### **Ultramar**

ALG: HAZMĀT

Signature Signat

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November 21, 1994

Mr. Scott O. Seery, CHMM
Senior Hazardous Materials Specialist
Alameda County Health Care Services
80 Swan Way, Room 200
Oakland, CA 94621

SUBJECT: FORMER BEACON STATION NO. 574, 22315 REDWOOD ROAD, CASTRO VALLEY,

**CALIFORNIA** 

Dear Mr. Seery:

Enclosed is a copy of the Problem Assessment Report/Remedial Action Plan for the above-referenced Ultramar facility prepared by Acton, Mickelson van Dam, Inc. Please do not hesitate to call if you have any questions about this project at (209) 583-5571.

Sincerely,

ULTRAMAR INC.

Kenneth R. Earnest

Environmental Specialist II

Marketing Environmental Department

Enclosure:

Problem Assessment Report/Remedial Action Plan

cc w/encl:

Mr. Rich Hiett, San Francisco Bay Region, RWQCB

Mr. Peter J. Pugnale, Shell Oil Company

Mr. Paul A. Wilson, Property Owner



### 22315 REDWOOD ROAD CASTRO VALLEY, CALIFORNIA AMV PROJECT NO. 19021.03

November 10, 1994

Prepared By

ACTON • MICKELSON • van DAM, INC. 4511 Golden Foothill Parkway, Suite 1 El Dorado Hills, California 95762 (916) 939-7550

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Date	Date



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### 22315 REDWOOD ROAD CASTRO VALLEY, CALIFORNIA AMV PROJECT NO. 19021.03

#### 1.0 INTRODUCTION

Acton • Mickelson • van Dam, Inc. (AMV), has been authorized by Ultramar Inc. (Ultramar), to continue an ongoing hydrogeologic investigation at former Beacon Station No. 574 located at 22315 Redwood Road, Castro Valley, Alameda County, California (Figures 1 and 2). This report summarizes the results of previous hydrogeologic investigations conducted by other consultants as well as work recently completed by AMV. AMV's recommendations for future work are included in this report.

### 1.1 Site Background

The site is located at the intersection of Redwood Road and Grove Way in Castro Valley, 700 feet north of the southwestward-flowing San Lorenzo Creek. An unnamed creek (tributary to San Lorenzo Creek) is located approximately 500 feet north of the site. The elevation of the site is approximately 150 feet above mean sea level. Castro Valley is situated in the east San Francisco Bay Area, south of the San Leandro Hills and northwest of Walpert Ridge. Ground surface in the area of the site generally slopes toward the southwest. The site is bounded on the north by Grove Way and on the east by Redwood Road. The surrounding area is predominantly commercial properties.

A total of eight monitoring wells have been installed on or near the site by Delta Environmental Consultants, Inc. (Delta), and AMV since 1991. Ultramar leased the site and petroleum product storage and distribution facilities and operated a retail gasoline service station at this site from 1981 to 1987. Prior to 1981, the site had been leased and operated by Shell Oil Company (Shell). Information provided by Ultramar indicates that in 1987, when Ultramar ceased leasing the property, all underground storage tanks then in existence were removed. Available data indicate that at least one previous generation of tanks had been installed and used at the site by Shell. The first generation of tanks was removed prior to Ultramar's lease of the property in 1981. It is AMV's understanding that Ultramar is not aware of any specific incidents in which gasoline leaked from the former underground storage tanks or was spilled during filling of any of the tanks. The site is currently occupied by commercial businesses in separate suites within a single building (illustrated on Figure 2).

### 1.2 Regional Geologic and Hydrogeologic Setting

The site is located in Castro Valley, California, in the eastern San Francisco Bay Area. Ground water has been reported at depths of 15 to 25 feet below grade at the site. The surface of Castro

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Valley is covered with Quaternary, nonmarine alluvium (referred to as "older alluvium" and described as dissected terrace deposits), probably deposited by San Lorenzo Creek and its tributaries (Wagner, et al., 1991). Cretaceous marine sedimentary rocks, assigned to the Panoche Formation, underlie the alluvium in Castro Valley, and form the surrounding hills and ridges. The northwest-trending Hayward fault zone is present west of the site.

### 2.0 RESULTS OF PREVIOUS PHASES OF HYDROGEOLOGIC INVESTIGATION

### 2.1 Underground Storage Tank Removal

According to a work plan prepared by Ultramar dated January 12, 1993, all underground tanks were removed from the site on May 5, 1987. Underground storage had previously consisted of one 500-gallon waste oil tank, two 5,000-gallon diesel tanks, a 7,000-gallon gasoline tank, and an 8,000-gallon gasoline tank. Records made available by Ultramar indicate that these tanks were originally installed and owned by Shell. These tanks replaced a set of three underground storage tanks that were removed by Shell sometime prior to 1981, when Ultramar assumed the lease on the property. The results of soil samples collected at the time of tank removal indicated the presence of petroleum hydrocarbon constituents in soil underlying the tanks. Overexcavation of the tank basin to a depth of approximately 20 feet was performed on May 18, 1987. After overexcavation, three of the seven soil samples collected at the limit of the excavation contained total volatile hydrocarbons at concentrations of 125.5, 208.7, and 1,989 parts per million (ppm).

### 2.2 Soil Borings and Monitoring Well Installation

On March 26, 1991, three soil borings were advanced at the site to depths of approximately 30 feet below grade and completed as 4-inch-diameter ground water monitoring wells MW-1, MW-2, and MW-3 (Figure 2). Ground water was encountered in the borings for these wells at approximately 22 feet below grade. Soil borings containing descriptions of soil encountered as the borings were advanced are contained in Appendix A. Soil samples collected as the borings for monitoring wells MW-1 and MW-2 were advanced consisted of gravelly sand to a depth of 6.5 feet below grade, underlain by sandy clay or clayey sand to approximately 22 feet, and sand and silty sand to the total boring depth of 30 feet below grade (Appendix A).

Soil samples collected from the soil borings were submitted for laboratory analysis of benzene, toluene, ethylbenzene, xylenes (BTEX), total petroleum hydrocarbons as gasoline (TPHg), and total petroleum hydrocarbons as diesel (TPHd). The results are compiled in Table 1. None of the soil samples contained detectable concentrations of TPHd. The soil samples collected from above the water table in the boring for monitoring well MW-2 (near the northwest corner of the

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first generation underground storage tanks operated by Shell) contained detectable concentrations of TPHg. The samples collected from 10 and 15 feet below grade in this boring contained 8.1 and 3,200 ppm TPHg, respectively.

The monitoring wells were installed as described in well construction diagrams contained in Appendix B. Water level measurements made in monitoring wells MW-1, MW-2, and MW-3 on March 26 and April 1, 1991 (Table 2), indicated a direction of ground water flow toward the southwest. The gradient of ground water flow was approximately 0.015 foot per foot. Ground water samples collected from monitoring wells MW-1, MW-2, and MW-3 on April 1, 1991, did not contain detectable concentrations of TPHd. BTEX and TPHg were detected in water samples collected from these wells. Benzene concentrations ranged from 41 micrograms per liter ( $\mu$ g/l) in a sample from monitoring well MW-3 to 650  $\mu$ g/l in the sample collected from monitoring well MW-2 (Table 3).

Based on the results of installation of monitoring wells MW-1, MW-2, and MW-3, Ultramar prepared a work plan for installation of additional monitoring wells (Work Plan, Subsurface Environmental Investigation at Former Beacon Station No. 574, 22315 Redwood Road, Castro Valley, California, January 11, 1993). The work plan proposed installation of five additional ground water monitoring wells. The proposed work was executed by AMV after approval of Ultramar's work plan on May 13 and 18, 1993. AMV advanced and sampled five soil borings which were then converted to 2-inch-diameter monitoring wells MW-4, MW-5, MW-6, MW-7, and MW-8 (Figure 2).

Soil encountered by AMV in the boring for monitoring well MW-6 included silty clay from the surface to 8.5 feet below grade, silty sand between 8.5 and 14 feet below grade, silty clay beneath the silty sand to a depth of 19.5 feet, sandy silt between 19.5 and 27 feet below grade, and gravelly sand between 27 and 30 feet (the total depth of the boring). Ground water was encountered at about 20 feet below grade in the borings for monitoring wells MW-4 through MW-8. Soil boring logs for soil borings for monitoring wells MW-4 through MW-8 are contained in Appendix A.

AMV submitted a total of 23 soil samples for laboratory analysis of BTEX and TPHg. None of the samples collected from the borings for monitoring wells MW-4 through MW-8 contained detectable concentrations of petroleum constituents (Table 1).

AMV completed monitoring wells MW-4 through MW-8 as described on well construction diagrams contained in Appendix B. AMV measured depth to ground water in each existing monitoring well (MW-1 through MW-8) on May 18, 1993. Depth to ground water ranged from 15.72 to 22.66 feet below the top of the well casings (Table 2). AMV's water level measurements indicated a direction of ground water flow toward the southwest at a gradient of 0.01 foot per foot.

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AMV collected ground water samples for analysis from monitoring wells MW-4 through MW-8 only on May 18, 1993 (monitoring wells MW-1 through MW-3 had been sampled on May 7, 1993) for laboratory analysis of BTEX and TPHg. BTEX constituents were not present at detectable concentrations in ground water samples collected from monitoring wells MW-4 through MW-8 (Table 3). The sample collected from monitoring well MW-6 did contain 170  $\mu$ g/l TPHg.

The most recent quarterly monitoring event at the site was conducted on September 9, 1994, by Doulos Environmental and reported by Fugro, Inc. Depth to ground water on this date ranged from 16.87 feet below grade (MW-5) to 23.93 feet below grade (MW-1). The direction of ground water flow was generally toward the southwest (Figure 3) at a gradient of 0.01 foot per foot.

Analytical results of ground water samples collected in September 1994 indicate that BTEX constituents were detected only in samples collected from monitoring wells MW-1, MW-2, and MW-3 (the sample collected from monitoring well MW-6 contained 140  $\mu$ g/l TPHg). The inferred distribution of benzene in ground water on September 9, 1994, beneath the site is illustrated on Figure 4.

### 2.3 Hydrogeologic Testing Results

On January 31 and February 1 and 2, 1994, AMV conducted an aquifer test, an air sparging test, and a vapor extraction test using wells at the site. Starting on January 31, 1994, a 24-hour, continuous pumping test was conducted, using monitoring well MW-1 as the pumping well. The pumping rate throughout the test was maintained at approximately 0.25 gallon per minute (gpm). Water levels were recorded in the pumping well and monitoring well MW-2 using an automated data logger. Monitoring well MW-2 is located approximately 55 feet from MW-1. After 24 hours of pumping, a drawdown of approximately 4.2 feet was measured in the pumping well, and approximately 0.11 foot of drawdown was measured in monitoring well MW-2. Aquifer test analytical methods indicated a calculated hours of the pumping well), indicates a downgradient capture zone extent of approximately 17 feet, and a crossgradient capture zone width of approximately 110 feet, and a crossgradient capture zone width of approximately 110 feet, and a crossgradient capture zone width of approximately 110 feet, and a crossgradient capture zone width of approximately 110 feet, and a crossgradient capture zone width of approximately 110 feet, and a crossgradient capture zone width of approximately 110 feet, and a crossgradient capture zone width of approximately 110 feet, and a crossgradient capture zone width of approximately 110 feet, and a crossgradient capture zone width of approximately 110 feet, and a crossgradient capture zone width of approximately 110 feet, and a crossgradient capture zone width of approximately 110 feet, and a crossgradient capture zone width of approximately 110 feet, and a crossgradient capture zone width of approximately 110 feet, and a crossgradient capture zone width of approximately 110 feet, and a crossgradient capture zone width of approximately 110 feet, and a crossgradient capture zone width of approximately 110 feet, and a crossgradient capture zone width of approximately 110 feet, and a crossgradient capture zone width of approxim

The soil vapor extraction test was performed over a 4 hour period using monitoring well MW-1 as the extraction well. Pumping of ground water from monitoring well MW-1 was continued during the soil vapor extraction test to maximize the open screened area in this well during the test. The airflow rate during the test was approximately 43.6 standard cubic feet per minute (scfm). Throughout the vapor extraction test. AMV measured a vacuum influence of about 0.35 inch of water column at the stories well MW-2 the standard a zone of vacuum influence around monitoring well MW-1 with a radius of at least 55 feet. Air samples collected during the vapor extraction test contained 66 ppm benzene and 7,800 ppm TPHg at the start of the test

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and 42 ppm benzene and 4,500 ppm TPHg at the end of the test. The analytical and flow rate data indicate an initial extraction rate for TPHg of 67.7 pounds per day (Ibs/day). The estimated initial extraction rate for benzene was 0.57 lbs/day.

d Direction

An 8-hour sparge test was conducted by injecting air through a temporary sparge point installed approximately 15 feet from monitoring well MW-1. Air was injected at a rate ranging from 7.0 to 7.7 scfm. Dissolved oxygen, carbon dioxide (CO<sub>2</sub>), and TPHg concentrations in water and air from monitoring well MW-2 were monitored in the field and with samples collected for laboratory analysis during the test. Dissolved oxygen content in water samples collected from monitoring well MW-1 increased from 2.6 percent (sample collected before sparging began) to 6.5 percent (sample collected at the end of the sparge test). These measurements indicated that a sparge rate averaging approximately 7.4 scfm had an influence at the monitoring well MW-1.

#### 3.0 SUMMARY OF HYDROGEOLOGIC ASSESSMENT

#### 3.1 Distribution of Petroleum Constituents in Soil

Soil samples collected from the borings for monitoring wells MW-4, MW-5, MW-6, MW-7, and MW-8 did not contain detectable concentrations of petroleum constituents. Soil samples collected from the borings for monitoring wells MW-1 and MW-3 at 20 feet below grade contained detectable concentrations of petroleum constituents; however, these samples were collected within the zone of water table fluctuation and probably reflect the presence of these constituents in ground water rather than the presence of these constituents in the vadose zone above ground water. Only the samples collected from above the water table in the boring for monitoring well MW-2, located near or possibly adjacent to the tank basin of the first generation tanks operated by Shell, contained detectable concentrations of TPHg. Soil sample analytical results and the results of a vapor extraction test performed on monitoring well MW-1 indicate that only soil in the vicinity of the former underground storage tanks contains petroleurgy constituents.

AMV has constructed two soil cross-sections to illustrate the inferred distribution of petroleum constituents in soil underlying the site. The cross-section locations are illustrated in Figure 5 and the cross-sections appear on Figure 6 (A-A') and Figure 7 (B-B').

#### 3.2 Distribution of Petroleum Constituents in Ground Water

The direction of ground water flow beneath the site has been consistently toward the southwest. The ground water gradient has typically been 0.01 foot per foot.

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The distribution of petroleum constituents in ground water is defined upgradient, downgradient and crossgradient of the site. Ground water samples collected from monitoring wells MW-8 (upgradient), MW-5 (downgradient), and MW-4 (crossgradient) have historically not contained detectable concentrations of petroleum constituents. The only detection in samples from monitoring well MW-7 was TPHg at  $60 \mu g/l$  in March 1994 (Table 3). Ground water samples collected from monitoring well MW-6 have consistently contained TPHg at concentrations ranging from 78 to  $210 \mu g/l$ . BTEX constituents have generally not been detected in samples from monitoring well MW-6.

Ground water samples collected from monitoring wells MW-1, MW-2, and MW-3 have consistently contained detectable concentrations of petroleum constituents. Benzene concentrations have been highest in samples collected from monitoring well MW-2, ranging from 650 to 3,100  $\mu$ g/l. The most recent benzene distribution map (Figure 4) indicates ground water containing dissolved petroleum constituents is limited to the area of the former underground storage tanks, with some dispersion towards the north (MW-3). The nearest monitoring wells at off-site locations do not contain dissolved benzene.

#### 4.0 DISCUSSION OF REMEDIATION ALTERNATIVES

As discussed in Section 3, the delineation of petroleum constituents in soil and ground water beneath the site appears to be complete. The extent of migration of ground water containing these constituents is defined. This section outlines as interim course of action for the remediation of soil and ground water underlying the site which contain petroleum constituents. The remediation activities discussed in this section have three goals:

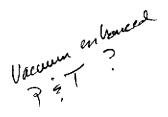
- Continued verification that ground water containing dissolved petroleum constituents has not migrated toward potential ground water users or surface water bodies.
- 2. Removal of petroleum constituents from ground water underlying the site.
- 3. Removal of petroleum constituents from soil underlying the site.

### 4.1 Removal of Petroleum Constituents from Ground Water

Strategies considered for interim remediation of ground water containing dissolved petroleum constituents include:

- Passive Remediation
- Ground Water Pumping and Aboveground Treatment

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- Vapor Extraction
- Vapor Extraction with Air Sparging

### 4.1.1 Passive Remediation

Passive remediation relies on existing natural processes to restrict migration of ground water containing dissolved petroleum constituents and remove these constituents from ground water. Continued volatilization and biodegradation of petroleum constituents in ground water and soil within the zone of water table fluctuation would be expected to reduce concentrations of these constituents with time. The available data indicate that natural mechanisms (including the relatively flat ground water gradient) are operating to restrict movement of ground water and/or the petroleum constituents in ground water. The pumping test results indicated a calculated & 3 x 10 - FH 5 hydraulic conductivity (K) value of 0.005 foot/min. The ground water gradient beneath the site 2.54 x105 ms is approximately 0.01 foot per foot. Using these values, an average linear ground water velocity selt/selts same of between 0.21 and 0.29 foot per day can be calculated (the lower velocity assumes a value for effective porosity of 0.35; the higher value assumes a value for effective porosity of 0.25). Using the lower velocity, petroleum constituents (including BTEX) would travel the distance from the former underground storage tanks to monitoring well MW-6 (approximately 80 feet) in approximately 380 days, or just over 1 year. With the higher velocity, petroleum constituents would reach MW-6 in just over 9 months. BTEX constituents have not yet reached MW-6, and the station ceased operation in early 1987, more than 7 years ago. It is likely that the release of petroleum constituents at the site took place sometime prior to 1987. This indicates that natural meghanisms are now acting and have previously acted to retard the movement of these constituents downgradien DO conc. ?

If this option is selected, it would be necessary to continue the existing ground water monitoring program (although the sampling interval or number of wells monitored could be modified) to verify that the historically slow rates of migration of petroleum constituents will continue. A change in existing conditions (drastic water level changes or local pumping of ground water) may warrant reevaluation of this alternative.

### 4.1.2 Ground Water Pumping and Aboveground Treatment

This remediation alternative involves recovery of ground water by pumping from one or more extraction wells. After aboveground treatment, possibilities for disposal of the ground water include discharge to the sanitary or storm sewer.

Implementation of ground water pumping constitutes a method for both controlling the migration of and removing petroleum constituents from ground water beneath the site. The pumping test on monitoring well MW-1 described in Section 2.3 indicates that this well will yield approximately 0.25 gpm (or less) on a long-term, continuous basis. The short-term empirical

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extent of the capture zone resulting from this pumping rate was about 110 feet crossgradient and 17 feet downgradient of the pumping well. Sustained, continuous pumping may be expected to result in a larger capture zone.

In general, implementation of ground water pumping by itself is not a time-effective remedial technique. At many sites, multi-year operation of ground water pumping alone has still not resulted in satisfactory remediation of ground water containing petroleum constituents. At sites where ground water flow velocities are high and off-site migration of ground water containing petroleum constituents represents a risk to potential receptors, ground water pumping can provide a positive means of controlling migration. At this site, ground water monitoring over the last 2 years does not indicate a rapid rate of migration, and the current monitoring well network indicates the distribution of petroleum constituents does not threaten potential receptors.

Drawbacks to implementing ground water pumping at this site include the cost to design, permit, construct, operate, monitor, and maintain a system. The treatment of the ground water results in removal of petroleum constituents either by adsorption onto carbon or air stripping and discharge to the atmosphere. In either case, the constituents removed from ground water must be disposed of in some manner, creating another potential source of contamination. The treated ground water must then be discharged to the sanitary sewer (if allowed) or to the storm sewer (surface waters). Either situation creates the possibility of accidental discharge of ground water containing residual petroleum constituents. Ground water pumping (even at low rates) disrupts the ambient flow conditions and can potentially result in migration of ground water impacted by off-site sources onto the former Beacon/Shell site.

### 4.1.3 Vapor Extraction

Though typically considered a soil remediation technology, utilization of vapor extraction for removing dissolved hydrocarbons from ground water can be viable under certain conditions. A vapor extraction system operates on the concepts of vapor-liquid equilibrium and vapor flow through soil. Upon applying vacuum to the soil overlying the water table, the reduced pressure in the overlying soil vapor causes the volatile hydrocarbons dissolved in ground water to move from the liquid to the vapor phase. The induced vacuum extraction flow above the water table surface removes the hydrocarbon-enriched vapors. Because the vapor extraction flow continually removes the hydrocarbons that migrate from the ground water into the soil vapor, a state of disequilibrium exists. The volatilization of dissolved hydrocarbons from the ground water into the overlying soil vapor will continue as the system moves toward equilibrium.

In addition, vapor extraction can promote natural biodegradation of dissolved hydrocarbons by providing a continual source of fresh oxygen to stimulate indigenous microorganisms, which convert the hydrocarbons to carbon dioxide and water. At the same time, vapor extraction

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would be removing the hydrocarbons in the soil above the water table that presumably impacted ground water in the past, and could potentially impact ground water again. A possible limitation of vapor extraction is inability to control migration of dissolved hydrocarbons in ground water.

Disadvantages of this method are principally the costs associated with design, permitting, installation, maintenance, monitoring, and operation of the vapor extraction system. In addition, as with ground water extraction, petroleum constituents extracted with soil vapors would need to be discharged to the atmosphere or collected in carbon canisters through adsorption, with the attendant disposal difficulties.

### 4.1.4 Vapor Extraction With Air Sparging

The use of air sparging can enhance the effectiveness of vapor extraction for removing dissolved hydrocarbons from ground water. Sparging air into the water table within the zone of influence of vapor extraction wells can speed remediation by means of air stripping dissolved hydrocarbons from the ground water as the air passes through the ground water enroute to the vapor extraction wells. Furthermore, introduction of air via sparging would provide additional oxygen for enhancing the biologic breakdown of hydrocarbon compounds in the subsurface. With strategically located sparge points, air sparging has the additional possible benefit of controlling the migration of ground water containing dissolved hydrocarbons.

The disadvantages of this method are: the costs associated with design, permitting, installation, maintenance, monitoring, and operation of the vapor extraction system. In addition, petroleum constituents extracted with soil vapors would need to be discharged to the atmosphere or collected in carbon canisters through adsorption, with the attendant disposal difficulties and the potential for contact during waste handling and transport. It is also possible for the physical process of air sparging to result in creation of localized ground water mounds, which could potentially result in undesirable movement of the dissolved petroleum constituent plume in ground water.

#### 4.2 Removal of Petroleum Constituents From Soil

Strategies considered for removing petroleum hydrocarbons from soil underlying the site include:

- Passive Remediation
- Soil Vapor Extraction

### 4.2.1 Passive Remediation

This alternative involves leaving the petroleum constituents in the soil and leaving the soil unaltered. Continuing natural volatilization and biodegradation of petroleum constituents in soil

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would be expected to reduce concentrations of petroleum constituents with time. The available data indicate that these natural agents have already attenuated the hydrocarbon impact to a certain degree.

While this method will take substantially longer than more active remedial strategies, low cost. Possess and low large than more active remedial strategies, low cost. and low impactato, properly use make it amontive at sitematic configurable solds. potential for receptor contact with impacted soil and ground water is low. As discussed in Section 3, this site falls in this category. If this option is selected, it would be necessary to continue the existing ground water monitoring program (although the sampling interval or number of wells monitored could be modified) to verify that the historically minor impacts to ground water due to migration of petroleum constituents from soil do not increase. A change in existing conditions (drastic water level changes or disturbance of the subsurface due to construction) may warrant reevaluation of this alternative.

### 4.2.2 Soil Vapor Extraction

Soil vapor extraction utilizes a vapor extraction well (or wells) to remove volatile hydrocarbons from the soil matrix. A vacuum applied to the extraction well results in the removal of soil vapors from the subsurface, accompanied by volatilization of petroleum constituents out of the soil matrix. Depending on the concentration levels of hydrocarbons entrained in the extracted vapor, the extracted soil vapors are either discharged directly to the atmosphere or treated before discharge to the atmosphere. The treatment would destroy or remove hydrocarbons from the discharged air in accordance with the local regulatory agency air discharge requirements. Extraction rates vary with the consistency, moisture content, and grain size of the soil horizon. In addition to the extraction benefit, soil venting can also be effective at promoting biologic breakdown of petroleum hydrocarbon compounds contained in soil and ground water by the introduction of additional oxygen into the subsurface.

The vacuum radius of influence and initial recovered petroleum constituent concentrations noted during the soil vapor extraction test (Mextion 2.3) indicated the reprinciples of the Technology would remove petroleum constituents from soil at this site. The site of this method are principally economic: the costs associated with design, permitting, installation, maintenance, monitoring, and operation of the vapor extraction system. In addition, as with ground water extraction, petroleum constituents extracted with soil vapors would need to be discharged to the atmosphere or collected in carbon canisters through adsorption, with the attendant disposal difficulties.

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5.0 RECOMMENDATIONS FOR INTERIM REMEDIATION

Based on data compiled for this site and the discussion of remedial alternatives in Section 4. AMV recommends that passive remediation of both soil and ground water be allowed to continue at the site. The existing assessment, testing, and monitoring data do not indicate an imminent threat to potential receptors nor that the distribution of dissolved petroleum constituents in ground water extends beyond the existing monitoring well network. AMV proposes that the existing monitoring program (in a modified version - see below) be continued to verify that migration of ground water containing petroleum constituents beyond the existing downgradient monitoring wells is not occurring. If the monitoring indicates that migration is occurring, or ground water or site use conditions change, reevaluation of the proposed interim remedial method may be warranted.

Charterly monitoring of existing monitoring wells MW-1 MW-2 MW-3 MW-3 and Market will be sufficient to detect changes in the maintaine of migraphotics and the particle of the remaining mentioning and the maintaine of the remaining mentioning and the market man closs may upgradient directions.

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6.0 REFERENCES

Wagner, D. L., E. J. Bortogno, and R. D. McJunkin. 1991. "Geologic Map of the San Francisco-San Jose Quadrangle, California, 1:250,000," California Department of Conservation, Division of Mines and Geology, Map No. 5A.

#### 7.0 REMARKS

The opinions and conclusions contained in this report represent our professional opinions. These opinions are based in part, on information provided by the client and were developed in accordance with currently accepted hydrogeologic and engineering practices at this time and location. Other than this, no warranty is implied nor intended.

TABLE 1

### SAMPLE ANALYTICAL RESULTS

Former Beacon Station #574

22315 Redwood Road, Castro Valley, California

(concentrations in

Monitoring Well	Date Sampled	Depth Sampled (feet)		Toluene	Ethylbenzene	Xylenes		ТРН₫⁵
MW-1	03-26-91	15	0.16	0.10	0.010	0.050	<1.0	<10
	03-26-91	<b>20</b>	13	110	<b>33</b>	<b>300</b>	<b>3,200</b>	<10
MW-2	03-26-91 03-26-91 03-26-91	10 15 20	0.013 19 0.39 *	0.26 120 h 0.22	0.11 42 0.11	0.68 <b>240 %</b> 0.41	8.1 3,200	<10 <10 <10
MW-3	03-26-91	15	<0.005	<0.005	<0.005	<0.005	<1.0	<10
	03-26-91	<b>20</b>	<0.005	0.18	0.44	5.9	<b>230</b>	<10
MW-4	05/14/93	5	<0.0050	<0.0050	<0.0050	<0.0050	<0.50	NA
	05/14/93	15	<0.0050	<0.0050	<0.0050	<0.0050	<0.50	NA
	05/14/93	20	<0.0050	<0.0050	<0.0050	<0.0050	<0.50	NA
MW-5	05/14/93	5	<0.0050	<0.0050	<0.0050	<0.0050	<0.50	NA
	05/14/93	10	<0.0050	<0.0050	<0.0050	<0.0050	<0.50	NA
	05/14/93	15	<0.0050	<0.0050	<0.0050	<0.0050	<0.50	NA
	05/14/93	20	<0.0050	<0.0050	<0.0050	<0.0050	<0.50	NA
MW-6	05/14/93	5	<0.0050	<0.0050	<0.0050	<0.0050	<0.50	NA
	05/14/93	10	<0.0050	<0.0050	<0.0050	<0.0050	<0.50	NA
	05/14/93	15	<0.0050	<0.0050	<0.0050	<0.0050	<0.50	NA
	05/14/93	20	<0.0050	<0.0050	<0.0050	<0.0050	<0.50	NA
MW-7	05/14/93	5	<0.0050	<0.0050	<0.0050	<0.0050	<0.50	NA
	05/14/93	10	<0.0050	<0.0050	<0.0050	<0.0050	<0.50	NA
	05/14/93	15	<0.0050	<0.0050	<0.0050	<0.0050	<0.50	NA
	05/14/93	20	<0.0050	<0.0050	<0.0050	<0.0050	<0.50	NA
MW-8	05/14/93	5	<0.0050	<0.0050	<0.0050	<0.0050	<0.50	NA
	05/14/93	10	<0.0050	<0.0050	<0.0050	<0.0050	<0.50	NA
	05/14/93	15	<0.0050	<0.0050	<0.0050	<0.0050	<0.50	NA
	05/14/93	20	<0.0050	<0.0050	<0.0050	<0.0050	<0.50	NA

<sup>\*</sup>TPHg = Total petroleum hydrocarbons as gasoline.

bTPHd = Total petroleum hydrocarbons as diesel.

TABLE 2

# WATER LEVEL DATA Former Beacon Station #574 22315 Redwood Road, Castro Valley, California

Monitoring Well	Date	Reference Elevation (feet)	Depth to Ground Water (feet)	Ground Water Elevation (feet)	Depth to Top of Screen (feet)	Well Depth (feet)
<u> </u>		yang ang ata yana ya diga at yana diga at sana ananang		Single Commence		**************************************
MW-1	03-26-91	156.55	22.43	134.12	10	NM NM
	04-01-91		22.37	134.18		NM NM
	03-27-92		22.43	134.12		NM
	06-04-92		23.4	133.15		NM NM
	09-23-92		24.07	132.48		29.33
	11-12-92		24.16	132.39 134.68		29.80
	02-02-93 05-07-93		21.87 22.58	133.97		29.84
	05-07-93		22.66	133.89		NM
	08-11-93		23.41	133.14		29.81
	11-05-93		24.09	132.46		29.81
•	03-01-94		22.76	133.79		29.85
	06-02-94		23.22	133.31		29.85
ļ	09-09-94		23.93	132.62		29.86
MW-2	03-26-91	155.17	20.91	134.26	10	NM
IVI VV -2.	03-20-91	133.17	20.82	134.35	10	NM
	03-27-92		20.82	134.35		NM
	06-04-92		21.81	133.36		NM
	09-23-92		22.45	132.72		NM
	11-12-92		22.6	132.57		29.71
	02-02-93		20.28	134.89		29.73
	05-07-93		20.97	134.20		29.73
	05-18-93		21.06	134.11		NM
	08-11-93		21.85	133.32		29.70
	11-05-93		22.32	132.85		29.70
	03-01-94		21.19	133.98		29.68
	06-02-94		21.59	133.58		29.69
	09-09-94		22.33	132.84		29.66
MW-3	03-26-91	157.13	21.62	135.51	10	NM
	04-01-91		21.55	135.58		NM
	03-27-92		21.46	135.67		NM
	06-04-92		22.34	134.79		NM
	09-23-92		22.84	134.29		NM
	11-12-92		23.04	134.09		29.55
	02-02-93		21.03	136.10		29.45
	05-07-93		21.59	135.54		29.53
	05-18-93		21.73	135.40		NM
	08-11-93		22.31	134.82		29.41
	11-05-93		22.85	134.28		29.41
	03-01-94		21.97	135.16	1	29.55
<b> </b>	06-02-94		22.29	134.84		29.56
	09-09-94		22.91	134.22		29.56

### TABLE 2 (continued)

# WATER LEVEL DATA Former Beacon Station #574 22315 Redwood Road, Castro Valley, California

Monitoring Well	Date	Reference Elevation (feet)	Depth to Ground Water (feet)	Ground Water Elevation (feet)	Depth to Top of Screen (feet)	Well Depth (feet)
MW-4	05-18-93	151.96	17.55	134.41 134.46	13	NM 28.43
	08-11-93 11-05-93		17.50 15.84	134.46		28.43
	03-01-94		17.35	134.61		28.11
	06-02-94		17.68	134.28		28.12
	09-09-94		18.19	133.77		28.13
MW-5	05-18-93	148.68	15.72	132.96	10	NM
	08-11-93		16.42	132.26		25.43
	11-05-93		16.92	131.76		25.43
	03-01-94		15.54	133.14		25.00
	06-02-94		16.19	132.49		25.00
	09-09-94		16.87	131.81		25.00
MW-6	05-18-93	153.96	20.80	133.16	15	NM
	08-11-93		21.64	132.32		31.15
	11-05-93		22.11	131.85	i	31.15
	03-01-94		20.80	133.16		29.96 29.98
	06-02-94		21.37	132.59 131.91		29.96
	09-09-94		22.05			
MW-7	05-18-93	156.09	22.64	133.45	15	NM
	08-11-93		23.25	132.84		30.75
	11-05-93		23.93	132.16		30.75 30.11
	03-01-94		22.72	133.37 132.87	1	30.11
	06-02-94 09-09-94		23.22 23.90	132.19		30.12
		450.04			10	NM
MW-8	05-18-93	158.04	21.55	136.49	18	NM 34.82
	08-11-93		22.43 23.00	135.61 135.04		34.82 34.82
	11-05-93 03-01-94		23.00	135.04		34.04
	05-01-94		22.29	135.75		34.04
	09-02-94		22.99	135.05		34.04

\*TPHg = Total petroleum hydrocarbons as gasoline.

bTPHd = Total petroleum hydrocarbons as diesel.

TABLE 3

GROUND WATER SAMPLE ANALYTICAL RESULTS
Former Beacon Station #574

22315 Redwood Road, Castro Valley, California

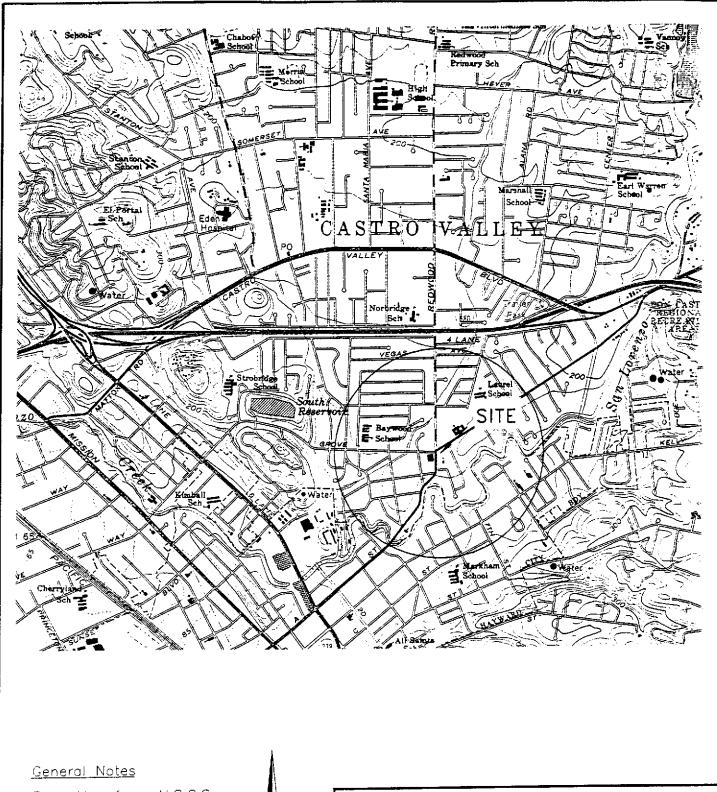
		0.0000000000000000000000000000000000000						Motor
Monitoring Well	Date Sampled	Веплепе	Toluene	Ethylbenzene	Xylenes	TPHg*	TPHdb	Oil
	-				Contract Medical Contract Contract		< 100	NA
MW-1	04-01-91 03-27-92	2	570 900	76 230	460	A salar	<50	<50
	l				1,100 440	3	< 800	NA
	06-04-92 09-23-92		57 430	230	550	4	NA	NA NA
		5.8	<5.0	110	330 340	42,34	NA NA	NA NA
	11-12-92 02-02-93	7 <b>6</b> 0	770	140 250	1,200	2.7000 0.5000	NA NA	NA NA
	02-02-93	970	630	280	1,500		NA NA	NA NA
					•	1 1 (1000)	NA NA	NA NA
	08-11-93	1,400	1,000	260	1,600	11,000	NA NA	NA NA
	11-05-93	6,200	4,700	1,400	7,100	36,000 3,8 <b>6</b> 0		NA NA
	03-01-94	580	490	110	620		NA NA	NA NA
	06-02-94	1,900	1,200	420	2,100 630	3,900	NA NA	NA NA
	09-09-94	749	290	200	630	##30E4	NA	NA
MW-2	04-01-91	650	640	150	960	io, este	< 100	NA
	03-27-92	2,400	2,300	870	3,300	14,000	< 50	< 50
	06-04-92	1,900	1,700	580	2,300	144	< 5,000	NA
	09-23-92	2,100	1,500	760	2,900	244	NA	NA
	11-12-92	2,400	860	540	3,500	<b>A</b>	NA	NA
	02-02-93	2,700	1,900	590	2,600	2.40	NA.	NA
	05-07-93	1,800	1,300	460	2,600	184,0000	NA	NA
	08-11-93	2,300	1,500	550	2,300	23,000	NA	NA
	11-05-93	3,100	2,900	860	3,700	<b>38</b> 0,000	NA	NA
	03-01-94	1,500	490	350	1,000	12,000	NA	NA
	06-02-94	2,000	790	460	13,000	12,000	NA	NA
	09-09-94	1,800	660	440	1,000	13,000	NA	NA
MW-3	04-01-91	41	91	37	420	9.00	<100	NA.
	03-27-92	9.2	4.8	10	23	9.00	< 50	< 50
j	06-04-92	7.5	2.7	0.5	15	180	< 50	NA
	09-23-92	8.3	4.3	6.2	19	220	NA	NA
İ	11-12-92	12	5.5	7.7	19	2370	NA	NA
	02-02-93	2.4	0.71	2.7	6.2	* \$6	NA	NA
l	05-07-93	2.6	1.2	3.9	8.4	140	NA	NA
	08-11-93	15	8.1	14	37	490	NA	NA
	11-05-93	45	24	34	93	820	NA	NA
	03-01-94	7.4	2.7	5.6	10	410	NA	NA
	06-02-94	13	4.9	14	31	440	NA	NA
	09-09-94	168	4.8	9.7	20	<b>62</b> 0	NA	NA

### TABLE 3 (continued)

### GROUND WATER SAMPLE ANALYTICAL RESULTS Former Beacon Station #574 22315 Redwood Road, Castro Valley, California

Monitoring Well	Date Sampled	Benzene	Toluene	Ethylbenzene	Xylenes	TPHg*	TPHd <sup>*</sup>	Mator Oil
MW-4	05-18-93	< 0.5	< 0.5	<0.5	< 0.5	< 50	NA	NA
	08-11-93	< 0.5	< 0.5	< 0.5	< 0.5	< 50	NA	NA
	11-05-93	< 0.5	< 0.5	< 0.5	< 0.5	< 50	NA	NA
	03-01-94	< 0.5	< 0.5	< 0.5	< 0.5	< 50	NA	NA
	06-02-94	< 0.5	< 0.5	<0.5	< 0.5	< 50	NA	NA
	09-09-94	< 0.5	< 0.5	<0.5	< 0.5	< 50	NA	NA
MW-5	05-18-93	< 0.5	< 0.5	<0.5	< 0.5	< 50	NA	NA
	08-11-93	< 0.5	< 0.5	< 0.5	< 0.5	< 50	NA	NA
	11-05-93	< 0.5	< 0.5	< 0.5	< 0.5	< 50	NA	NA
	03-01-94	< 0.5	< 0.5	< 0.5	< 0.5	< 50	NA	NA
	06-02-94	< 0.5	< 0.5	< 0.5	< 0.5	< 50	NA	NA
	09-09-94	< 0.5	< 0.5	< 0.5	< 0.5	< 50	NA	NA
MW-6	05-18-93	< 0.5	<0.5	<0.5	< 0.5	120	NA	NA
	08-11-93	< 0.5	< 0.5	< 0.5	< 0.5		NA	NA
	11-05-93	< 0.5	< 0.5	< 0.5	0.65	<b>(70</b> )	NA	NA
	03-01-94	< 0.5	< 0.5	< 0.5	< 0.5	110	NA	NA
	06-02-94	< 0.5	< 0.5	< 0.5	< 0.5	190	NA	NA
	09-09-94	< 0.5	< 0.5	<0.5	< 0.5	MD.	NA	NA
MW-7	05-18-93	< 0.5	< 0.5	< 0.5	< 0.5	< 50	NA	NA
	08-11-93	< 0.5	< 0.5	< 0.5	< 0.5	< 50	NA	NA
	11-05-93	< 0.5	< 0.5	< 0.5	< 0.5	68	NA	NA
	03-01-94	< 0.5	< 0.5	< 0.5	< 0.5	< 50	NA	NA
	06-02-94	< 0.5	< 0.5	< 0.5	< 0.5	< 50	NA	NA
	09-09-94	< 0.5	< 0.5	<0.5	< 0.5	< 50	NA	NA
MW-8	05-18-93	< 0.5	< 0.5	< 0.5	< 0.5	< 50	NA	NA
	08-11-93	< 0.5	< 0.5	< 0.5	< 0.5	< 50	NA	NA
	11-05-93	< 0.5	< 0.5	< 0.5	< 0.5	< 50	NA	NA
	03-01-94	< 0.5	< 0.5	< 0.5	< 0.5	< 50	NA	NA
	06-02-94	< 0.5	< 0.5	< 0.5	< 0.5	< 50	NA	NA
	09-09-94	< 0.5	< 0.5	< 0.5	< 0.5	< 50	NA	NA

<sup>a</sup>TPHg = Total petroleum hydrocarbons as gasoline. <sup>b</sup>TPHd = Total petroleum hydrocarbons as diesel.



Base Map from U.S.G.S. Hayward, California 7.5 Minute Topographic Photorevised 1980



O 2,000

Approximate Scale (in feet)

### FIGURE 1

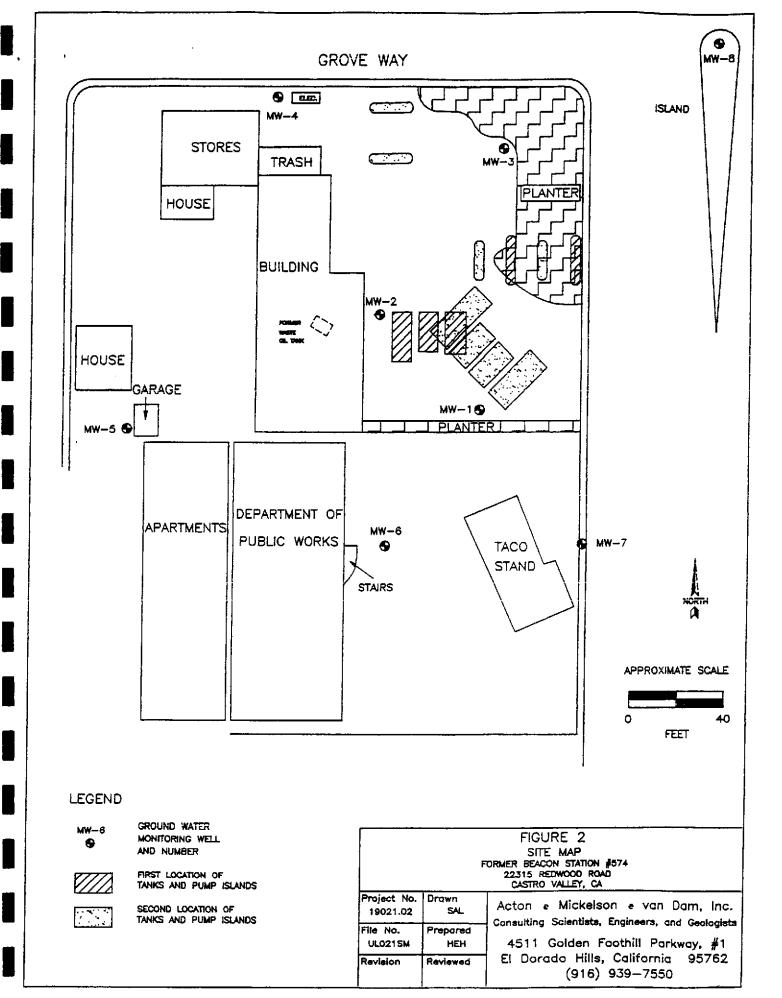
SITE LOCATION MAP FORMER BEACON STATION #574 22315 REDWOOD ROAD CASTRO VALLEY, CALIFORNIA

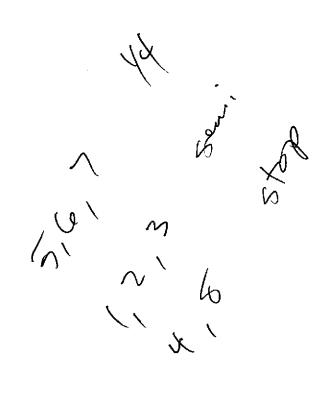
Project No.	Drawn
19021.02	DA
File No.	Prepared
FIG1	SAL
Revision	Reviewed
i	t

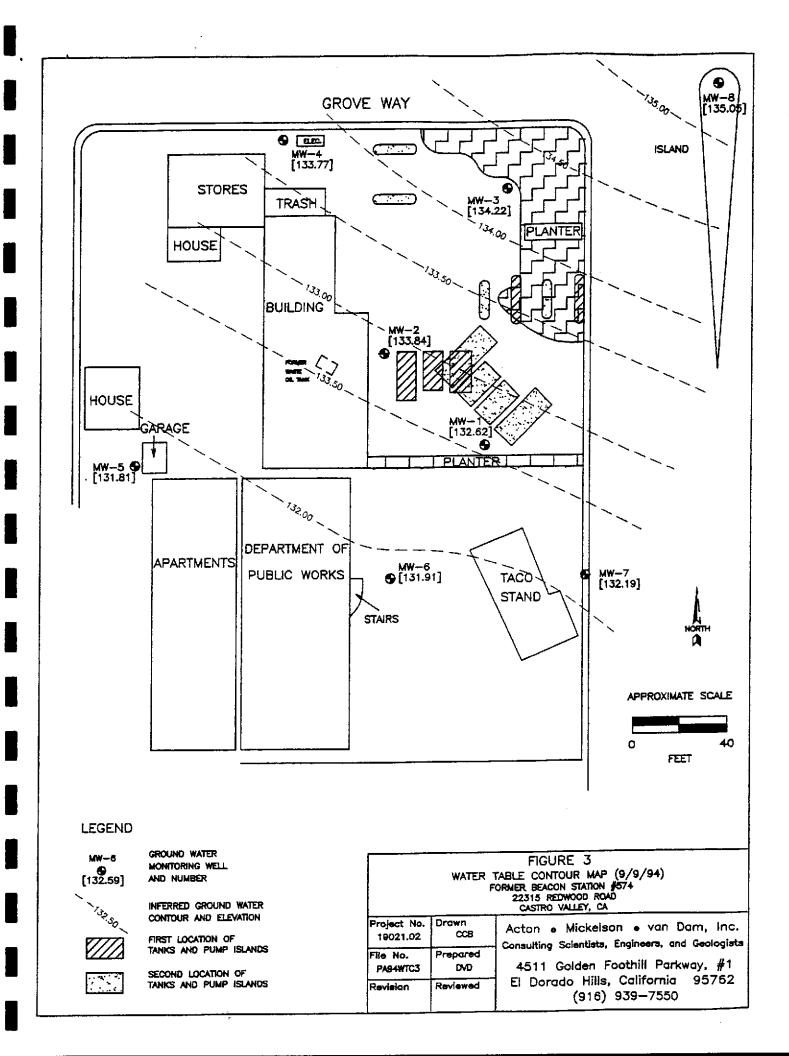
Acton • Mickelson • van Dam, Inc.
Consulting Scientists, Engineers, and Geologists

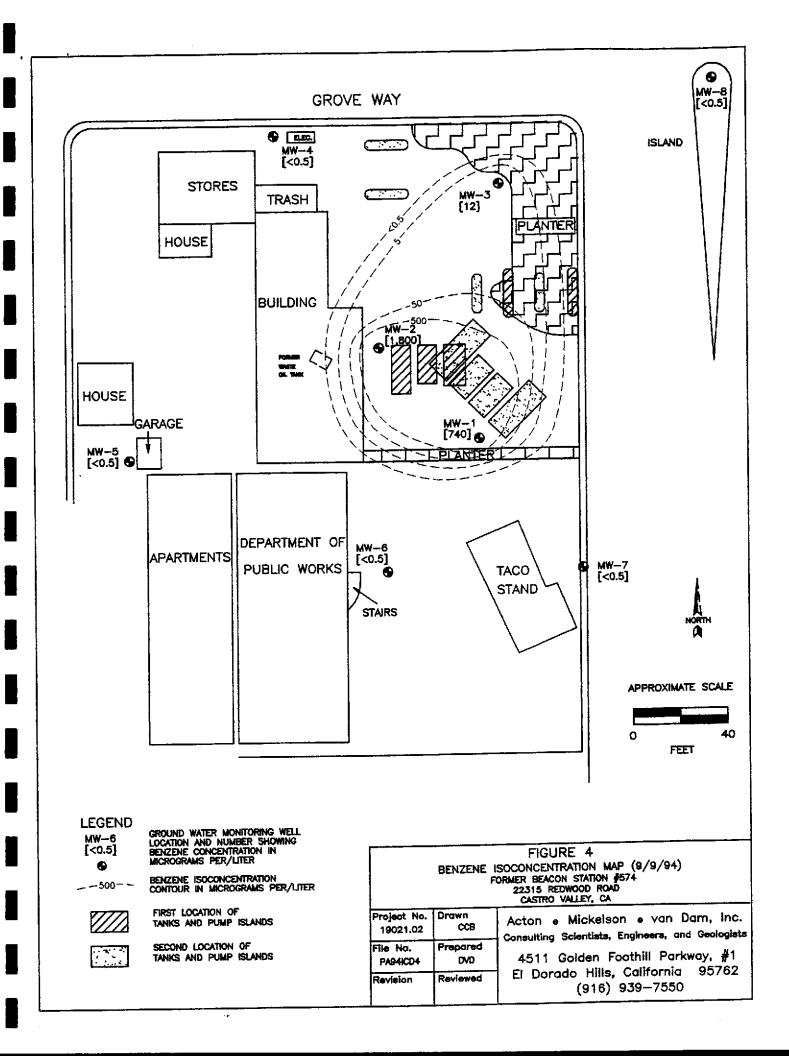
4511 Golden Foothill Parkway, #1
El Dorado Hills, California 95762

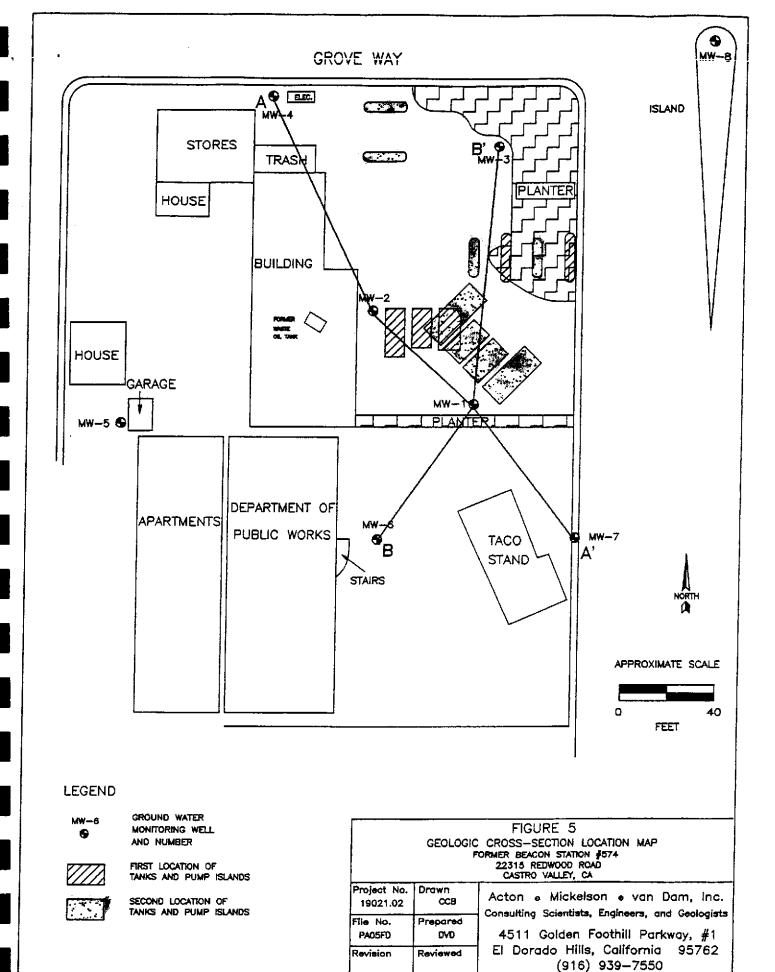
(916) 939-7550

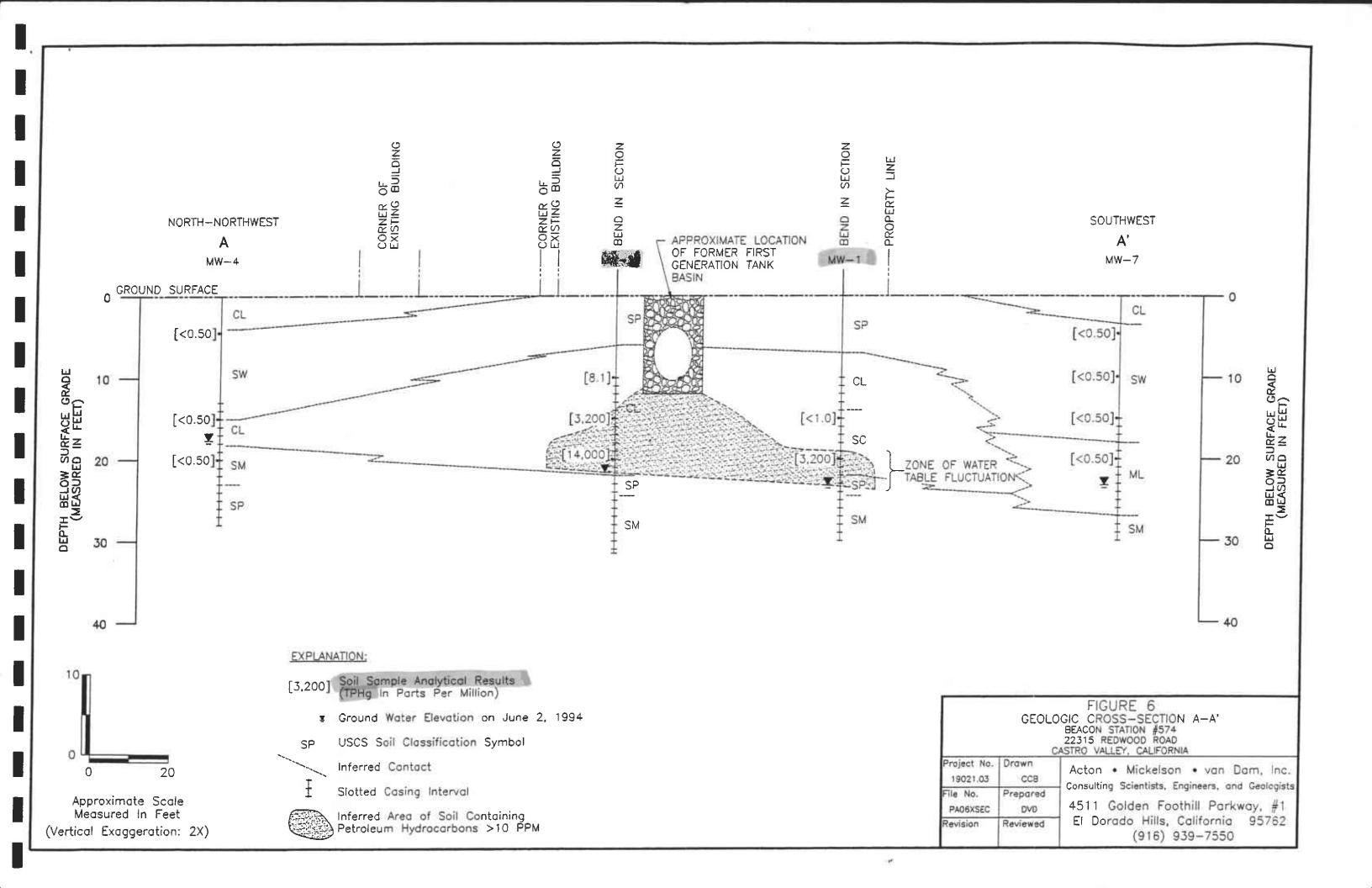


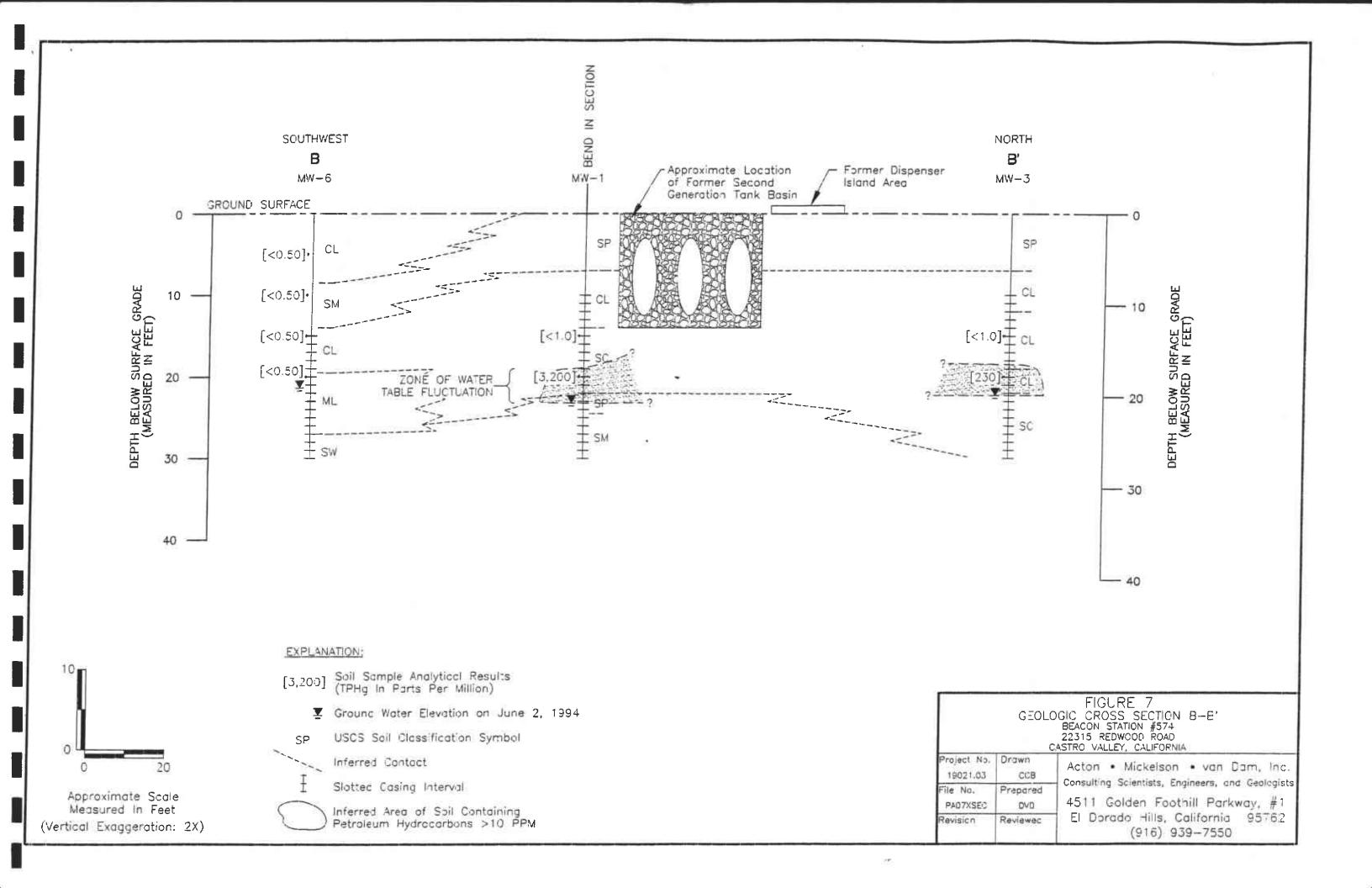












# APPENDIX A SOIL BORING LOGS

				_		
, I	PROJECT NAME / LOCATION Former Beacon Station #574					PROJECT BORING SHEET 1 OF 2 NUMBER: MW-1
B	2231	5 Redw	ocon St rocd Ro ley, C	xad .	#574	CONTRACTOR: DRILLING METHOD: H.S.A.
_						DRILLER: DRILLING RIG: Acker
						START: 8:15/03-26-91 COMPLETED: 9:30/03-26-91
I	AND WNER:	Paul	Wilso	n		SURFACE LOGGED BY: ELEVATION: 156.55 Hal Hansen
$\frac{1}{s}$	TS 1	ВС	SI	S R A E		CONTAMINANT
A M P	SAM MAPLE	LOW HS	AN MT P L	A E M C P V	DEPIH	DESCRIPTIONS OF MATERIALS AND CONDITIONS OBSERVATION OBSERVATION OBSERVATION OBSERVATION OBSERVATION OBSERVATION OBSERVATION
P L E	EF	S	E(ft)	E(in)	SCALE 1"= 4"	UNITS: POR
_		<del> </del>			1-	ASPHALT AND ROADBASE
					2 +	- GRAVELLY SAND; olive, fine —
					3 —	to coarse-grained, common - plastic fines, moist (SP) -
					4 +	
■ CA	MW-	15/	5.0-	18"	5 —	
	1-	30/ 50	6.5		6 —	
	_	for 5"			7 +	
		٦,			1	SANDY CLAY; olive, moderately
					8	plastic, fine to coarse — sand, some gravel, moist (CL)
					9 —	
CA		37/	10.0- 11.5	18"	10 —	- O
_	1-2	20′			11 +	<b>-</b>
					12	-
_					13 —	
					14 —	TAVEY CAME: Olive-hman
CA		50	15.0-	7"	15 —	fine to coarse sand, moist — 60
	1-3	for 6"	16.5		16 +	(SC)
					17 -	4
_					18 —	
					19	
■ CA	MW-	30/	20 0-	8"	20 —	
	1-	50	20.0-21.5	١	21 —	
	"	for 5"			22	
_						grained, september 5P)
					23 —	granieu, ————————————————————————————————————
	WA	TER L	EVEL D	ATA	GEOLOGI	SIST
D	ATE	03-2	26		0,1	001
	IME	6:29				Havon
<b>—</b>	√L	22.4			- SIGNATUR	<b>∤</b>
	ASING			+	- Hal Hans	
<b>■</b>	PIH				TYPED N	TAME
					·r	

	ROJE	T NAM	E / LO	CATION		PROJECT BORING SHEET 2 OF NUMBER: 40-90-818 NUMBER: MW-1	2
	Forms	er Bea Redw	con St ood Ro ley, C	ation :	<b>#574</b>	CONTRACTOR: DRILLING West Hazmat Drilling METHOD: H.S.A.	
	Casu	.U vai	rey, c	A		DRILLER: DRILLING RIG: Acker	
						START: 8:15/03-26-91 COMPLETED: 9:30/03-26-	-91
- - -	AND	Dani	Wilso	n		SURFACE LOGGED BY: ELEVATION: 156.55 Hal Hansen	
						CONTAMINANT OBSERVATION GENERAL	
A M P L	Y A L	BLOW	S I A N M T P	S R C O	DEPIH SCALE	DESCRIPTIONS OF MATERIALS AND CONDITIONS INSTRUMENT: NOTES hnu	NC
E L	E	Š	L E(ft)	PO LV E(in)	1"= 4"	UNITS: ppm	
C.P			25.0- 26.5	811	25	STITY SHIP olive-brown, fine-8 grained sand, was (SM)	
	5	25			26 —		
					27 —	7	
_					28 —	7	
					29 —	3	
C.F.	MW- 1- 6	12/ 14/ 50	30.0- 31.5	7"	30 —	]	
	6	50   for   5"			31 — 32 — 3	Total Depth 31.5 feet —	
		5"			33 -	iotal beput 51.5 rees	
			:		34 —		
					35 —		
					36 —		
					37 —		
					38	<u> </u>	
					39 +		
					40 +		
					41 —	<u>-</u> ]	
_					42 —	<del>-</del> -	
					43 —	<u> </u>	
_					44 —	<del>-</del>	
					45 —		
					46 ——		
					47 —	7	
_ _	WA	TER L	EVEL D	LLLL ATA	GEOLOGIS	ST	
	ATE	03-	26		9/10		
Ī	TME	6:2	9		SIGNATURE	Faron	
G	WL	22.	43		Hal Hanse	· · · · · · · · · · · · · · · · · · ·	
D D	ASING EPIH	30	1		TYPED NAM		

r

	•		•	CATION		PROJECT BORING SHEET 1 OF 2 NUMBER: MINES
2	2315	Rectv	icon St vood Ro ley, C	ation : ad 'A	#574	CONTRACTOR: West Hazmat Drilling DRILLING METHOD: H.S.A.
						DRILLER: DRILLING  Gene Reinhart RIG: Acker
						START: 10:30/03-26-91 COMPLETED:11:45/03-26-91
LA OW	ND NER:	Paul	Wilso	n		SURFACE LOGGED BY: ELEVATION: 155.17 LOGGED BY: Hal Hansen
	s N	ВС	SIAN	SR		CONTAMINANT OBSERVATION GENERAL
AY MP PE	S N A U M M P B L E	9 8	IM T	S R A E M C	DEPTH	DESCRIPTIONS OF MATERIALS AND CONDITIONS INSTRUMENT: NOTES
A Y M M P L L	M M P B L E E R	LOWITS	P L E(ft)	PO LV E(in)	SCALE 1"= 4'	UNITS: ppm comple
						ASPHALT AND ROADBASE
					1 +	Annual Color Sino
					2 🛨	to coarse-grained, common - plastic fines, moist (SP)
		,	1		3 🛨	plastic fines, moist (SP)
		20/ 30/ 50 for 5"		7"	4 - 1	- ¬
A	MW- 2- 1		5.0- 6.5		5 🕂	— 15 — 15
					6	SALLY COLOR, moderately
					7 🕂	plastic, fine to coarse sand- some gravel, moist (CL)
					8 —	- <u>-                                   </u>
					9 🛨	<b>-</b>
A	MW- 2-	10/ 50	10.0- 11.5	12"	10 -	30
	2	for	11.5		11 +	
		0			12 —	
					13 🕂	-
		30/ 50 for 5"	15.0- 16.5	7"	14 —	90
A	MM-				15 —	90
	MW- 2- 3		10.5		16 —	
		5"			17 —	-
					18 🕂	
					19 🕂	
A	MM-	7/	20.0- 21.5	15"	20 —	90
	MW- 2- 4	7/ 14/ 15	21.5		21 🕂	
					22 —	- Time have fine
					23 🕂	grained, saturate (SP)
	WATER LEVEL DATA		GEOLOG	GIST		
DA'	ΤE	03 <b>-</b> 26			91	l Hansen
TI	ME				SIGNATU	
GW.	Ĺ	20.	91		Hal Har	·
CASING		30'		•	}	
DΕ	PIH				TYPED N	VAITE

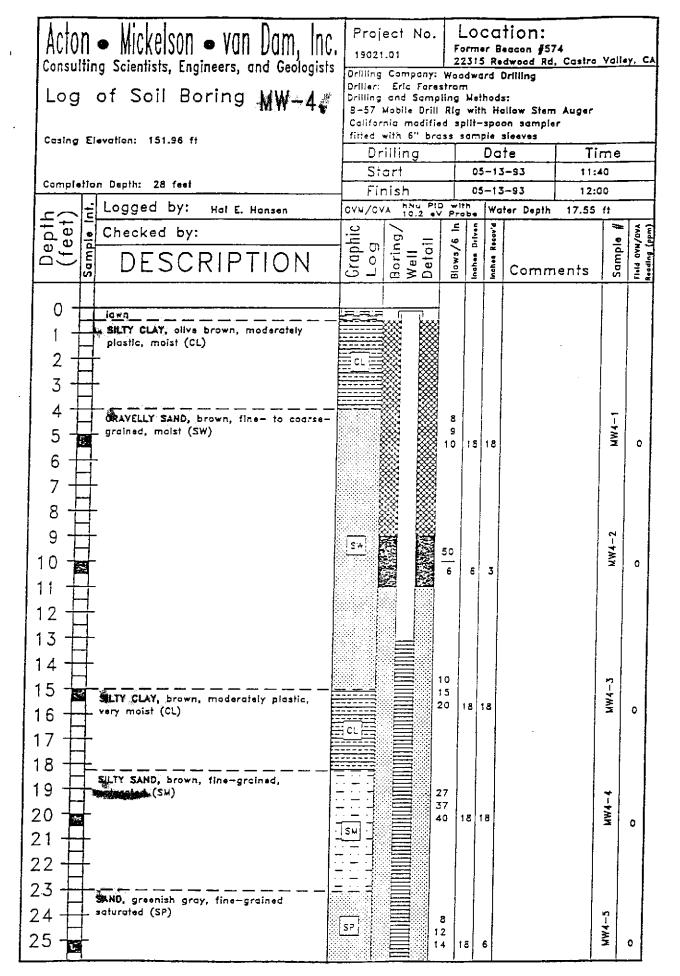
PF	PROJECT NAME / LOCATION						40-90-818	BORING NUMBER: M	₩ <b>-</b> 2	SHEET	2	OF	2
F 2 C	orme 2315 astr	r Bea Redw o Val	con St rood Ro ley, C	ation ; ad A	<b>#574</b>	CONTRACT			DRILL METHO	ING D:	H.S.A		
						DRILLER: Gene Reinhart			DRILLING RIG: Acker				
					:	START: 10:30/03-26-91			COMPLETED: 11:45/03-26-91				
IA OW	ND NER:	Paul	Wilso	n		SURFACE FLEVATION: 155.17			IOGGED BY: Hal Hansen				
STAY	TSNBCSISR YAULOAN AE PMMOUMT MC DEPTH				December 1	DECOSTOR		NTAMINANT SERVATION GENERAL OBSERVATION			EON		
A Y P E L E	NAMAHER	BLOWES	P L	M C P O L V E(in)	DEPIH SCALE 1"= 4'	DESCRIPTIONS OF MATERIALS AND CONDITIONS				MENT: hNu ppm			
CA			E(ft)			TITY SAN	olive-br	own, fine					
ÇA.	MW- 2- 5	15/ 16/ 18	26.5	10	26 <del> </del>	rained sa	olive-brand, <b>teating</b>	(SM) -					
					27 —			_		<u>.</u>			
					28 —								
					29 🕂			, <del>-</del>	•		:		
CA	MW- 2-	14/ 22/ 43	30.0- 31.5	14"	30 +				0				
	6	43			31 +	<del> </del>	) on 5 6						
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					33 +								
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E					35 —								
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	WAY	TER L	EVEL D	ATA	GEOLOGIS	r		· · · · · · · · · · · · · · · · · · ·			L	<u> </u>	
DA	DATE 03-26		970	91									
TI	TIME 6:22		SIGNATURE	STENATURE									
GW.	GWL 20.91		- Hal Hanse	n						;			
CA: DE	CASING 30' DEPIH			TYPED NAME									

	A) TEX	אגוא ידי	OF / IC	XATION		PROJECT	BORING	SHEET	1 OF 2			
<b>'</b>	t		•	ation		NUMBER: 40-90-81	L8 NUMBER: 1	M/-3 &				
1 2	2315	Redv	rood Ro	oad.	11071	CONTRACTOR: West Haz	zmat Drilling	DRILLING METHOD: H.S.A.				
						DRILLER: Gene Rei	inhart	DRILLING RIG: Acker				
						START: 1:40/03-	-26-91	COMPLETED: 3:00/03-26-91 LOGGED BY: Hal Hansen				
IA Ow	ND NER:	Paul	Wilso	on.		SURFACE ELEVATION: 157.1	13					
s Ţ	TSNBCSISR YAULOANAE PMMOUMTMCDEPIH EPBWNPPO LETLLYSCALE ERSE(ft) E(in) 1"= 4"							CONTAMINANT GENERAL				
SA PPLE	MM	ថ្ពីស្ព	S I A N M T	IMC	DEPTH	DESCRIPTIONS OF MATERIALS AND CONDITIONS		INSTRUMENT:	OBSERVATION NOTES			
L L	Į į	T T	P L E(ft)	PO LV E(in)	SCALE 1"= 4"			hNu UNITS: ppm	sample use lite			
_ <del>-</del>	ER		E(IC)	E(11)		—ASPHALIT AND ROA	ADBASE		WAS LITE			
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					2 — V	hrown, fine- ell sorted moist	(SP) —	1	:			
					з —		<del>-</del>					
'					4 —		<u>.</u>	:				
CA	MW-	15/	5.0-	18"	5 🕂		_	0	;			
	3- 1	15/ 26/ 37	6.5		6 —			]				
,					7 +							
					8 <del> </del>	lastic, moist (CI	r) — Taurth					
					9 + -							
CA	MW-	16/	10.0-	7"	10 +			0				
\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	3-	16/ 18/ 32	11.5		11 +		, 					
	2	32			12	. <u></u>						
					13 — T	ANDY CLAY: olive- oderately plastic	brown,	}				
					+ (	L)						
		·		044	14 —— `		1					
CA	MW 3	23/ 50	15.0- 16.5	811	15 —		-	1				
	3	for 5"			16 —							
					17 —			1				
					18 —		<u></u>					
					19 🕂 📆	IIIY CIAY; olive, lastic, very mois						
CA	MW- 3-	50 for	20.0- 21.5	7"	20 — p	lastic, very mois	t (CL)	8				
	4	6"			21 —							
					22 ———							
					23 —		<del>-</del>					
		THE TO THE	100 H21 12	2002	Torrara	m		<u> </u>				
			GEOLOGIS	1								
	DATE		03-26		- Wal	Warren						
	TIME		6:14		SIGNATURE	<del>, , , , , , , , , , , , , , , , , , , </del>			:			
GWL		<del>-</del>	21.62		Hal Hanse	n						
CA. DE	SING PIH	30	30'		TYPED NAM	E						

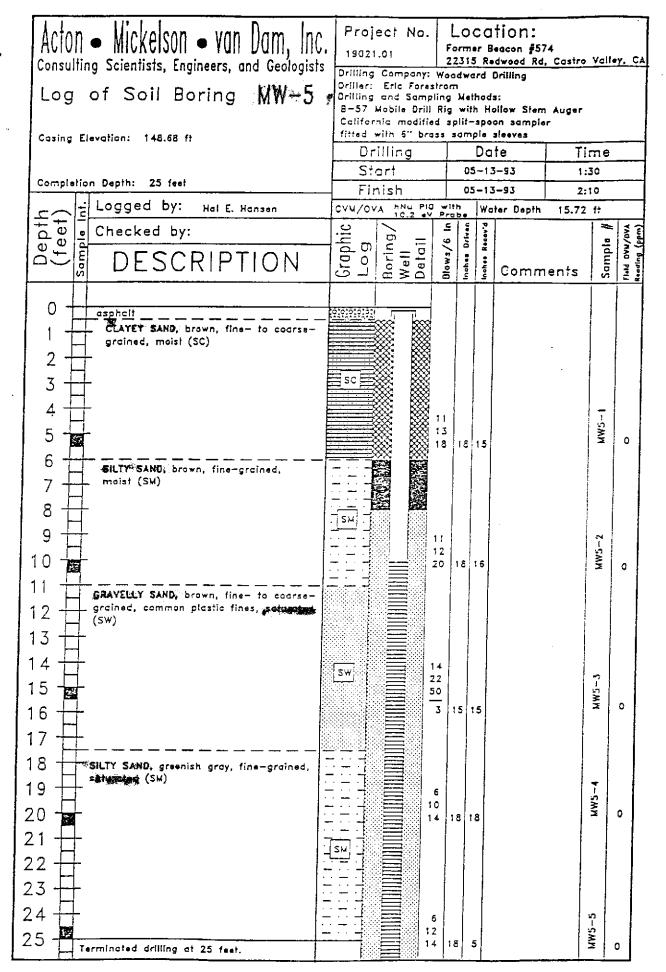
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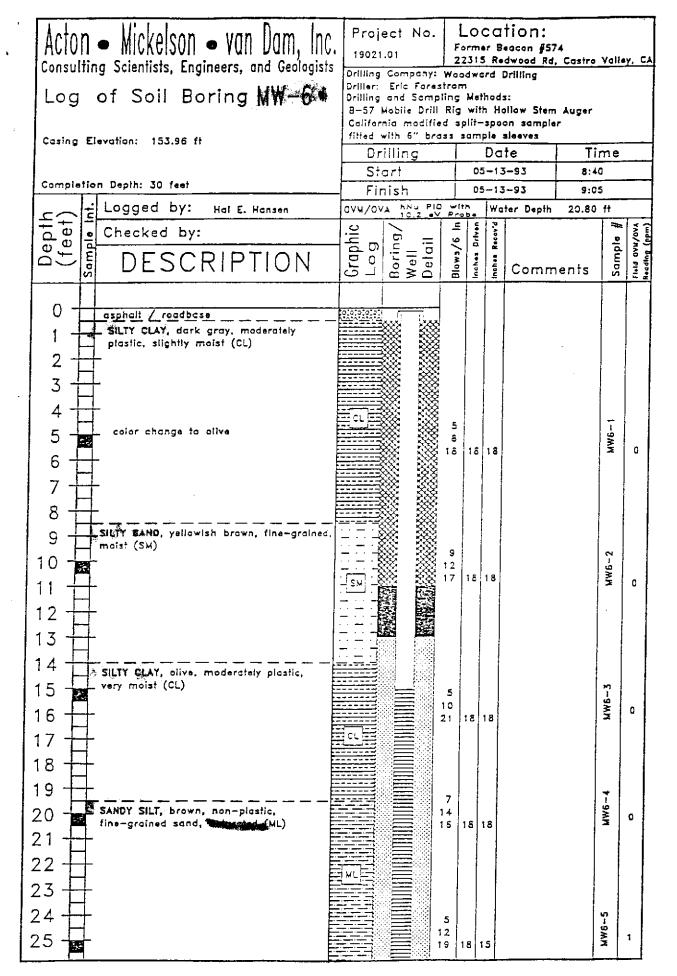
		PROJECT NAME / LOCATION						PROJECT NUMBER:	40-90-818	BORING NUMBER: M	W-3	SHEET	2	OF	2
	2	Former Beacon Station #574 22315 Redwood Road Castro Valley, CA							IOR: West Hazma	t Drilling	DRILLING METHOD: H.S.A.			•	
								DRILLER: Gene Reinhart			DRILLING RIG: Acker				
									1:40/03-26	<del>-9</del> 1	COMPLETED: 3:00/03-26-9				
<u> </u>	LAND OWNER: Paul Wilson							SURFACE ELEVATION	ON: 157.13	IOGGED BY: Hal Hansen					
-	s T										[MAMIM MOTTAV		NERAL		
	SAMPE E	AUMM	OU	S I A N M T	S R E C O V	DEPTH	Γ	DESCRIPTIONS OF MATERIALS AND CONDITIONS				UMENT	- OBSE	OBSERVATION NOTES	
	PE	PB	N W T	P	P &	SCALE						hNu	WOILS		
	Ē	ER	s	E(ft)	E(in)	1"= 4'		<u></u>			UNITS	: ppm	<u> </u>	· · · · · ·	
	ß	MW-	13/	25.0-	8"	25 —	CI	AYEY SAI	ND; olive-b	rown,	60				
	Ŭ.	ე ე	13/ 50 for	26.5		26	me	medium-grained sand, (SC)							
,		5	6"			27 +	,-	,							
						28				· -		•			
						+	•			<u>.</u>					
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'	CA	MW- 3-	14/ 50	30.0- 31.5	8"	30	-				U				
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						33 🛨									
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						46 —	-								
						47 🕂				-					
<b>\</b>	]	WATER LEVEL DATA GEOLOGIS				SIST				<u> </u>		<u> </u>			
	DAUE 02-26				00	/									
-	TIME 6:14				Gal Hansen										
1							SIGNATURE							:	
+	GWL 21.62 CASING 30'				Hal Hansen										
	CASING 30'				TYPED NAME										

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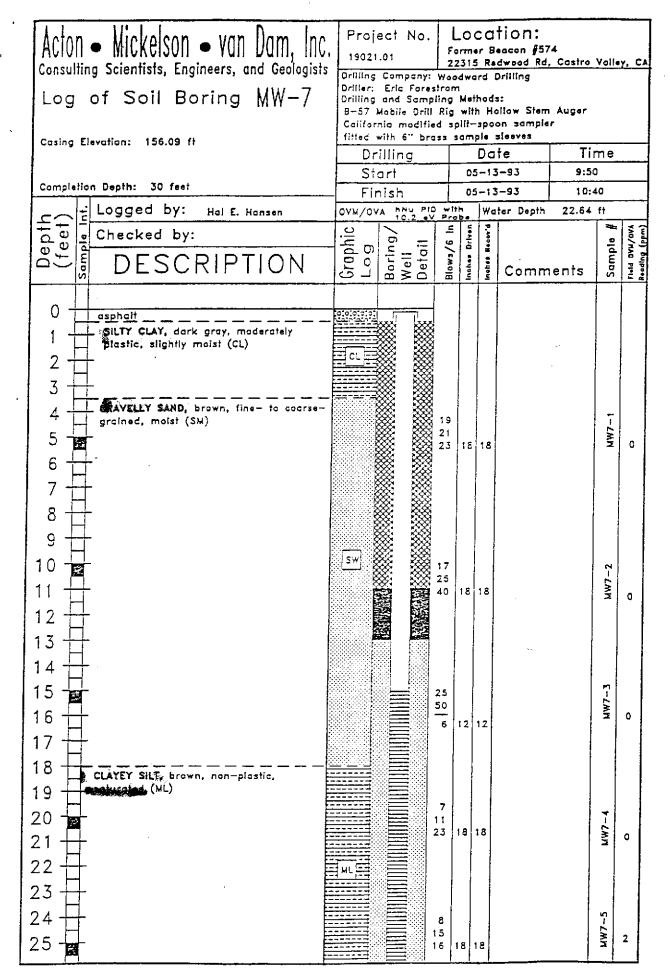


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Acton - Mickelson - van Dam, Inc.	Project No.		ation:	-		•
Consulting Scientists, Engineers, and Geologists	1	22315	Beacon #5 Redwood Rd	74 , Castro_	Valley,	CA
	Drilling Company: Orliler: Eric Foresi	Woodwar	d Drilling			
Log of Soil Boring MW-4	Oritling and Sampl 8-57 Mobile Drill	ing Meth		Auger		
	California modified	d spilt-s	poon sample			
Casing Elevation: 151,95 ft	fitted with 6" bra: Drilling	·	ate	Ti	me	
	Start	<del></del>	13-93	11:4		_
Completion Depth: 28 feet	Finish	05-13-93		12:00		
Logged by: Hal E. Hansen	OVM/OVA THE PID		Water Depth	17.55		
Checked by:  DFSCRIPTION	를 들 =	orly or	A. V. O.		10 H	(mad)
DESCRIPTION	Graphic Log Boring/ Well Detail		Comm	ents	Sample #	Reading
continued from above		8				
SP)		12 18	6		WW4-5	ĺ
26	SP					
27						١
28 Terminated drilling at 28 feet.				İ		
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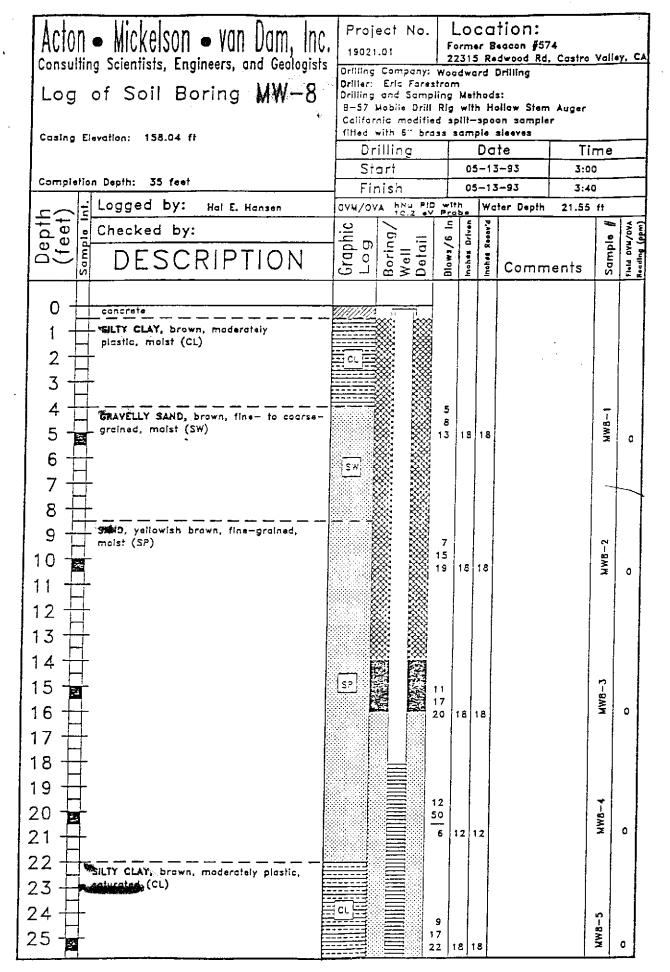




Acton - Mickelson - van Dam, Inc.	Project No.	Location: Former Beacon #57		
Consulting Scientists, Engineers, and Geologists	L	/4 , Castro Vall	ey, CA	
	Orilling Company: \ Driller: Eric Forest	Hoodward Drilling rom		
Log of Soil Boring MW-6	Drilling and Sampli	ing Methods: Rig with Hollow Sterr	Auger	
	California modified	i split-spoon sample		
Casing Elevation: 153.96 ft	fitted with 6" bres	Date	Time	
	Start	05-13-93	8:40	
Completion Depth: 30 feet	Finish	05-13-93	9:05	
Logged by: Hal E. Hansen	OVM/OVA hNU PID		20.80 ft	
Checked by:  DFSCRIPTION	Graphic Log Boring/ Well Detail	Driven Becovid	- T	Field OVM/DVA Reading (ppm)
DESCRIPTION	Graphi Log Boring, Well Detail	\$   5   5	nents s	John (
B DESCRIPTION	Q -   8 × Q	<del>- 1 - 1 - 1</del>		Te a
25 - south silts brown, non-plastic,		5	WW6-5	
(WE)		19 18 15	M.	1
26				
27 MAYELLY SAND, olive, fine- to cocree-				
28 grained, (SW)			ی	
29 🗍	**************************************	5	9-9WF	,
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	Acton - Mickelson - van Dam, Inc	Proj		No	- 1			tion:				
i	Consulting Scientists, Engineers, and Geologists	.   ''''			:	22315	5 R.	dwood Rd.	, Castro	yal	ley,	C.
	·	Orillar:	Erle	s Fa	restro	m		Drilling				
	Log of Soil Boring MW-7	Orilling B-57						s: ollow Stem	Auger			
		Cailfor	raic I	modi	ified :	-tiiqe	spo	on sample sleeves	r			
	Casing Elevation: 156.09 ft		-illir		or ass	3011	Da		T	ime		_
		<u> </u>	art	· <u>· · · · · · · · · · · · · · · · · · </u>		0.5		5-93	9::			
}	Completion Depth: 30 feet	Fi	Finish 05-13-93		5-93	10:40						
1	Logged by: Hal E. Hansen	יס/אאס	OVM/OVA HNU PIO			lih obe	-	ter Depth	22.64	22.64 ft		
	Checked by:	Graphic Log	9/	-	_   4	Inches Driven	Recev'd	l		=	Meld OVIL/OVA	(wad
1	DESCRIPTION	1 de 6	[년	Well	Blows /6					Sample	8	) But
	S DESCRIPTION	رق ا	Bo	≥ ≤	ž į	1 5	- Tahen	Comm	ents		1 3	Read
1	25 continued from above CLAYEY SILT, brown, non-plastic		E		∭ 8 ∷ 15	,				WW7-5		
	ESTOROTEC (MC)	J.			16		18	 		_   ₹	2	
	26 🕁								÷			
	27 SILTY SAND, greenish blue, fine- to	-	E	=8								1
	28 coarse-grained, saturated, common								•			1
	piastic fines (SM)	_ SM _			9					MW7-6		-
- (	30				22 23		12			×	0	
1	Terminated drilling at 30 feet.											
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Acton - Mickelson - van Dam, Inc.	Proj	ect No.				tion:	74			
Consulting Scientists, Engineers, and Geologists	, <b>[</b> .			2231	5 Re	dwood Rd.		Valle	y, CA	
	Orillar:	Company: Eric Fore	stra	ET .		-				
Log of Soil Boring MW-8		and Sam Moblie Drii					Auger			
	Califor	nía <mark>mod</mark> lfl	ed :	-filqe	Spo.	on sample				
Casing Elevation: 158.04 ft		fitted with 6" brass sample sleeves  Drilling Date						Time		
		art		0.4		1e 5-93	3:0			
Completion Depth: 35 feet	ļ	nish				5-93	3:4			
Logged by: Hal E. Hansen	OVM/OVA hNu PID			lth obs	th Water Depth 21.5					
Checked by:	္ဆ		T.	=   =	Pedev'd			***	¥ ( w	
DESCRIPTION	Graphic Log	in = ta	1	Inohes Briven				Sample	9 9	
DESCRIPTION	Gre	Boring, Well Detail		Inah	Inches	Comm	ents	Sar	Field DVM/DVA Reading (ppm)	
continued from above			9					-5		
25 SILTY CLAY, brown, moderately plastic, (CL)	□ cr ⊨		17	1	15			WWB		
126 ++								-		
27										
28 grdined, seemish gray, fine-						-				
}			8	İ						
29 +	SM -		13					WW86		
30			14	18	12			ž	0	
31 ++										
32 SND, greenish gray, medium-grained,	; 									
33 (SP)	· · · · · · · · · · · · · · · · · · ·									
34 🕂	SP							-7		
			50					KW8		
35 Terminated drilling at 35 feet.			5	5	5			×	0	
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# APPENDIX B WELL CONSTRUCTION DIAGRAMS

## INSTALLATION OF FLUSH GRADE MONITORING WELL

MONITORING WELL NO. \_\_MW-1 PROJECT Former Beacon Station #574 22315 Redwood Road, Castro Valley, ELEVATIONS, TOP OF RISER 156.55 GROUND LEVEL \_\_\_ DELTA NO. 40-90-818 PROTECTIVE CASING LOCKING VATER TIGHT CAP - FLUSH GROVE VOLL CONSTRUCTION 12-inch steel BLANETER AND HATERIAL 12 inches TOTAL LENGTH ł inch LENGTH ARTIVE GROUND 2-feet concrete THIDDHESS AND TYPE OF SEAL 4-inch Sch 40 PVC BIANCTER MATERIAL AND JUINT TYPE OF RISER PIPE \_ Flush Thread Neat cement containing TYPE OF BACKFILL AROUND RISER 5% bentonite 2-feet bentonite THICKNESS AND TYPE OF SEAL pellets 2 feet DISTANCE OF FILTER SAND ABOVE TOP OF SCREEN #3 lonestar TYPE OF FILTER AROUND SCREEN Sch 40 PVC HENTTERING VELL HATERIAL 0.01 inch SCREEN GAUGE OR SIZE OF OPENINGS CILLIT SIZED 4 inch x 20 feet DIAMETER AND LENGTH OF SCREEN 30 feet DEPTH TO THE BOTTOM OF MONITORING VELL 30 feet DEPTH TO THE BOTTOM OF FILTER SAND N/A THEORNESS AND TYPE OF SEAL 10 inches - BLANETER OF BOREHOLE MUNITURING WELL WATER LEVEL MEASUREMENTS 0.25 9.75 VATER LEVEL = TIME DATE 22.43 6:29 3-26-91 20 30 INSTALLATION COMPLETED 3/26/91 Top of casing 10:30 Delto Environmental Consultants, Inc.

1022 B/3-89

## INSTALLATION OF FLUSH GRADE MONITORING WELL

PROJECT Former Beacon Station #574  22315 Redwood Road, Castro Valle	MONITOR	ING WELL	NO. MW-2	17			
22315 Redwood Road, Castro Vario	CA ELEVATI	באסון הפחווי	OF RISER TOOM	<u> </u>			
DELTA NO. 40-90-818		GRUSI	10				
PRITECTIVE CASING	i		-				
LICKING VATER TIGHT C	AP.						
FLUSH GROSE VE		12-ir	ch steel				
	DIANCTER AND HATERIAL — TOTAL LENGTH —						
цэман	H ABOVE GROUND	<u> } inc</u>	才 inch 2-feet concrete				
THEORETZ AND THE	PE OF SEAL	_ <u></u>	et concrete				
STANETER, NATERIAL AND .		and 4-ind	h Sch 40 PVC				
STANETER, MATERIAL AND	MINI TIPE UP, RUSE	Flush	Thread				
		Neat	cement contain	ning			
TYPE OF BACKFEL AREA	O RESER		entonite				
		2-fe	et bentonite				
THECKNESS AND TYPE OF		pelle	pellets				
DISTANCE OF FILTER SAN	DISTANCE OF FILTER SANG ABOVE TOP OF SCREEN 2 feet #3 lonestar						
TYPE OF FILTER ARCHO		#5 1	Jilestar				
HOUTTORING VELL HATER	HONGTURING VELL HATERIAL Sch 40 PVC						
SCREEN GAUGE OR STZE O	- screen gauge or size of openings court size 0.01 inch 4 inch x 20 feet						
STANETER AND LENGTH OF	TANETER MID LENGTH OF SCREEN  4 inch x 20 feet						
		22.5					
ספידוו זמ זואני אמדומא סי	HONITORING VELL	30 f	eet				
שבידו דנו דו-ב פסדונא סי	ETT TEP SAME	30_f	eet				
		<del></del>					
THOUGHESS AND TYPE OF	SEAL	_N/A_					
		10 1	nches				
MANCTER OF BOREHOLE			HOLLES				
0.25	HONITORING VI	ELL VATER (	EVEL MEASUREME	гтя			
9.75	DATE	TIME	VATER LEVEL	¥			
( 2 = FT.	3-26-91	6:22	20.91				
L3 = FT.	3-20-31						
30							
DISTALLATION COMPLETED 3/26/91			<u></u>				
12:45		HEASURE POINT	Top of casi	ing			
	Eustrouweugi — Belta			:			

1022 B/3-89

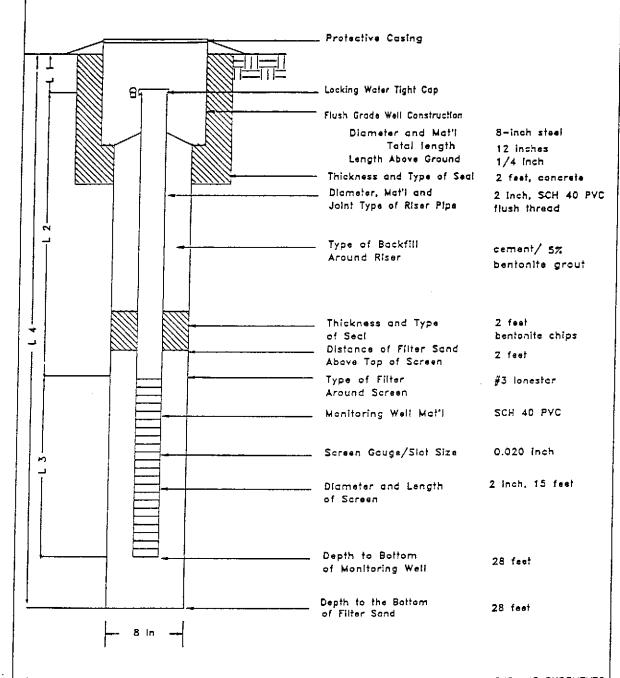
### INSTALLATION OF FLUSH GRADE MONITORING WELL

PROJECT Former Beacon Station #574 MONITORING WELL NO. \_\_\_MW-3 22315 Redwood Road, Castro Valley, ELEVATIONS, TOP OF RISER 157.13 GROUND LEVEL \_\_\_\_ DELTA NO. 40-90-818 PRETECTIVE CASING LOCKING VATER TIGHT CAP FLUSH GROSE VELL CONSTRUCTION 12-inch steel BLANETER AND HATERIAL 12 inches TUTAL LENGTH inch LENGTH ABOVE GROWING 2-feet concrete - THICHONESS AND TYPE OF SEAL 4-inch Sch 40 PVC - Blaheter, Haterial, and Joint Type of Riser Pipe . Flush Thread Neat cement containing TYPE OF BACKFILL AROUND RESER 5% bentonite 2 feet bentonite THECKNESS AND TYPE OF SEAL pellets 2 feet DISTANCE OF FILTER SAND ABOVE TOP OF SCREEN #3 lonestar - TYPE OF FILTER AROUND SCREEN Sch 40 PVC HONOTORING VELL HATERIAL SCREEN GAUGE OR SIZE OF OPPORINGS CILITY SIZED 0.01 inch 4 inch x 20 feet - DIAMETER AND LENGTH OF SCREEN 30 feet DEPTH TO THE BOTTON OF NONTTORONG VELL 30 feet DEPTH TO THE BUTTOM OF FILTER SAND N/A THEORYESS AND TYPE OF SEAL 10 inches - BEAMETER OF BOREHOLE 0.25 MONITORING VELL VATER LEVEL MEASUREMENTS 9.75 TIME VATER LEVEL = DATE 20 21.62 3-26-91 6:14 30 DISTALLATION COMPLETEDS BATE 3/26/91 - HEASURE PRINTS TOD OF CASING 4:30 Delta Environmental Consultants, Inc. 1022 B/3-89 (

PROJECT: Former Beacon #574

22315 Redwood Rd Castro Valley, CA MONITORING WELL NO.: MW-4

ELEVATION: 151.96 ft



L1 = 0.25 ft

L2 = 12.75 ft

L3 = 15 ft

L4 = 28 ft

Completion Date and Time

05-13-93 12:25

MONITORING WELL WATER LEVEL MEASUREMENTS

DATE	TIME	WATER LEVEL*
05-18-93	8:22	17.55 ft

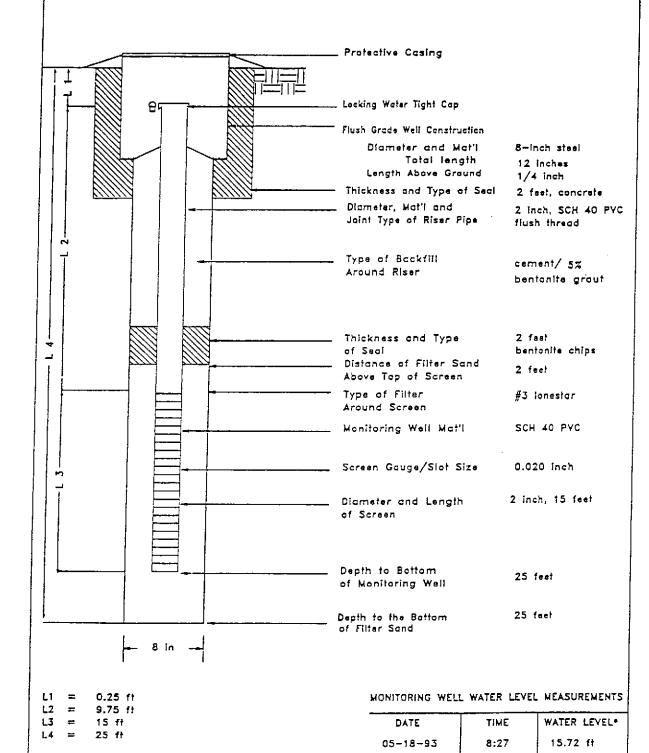
\*Measuring Point Top of casing

. ACTON • MICKELSON • VAN DAM, INC. \_

PROJECT: Former Beacon #574

22315 Redwood Rd Castro Valley, CA MONITORING WELL NO .: MW-5

ELEVATION: 148.68 ff



Completion Date and Time

05-13-93 2:30

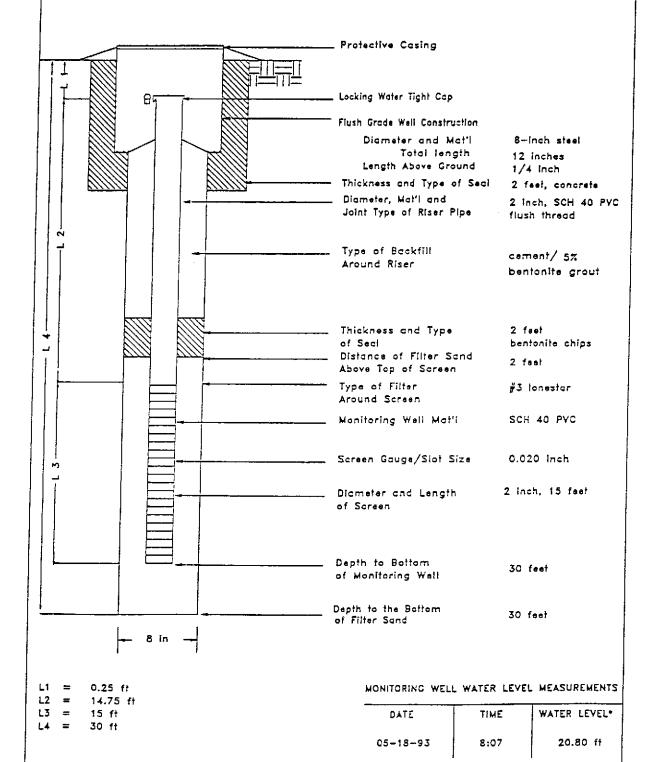
ACTON • MICKELSON • VAN DAM, INC. \_\_

\*Medauring Point Top of casing

File #19021011

PROJECT: Former Beacon #574 22315 Redwood Rd Castro Valley, CA

MONITORING WELL NO.: MW-6 ELEVATION: 153.96 ft



\*Measuring Point Top of casing

ACTON • MICKELSON • VAN DAM, INC.\_

Completion Date and Time

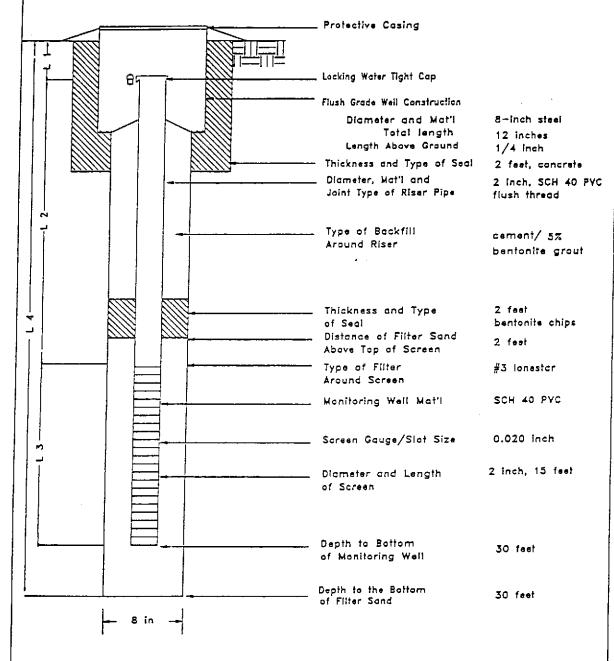
05-13-93 9:30

#### - MONITORING WELL ---CONSTRUCTION DETAILS

PROJECT: Former Beacon #574 22315 Redwood Rd Castro Valley, CA

MONITORING WELL NO .: MW-7

ELEVATION: 156.09 ft



LI = 0.25 ft

L2 = 14.75 ft

L3 = 15 ft

30 ft

Completion Date and Time

05-13-93 10:55

MONITORING WELL WATER LEVEL MEASUREMENTS

DATE	TIME	WATER LEVEL*
05-18-93	8:13	22.64 fi
		•

\*Measuring Paint Top of casing

ACTON . MICKELSON . VAN DAM, INC. \_\_

File #19021013

PROJECT: Former Beacon #574
22315 Redward Rd

22315 Redwood Rd Castro Volley, CA MONITORING WELL NO .: MW-8

ELEVATION: 158.04 ft

MONITORING WELL WATER LEVEL MEASUREMENTS

TIME

8:16

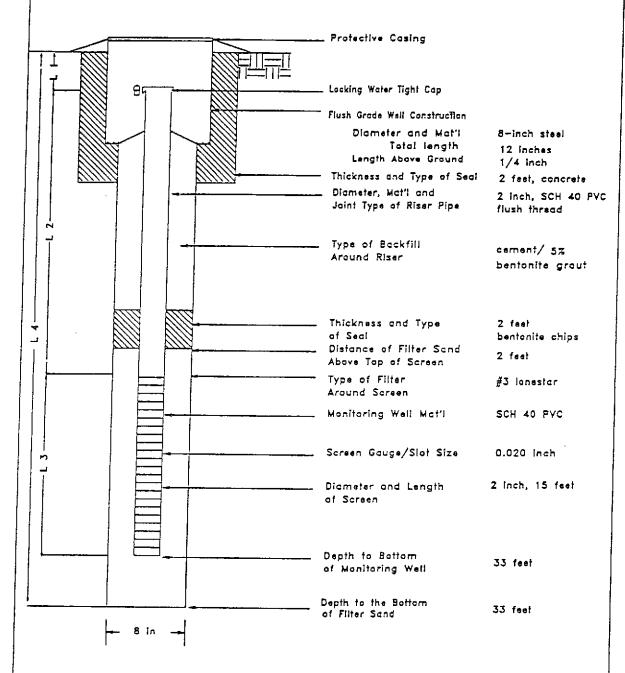
\*Measuring Point Top of casing

DATE

05-18-93

WATER LEVEL\*

21.55 ft



L1 = 0.25 ft

L2 = 17.75 ft

L3 = 15 ft

L4 = 33 ft

Completion Date and Time

05-13-93 5:00

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File #19021014