

**ensco
environmental
services, inc.**

**SHALLOW GROUNDWATER
AQUIFER PUMP TEST**

AT

**FORMER SHELL OIL COMPANY
SERVICE STATION
7194 AMADOR VALLEY BOULEVARD
DUBLIN, CALIFORNIA**

**Project No. 1826G
Shell P.O. No. MOH 237138
November 1989**

Corporate Offices

41674 Christy Street, Fremont, CA 94538-3114 (415) 659-0404 Fax (415) 651-4677 Contr Lic No. 550205



December 15, 1989

Shell Oil Company
1390 Willow Pass Road, Suite 900
Concord, CA 94520

Attention: Ms. Diane Lundquist

Subject: Shallow Groundwater Aquifer Pump Test
Former Shell Service Station
7194 Amador Valley Boulevard, Dublin, California
Shell P.O. No. MOH 237138
EES Project No. 1826G

Dear Ms. Lundquist:

Enesco Environmental Services, Inc., (EES) is pleased to submit this report which details the procedures and results of a Shallow Groundwater Aquifer Pump Test conducted at the facility noted above. If you have any questions concerning the report, please call.

Sincerely,
Enesco Environmental Services, Inc.

A handwritten signature in black ink that appears to read "Cynthia R. Virostko".

Cynthia R. Virostko
Staff Geologist

A handwritten signature in black ink that appears to read "Douglas T. Young".

Douglas T. Young
Senior Project Hydrogeologist

A handwritten signature in black ink that appears to read "Lawrence D. Pavlak".

Lawrence D. Pavlak, C.E.G. 1187
Senior Program Geologist

CRV/DTY/LDP/sw
Enclosure

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EXECUTIVE SUMMARY

Enesco Environmental Services, Inc. (EES) has issued this report to summarize the results of the shallow groundwater aquifer pump test conducted from August 1 through 4, 1989, at the subject site located in the City of Dublin, Alameda County, California. EES's field investigation and findings of the test may be summarized as follows:

1. A 30-foot deep, 6-inch-diameter test recovery well (RW-1) was installed on July 27, 1989, at the location shown on Figure 2.
2. A study of background fluctuations in groundwater levels were performed using existing wells at the site.
3. An electric submersible pump was installed in RW-1. Pressure-sensitive electronic water depth transducers were then installed in RW-1 and five existing on-site groundwater monitoring wells (MW-1, MW-2, MW-3, MW-4, and MW-5). A 21,000 gallon portable Baker tank was placed at the site to store purged groundwater.
4. A preliminary step-drawdown test was conducted on July 31, 1989 to determine the optimum pump discharge rate. This rate was determined to be 3.0 gallons per minute (gpm).

5. A constant-discharge pump test was performed for 72 hours. Water levels in wells that contained transducers were recorded electronically by a data logger. Wells without transducers were measured manually with an electronic sounding tape at regular intervals.
6. Following the pump test, groundwater levels were measured at regular intervals in all wells at the site during the recovery period.
7. Data obtained from the test was analyzed and values calculated for hydraulic conductivity, transmissivity, and storativity for each well within the observed radius of influence. A radius of influence (cone of depression) for the recovery well was calculated to be approximately 200 feet. With this radius of influence, it is probable that a zone of capture covering the entire site can be created with one recovery well.

3 gpm = ~~is~~ radius of influence
of 200 ft.

**SHALLOW GROUNDWATER
AQUIFER PUMP TEST**

AT

**FORMER SHELL OIL COMPANY
SERVICE STATION
7194 AMADOR VALLEY BOULEVARD
DUBLIN, CALIFORNIA**

At the request of Shell Oil Company (Shell), Enesco Environmental Services, Inc. (EES) has conducted a shallow groundwater aquifer pump test at the former Shell Service Station located at 7194 Amador Valley Boulevard in the City of Dublin, Alameda County, California (Figure 1). This was done for the following purposes:

1. To determine aquifer characteristics and the feasibility of achieving hydraulic control of the site.
2. To determine the feasibility of using recovery wells to remove separate-phase floating product and soluble hydrocarbon contamination from the groundwater, and to determine the zone of capture.

RECOVERY WELL CONSTRUCTION

EES drilled an exploratory boring and installed recovery well RW-1 on July 27, 1988, at the location shown on Figure 2. The log of the boring is presented in Appendix A along with the well construction details. The boring was drilled with EES's truck-mounted B-61 drill rig using a 10-inch-diameter, hollow-stem auger to a depth of 31.5 feet. The auger and other tools used to advance the boring were steam cleaned before use to minimize the possibility of cross-contamination.

After drilling to the desired depth, EES installed one recovery well in the exploratory boring. The recovery well was constructed of 6-inch-diameter, schedule 40, flush-threaded polyvinyl chloride (PVC) casing: no glues or solvents were used. The PVC casing, measuring a total of 30 feet, contained a 20-foot screened interval with three rows of 0.020-inch slots. A sandpack was slowly poured into the borehole annulus to

approximately 1 foot above the screened interval, followed by a 1-foot seal of hydrated bentonite pellets. The remaining portion of the annular space was sealed with neat cement. The top of the well was set in a wooden frame with a PVC locking cap to provide security. The boring log and recovery well construction details can be found in Appendix A.

After construction, the well was thoroughly surged and developed using an air-lift purge pump to align the grains of the aquifer material around the screened interval for more efficient groundwater flow; and to remove fine sediments from the well casing and sand pack. Approximately 10 well volumes of groundwater were removed from the extraction well during the operation and stored in drums at the site. The drums of water were subsequently removed and properly disposed of.

EQUIPMENT SETUP

A Grundfos SP-1-9 submersible electric purge pump was installed in well RW-1. Electric power was supplied by a 230-volt AC, diesel-driven generator. The discharged groundwater was carried from the pump by a plastic hose. This was run in series through a totalizer, control valve, and a 0-5-gpm flowmeter. The purged groundwater was then stored at the site in a portable 21,000-gallon capacity poly tank.

A total of six pressure-sensitive electronic transducers were installed in wells RW-1, MW-1, MW-2, MW-3, MW-4, and MW-5. These were interfaced with a Terrascience Systems, Ltd. Terra 8 Datalogger that recorded groundwater depths at regular time intervals. The transducers measured the pressure of the overlying water, which was converted by the Datalogger into feet of pressure head. Data stored in the Datalogger was downloaded into a portable IBM-PC-compatible computer on-site. The computer was also used to start, stop, and modify the Datalogger program.

BACKGROUND DATA

To verify the validity of groundwater level changes recorded during the pump test, it was necessary to correlate them with the natural cycle of groundwater level fluctuations as measured over a period of time. Groundwater elevation contours

calculated from measurements taken on June 28, 1989 are shown in Figure 3. The groundwater elevation data for Figure 3 is listed in Table 1. The apparent direction of groundwater flow was to the southeast at an average gradient of 0.0025 feet/foot.

Data for background fluctuations of groundwater levels were obtained during the two weeks from July 20 through 26, 1989 and stored in the datalogger. This information was obtained from transducers in wells RW-1 MW-1, MW-2, MW-3, MW-4, and MW-5. Graphs of the background fluctuation data are shown on Figures 4 through 8. Graphical analyses for well MW-5 were not conducted since it is screened at a lower depth than wells MW-1 through MW-4. Information stored in the datalogger for the background fluctuation is included in Appendix B. The fluctuations typically occur over a cycle of 24 hours, and are probably influenced by barometric pressure forces. The mean maximum fluctuation for these five wells within a 72 hour period was 0.26 feet.

STEP/DRAWDOWN TEST

To determine the optimum recovery well discharge rate at which maximum drawdown can be maintained in a relative state of equilibrium, a step/drawdown test was performed on July 31, 1989. The pump was started with an initial flow of 3.0 gpm and was increased at stepped intervals to a maximum of 5 gpm. It was found that the optimum discharge rate for the recovery well was 3.0 gpm.

CONSTANT DISCHARGE PUMP TEST/RECOVERY TEST

Commencing on August 1, 1989, the pump was run at a constant discharge rate of 3.0 gpm for 72 hours. Groundwater level data for the wells with transducers installed was stored in the Datalogger for later computer analysis. Groundwater depths for the remaining wells were manually measured at one-hour intervals with electronic sounders. RW-1 was also measured periodically with an electronic sounder in addition to a transducer.

After the pumping was halted on August 4, 1989, the recovery phase of the test was initiated. Groundwater level data were acquired throughout the recovery phase until groundwater levels reached equilibrium, a period of approximately 2.75 hours. At this point, the test was completed. Purged groundwater stored in the portable tank at the

site (a total of 16,737 gallons) was removed for disposal by a registered hazardous waste hauler (Crosby and Overton, Inc.).

DATA ANALYSIS, PUMP TEST

Data obtained during the pump test from those wells with transducers (RW-1, MW-1, MW-2, MW-3, MW-4, and MW-5) was first downloaded from the Datalogger, processed using the Terrascience Systems Ltd. Terra 8 software, and compiled into a data report (Appendix B) using software from Golden Software, Inc. on an IBM-PC-compatible computer. Data collected by manual electronic sounding from wells without transducers were tabulated by hand and compiled into data files using the Golden software. From these files, groundwater contour maps were generated by computer using the Surfer program by Golden Software, Inc.

A groundwater elevation contour map for August 4, 1989, at the time of maximum drawdown, is shown in Figure 9. A maximum drawdown contour map for the same period of time is shown in Figure 10. Groundwater elevation and maximum drawdown data used for Figures 9 and 10 are presented in Tables 2 and 3, respectively. As seen in Figure 10, the radius of the cone of depression is approximately 200 feet. This was calculated by averaging the distance between the 0.00 foot contour (no influence) and the -0.40 foot contour (first calculated influence). Because background 72 hour water level fluctuations had a mean maximum of 0.26 feet, only those wells with a maximum drawdown greater than that were considered for data analysis and in determining the radius of influence (radius of the cone of depression generated by the recovery well).

Data obtained from the pump test for those wells with a maximum drawdown of 0.26 feet or greater was analyzed using the Graphical Well Analysis Package by Groundwater Graphics on an IBM-PC-compatible computer. This software package calculates aquifer characteristics by using the Theis Nonequilibrium Well Equation. For application of this equation to the aquifer characteristics of this site the Neuman (1975) modification of the Theis equation for water-table aquifers was used. This analysis makes the following generalized assumptions about the aquifer:

1. The aquifer is unconfined.
2. The aquifer is level and infinite in horizontal extent.
3. The aquifer is homogeneous and isotropic.

4. The pumping well fully penetrates the aquifer.
5. Discharge from the well is at a constant rate.
6. There is no storage within the well itself.
7. The aquifer response to drawdown is elastic (early response).

The Theis equation for elastic response of water-table aquifers is as follows:

$$T = Q/(4\pi s W(U_A, B))$$

Where: $U_A = (r^2 S_s)/(4 T t)$

$$B = r^2/b^2$$

T = transmissivity

Q = pumping rate

s = drawdown

W = well function

r = radial distance from pumping well

S_s = storativity coefficient

t = time since pumping started

b = initial standard thickness of aquifer

Sources: Dansby and Price (1987), p. B.7, eqs. B.7, B.8; Fetter (1988), p. 192, eqs. 6-48, 6-49

Hydraulic conductivity is calculated by:

$$K = T/b$$

Where: K = hydraulic conductivity

T = transmissivity

b = initial saturated thickness of aquifer

Source: Fetter (1988), p. 105, eq. 4-16

Figures 11 through 21 show Theis curve plots and values for transmissivity, aquifer thickness, hydraulic conductivity, and storativity for RW-1, MW-1 through MW-4, MW-6, and MW-8 through MW-12. A summary of these results is given in Table 4.

Data obtained from monitoring wells MW-5 and MW-7 were found to be anomalous since; 1) the screened interval for MW-5 is different from the other monitoring wells, and; 2) water levels for MW-7 showed a consistent rise in the water table during the testing.

Transmissivity values were calculated from the observation wells and ranged from 844 gallons per day per foot (gpd/ft) for MW-1 to 5450 gpd/ft for MW-12. Hydraulic conductivity varied from 48.9 gpd/ft² for MW-1 to 527 gpd/ft² for MW-12.

For all wells, excluding MW-5 and MW-7 for reasons stated above, the saturated aquifer thickness ranged from 6.92 feet at MW-8 to 0.185 feet at MW-1. Storativity coefficients varied from 0.00172 for MW-2 to 0.185 for MW-1.

DATA ANALYSIS, RECOVERY TEST

During the recovery phase of the test, water levels were measured by the datalogger in wells that contained transducers, and by hand with an electronic depth sounder in the wells without transducers. Water levels for RW-1 were measured by both datalogger and electronic depth sounder.

The datalogger measured water levels beginning with approximately 2-second intervals, gradually lengthening to half-hour intervals. Water levels taken by electronic depth sounder were measured at half-hour intervals until the end of the recovery phase. A groundwater elevation contour map for the end of the recovery phase at 17:58 on August 4, 1989, is shown in Figure 22. Groundwater level data for RW-1 during the recovery phase are included in Table 5.

The data was plotted as residual drawdown (s') vs. the log of the ratio t/t'' (where t = time since start of pumping and t'' = time since pumping stopped). This is a

modification of the Jacob Straight-Line Method as discussed in "Groundwater and Wells," pp. 256-257 (Driscoll, 1986). Transmissivity is calculated by the equation:

$$T = \frac{264 Q}{\Delta s'}$$

Where: T = transmissivity in gpd/ft
 Q = pumping rate in gpm
 $\Delta s'$ = change in drawdown over 1 log cycle in feet
264 = conversion factor for gpm to gpd

The graph, calculations, and value for transmissivity for the recovery test analysis are shown in Figure 23. The value for transmissivity is calculated as 628 gpd/ft, which compares with 433 gpd/ft as calculated from the pumping test data. The values are within one order of magnitude of each other, which is acceptable accuracy considering differences in measurement technique, data analysis, and change in aquifer storativity as air occupies voids in the aquifer material during dewatering and is trapped during recovery. Theoretically, the drawdown and recovery curves and aquifer characteristic values should be identical (Driscoll, 1986, pp. 257-260).

CAPTURE ZONE ANALYSES

Calculation of the capture zone symmetry was performed using the RESSQ semianalytical contaminant transport model presented in the American Geophysical Union, Water Resources Monograph No. 10 for groundwater transport models. The model uses a series of injection well points to (1) create point sources for flow lines and (2) generate a regional flow equivalent to the groundwater gradient observed beneath the site. The program then uses extraction well points to represent groundwater recovery wells using pumping rates determined from the pump tests. The model combines the equations for complex velocity potential, uniform flow, number of point sources, and point sinks to calculate the symmetry of the capture zone. This analysis does make some general assumptions about the aquifer which include: (1) the aquifer is infinite in horizontal extent; (2) the aquifer is homogeneous and isotropic; (3) the aquifer is of uniform thickness; and (4) a steady state flow (gradient and direction) exists beneath the site.

Initial pumping at the site in September 1988 was conducted at a rate of 5 gpm. The recovery well (RW-1) dewatered approximately 13 hours after the start of pumping. This indicated that a lower pumping rate would be needed to conduct a long-term constant drawdown test. A step drawdown test was performed in July 31, 1989 that indicated an optimum pumping rate of 3 gpm could be sustained by RW-1 during the constant discharge test. This result was confirmed when the constant drawdown test was performed from August 1 through 4, 1989. It is this rate at which the capture zone configuration model was run. Figure 24 presents the flow symmetry and capture zone resulting from the simulated use of existing extraction well RW-1 pumping at 3 gpm. As can be seen by the diagram, the capture zone extends as far as MW-6 to the northeast and as far as MW-2 to the southwest. Data used to generate the capture zone model are presented in Appendix C.

CONCLUSIONS

Data obtained from the constant-discharge aquifer pump and recovery test of August 1 through 4, 1989, for Shell indicate that aquifer characteristics at the site are generally isotropic and heterogeneous. The radius of influence of the recovery well RW-1 has been determined to be approximately 200 feet. It is estimated that one recovery well would generate a capture zone sufficient to cover the entire site. It appears that extracting groundwater using RW-1 at the rate of 3 gpm will result in a capture zone extensive enough to recover all contaminated groundwater beneath the site as well as contaminated groundwater identified in monitoring wells off-site.

REFERENCES

- Dansby, D.A. and C.A. Price, 1987. Graphical Well Analysis Package, Version 2.0 - User Manual. Groundwater Graphics, Oceanside, CA., pp. B3 - B8.
- Driscoll, G. 1986. Groundwater and Wells, Second Edition. Johnson Division, St. Paul, MN., pp. 256-260.

Enesco Environmental Services, Inc., September Quarterly Report Groundwater Sampling and Analysis for Former Shell Station, 7194 Amador Valley Boulevard, Dublin, California, EES Project No. 1826G, September 1989.

Javandel, I., Doughty C. and Tsang, C.E., Groundwater Transport: Handbook of Mathematical Models, American Geophysical Union Water Resources Monograph No. 10, pp 228, 1987.

Fetter, C.W., Applied Hydrogeology, Second Edition, Merrill Publishing Company, Columbus, OH., p. 105, 192, 1988.

Neuman, S.P., Analysis of pumping test data from unconfined aquifers considering delayed gravity response, Water Resources Res., 11, pp. 329-342, 1975.

REPORTING REQUIREMENTS

A copy of this report should be forwarded by Shell Oil Company to the following agencies:

Alameda County Flood Control and
Water Conservation District (Zone 7)
5997 Parkside Drive
Pleasanton, California 94566
Attention: Mr. Craig Mayfield

Alameda County Health Care Services
Department of Environmental Health
80 Swan Way, Suite 200
Oakland, California 94621
Attention: Mr. Storm Goranson

California Regional Water Quality Control Board
San Francisco Bay Region
1800 Harrison Street, Suite 700
Oakland, California 94612-3429
Attention: Mr. Donald Dalke

DISCLAIMER

This report has been prepared solely for the use of Shell and any reliance on this report by third parties shall be as such party's sole risk.

LIMITATIONS

The discussion and recommendations presented in this report are based on the following:

1. The exploratory test borings drilled at the site.
2. The observations of field personnel.
3. Data obtained from the aquifer tests performed by EES.
4. Referenced documents.
5. Our understanding of the regulations of the State of California and the Alameda County and/or the City of Dublin.

It is possible that variations in the soil or groundwater conditions could exist beyond the points explored in this investigation. Also, changes in the groundwater conditions could occur at some time in the future due to variations in rainfall, temperature, regional water usage, or other factors.

The service performed by EES has been conducted in a manner consistent with the level of care and skill ordinarily exercised by members of our profession currently practicing under similar conditions in the Alameda County area. Please note that contamination of soil and groundwater must be reported to the appropriate agencies in a timely manner. No other warranty, expressed or implied, is made.

EES includes in this report chemical analytical data from a state-certified laboratory. The analytical results are performed according to procedures suggested by the U.S. EPA and State of California. EES is not responsible for laboratory errors in procedure or result reporting.

TABLE 1
GROUNDWATER ELEVATION DATA

Pre-Pump Test
June 28 through 30, 1989

Well No.	Date	Groundwater Elevation (ft. datum MSL)	Distance From RW-1 (ft.)
MW-1	6/29/89	326.23	25
MW-2	6/29/89	326.06	85
MW-3	6/29/89	326.36	160
MW-4	6/29/89	326.14	140
MW-6	6/29/89	326.12	135
MW-7	6/29/89	326.38	125
MW-8	6/29/89	326.40	275
MW-9	6/29/89	325.57	210
MW-10	6/29/89	326.32	175
MW-11	6/29/89	325.90	130
MW-12	6/29/89	325.53	275
RW-1	6/30/89	326.29	0

TABLE 2
GROUNDWATER ELEVATION DATA

Maximum Drawdown
14:03 August 4, 1989

Well Number	Groundwater Elevation (ft. datum MSL)
MW-1	324.13
MW-2	324.91
MW-3	325.88
MW-4	325.45
MW-6	325.62
MW-7	326.98
MW-8	326.14
MW-9	325.12
MW-10	325.88
MW-11	325.15
MW-12	325.38
RW-1	321.74

TABLE 3
MAXIMUM DRAWDOWN DATA

Ends of Pump Test
14:03 August 4, 1989

Well Number	Groundwater Elevation (ft. datum MSL)
MW-1	-1.84
MW-2	-0.89
MW-3	-0.22
MW-4	-0.43
MW-6	-0.24
MW-7	0.00
MW-8	0.00
MW-9	-0.19
MW-10	-0.18
MW-11	-0.49
MW-12	0.00
RW-1	-4.29

TABLE 4
AQUIFER CHARACTERISTICS

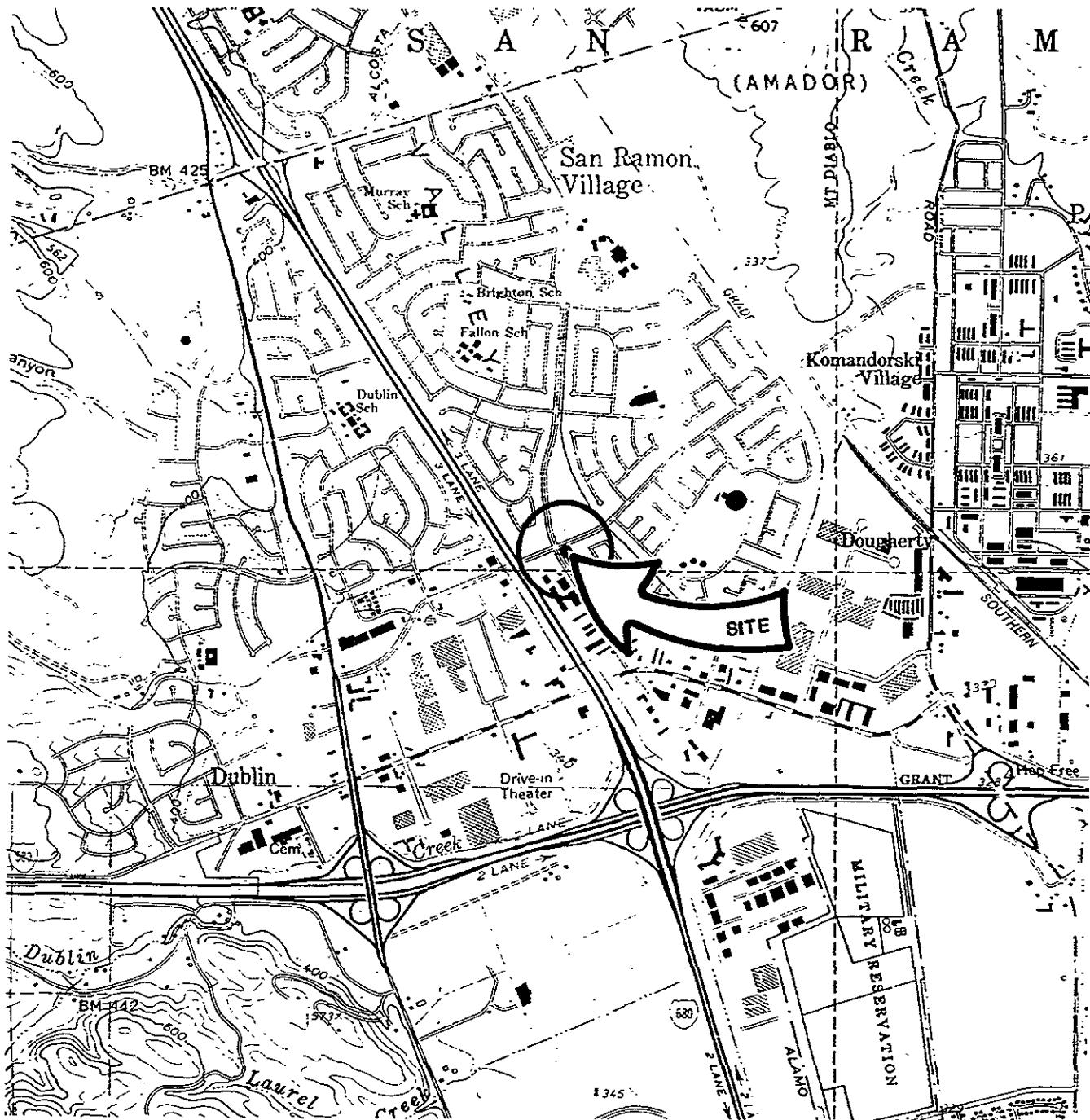
Constant Discharge Pump Test Analysis
August 1 through 4, 1989

Well Number	Transmissivity (gpd/ft.)	Saturated Aquifer Thickness (ft.)	Hydraulic Conductivity (gpd/ft ²)	Storativity Coeffecient
MW-1	844	17.3	48.9	0.185
MW-2	1160	14.8	78.7	0.00172
MW-3	2020	15.1	134	0.00202
MW-4	1610	14.7	110	0.00262
MW-6	2550	13.8	185	0.00221
MW-8	2670	6.92	386	0.00426
MW-9	1890	9.36	202	0.00292
MW-10	1930	8.90	217	0.00370
MW-11	1430	8.42	170	0.00309
MW-12	5450	10.3	527	0.00804
RW-1	433	20.6	21.0	0.226

TABLE 5
GROUNDWATER ELEVATION DATA

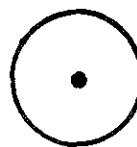
Maximum Drawdown
14:03 August 4, 1989

Well Number	Groundwater Elevation (ft. datum MSL)
MW-1	326.21
MW-2	325.98
MW-3	326.33
MW-4	326.02
MW-6	325.69
MW-7	326.98
MW-8	326.14
MW-9	325.13
MW-10	325.47
MW-11	325.22
MW-12	325.38
RW-1	325.31



SOURCE: USGS 7.5' MAP, DUBLIN QUADRANGLE

LEGEND



SITE LOCATION

0 1
SCALE IN MILES



SITE LOCATION MAP

FORMER SHELL STATION

7194 AMADOR VALLEY BLVD

DUBLIN, CALIFORNIA

REVIEWED BY

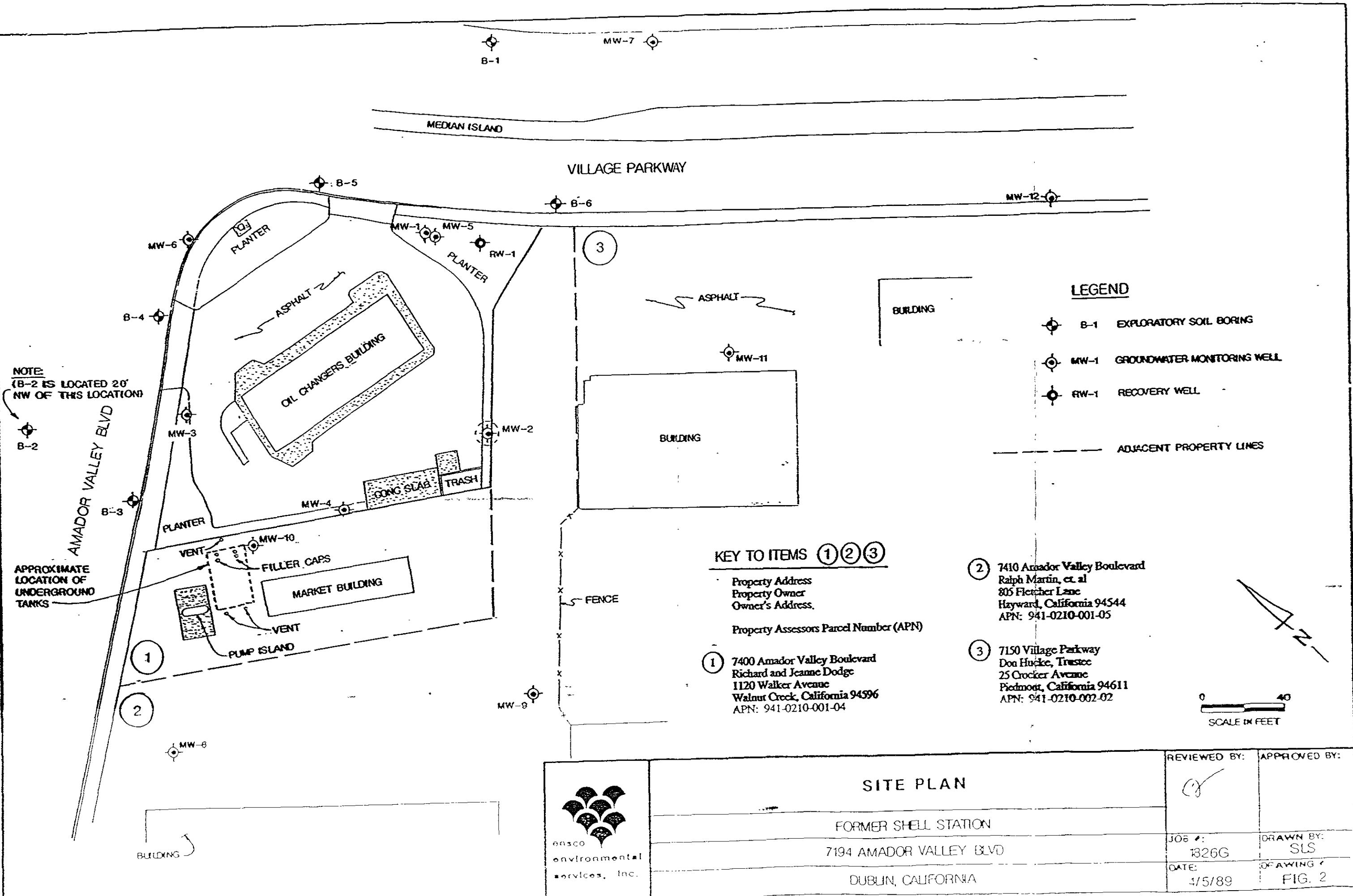
APPROVED BY

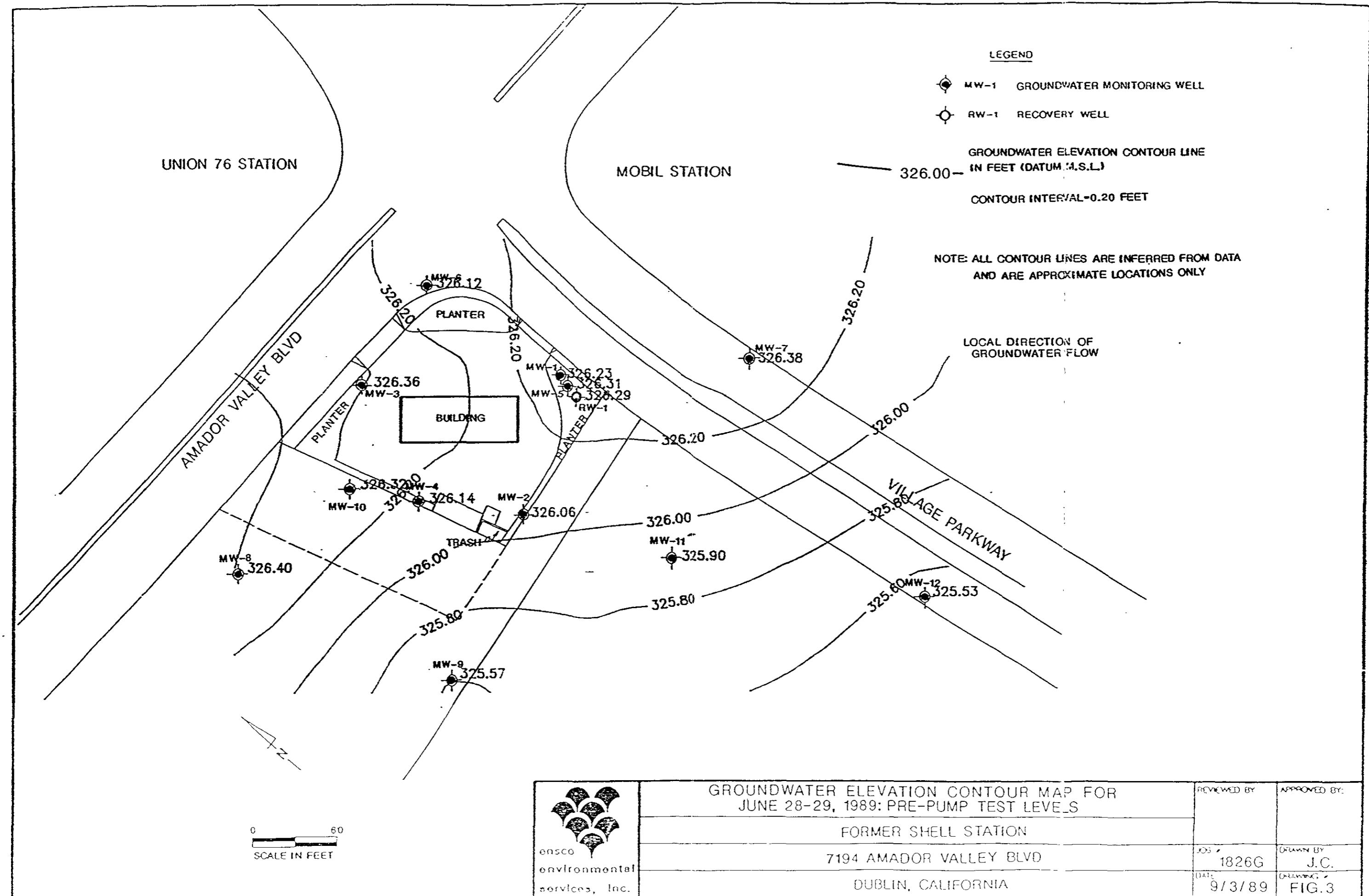
JOB #
1826G

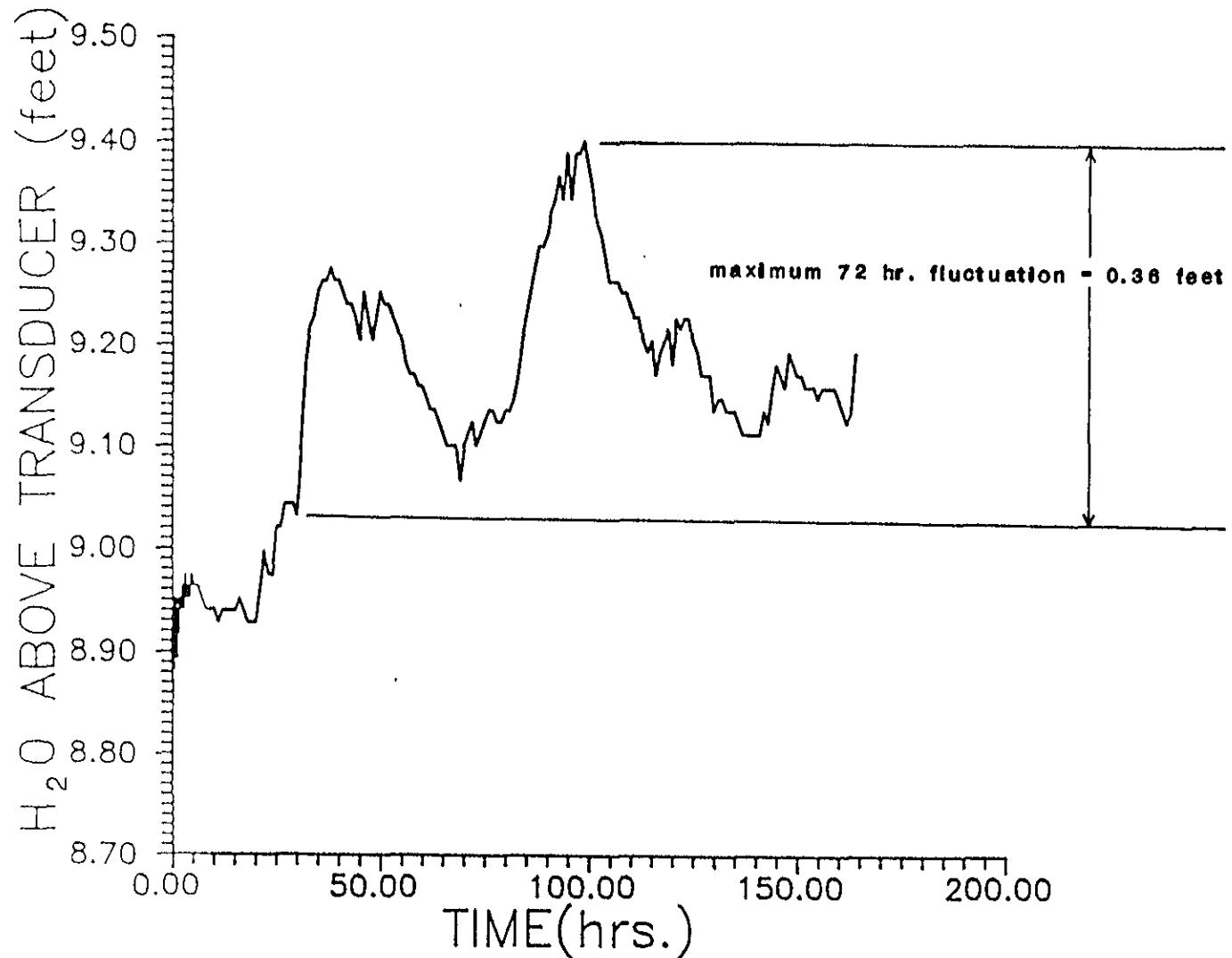
DRAWN BY
J.C.

DATE
4-5-89

DRAWING #
FIG. 1







RW-1 GROUNDWATER LEVEL BACKGROUND FLUCTUATIONS (JULY 20-27, 1989)

FORMER SHELL SERVICE STATION

7194 AMADOR VALLEY BLVD.

DUBLIN, CALIFORNIA

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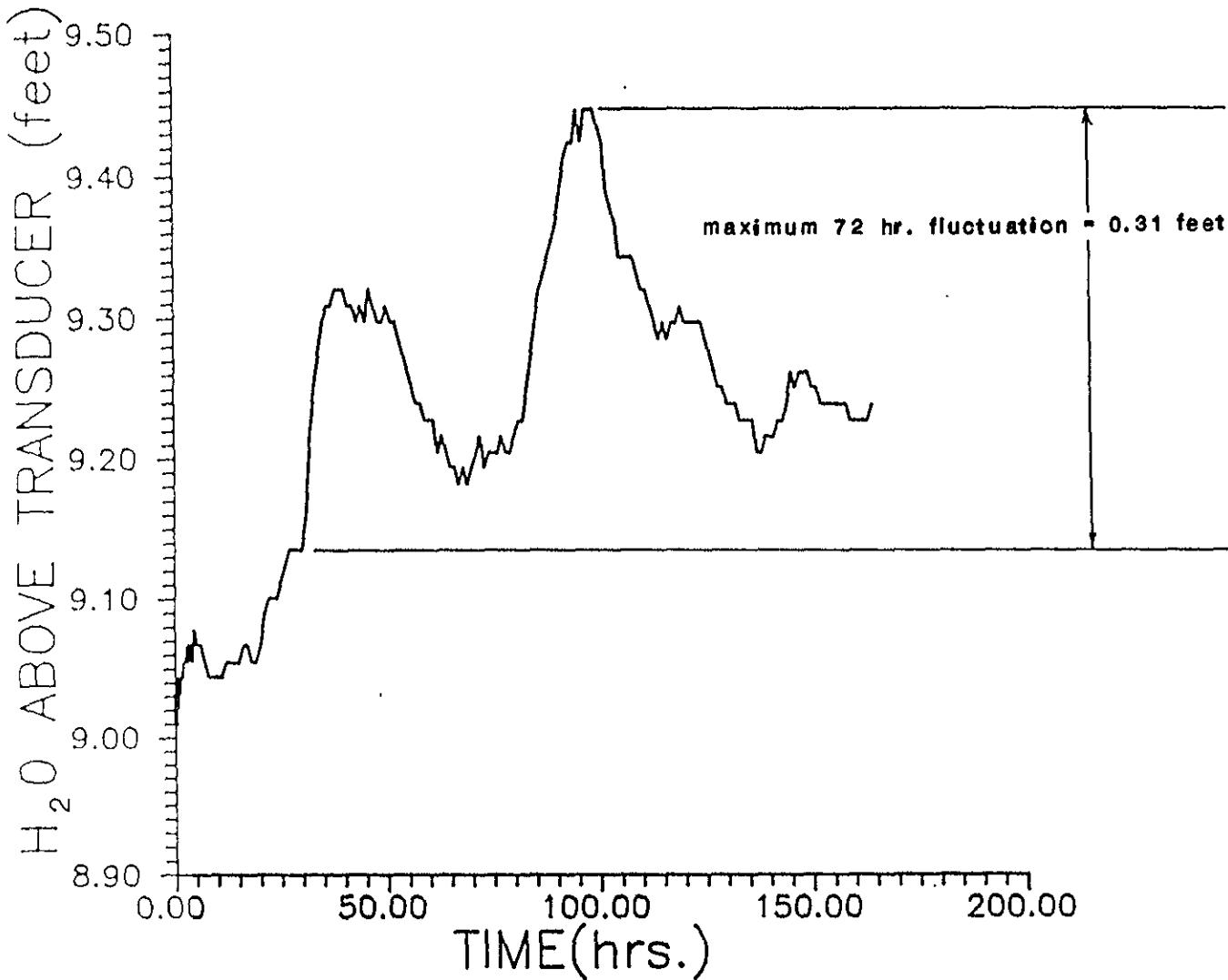
APPROVED BY

JOB
1826G

DRAWN BY
J.C.

DATE
8-25-89

DRAWING
FIG. 4



**MW-1 GROUNDWATER LEVEL BACKGROUND FLUCTUATIONS
(JULY 20-27, 1989)**

FORMER SHELL SERVICE STATION

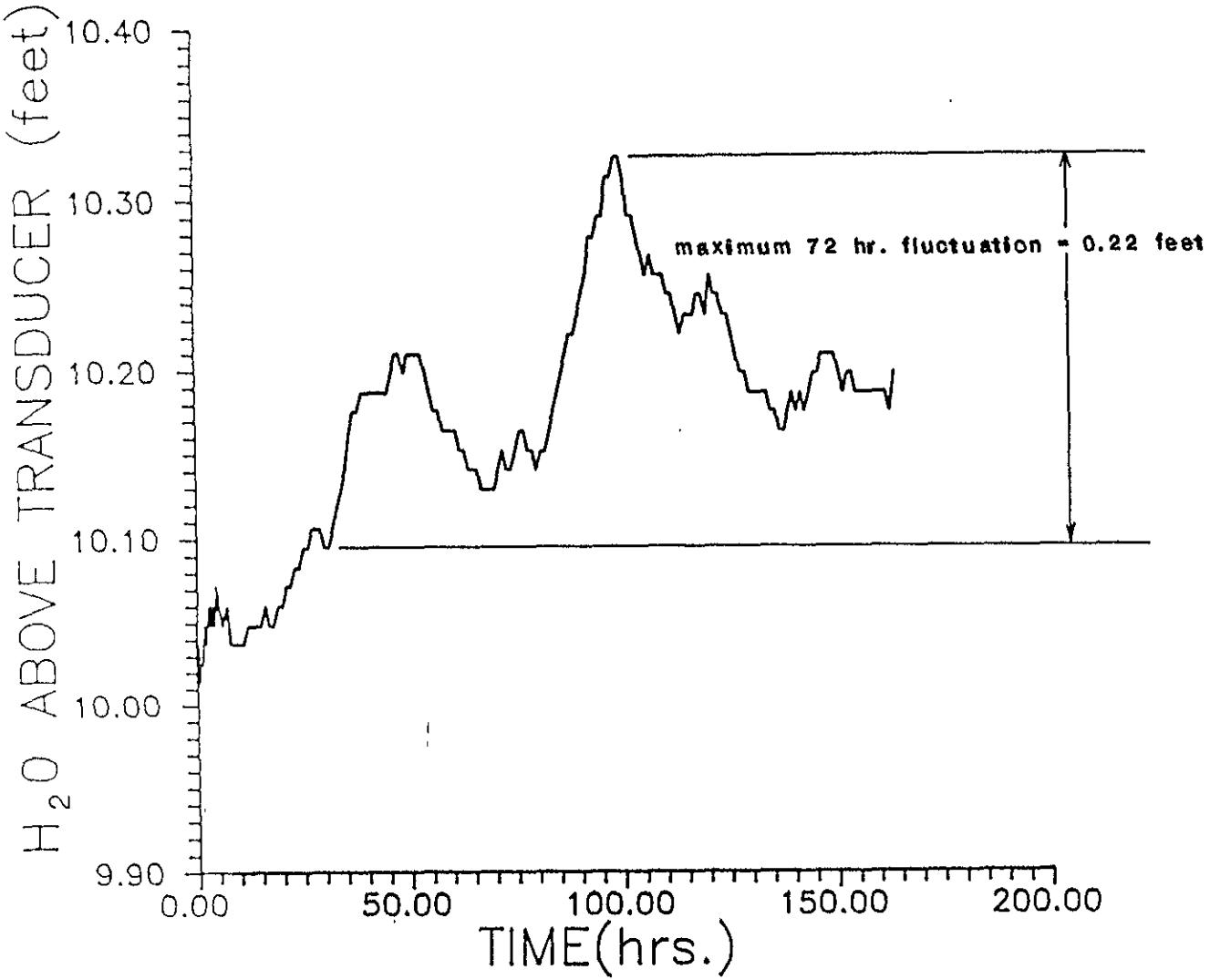
7194 AMADOR VALLEY BLVD.

DUBLIN, CALIFORNIA

REVIEWED BY: APPROVED BY:

JOB # 1826G DRAWN BY: J.C.

DATE: 8-25-89 DRAWING # FIG. 5



**MW-2 GROUNDWATER LEVEL BACKGROUND FLUCTUATIONS
(JULY 20-27, 1989)**

FORMER SHELL SERVICE STATION

7194 AMADOR VALLEY BLVD.

DUBLIN, CALIFORNIA

REVIEWED BY

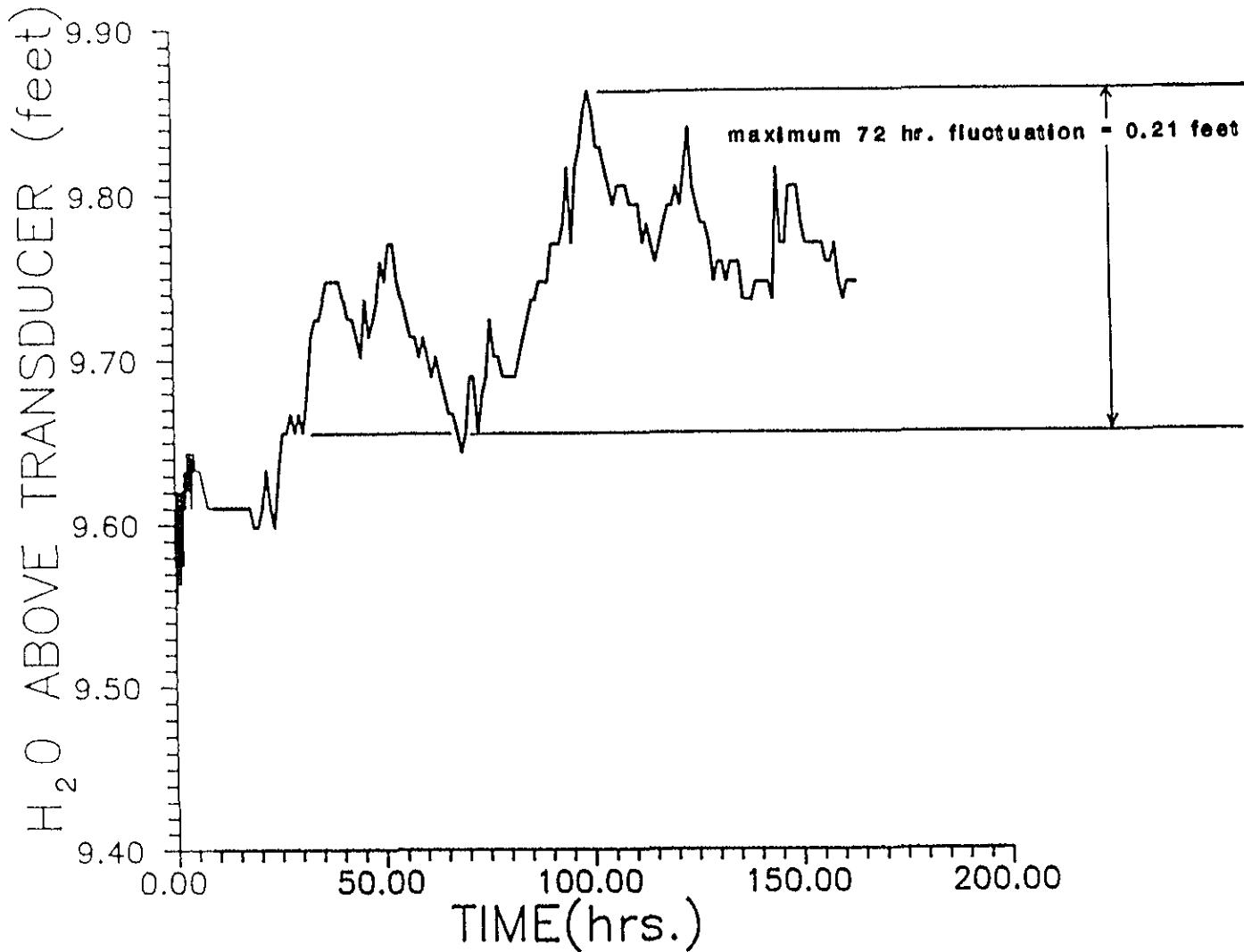
APPROVED BY

JOB #
1826G

DRAWN BY
J.C.

DATE
8-25-89

DRAWING #
FIG. 6



**MW-3 GROUNDWATER LEVEL BACKGROUND FLUCTUATIONS
(JULY 20-27, 1989)**

FORMER SHELL SERVICE STATION

7194 AMADOR VALLEY BLVD.

DUBLIN, CALIFORNIA

REVIEWED BY:

APPROVED BY:

JOB #

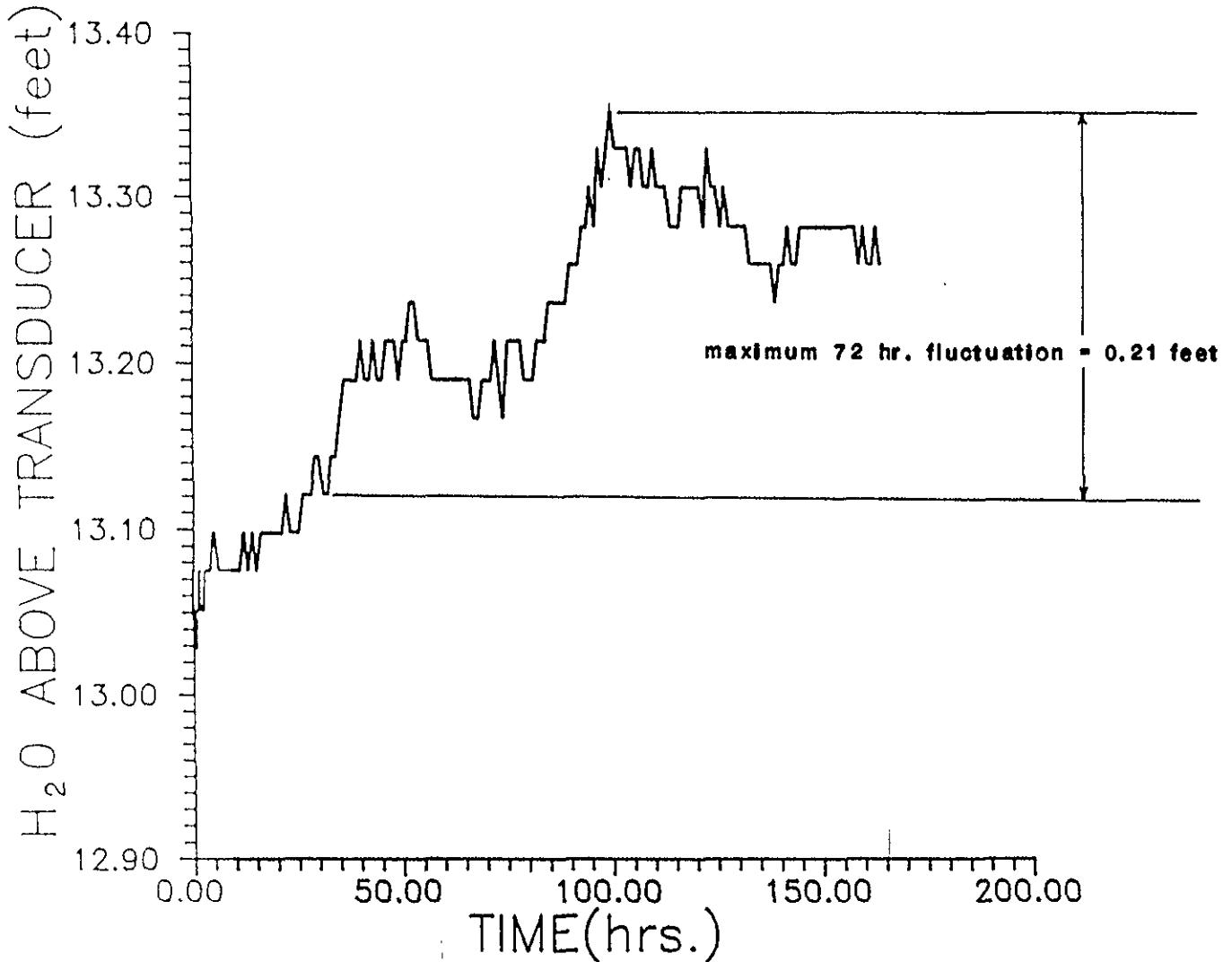
1826G

DRAWN BY:
J.C.

DATE:

8-25-89

DRAWING #:
FIG. 7



**MW-4 GROUNDWATER LEVEL BACKGROUND FLUCTUATIONS
(JULY 20-27, 1989)**

FORMER SHELL SERVICE STATION

7194 AMADOR VALLEY BLVD.

DUBLIN, CALIFORNIA

REVIEWED BY:

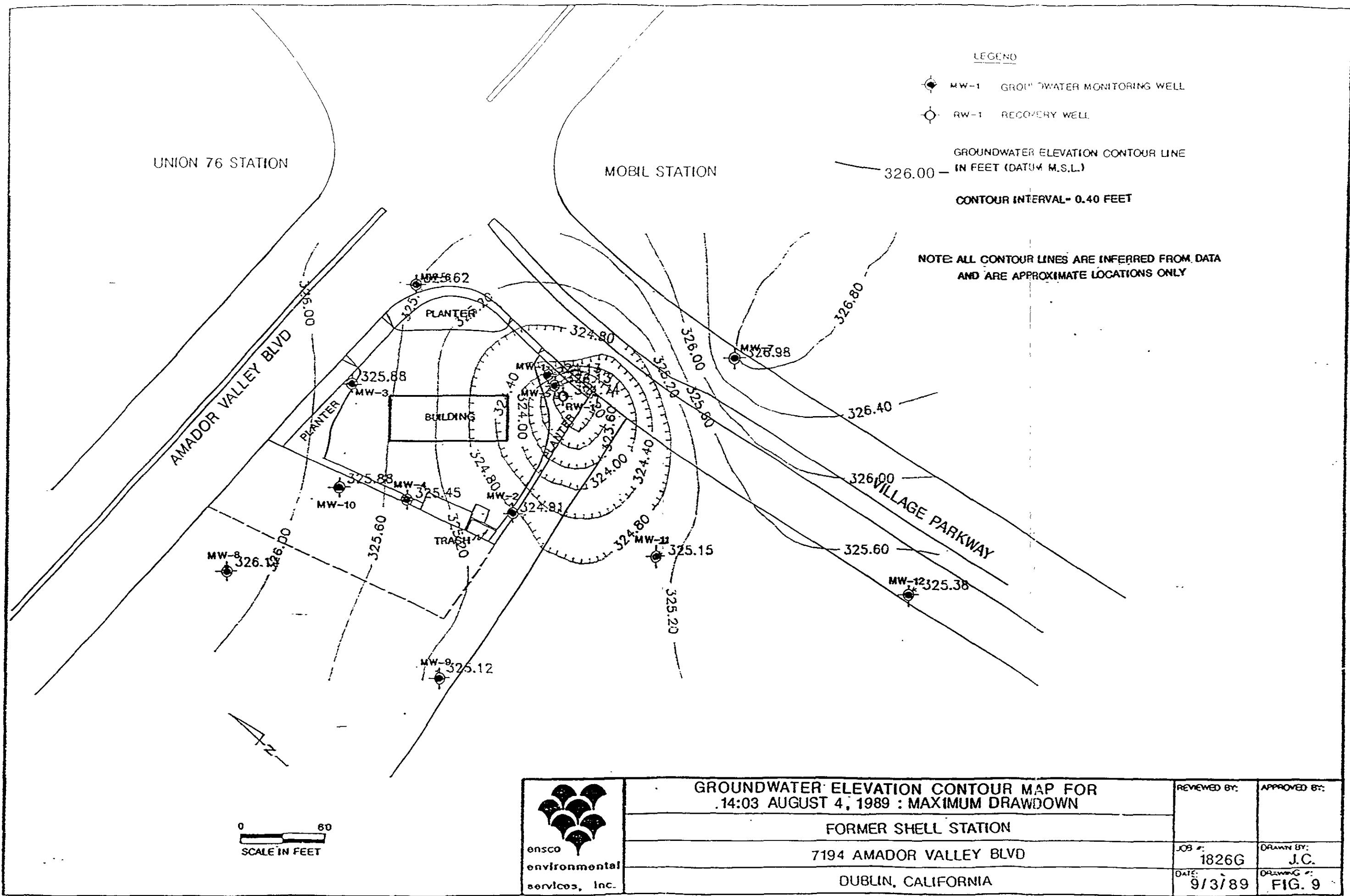
APPROVED BY:

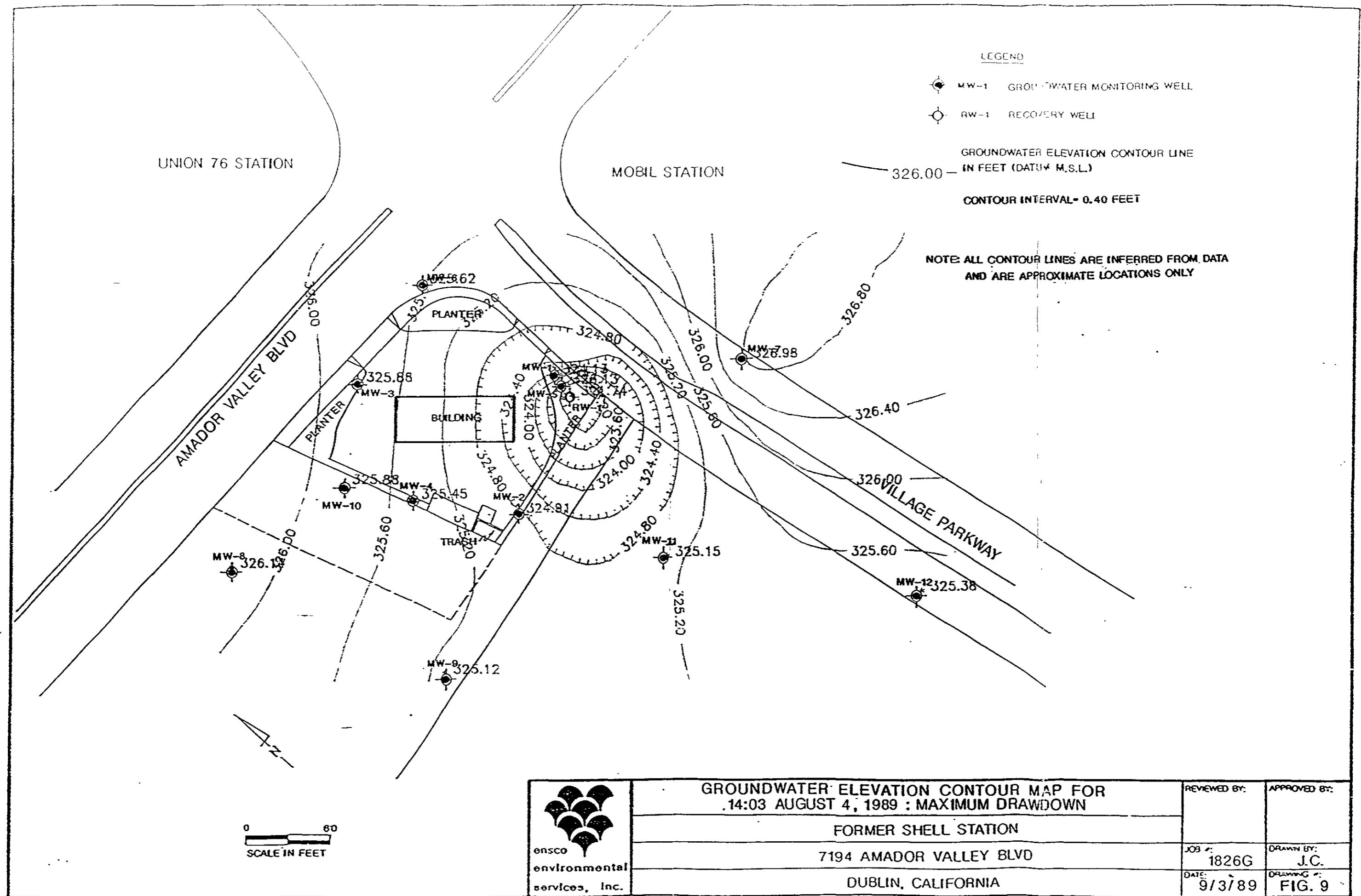
JOB #
1826G

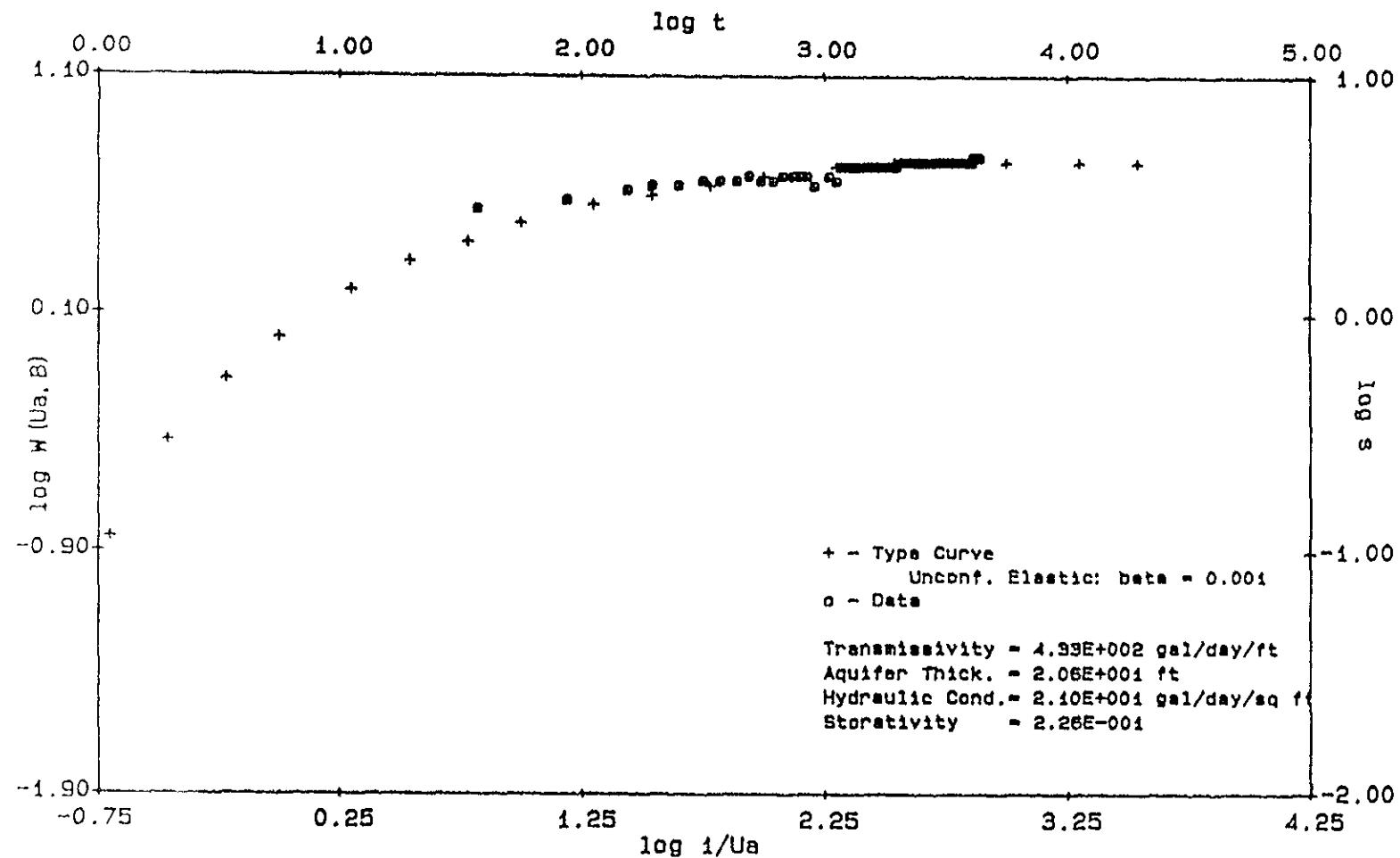
DRAWN BY
J.C.

DATE
8-25-89

DRAWING
FIG. 8







RW-1 CONSTANT DISCHARGE PUMP TEST ANALYSIS (AUGUST 1-4, 1989)

FORMER SHELL SERVICE STATION

7194 AMADOR VALLEY BLVD.

DUBLIN, CALIFORNIA

REVIEWED BY:

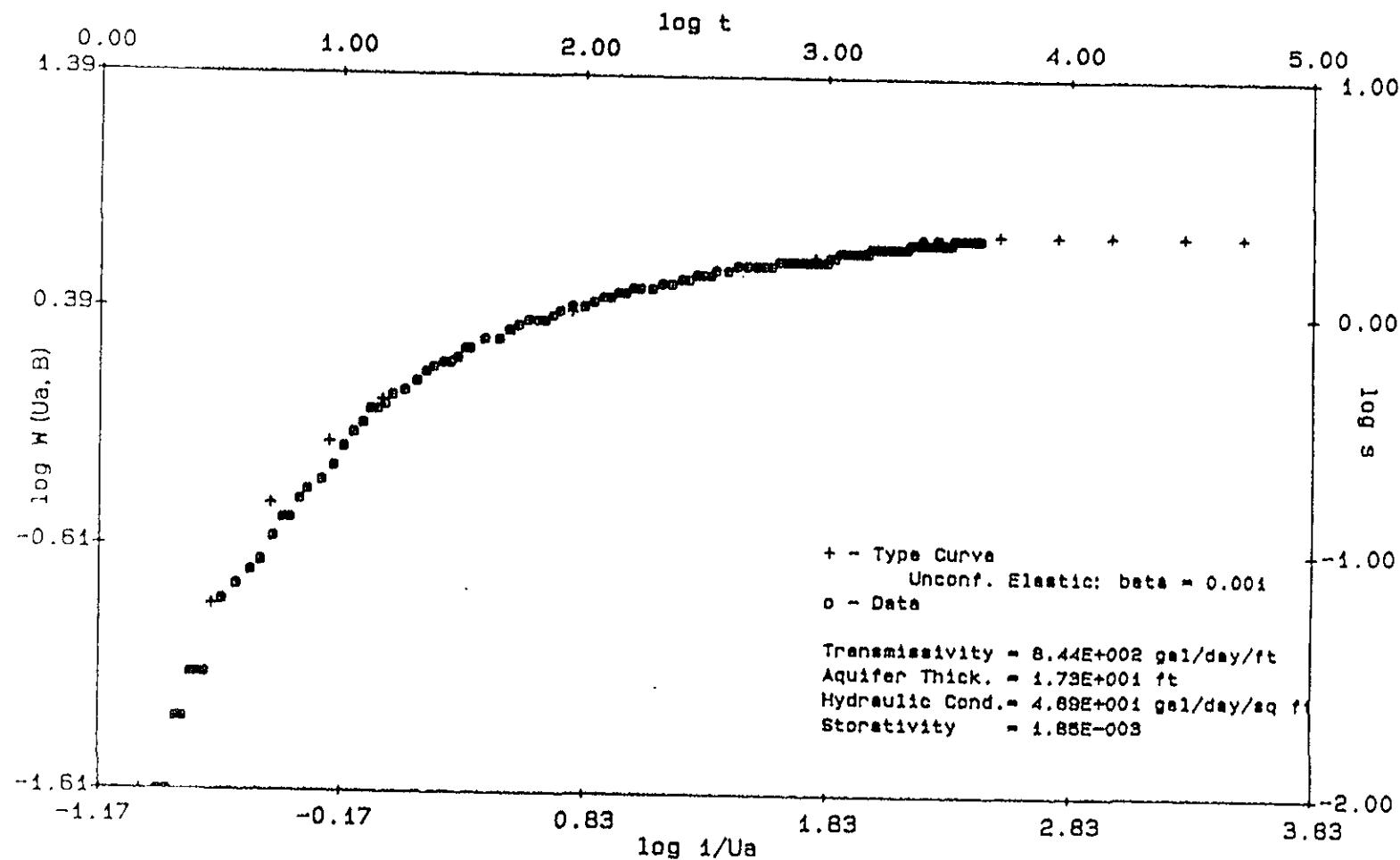
APPROVED BY:

JOB #
1826G

DRAWN BY:
J.C.

DATE:
8-25-89

DRAWING #: FIG. 11



**MW-1 CONSTANT DISCHARGE PUMP TEST ANALYSIS
(AUGUST 1-4, 1989)**

FORMER SHELL SERVICE STATION

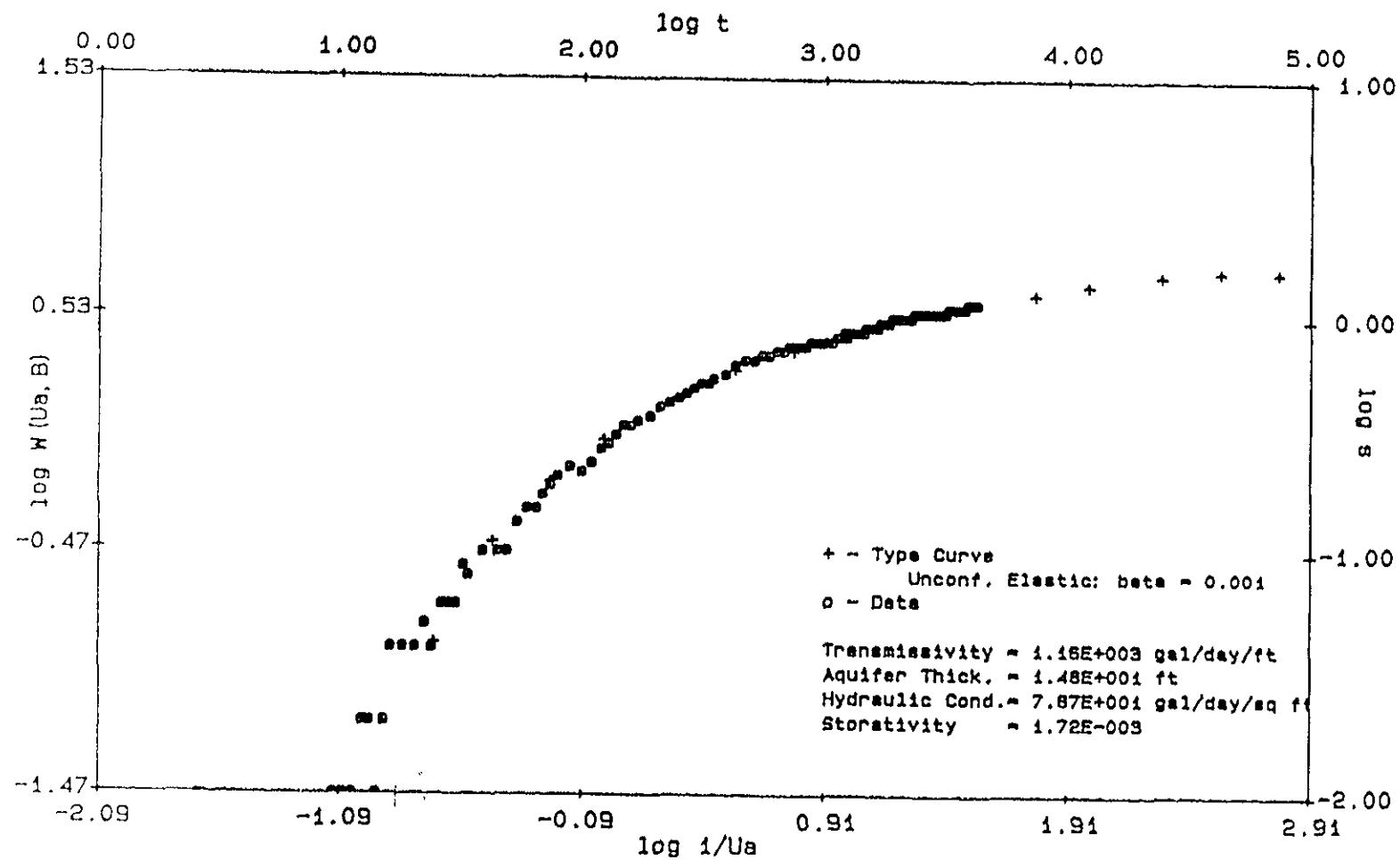
7194 AMADOR VALLEY BLVD.
DUBLIN, CALIFORNIA

REVIEWED BY: _____

APPROVED BY: _____

JOB # 1826G DRAWN BY J.C.

DATE: 8-25-89 DRAWING # FIG. 12

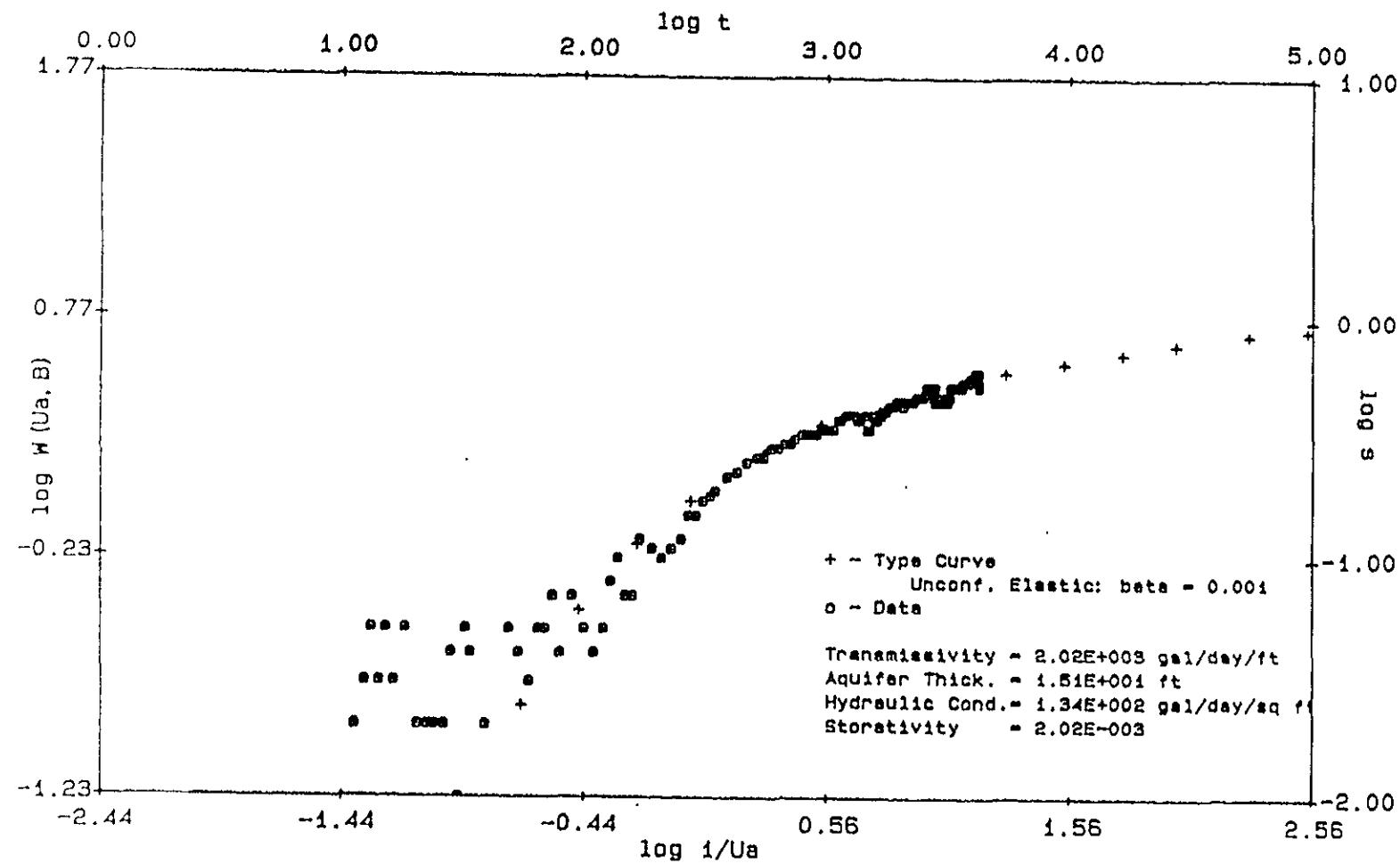


MW-2 CONSTANT DISCHARGE PUMP TEST ANALYSIS
(AUGUST 1-4, 1989)

FORMER SHELL SERVICE STATION

7194 AMADOR VALLEY BLVD.
 DUBLIN, CALIFORNIA

REVIEWED BY:	APPROVED BY:
JOB # 1826G	DRAWN BY J.C.
DATE: 8-25-89	DRAWING # FIG. 13



**MW-3 CONSTANT DISCHARGE PUMP TEST ANALYSIS
(AUGUST 1-4, 1989)**

FORMER SHELL SERVICE STATION

7194 AMADOR VALLEY BLVD.
DUBLIN, CALIFORNIA

REVIEWED BY:

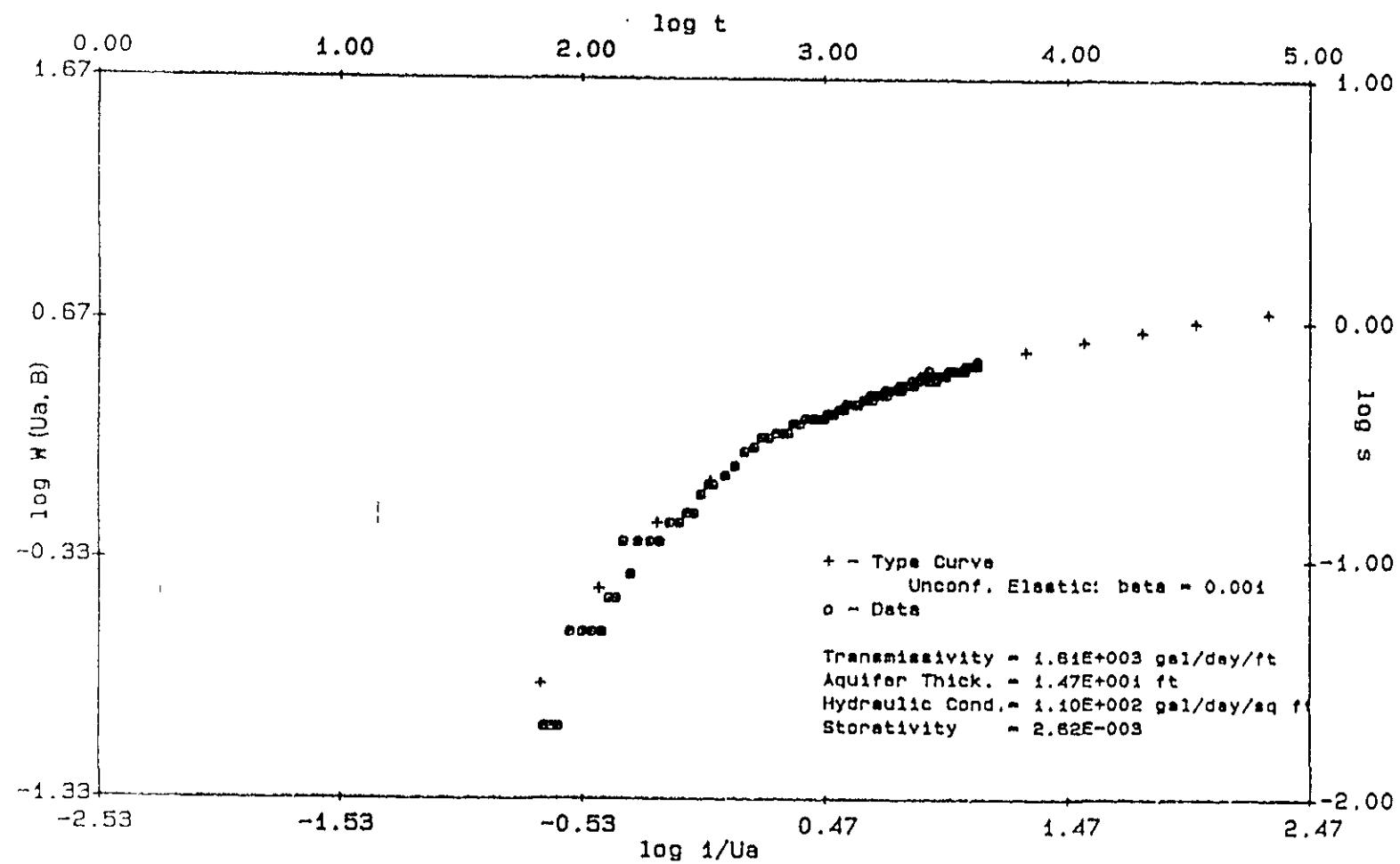
APPROVED BY:

JOB #:
1826G

DRAWN BY:
J.C.

DATE:
8-25-89

DRAWING #:
FIG. 14

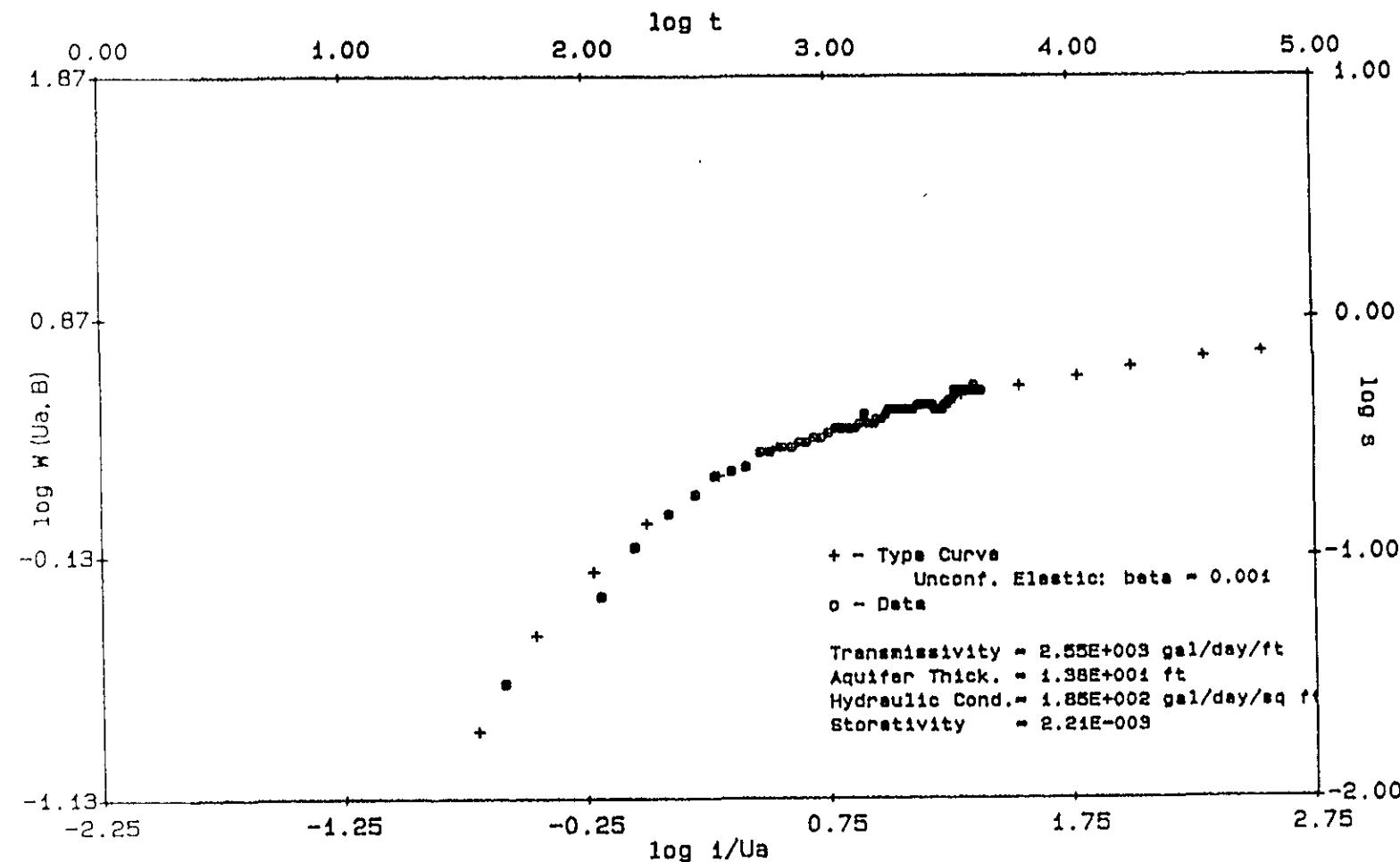


MW-4 CONSTANT DISCHARGE PUMP TEST ANALYSIS (AUGUST 1-4, 1989)

FORMER SHELL SERVICE STATION

7194 AMADOR VALLEY BLVD.
DUBLIN, CALIFORNIA

REVIEWED BY:	APPROVED BY:
JOB #: 1826G	DRAWN BY: J.C.
DATE: 8-25-89	DRAWING #: FIG. 15



MW-6 CONSTANT DISCHARGE PUMP TEST ANALYSIS (AUGUST 1-4, 1989)

FORMER SHELL SERVICE STATION

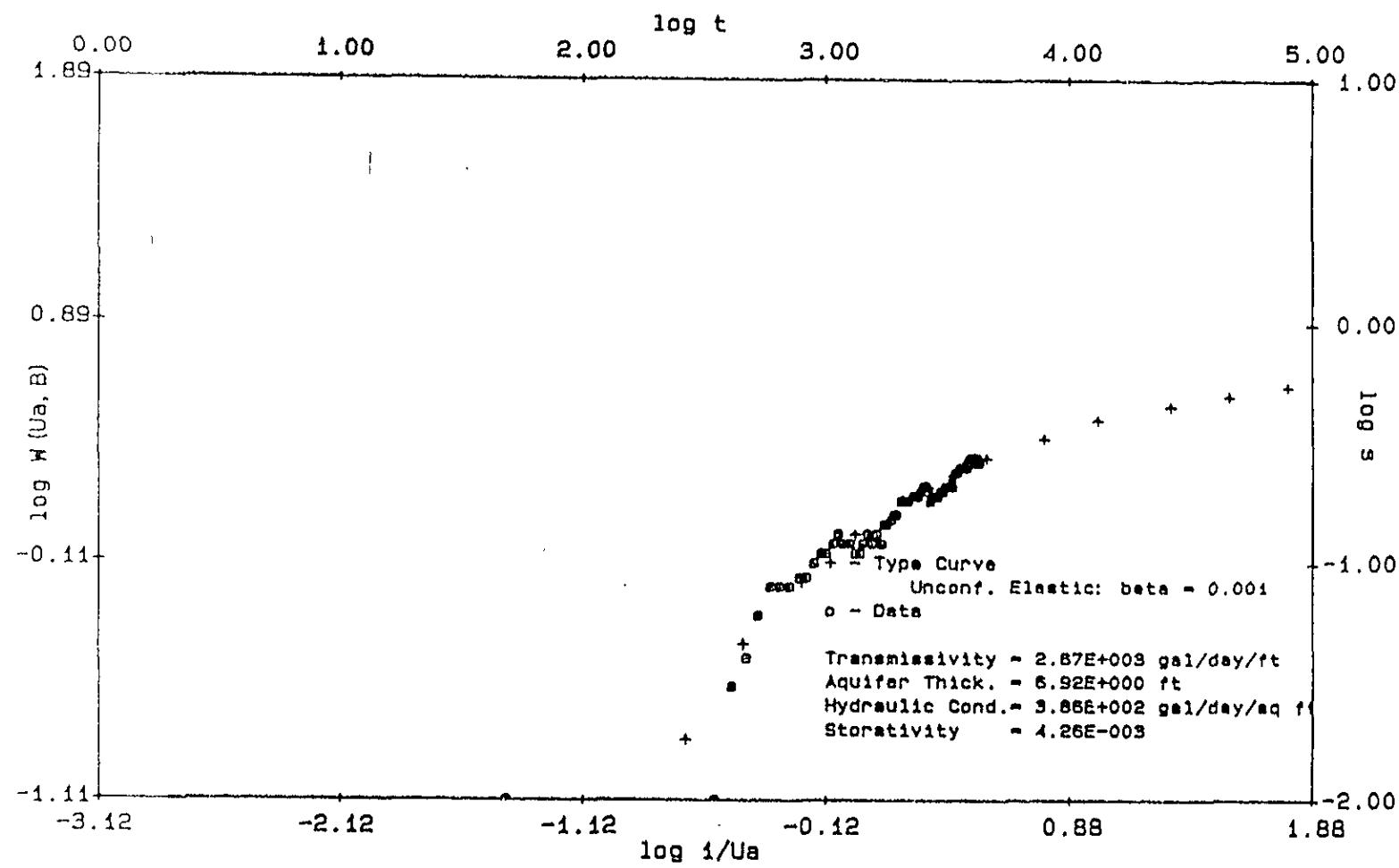
7194 AMADOR VALLEY BLVD.

DUBLIN, CALIFORNIA

REVIEWED BY: APPROVED BY:

JOB #: 1826G DRAWN BY: J.C.

DATE: 8-25-89 DRAWING #: FIG. 16



MW-8 CONSTANT DISCHARGE PUMP TEST ANALYSIS
(AUGUST 1-4, 1989)

FORMER SHELL SERVICE STATION

7194 AMADOR VALLEY BLVD.

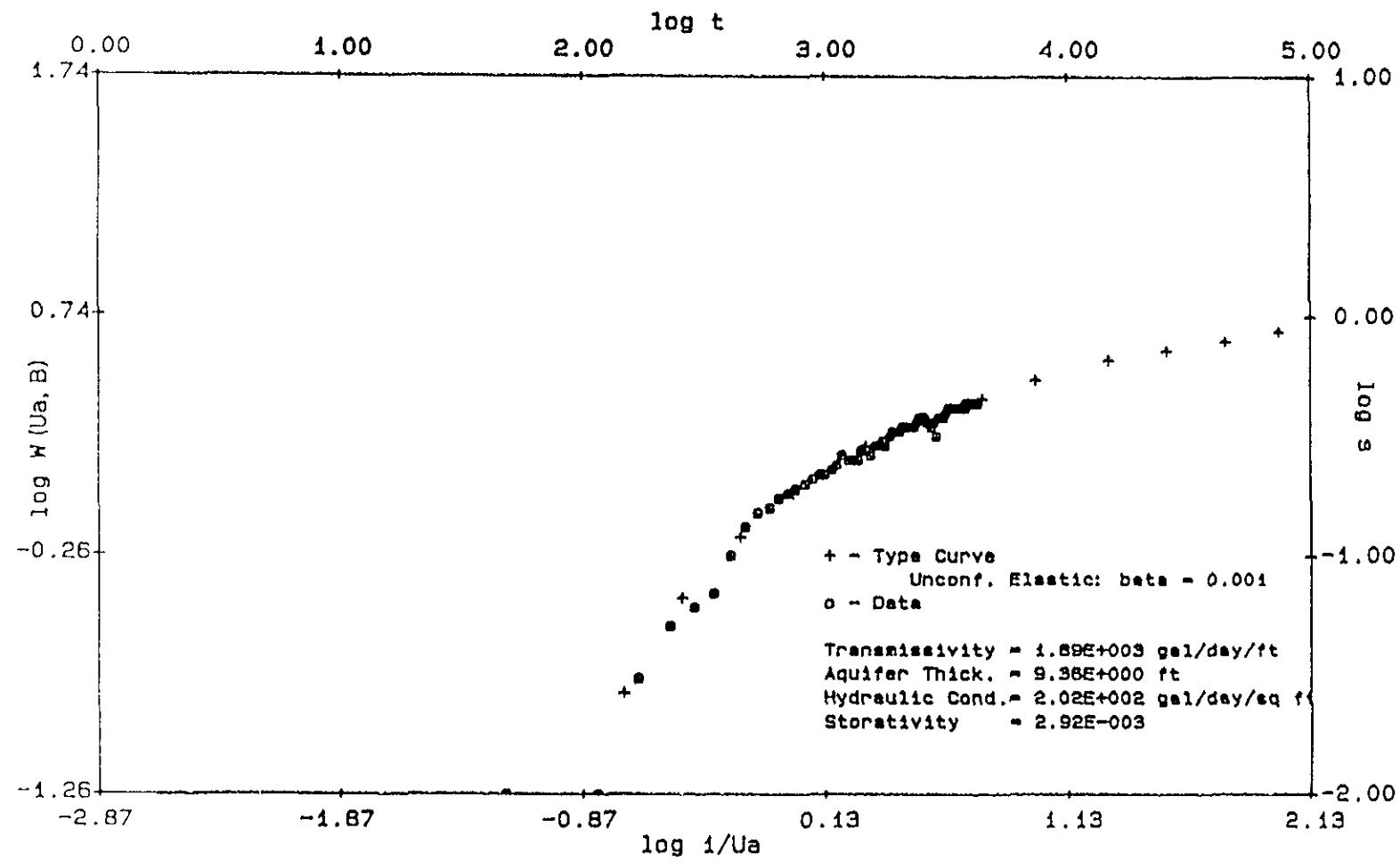
DUBLIN, CALIFORNIA

REVIEWED BY: _____

APPROVED BY: _____

JOB #: 1826G DRAWN BY: J.C.

DATE: 8-25-89 DRAWING #: FIG. 17



MW-9 CONSTANT DISCHARGE PUMP TEST ANALYSIS (AUGUST 1-4, 1989)

FORMER SHELL SERVICE STATION

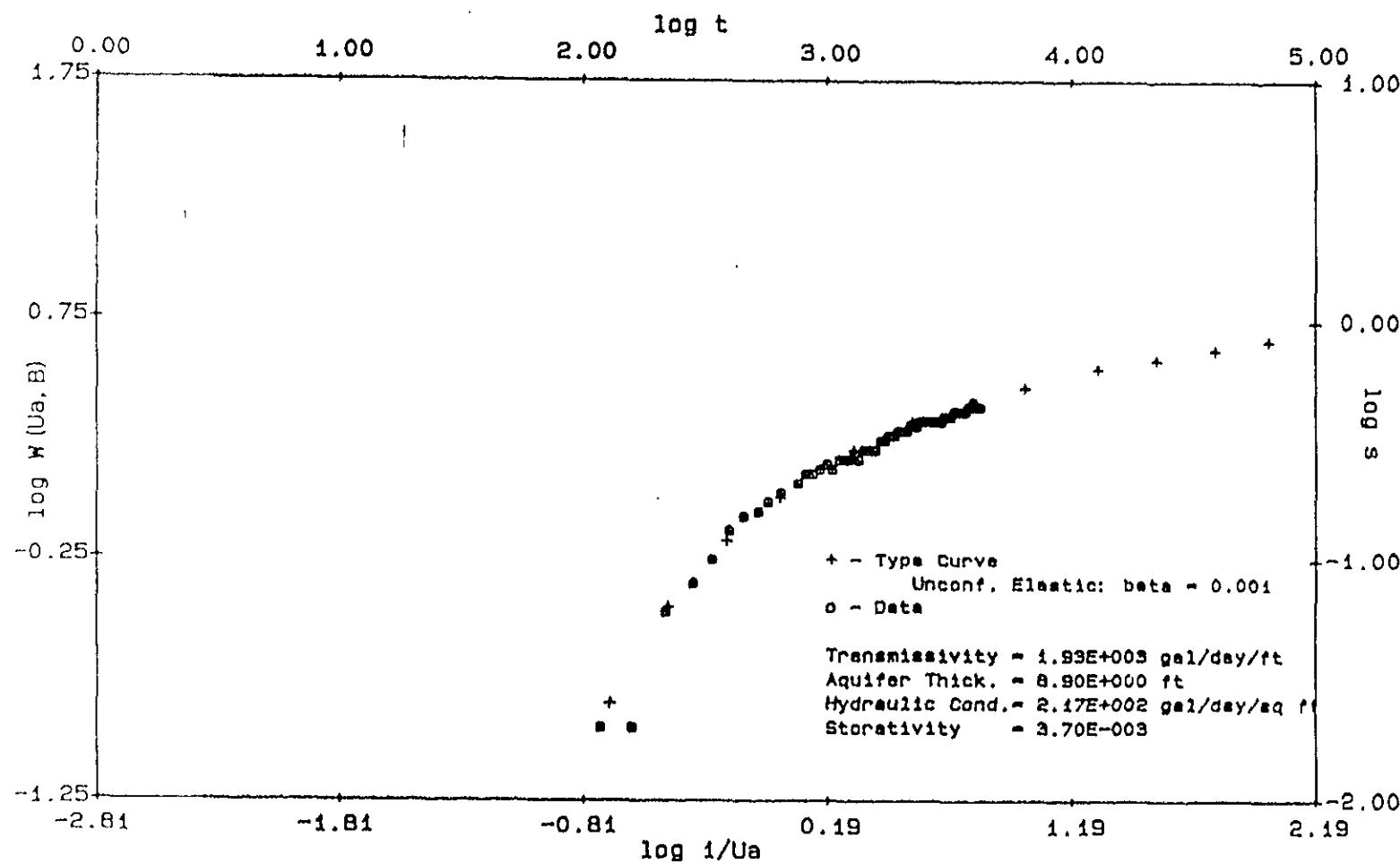
7194 AMADOR VALLEY BLVD.

DUBLIN, CALIFORNIA

REVIEWED BY: APPROVED BY:

JOB #: 1826G DRAWN BY: J.C.

DATE: 8-25-89 DRAWING #: FIG. 18

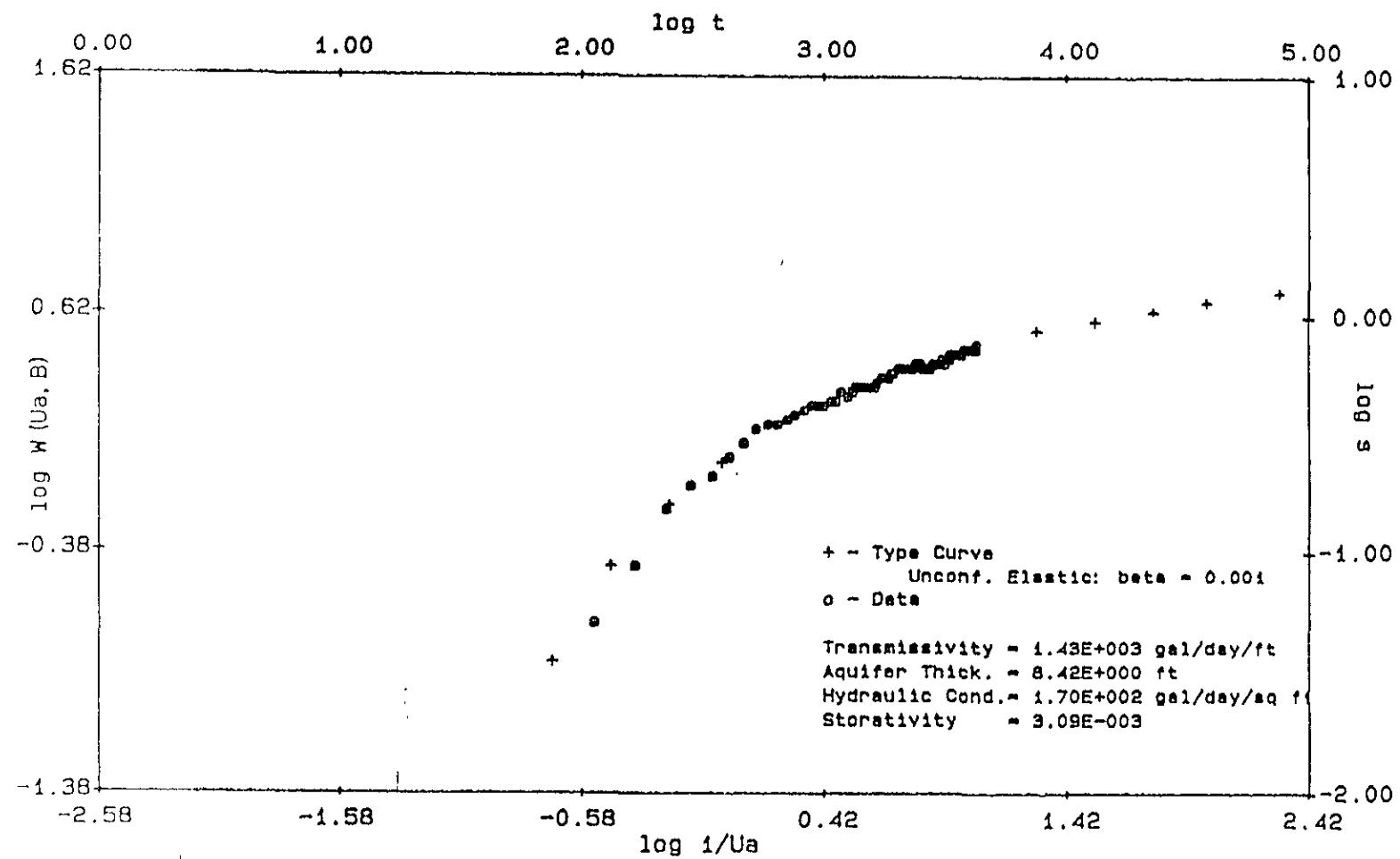


MW-10 CONSTANT DISCHARGE PUMP TEST ANALYSIS (AUGUST 1-4, 1989)

FORMER SHELL SERVICE STATION

7194 AMADOR VALLEY BLVD.
DUBLIN, CALIFORNIA

REVIEWED BY:	APPROVED BY:
JOE 1826G	DRAWN BY: J.C.
DRAWING #: FIG. 19	

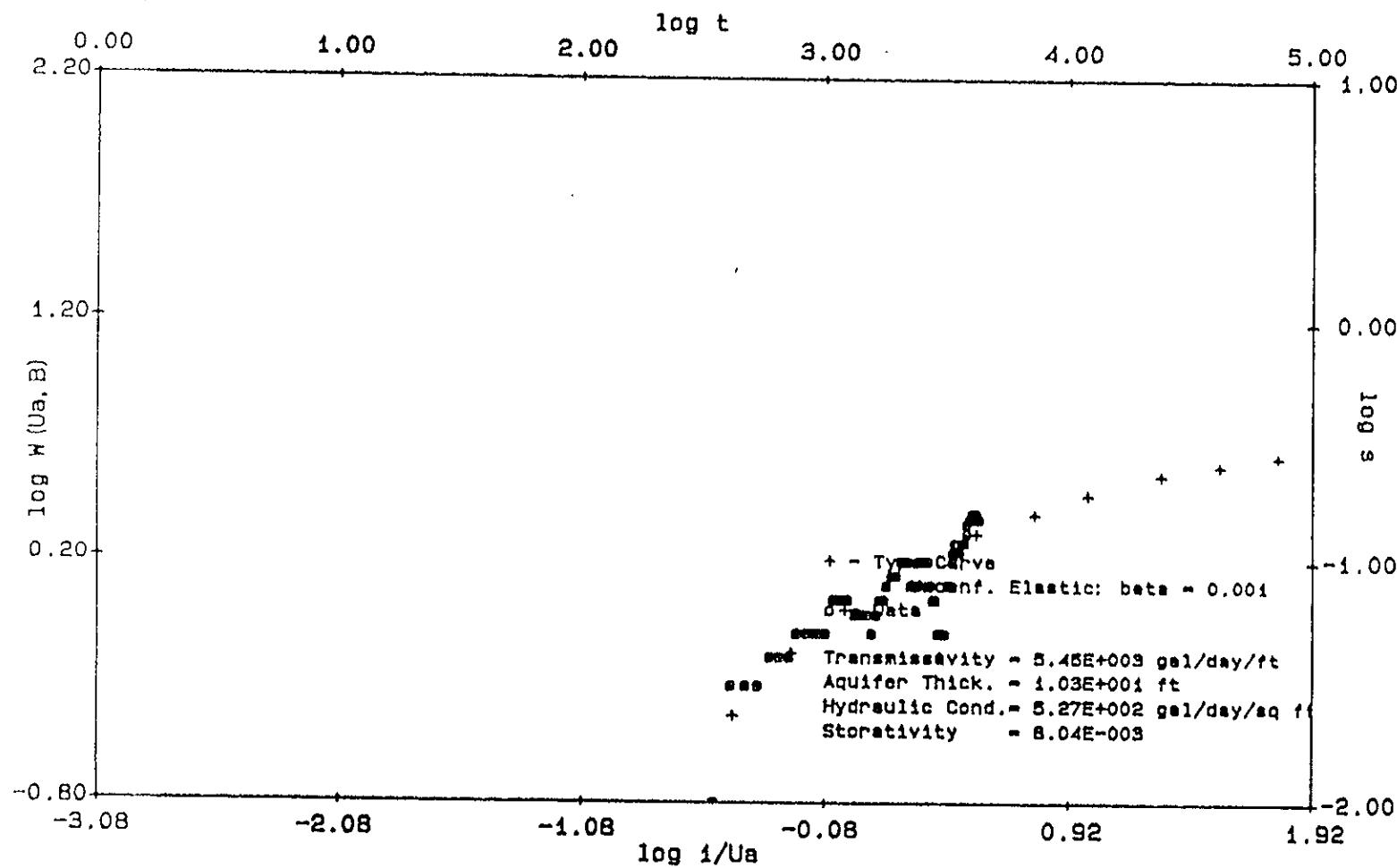


MW-11 CONSTANT DISCHARGE PUMP TEST ANALYSIS (AUGUST 1-4, 1989)

FORMER SHELL SERVICE STATION

7194 AMADOR VALLEY BLVD.
DUBLIN, CALIFORNIA

REVIEWED BY:	APPROVED BY:
JOB #: 1826G	DRAWN BY: J.C.
DATE: 8-25-89	DRAWING #: FIG. 20



MW-12 CONSTANT DISCHARGE PUMP TEST ANALYSIS
(AUGUST 1-4, 1989)

FORMER SHELL SERVICE STATION

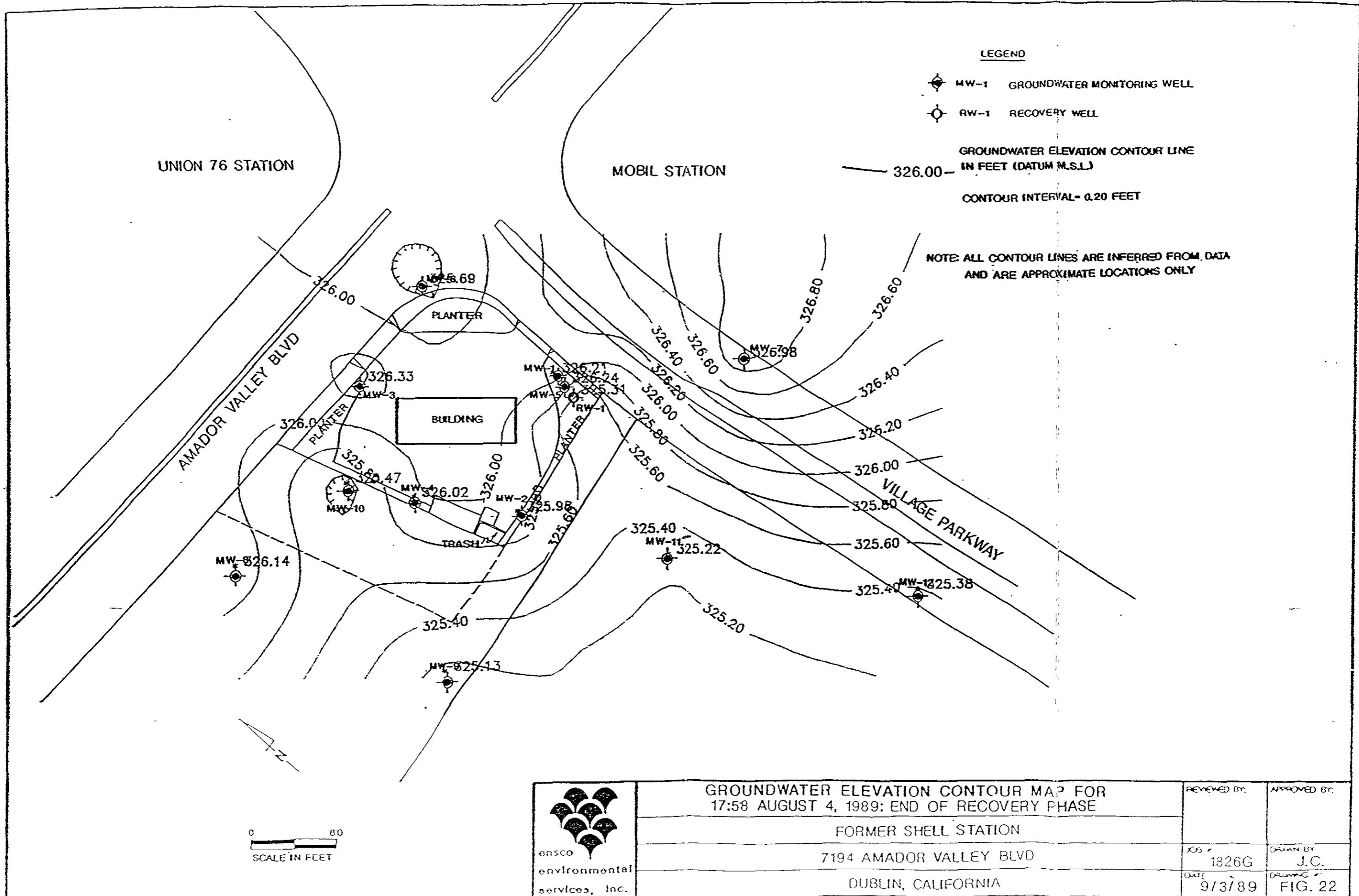
7194 AMADOR VALLEY BLVD.

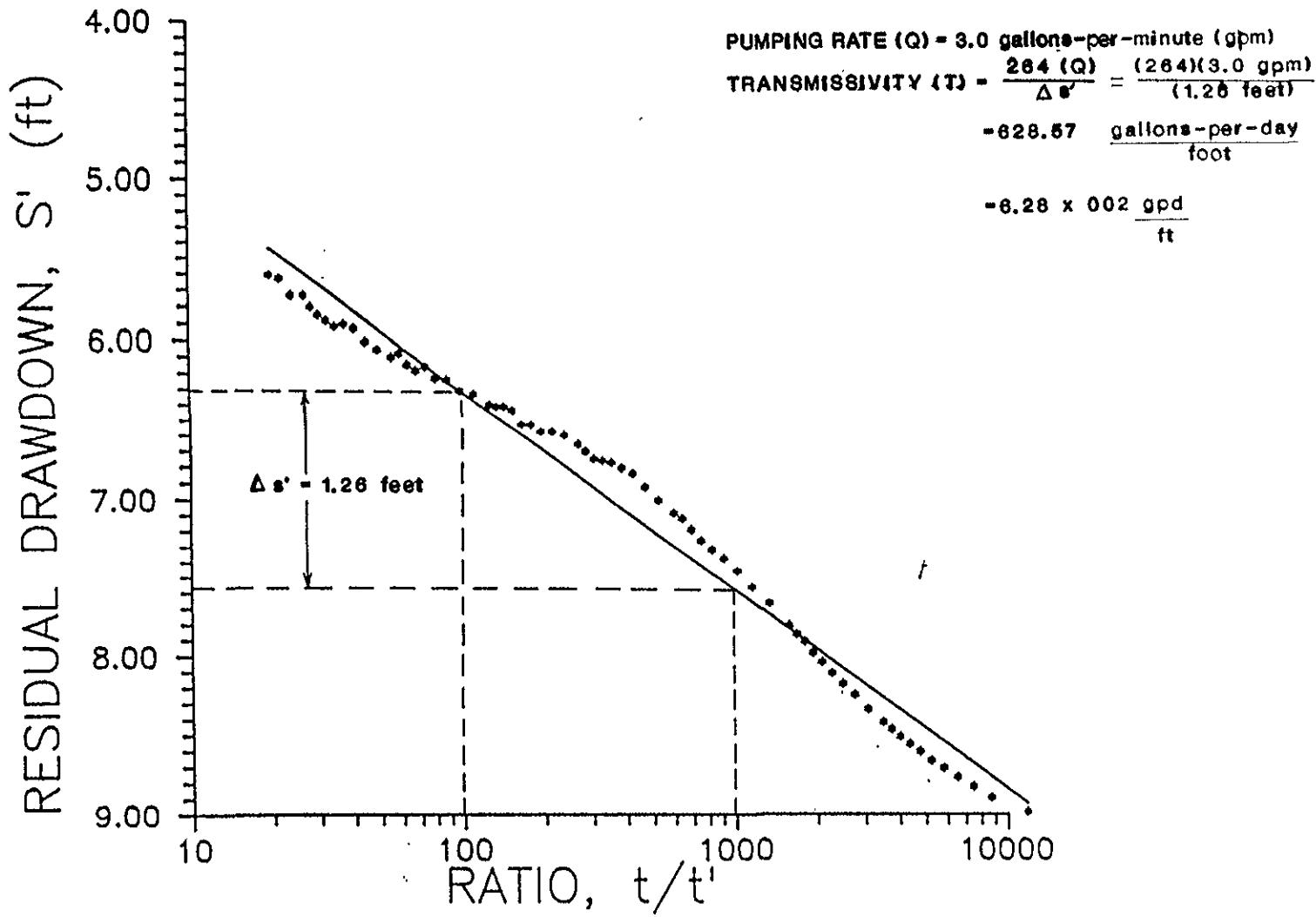
DUBLIN, CALIFORNIA

REVIEWED BY: APPROVED BY:

JOB #: 1826G DRAWN BY: J.C.

DATE: 8-25-89 DRAWING #: FIG. 21





**RW-1 RECOVERY TEST ANALYSIS
(AUGUST 4, 1989)**

FORMER SHELL SERVICE STATION

7194 AMADOR VALLEY BLVD

DUBLIN, CALIFORNIA

REVIEWED BY

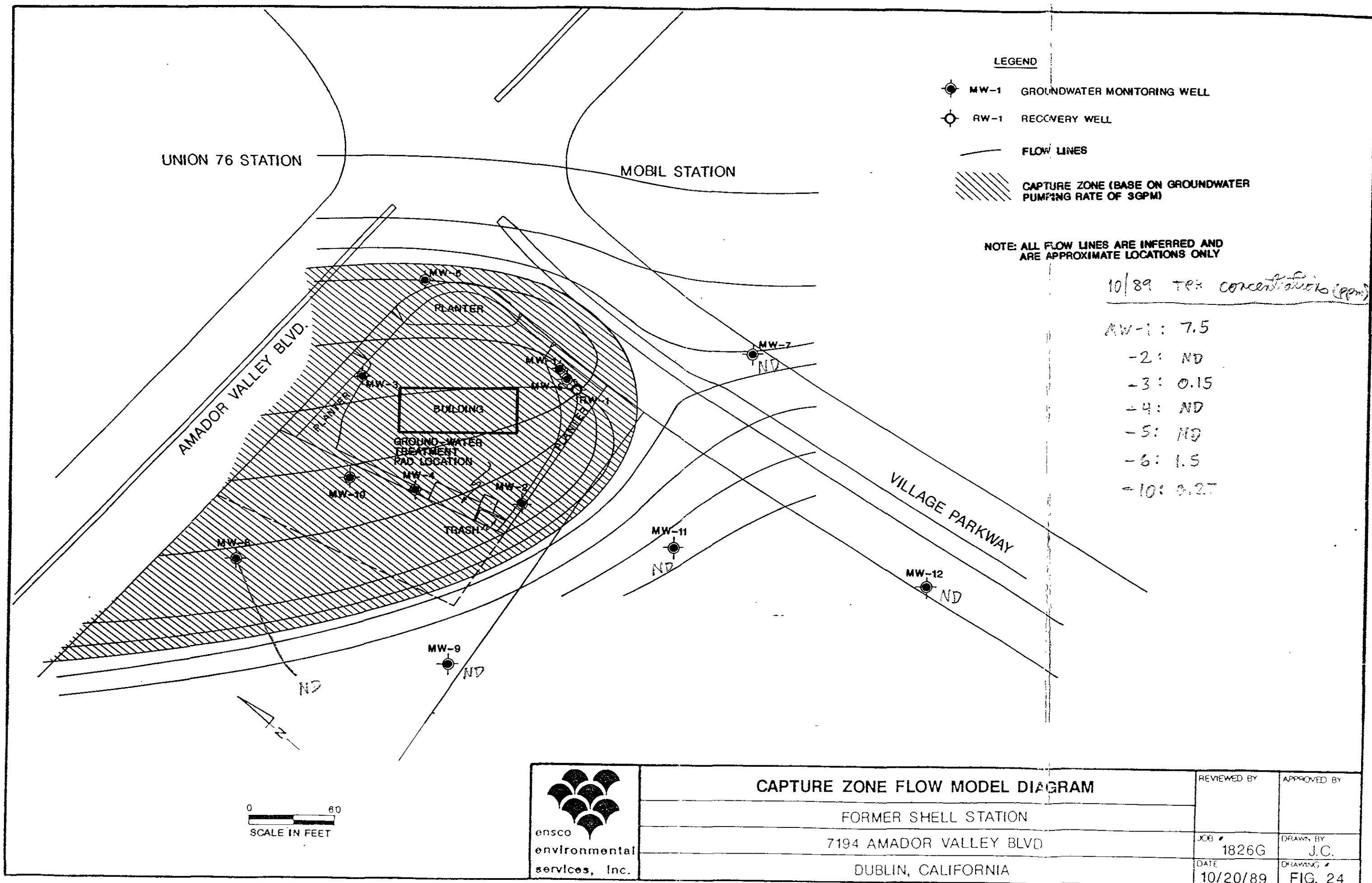
APPROVED BY

JOB
1826G

DRAWN BY
J.C.

DATE
8-25-89

DRAWING
FIG. 23



APPENDIX A

BORING LOGS AND WELL CONSTRUCTION DETAILS FOR RW-1

EXPLORATORY BORING LOG

Page 1 of 2



**ensco
environmental
services, Inc.**

PROJECT NAME: Shell Oil, Dublin
7194 Amador Valley Blvd.

BORING NO. RW-1

DATE DRILLED: 7/27/89

PROJECT NUMBER: 1826G

LOGGED BY: S.C.

DEPTH (ft.)	SAMPLE No	BLOWS/FOOT	UNIFIED SOIL CLASSIFICATION	SOIL DESCRIPTION	WATER LEVEL	GYM READING ppm
1				FILL: Sandy Gravel, 75% fine to coarse gravel, 25% medium to coarse sand, damp to dry		
2						
3			CH	SILTY CLAY, black (5YR 2.5/1), trace fine sand, trace fine gravel, high plasticity, stiff, damp		
4						
5						
6	R1-1	13				5
7						
8						
9						
10						
11	R1-2	10		CLAY, black (10YR 2/1), trace of sand, minor roots, high plasticity, stiff, moist		20
12						310
13						
14						
15						
16	R1-3	8	CH	Color change to dark grayish brown (2.5Y 4/2) mottled with very dark gray (10YR 3/1), becomes silty, trace fine to coarse sand, rare fine gravel, few to common decayed roots, common rootholes (wet), medium stiff, wet, water noted in holes		0.5
17						
18						
19						
20						
21	R1-3	10		Color change to black (5Y 2.5/1), no gravel, no roots, few rootholes (wet), stiff, wet		0.5

REVIEWED BY R.G /C E.G.

EXPLORATORY BORING LOG

Page 2 of 2



**ensco
environmental
services, inc.**

PROJECT NAME: Shell Oil, Dublin
7194 Amador Valley Blvd.

BORING NO. RW-1

DATE DRILLED: 7/27/89

PROJECT NUMBER: 1826G

LOGGED BY: S.C.

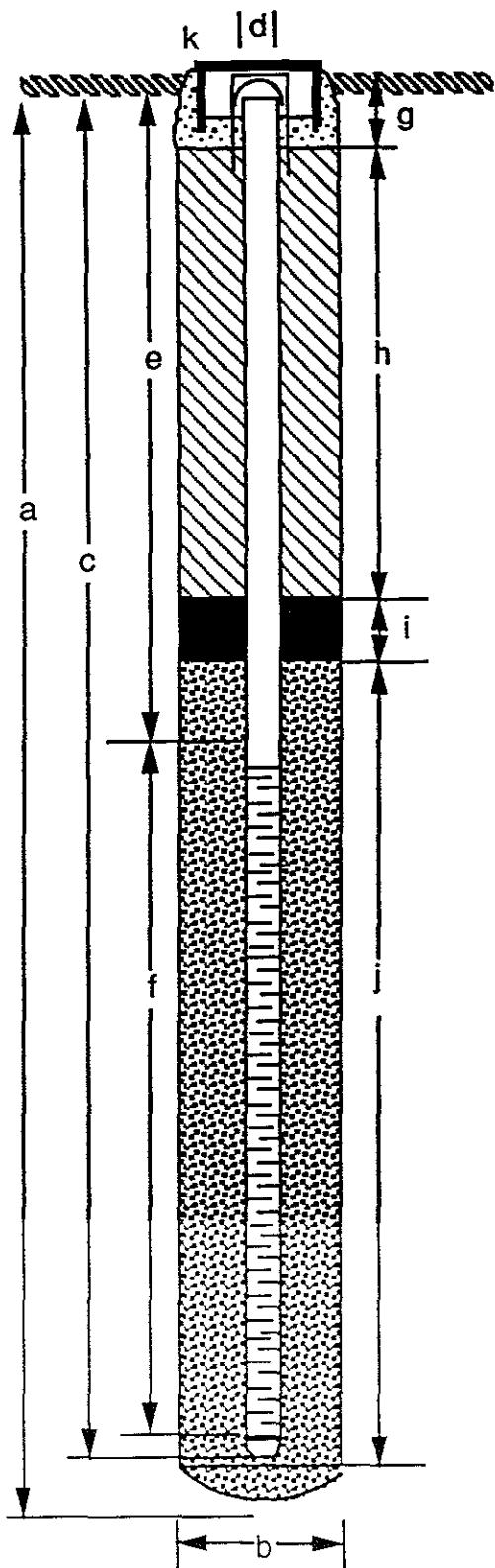
DEPTH (ft.)	SAMPLE No	BLOWS/FOOT	UNIFIED SOIL CLASSIFICATION	SOIL DESCRIPTION	WATER LEVEL	OVM READING ppm
-22			CH	SILTY CLAY, as above		
-23						
-24						
-25			CL	SANDY CLAY, dark gray (5Y 4/1), 15% fine to coarse sand, rare root fibers, rare root holes, trace black organic staining, low to moderate plasticity, stiff, damp		
-26	R1-5	16				0.5
-27						
-28						
-29			CH	SANDY CLAY, dark gray (5Y 4/1) with very slight orange-brown staining, 15% fine sand, becomes 40% fine to coarse sand at shoe, some rootholes, very stiff, wet		
-30						
-31	R1-6	19				0.5
-32				Bottom of Boring = 31.5 feet		
-33						
-34						
-35						
-36						
-37						
-38						
-39						
-40						
-41						
-42						

REVIEWED BY R.G /C.E.G

Recovery Well Detail

PROJECT NUMBER 1826G Shell Oil
 PROJECT NAME 7194 Amador Valley Blvd.
 COUNTY Alameda
 WELL PERMIT NO. _____

BORING / WELL NO. RW-1
 TOP OF CASING ELEV. _____
 GROUND SURFACE ELEV. _____
 DATUM Mean Sea Level

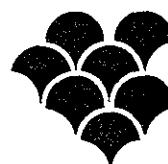


EXPLORATORY BORING

- a. Total Depth 31.5 ft.
 b. Diameter 10 in.
 Drilling method Hollow Stem Auger

WELL CONSTRUCTION

- c. Casing length 30 ft.
 Material Schedule 40 PVC
 d. Diameter 6 in.
 e. Depth to top perforations 10 ft.
 f. Perforated length 20 ft.
 Perforated interval from 30 to 10 ft.
 Perforation type Machine Slot
 Perforation size 0.020 in.
 g. Surface seal -- ft.
 Seal Material n/a
 h. Backfill 8 ft.
 Backfill material Grout
 i. Seal 1 ft.
 Seal Material Bentonite
 j. Gravel pack 21 ft.
 Pack material 2/12 Monterey Type Sand
 k. _____



ensco
 environmental
 services, inc.

APPENDIX B

TERRA 8

DATA COLLECTION REPORTS

FOR

RW-1, MW-1, MW-2,

MW-3, MW-4, AND MW-5

- **Background Data**
- **72-Hour Constant Discharge Pump Test Data**
- **Pump Test Recovery Data**

Background Data

BACKGROUND DATA

"Time since Last Configuration Report: 00:00:00"

"Firmware Version: 6.1.87"

"Number of Bytes in Data Dump: 6332"

"Programmed Software Version: 6.1.87"

"Time Header Block Loaded: 04/24/10 12:59:59:50"

"Time Data File Dumped: 04/30/10 23:52:28:90"

"Remaining Memory: 59204"

"Number of Logs: 299"

"Type of Data Memory: Memory Board"

"Data Memory Board Type: Memory Board"

"Data Memory Board Revision Period: 0000"

Terra8 Channel Setup:

"Number of Declared Analog Channels = 6"

Ch#	Description	Units	Delay	M	B
1	PSI.....	PSI....	100	2.310	0.000"
2	5-PSI.....	PSI....	100	2.310	0.000"
3	0-5 PSI.....	PSI....	100	2.310	0.000"
4	0-5 PSI.....	PSI....	100	2.310	0.000"
5	0-10 PSI.....	PSI....	100	4.620	0.000"
6	0-15 PSI.....	PSI....	100	6.930	0.000"

Terra8 Channel Setup:

"Number of Declared Digital Channels = 0"

Ch#	Description	Units	Delay	M	B
-----	-------------	-------	-------	---	---

"*Initial Scan at "4 24 3 29 37 40"

"Next Scan at "4 24 3 29 37 40"

"Time Analog#01"" Analog#02"" Analog#03"" Analog#04"" Analog#05"

SECONDS	RW-1	MW-2	MW-3	MW-1	MW-4	MW-5
0.00	8.905	10.025	9.575	9.032	13.051	16.078
3.00	8.905	10.037	9.575	9.032	13.051	16.078
5.50	8.905	10.037	9.586	9.032	13.051	16.112
7.90	8.905	10.037	9.586	9.021	13.051	16.112
10.40	8.905	10.025	9.575	9.032	13.051	16.078
12.90	8.905	10.025	9.586	9.032	13.051	16.078
15.30	8.905	10.025	9.586	9.021	13.051	16.078
17.80	8.895	10.025	9.586	9.021	13.051	16.112
20.30	8.895	10.025	9.586	9.021	13.051	16.078
22.70	8.895	10.037	9.586	9.072	13.051	16.078
25.20	8.895	10.075	9.586	9.021	13.051	16.078
27.60	8.895	10.025	9.586	9.021	13.051	16.078
30.10	8.895	10.025	9.586	9.021	13.051	16.078
32.60	8.895	10.025	9.586	9.021	13.051	16.078
35.10	8.895	10.017	9.586	9.021	13.075	16.112
37.60	8.895	10.013	9.575	9.021	13.051	16.078
40.00	8.895	10.025	9.575	9.021	13.051	16.078
42.50	8.895	10.025	9.575	9.021	13.051	16.078
45.00	8.895	10.025	9.575	9.021	13.051	16.078
47.50	8.895	10.025	9.575	9.021	13.051	16.078
50.00	8.895	10.025	9.575	9.021	13.051	16.078
52.50	8.895	10.025	9.575	9.021	13.051	16.078
55.00	8.895	10.025	9.575	9.021	13.051	16.078

1363.00	8.905	10.025	9.586	9.021	13.028	16.078
1423.00	8.893	10.025	9.586	9.032	13.051	16.078
1483.00	8.893	10.025	9.575	9.021	13.051	16.078
1543.00	8.893	10.014	9.563	9.021	13.028	16.078
1603.00	8.882	10.014	9.552	9.021	13.028	16.078
1763.00	8.882	10.015	9.552	9.021	13.028	16.078
1843.00	8.928	10.025	9.598	9.032	13.051	16.112
1903.00	8.905	10.014	9.586	9.021	13.028	16.078
1963.00	8.917	10.014	9.586	9.021	13.051	16.078
2023.00	8.917	10.025	9.586	9.032	13.051	16.078
2083.00	8.917	10.025	9.586	9.021	13.051	16.078
2143.00	8.917	10.025	9.552	9.009	13.028	16.078
2203.00	8.893	10.025	9.563	9.032	13.051	16.078
2263.00	8.905	10.014	9.586	9.032	13.051	16.078
2323.00	8.917	10.025	9.586	9.032	13.051	16.078
2383.00	8.905	10.025	9.575	9.021	13.028	16.078
2443.00	8.905	10.025	9.575	9.021	13.051	16.078
2503.00	8.905	10.014	9.586	9.021	13.028	16.078
2563.00	8.893	10.025	9.563	9.021	13.028	16.078
2683.00	8.917	10.025	9.586	9.032	13.051	16.078
2803.00	8.893	10.025	9.563	9.021	13.028	16.078
2923.00	8.928	10.025	9.586	9.032	13.051	16.078
3043.00	8.917	10.025	9.586	9.032	13.051	16.078
3163.00	8.928	10.025	9.610	9.032	13.051	16.078
3283.00	8.951	10.025	9.621	9.032	13.051	16.112
3403.00	8.928	10.025	9.598	9.021	13.051	16.078
3703.00	8.928	10.025	9.598	9.032	13.051	16.112
4003.00	8.917	10.025	9.598	9.032	13.051	16.078
4303.00	8.940	10.025	9.610	9.044	13.051	16.078
4603.00	8.917	10.025	9.598	9.032	13.051	16.078
4903.00	8.893	10.025	9.575	9.032	13.051	16.078
5203.00	8.928	10.025	9.610	9.044	13.075	16.078
5503.00	8.928	10.037	9.563	9.044	13.051	16.078
5803.00	8.928	10.037	9.586	9.044	13.075	16.078
6103.00	8.917	10.037	9.598	9.044	13.051	16.078
6403.00	8.917	10.037	9.610	9.044	13.051	16.078
6703.00	8.951	10.037	9.621	9.044	13.051	16.078
7303.00	8.940	10.048	9.610	9.055	13.051	16.078
7903.00	8.940	10.048	9.575	9.044	13.051	16.078
8503.00	8.951	10.037	9.633	9.055	13.051	16.078
9103.00	8.963	10.048	9.610	9.055	13.051	16.078
9703.00	8.963	10.048	9.610	9.055	13.051	16.078
10303.00	8.940	10.060	9.610	9.067	13.075	16.078
10903.00	8.963	10.060	9.644	9.067	13.075	16.078
11503.00	8.974	10.048	9.533	9.055	13.075	16.078
12102.90	8.963	10.060	9.633	9.067	13.075	16.078
12703.00	8.951	10.048	9.621	9.067	13.075	16.078
13303.00	8.963	10.060	9.644	9.067	13.075	16.078
13403.00	8.951	10.048	9.610	9.055	13.075	16.078
13803.00	8.974	10.072	9.610	9.055	13.075	16.078
14503.00	8.963	10.060	9.644	9.067	13.075	16.078
17202.90	8.963	10.048	9.633	9.067	17.075	16.078
22603.00	8.951	10.060	9.571	9.055	17.075	16.078
22603.00	8.940	10.047	9.571	9.044	17.075	16.078
22803.00	8.941	10.048	9.571	9.044	17.075	16.078

544303.00	9.159	10.199	9.783	9.252	13.282	16.182
547903.00	9.159	10.187	9.771	9.240	13.282	16.182
551503.00	9.159	10.199	9.771	9.240	13.282	16.182
555103.00	9.159	10.199	9.771	9.240	13.282	16.182
558703.00	9.148	10.187	9.771	9.240	13.282	16.182

571103.00	9.159	10.187	9.771	9.228	13.259	16.182
573103.00	9.159	10.187	9.771	9.228	13.259	16.182
576703.00	9.148	10.187	9.748	9.228	13.282	16.182
580303.00	9.136	10.187	9.737	9.228	13.259	16.182
583903.00	9.124	10.187	9.748	9.228	13.259	16.182
587503.00	9.136	10.176	9.748	9.228	13.282	16.182

last Scan at 24-02-2011 20:40

**72-Hour Constant Discharge
Pump Test Data**

1-HOUR CONSTANT DISCHARGE PUMP TEST DATA

Firmware Version: "2.2.6.1/87"

Number of Bytes in Data Dump: 3992"

User Supplied Comment:

"None. READING BLOCKS loaded" "000100:34-34-40"

"None. READING DUMPED" "000100:34-34-40"

"None. READING MEMORY" "154-154-154"

Number of Logs: 182"

Type of Data Memory: "Memory Board"

Logs/Timestamp: 1"

Power was OK During Data Collection Period:

Terra8 Channel Setup:"

Number of Declared Analog Channels = 6"

Ch#	Description	Units	Delay	M	B
1	5 PSI	FEET	100	2.310	0.000
2	5 PSI	FEET	100	2.310	0.000
3	5 PSI	FEET	100	2.310	0.000
4	5 PSI	FEET	100	2.310	0.000
5	10 PSI	FEET	100	4.620	0.000
6	15 PSI	FEET	100	6.930	0.000

Terra8 Channel Setup:"

Number of Declared Digital Channels = 0"

Ch#	Description	Units	Delay	M	B
-----	-------------	-------	-------	---	---

*Initial Scan at "1 1 0 34 34 40

*Next Scan at "1 1 0 34 34 40

Time : Analog#01" "Analog#02" "Analog#03" "Analog#04" "Analog#05"

SECONDS	RW-1	MW-2	MW-3	MW-1	MW-4	MW-5
0.00	11.816	10.499	9.817	9.413	13.329	16.141
2.80	11.816	10.499	9.817	9.413	13.329	16.141
5.20	11.816	10.487	9.817	9.413	13.329	16.141
7.60	11.816	10.487	9.817	9.425	13.329	16.141
10.00	11.816	10.499	9.817	9.413	13.329	16.141
12.40	11.816	10.499	9.817	9.413	13.329	16.141
14.80	11.816	10.487	9.817	9.413	13.329	16.141
17.20	11.816	10.499	9.817	9.413	13.329	16.141
19.60	11.816	10.487	9.817	9.413	13.329	16.141
22.00	11.816	10.499	9.817	9.413	13.329	16.141
28.20	11.816	10.487	9.817	9.412	13.329	16.141
33.90	11.816	10.487	9.817	9.411	13.329	16.141
36.30	11.816	10.499	9.817	9.411	13.329	16.141
41.10	11.816	10.499	9.817	9.411	13.329	16.141
48.90	11.816	10.476	9.817	9.412	13.329	16.141
57.90	11.816	10.476	9.817	9.412	13.329	16.111
58.90	11.816	10.476	9.817	9.412	13.329	16.141
60.90	11.816	10.476	9.817	9.412	13.329	16.141
68.90	11.816	10.477	9.817	9.412	13.329	16.141

593.90	11.816	10.487	9.829	9.402	13.306	16.147
103.90	11.816	10.487	9.817	9.390	13.306	16.147
113.90	11.816	10.476	9.817	9.390	13.306	16.147
123.90	11.816	10.487	9.806	9.379	13.329	16.112
133.90	11.816	10.487	9.794	9.379	13.329	16.147
143.90	11.816	10.487	9.783	9.379	13.329	16.147
153.90	11.816	10.487	9.773	9.379	13.329	16.147
193.90	11.816	10.487	9.794	9.344	13.329	16.112
223.90	11.816	10.487	9.817	9.332	13.329	16.112
253.90	11.816	10.487	9.817	9.321	13.329	16.147
283.90	11.816	10.499	9.829	9.309	13.329	16.147
313.90	11.816	10.487	9.841	9.286	13.329	16.147
343.90	11.816	10.499	9.852	9.273	13.329	16.147
373.90	11.816	10.487	9.852	9.275	13.329	16.147
403.90	11.816	10.487	9.841	9.240	13.306	16.147
433.90	11.816	10.487	9.817	9.228	13.329	16.112
493.90	11.816	10.499	9.829	9.205	13.329	16.147
553.90	11.816	10.510	9.864	9.182	13.329	16.147
613.90	11.816	10.487	9.864	9.136	13.329	16.147
673.90	11.816	10.499	9.841	9.101	13.329	16.147
733.90	11.816	10.476	9.829	9.067	13.306	16.147
793.90	11.816	10.476	9.806	9.032	13.329	16.147
853.90	11.816	10.487	9.829	9.021	13.329	16.147
913.90	11.816	10.476	9.806	8.997	13.329	16.147
973.90	11.816	10.464	9.829	8.963	13.306	16.112
1093.90	11.816	10.464	9.806	8.928	13.306	16.147
1213.90	11.816	10.464	9.841	8.893	13.329	16.147
1333.90	11.816	10.453	9.841	8.847	13.329	16.147
1453.90	11.816	10.464	9.841	8.824	13.329	16.147
1573.90	11.816	10.441	9.841	8.790	13.329	16.147
1693.90	11.816	10.441	9.817	8.778	13.329	16.147
1813.90	11.816	10.441	9.852	8.755	13.352	16.147
1933.90	11.816	10.407	9.806	8.697	13.306	16.147
2053.90	11.816	10.418	9.817	8.697	13.306	16.147
2353.90	11.816	10.395	9.841	8.639	13.306	16.147
2653.90	11.816	10.395	9.864	8.616	13.329	16.182
2953.90	11.816	10.395	9.806	8.570	13.329	16.182
3253.90	11.816	10.372	9.817	8.524	13.329	16.182
3553.90	11.816	10.349	9.829	8.489	13.306	16.147
3853.90	11.816	10.349	9.806	8.478	13.329	16.182
4153.90	11.816	10.326	9.806	8.455	13.306	16.182
4453.90	11.816	10.314	9.794	8.431	13.306	16.182
4753.90	11.816	10.291	9.817	8.397	13.306	16.182
5353.90	11.816	10.268	9.794	8.351	13.282	16.182
5953.90	11.816	10.279	9.806	8.316	13.282	16.182
6553.90	11.816	10.256	9.817	8.293	13.282	16.182
7153.90	11.816	10.233	9.806	8.247	13.282	16.182
7753.90	11.816	10.210	9.783	8.224	13.259	16.182
8354.00	11.816	10.187	9.760	8.189	13.259	16.182
8954.00	11.816	10.154	9.744	8.155	13.213	16.182
9553.00	11.816	10.151	9.744	8.155	13.216	16.182
11154.00	11.816	10.141	9.721	8.131	13.213	16.182
11753.90	11.816	10.118	9.746	8.097	13.213	16.182
12554.00	11.816	10.075	9.749	8.071	13.213	16.216
13754.00	11.816	10.060	9.724	8.046	13.190	16.216
1453.90	11.816	10.016	9.711	8.031	13.190	16.216
16154.00	11.816	10.016	9.714	8.027	13.197	16.216
17354.00	11.816	10.016	9.714	8.027	13.197	16.216
18554.00	11.816	10.016	9.709	8.020	13.194	16.216
19754.00	11.816	10.016	9.709	8.020	13.194	16.216
2129	11.816	10.016	9.709	8.020	13.194	16.216
2153	11.816	10.016	9.709	8.020	13.194	16.216
2179	11.816	10.016	9.709	8.020	13.194	16.216
2193	11.816	10.016	9.709	8.020	13.194	16.216
2219	11.816	10.016	9.709	8.020	13.194	16.216

32854.00	11.816	9.806	9.598	7.773	13.005	16.216
35354.00	11.816	9.794	9.575	7.762	13.005	16.216
37754.00	11.816	9.771	9.575	7.750	12.982	16.216
40154.00	11.816	9.760	9.563	7.727	12.982	16.216
42554.00	11.816	9.748	9.563	7.750	12.982	16.216
44954.00	11.816	9.736	9.563	7.750	12.982	16.216
47354.00	11.816	9.714	9.540	7.715	12.936	16.182
54554.00	11.816	9.714	9.529	7.738	12.936	16.182
56954.00	11.816	9.702	9.517	7.727	12.936	16.182
59354.00	11.816	9.702	9.517	7.727	12.936	16.182
61754.00	11.816	9.679	9.505	7.569	12.915	16.182
63154.00	11.816	9.679	9.505	7.569	12.915	16.182
66554.00	11.816	9.667	9.483	7.600	12.913	16.182
68954.00	11.816	9.656	9.483	7.588	12.890	16.182
71354.00	11.816	9.633	9.471	7.577	12.890	16.147
73754.00	11.816	9.644	9.471	7.565	12.867	16.182
76154.00	11.816	9.621	9.471	7.542	12.867	16.147
78554.00	11.816	9.621	9.459	7.542	12.890	16.182
80954.00	11.816	9.610	9.483	7.542	12.867	16.182
83354.00	11.816	9.598	9.483	7.519	12.867	16.147
85754.00	11.816	9.598	9.471	7.531	12.844	16.147
88154.00	11.816	9.586	9.517	7.519	12.844	16.147
90554.00	11.816	9.586	9.517	7.507	12.844	16.147
92954.00	11.816	9.575	9.459	7.507	12.820	16.147
95354.00	11.816	9.586	9.483	7.507	12.844	16.147
97754.00	11.816	9.563	9.494	7.507	12.820	16.147
100154.00	11.816	9.563	9.471	7.496	12.820	16.147
102554.00	11.816	9.552	9.471	7.484	12.820	16.147
104954.00	11.816	9.540	9.448	7.473	12.820	16.112
107354.00	11.816	9.529	9.448	7.473	12.797	16.147
109754.00	11.816	9.529	9.425	7.450	12.821	16.147
112154.00	11.816	9.517	9.425	7.450	12.797	16.112
114554.00	11.816	9.506	9.413	7.450	12.797	16.112
116954.00	11.816	9.506	9.402	7.450	12.797	16.112
119354.00	11.816	9.506	9.402	7.438	12.797	16.112
121754.00	11.816	9.494	9.402	7.427	12.774	16.112
124154.00	11.816	9.494	9.413	7.427	12.797	16.112
126554.00	11.816	9.483	9.402	7.427	12.774	16.078
128954.00	11.816	9.483	9.402	7.427	12.774	16.112
131354.00	11.816	9.483	9.402	7.415	12.774	16.078
133754.00	11.816	9.471	9.390	7.415	12.774	16.078
136154.00	11.816	9.471	9.390	7.415	12.774	16.078
138554.00	11.816	9.471	9.390	7.415	12.751	16.078
140954.00	11.816	9.459	9.379	7.404	12.774	16.078
143354.00	11.816	9.459	9.379	7.404	12.751	16.078
145754.00	11.816	9.459	9.379	7.392	12.751	16.078
148154.00	11.816	9.448	9.367	7.392	12.751	16.078
150554.00	11.816	9.436	9.367	7.392	12.728	16.078
152954.00	11.816	9.442	9.363	7.351	12.711	16.078
155354.00	11.816	9.448	9.344	7.351	12.728	16.078
157754.00	11.816	9.456	9.344	7.351	12.711	16.078
160154.00	11.816	9.448	9.344	7.352	12.751	16.043
162554.00	11.816	9.448	9.358	7.351	12.705	16.043
164954.00	11.816	9.456	9.367	7.360	12.728	16.043
167354.00	11.816	9.456	9.374	7.371	12.711	16.043
169754.00	11.816	9.441	9.341	7.371	12.711	16.043
172154.00	11.816	9.441	9.341	7.371	12.711	16.043
174554.00	11.816	9.441	9.341	7.371	12.711	16.043
176954.00	11.816	9.425	9.341	7.371	12.711	16.043
178354.00	11.816	9.425	9.341	7.371	12.711	16.043
180754.00	11.816	9.424	9.341	7.371	12.711	16.043

191354.00	11.816	9.425	9.379	7.369	12.682	15.008
193754.00	11.816	9.413	9.367	7.369	12.682	15.043
196154.00	11.816	9.402	9.344	7.346	12.705	15.043
198554.00	11.816	9.390	9.332	7.346	12.682	15.043
200954.00	11.816	9.390	9.332	7.334	12.682	15.008
203354.00	11.816	9.379	9.321	7.334	12.682	15.008
205754.00	11.816	9.379	9.321	7.334	12.682	15.008
210554.00	11.816	9.379	9.321	7.334	12.682	15.008
212954.00	11.816	9.379	9.321	7.334	12.682	15.008
215354.00	11.816	9.379	9.309	7.334	12.682	15.008
217754.00	11.816	9.379	9.321	7.323	12.682	15.008
220154.00	11.816	9.379	9.309	7.323	12.682	15.008
222554.00	11.816	9.379	9.309	7.323	12.682	15.008
224954.00	11.816	9.367	9.309	7.323	12.682	15.008
227354.00	11.816	9.367	9.309	7.323	12.682	15.008
229754.00	11.816	9.367	9.309	7.323	12.659	15.008
232154.00	11.816	9.355	9.298	7.311	12.659	15.008
234554.00	11.816	9.355	9.286	7.311	12.659	15.008
236954.00	11.816	9.344	9.286	7.311	12.659	15.008
239354.00	11.816	9.355	9.275	7.300	12.659	15.008
241754.00	11.816	9.344	9.275	7.300	12.659	15.974
244154.00	11.816	9.344	9.252	7.300	12.659	15.974
246554.00	11.816	9.355	9.263	7.311	12.659	15.008
248954.00	11.816	9.344	9.275	7.300	12.659	15.974
251354.00	11.816	9.344	9.252	7.288	12.659	15.974
253754.00	5.717	9.355	9.252	7.300	12.636	15.974
256154.00	5.590	9.344	9.298	7.300	12.659	15.974
258554.00	5.613	9.355	9.344	7.311	12.636	15.974

"*Last Scan at "1 4 0 23 48 40

Pump Test Recovery Data

PUMP TEST RECOVERY DATA

"Firmware Version" "6.1/87"

"Number of Bytes in Data Dump" "7552"

"User Supplied Comment"

"Time Header Block Loaded" "201/01/00 00:34:36.40"

"Time Data File Dumped" "201/06/22 14:13:50"

"Remaining Memory" "1357984"

"Number of Logs" "360"

"Type of Data Memory" "Memory Board"

"Logs/Timestamp" "1"

"Power was OK During Data Collection Period"

Terra8 Channel Setup:

"Number of Declared Analog Channels = 6"

Ch#	Description	Units	Delay	M	B
" 1	5 PSI.....	FEET....	100	2.310	0.000"
" 2	5 PSI.....	FEET....	100	2.310	0.000"
" 3	5 PSI.....	FEET....	100	2.310	0.000"
" 4	5 PSI.....	FEET....	100	2.310	0.000"
" 5	10 PSI.....	FEET....	100	4.620	0.000"
" 6	15 PSI.....	FEET....	100	6.930	0.000"

Terra8 Channel Setup:

"Number of Declared Digital Channels = 0"

Ch#	Description	Units	Delay	M	B
"	"	"	"	"	"

"*Initial Scan at "1 1 0 34 34 40

"*Next Scan at "1 1 0 34 34 40

Time	" Analog#01"	" Analog#02"	" Analog#03"	" Analog#04"	" Analog#05"	
SECONDS	RW-1	MW-2	MW-3	MW-1	MW-4	MW-5
0.00	11.816	10.499	9.817	9.413	13.329	16.147
2.80	11.816	10.499	9.817	9.413	13.329	16.147
5.20	11.816	10.487	9.817	9.413	13.329	16.147
7.60	11.816	10.487	9.817	9.425	13.329	16.147
10.00	11.816	10.499	9.817	9.413	13.329	16.147
12.40	11.816	10.499	9.817	9.413	13.329	16.147
14.80	11.816	10.487	9.817	9.413	13.329	16.147
17.20	11.816	10.499	9.817	9.413	13.329	16.147
19.60	11.816	10.487	9.817	9.413	13.329	16.147
22.00	11.816	10.499	9.817	9.413	13.329	16.147
24.40	11.816	10.497	9.806	9.402	13.329	16.147
26.80	11.816	10.487	9.817	9.413	13.329	16.147
29.20	11.816	10.499	9.817	9.413	13.329	16.147
31.60	11.816	10.492	9.817	9.413	13.329	16.147
34.00	11.816	10.476	9.617	9.402	13.306	16.147
36.40	11.816	10.476	9.617	9.402	13.329	16.147
38.80	11.816	10.476	9.627	9.402	13.306	16.147
41.20	11.816	10.476	9.627	9.402	13.329	16.147
43.60	11.816	10.476	9.627	9.402	13.306	16.147
46.00	11.816	10.476	9.627	9.402	13.329	16.147
48.40	11.816	10.476	9.627	9.402	13.306	16.147
50.80	11.816	10.476	9.627	9.402	13.329	16.147

93.90	11.816	10.487	9.829	9.402	13.329	16.147
103.90	11.816	10.487	9.817	9.390	13.306	16.147
113.90	11.816	10.476	9.817	9.390	13.306	16.147
123.90	11.816	10.487	9.806	9.379	13.329	16.112
133.90	11.816	10.487	9.794	9.379	13.329	16.147
143.90	11.816	10.487	9.783	9.379	13.329	16.147
153.90	11.816	10.487	9.773	9.379	13.329	16.147
163.90	11.816	10.487	9.763	9.379	13.329	16.147
173.90	11.816	10.487	9.754	9.379	13.329	16.147
183.90	11.816	10.489	9.829	9.309	13.329	16.147
193.90	11.816	10.487	9.841	9.286	13.329	16.147
203.90	11.816	10.487	9.841	9.286	13.329	16.147
213.90	11.816	10.487	9.841	9.286	13.329	16.147
223.90	11.816	10.487	9.817	9.332	13.329	16.112
233.90	11.816	10.487	9.817	9.321	13.329	16.147
243.90	11.816	10.489	9.852	9.275	13.329	16.147
253.90	11.816	10.487	9.841	9.240	13.306	16.147
263.90	11.816	10.487	9.817	9.228	13.329	16.112
273.90	11.816	10.499	9.829	9.205	13.329	16.147
283.90	11.816	10.499	9.864	9.182	13.329	16.147
293.90	11.816	10.510	9.864	9.136	13.329	16.147
303.90	11.816	10.487	9.864	9.101	13.329	16.147
313.90	11.816	10.476	9.829	9.067	13.306	16.147
323.90	11.816	10.476	9.806	9.032	13.329	16.147
333.90	11.816	10.487	9.829	9.021	13.329	16.147
343.90	11.816	10.464	9.841	8.997	13.329	16.147
353.90	11.816	10.464	9.806	8.963	13.306	16.112
363.90	11.816	10.464	9.829	8.928	13.306	16.147
373.90	11.816	10.464	9.841	8.893	13.329	16.147
383.90	11.816	10.453	9.841	8.847	13.329	16.147
393.90	11.816	10.464	9.841	8.824	13.329	16.147
403.90	11.816	10.441	9.841	8.790	13.329	16.147
413.90	11.816	10.441	9.817	8.778	13.329	16.147
423.90	11.816	10.441	9.852	8.755	13.352	16.147
433.90	11.816	10.407	9.806	8.697	13.306	16.147
443.90	11.816	10.418	9.817	8.697	13.306	16.147
453.90	11.816	10.395	9.841	8.639	13.306	16.147
463.90	11.816	10.395	9.864	8.616	13.329	16.182
473.90	11.816	10.395	9.806	8.570	13.329	16.182
483.90	11.816	10.372	9.817	8.524	13.329	16.182
493.90	11.816	10.349	9.829	8.489	13.306	16.147
503.90	11.816	10.349	9.806	8.478	13.329	16.182
513.90	11.816	10.326	9.806	8.455	13.306	16.182
523.90	11.816	10.314	9.794	8.431	13.306	16.182
533.90	11.816	10.291	9.817	8.397	13.306	16.182
543.90	11.816	10.268	9.794	8.351	13.282	16.182
553.90	11.816	10.279	9.806	8.316	13.282	16.182
563.90	11.816	10.255	9.817	8.293	13.282	16.182
573.90	11.816	10.233	9.806	8.247	13.282	16.182
583.90	11.816	10.210	9.783	8.224	13.259	16.182
593.90	11.816	10.187	9.760	8.189	13.259	16.182
603.90	11.816	10.164	9.744	8.156	13.213	16.112
613.90	11.816	10.151	9.744	8.134	13.226	16.152
623.90	11.816	10.128	9.741	8.111	13.212	16.132
633.90	11.816	10.115	9.748	8.097	13.213	16.132
643.90	11.816	10.092	9.760	8.073	13.213	16.216
653.90	11.816	10.069	9.745	8.019	13.170	16.217
663.90	11.816	10.046	9.737	8.040	13.190	16.216
673.90	11.816	10.023	9.747	8.064	13.190	16.216
683.90	11.816	10.000	9.747	8.084	13.190	16.216
693.90	11.816	9.977	9.747	8.105	13.144	16.216
703.90	11.816	9.954	9.747	8.111	13.191	16.216
713.90	11.816	9.931	9.747	8.112	13.191	16.216
723.90	11.816	9.908	9.747	8.113	13.191	16.216
733.90	11.816	9.885	9.747	8.114	13.191	16.216

32954.00	11.816	9.806	9.598	7.773	12.905	16.216
35354.00	11.816	9.794	9.575	7.762	13.005	16.216
37754.00	11.816	9.771	9.575	7.750	12.982	16.216
40154.00	11.816	9.760	9.563	7.727	12.982	16.216
42554.00	11.816	9.748	9.563	7.750	12.982	16.216
44954.00	11.816	9.736	9.563	7.750	12.982	16.216
47354.00	11.816	9.714	9.540	7.715	12.936	16.182
50754.00	11.816	9.714	9.529	7.738	12.936	16.182
53154.00	11.816	9.702	9.517	7.727	12.936	16.182
55554.00	11.816	9.702	9.517	7.727	12.936	16.182
57954.00	11.816	9.679	9.506	7.669	12.913	16.182
60354.00	11.816	9.679	9.506	7.669	12.913	16.182
62754.00	11.816	9.667	9.483	7.600	12.913	16.182
65154.00	11.816	9.656	9.483	7.588	12.890	16.182
67554.00	11.816	9.633	9.471	7.577	12.890	16.147
70054.00	11.816	9.614	9.471	7.565	12.867	16.182
72454.00	11.816	9.621	9.471	7.542	12.867	16.147
74854.00	11.816	9.621	9.459	7.542	12.890	16.182
77254.00	11.816	9.610	9.483	7.542	12.867	16.182
79654.00	11.816	9.598	9.483	7.519	12.867	16.147
82054.00	11.816	9.598	9.471	7.531	12.844	16.147
84454.00	11.816	9.586	9.517	7.519	12.844	16.147
86854.00	11.816	9.586	9.517	7.507	12.844	16.147
89254.00	11.816	9.575	9.459	7.507	12.820	16.147
91654.00	11.816	9.586	9.483	7.507	12.844	16.147
94054.00	11.816	9.563	9.494	7.507	12.820	16.147
96454.00	11.816	9.563	9.471	7.496	12.820	16.147
98854.00	11.816	9.552	9.471	7.484	12.820	16.147
101254.00	11.816	9.540	9.448	7.473	12.820	16.112
103654.00	11.816	9.529	9.448	7.473	12.797	16.147
106054.00	11.816	9.529	9.425	7.450	12.820	16.147
108454.00	11.816	9.517	9.425	7.450	12.797	16.112
110854.00	11.816	9.506	9.413	7.450	12.797	16.112
113254.00	11.816	9.506	9.402	7.450	12.797	16.112
115654.00	11.816	9.506	9.402	7.438	12.797	16.112
118054.00	11.816	9.494	9.402	7.427	12.774	16.112
120454.00	11.816	9.494	9.413	7.427	12.797	16.112
122854.00	11.816	9.483	9.402	7.427	12.774	16.078
125254.00	11.816	9.483	9.402	7.427	12.774	16.078
127654.00	11.816	9.483	9.402	7.427	12.774	16.112
130054.00	11.816	9.483	9.402	7.415	12.774	16.078
132454.00	11.816	9.471	9.390	7.415	12.774	16.078
134854.00	11.816	9.471	9.390	7.415	12.774	16.078
137254.00	11.816	9.471	9.390	7.415	12.774	16.078
140054.00	11.816	9.471	9.379	7.404	12.774	16.078
143454.00	11.816	9.459	9.379	7.404	12.751	16.078
145854.00	11.816	9.459	9.379	7.392	12.751	16.078
148254.00	11.816	9.448	9.367	7.392	12.751	16.078
150654.00	11.816	9.436	9.367	7.392	12.728	16.078
153054.00	11.816	9.425	9.351	7.371	12.728	16.078
155454.00	11.816	9.425	9.341	7.371	12.728	16.078
157854.00	11.816	9.417	9.341	7.359	12.728	16.078
160254.00	11.816	9.448	9.341	7.392	12.751	16.043
162654.00	11.816	9.448	9.355	7.392	12.705	16.043
165054.00	11.816	9.426	9.367	7.371	12.728	16.078
167454.00	11.816	9.426	9.371	7.371	12.728	16.078
170054.00	11.816	9.417	9.311	7.359	12.728	16.078
172454.00	11.816	9.417	9.311	7.371	12.728	16.078
174854.00	11.816	9.402	9.311	7.371	12.728	16.078
177254.00	11.816	9.402	9.311	7.371	12.728	16.078
180054.00	11.816	9.417	9.311	7.371	12.728	16.078
182454.00	11.816	9.417	9.311	7.371	12.728	16.078

486762.00	10.938	10.372	9.667	9.355	13.190	16.078
486762.00	10.938	10.372	9.656	9.355	13.190	16.078
486762.00	10.926	10.372	9.656	9.344	13.170	16.078
486762.00	10.938	10.372	9.656	9.344	13.190	16.078
496362.00	10.926	10.372	9.656	9.355	13.190	16.078
498762.00	10.926	10.383	9.656	9.344	13.190	16.078
501182.00	10.949	10.383	9.679	9.355	13.170	16.078
503562.00	10.922	10.380	9.621	9.332	13.160	16.043
506762.00	10.925	10.383	9.667	9.355	13.190	16.078
508362.00	10.961	10.395	9.714	9.367	13.213	16.078

Scan at 11-6-21 47 16:40

APPENDIX C

**RESSQ DATA FILE FOR
CAPTURE ZONE ANALYSES**

1: *SHELL DUBLIN PUMP TEST

2:	19	1	0.	.01		
3:		2.4	.10	191.50	10.	.05
4:		IW1	0.	0.	0.	10. 1 1-1
5:		IW2	0.	16.29	0.	10. 1 1-1
6:		IW3	0.	36.57	0.	10. 1 1-1
7:		IW4	0.	54.86	0.	10. 1 1-1
8:		IW5	0.	73.15	0.	10. 1 1-1
9:		IW6	0.	91.44	0.	10. 1 1-1
10:		IW6.5	0.	100.59	0.	10. 1 1-1
11:		IW61	0.	109.73	0.	10. 1 1-1
12:		IW62	0.	128.02	0.	10. 1 1-1
13:		IW62.5	0.	137.30	0.	10. 1 1-1
14:		IW63	0.	146.30	0.	10. 1 1-1
15:		IW7	18.28	0.	0.	10. 1 1-1
16:		IW8	36.58	0.	0.	10. 1 1-1
17:		IW9	54.87	0.	0.	10. 1 1-1
18:		IW10	73.15	0.	0.	10. 1 1-1
19:		IW11	91.44	0.	0.	10. 1 1-1
20:		IW12.5	118.87	0.	0.	10. 1 1-1
21:		IW12	109.73	0.	0.	10. 1 1-1
22:		IW13	128.02	0.	0.	10. 1 1-1
23:		RW1	79.25	59.44	0.680	
24:	1	5.				
25:	10.0	5.		-1		