clay; no chemical odor.
34	5 7 18	S&H	SR1-35	35					
				36					
				37					
				38					
				39					SAND (SP) - dark grayish brown (2.5Y 3/2), saturated, dense, very fine to medium sand; interbeds of fine
Remarks:									



GeoStrategies Inc.

Log of Boring

BORING NO.

SR-1

JOB NUMBER  
7615

REVIEWED BY RG/CEG  
CWP ceg 1262

DATE  
11/89

REVISED DATE

REVISED DATE

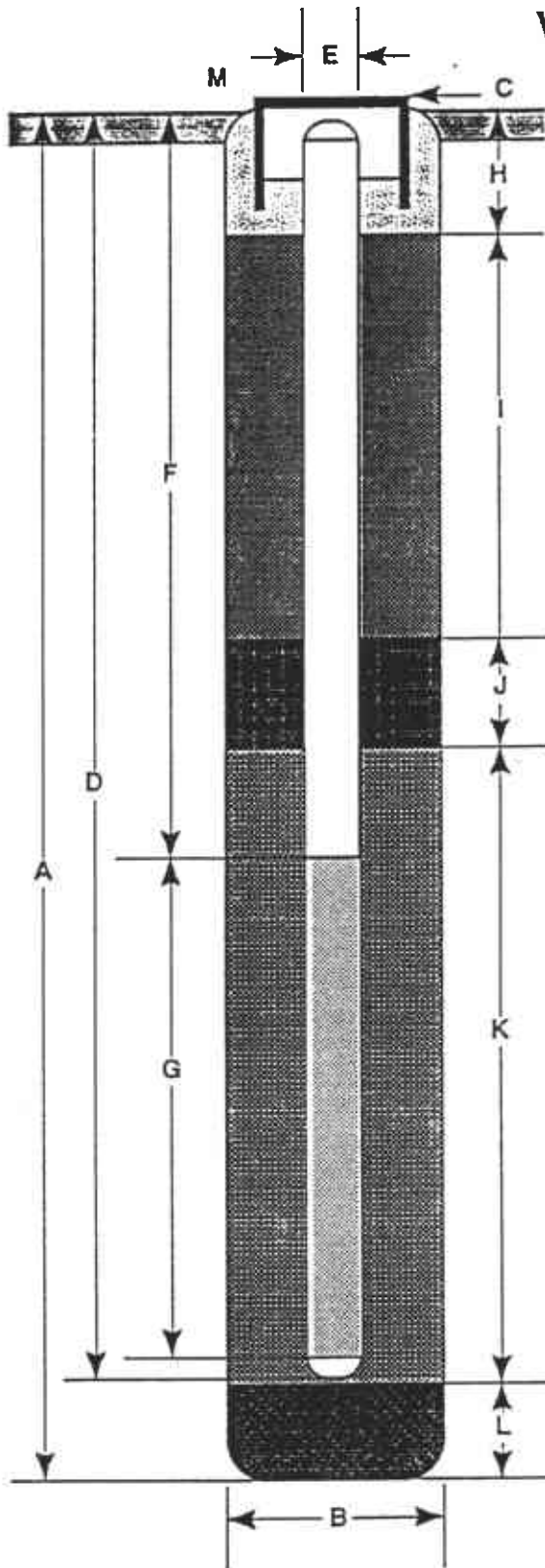
Field location of boring:  (See Plate 2)	Project No.: 7615	Date: 10/27/89	Boring No:
	Client: Shell Oil Company		SR-1
	Location: 15275 Washington Avenue		
	City: San Leandro, California		Sheet 3
	Logged by: M.J.J.	Drill: Bayland	of 3

Drilling method: Hollow-Stem Auger	Pilot Boring
Hole diameter: 8-inches	Top of Box Elevation: Datum:

P.D. (gpm)	Blows/ft. or Pressure (psf)	Type of Sample	Sample Number	Depth (ft.)	Sample	Well Detail	Soil Group Symbol (USCS)	Water Level	Time	Date	Description
	9										
8.2	13	S&H	SR1-40	40							silty sand 0.5 to 3.0 inches thick; no chemical odor.
	17										Bottom of boring at 40.5 feet.
				41							Bottom of sample at 40.5 feet.
				42							10/27/89
				43							
				44							
				45							
				46							
				47							
				48							
				49							
				50							
				51							
				52							
				53							
				54							
				55							
				56							
				57							
				58							
				59							

Remarks: Boring caved to 30 feet, Bentonite from 19 to 30 feet.

# WELL CONSTRUCTION DETAIL



- A Total Depth of Boring \_\_\_\_\_ 40.5 ft.
- B Diameter of Boring \_\_\_\_\_ 20 in.  
Drilling Method \_\_\_\_\_ Bucket Auger
- C Top of Box Elevation \_\_\_\_\_ ft.  
 Referenced to Mean Sea Level  
 Referenced to Project Datum
- D Casing Length \_\_\_\_\_ 21 ft.  
Material \_\_\_\_\_ Schedule 40 PVC
- E Casing Diameter \_\_\_\_\_ 6 in.
- F Depth to Top Perforations \_\_\_\_\_ 6.5 ft.
- G Perforated Length \_\_\_\_\_ 15 ft.  
Perforated Interval from \_\_\_\_\_ 6.5 to \_\_\_\_\_ 21.5 ft.  
Perforation Type \_\_\_\_\_ Machine Slot  
Perforation Size \_\_\_\_\_ 0.020 in.
- H Surface Seal from \_\_\_\_\_ 0.5 to \_\_\_\_\_ 1.0 ft.  
Seal Material \_\_\_\_\_ concrete
- I Backfill from \_\_\_\_\_ 1.0 to \_\_\_\_\_ 4.5 ft.  
Backfill Material \_\_\_\_\_ cement
- J Seal from \_\_\_\_\_ 4.5 to \_\_\_\_\_ 5.5 ft.  
Seal Material \_\_\_\_\_ Bentonite
- K Gravel Pack from \_\_\_\_\_ 5.5 to \_\_\_\_\_ 21.5 ft.  
Pack Material \_\_\_\_\_ 2/12 Lonestar sand
- L Bottom Seal \_\_\_\_\_ 21.5-30 ft.  
Seal Material \_\_\_\_\_ Bentonite
- M \_\_\_\_\_ Christy Box

Note: 30 to 40.5 Native Material (slough)



GeoStrategies Inc.

Well Construction Detail

WELL NO.

SR-1

JOB NUMBER  
7615

REVIEWED BY RG/CEG  
*Clayton*

DATE  
10/89

REVISED DATE

REVISED DATE

Field location of boring:

(See Plate 2)

Project No.: 761502 Date: 05/16/91 Boring No: S-18  
 Client: Shell Oil Company  
 Location: 15275 Washington  
 City: San Leandro, California Sheet 1 of 2  
 Logged by: E.C.F. Driller: Bayland  
 Casing installation data: (See Well Construction Detail)

Drilling method: Hollow Stem Auger  
 Hole diameter: 8-inches

Top of Box Elevation: Datum:  
 Water Level 7.5' 7.6'  
 Time 10:00 12:03  
 Date 05/16/91 05/16/91  
 Description

PO (ppm)	Blowft. * or Pressure (psf)	Type of Sample	Sample Number	Depth (ft.)	Sample	Well Detail	Soil Group Symbol (USCS)
				0			
				1			
				2			
				3			
				4			
0	450	S&H		5			
	450		S18-4.5				
	450			6			
				7			
0	4	S&H		8			
			S18-8				
				9			
				10			
0	6	S&H		10			
			S18-10				
				11			
				12			
				13			
				14			
0	16	S&H		15			
			S18-15				
				16			
				17			
				18			
				19			

PAVEMENT SECTION - 0.33 feet  
 SAND (SP) - yellowish brown (10YR 5/4), medium dense, damp; 80% coarse to medium sand; 15% gravel; 5% fines (FILL).

SILT with SAND (ML) - very dark gray (7.5YR N3/), stiff, damp; 80% silt; 20% very fine sand (ALLUVIUM).

Soft drilling at 7.0 feet.  
 SILTY SAND (SM) - dark grayish brown (10YR 4/2), loose, saturated; 70% sand; 30% silt.

Increasing moisture and silt content with depth.

CLAY (CL) - gray brown (2.5Y 5/2), stiff, moist; trace fine sand with rootholes and vertical dark stains.

Remarks: \* Converted to equivalent Standard Penetration blows/ft.

Log of Boring

BORING NO.



GeoStrategies Inc.

S-18

JOB NUMBER 761502

REVIEWED BY RGCEG  
 DHP

DATE 05/91

REVISED DATE

REVISED DATE

Field location of boring:

(See Plate 2)

Project No.: 761502	Date: 05/16/91	Boring No:
Client: Shell Oil Company		S-18
Location: 15275 Washington		Sheet 2
City: San Leandro, California		of 2
Logged by: E.C.F.	Driller: Bayland	
Casing installation data:		

Drilling method: Hollow Stem Auger  
 Hole diameter: 8-Inches

Top of Box Elevation: \_\_\_\_\_ Datum: \_\_\_\_\_

PO (ppm)	Blows/ft. * or Pressure (psf)	Type of Sample	Sample Number	Depth (ft.)	Sample	Well Detail	Soil Group Symbol (USCS)	Water Level	Time	Date	Description
	12	S&H		20							
			S18-20.5	21							COLOR CHANGE to light yellow brown (2.5YR 6/4), stiff, damp; 80% clay; 20% coarse sand.
				22							
				23							Bottom of boring at 19.0 feet.
				24							Bottom of sample at 20.5 feet.
				25							
				26							
				27							
				28							
				29							
				30							
				31							
				32							
				33							
				34							
				35							
				36							
				37							
				38							
				39							

Remarks:

### Log of Boring

BORING NO.



GeoStrategies Inc.

# S-18

JOB NUMBER  
761502

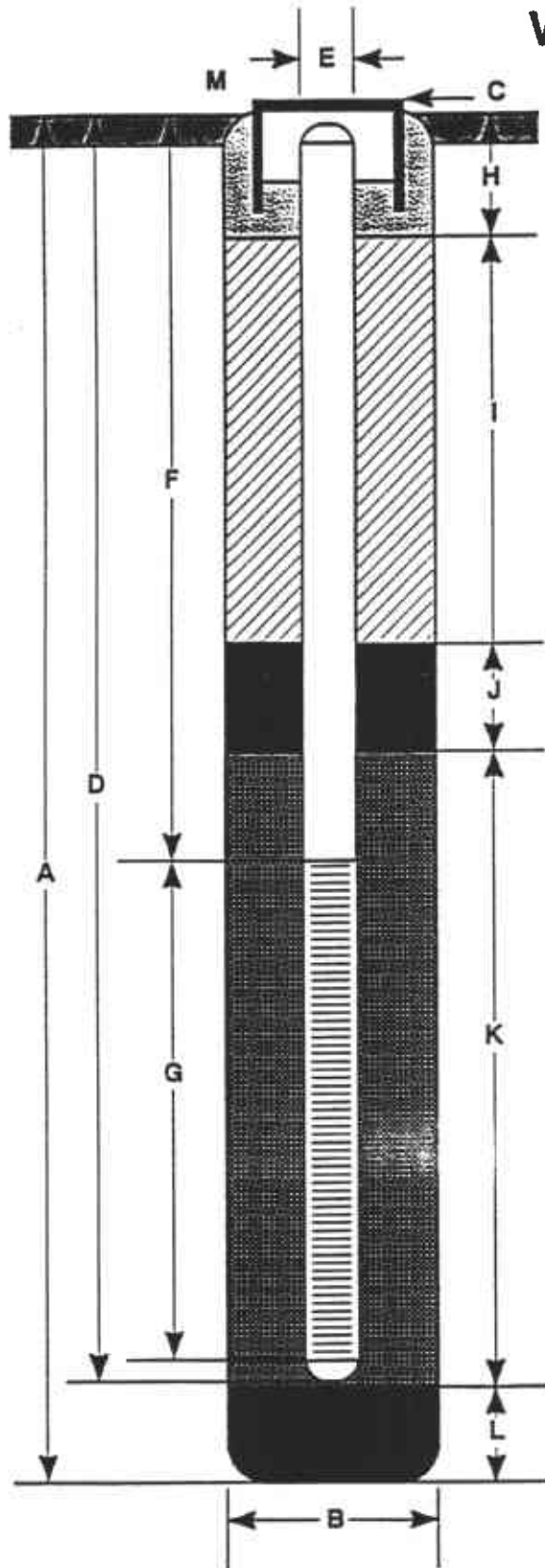
REVIEWED BY: RJC/CEG  
DHP

DATE  
05/91

REVISED DATE

REVISED DATE

# WELL CONSTRUCTION DETAIL



- A Total Depth of Boring \_\_\_\_\_ 19.0 ft.
- B Diameter of Boring \_\_\_\_\_ 8 in.  
Drilling Method \_\_\_\_\_ Hollow Stem Auger
- C Top of Box Elevation \_\_\_\_\_ ft.  
 Referenced to Mean Sea Level  
 Referenced to Project Datum
- D Casing Length \_\_\_\_\_ 18.0 ft.  
Material \_\_\_\_\_ Schedule 40 PVC
- E Casing Diameter \_\_\_\_\_ 3 in.
- F Depth to Top Perforations \_\_\_\_\_ 4 ft.
- G Perforated Length \_\_\_\_\_ 12 ft.  
Perforated Interval from \_\_\_\_\_ 4 to \_\_\_\_\_ 18 ft.  
Perforation Type \_\_\_\_\_ Machine Slotted  
Perforation Size \_\_\_\_\_ 0.02 in.
- H Surface Seal from \_\_\_\_\_ 0 to \_\_\_\_\_ 1.5 ft.  
Seal Material \_\_\_\_\_ Concrete
- I Backfill from \_\_\_\_\_ 1.5 to \_\_\_\_\_ 2 ft.  
Backfill Material \_\_\_\_\_ Concrete
- J Seal from \_\_\_\_\_ 2 to \_\_\_\_\_ 3 ft.  
Seal Material \_\_\_\_\_ Bentonite
- K Gravel Pack from \_\_\_\_\_ 3 to \_\_\_\_\_ 18 ft.  
Pack Material \_\_\_\_\_ 2/12 Lonestar Sand
- L Bottom Seal \_\_\_\_\_ 1 ft.  
Seal Material \_\_\_\_\_ Bentonite
- M \_\_\_\_\_ Underground vault with cover, cap and lock.

Note: Depths measured from initial ground surface.



GeoStrategies Inc.

Well Construction Detail

WELL NO.

S-18

JOB NUMBER  
761502

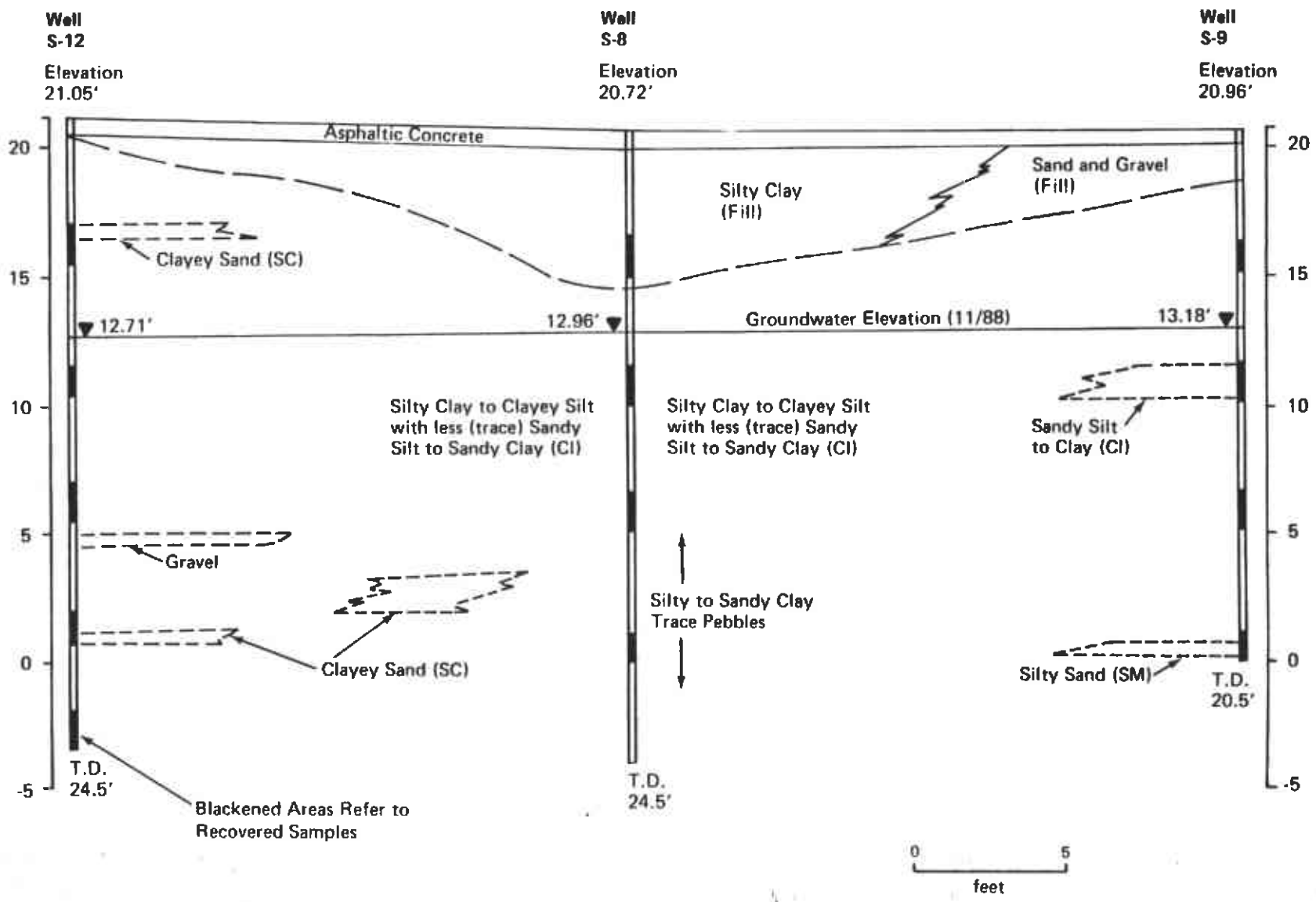
REVIEWED BY RG/CEG  
DHP

DATE  
5/91

REVISED DATE

REVISED DATE

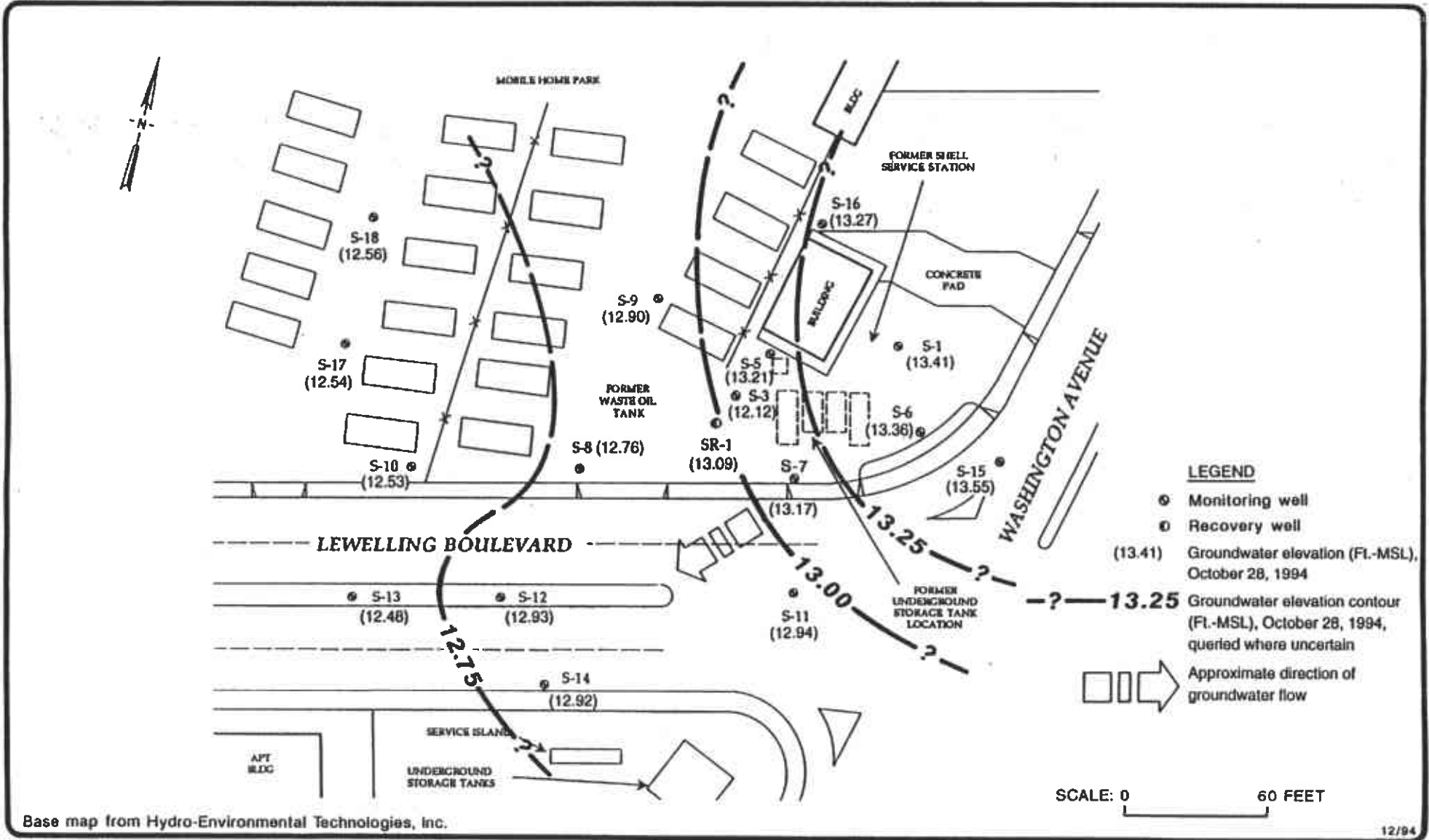
<b>Woodward-Clyde Consultants</b>	Project No. 8820011A
	Gertler Ryan
<b>CROSS SECTION SHELL SERVICE STATION LEWELLING BLVD. AND WASHINGTON AVE. SAN LEANDRO, CALIFORNIA</b>	
	Figure 6



**APPENDIX B**

**Fourth Quarter 1994  
Groundwater Contour Map**






**EMCON**  
Associates  
Sacramento, California

SHELL OIL COMPANY  
FORMER SHELL SERVICE STATION  
15275 WASHINGTON AVENUE  
SAN LEANDRO, CALIFORNIA

---

GROUNDWATER CONTOUR MAP, OCTOBER 28, 1994

FIGURE  
**2**  
PROJECT NO.  
0117-115.01

## APPENDIX C

### Well Survey Data



COUNTY OF ALAMEDA  
PUBLIC WORKS AGENCY

399 Elmhurst Street • Hayward, CA 94544-1395  
(510) 670-5480  
FAX (510) 670-5262

FAX TRANSMITTAL    FAX TRANSMITTAL    FAX TRANSMITTAL    FAX TRANSMITTAL

DATE: 3-30-95

TO: ENVIROS  
Box 259  
SONOMA, CA 95476

FROM: CRAIG JOHNSON  
(510) 670-5248

ATTN: GREG VAUGHN

(707) 939-2131  
(707) 935-6649

# OF PAGES (INCLUDING COVER SHEET) 9

COMMENTS:

WELL SURVEY .5 MILE RADIUS FROM LEWELLING + WASHINGTON,  
SAN LEANDRO.

COVER SHEET, 1 MAP, 3 DATA, 4 EXPLANATION SHEETS.

If you do not receive the entire transmittal, or if it is illegible,  
please call \_\_\_\_\_ at (510) 670-5543

## WELL INVENTORY FILE

Definitions and abbreviations for items listed in the well inventory file are as follows:

[WELLNO] Well number - Wells are numbered according to their location in the rectangular system of the Public Land Survey. The part of the number preceding the slash indicates the township; the part following the slash indicates the range and section number; the letter following the section number indicates the 40-acre subdivision; and the final digit is a serial number for wells in each 40-acre subdivision.

[DAT] Date - The month and year when drilling or boring was completed.

[ELEV] Surface elevation - The surface elevation of the well, if known, in feet above mean sea level. A zero designates an unknown elevation.

[TD] Total depth - The depth of the well. This usually designates the completed well depth. If the well has a well log available on file, then the total drilled depth of the well is given. The inventory does not show total depth data for geotechnical borings. This is because only one state well number is assigned to one boring at a site, and there are usually several borings of different depth.

[DTW] Depth to water - This category usually indicates the standing groundwater level in the well on the date of completion. The "depth to first water encountered" is recorded in the inventory when it is the only water level data reported on the well driller's report.

[USE] Use - The well use (or in the case of cathodic protection wells and geotechnical borings, the reason for the excavation) as indicated in the well driller's report or data sheets. A plus sign (+) after the well use indicates a well in the current ACFC & WCD monitoring network.

[ABN] Abandoned well - A well whose use has been permanently discontinued or which is in such a state of disrepair that no water can be produced. In the inventory, this may include wells which are covered or capped but not properly destroyed.

[DES] Destroyed well - A well that has been properly filled so that it cannot produce water nor act as a vertical conduit for the movement of groundwater.

[DOM] Domestic well - A water well which is used to supply water for the domestic needs of an individual residence or systems of four or less service connections or "hookups".

[INA] Inactive well - A well not routinely operating but capable of being made operable with a minimum of effort. Also called a "standby well".

[IND] Industrial well - A water well used to supply industry on an individual basis.

[IRR] Irrigation well - A water well used to supply water only for irrigation or other agricultural purposes. In the inventory, this category includes large capacity wells as well as small capacity wells for lawn irrigation.

[MON] Monitoring or observation well - Wells constructed for the purpose of observing or monitoring groundwater conditions. (see piezometer).

[MUN] Municipal well - A water well used to supply water for domestic purposes in systems subject to Chapter 7, Part 1, Division 5 of the California Health and Safety Code. Included are wells supplying public water systems classified by the Department of Health Services. (Also referred to as community water supply wells).

[PIE] Piezometer - A piezometer is a well specifically designated to measure the hydraulic head within a zone small enough to be considered a point as contrasted with a well that reflects the average head of the aquifer for the screened interval.

[STO] Stock - A water well used primarily for livestock.

[TES] Test well and test hole - A test well is constructed for the purpose of obtaining the information needed to design a well prior to its construction. Such wells are not to be confused with "test holes" which are temporary in nature (i.e., uncased excavations whose purpose is the immediate determination of existing geologic and hydrologic conditions). Test wells are cased and can be converted to observation or monitoring wells, and under certain circumstances, to production wells. In the inventory, "TES" includes both test wells and test holes.

[?] Unidentified use - This indicates water wells whose use could not be ascertained from the available well data.

[CAT] Cathodic protection well - Any artificial excavation constructed by any method for the purpose of installing equipment or facilities for the protection from

corrosion by electrochemical methods of metallic equipment (usually piping) in contact with the ground; commonly referred to as cathodic protection.

[GEO] Geotechnical boring - A temporary boring made to determine certain engineering properties of soils. An asterisk (\*) indicates that the state well number assigned to the boring represents more than one boring at a particular site.

[LOG] Log - This category indicates whether a geologic record, or log, for the well or boring is available in the Agency's files. Abbreviations are as follows:

D - well driller's log

G - geotechnical boring log

E - electric (resistivity) log or other subsurface geophysical logs.

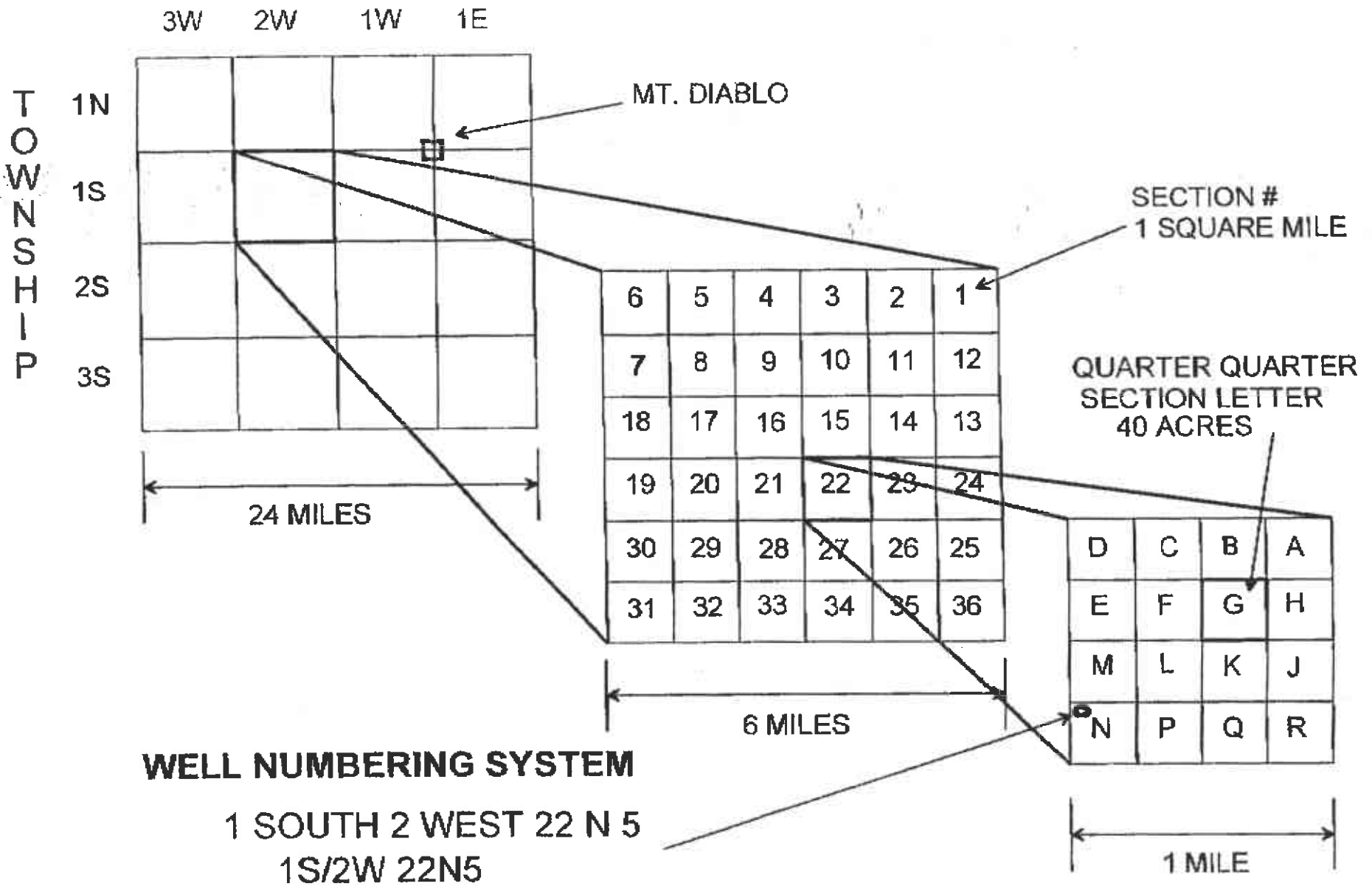
[WQ] Water quality data available - This category indicates which wells have water quality data available in ACFC & WCD files. The numbers 1 through 9 signify the number of sets of water quality measurements available for that well. A plus sign (+) indicates that 10 or more sets of data are available. A "0" indicates that no data is available.

[WL] Water level data available - This category indicates which wells have water level data other than the data reported on the well driller's logs. The numbers 1 through 9 signify the number of water level measurements available. A plus sign (+) indicates that 10 or more measurements are available for that well. A "0" indicates that no data is available.

[YLD] Yield - The maximum pumping rate in gallons per minute that can be supplied by a well without lowering the water level in the well below the pump intake. This data is taken from pump test data recorded in the driller's records. Some of the yield data reflects current production rates and does not reflect maximum yield values determined in a capacity test.

[DIA] Diameter - The diameter in inches of the main casing in a well. May also indicate the diameter of a hand-dug well. Diameter data is not recorded for geotechnical borings.

# RANGE



SECTION #  
1 SQUARE MILE

QUARTER QUARTER  
SECTION LETTER  
40 ACRES

## WELL NUMBERING SYSTEM

1 SOUTH 2 WEST 22 N 5  
1S/2W 22N5

Table with columns: WELL #, CITY, ADDRESS, OWNER, PHONE USE, DR. DATE, DIAM, TOT. DEPTH, DTW, ST. SLEV, WA. SLEV, YIELD, LOG, EQ, WL, DATA, ORGN, MARGIN. The table lists well information for a .5 mile radius from Lewelling & Washington Ave.

Page #1

FILED -30-95 THU 17:05 ID: ALAMEDA CO PUBLIC WK FAX NO: 510/570-5222



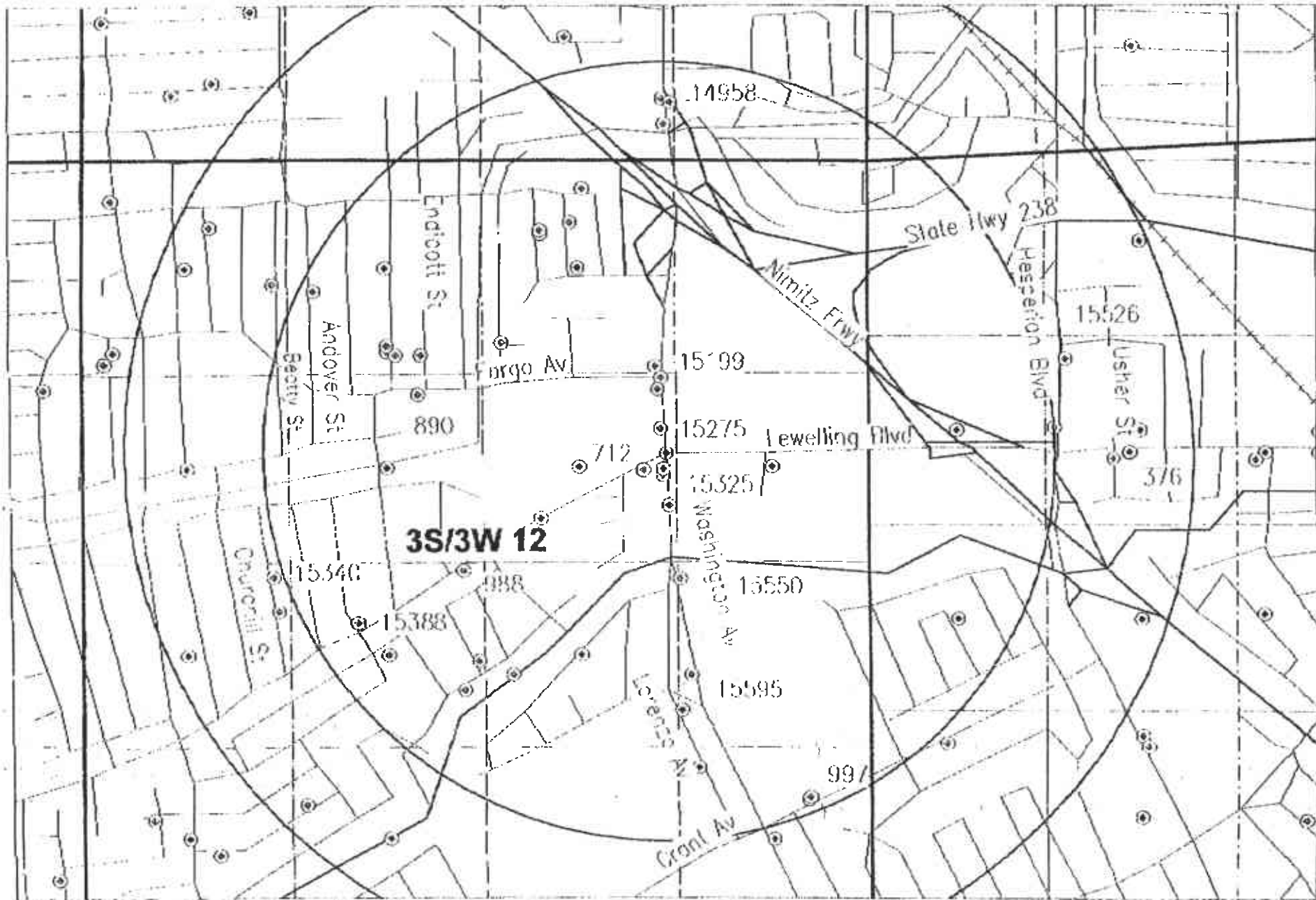


WELL #	CITY	ADDRESS	OWNER	PHONE USE	DR. DATE	DIAM	TOT. DEPTH	DTW	ST. ELEV	WA. ELEV	YIELD	LOG	WQ	WL	DATA	ORGN	MARGIN
38/3W 12R 8	SLZ	997 Grant Ave	Chevron USA	0 MON	11/90	2	27	12	0	0	0	D	0	0			D
38/3W 12R 8	SLZ	997 Grant Ave	Chevron USA	0 MON	2/91	2	14	4	180	96	0	G					D
38/3W 12R 9	SLZ	15703 Lorenzo Ave.	SLZ Unified School Distri	0 MON	8/92	2	24	20	0	0	0	D	0	0			D
38/3W 12R10	SLZ	15221 Wicke Blvd.	SLZ Unified School Dist.	0 MON	8/92	2	25	14	0	0	3	D	0	0			D
38/3W 12R11	SLZ	15221 Wicke Blvd.	SLZ Unified School Dist.	0 MON	8/92	2	20	11	0	0	3	D	0	0			D
38/3W 12R12	SLZ	15221 Wicke Blvd.	SLZ Unified School Dist.	0 MON	8/92	2	20	9	0	0	0	D	0	0			D
38/3W 12R13	SLZ	997 Grant Ave	Chevron USA C-5	0 MON	2/93	2	21	15	0	0	0	G	0	0			D
38/3W 13B 1	SLZ	15550 WASHINGTON AV	NORERN VEGETABLE NURSERY	0 TRR	6/48	12	550	0	0	0	0	D	0	0			L
38/3W 14A 2	SLZ	SAN LORENZO WELL FIELD	MBWCO	0 MUN	10/15	10	834	0	7	0	0	D	0	0			L
38/3W 14B 1	SLZ	LEWELLING	TROJAN POWDER CO.	0 ABN	?	12	533	0	6	0	0	D	0	0			L
38/3W 14C 4	SLZ	LEWELLING BLVD	LIVERMORE-AMADOR VALLEY	0 CAT	5/79	0	140	0	0	0	0	D	0	0			L
38/3W 14F 1	SLZ	LEWELLING BLVD	TROJAN POWDER CO.	0 ABN	10/15	12	769	0	0	0	0	D	0	0			L
38/3W 14G 1	SLZ	LEWELLING	TROJAN POWDER CO.	0 ABN	8/15	12	600	0	0	0	0	D	0	0			L
38/3W 14G 3	SLZ	LEWELLING BLVD	TROJAN POWDER CO.	0 ABN	9/19	12	785	0	5	0	0	D	0	0			L
38/3W 14H 3	SLZ	LEWELLING BLVD	TROJAN POWDER CO.	0 ABN	?	10	0	0	0	0	0	D	7	0			L

#263 P09

MAR-30-'95 THU 17:10 ID:ALAMEDA CO PUBLIC WIK FAX NO:510/670-5262

MR-30-35 THU 17:05 10:11:11:01 99:17:05 00 PUBLIC WK FRS NUTRITION/DIV/03/30/95



**.5 mile radius from Lewelling & Washington Ave.  
03/30/1995**

EMCON WELL NUMBER	DATE DRILLED, DRILLER	WELL OWNER LISTED	STATUS IF KNOWN	WELL CONSTRUCTION DETAILS								EDITED DRILLER REPORTS	
				TOT. DPTH (FT.)	COMP. DPTH (FT.)	PERF. INTER. (FT.)	SEAL DPTH (FT.)	CASE DIA. (IN.)	CASE MAT.	WAT. LEV. (FT.)	EST. Q (GPM)		SURF. ELEV. (FT.)
1	1900 Owner	Heide 90 Grant San Lorenzo	Domestic	?	36			6					
2	1935 Owner	Gianelli 143 Grant San Lorenzo	Irrig.	?	113	48-113		10-8					
?	6/12/48 ?	Modern Vec. Nursery 15550 Washington Ave. San Lorenzo	Irrig.	?	?			12					
4	? ?	Gianelli 15841 Nielson Ave San Lorenzo	Irrig.	?	113	48-113							
5	Owner ?	Bratton 15868 Corte Ulisse, San Lorenzo	Irrig.	?	21								
6	Owner ?	Moyers 1508 Via Hermana San Lorenzo	Irrig.	?	30								
7	? ?	Norris 16030 Via Nueva San Lorenzo	Irrig.	?	20								
8	8/5/56 Domestic Water Well Company	Lichty 16148 Channel St. San Lorenzo	Irrig.	?	30	15-30		6					

EMCON WELL NUMBER	DATE DRILLED, DRILLER	WELL OWNER LISTED	STATUS IF KNOWN	WELL CONSTRUCTION DETAILS									EDITED DRILLER REPORTS
				TOT. DPTH (FT.)	COMP. DPTH (FT.)	PERF. INTER. (FT.)	SEAL DPTH (FT.)	CASE DIA. (IN.)	CASE MAT.	WAT. LEV. (FT.)	EST. Q (GPM)	SURF. ELEV. (FT.)	
9	1920 ?	Marengo 14953 Washington San Lorenzo		?	60			8					
10	1936 White	Twn. Nursery Irrig. Corp. 14958 Washington San Lorenzo		?	335			14				23	
11	1936 White	Twn. Nursery Irrig. Corp. 14958 Washington San Lorenzo		?	325			14				23	
12	5/26/78 AR-GO Pump Co.	McCarthy 2770 Scott Blvd. Santa Clara		?	?								
13	1930 ?	Fara Bros Domestic 391 W. 150th San Lorenzo		?	120	99-110		10				20	
14	1949 Owner	Ramirez Irrig. 14960 Crosby San Lorenzo		?	32	22-32		4					
15	9/28/34 G.P. Nelson	Gansberger		?	545	487-492 518-520 521-528 530-540		12				35	





EMCON WELL NUMBER	DATE DRILLED, DRILLER	WELL OWNER LISTED	STATUS IF KNOWN	WELL CONSTRUCTION DETAILS									EDITED DRILLER REPORTS	
				TOT. DPTH (FT.)	COMP. DPTH (FT.)	PERF. INTER. (FT.)	SEAL DPTH (FT.)	CASE DIA. (IN.)	CASE MAT.	WAT. LEV. (FT.)	EST. Q (GPM)	SURF. ELEV. (FT.)		
40	1932	Modern Vegetable Nursery 15550 Washington San Leandro	Irrig.	?	350	340-350		12					24	
41	1920 Swan	Gualco 15325 Washington San Leandro	Irrig.	?	130			10					24	
42	1978 Wood Co.	Perry 15600 Lorenzo San Lorenzo	Irrig.	?	?									
43	1925 Nunes	Pianetta 915 Lewelling San Lorenzo	Irrig.	?	120	100-120		12					17	
44	Owner	Jones 983 Lewelling San Lorenzo	Irrig.	?	42	30-42		6					17	
45		Raele 15547 Sedgeham San Leandro	Irrig.	?	?									
46	1957 Owner	Pianetta 15388 Andover San Leandro	Irrig.	?	22			6					21	







EMCON WELL NUMBER	DATE DRILLED, DRILLER	WELL OWNER LISTED	STATUS IF KNOWN	WELL CONSTRUCTION DETAILS									EDITED DRILLER REPORTS	
				TOT. DPTH (FT.)	COMP. DPTH (FT.)	PERF. INTER. (FT.)	SEAL DPTH (FT.)	CASE DIA. (IN.)	CASE MAT.	WAT. LEV. (FT.)	EST. Q (GPM)	SURF. ELEV. (FT.)		
63	1946 Basset	Richols 3000 Halcolm	Domestic ?		197				10					
64	1937 Jet	San Leandro Moore 15241 Upton San Leandro	Irrig.	?	50	30-47		6					26	
65	1952 Owner	Crane 487 Lloyd San Leandro	Irrig	?	20			4					29	
66	1953 Owner	Wilson 15360 Dermody San Leandro	Irrig.	?	25			8					27	
67	1958 Owner	Cuimente 15508 Werner San Leandro	Irrig	?	20			6					28	
68	1935 Silva	Stewzel Sycamore San Leandro	Irrig	?	270			10					38	
69	? ?	Twin Nursery Washington Street San Leandro	Irrig	?	?								31	
70	? ?	Twin Nursery Washington St. San Leandro	Abandoned		?			8					30	

EMCON WELL NUMBER	DATE DRILLED, DRILLER	WELL OWNER LISTED	STATUS IF KNOWN	WELL CONSTRUCTION DETAILS								SURF. ELEV. (FT.)	EDITED DRILLER REPORTS
				TOT. DPTH (FT.)	COMP. DPTH (FT.)	PERF. INTER. (FT.)	SEAL DPTH (FT.)	CASE DIA. (IN.)	CASE MAT.	WAT. LEV. (FT.)	EST. Q (GPM)		
71	? ?	Gonzales 15559 Usher Irrig San Leandro		? ?	25							38	
72	1955 Owner	Maciel 15594 Sharon San Lorenzo	Irrig.	? ?	27			4				44	
73	1951 Western Well	Hayward Union High Irrig School Dist. San Lorenzo	Domestic	? ?	616			30/14				42	
74	1937 Swanson	Teel 624 Lewelling San Lorenzo	Domestic	? ?	75			8					
75	1949 Anderson	Ratti Lewelling Hesperian San Lorenzo	Domestic ? Irrig.	? ?	410								
76	? ?	Levy 646 Via Del Oro San Lorenzo	Irrig.	? ?	22			4				28	
77	1920 ?	Kino Nurs- ery 880 Lewelling San Lorenzo	Irrig	? ?	150			12				33	

EMCON WELL NUMBER	DATE DRILLED, DRILLER	WELL OWNER LISTED	STATUS IF KNOWN	WELL CONSTRUCTION DETAILS									
				TOT. DPTH (FT.)	COMP. DPTH (FT.)	PERF. INTER. (FT.)	SEAL DPTH (FT.)	CASE DIA. (IN.)	CASE MAT.	WAT. LEV. (FT.)	EST. Q (GPM)	SURF. ELEV. (FT.)	
		P. Duncan	Irrig.	?	?								
78	?	16089 Via Alamos											
	?	San Lorenzo											
		Avansino											
79	1951	1441	Irrig.	?	701			12				36	
		Bassett	Washington										
			San Leandro										
80	1951	Abansino	Irrig.	?	701							35	
	?	Mortenson Nursery Co.											
			14441 Washington										
			San Leandro										
81	1952	Abansino	Irrig.	?	701							32	
	?	Mortenson Nursery Co.											
			14441 Washington										
			San Leandro										
82	1937	Abansino	Irrig.	?	288			10				35	
	?	Mortenson Nursery Co.											
			14441 Washington										
			San Leandro										
83	?	Abansino	Irrig.	?	135			8/10				38	
	?	Mortenson Nursery Co.											
			14441 Washington										
			San Leandro										
84	1931	Abansino	Irrig.	?	235			12				34	
	?	Mortenson Nursery Co.											
			14441 Washington										
			San Leandro										

EDITED  
DRILLER REPORTS

EMCON WELL NUMBER	DATE DRILLED, DRILLER	WELL OWNER LISTED	STATUS IF KNOWN	WELL CONSTRUCTION DETAILS								
				TOT. DPTH (FT.)	COMP. DPTH (FT.)	PERF. INTER. (FT.)	SEAL DPTH (FT.)	CASE DIA. (IN.)	CASE MAT.	WAT. LEV. (FT.)	EST. Q (GPM)	SURF. ELEV. (FT.)
85	?	Abansino	Irrig.	?	254			12				
	?	Mortenson 14441 Wash San Leandro	Nursery Co.									
86	1931	Avansino	Irrig.	?	235			12				34
	?	Mortenson 14441 Wash San Leandro	Nursery Co.									
87	?	Avansino	Irrig.	?	135			12				
	?	Mortenson 14441 Wash San Leandro										
88	1956	Clark	Irrig.	?	30			6				
		Domestic Well	417 Bradrick San Leandro									
89	1930	Cardoza	Domestic	?	150			10				
	?	14700 Washington San Leandro	Irrig.									
90	?	Olsen	Irrig.	62	60							
		AAA Drill ing	14737 Harold San Leandro									
91	1951	K-Mart	Irrig.	?	701			12				35
		Bassett 14441 Wash San Leandro										

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92	1957	Graves	Irrig.	?	23			4					
	Owner	3894 Carmel San Leandro											
93	1958	Kirkland	Irrig.	?	19			4					
	Owner	883 Halycon San Leandro											
	1956	Grego	Irrig.	?	125			5				30	
	Murphy	3701 Monterey San Leandro											
95	?	Hastie											
	?	3712 Awravy	Irrig.	?	?								
		San Leandro											
96	1955	Thomas	Irrig.	?	29			4					
	Owner	3689 Figueroa San Leandro											
97	?	Bolesworth	Irrig.	?	?								
	?	1044 Marquette San Leandro											
98	1977	Spitznagle	Irrig.	?	38								
	?	1075 Tulane San Leandro											
99	1956	Smith	Irrig.	?	16			5					
	Owner	1227 Purdue San Leandro											

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DRILLER REPORTS

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100	1957 Owner	Hawks 1051 Tulane San Leandro	Irrig.	?	60			4				27
101	? ?	Tavis 1144 Avon San Leandro	Irrig.	?	?							
102	1977 ?	Brannon 1075 Avon San Leandro	Irrig.	?	36							
103	1957 Leite	Heisler 14861 Crosby San Leandro	Irrig.	?	37			6				
104	1952 Owner	Souza 1009 Cumberland San Leandro	Irrig.	?	27			6				
105	1977 ?	Friesen 324 Anza San Leandro	Domestic	?	84							
106	? Owner	Chuck 335 Aloha San Lorenzo	Irrig.	?	30			4				
107	1958 Owner	Calvao 830 Crespi San Leandro	Irrig.	?	23	15-23		5				

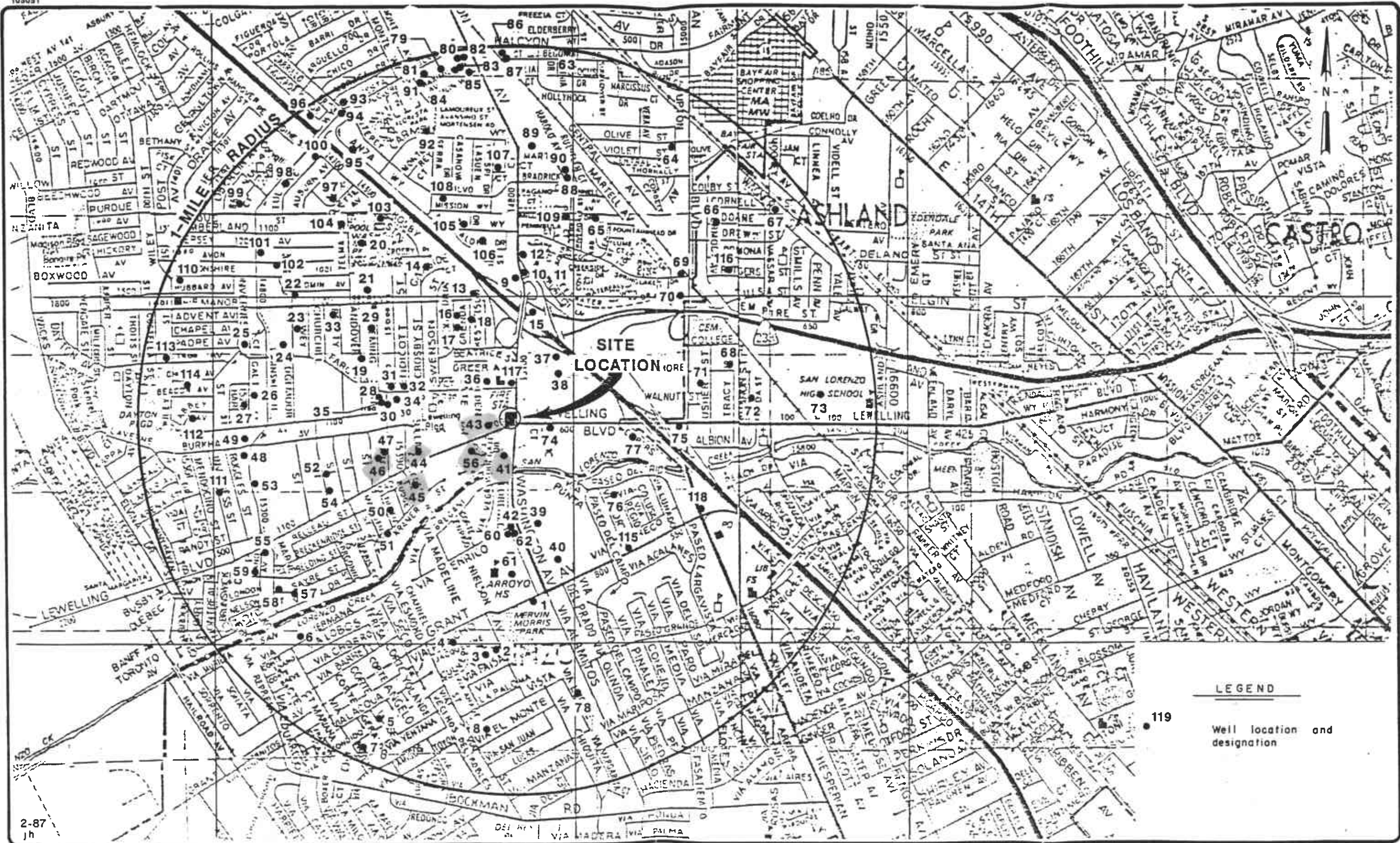
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108	1957 Owner	Payne 916 Sierra San Leandro	Irrig.	?	14									
109	1955 Owner	Davies 418 Lloyd San Leandro	Irrig.	?	28									
110	1977 ?	Brooks 1341 Devonshire San Leandro	Irrig.	?	?									
111	1977 ?	Henwood 15700 Inverness San Leandro	Irrig.	18	18									
112	1977 ?	Knupler 1439 Abbey San Leandro	Irrig.	25	25									
113	1977 ?	Tatman 15149 Wiley San Leandro	Irrig.	27	27									
114	1977 ?	Gietzen 1435 Church San Leandro	Irrig.	28	27									
115	1977 ?	Frink 754 Grant San Lorenzo	Irrig.	?	?									

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DRILLER REPORTS



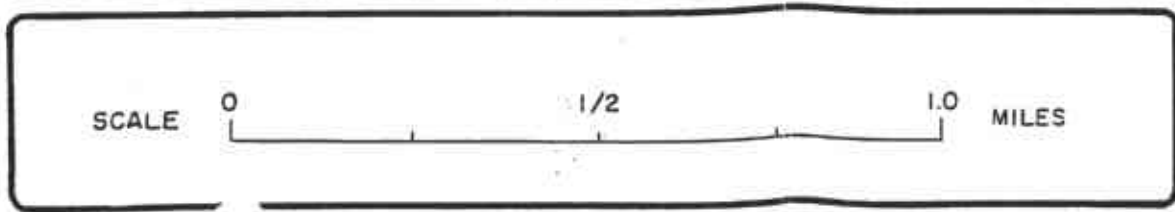


2-87  
jh

**LEGEND**

● Well location and designation

119



GETTLER-RYAN INC.  
SUBSURFACE HYDROGEOLOGIC INVESTIGATION  
SHELL SERVICE STATION, 15275 WASHINGTON AVE.  
SAN LORENZO, CALIFORNIA

WELL SURVEY MAP

FIGURE  
1  
PROJECT NO.  
738-08.03

**APPENDIX D**  
**FATE2 Model Parameters**

## Domenico's Model...

Assumes: uniform and constant aquifer properties, one dimensional groundwater flow, first-order contaminant decay, degradation, or transformation, constant contaminant source of rectangular cross-section in the plane perpendicular to groundwater flow.

Maximum Centerline Concentration at Steady-State:

$$\frac{C(x, y=0, z=0)}{C_{\text{source}}} = \exp\left\{\frac{x}{2\alpha_x} \left[1 - \left(1 + 4\lambda \frac{\alpha_x}{q}\right)^{1/2}\right]\right\} \left(\operatorname{erf}\left[\frac{Y}{4\sqrt{\alpha_y x}}\right]\right) \left(\operatorname{erf}\left[\frac{Z}{4\sqrt{\alpha_z x}}\right]\right)$$

$C(x,y,z)$	= solute concentration at location (x,y,z) [mg/l]
$C_{\text{source}}$	= solute concentration at (x=0,y=0,z=0) [mg/l]
$x$	= distance downgradient of source [ft]
$\alpha_x$	= $0.1x$ = longitudinal (x) dispersivity [ft]
$\alpha_y$	= $\alpha_x/3$ = transverse (y) dispersivity [ft]
$\alpha_z$	= $0.05 \alpha_x$ = vertical (z) dispersivity [ft]
$q$	= groundwater velocity (or specific discharge) [ft/d]
$\lambda$	= attenuation (degradation) coefficient [d <sup>-1</sup> ]
$Y$	= source width (perpendicular to groundwater flow in the horizontal plane) [ft]
$Z$	= source depth (perpendicular to groundwater flow in the vertical plane) [ft]
$\operatorname{erf}(h)$	= Error Function evaluated for value (h)

# Plume Attenuation Model: FATE2

## MODEL PARAMETER INPUT

### 1) Input Flow Model Parameters:

	<b>Input</b>	<b>Min</b>	<b>Max</b>
n - Porosity [ft <sup>3</sup> /ft <sup>3</sup> ]	<b>0.35</b>	0.25	0.6
K - Hydraulic Conductivity [ft/day]	<b>3</b>	0.0001	100
i - Groundwater Gradient [ft/ft]	<b>0.005</b>	0.001	0.01
lamda - attenuation rate [1/day]	<b>0.0025</b>	0.001	0.01
Mx - multiplier for longitudinal dispersivity [ $\alpha_x = Mx \cdot x$ ]	<b>0.1</b>	0.05	0.2
My - multiplier for transverse dispersivity [ $\alpha_y = My \cdot \alpha_x$ ]	<b>0.033 Min</b>	0.1	0.3333
Mz - multiplier for vertical dispersivity [ $\alpha_z = Mz \cdot \alpha_x$ ]	<b>0.005 Min</b>	0.0125	0.1

### 2) Input Source Data:

Cs - Source Concentration [mg/l]	<b>36</b>
Y - source width perpendicular to groundwater flow [ft]	<b>40</b>
Z - source depth below water table [ft]	<b>7</b>
L - farthest distance to be evaluated from source [ft]	<b>660</b>

### 3) Input Monitoring Point Data:

Monitoring Point	<b>1</b>	<b>2</b>	<b>3</b>
Cm - concentration at monitoring locations [mg/l]	<b>36</b>	<b>0.65</b>	<b>0.0024</b>
M - Distance to Monitoring Locations [ft]	<b>25</b>	<b>90</b>	<b>155</b>

### 4) Input Receptor Data:

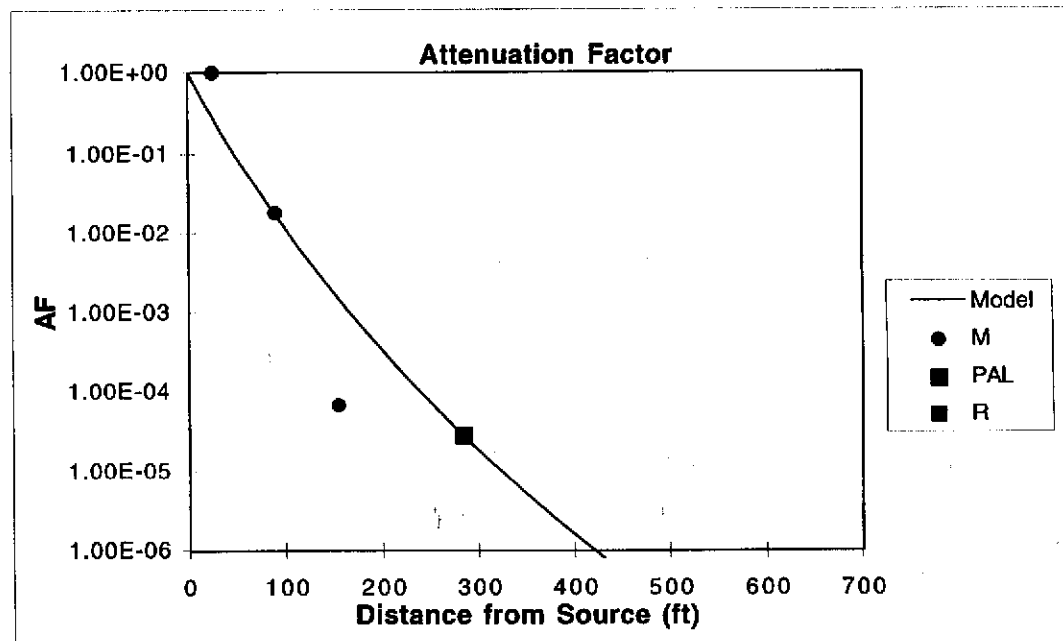
R - Distance to Nearest Receptor Location [ft]	<b>660</b>
Cgw* - Target Concentration [mg/l]	<b>0.001</b>

# Plume Attenuation Model: FATE2

## MODEL CALIBRATION

### 5) Run Calibration Macros

lamda - attenuation rate [1/day] (.001 - .01)	0.0025	(from cell B8)
Mx - multiplier for longitudinal dispersivity [ $\alpha_x = Mx \cdot x$ ] (0.1)	0.1000	(from cell B9)
AFm - attenuation factor at location m	1.00E+00	1.81E-02 6.67E-05
AFm* - modeled attenuation factor at location m	2.75E-01	1.73E-02 1.49E-03
(1-AFm*/AFm)^2	5.26E-01	1.71E-03 4.58E+02
Sum of Squares (1-AFm*/AFm)^2	4.58E+02	



## Plume Attenuation Model: FATE2

### MODEL OUTPUT

#### 6) Run Plume Attenuation Length Macro "PAL"

Cgw*/Cs - attenuation factor at target concentration	2.78E-05
(Cgw*/Cs - AFpal)/(Cgw*/Cs)	-9.78E-04

PAL - Plume Attenuation Length [ft]	284
PAL/L - Scaled Plume Attenuation Length	0.43
R - Distance to Nearest Receptor Location [ft]	660

#### 7) Receptor Attenuation

AFr - Attenuation Factor at Receptor	9.24E-09
Cr - Concentration at Receptor [mg/l]	3.33E-07
Cgw* - Target Concentration [mg/l]	0.001

#### 8) Input Contaminant Data

S - Solubility Limit of Contaminant (mg/l)	36.48 Benzene in Gasoline
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#### 9) Target Source Concentration

Cs* - Maximum Source Concentration [mg/l]	>S
Cs - Source Concentration [mg/l]	36



## Plume Attenuation Model: FATE2

### MODEL PARAMETER INPUT

#### 1) Input Flow Model Parameters:

	<u>Input</u>	<u>Min</u>	<u>Max</u>
n - Porosity [ft <sup>3</sup> /ft <sup>3</sup> ]	0.35	0.25	0.6
K - Hydraulic Conductivity [ft/day]	3	0.0001	100
i - Groundwater Gradient [ft/ft]	0.005	0.001	0.01
lamda - attenuation rate [1/day]	0.0015	0.001	0.01
Mx - multiplier for longitudinal dispersivity [alpha-x = Mx*x]	0.1	0.05	0.2
My - multiplier for transverse dispersivity [alpha-y = My*alpha-x]	0.033 Min	0.1	0.3333
Mz - multiplier for vertical dispersivity [alpha-z = Mz*alpha-x]	0.005 Min	0.0125	0.1

#### 2) Input Source Data:

Cs - Source Concentration [mg/l]	140
Y - source width perpendicular to groundwater flow [ft]	40
Z - source depth below water table [ft]	7
L - farthest distance to be evaluated from source [ft]	660

#### 3) Input Monitoring Point Data:

Monitoring Point	1	2	3
Cm - concentration at monitoring locations [mg/l]	140	1.1	0.59
M - Distance to Monitoring Locations [ft]	25	90	155

#### 4) Input Receptor Data:

R - Distance to Nearest Receptor Location [ft]	660
Cgw* - Target Concentration [mg/l]	0.05

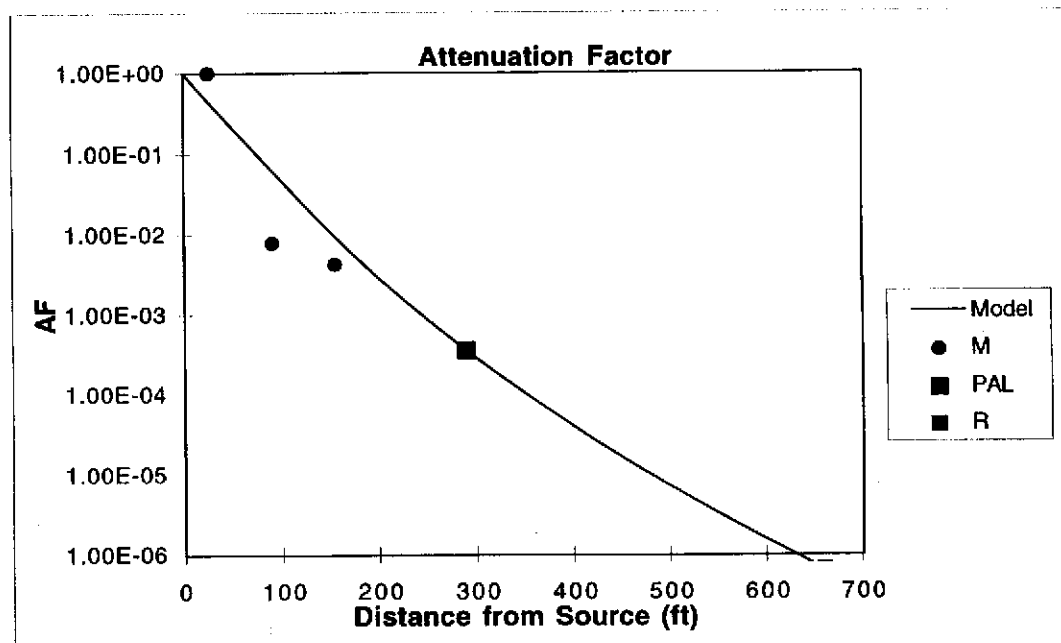
# Plume Attenuation Model: FATE2

## MODEL CALIBRATION

### 5) Run Calibration Macros

lamda - attenuation rate [1/day] (.001 - .01) 0.0015 (from cell B8)  
 Mx - multiplier for longitudinal dispersivity [ $\alpha_x = Mx \cdot x$ ] (0.1) 0.1000 (from cell B9)

AFm - attenuation factor at location m 1.00E+00 7.86E-03 4.21E-03  
 AFm\* - modeled attenuation factor at location m 4.45E-01 6.27E-02 9.41E-03  
 (1-AFm\*/AFm)^2 3.08E-01 4.87E+01 1.52E+00  
 Sum of Squares (1-AFm\*/AFm)^2 5.05E+01



## Plume Attenuation Model: FATE2

Cgw\*/Cs - attenuation factor at target concentration 3.57E-04  
(Cgw\*/Cs - AFpal)/(Cgw\*/Cs) 2.32E-04

PAL - Plume Attenuation Length [ft] 217  
PAL/L - Scaled Plume Attenuation Length 0.33  
R - Distance to Nearest Receptor Location [ft] 660

### 7) Receptor Attenuation

AFr - Attenuation Factor at Receptor 2.12E-07  
Cr - Concentration at Receptor [mg/l] 2.97E-05  
Cgw\* - Target Concentration [mg/l] 0.05

### 8) Input Contaminant Data

S - Solubility Limit of Contaminant (mg/l) 140.5 Gasoline

### 9) Target Source Concentration

Cs\* - Maximum Source Concentration [mg/l] >S  
Cs - Source Concentration [mg/l] 140