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April 23, 2013

Ms. Keith Nowell  
Alameda County Health Care Services Agency  
1131 Harbor Bay Parkway, Suite 250  
Alameda, CA 94502-6577

**Subject: Remedial Action Plan**  
**Site: 76 Station No. 5191/5043**  
**449 Hegenberger Road**  
**Oakland, California**  
**Fuel Leak Case No. RO0000219**

Dear Mr. Nowell;

I declare under penalty of perjury that to the best of my knowledge the information and/or recommendations contained in the attached report is/are true and correct.

If you have any questions or need additional information, please call:

Walter T. Sprague  
Pacific Convenience & Fuel  
7180 Koll Center Parkway, Suite 100  
Pleasanton, California 94566  
Tel: (925) 931-5714  
Fax: (925) 905-2746  
WSprague@pcandf.com

Sincerely,

**PACIFIC CONVENIENCE & FUEL**



**WALTER SPRAGUE**  
Director of Retail Services

Attachment

## ***Remedial Action Plan***

***76 Service Station No. 5191/5043  
449 Hegenberger Road  
Oakland, California***

*Alameda County Health Care Services Agency Fuel Leak Case No. R00000219*

*San Francisco Bay, Regional Water Quality Control Board Case No. 01-1601*

*GeoTracker Global ID No.T0600101476*

*Antea Group Project No. I42705191*

*Prepared for:*

**Mr. Keith Nowell**

Alameda County Health Care Services  
Agency  
1131 Harbor Bay Parkway, Suite 250  
Alameda, CA 94502-6577

*Prepared by:*

**Antea®Group**

11050 White Rock Road,  
Suite 110  
Rancho Cordova, CA  
95670  
+1 800 477 7411

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**Antea<sup>™</sup>Group**

11050 White Rock Road, Suite 110  
Rancho Cordova, CA 95670  
+1 800 477 7411

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# Remedial Action Plan

## 1.0 INTRODUCTION

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Antea™Group is pleased to submit this *Remedial Action Plan* (RAP) to the Alameda County Health Care Services Agency (ACHCSA) for the referenced site in Oakland, California (**Figure 1**).

This RAP details Antea Group's proposed shallow soil excavation in the southwest and eastern portions of the site. The goal of this proposed remedial action is to excavate the majority of the residual petroleum hydrocarbons in soil contributing to dissolved groundwater concentrations of total petroleum hydrocarbons - gasoline range organics (GRO), benzene, ethylbenzene, naphthalene, and methyl tertiary-butyl ether (MTBE).

## 2.0 SITE DESCRIPTION

---

The subject site is an operating 76 station located on the southwestern corner of Hegenberger Road and Edgewater Drive in Oakland, California (**Figure 1**). This site contains six fuel dispensers on two islands under a single canopy, three fuel underground storage tanks (USTs) on the north side of the site, a carwash facility on the west side of the site, and a station building in the central portion of the site. The current site features are shown on **Figure 2**. A summary of previous site assessment, environmental investigations, remedial activities, and sensitive receptors are presented in **Appendix A**.

## 3.0 GEOLOGY AND HYDROGEOLOGY

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The following sections provide a summary of the regional and site-specific geologic and hydrogeologic setting.

### 3.1 Regional Geologic Setting

The site is located on the western portion of the East Bay Plain Subbasin near the Oakland Airport. This area is primarily underlain by bay mud and artificial fill.

### 3.2 Regional Hydrogeologic Setting

According to the California Department of Water Resources' (DWR) *California's Groundwater, Bulletin 118 – Update 2004*, the site is located in the Santa Clara Valley Groundwater Basin – East Bay Plain Subbasin. Groundwater bearing formations in the subbasin include the Early Pleistocene Santa Clara Formation, Late Pleistocene Alameda Formation, Early Holocene Temescal Formation, and artificial fill. East Bay Plain Subbasin has existing beneficial uses as irrigation, municipal, and domestic water supplies (DWR, 2004).

### **3.3 Site Geologic and Hydrogeologic Conditions**

The site is underlain by Holocene-age bay mud. The bay mud typically consists of unconsolidated, saturated clay and sandy clay that is rich in organic material. The bay mud locally contains lenses and stringers of silt, well-sorted sand and gravel, and beds of peat. The most recent monitoring and sampling event was conducted at the site on December 13, 2012. The measured depth to groundwater ranged from 1.56 feet to 4.20 feet below top of casing (TOC). The groundwater flow direction was southeast with a hydraulic gradient of 0.02 foot per foot. **Figure 3** depicts the groundwater elevation contours on December 13, 2013.

### **3.4 Sensitive Receptors**

On April 24, 2006 TRC completed a sensitive receptor survey for the site. According to the Department of Water Resources (DWR) records, there are two irrigation wells and one industrial well located within one-half mile of the site. The nearest well, is an irrigation well located approximately 1,080 feet southeast of the site. The other irrigation well is located approximately 2,623 feet southeast of the site and the industrial well is located approximately 2,570 feet northeast of the site.

In addition, two surface water bodies were observed within a one-half mile radius of the site. San Leandro Creek is located approximately 1,400 feet southwest of the site and flows into the San Leandro Bay. Elmhurst Creek is located approximately 2,220 feet north of the site and also flows into the San Leandro Bay.

## **4.0 EXTENT OF CONTAMINANTS OF CONCERN (COCS)**

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The following sections provide a summary of the extent of the site's primary COCs (benzene, ethylbenzene, and methyl tertiary-butyl ether (MTBE)) in soil and groundwater. Refer to Delta and Antea Group's site assessment reports dated February 15, 2010, July 26, 2010, and August 26, 2011 for more details regarding recent soil data. Refer to Antea Group's *Quarterly Monitoring Report – Fourth Quarter 2012* for additional details regarding current groundwater conditions.

### **4.1 Former USTs**

In October 1991, the product lines were excavated during dispenser island modifications. During the excavation four (4) soil samples were collected at 3 feet below ground surface (bgs). Maximum concentrations of petroleum hydrocarbons reported in the soil samples were 9,000 milligrams per kilogram (mg/kg) total petroleum hydrocarbons as gasoline (TPHg), 8,400 mg/kg TPH as diesel (TPHd), 48 mg/kg benzene, and 330 mg/kg ethylbenzene. The excavation was completed to 4.5 feet bgs.

In September 1994, a 280-gallon waste oil tank was removed from the site. The tank was reported to be in good condition upon removal with no visible holes or cracks. Soil around the tank was excavated to a depth of nine (9) feet bgs. A confirmation soil sample was collected from beneath the tank at nine (9) feet bgs. Concentrations of

TPHg, TPHd, benzene, and ethylbenzene were reported below the laboratory's indicated reporting limits for each constituent.

In September 1994, one (1) oil-water separator and three (3) hydraulic hoists were removed from the site. Maximum concentrations of petroleum hydrocarbons reported in the soil samples were 1.6 mg/kg TPHg, <1.0 mg/kg TPHd, 0.014 mg/kg benzene, and 0.15 mg/kg ethylbenzene.

In March and April 1995, two 10,000-gallon gasoline USTs and one 10,000-gallon diesel UST were removed during a site rebuild. The product lines, dispenser islands, and the station building were also removed and excavation in those areas took place. Approximately 2,729 cubic yards of soil were removed from the site during the excavations. Maximum concentrations of petroleum hydrocarbons reported in the soil samples were 3,300 mg/kg TPHg, 330 mg/kg TPHd, 18 mg/kg benzene, and 110 mg/kg ethylbenzene.

#### **4.2 Distribution of Contaminants in Groundwater**

The most recent grab groundwater samples were collected at the site during a 2009 investigation. The highest concentrations of petroleum hydrocarbons in groundwater during the 2009 investigation were reported in grab groundwater samples collected from boring B-5 at a depth of 20 feet bgs, located east of the dispenser islands. TPHg was reported in the at a concentration of 23,500,000 micrograms per liter ( $\mu\text{g/L}$ ), TPHd was reported at a concentrations of 20,400,000  $\mu\text{g/L}$ , benzene was reported at a concentration of 324,000  $\mu\text{g/L}$ , and MTBE was reported at <50  $\mu\text{g/L}$ . MTBE was reported at a maximum concentration of 632  $\mu\text{g/L}$  in a grab groundwater sample collected from boring B-5, at a depth of 32 feet bgs.

Based on the recent fourth quarter 2012 groundwater sampling data, the dissolved-phase plume extends off-site in the east direction from MW-17 and to the west from MW-14. The greatest concentrations of COCs are reported in the vicinity of the southeast dispenser island and planter and just southwest of the station building. **Figures 4 through 7** depict iso-concentration maps for TPHg, TPHd, benzene, and MTBE as reported in groundwater samples collected during the fourth quarter 2012. **Table 1** summaries well construction details. **Table 2 and 2A** summarize current and historical groundwater monitoring well analytical data.



### 4.3 Distribution of Contaminants in Soil

Lateral and vertical extents of the COCs in soil are depicted in **Figure 8** which includes historical concentrations measured in soil samples collected at the site and in the site vicinity. The following table contains maximum concentrations of COCs in soil before the excavations that took place in 1995.

Constituent	Maximum Concentration (mg/kg)	Sample Location
Benzene	160	MW-1 at 2.5 feet bgs
Ethylbenzene	470	MW-1 at 2.5 feet bgs

In 1995, the area around monitoring well MW-1 was over excavated to a depth of 16 feet bgs and the area around soil sample location P2 was over excavated to a depth of 6 feet bgs, effectively removing the contamination associated with the above samples. Maximum concentrations of COCs in soil since the 1995 excavation are detailed in the table below.

Constituent	Maximum Concentration (mg/kg)	Sample Location	Maximum Concentration in Shallow Soil (<10 ft bgs) (mg/kg)	Sample Location
Benzene	80.9	MW-12A at 26 ft bgs	26.4	B-6 at 9 ft bgs
Ethylbenzene	178	MW-12A at 26 ft bgs	58.1	B-6 at 9 ft bgs

### 4.4 Total Oxygen Demand (TOD) Bench Scale Test

Antea Group and PTS performed a TOD bench scale test on soil samples from hand auger boring HA 1 and a groundwater sample collected from monitoring well MW-14. The test evaluated TOD and the oxidant persistence during chemical oxidation treatment using stabilized hydrogen peroxide activated sodium persulfate. A copy of PTS's lab report is included as **Appendix B**.

The TOD bench scale test applied Oxygen BioChem (OBC) to soil and groundwater samples collected from the site. OBC was applied in two concentrations to the same soil and ground water sample volume in a reactor vessel for a period of twenty eight (28) days, a low concentration dose (8 [grams per liter] g/L) and a high concentration dose (15 g/L). Aliquots of the sample were removed from the vessel and analyzed for pH each day during the test. At the culmination of the 28 day test each sample TOD analysis was completed on both the high and low concentration dose vessels.

The initial pH readings were 9.04 and 9.98 for the low and high concentration doses, respectively. After four (4) hours the pH levels rose to 9.60 and 10.03, but dropped down to 8.34 and 8.46 after 24 hours. After the initial decrease, pH levels stayed relatively stable over the course of the test, staying slightly basic at the end of the 28 days. The final TOD analysis results for the low and high concentration dose vessels were 12.1 g/Kg and 18.3 g/kg, respectively.

The typical TOD range for cost effective use of persulfate is 5-10 g/kg (grams persulfate to kilograms soil mass). In addition, the stabilized pH range of the sample vessels was lower than typically required (pH 10-10.5 SU) for effective use of persulfate. Based on results of the test, Antea Group does not recommend the use of stabilized hydrogen peroxide activated sodium persulfate for site remediation.

## 5.0 REGULATORY CLEANUP GOALS

The tables below compare maximum historical soil concentration and current groundwater concentrations for the primary COCs (Naphthalene, Benzene, Ethylbenzene and MTBE) at this site with general soil and groundwater cleanup objectives from the respective oversight agencies. Attached **Tables 2 and 2A** summarizes current and historical groundwater analytical data and **Table 3** summaries historical soil analytical data. The proposed excavation will consist of two areas on the site designated as A1 and A2.

### 5.1 Cleanup Goals for Groundwater (SWRCB Low –Threat Closure Goals)

The ACHCSA is the oversight agency for groundwater cleanup at this site under the direction of the Regional Water Quality Control Board, San Francisco Bay Region. Below are the State Water Resources Control Board (SWRCB) Low-Threat Closure cleanup goals for the primary COCs compared with the current maximum dissolved groundwater concentrations:

	Benzene (µg/L)	MTBE (µg/L)
<b>MW-6 (A2)</b>	2,130 (6/30/2010) 2,300 (9/20/2010) 1,300 (12/8/2010) 1,020 (3/6/2012)	19 (9/20/2010) 16 (3/14/2011) 15 (12/5/2011) 11 (6/12/2012)
<b>MW-12 (A1)</b>	1,030 (7/6/2010) 6,020 (9/20/2010)	1650 (7/6/2010) 1470 (12/8/2010)

	Benzene (µg/L)	MTBE (µg/L)
	<b>688 (6/02/2011)</b> <b>920 (9/7/2011)</b>	<b>1020 (3/14/2011)</b> <b>1040 (12/5/2011)</b>
SWRCB Low- Threat 100' plume	'No Free Product Present'	
SWRCB Low- Threat 250' plume	3000	1000

## 5.2 Cleanup Goals for Soil (SWRCB Low –Threat Closure Goals)

The following table compares the greatest soil concentration of each of the primary COCs reported at the site to date with the general Low-Threat Closure Goals established by the SWRCB for soil:

	Naphthalene (mg/kg)	Benzene (mg/kg)	Ethylbenzene (mg/kg)
<b>Maximum Concentration Reported in Soil Samples (A1)</b>	<b>Note 1</b>	<b>26.4</b> <b>(B-6 @ 9' 5/18/11)</b>	<b>58.1</b> <b>(B-6 @ 9' 5/18/11)</b>
<b>Maximum Concentration Reported in Soil Samples (A2)</b>	<b>Note 1</b>	<b>0.9</b> <b>(MW-6 @ 5'</b> <b>8/21/1992)</b>	<b>1.0</b> <b>(MW-6 @ 5'</b> <b>8/21/1992)</b>
SWRCB Low- Threat No Significant Threat Soil Concentrations ( 0-5 bgs)	45	8.2	89
SWRCB Low- Threat No Significant Threat Soil Concentrations ( 0-10 bgs)	219	14	314

Note 1: No historical data.

The area and depth of the proposed excavation are discussed in the following section. Impacts in soil above the Low Threat Closure goal levels may remain outside the proposed excavation areas (A1 and A2). However, it is anticipated the excavation will remove the majority of the secondary source material. Groundwater concentrations are expected to decrease following the excavation due to the removal of the residual soil impacts.

## 6.0 PROPOSED ACTIVITIES

### 6.1 Permitting, Utility Notification, and Borehole Clearance

Before commencing field activities Antea Group will prepare a Health and Safety Plan in accordance with state and federal requirements for use during investigation activities. Drilling permits will be obtained for the three (3) monitoring well destructions and the seven (7) soil borings from the Alameda County Public Works Agency. Prior to drilling, Underground Service Alert (USA) will be notified as required by law and a private utility locator will be employed to clear each boring location for underground utilities. In addition, an air- knife will be used to clear each boring location to a depth of 5 feet bgs prior borehole advancement.

## **6.2 Monitoring Well Destruction**

Antea Group will supervise the destruction of three (3) monitoring wells (MW-6, MW-12, and MW-12a) in preparation for the excavation. A licensed drilling company under the supervision of an Antea Group geologist will pressure grout the wells by pumping neat cement into the monitoring well casing at a pressure of approximately 25 pounds per square inch. The well boxes will be removed during the excavation. Boring logs are presented in **Appendix C**.

## **6.3 Soil Boring**

Antea Group will supervise the advancement of seven (7) soil borings in the vicinity of monitoring well MW-6 to refine the boundaries of the proposed excavation (**Figure 9**). A licensed driller, under the supervision of an Antea Group geologist, will advance the borings using a limited access drill rig with direct push technology. The total depth of the borings will be determined in the field but is anticipated to be approximately 11 feet bgs. Soil samples will be collected continuously beginning at a depth of approximately 5 feet bgs and logged using the USCS for lithologic interpretation and field screened for the presence of volatile organic compounds by headspace analysis using a pre-calibrated PID. Soil samples from the boring will be retained for laboratory analysis. The samples will be chosen based on PID readings, changes in lithology, groundwater elevation, and the total depth of the boring.

## **6.4 Soil Sampling**

Soil samples retained for analysis will be analyzed for TPHg, benzene, toluene, ethylbenzene, and total xylenes (BTEX), and MTBE, and naphthalene by Environmental Protection Agency (EPA) Method 8260B and TPHd with silica gel treatment by EPA Method 8015M. The samples will be submitted with chain-of-custody documentation to Kiff Analytical LLC (Kiff), a state of California Environmental Laboratory Accreditation Program (ELAP) certified laboratory (Certification No. 08263CA).

## **6.5 Reporting**

A summary of the well destruction and soil boring advancement activities will be submitted in a RAP addendum report. The addendum report will include a discussion of the extent of the proposed excavation. Required electronic submittals will be uploaded to the State Geotracker database.

## **7.0 PROPOSED SOIL REMEDIATION ACTION**

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Based on a review of the results of the hydraulic profile tool, TOD Bench Scale Test discussed above, current site conditions, and the distribution of petroleum impacts in soil and groundwater, Antea Group proposes the following shallow excavation to remove remaining secondary soil impacts at the site. **Figure 9** depicts the proposed extent of excavation.

### **7.1 Permitting, Notifications, and Utility Clearance**

#### **7.1.1 City and County Notifications**

The following agencies will be notified at least 10 days prior to the start of excavation activities: Alameda County Public Works Agency, City of Oakland Building and Planning Department, City of Oakland Fire Department, and the ACHCSA. Local utility companies will, also, be contacted to mark, physically expose, and provide clearance of underground utilities within 10 feet of the proposed excavation area.

#### **7.1.2 Excavation and Grading Permits**

A soil excavation permit will be obtained through the appropriate city and county public agencies. No soil excavation permits are required by the ACHCSA.

Post-excavation backfill, compaction and restoration activities within the service station property boundaries will be completed to existing grade.

#### **7.1.3 Well Destruction Permits**

A well abandonment permit application will be submitted to the Alameda County Public Works Agency for the destruction of monitoring wells MW-6, MW-12, and MW-12A, which are located within the excavation limits.

#### **7.1.4 Water Discharge Permit**

Antea Group is considering three options for disposal of water generated during dewatering of the excavation areas. These options include pumping the water into a holding tank and disposing of it off-site, discharging the water to the sewer system under permit with East Bay Municipal Utilities District, or discharging the waters to the storm drain under permit with Alameda County Flood Control and Water Conservation District. Water quality requirements, permit requirements, and the anticipated amount of generated water will be used as factors in determining which option works best for the site.

## **7.2 Site Preparation**

As indicated above, prior to initiation of field activities, Antea Group will produce a Health and Safety Plan (HASP) in accordance with Title 8, Section 5192 of the California Code of Regulations. Field personnel will perform a daily review of the HASP containing a list of emergency contacts as well as a hospital route map to the nearest emergency facility.

Pacific Convenience & Fuels (PC&F) plans to raze and rebuild the site during the second quarter of 2013. As of March 2013 these plans have not been finalized, including the final foot print of the site. Antea Group will coordinate excavation activities included in this RAP in conjunction with PC&F's proposed raze and rebuild. The excavation is contingent upon PC&F moving forward with the planned raze and rebuild. In the event, PC&F does not proceed, as planned; feasibility of implementing the excavation described herein will be re-evaluated.

### **7.2.1 Well Destruction Activities**

There are three monitoring wells MW-6, MW-12, and MW-12A located within the planned excavation limits. Since the total depths of the wells extend below the excavation depth, Antea Group will pressure grout and over excavate the wells in accordance with the requirements of the Alameda Public Works Agency. Subsequent to the proposed excavation activities only monitoring well MW-6 will be replaced.

### **7.2.2 Utility Locate and Clearance Activities**

Antea Group will contact Underground Service Alert (USA) and employ a private utility locator at least 72 hours prior to the initiation of field activities in order to clear the proposed excavation area of underground utilities. Antea Group will additionally request that utilities identified within 10 feet of the excavation limits be physically exposed by the utility owner. Figure 10 depicts known utilities at the station.

### **7.2.3 Site Set-up**

Prior to the start of excavation activities, the following set-up will be implemented at the site:

- Set-up traffic and pedestrian controls per appropriate city and/ or county public agencies approved traffic control plans;
- Set-up temporary fencing or barricades around excavation and work areas;
- Post placards and notifications at site entrance and exits identifying work, physical/chemical/environmental hazards (including Proposition 65 warnings and personal protective equipment required) and emergency contact information;
- Establish and set-up exclusion, contamination reduction, and support zones;
- Establish staging area and truck/equipment entrance and exits;

- Set-up real-time air monitoring stations and storm water control measures.

### **7.3 Excavation Extent and Methods**

#### **7.3.1 Excavation Volume and Limits**

Based on historical concentrations of COCs in soil reported at the site, the anticipated extent of excavation areas are depicted on Figure 9. The excavation will consist of two excavation areas, A1 and A2.

Excavation area A1 is bordered by a planter area to the east and a dispensing island to the west. The excavation area A1 extends south to the envelope of the dispenser island and canopy area and extends north of the location of previous monitoring well MW-2. The approximate dimensions of the excavation area A1 are 40-feet along on the north-south axis and 15-feet long along the east-west axis. The average depth of excavation anticipated to remove residual soil impacts contained in the upper clay unit of the site is approximately 11-feet bgs.

Excavation area A2 is located in the southwest corner of the site. The northwest corner of the excavation is just slightly south and west of the sump located next to the car wash. The northeast corner of the excavation is located at the edge of the canopy station building, mid-way along the south facing wall of the building. The southeast corner of the excavation is located at the border between the paved area of the site and the vegetation border to the south of the station building. The southwest corner of the excavation extends into the vegetation area along a line parallel to the canopy of the car wash. The approximate dimensions of the excavation area A2 are 50 feet along the north-south axis and 60 feet along the east-west axis. The average depth of excavation anticipated to remove residual soil impacts contained in the upper clay unit of the site is approximately 11 feet bgs.

Approximately 244 cubic yards of impacted soil will be removed from excavation area A1, and approximately 1221 cubic yards of impacted soil will be removed from excavation area A2. A total of approximately 1465 cubic yards (approximately 2124 tons using a conversion factor of 1.45 tons/ cubic yard) of impacted soil will be excavated for off-site disposal. However, the limits of excavation A2 will likely be modified and the final extent will be based on the analytical results of the soil samples collected from the seven direct push borings proposed in section 6.3, above.

#### **7.3.2 Methods of Excavation**

The specific equipment and means utilized to execute the scope of work proposed herein will be at the discretion of the selected State of California Class A licensed General Engineering Contractor. It is anticipated that this soil remediation can be accomplished using standard equipment including but not limited to an excavator, front-end loader, backhoe, end-dump trucks, and a roller wheeled compactor.

### **7.3.3 Shoring**

A temporary shoring system will be utilized to complete excavation activities. To protect the existing USTs and on-site buildings, the western, eastern, southern, and northern sidewalls of both excavation areas will be shored. Temporary shoring support will consist of traditional sheet pile shoring with lateral supports. The shoring system will be designed and stamped by a civil professional engineer.

### **7.3.4 Dewatering**

Based on the depth of the excavation and historic ground water elevations indicated in the *Quarterly Summary Report, Fourth Quarter 2012*, the excavations will require dewatering. The average depth to water during the previous three years in excavation area A1 (MW-6) has been 3.7 feet with a range of 2.9-8.4 feet; and, the average depth to water during the previous two years in excavation area A1 (MW-12) has been 4.0 feet with a range of 3.35-4.4 feet. Based on a soil porosity of 30%, the approximated volumes to be de-watered from each excavation area are: 15,000 gallons from A1, and 74,000 gallons from A2. Based on lithology of the site being homogeneous across the site and the re-charge rate of MW-6 a constant pump rate of at least 0.5 gallons/minute will be maintained during excavation and backfilling activities after initial de-watering is complete. Based on this data, Antea Group anticipates that the excavations can be dewatered to twelve (12) feet effectively using a submersible or centrifugal pump. Water generated during the dewatering will be discharged as described in Section 7.1.4.

### **7.3.5 Environmental Control Measures**

A basic and site-specific storm water pollution prevention plan (SWPPP) will be prepared using best management practices (BMPs) such as those described in the *Construction Best Management Practice Handbook* prepared by the California Stormwater Quality Association (CASQA) in 2009. Antea Group will coordinate with PC&F in determining the potential need to obtain a *Construction General Permit* for discharge..

Types of minimum techniques and practices defined in the SWPPP and implemented by the General Engineering Contractor may include the following:

- Berming down-sloping portions of the site with booms/sand/gravel bags;
- Installing stormwater control devices around the site perimeter;
- Protecting existing catch basins with booms/sand/gravel bags.

Dust control techniques will be implemented by the General Engineering Contractor at all times during the excavation, loading, and backfilling activities to prevent the formation and migration of visible dust. These techniques may include the following:

- Misting or spraying water at least twice daily to prevent formation of dust while excavating, loading, or backfilling;
- Controlling and monitoring excavation activities to minimize the generation of dust;



- Minimizing drop heights while loading transportation vehicles;
- Covering all trucks hauling soils or backfill materials, and requiring all trucks to maintain at least 2-feet of freeboard.
- Covering any stockpiles of clean fill material or top soils with weighted plastic;
- Sweep site daily if visible soil is on paved areas and being carried on public right-of-way.

Air monitoring will be performed to establish background air quality using a photoionization detector (PID) to measure ambient volatile organic compound (VOCs) concentrations, and a multi-gas lower explosive limit (LEL) detector to measure. Antea Group will prepare an Air Monitoring Plan for use during excavation activities.

### **7.3.6 Soil Transportation and Disposal Plan & Waste Characterization**

Waste hauling will be performed by a hauling contractor arranged by the General Engineering Contractor that is licensed and permitted as required by the United States Environmental Protection Agency (EPA), Department of Transportation, and the State of California. Trucks will use only pre-planned and authorized routes established in a site-specific Traffic Control and Waste Transportation Plan. Trucks used for the off-site transportation of contaminated soil and debris will remain in clean, regularly swept areas, to the extent possible, to minimize the need to decontaminate the truck tires. Each loaded truck will be equipped to fully cover all soil and debris during transportation and leave the site with a completed manifest or bill of lading for transport of the soil to the assigned disposal facility.

Soil samples from borings discussed in section 6.3 will be used to initially characterize the soil for waste disposal and select an appropriate class, State of California-permitted disposal facility. Antea Group may collect and submit additional waste samples for waste characterization analyses as requested by the selected disposal facility.

Following the approval of this RAP, Antea Group will prepare a site-specific Traffic Control and Waste Transportation Plan for implementation during soil removal activities. The Traffic Control and Waste Transportation Plan will be prepared in accordance with the Department of Toxic Substances Control (DTSC) *Transportation Plan, Preparation Guidance for Site Remediation* dated December 2001.

### **7.3.7 Confirmation Sampling Plan**

Confirmation soil samples will be collected at the final depth of the soil excavation and at accessible sidewalls. Confirmation samples will be collected at discrete locations using an approximate 20-foot by 20-foot grid for the bottom of each excavation area and approximately every 20 linear feet along the length of accessible excavation sidewalls. Since the total depth of the excavation areas is greater than 4-feet deep, confirmation samples will be collected from the excavator bucket. Antea Group personnel will screen soil samples using a PID prior to submitting the samples for laboratory analyses.

Confirmation soil samples collected for laboratory analyses will be submitted to a California Environmental Laboratory Accreditation Program (ELAP) certified laboratory for the following analyses:

- TPHg, BTEX, MTBE, tertiary-butyl alcohol (TBA), ethyl-tertiary-butyl ether (ETBE), tertiary-amyl methyl ether (TAME), di-isopropyl ether (DIPE), ethylene dibromide (EDB), ethanol, 1,2-dichloroethane (1,2-DCA), and naphthalene by EPA Method 8260B.

### **7.3.8 Backfill Materials and Methods**

Certified clean backfill materials will be mobilized to the site as arranged by the General Engineering Contractor. Following the completion of the soil excavation and confirmation sampling, the excavation area will be backfilled and compacted.

Fill material will be placed in maximum 12-inch lifts and compacted to not less than 95 percent relative compaction per standard proctor method (American Society of Testing and Materials D698). As backfill operations progress, shoring will be removed to ensure that compaction testing meets the required specifications. Compaction results will be certified by a civil or geotechnical professional engineer.

### **7.3.9 In-Situ Chemical Oxidation**

To accelerate biodegradation of the dissolved hydrocarbon plume, Regenesis brand Oxygen Release Compound® (ORC®) will be added to the excavation backfill. ORC is a proprietary formulation of phosphate-intercalated magnesium peroxide that, when hydrated, produces controlled-release oxygen. Based on calculations using Regenesis' Remediation Design Software, a minimum of approximately 100 pounds of ORC-A® for excavation area A1, and a minimum of approximately 1,100 pounds of ORC-A® for excavation area A2 will be distributed with the backfill material below the water table. This is the minimum amount needed to remediate the remaining COCs estimated in groundwater based on stoichiometric calculations. Additional ORC may be added to the excavation area to increase the migration potential of dissolved oxygen laterally across the site and to offsite areas. The groundwater infiltration into the backfilled excavation will assist in the releasing of oxygen to the shallow aquifer. The amount of ORC-A used will be based upon the limits of the final excavations. The Material Safety Data Sheet for ORC-A® is attached as **Appendix D**.

### **7.3.10 Record Keeping**

At minimum, Antea Group will measure and record the limits of excavation, daily air monitoring data, daily dewatering and discharge volumes, confirmation sampling locations and PID results and import fill material types

and quantities. Antea Group will also maintain a daily log of site personnel arriving and leaving, complete a daily checklist for site set-up and control measures and retain copies of bills of lading and manifests.

A detailed log of the soil hauled off-site will be maintained. The log will include, at minimum, the date and time trucks are loaded, the destination, size (estimated volume and weight) of the load, description of contents, name and signature of the hauler, truck license plate number, name and signature of Antea Group personnel or the General Engineering Contractor personnel.

#### **7.4 Post-Excavation Monitoring Plan**

Antea Group proposes to replace only monitoring well MW-6 subsequent to the remediation excavation and ORC-A® application. Antea Group has already submitted a work plan proposing the removal of monitoring well MW-12A, so this monitoring well will not be replaced. In addition, there are currently two monitoring wells in the vicinity and down-gradient of monitoring well MW-12, so Antea Group does not propose that this monitoring well be replaced. Antea Group further recommends that the site monitoring wells in the vicinity of the two excavations and monitoring well MW-6R be monitoring and sampled on a quarterly basis, subsequent to the remediation excavation and ORC-A® application to evaluate the on-site effect of removing the residual impacted soil material.


### **8.0 IMPLEMENTATION SCHEDULE**

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Antea Group is prepared to implement this remedial action plan in conjunction with the raise and rebuild activities being conducted by PC&F, which are anticipated to take place during the second quarter of 2013. Accordingly, Antea Group requests a timely review, within 60 days, of this remedial action plan.

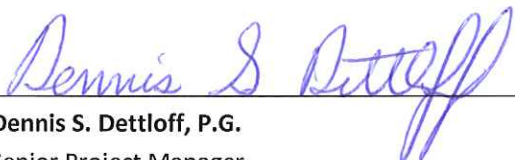
## 9.0 REMARKS

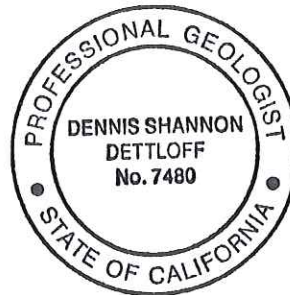
The recommendations contained in this report represent Antea USA, Inc.'s professional opinions based upon the currently available information and are arrived at in accordance with currently accepted professional standards. This report is based upon a specific scope of work requested by the client. For any reports cited that were not generated by Delta or Antea Group, the data from those reports is used "as is" and is assumed to be accurate. Antea Group does not guarantee the accuracy of this data for the referenced work performed nor the inferences or conclusions stated in these reports. The contract between Antea USA, Inc. and its client outlines the scope of work, and only those tasks specifically authorized by that contract or outlined in this report were performed. This report is intended only for the use of Antea USA, Inc.'s client and anyone else specifically identified in writing by Antea USA, Inc. as a user of this report. Antea USA, Inc. will not and cannot be liable for unauthorized reliance by any other third party. Other than as contained in this paragraph, Antea USA, Inc. makes no express or implied warranty as to the contents of this report.

 For:  
\_\_\_\_\_  
**Garrett Griffiths, CHMM**  
Project Manager  
Antea Group

 For:  
\_\_\_\_\_  
**Josh Mahoney**  
Senior Project Manager  
Antea Group

Reviewed by:

\_\_\_\_\_  
**Dennis S. Dettloff, P.G.**  
Senior Project Manager  
California Registered Professional Geologist No. 7480  
Antea Group



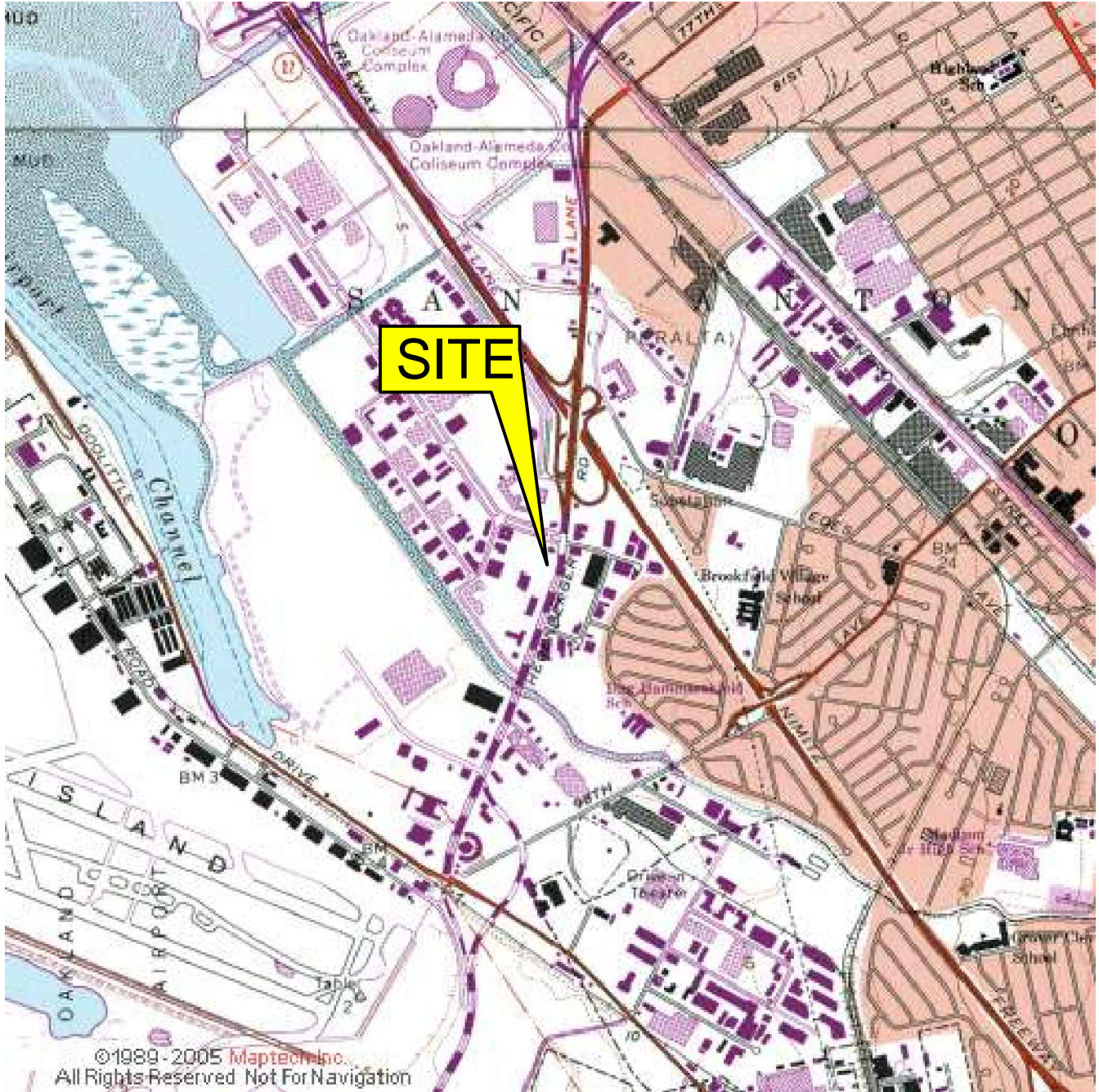
cc: GeoTracker

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## **Figures**

- Figure 1 Site Location Map
- Figure 2 Site Plan
- Figure 3 Groundwater Elevation Contour Map, December 13, 2012
- Figure 4 Dissolved Phase TPHg Isoconcentration Map, December 13, 2012
- Figure 5 Dissolved Phase TPHd Isoconcentration Map, December 13, 2012
- Figure 6 Dissolved Phase MTBE Isoconcentration Map, December 13, 2012
- Figure 7 Dissolved Phase Benzene Isoconcentration Map, December 13, 2012
- Figure 8 Site Plan with Historical Sample Locations and Concentrations
- Figure 9 Site Plan with Proposed Excavation
- Figure 10 Site Plan with Utilities





North

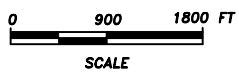


FIGURE 1  
SITE LOCATION

76 STATION NO. 5191/5043  
449 HEGENBERGER ROAD  
OAKLAND, CALIFORNIA

PROJECT NO. 142705191	PREPARED BY EW	DRAWN BY DR/JH
DATE 4/11/13	REVIEWED BY DD	FILE NAME 5043-SiteLocator



EDGEWATER DR.

LEGEND

- ⊕ MW- MONITORING WELL
- ⊙ MW- ABANDONED MONITORING WELL

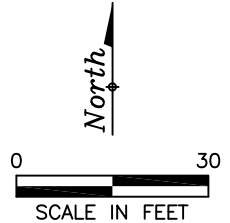
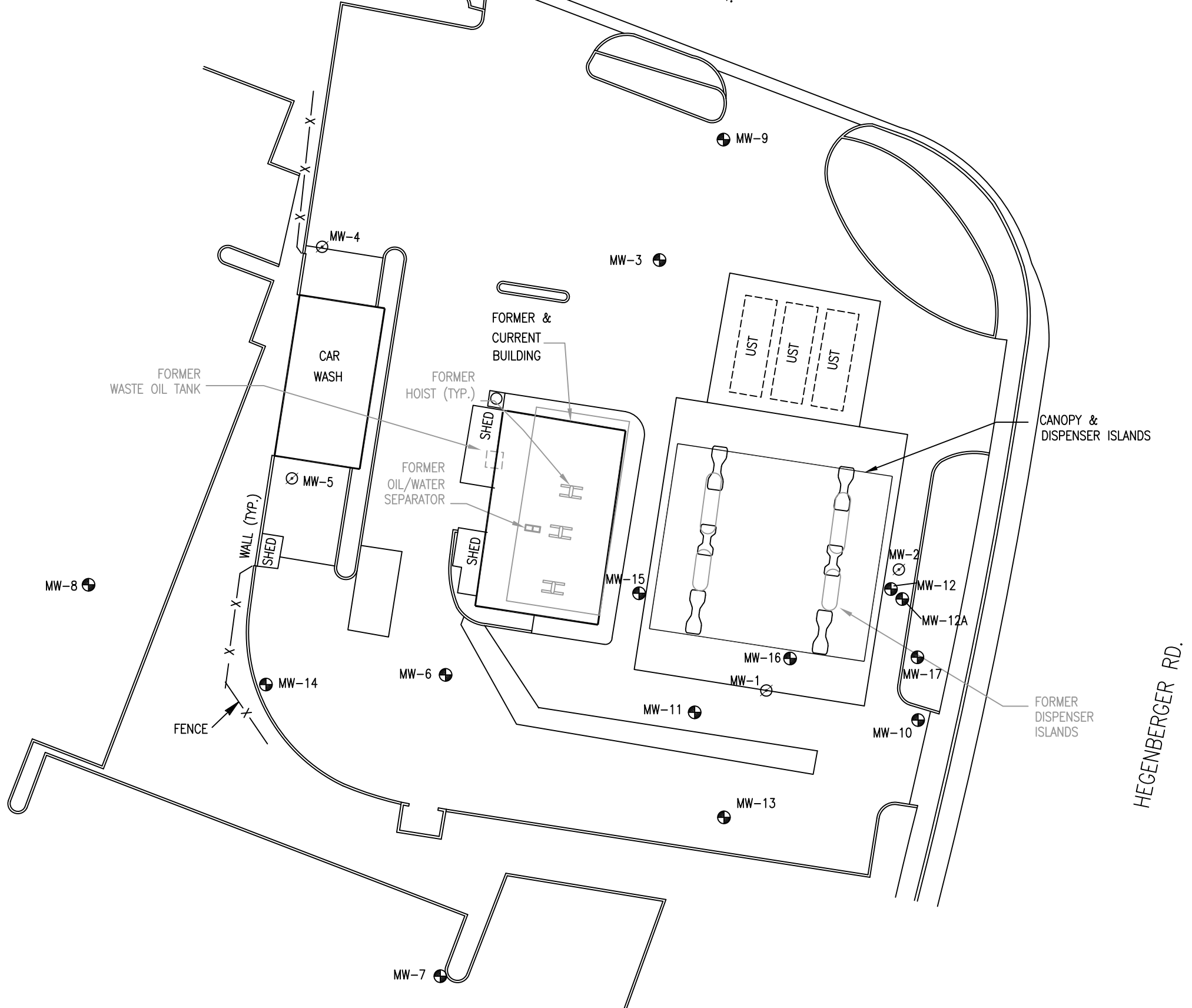

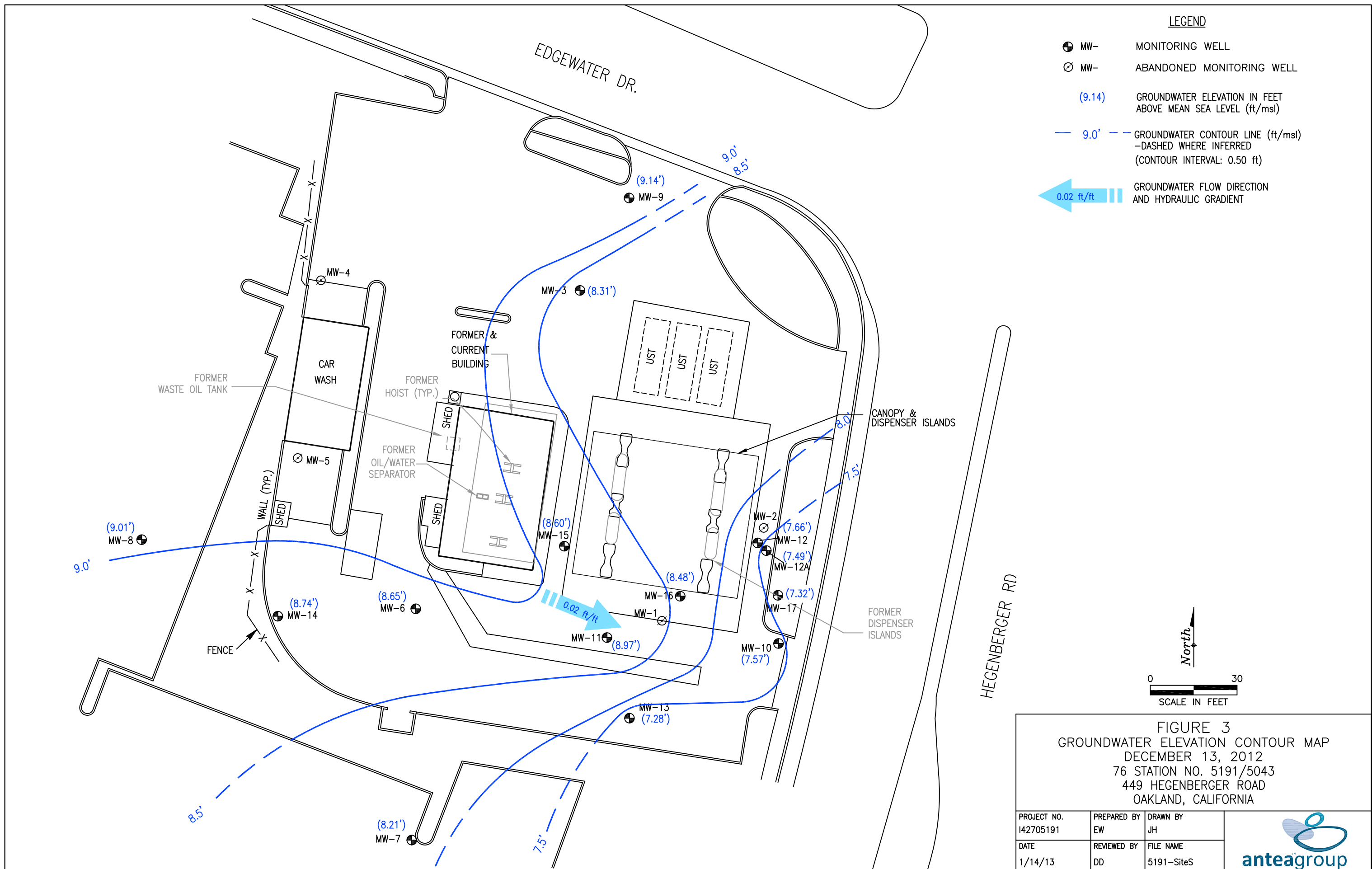


FIGURE 2  
SITE PLAN

76 STATION NO. 5191/5043  
449 HEGENBERGER ROAD  
OAKLAND, CALIFORNIA

PROJECT NO. 142705191	PREPARED BY DD	DRAWN BY JH	
DATE 5/26/11	REVIEWED BY DD	FILE NAME 5191-SiteS	



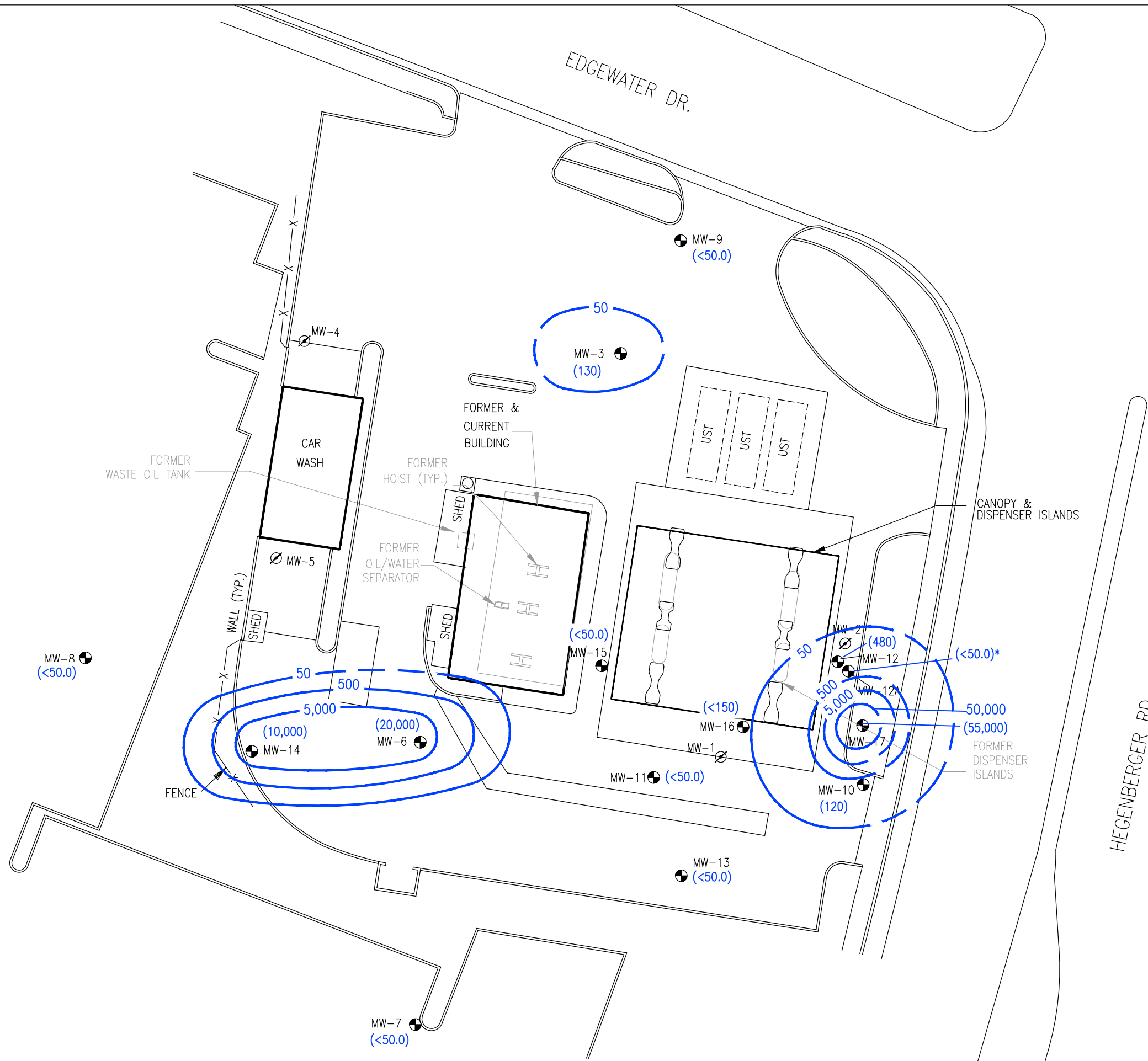


**FIGURE 3**  
**GROUNDWATER ELEVATION CONTOUR MAP**  
 DECEMBER 13, 2012  
 76 STATION NO. 5191/5043  
 449 HEGENBERGER ROAD  
 OAKLAND, CALIFORNIA

PROJECT NO. 142705191	PREPARED BY EW	DRAWN BY JH
DATE 1/14/13	REVIEWED BY DD	FILE NAME 5191-SiteS





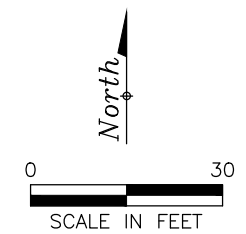


**LEGEND**

- MW- MONITORING WELL
- ⊘ MW- ABANDONED MONITORING WELL
- (55,000) DISSOLVED PHASE TPHg ISOCONCENTRATION (µg/L)
- 5,000 — DISSOLVED PHASE TPHg ISOCONTOUR (µg/L)  
-DASHED WHERE INFERRED

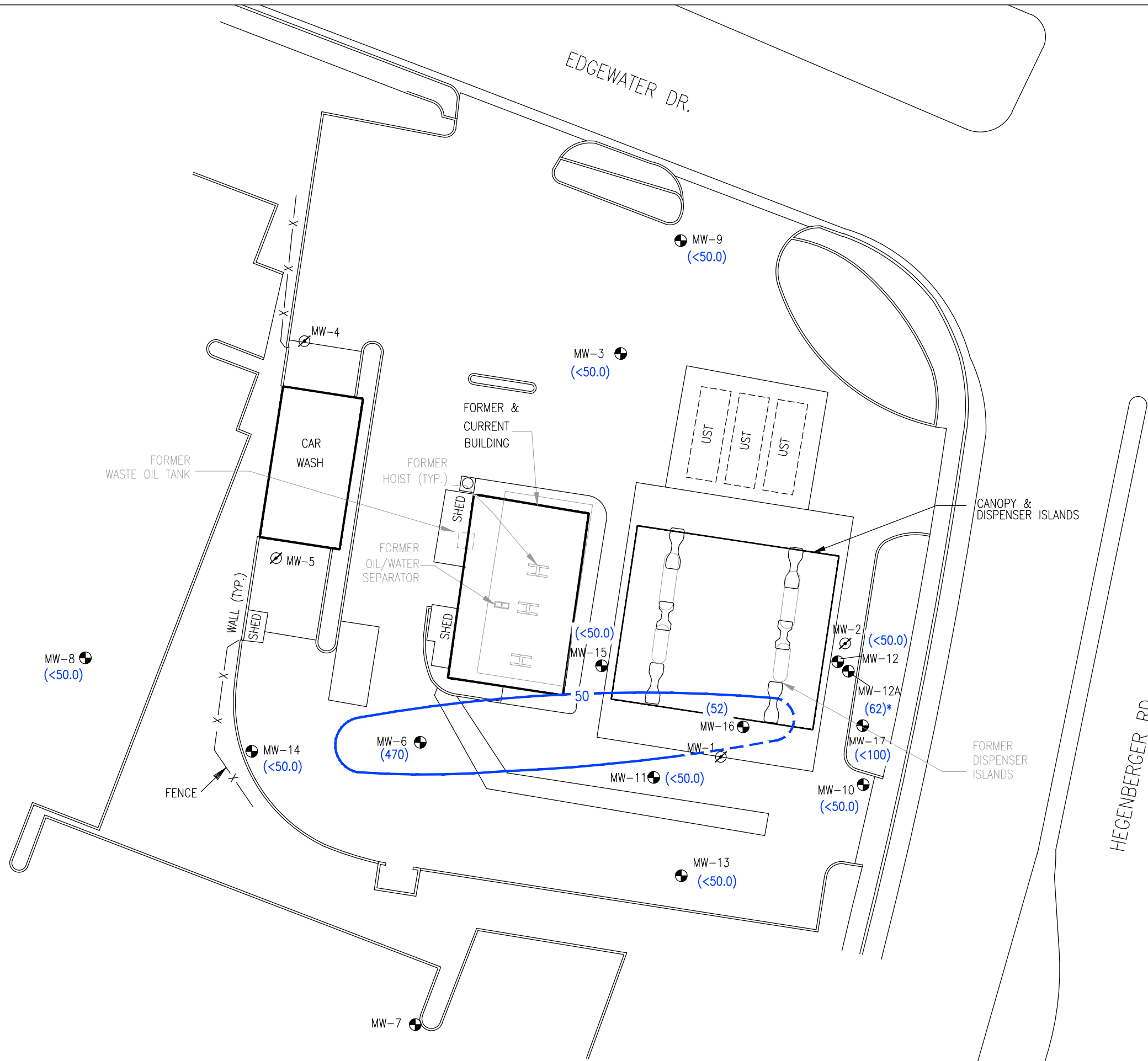
**NOTES:**

- TPHg = TOTAL PETROLEUM HYDROCARBONS AS GASOLINE
- µg/L = MICROGRAMS PER LITER
- <50 = LESS THAN LABORATORY INDICATED REPORTING LIMIT
- \* = NOT USED IN CONTOURING



**FIGURE 4**  
 DISSOLVED PHASE TPHg ISOCONCENTRATION MAP  
 DECEMBER 13, 2012  
 76 STATION NO. 5191/5043  
 449 HEGENBERGER ROAD  
 OAKLAND, CALIFORNIA

PROJECT NO. I42705191	PREPARED BY EW	DRAWN BY JH	
DATE 1/14/13	REVIEWED BY DD	FILE NAME 5191-SiteS	

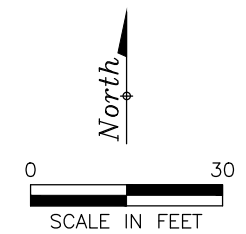


**LEGEND**

- MW- MONITORING WELL
- ⊘ MW- ABANDONED MONITORING WELL
- (420) DISSOLVED PHASE TPHd ISOCONCENTRATION (µg/L)
- 50 — DISSOLVED PHASE TPHd ISOCONTOUR (µg/L)  
-DASHED WHERE INFERRED

**NOTES:**

TPHd = TOTAL PETROLEUM HYDROCARBONS AS DIESEL  
 µg/L = MICROGRAMS PER LITER  
 <50.0 = LESS THAN LABORATORY INDICATED REPORTING LIMIT  
 \* = NOT USED IN CONTOURING



**FIGURE 5**  
 DISSOLVED PHASE TPHd ISOCONCENTRATION MAP  
 DECEMBER 13, 2012  
 76 STATION NO. 5191/5043  
 449 HEGENBERGER ROAD  
 OAKLAND, CALIFORNIA

PROJECT NO. I42705191	PREPARED BY EW	DRAWN BY JH
DATE 1/14/13	REVIEWED BY DD	FILE NAME 5191-SiteS



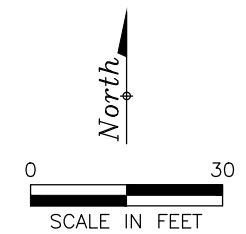


**LEGEND**

- MW- MONITORING WELL
- ⊘ MW- ABANDONED MONITORING WELL
- (980) DISSOLVED PHASE MTBE ISOCONCENTRATION (µg/L)
- 500 — DISSOLVED PHASE MTBE ISOCONTOUR (µg/L)  
-DASHED WHERE INFERRED

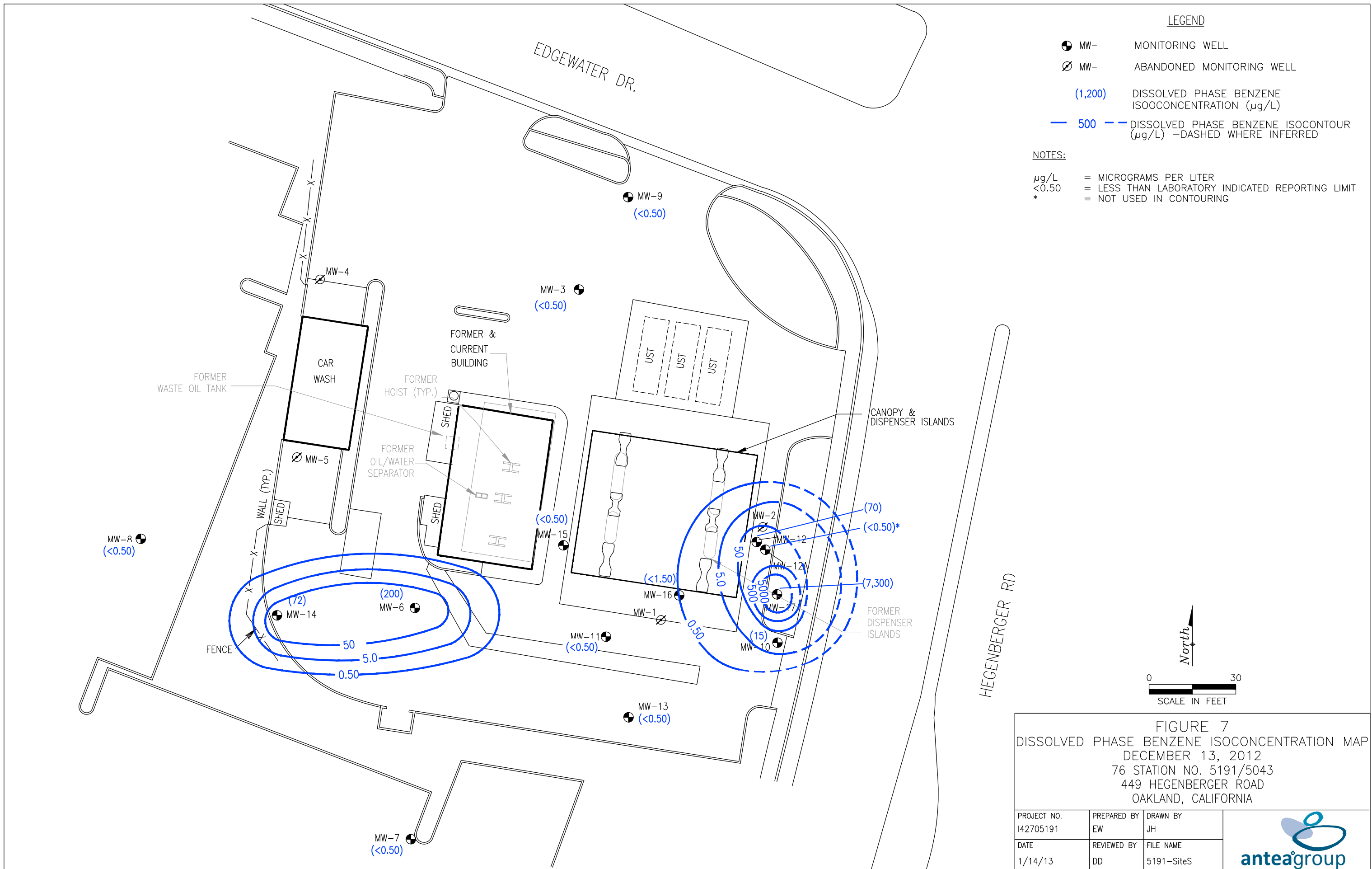
**NOTES:**

MTBE = METHYL TERTIARY BUTYL ETHER  
 µg/L = MICROGRAMS PER LITER  
 <0.50= LESS THAN LABORATORY INDICATED REPORTING LIMIT  
 \* = NOT USED IN CONTOURING



**FIGURE 6**  
 DISSOLVED PHASE MTBE ISOCONCENTRATION MAP  
 DECEMBER 13, 2012  
 76 STATION NO. 5191/5043  
 449 HEGENBERGER ROAD  
 OAKLAND, CALIFORNIA

PROJECT NO. I42705191	PREPARED BY EW	DRAWN BY JH	
DATE 1/14/13	REVIEWED BY DD	FILE NAME 5191-SiteS	

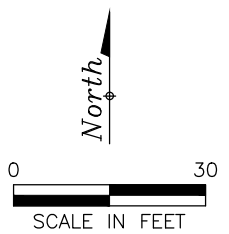


**LEGEND**

- MW- MONITORING WELL
- ⊘ MW- ABANDONED MONITORING WELL
- (1,200) DISSOLVED PHASE BENZENE ISOCONCENTRATION (µg/L)
- 500 — DISSOLVED PHASE BENZENE ISOCONTOUR (µg/L) -DASHED WHERE INFERRED

**NOTES:**

- µg/L = MICROGRAMS PER LITER
- <0.50 = LESS THAN LABORATORY INDICATED REPORTING LIMIT
- \* = NOT USED IN CONTOURING

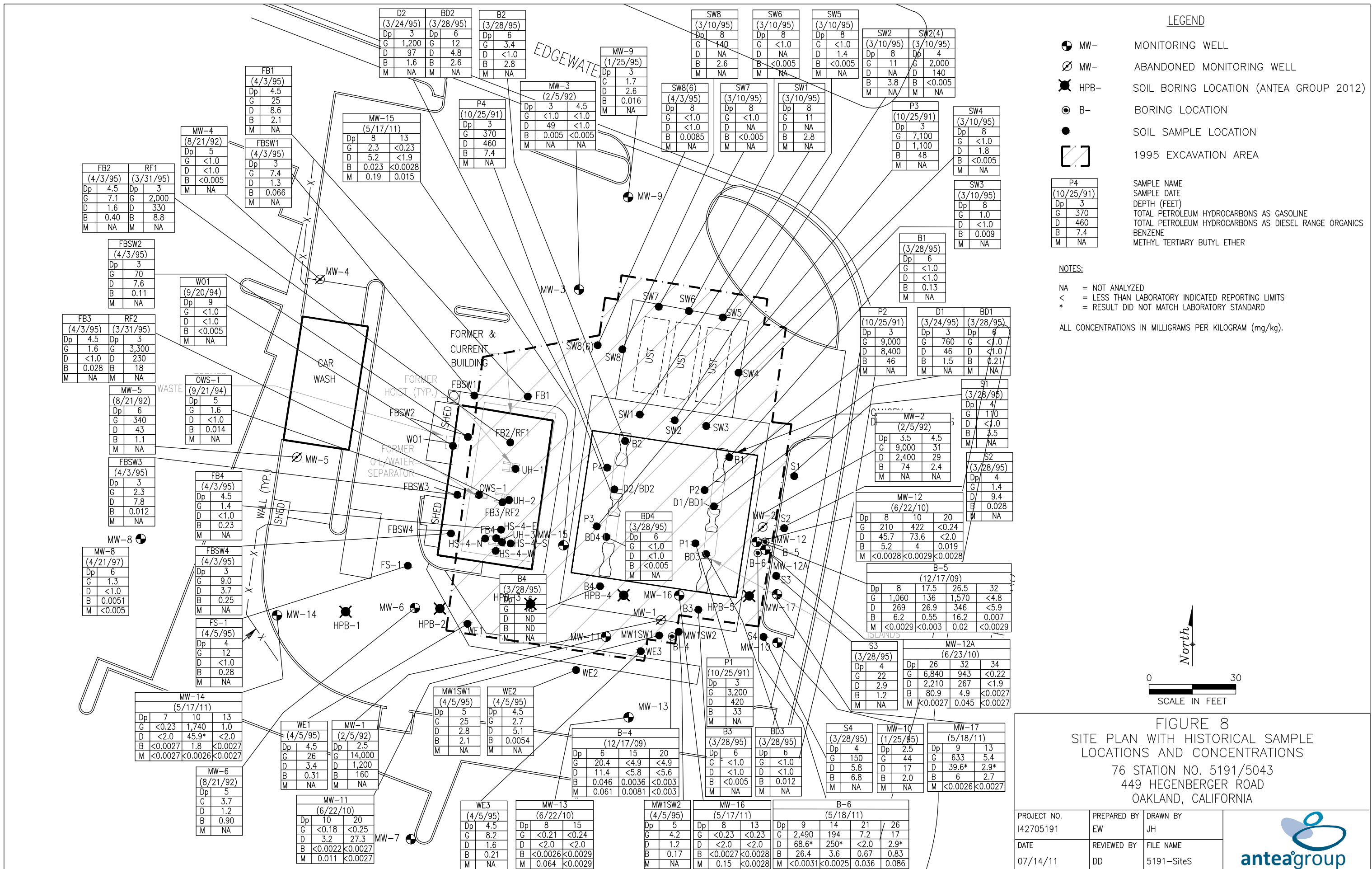


**FIGURE 7**  
 DISSOLVED PHASE BENZENE ISOCONCENTRATION MAP  
 DECEMBER 13, 2012  
 76 STATION NO. 5191/5043  
 449 HEGENBERGER ROAD  
 OAKLAND, CALIFORNIA

PROJECT NO. I42705191	PREPARED BY EW	DRAWN BY JH
DATE 1/14/13	REVIEWED BY DD	FILE NAME 5191-SiteS







LEGEND

- MW- MONITORING WELL
- ⊗ MW- ABANDONED MONITORING WELL
- ⊗ HPB- SOIL BORING LOCATION (ANTEA GROUP 2012)
- B- BORING LOCATION
- SOIL SAMPLE LOCATION
- 1995 EXCAVATION AREA

P4	
(10/25/91)	SAMPLE NAME
Dp 3	SAMPLE DATE
G 370	DEPTH (FEET)
D 460	TOTAL PETROLEUM HYDROCARBONS AS GASOLINE
B 7.4	TOTAL PETROLEUM HYDROCARBONS AS DIESEL RANGE ORGANICS
M NA	BENZENE
	METHYL TERTIARY BUTYL ETHER

- NOTES:
- NA = NOT ANALYZED
  - < = LESS THAN LABORATORY INDICATED REPORTING LIMITS
  - \* = RESULT DID NOT MATCH LABORATORY STANDARD

ALL CONCENTRATIONS IN MILLIGRAMS PER KILOGRAM (mg/kg).

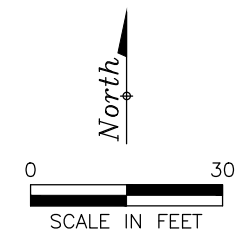
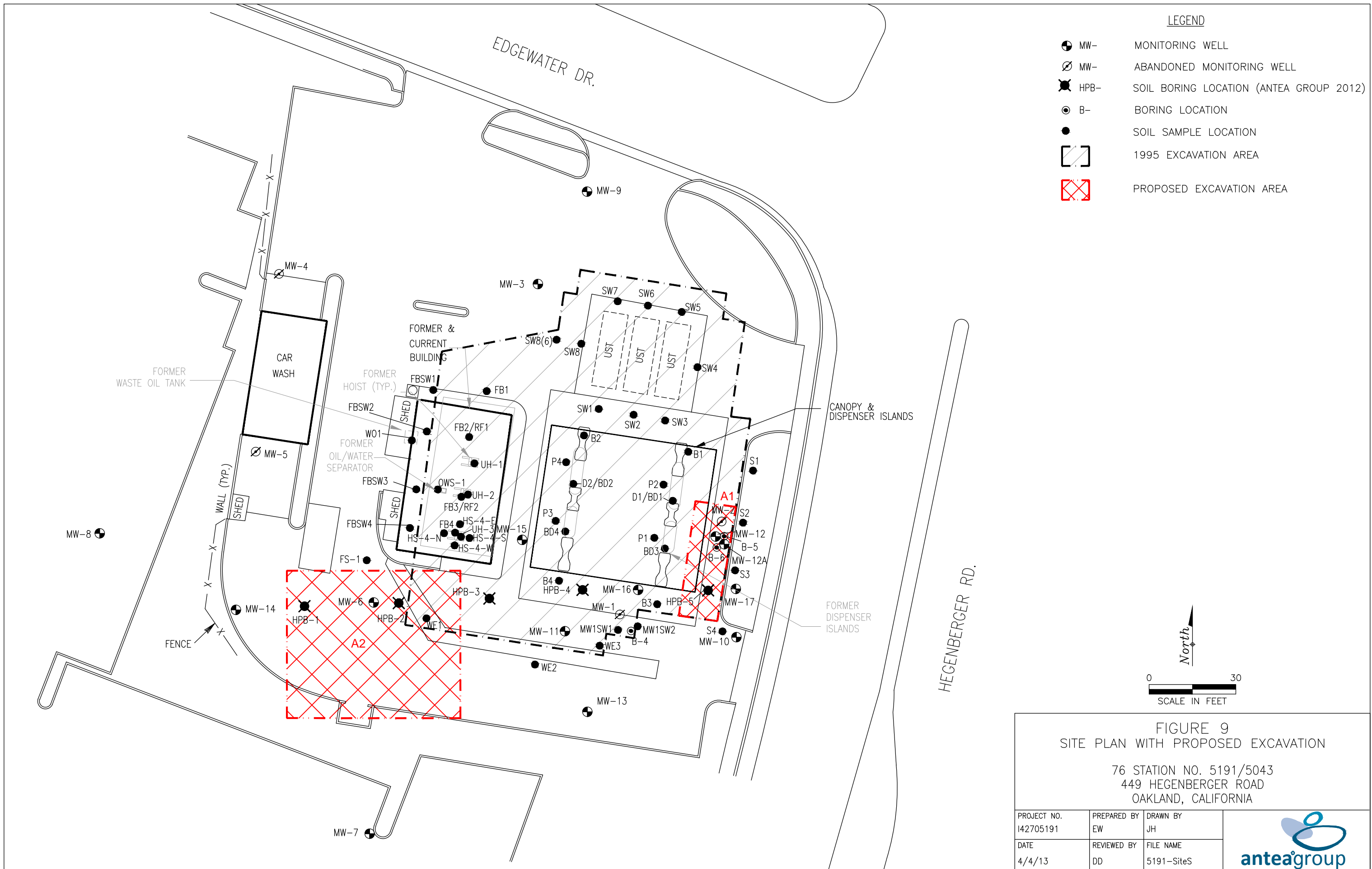


FIGURE 8  
 SITE PLAN WITH HISTORICAL SAMPLE  
 LOCATIONS AND CONCENTRATIONS  
 76 STATION NO. 5191/5043  
 449 HEGENBERGER ROAD  
 OAKLAND, CALIFORNIA

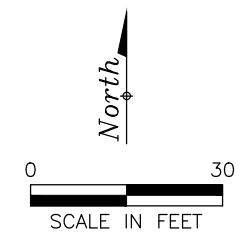
PROJECT NO. I42705191	PREPARED BY EW	DRAWN BY JH
DATE 07/14/11	REVIEWED BY DD	FILE NAME 5191-SiteS





**LEGEND**

- MW- MONITORING WELL
- ⊘ MW- ABANDONED MONITORING WELL
- ⊗ HPB- SOIL BORING LOCATION (ANTEA GROUP 2012)
- ⊙ B- BORING LOCATION
- SOIL SAMPLE LOCATION
- ▭ 1995 EXCAVATION AREA
- ▭ (red cross-hatch) PROPOSED EXCAVATION AREA

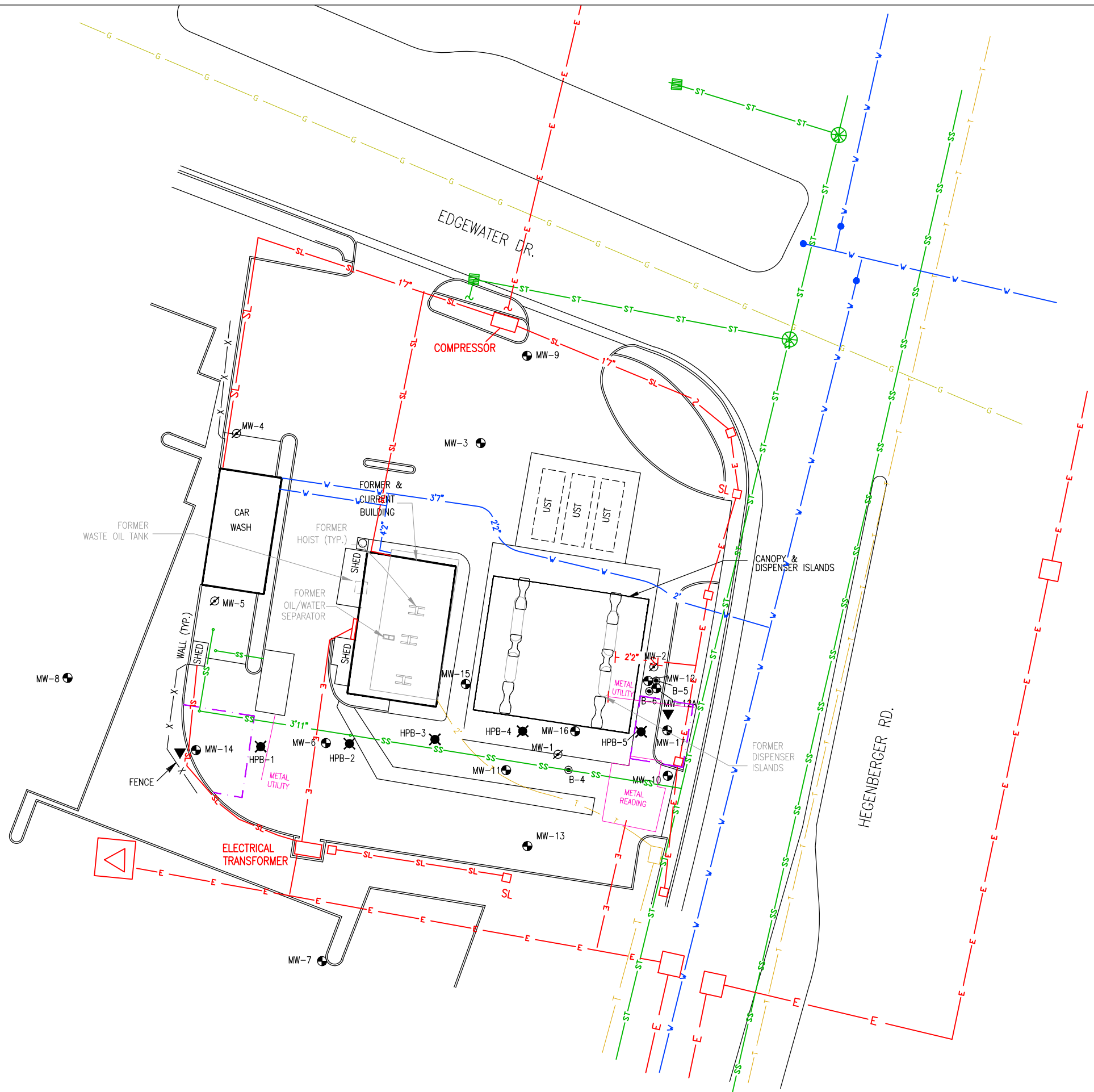


**FIGURE 9**  
SITE PLAN WITH PROPOSED EXCAVATION

76 STATION NO. 5191/5043  
449 HEGENBERGER ROAD  
OAKLAND, CALIFORNIA

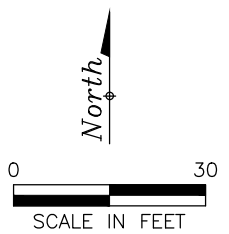
PROJECT NO. I42705191	PREPARED BY EW	DRAWN BY JH
DATE 4/4/13	REVIEWED BY DD	FILE NAME 5191-SiteS





**LEGEND**

- MW- MONITORING WELL
- MW- ABANDONED MONITORING WELL
- HPB- SOIL BORING LOCATION (ANTEA GROUP 2012)
- B- BORING LOCATION
- T TELEPHONE
- SS SEWER
- W WATER
- ST STORM DRAIN
- E ELECTRIC
- G GAS
- SL STREET LIGHT
- ▼ SOIL BUFFERING TEST LOCATION
- [ ] PILOT TEST INJECTION AREA



**FIGURE 10**  
**SITE PLAN WITH UTILITIES**  
 76 STATION NO. 5191/5043  
 449 HEGENBERGER ROAD  
 OAKLAND, CALIFORNIA

PROJECT NO. I42705191	PREPARED BY EW	DRAWN BY JH
DATE 4/4/13	REVIEWED BY DD	FILE NAME 5191-SiteS



**Remedial Action Plan**  
**76 Service Station No. 5191/5043**  
**449 Hegenberger Road**  
**Oakland, California**  
**Antea Group Project No. I42705191**



## ***Tables***

Table 1	Well Construction Details
Table 2	Current Groundwater Gauging and Analytical Data
Table 2a	Historical Groundwater Gauging and Analytical Data
Table 3	Historical Soil Analytical Results



**TABLE 1**  
**WELL CONSTRUCTION DETAILS**  
**76 STATION NO. 5191/5043**  
**449 HEGENBERGER ROAD**  
**OAKLAND, CALIFORNIA**



Well	Drill	Well		Screen		Screen	Comments
		Depth	Diameter	Top	Bottom	Length	
I.D.	Date	(feet bgs)	(inches)	(feet bgs)	(feet bgs)	(feet)	
<b>Monitoring Wells</b>							
MW-1	02/05/91	13.5	2	2.0	13.0	11.0	Abandoned
MW-2	02/05/91	15.0	2	3.0	15.0	12.0	Abandoned
MW-3	02/05/91	14.0	2	2.0	14.0	12.0	
MW-4	08/21/92	13.5	2	2.5	13.5	11.0	Abandoned
MW-5	08/21/92	13.5	2	2.5	13.5	11.0	Abandoned
MW-6	08/21/92	13.5	2	2.5	13.5	11.0	
MW-7	04/21/97	13.0	2	3.0	13.0	10.0	
MW-8	04/21/97	15.0	2	3.0	15.0	12.0	
MW-9	01/25/95	13.0	2	3.0	13.0	10.0	
MW-10	01/25/95	13.0	2	3.0	13.0	10.0	
MW-11	06/22/10	20.0	4	5.0	20.0	15.0	
MW-12	06/22/10	20.0	4	5.0	20.0	15.0	
MW-12A	06/23/10	34.0	2	30.0	34.0	4.0	
MW-13	06/22/10	15.0	2	5.0	15.0	10.0	
MW-14	05/17/11	13.0	2	3.0	13.0	10.0	
MW-15	05/17/11	13.0	2	3.0	13.0	10.0	
MW-16	05/17/11	13.0	2	3.0	13.0	10.0	
MW-17	05/18/11	13.0	2	3.0	13.0	10.0	

**Explanation**

Wells are of poly-vinyl-chloride (PVC) construction

bgs = Below ground surface

TABLE 2  
 CURRENT GROUNDWATER GAUGING AND ANALYTICAL DATA  
 76 STATION NO. 5191/5043  
 449 HEGENBERGER ROAD  
 OAKLAND, CALIFORNIA



Well I.D.	Date	GROUNDWATER GAUGING DATA				GROUNDWATER ANALYTICAL DATA								
		TOC Elevation (ft)	Depth to Water (ft)	LNAPL Thickness (ft)	Water Elevation* (ft)	TPHd (ug/L)	TPHg (ug/L)	Benzene (ug/L)	Toluene (ug/L)	Ethylbenzene (ug/L)	Total Xylenes (ug/L)	MTBE (ug/L)	TBA (ug/L)	Ethanol (ug/L)
MW-3	12/13/2012	10.81	2.50	NP	8.31	<50	<b>130</b>	<0.50	<0.50	<0.50	<0.50	<b>28</b>	<b>77</b>	<5.0
MW-6	12/13/2012	11.55	2.90	NP	8.65	<b>470</b>	<b>20,000</b>	<b>200</b>	<b>16</b>	<b>350</b>	<b>1,100</b>	<4.0	<b>22</b>	<40
MW-7	12/13/2012	11.64	3.43	NP	8.21	<50	<50	<0.50	<0.50	<0.50	<0.50	<0.50	<5.0	<5.0
MW-8	12/13/2012	11.32	2.31	NP	9.01	<50	<50	<0.50	<0.50	<0.50	<0.50	<0.50	<5.0	<5.0
MW-9	12/13/2012	10.94	1.80	NP	9.14	<50	<50	<0.50	<0.50	<0.50	<0.50	<0.50	<5.0	<5.0
MW-10	12/13/2012	10.97	3.40	NP	7.57	<50	<b>120</b>	<b>15</b>	<b>1.1</b>	<b>1.7</b>	<b>5.2</b>	<0.50	<5.0	<5.0
MW-11	12/13/2012	10.53	1.56	NP	8.97	<50	<50	<0.50	<0.50	<0.50	<0.50	<b>27</b>	<5.0	<5.0
MW-12	12/13/2012	11.01	3.35	NP	7.66	<50	<b>480</b>	<b>70</b>	<b>4.6</b>	<b>7.2</b>	<b>19</b>	<b>820</b>	<b>19</b>	<15
MW-12A	12/13/2012	11.29	3.80	NP	7.49	<b>62</b>	<50	<0.50	<0.50	<0.50	<0.50	<0.50	<5.0	<5.0
MW-13	12/13/2012	11.08	3.80	NP	7.28	<50	<50	<0.50	<0.50	<0.50	<0.50	<b>130</b>	<b>14</b>	<5.0
MW-14	12/13/2012	12.00	3.26	NP	8.74	<50	<b>10,000</b>	<b>72</b>	<b>5.8</b>	<b>610</b>	<b>780</b>	<1.5	<7.0	<15
MW-15	12/13/2012	11.11	2.51	NP	8.60	<50	<50	<0.50	<0.50	<0.50	<0.50	<b>33</b>	<b>7.4</b>	<5.0
MW-16	12/13/2012	10.98	2.50	NP	8.48	<b>52</b>	<150	<1.5	<1.5	<1.5	<1.5	<b>980</b>	<b>55</b>	<20
MW-17	12/13/2012	11.52	4.20	NP	7.32	<100	<b>55,000</b>	<b>7,300</b>	<b>2,700</b>	<b>1,700</b>	<b>4,600</b>	<10	<b>300</b>	<100

**Gauging Notes:**

TOS - Top of Screen  
 ft - Feet  
 NP - LNAPL not present  
 LNAPL - Light non-aqueous phase liquid  
 \* - Corrected for LNAPL if present (assumes LNAPL specific gravity = 0.75)  
 --- No information available

**Analytical Notes:**

< - Below laboratory's indicated reporting limit  
 ug/L - micrograms/liter  
 TPHd- Total petroleum hydrocarbons as diesel  
 TPHg- Total petroleum hydrocarbons as gasoline  
 MTBE- Methyl tertiary-butyl ether  
 TBA- Tertiary-butyl alcohol  
**Bold** - Above the laboratory's indicated reporting limit

TABLE 2a  
HISTORICAL GROUNDWATER GAUGING AND ANALYTICAL DATA  
76 STATION NO. 5191/5043  
449 HEGENBERGER ROAD  
OAKLAND, CALIFORNIA



Well I.D.	Date	GROUNDWATER GAUGING DATA				GROUNDWATER ANALYTICAL DATA															
		TOC Elevation (ft)	Depth to Water (ft)	LNAPL Thickness (ft)	Water Elevation* (ft)	TPHd (ug/L)	TPHg (ug/L)	Benzene (ug/L)	Toluene (ug/L)	Ethylbenzene (ug/L)	Total Xylenes (ug/L)	MTBE (SW8021B) (ug/L)	MTBE (SW8260B) (ug/L)	DIPE (ug/L)	ETBE (ug/L)	TAME (ug/L)	TBA (ug/L)	Ethanol (ug/L)	1,2-Dibromoethane (EDB) (ug/L)	1,2-Dichloroethane (ug/L)	
MW-1	2/18/1992	NSVD	NG	NG	NG	13,000	150,000	17,000	26,000	5,200	26,000	--	--	--	--	--	--	--	--	--	
	5/20/1992	NSVD	NG	NG	NG	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	
	8/31/1992	NSVD	NG	NG	NG	8,900	64,000	13,000	12,000	2,500	22,000	--	--	--	--	--	--	--	--	--	
	11/30/1992	NSVD	NG	NG	NG	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	
	2/4/1993	NSVD	NG	NG	NG	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	
	5/4/1993	8.96	2.13	0.10	6.91	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	8/4/1993	8.96	2.92	0.03	6.06	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	11/3/1993	7.38	3.04	NP	4.34	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	2/7/1994	7.38	2.55	0.03	4.85	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	5/19/1994	7.38	2.23	0.01	5.16	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	6/25/1994	7.38	2.49	0.01	4.90	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	7/27/1994	7.38	3.10	NP	4.28	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	8/15/1994	7.38	2.85	0.11	4.61	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	11/14/1994	7.38	2.97	0.12	4.50	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	2/21/1995	7.38	1.53	0.02	5.87	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
5/18/1995	NSVD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	
MW-2	2/18/1992	NSVD	NG	NG	NG	4,300	29,000	1,000	5,300	260	7,900	--	--	--	--	--	--	--	--	--	
	5/20/1992	NSVD	NG	NG	NG	4,300	24,000	2,200	7,600	630	11,000	--	--	--	--	--	--	--	--	--	--
	8/31/1992	NSVD	NG	NG	NG	1,600	9,000	1,800	640	140	2,000	--	--	--	--	--	--	--	--	--	--
	11/30/1992	NSVD	NG	NG	NG	5,700	29,000	2,000	3,400	1,200	6,900	--	--	--	--	--	--	--	--	--	--
	2/4/1993	NSVD	NG	NG	NG	6,100	18,000	1,600	3,000	ND	6,900	--	--	--	--	--	--	--	--	--	--
	5/4/1993	8.96	2.48	NP	6.48	7,100	63,000	3,200	17,000	470	17,000	--	--	--	--	--	--	--	--	--	--
	8/4/1993	8.96	3.20	NP	5.76	1,800	45,000	2,100	6,600	1,400	12,000	--	--	--	--	--	--	--	--	--	--
	11/3/1993	8.58	3.37	NP	5.21	2,600	72,000	3,700	16,000	3,700	20,000	--	--	--	--	--	--	--	--	--	--
	2/7/1994	8.58	2.40	NP	6.18	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	5/19/1994	8.58	2.13	NP	6.45	3,000	42,000	2,500	1,300	2,300	13,000	--	--	--	--	--	--	--	--	--	--
	6/25/1994	8.58	2.65	NP	5.93	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	7/27/1994	8.58	3.44	NP	5.14	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	8/15/1994	8.58	3.25	NP	5.33	2,800	35,000	2,400	850	1,700	15,000	--	--	--	--	--	--	--	--	--	--
	11/14/1994	8.58	2.13	NP	6.45	10,000	43,000	2,200	6,500	1,800	14,000	--	--	--	--	--	--	--	--	--	--
	2/21/1995	8.58	1.65	NP	6.93	2,000	44,000	2,200	3,200	1,300	1,500	--	--	--	--	--	--	--	--	--	--
5/18/1995	NSVD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	
MW-3	2/18/1992	NSVD	NG	NG	NG	ND	230	5	22	2	33	--	--	--	--	--	--	--	--	--	
	5/20/1992	NSVD	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI
	8/31/1992	NSVD	NG	NG	NG	92	210	1	ND	ND	ND	--	--	--	--	--	--	--	--	--	--
	11/30/1992	NSVD	NG	NG	NG	94	790	ND	ND	ND	ND	--	--	--	--	--	--	--	--	--	--
	2/4/1993	NSVD	NG	NG	NG	550	3,300	320	ND	96	6	--	--	--	--	--	--	--	--	--	--
	5/4/1993	7.84	4.32	NP	3.52	250	1,800	95	ND	ND	ND	--	--	--	--	--	--	--	--	--	--
	8/4/1993	7.84	4.94	NP	2.90	100	210	ND	ND	ND	ND	--	--	--	--	--	--	--	--	--	--
	11/3/1993	7.42	4.53	NP	2.89	160	640	ND	ND	ND	ND	--	--	--	--	--	--	--	--	--	--
	2/7/1994	7.42	2.40	NP	5.02	620	2,700	110	ND	17	ND	--	--	--	--	--	--	--	--	--	--
	5/19/1994	7.42	3.60	NP	3.82	480	1,800	83	ND	6	9	--	--	--	--	--	--	--	--	--	--
	6/25/1994	7.42	4.58	NP	2.84	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	7/27/1994	7.42	4.58	NP	2.84	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	8/15/1994	7.42	4.65	NP	2.77	110	130	1	1	ND	1	--	--	--	--	--	--	--	--	--	--
	11/14/1994	7.42	3.18	NP	4.24	150	1,600	ND	ND	ND	ND	--	--	--	--	--	--	--	--	--	--
	2/21/1995	7.42	1.81	NP	5.61	850	3,800	350	ND	130	22	--	--	--	--	--	--	--	--	--	--
5/18/1995	7.42	4.56	NP	2.86	150	1,300	42	ND	ND	ND	--	--	--	--	--	--	--	--	--	--	
8/17/1995	7.42	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	
7/26/1996	7.42	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	

TABLE 2a  
HISTORICAL GROUNDWATER GAUGING AND ANALYTICAL DATA  
76 STATION NO. 5191/5043  
449 HEGENBERGER ROAD  
OAKLAND, CALIFORNIA



Well I.D.	Date	GROUNDWATER GAUGING DATA				GROUNDWATER ANALYTICAL DATA														
		TOC Elevation (ft)	Depth to Water (ft)	LNAPL Thickness (ft)	Water Elevation* (ft)	TPHd (ug/L)	TPHg (ug/L)	Benzene (ug/L)	Toluene (ug/L)	Ethylbenzene (ug/L)	Total Xylenes (ug/L)	MTBE (SW8021B) (ug/L)	MTBE (SW8260B) (ug/L)	DIPE (ug/L)	ETBE (ug/L)	TAME (ug/L)	TBA (ug/L)	Ethanol (ug/L)	1,2-Dibromoethane (EDB) (ug/L)	1,2-Dichloroethane (ug/L)
MW-3	10/28/1996	7.42	WO	WO	WO	WO	WO	WO	WO	WO	WO	WO	WO	WO	WO	WO	WO	WO	WO	WO
	1/29/1997	7.42	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI
	4/15/1997	7.42	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI
	5/27/1997	7.42	3.45	NP	3.97	--	670	7	ND	ND	ND	250	--	--	--	--	--	--	--	--
	6/1/1997	7.42	3.50	NP	3.92	610	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	7/15/1997	8.04	3.71	NP	4.33	240	240	ND	ND	ND	ND	490	--	--	--	--	--	--	--	--
	10/9/1997	8.04	3.70	NP	4.34	500	270	1	ND	2	1	910	--	--	--	--	--	--	--	--
	1/14/1998	8.04	2.16	NP	5.88	340	310	ND	ND	1	1	140	--	--	--	--	--	--	--	--
	4/1/1998	8.04	2.20	NP	5.84	320	370	6	ND	ND	ND	93	--	--	--	--	--	--	--	--
	7/15/1998	8.04	3.38	NP	4.66	510	460	ND	ND	ND	ND	230	--	--	--	--	--	--	--	--
	10/16/1998	8.04	2.30	NP	5.74	67	330	5	ND	ND	ND	60	--	--	--	--	--	--	--	--
	1/25/1999	8.04	2.42	NP	5.62	120	420	2	ND	ND	ND	180	--	--	--	--	--	--	--	--
	4/15/1999	8.04	2.16	NP	5.88	170	290	1	ND	ND	ND	160	--	--	--	--	--	--	--	--
	7/14/1999	8.04	2.35	NP	5.69	420	290	3	ND	ND	ND	160	--	--	--	--	--	--	--	--
	10/21/1999	8.04	2.49	NP	5.55	350	360	1	ND	ND	ND	82	--	--	--	--	--	--	--	--
	1/20/2000	8.04	2.38	NP	5.66	2,060	ND	1	ND	ND	ND	54	--	--	--	--	--	--	--	--
	4/13/2000	8.04	2.76	NP	5.28	200	250	1	ND	ND	ND	91	150	ND	ND	ND	ND	ND	ND	ND
	7/14/2000	8.04	3.26	NP	4.78	423	345	ND	ND	ND	ND	95	--	--	--	--	--	--	--	--
	10/26/2000	8.04	3.12	NP	4.92	330	480	6.0	ND	ND	ND	120	--	--	--	--	--	--	--	--
	1/3/2001	8.04	3.65	NP	4.39	287	364	2	ND	ND	ND	118	--	--	--	--	--	--	--	--
	4/4/2001	8.04	3.98	NP	4.06	360	417	1	ND	ND	1	237	--	--	--	--	--	--	--	--
	7/17/2001	8.04	3.12	NP	4.92	270	480	ND	ND	ND	ND	150	--	--	--	--	--	--	--	--
	10/1/2001	8.04	3.25	NP	4.79	270	310	1.0	<0.50	<0.50	<0.50	53	--	--	--	--	--	--	--	--
	1/31/2002	8.04	2.27	NP	5.77	250	250	4	<1.0	<1.0	<1.0	110	--	--	--	--	--	--	--	--
	4/18/2002	8.04	3.55	NP	4.49	320	300	<2.0	<2.0	<2.0	<2.0	--	59	--	--	--	--	--	--	--
	7/28/2002	8.04	2.55	NP	5.49	310	500	<0.50	<0.50	<0.50	<1.0	--	130	--	--	--	--	--	--	--
	10/9/2002	8.04	2.47	NP	5.57	700	690	<5	<5	<5	<10	--	120	--	--	--	--	--	--	--
	1/2/2003	8.04	1.70	NP	6.34	210	310	<0.50	<0.50	<0.50	<1.0	--	110	<2.0	<2.0	<2.0	<100	<500	<2.0	<2.0
	4/1/2003	8.04	3.48	NP	4.56	200	250	<1.0	<1.0	<1.0	<2.0	--	210	--	--	--	--	--	--	--
	7/1/2003	8.04	2.65	NP	5.39	380	450	<2.5	<2.5	<2.5	<5.0	--	70	--	--	--	--	--	<2500	--
	10/2/2003	8.04	3.12	NP	4.92	300	<250	<2.5	<2.5	<2.5	<5.0	--	210	--	--	--	--	--	<2500	--
	1/9/2004	8.04	2.39	NP	5.65	200	300	<0.50	1	1	2	--	66	--	--	--	--	<500	--	--
	4/26/2004	8.04	3.11	NP	4.93	160	440	3	6	3	9	--	81	--	--	--	--	<50	--	--
	7/22/2004	8.04	2.51	NP	5.53	330	420	<0.5	<0.5	<0.5	<1	--	72	--	--	--	--	<1000	--	--
	10/29/2004	8.04	2.00	NP	6.04	200	460	6	15	10	46	--	48	--	--	--	--	<50	--	--
	1/10/2005	8.04	1.52	NP	6.52	250	280	<0.50	1	<0.50	2	--	64	--	--	--	--	<50	--	--
	6/15/2005	8.04	2.00	NP	6.04	360	460	<0.50	0.70	0.56	2	--	110	--	--	--	--	<50	--	--
	9/27/2005	8.04	1.90	NP	6.14	<200	210	<0.50	0.60	<0.50	<1.0	--	100	<0.50	<0.50	<0.50	79	<250	--	--
	12/13/2005	8.04	2.35	NP	5.69	230	230	<0.50	<0.50	<0.50	<1.0	--	92	--	--	--	--	<250	--	--
	3/23/2006	8.04	1.84	NP	6.20	260	290	<0.50	<0.50	<0.50	<1.0	--	88	--	--	--	--	<250	--	--
6/23/2006	8.04	2.26	NP	5.78	330	500	<0.50	<0.50	<0.50	<1.0	--	75	--	--	--	--	<250	--	--	
9/26/2006	8.04	2.08	NP	5.96	260	270	<0.50	<0.50	<0.50	<0.50	--	73	--	--	--	--	<250	--	--	
12/22/2006	8.04	1.88	NP	6.16	250	260	<0.50	<0.50	<0.50	1	--	71	--	--	--	--	<250	--	--	
3/30/2007	8.04	2.47	NP	5.57	210	390	<0.50	<0.50	<0.50	<0.50	--	120	--	--	--	--	<250	--	--	
6/28/2007	8.04	2.54	NP	5.50	290	370	<0.50	<0.50	<0.50	<0.50	--	55	--	--	--	--	<250	--	--	
9/25/2007	8.04	2.56	NP	5.48	210	350	<0.50	<0.50	<0.50	<0.50	--	61	--	--	--	--	<250	--	--	
12/28/2007	8.04	2.29	NP	5.75	150	260	<0.50	<0.50	<0.50	<1.0	--	66	--	--	--	--	<250	--	--	
3/22/2008	8.04	3.26	NP	4.78	230	390	<0.50	<0.50	<0.50	<1.0	--	39	--	--	--	--	<250	--	--	
6/23/2008	8.04	2.60	NP	5.44	130	200	<0.50	<0.50	<0.50	<1.0	--	46	--	--	--	--	<250	--	--	
9/19/2008	8.04	3.45	NP	4.59	93	180	<0.50	<0.50	<0.50	<1.0	--	120	--	--	--	--	<250	--	--	

TABLE 2a  
HISTORICAL GROUNDWATER GAUGING AND ANALYTICAL DATA  
76 STATION NO. 5191/5043  
449 HEGENBERGER ROAD  
OAKLAND, CALIFORNIA



Well I.D.	Date	GROUNDWATER GAUGING DATA				GROUNDWATER ANALYTICAL DATA															
		TOC Elevation (ft)	Depth to Water (ft)	LNAPL Thickness (ft)	Water Elevation* (ft)	TPHd (ug/L)	TPHg (ug/L)	Benzene (ug/L)	Toluene (ug/L)	Ethylbenzene (ug/L)	Total Xylenes (ug/L)	MTBE (SW8021B) (ug/L)	MTBE (SW8260B) (ug/L)	DIPE (ug/L)	ETBE (ug/L)	TAME (ug/L)	TBA (ug/L)	Ethanol (ug/L)	1,2-Dibromoethane (EDB) (ug/L)	1,2-Dichloroethane (ug/L)	
MW-3	12/31/2008	8.04	2.55	NP	5.49	110	190	<0.50	<0.50	<0.50	<1.0	--	38	--	--	--	--	<250	--	--	
	3/27/2009	8.04	2.37	NP	5.67	130	150	<0.50	<0.50	<0.50	<1.0	--	50	--	--	--	--	<250	--	--	
	5/28/2009	8.04	3.32	NP	4.72	120	190	<0.50	<0.50	<0.50	<1.0	--	60	--	--	--	--	<250	--	--	
	9/17/2009	8.04	2.63	NP	5.41	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS
	12/17/2009	8.04	2.13	NP	5.91	338	300	<0.50	<0.50	1	<1.5	--	43	--	--	--	--	<250	--	--	
	3/29/2010	8.04	2.22	NP	5.82	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	6/30/2010	10.81	2.91	NP	7.90	90	261	<0.50	<0.50	<0.50	<1.5	--	89.0	--	--	--	--	<250	--	--	
	7/6/2010	10.81	2.66	NP	8.15	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	9/20/2010	10.81	3.12	NP	7.69	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	12/8/2010	10.81	2.37	NP	8.44	137	306	<0.50	<0.50	<0.50	<1.5	--	58.8	--	--	--	--	<250	--	--	
	3/14/2011	10.81	2.26	NP	8.55	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	6/2/2011	10.81	2.43	NP	8.38	155	283	0.58	1.3	<0.50	2.2	--	42.1	--	--	--	--	55.7	<250	--	--
	9/7/2011	10.81	2.36	NP	8.45	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	12/5/2011	10.81	2.55	NP	8.26	81.7	381	<0.50	<0.50	<0.50	<1.5	--	41.8	--	--	--	--	<250	--	--	
	3/6/2012	10.81	2.63	NP	8.18	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
6/11/2012	10.81	2.99	NP	7.82	87.9	371	<0.50	<0.50	<0.50	<1.5	--	55.7	--	--	--	--	77.2	<250	--	--	
9/6/2012	10.81	2.50	NP	8.31	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	
12/13/2012	10.81	2.50	NP	8.31	<50	130	<0.50	<0.50	<0.50	<0.50	--	28	--	--	--	--	77	<5.0	--	--	
MW-4	8/31/1992	NSVD	NG	NG	NG	90	240	ND	ND	ND	0.54	--	--	--	--	--	--	--	--	--	
	11/30/1992	NSVD	NG	NG	NG	61	420	ND	ND	ND	ND	--	--	--	--	--	--	--	--	--	
	2/4/1993	NSVD	NG	NG	NG	ND	ND	ND	ND	ND	ND	--	--	--	--	--	--	--	--	--	
	5/4/1993	9.00	4.09	NP	4.91	ND	110	0.95	ND	ND	ND	--	--	--	--	--	--	--	--	--	
	8/4/1993	9.00	5.01	NP	3.99	81	250	ND	3.5	ND	4.1	--	--	--	--	--	--	--	--	--	
	11/3/1993	8.41	4.23	NP	4.18	68	130	ND	ND	ND	ND	--	--	--	--	--	--	--	--	--	
	2/7/1994	8.41	3.35	NP	5.06	ND	56	ND	ND	ND	ND	--	--	--	--	--	--	--	--	--	
	5/19/1994	8.41	3.92	NP	4.49	90	140	ND	ND	ND	ND	--	--	--	--	--	--	--	--	--	
	6/25/1994	8.41	4.35	NP	4.06	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	7/27/1994	8.41	4.28	NP	4.13	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	8/15/1994	8.41	4.27	NP	4.14	72	59	ND	0.6	ND	ND	--	--	--	--	--	--	--	--	--	--
	11/14/1994	8.41	4.05	NP	4.36	ND	130	ND	ND	ND	ND	--	--	--	--	--	--	--	--	--	--
	2/21/1995	NSVD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD
MW-5	8/31/1992	NSVD	NG	NG	NG	690	78	1	ND	ND	13	--	--	--	--	--	--	--	--	--	
	11/30/1992	NSVD	NG	NG	NG	470	930	70	290	1	14	--	--	--	--	--	--	--	--	--	
	2/4/1993	NSVD	NG	NG	NG	5,500	5,700	38	ND	620	170	--	--	--	--	--	--	--	--	--	
	5/4/1993	8.95	4.37	NP	4.58	4,600	7,400	41	ND	1,000	35	--	--	--	--	--	--	--	--	--	
	8/4/1993	8.95	5.81	NP	3.14	970	1,500	130	1	460	11	--	--	--	--	--	--	--	--	--	
	11/3/1993	8.95	5.68	NP	3.27	2,100	13,000	350	ND	3,500	530	--	--	--	--	--	--	--	--	--	
	2/7/1994	8.95	5.11	NP	3.84	830	2,000	87	ND	370	110	--	--	--	--	--	--	--	--	--	
	5/19/1994	8.95	5.09	NP	3.86	600	260	44	ND	32	4	--	--	--	--	--	--	--	--	--	
	6/25/1994	8.95	4.55	NP	4.40	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	7/27/1994	8.95	5.72	NP	3.23	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	8/15/1994	8.95	5.68	NP	3.27	860	1,600	110	ND	340	72	--	--	--	--	--	--	--	--	--	--
	11/14/1994	8.95	5.63	NP	3.32	290	250	40	ND	ND	5	--	--	--	--	--	--	--	--	--	--
	2/21/1995	NSVD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD	WD

TABLE 2a  
HISTORICAL GROUNDWATER GAUGING AND ANALYTICAL DATA  
76 STATION NO. 5191/5043  
449 HEGENBERGER ROAD  
OAKLAND, CALIFORNIA



Well I.D.	Date	GROUNDWATER GAUGING DATA				GROUNDWATER ANALYTICAL DATA															
		TOC Elevation (ft)	Depth to Water (ft)	LNAPL Thickness (ft)	Water Elevation* (ft)	TPHd (ug/L)	TPHg (ug/L)	Benzene (ug/L)	Toluene (ug/L)	Ethylbenzene (ug/L)	Total Xylenes (ug/L)	MTBE (SW8021B) (ug/L)	MTBE (SW8260B) (ug/L)	DIPE (ug/L)	ETBE (ug/L)	TAME (ug/L)	TBA (ug/L)	Ethanol (ug/L)	1,2-Dibromoethane (EDB) (ug/L)	1,2-Dichloroethane (ug/L)	
MW-6	8/31/1992	NSVD	NG	NG	NG	750	ND	ND	ND	ND	ND	--	--	--	--	--	--	--	--	--	
	11/30/1992	NSVD	NG	NG	NG	1,400	9,200	550	ND	740	1,600	--	--	--	--	--	--	--	--	--	
	2/4/1993	NSVD	NG	NG	NG	890	3,600	340	ND	290	550	--	--	--	--	--	--	--	--	--	
	5/4/1993	9.12	3.72	NP	5.40	1,800	4,900	360	18	450	430	--	--	--	--	--	--	--	--	--	
	8/4/1993	9.12	5.15	NP	3.97	1,100	3,400	390	ND	440	190	--	--	--	--	--	--	--	--	--	
	11/3/1993	8.87	5.25	NP	3.62	390	1,400	320	ND	200	8	--	--	--	--	--	--	--	--	--	
	2/7/1994	8.87	4.55	NP	4.32	970	4,900	650	ND	250	35	--	--	--	--	--	--	--	--	--	
	5/19/1994	8.87	4.62	NP	4.25	1,400	3,600	300	2	210	41	--	--	--	--	--	--	--	--	--	
	8/15/1994	8.87	5.08	NP	3.79	790	1,300	130	7	54	57	--	--	--	--	--	--	--	--	--	
	11/14/1994	8.87	5.30	NP	3.57	800	730	50	ND	ND	39	--	--	--	--	--	--	--	--	--	
	2/21/1995	8.87	5.37	NP	3.50	730	2,000	250	5	25	30	--	--	--	--	--	--	--	--	--	
	5/18/1995	8.87	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI
	8/17/1995	8.87	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI	WI
	7/26/1996	8.87	6.40	3.33	4.97	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	10/28/1996	8.87	4.10	0.21	4.93	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	11/13/1996	8.87	4.02	0.25	5.04	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	11/25/1996	8.87	4.01	0.75	5.42	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	12/4/1996	8.87	3.65	0.50	5.60	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	12/19/1996	8.87	4.80	2.20	5.72	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	1/8/1997	8.87	4.84	1.75	5.34	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	1/14/1997	8.87	4.51	1.15	5.22	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	1/27/1997	8.87	4.00	1.75	6.18	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	1/29/1997	8.87	3.24	0.31	5.86	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	2/11/1997	8.87	4.65	1.20	5.12	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	2/24/1997	8.87	4.81	1.10	4.89	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	3/10/1997	8.87	4.60	0.95	4.98	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	3/17/1997	8.87	4.50	0.89	5.04	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	3/31/1997	8.87	4.65	1.00	4.97	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	4/15/1997	8.87	4.90	1.03	4.74	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	4/28/1997	8.87	4.78	0.03	4.11	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	5/15/1997	8.87	4.60	0.25	4.46	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	5/27/1997	8.87	4.50	0.25	4.56	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	6/9/1997	8.87	4.60	0.20	4.42	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	6/24/1997	8.87	4.50	0.25	4.56	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	7/9/1997	8.87	4.80	0.60	4.52	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	7/15/1997	8.87	4.63	0.42	4.56	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	7/21/1997	8.87	4.75	0.25	4.31	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	8/6/1997	8.87	4.50	0.10	4.45	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	8/20/1997	8.87	4.55	0.10	4.40	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	9/2/1997	8.87	4.75	0.05	4.16	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
10/9/1997	8.87	4.84	0.04	4.06	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	
1/14/1998	8.87	3.90	0.94	5.68	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	
2/12/1998	8.87	3.35	0.64	6.00	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	
3/3/1998	8.87	4.51	0.02	4.38	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	
4/1/1998	8.87	3.67	1.60	6.40	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	
5/26/1998	8.87	4.11	0.50	5.14	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	
6/15/1998	8.87	5.03	0.30	4.07	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	
7/15/1998	8.87	4.56	0.05	4.35	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	
8/21/1998	8.87	4.77	0.02	4.12	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	
9/30/1998	8.87	5.08	0.03	3.81	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	
10/16/1998	8.87	4.31	2.40	6.36	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	
11/6/1998	8.87	3.98	0.17	5.02	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	



TABLE 2a  
HISTORICAL GROUNDWATER GAUGING AND ANALYTICAL DATA  
76 STATION NO. 5191/5043  
449 HEGENBERGER ROAD  
OAKLAND, CALIFORNIA



Well I.D.	Date	GROUNDWATER GAUGING DATA				GROUNDWATER ANALYTICAL DATA															
		TOC Elevation (ft)	Depth to Water (ft)	LNAPL Thickness (ft)	Water Elevation* (ft)	TPHd (ug/L)	TPHg (ug/L)	Benzene (ug/L)	Toluene (ug/L)	Ethylbenzene (ug/L)	Total Xylenes (ug/L)	MTBE (SW8021B) (ug/L)	MTBE (SW8260B) (ug/L)	DIPE (ug/L)	ETBE (ug/L)	TAME (ug/L)	TBA (ug/L)	Ethanol (ug/L)	1,2-Dibromoethane (EDB) (ug/L)	1,2-Dichloroethane (ug/L)	
MW-6	11/25/1998	8.87	3.92	0.10	5.03	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	12/28/1998	8.87	3.90	0.20	5.12	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	1/25/1999	8.87	4.18	0.60	5.14	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	2/22/1999	8.87	4.07	0.22	4.97	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	3/22/1999	8.87	4.32	0.15	4.66	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	4/15/1999	8.87	4.23	0.95	5.35	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	5/28/1999	8.87	4.38	0.39	4.78	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	6/29/1999	8.87	4.12	0.02	4.77	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	7/14/1999	8.87	4.20	0.03	4.69	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	8/23/1999	8.87	4.51	0.24	4.54	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	9/30/1999	8.87	4.17	0.17	4.83	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	10/21/1999	8.87	4.27	0.12	4.69	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	11/29/1999	8.87	4.18	NP	4.69	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	12/20/1999	8.87	4.26	0.01	4.62	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH	LPH
	1/20/2000	8.87	4.31	NP	4.56	67,600	130,000	2,900	8,600	2,000	16,000	ND	--	--	--	--	--	--	--	--	--
	2/26/2000	8.87	3.98	NP	4.89	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	3/31/2000	8.87	4.14	NP	4.73	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	4/13/2000	8.87	4.04	NP	4.83	8,700	140,000	5,000	14,000	3,600	27,000	7,700	--	--	--	--	--	--	--	--	--
	5/26/2000	8.87	4.41	NP	4.46	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	6/17/2000	8.87	4.35	NP	4.52	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	7/14/2000	8.87	4.47	NP	4.40	133,000	259,000	7,670	13,700	6,860	40,700	ND	ND	--	--	--	--	--	--	--	--
	8/24/2000	8.87	3.71	NP	5.16	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	9/27/2000	8.87	4.33	NP	4.54	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	10/26/2000	8.87	4.32	NP	4.55	61,000	110,000	7,000	6,200	3,700	12,000	670	43	--	--	--	--	--	--	--	--
	1/3/2001	8.87	4.52	NP	4.35	929	84,700	3,950	4,130	3,650	11,800	ND	ND	--	--	--	--	--	--	--	--
	4/4/2001	8.87	4.29	NP	4.58	18,000	69,800	2,060	2,840	3,650	10,900	ND	48	ND	ND	ND	ND	ND	ND	ND	ND
	7/17/2001	8.87	4.37	NP	4.50	20,000	100,000	3,200	3,300	3,400	12,000	ND	--	--	--	--	--	--	--	--	--
	10/1/2001	8.87	4.45	NP	4.42	24,000	110,000	3,200	2,400	4,500	13,000	<1000	--	--	--	--	--	--	--	--	--
	1/31/2002	8.87	4.03	NP	4.84	11,000	230,000	2,400	1,800	5,400	16,000	<2500	--	--	--	--	--	--	--	--	--
	4/18/2002	8.87	3.45	NP	5.42	3,500	94,000	6,800	13,000	3,000	19,000	<500	--	--	--	--	--	--	--	--	--
	7/28/2002	8.87	2.24	NP	6.63	27,000	110,000	530	170	3,200	7,300	--	<100	--	--	--	--	--	--	--	--
	10/9/2002	8.87	3.53	NP	5.34	170,000	970,000	10,000	39,000	13,000	94,000	--	<2000	--	--	--	--	--	--	--	--
	1/2/2003	8.87	2.34	NP	6.53	66,000	270,000	6,100	15,000	5,400	37,000	--	<200	--	--	--	--	--	--	--	--
	4/1/2003	8.87	3.17	NP	5.70	35,000	3,000,000	8,000	39,000	37,000	260,000	--	<2000	--	--	--	--	--	--	--	--
	7/1/2003	8.87	3.55	NP	5.32	11,000	38,000	2,100	990	2,700	6,500	--	<100	--	--	--	--	--	<25000	--	--
	10/2/2003	8.87	3.82	NP	5.05	<50	100,000	5,600	6,900	4,700	18,000	--	<800	--	--	--	--	--	<200000	--	--
1/9/2004	8.87	2.80	NP	6.07	20,000	170,000	2,800	3,300	4,700	16,000	--	<200	--	--	--	--	--	<50000	--	--	
4/26/2004	8.87	3.40	NP	5.47	13,000	97,000	5,900	9,000	5,100	23,000	--	<50	--	--	--	--	--	<5000	--	--	
7/22/2004	8.87	3.54	NP	5.33	33,000	110,000	4,100	5,100	4,000	16,000	--	<200	--	--	--	--	--	<300000	--	--	
10/29/2004	8.87	3.03	NP	5.84	78,000	100,000	5,200	6,100	4,200	15,000	--	<50	--	--	--	--	--	<5000	--	--	
1/10/2005	8.87	2.35	NP	6.52	12,000	71,000	1,600	3,700	2,100	9,900	--	<50	--	--	--	--	--	<5000	--	--	
6/15/2005	8.87	2.47	NP	6.40	16,000	130,000	800	1,800	2,200	9,300	--	<50	--	--	--	--	--	<5000	--	--	
9/27/2005	8.87	2.55	NP	6.32	2,500	13,000	82	120	430	990	--	1	2	<0.50	<0.50	<10	<250	--	--	--	
12/13/2005	8.87	3.28	NP	5.59	18,000	68,000	1,500	1,100	2,200	7,700	--	<50	--	--	--	--	--	<25000	--	--	





TABLE 2a  
HISTORICAL GROUNDWATER GAUGING AND ANALYTICAL DATA  
76 STATION NO. 5191/5043  
449 HEGENBERGER ROAD  
OAKLAND, CALIFORNIA



Well I.D.	Date	GROUNDWATER GAUGING DATA				GROUNDWATER ANALYTICAL DATA														
		TOC Elevation (ft)	Depth to Water (ft)	LNAPL Thickness (ft)	Water Elevation* (ft)	TPHd (ug/L)	TPHg (ug/L)	Benzene (ug/L)	Toluene (ug/L)	Ethylbenzene (ug/L)	Total Xylenes (ug/L)	MTBE (SW8021B) (ug/L)	MTBE (SW8260B) (ug/L)	DIPE (ug/L)	ETBE (ug/L)	TAME (ug/L)	TBA (ug/L)	Ethanol (ug/L)	1,2-Dibromoethane (EDB) (ug/L)	1,2-Dichloroethane (ug/L)
MW-8	10/29/2004	8.52	3.06	NP	5.46	120	<50	<0.50	<0.50	0.82	2.5	--	<0.50	--	--	--	--	<50	--	--
	1/10/2005	8.52	1.92	NP	6.60	140	58	<0.50	0.61	1.2	4.0	--	<0.50	--	--	--	--	<50	--	--
	6/15/2005	8.52	2.22	NP	6.30	140	<50	<0.50	<0.50	<0.50	<1.0	--	<0.50	--	--	--	--	<50	--	--
	9/27/2005	8.52	2.43	NP	6.09	<200	<50	<0.50	<0.50	1.2	<1.0	--	<0.50	<0.50	<0.50	<0.50	<10	<250	--	--
	12/13/2005	8.52	2.89	NP	5.63	<200	<50	<0.50	<0.50	<0.50	<1.0	--	<0.50	--	--	--	--	<250	--	--
	3/23/2006	8.52	2.12	NP	6.40	<200	<50	<0.50	<0.50	<0.50	<1.0	--	<0.50	--	--	--	--	<250	--	--
	6/23/2006	8.52	2.65	NP	5.87	<230	<50	<0.50	<0.50	<0.50	<1.0	--	<0.50	--	--	--	--	<250	--	--
	9/26/2006	8.52	2.75	NP	5.77	110	<50	<0.50	<0.50	<0.50	<0.50	--	<0.50	--	--	--	--	<250	--	--
	12/22/2006	8.52	2.58	NP	5.94	100	<50	<0.50	<0.50	<0.50	<0.50	--	<0.50	--	--	--	--	<250	--	--
	3/30/2007	8.52	2.74	NP	5.78	120	<50	<0.50	<0.50	<0.50	<0.50	--	<0.50	--	--	--	--	<250	--	--
	6/28/2007	8.52	2.90	NP	5.62	140	<50	<0.50	<0.50	<0.50	<0.50	--	<0.50	--	--	--	--	<250	--	--
	9/25/2007	8.52	3.26	NP	5.26	110	<50	<0.50	<0.50	<0.50	<0.50	--	<0.50	--	--	--	--	<250	--	--
	12/28/2007	8.52	2.64	NP	5.88	110	<50	<0.50	<0.50	<0.50	<1.0	--	<0.50	--	--	--	--	<250	--	--
	3/22/2008	8.52	2.31	NP	6.21	<50	<50	<0.50	<0.50	<0.50	<1.0	--	<0.50	--	--	--	--	<250	--	--
	6/23/2008	8.52	3.13	NP	5.39	<58	<50	<0.50	<0.50	<0.50	<1.0	--	<0.50	--	--	--	--	<250	--	--
	9/19/2008	8.52	3.72	NP	4.80	79	<50	<0.50	<0.50	<0.50	<1.0	--	<0.50	--	--	--	--	<250	--	--
	12/31/2008	8.52	2.98	NP	5.54	110	<50	<0.50	<0.50	<0.50	<1.0	--	<0.50	--	--	--	--	<250	--	--
	3/27/2009	8.52	2.49	NP	6.03	89	<50	<0.50	<0.50	<0.50	<1.0	--	<0.50	--	--	--	--	<250	--	--
	5/28/2009	8.52	3.12	NP	5.40	91	<50	<0.50	<0.50	<0.50	<1.0	--	<0.50	--	--	--	--	<250	--	--
	9/17/2009	8.52	3.63	NP	4.89	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS
	3/29/2010	8.52	WI	WI	WI	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	6/30/2010	11.32	2.60	NP	8.72	182	<50.0	<0.50	<0.50	<0.50	<1.5	--	<0.50	--	--	--	--	<250	--	--
	7/6/2010	11.32	3.03	NP	8.29	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	9/20/2010	11.32	3.33	NP	7.99	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	12/8/2010	11.32	2.82	NP	8.50	116	<50.0	<0.50	<0.50	<0.50	<1.5	--	<0.50	--	--	--	--	<250	--	--
	3/14/2011	11.32	3.84	NP	7.48	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
6/2/2011	11.32	2.77	NP	8.55	--	<50.0	<0.50	<0.50	<0.50	<1.5	--	<0.50	--	--	--	<5.0	<250	--	--	
9/7/2011	11.32	2.84	NP	8.48	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	
12/5/2011	11.32	2.68	NP	8.64	<50.0	<50.0	<0.50	<0.50	<0.50	<1.5	--	<0.50	--	--	--	--	<250	--	--	
3/6/2012	11.32	3.07	NP	8.25	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	
6/11/2012	11.32	3.08	NP	8.24	<37.9	<50.0	<0.50	<0.50	<0.50	<1.5	--	<0.50	--	--	--	8.3	<250	--	--	
9/6/2012	11.32	2.91	NP	8.41	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	
12/13/2012	11.32	2.31	NP	9.01	<50	<50	<0.50	<0.50	<0.50	<0.50	--	<0.50	--	--	--	<5.0	<5.0	--	--	
MW-9	2/21/1995	8.29	1.98	NP	6.31	71	70	ND	ND	ND	ND	--	--	--	--	--	--	--	--	
	5/18/1995	8.29	3.47	NP	4.82	ND	52	ND	1.1	ND	1.9	--	--	--	--	--	--	--	--	
	8/17/1995	8.29	1.49	NP	6.80	ND	ND	ND	ND	ND	ND	--	--	--	--	--	--	--	--	
	7/26/1996	8.29	0.28	NP	8.01	98	ND	ND	ND	ND	ND	ND	--	--	--	--	--	--	--	
	10/28/1996	8.29	1.15	NP	7.14	99	ND	ND	ND	ND	ND	7.6	--	--	--	--	--	--	--	
	1/29/1997	8.29	1.05	NP	7.24	54	ND	ND	ND	ND	ND	5.4	--	--	--	--	--	--	--	
	4/15/1997	8.29	1.88	NP	6.41	94	ND	ND	ND	ND	ND	5.4	--	--	--	--	--	--	--	
	5/27/1997	8.29	1.05	NP	7.24	--	--	--	--	--	--	--	--	--	--	--	--	--	--	
	7/15/1997	8.29	1.90	NP	6.39	ND	ND	ND	ND	ND	ND	ND	--	--	--	--	--	--	--	
	10/9/1997	8.29	1.76	NP	6.53	160	ND	ND	ND	ND	ND	ND	--	--	--	--	--	--	--	
	1/14/1998	8.29	1.26	NP	7.03	110	ND	ND	ND	ND	ND	3.0	--	--	--	--	--	--	--	
	4/1/1998	8.29	0.85	NP	7.44	110	ND	ND	ND	ND	ND	ND	--	--	--	--	--	--	--	
	7/15/1998	8.29	1.52	NP	6.77	200	ND	ND	ND	ND	ND	ND	--	--	--	--	--	--	--	
	10/16/1998	8.29	0.81	NP	7.48	ND	ND	ND	ND	ND	ND	ND	--	--	--	--	--	--	--	
	1/25/1999	8.29	0.92	NP	7.37	ND	ND	ND	ND	ND	ND	ND	--	--	--	--	--	--	--	
	4/15/1999	8.29	0.90	NP	7.39	ND	75	21	ND	ND	1.1	680	--	--	--	--	--	--	--	
	7/14/1999	8.29	1.04	NP	7.25	140	ND	1.9	ND	ND	ND	260	--	--	--	--	--	--	--	
	10/21/1999	8.29	1.23	NP	7.06	210	ND	ND	ND	ND	ND	170	--	--	--	--	--	--	--	
	1/20/2000	8.29	1.18	NP	7.11	519	ND	1.1	ND	ND	ND	35	--	--	--	--	--	--	--	
	4/13/2000	8.29	1.08	NP	7.21	81	160	0.64	ND	ND	ND	53	--	--	--	--	--	--	--	
	7/14/2000	8.29	1.43	NP	6.86	107	ND	ND	ND	ND	ND	20.2	--	--	--	--	--	--	--	
	10/26/2000	8.29	1.38	NP	6.91	240	240	2.9	ND	ND	ND	56	--	--	--	--	--	--	--	
	1/3/2001	8.29	1.66	NP	6.63	164	166	0.763	0.776	ND	1.28	50.2	--	--	--	--	--	--	--	
	4/4/2001	8.29	1.27	NP	7.02	240	296	0.738	ND	ND	0.907	135	--	--	--	--	--	--	--	
	7/17/2001	8.29	1.38	NP	6.91	ND	ND	ND	ND	ND	ND	13	--	--	--	--	--	--	--	
	10/1/2001	8.29	1.93	NP	6.36	<52	51	<0.50	<0.50	<0.50	<0.50	5.0	--	--	--	--	--	--	--	
1/31/2002	8.29	2.08	NP	6.21	200	<50	<0.50	<0.50	<0.50	<0.50	5.8	--	--	--	--	--	--	--		



TABLE 2a  
HISTORICAL GROUNDWATER GAUGING AND ANALYTICAL DATA  
76 STATION NO. 5191/5043  
449 HEGENBERGER ROAD  
OAKLAND, CALIFORNIA



Well I.D.	Date	GROUNDWATER GAUGING DATA				GROUNDWATER ANALYTICAL DATA														
		TOC Elevation (ft)	Depth to Water (ft)	LNAPL Thickness (ft)	Water Elevation* (ft)	TPHd (ug/L)	TPHg (ug/L)	Benzene (ug/L)	Toluene (ug/L)	Ethylbenzene (ug/L)	Total Xylenes (ug/L)	MTBE (SW8021B) (ug/L)	MTBE (SW8260B) (ug/L)	DIPE (ug/L)	ETBE (ug/L)	TAME (ug/L)	TBA (ug/L)	Ethanol (ug/L)	1,2-Dibromoethane (EDB) (ug/L)	1,2-Dichloroethane (ug/L)
MW-10	7/14/1999	8.62	3.89	NP	4.73	180	280	55	3.2	11	31	6.1	--	--	--	--	--	--	--	--
	10/21/1999	8.62	4.09	NP	4.53	96	140	22	0.59	1.7	7.7	5.3	--	--	--	--	--	--	--	--
	1/20/2000	8.62	3.92	NP	4.70	252	ND	0.73	0.86	ND	ND	5.2	--	--	--	--	--	--	--	--
	4/13/2000	8.62	3.85	NP	4.77	69	67	54	ND	2.6	ND	3.8	--	--	--	--	--	--	--	--
	7/14/2000	8.62	4.18	NP	4.44	149	ND	0.547	ND	ND	ND	ND	--	--	--	--	--	--	--	--
	10/26/2000	8.62	3.96	NP	4.66	83	ND	3.3	ND	0.83	1.5	ND	--	--	--	--	--	--	--	--
	1/3/2001	8.62	4.14	NP	4.48	126	52.7	5.15	ND	0.823	1.57	ND	--	--	--	--	--	--	--	--
	4/4/2001	8.62	3.88	NP	4.74	75	129	28.1	1.67	4.97	10.1	ND	--	--	--	--	--	--	--	--
	7/17/2001	8.62	4.08	NP	4.54	ND	ND	4.1	ND	1.0	1.8	ND	--	--	--	--	--	--	--	--
	10/1/2001	8.62	4.22	NP	4.40	100	140	30	0.51	4.0	12	<5.0	--	--	--	--	--	--	--	--
	1/31/2002	8.62	3.68	NP	4.94	170	110	16	<0.50	2.3	5.6	<2.5	--	--	--	--	--	--	--	--
	4/18/2002	8.62	4.01	NP	4.61	130	<50	11	<0.50	1.4	4.5	<2.5	--	--	--	--	--	--	--	--
	7/28/2002	8.62	4.11	NP	4.51	58	67	15	<0.50	0.94	7.3	--	<2.0	--	--	--	--	--	--	--
	10/9/2002	8.62	3.97	NP	4.65	<94	<50	0.67	<0.50	<0.50	<1.0	--	<2.0	--	--	--	--	--	--	--
	1/2/2003	8.62	3.03	NP	5.59	64	<50	<0.50	<0.50	<0.50	<1.0	--	<2.0	--	--	--	--	--	--	--
	4/1/2003	8.62	3.83	NP	4.79	76	<50	11	<0.50	<0.50	<1.0	--	<2.0	--	--	--	--	--	--	--
	7/1/2003	8.62	4.13	NP	4.49	87	<50	<0.50	<0.50	<0.50	<1.0	--	<2.0	--	--	--	--	<500	--	--
	10/2/2003	8.62	4.05	NP	4.57	160	77	9.9	0.78	2.3	4.9	--	<2.0	--	--	--	--	<500	--	--
	1/9/2004	8.62	3.40	NP	5.22	74	53	1.2	<0.50	0.70	1.6	--	<2.0	--	--	--	--	<500	--	--
	4/26/2004	8.62	3.89	NP	4.73	<50	<50	2.8	1.3	1.0	2.9	--	<0.50	--	--	--	--	<50	--	--
	7/22/2004	8.62	3.73	NP	4.89	<200	<50	<0.5	<0.5	<0.5	<1	--	<0.5	--	--	--	--	<1000	--	--
	10/29/2004	8.62	3.41	NP	5.21	<50	100	2.0	1.2	1.1	3.6	--	<0.50	--	--	--	--	<50	--	--
	1/10/2005	8.62	2.68	NP	5.94	94	84	7.8	2.7	2.2	8.9	--	<0.50	--	--	--	--	<50	--	--
	6/15/2005	8.62	4.63	NP	3.99	62	<50	<0.50	<0.50	<0.50	<1.0	--	<0.50	--	--	--	--	<50	--	--
	9/27/2005	8.62	3.96	NP	4.66	<200	<50	<0.50	<0.50	<0.50	<1.0	--	<0.50	<0.50	<0.50	<0.50	<10	<250	--	--
	12/13/2005	8.62	3.75	NP	4.87	<200	<50	<0.50	<0.50	<0.50	<1.0	--	<0.50	--	--	--	--	<250	--	--
	3/23/2006	8.62	3.13	NP	5.49	<200	50	13	<0.50	<0.50	<1.0	--	<0.50	--	--	--	--	<250	--	--
	6/23/2006	8.62	3.90	NP	4.72	<200	<50	<0.50	<0.50	<0.50	<1.0	--	<0.50	--	--	--	--	<250	--	--
	9/26/2006	8.62	3.66	NP	4.96	<50	<50	<0.50	<0.50	<0.50	<0.50	--	<0.50	--	--	--	--	<250	--	--
	12/22/2006	8.62	3.56	NP	5.06	81	<50	<0.50	<0.50	<0.50	1.8	--	<0.50	--	--	--	--	<250	--	--
	3/30/2007	8.62	3.93	NP	4.69	82	<50	<0.50	<0.50	<0.50	<0.50	--	<0.50	--	--	--	--	<250	--	--
	6/28/2007	8.62	4.03	NP	4.59	57	<50	<0.50	<0.50	<0.50	<0.50	--	<0.50	--	--	--	--	<250	--	--
	9/25/2007	8.62	3.91	NP	4.71	82	<50	<0.50	<0.50	<0.50	<0.50	--	<0.50	--	--	--	--	<250	--	--
	12/28/2007	8.62	3.64	NP	4.98	62	<50	2.1	<0.50	<0.50	<1.0	--	<0.50	--	--	--	--	<250	--	--
	3/22/2008	8.62	4.00	NP	4.62	<50	64	13	<0.50	<0.50	<1.0	--	<0.50	--	--	--	--	<250	--	--
	6/23/2008	8.62	3.90	NP	4.72	<50	94	30	0.53	3.4	3.5	--	<0.50	--	--	--	--	<250	--	--
	9/19/2008	8.62	3.85	NP	4.77	<50	130	15	1.7	5.7	11	--	<0.50	--	--	--	--	<250	--	--
	12/31/2008	8.62	3.69	NP	4.93	<50	82	11	<0.50	0.81	1.7	--	<0.50	--	--	--	--	<250	--	--
	3/27/2009	8.62	3.75	NP	4.87	730	210	28	1.4	1.2	3.9	--	<0.50	--	--	--	--	<250	--	--
	5/28/2009	8.62	3.66	NP	4.96	<50	<50	0.91	<0.50	<0.50	<1.0	--	<0.50	--	--	--	--	<250	--	--
9/17/2009	8.62	3.85	NP	4.77	65	<50	<0.50	<0.50	<0.50	<1.0	--	<0.50	--	--	--	--	<250	--	--	
12/17/2009	8.62	3.00	NP	5.62	57.7	<50.0	1.2	<0.50	<0.50	<1.5	--	<0.50	--	--	--	--	<250	--	--	
3/29/2010	8.62	3.81	NP	4.81	82.2	<50.0	0.77	<0.50	<0.50	3.4	--	<0.50	--	--	--	--	<250	--	--	
6/30/2010	10.97	3.90	NP	7.07	53.4	<50.0	<0.50	<0.50	<0.50	<1.5	--	<0.50	--	--	--	--	<250	--	--	
7/6/2010	10.97	3.73	NP	7.24	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	
9/20/2010	10.97	3.85	NP	7.12	<50.0	<50.0	<0.50	<0.50	<0.50	<1.5	--	<0.50	--	--	--	--	<250	--	--	
12/8/2010	10.97	3.63	NP	7.34	<50.0	<50.0	1.8	<0.50	<0.50	<1.5	--	<0.50	--	--	--	--	<250	--	--	
3/14/2011	10.97	3.46	NP	7.51	63.3	<50.0	1.1	<0.50	<0.50	<1.5	--	<0.50	--	--	--	<5.0	<250	--	--	
6/2/2011	10.97	3.92	NP	7.05	<50.0	58.7	4.8	4.2	0.96	5.1	--	<0.50	--	--	--	<5.0	<250	--	--	
9/7/2011	10.97	4.06	NP	6.91	<50.0	<50.0	4.1	<0.50	0.66	2.4	--	<0.50	--	--	--	--	<250	--	--	
12/5/2011	10.97	3.82	NP	7.15	<50.0	<50.0	<0.50	<0.50	<0.50	<1.5	--	<0.50	--	--	--	--	<250	--	--	
3/6/2012	10.97	3.74	NP	7.23	<50.0	<50.0	<0.50	<0.50	<0.50	<1.5	--	<0.50	--	--	--	58.7	<250	--	--	
6/11/2012	10.97	3.99	NP	6.98	<37.9	<50.0	0.79	<0.50	<0.50	<1.5	--	0.72	--	--	--	17.2	<250	--	--	
9/6/2012	10.97	4.00	NP	6.97	110	64	6.9	0.89	1.8	3.9	--	<0.50	<0.50	<0.50	<5.0	<5.0	<5.0	<0.50	<0.50	
9/11/2012	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	
12/13/2012	10.97	3.40	NP	7.57	<50	120	15	1.1	1.7	5.2	--	<0.50	--	--	--	<5.0	<5.0	--	--	



TABLE 2a  
HISTORICAL GROUNDWATER GAUGING AND ANALYTICAL DATA  
76 STATION NO. 5191/5043  
449 HEGENBERGER ROAD  
OAKLAND, CALIFORNIA



Well I.D.	Date	GROUNDWATER GAUGING DATA				GROUNDWATER ANALYTICAL DATA														
		TOC Elevation (ft)	Depth to Water (ft)	LNAPL Thickness (ft)	Water Elevation* (ft)	TPHd (ug/L)	TPHg (ug/L)	Benzene (ug/L)	Toluene (ug/L)	Ethylbenzene (ug/L)	Total Xylenes (ug/L)	MTBE (SW8021B) (ug/L)	MTBE (SW8260B) (ug/L)	DIPE (ug/L)	ETBE (ug/L)	TAME (ug/L)	TBA (ug/L)	Ethanol (ug/L)	1,2-Dibromoethane (EDB) (ug/L)	1,2-Dichloroethane (ug/L)
MW-11	7/6/2010	10.53	2.44	NP	8.09	226	99.2	<0.50	<0.50	<0.50	<1.5	--	165	<0.50	<0.50	<0.50	174	<250	<1.0	<1.0
	9/20/2010	10.53	2.80	NP	7.73	<50.0	76.4 1n	<0.50	<0.50	<0.50	<1.5	--	82.7	--	--	--	--	<250	--	--
	12/8/2010	10.53	1.90	NP	8.63	52.7	<50.0	<0.50	<0.50	<0.50	<1.5	--	59.1	--	--	--	--	<250	--	--
	3/14/2011	10.53	1.89	NP	8.64	67.8	<50.0	<0.50	<0.50	<0.50	<1.5	--	44.0	--	--	--	<5.0	<250	--	--
	6/2/2011	10.53	1.75	NP	8.78	69.0 T4	<50.0	<0.50	0.61	<0.50	<1.5	--	24.9	--	--	--	7.1	<250	--	--
	9/7/2011	10.53	1.56	NP	8.97	<50.0	<50.0	<0.50	<0.50	<0.50	<1.5	--	3.8	--	--	--	--	<250	--	--
	12/5/2011	10.53	2.05	NP	8.48	<50.0	<50.0	<0.50	<0.50	<0.50	<1.5	--	26.4	--	--	--	--	<250	--	--
	3/6/2012	10.53	2.31	NP	8.22	<50.0	<50.0	<0.50	<0.50	<0.50	<1.5	--	35.3	--	--	--	5.7	<250	--	--
	6/11/2012	10.53	2.24	NP	8.29	<37.9	<50.0	<0.50	<0.50	<0.50	<1.5	--	20.9	--	--	--	10.4	<250	--	--
	9/6/2012	10.53	1.70	NP	8.83	64	<50	<0.50	<0.50	<0.50	<0.50	--	7.7	<0.50	<0.50	<0.50	<5.0	<5.0	<0.50	<0.50
	12/13/2012	10.53	1.56	NP	8.97	<50	<50	<0.50	<0.50	<0.50	<0.50	--	27	--	--	--	<5.0	<5.0	--	--
	MW-12	7/6/2010	11.01	4.00	NP	7.01	990	20,300	1,030	955	311	2,450	--	1,650	<0.50	<0.50	1.0	1,430	<250	<1.0
9/20/2010		11.01	4.18	NP	6.83	5,220	73,700	6,020	6,390	2,970	18,300	--	894	--	--	--	--	<250	--	--
12/8/2010		11.01	3.92	NP	7.09	428	3,350	249	117	90	558	--	1,470	--	--	--	--	<2500	--	--
3/14/2011		11.01	3.70	NP	7.31	283	2,420	287	81	49	243	--	1,020	--	--	--	70	<250	--	--
6/2/2011		11.01	4.40	NP	6.61	1,330 T4	12,200	688	71	225	619	--	824	--	--	--	110	<250	--	--
9/7/2011		11.01	4.37	NP	6.64	1,270 T4	7,900	920	25	187	267	--	896	--	--	--	--	<2500	--	--
12/5/2011		11.01	4.32	NP	6.69	286 T4	2,240	296	38	38.0	122	--	1,040	--	--	--	--	<250	--	--
3/6/2012		11.01	4.01	NP	7.00	272 T4	1,260	193	23	29	81	--	835	--	--	--	78	<250	--	--
6/11/2012		11.01	4.20	NP	6.81	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
6/12/2012		--	--	--	--	957 T4	1,030	178	17.0	24	69	--	993	--	--	--	448	<250	--	--
9/6/2012		11.01	4.15	NP	6.86	<200	580	120	10	15	37	--	840	<1.5	<1.5	<1.5	15	<15	<1.5	14
12/13/2012		11.01	3.35	NP	7.66	<50	480	70	5	7	19	--	820	--	--	--	19	<15	--	--
MW-12A	7/6/2010	11.29	4.22	NP	7.07	89	664	18	1	2	50	--	14	<0.50	<0.50	<0.50	12	<250	<1.0	<1.0
	9/20/2010	11.29	4.39	NP	6.90	<50.0	<50.0	<0.50	<0.50	<0.50	<1.5	--	9	--	--	--	--	<250	--	--
	12/8/2010	11.29	4.00	NP	7.29	76	<50.0	<0.50	<0.50	<0.50	<1.5	--	9	--	--	--	--	<250	--	--
	3/14/2011	11.29	3.81	NP	7.48	62	<50.0	<0.50	<0.50	<0.50	<1.5	--	<0.50	--	--	--	<5.0	<250	--	--
	6/2/2011	11.29	4.20	NP	7.09	<50.0	<50.0	<0.50	<0.50	<0.50	<1.5	--	<0.50	--	--	--	<5.0	<250	--	--
	9/7/2011	11.29	4.42	NP	6.87	<50.0	<50.0	<0.50	<0.50	<0.50	<1.5	--	1	--	--	--	--	<250	--	--
	12/5/2011	11.29	4.30	NP	6.99	<50.0	<50.0	<0.50	<0.50	<0.50	<1.5	--	<0.50	--	--	--	--	<250	--	--
	3/6/2012	11.29	4.32	NP	6.97	52.0 T4	<50.0	<0.50	<0.50	<0.50	<1.5	--	<0.50	--	--	--	<5.0	<250	--	--
	6/11/2012	11.29	4.36	NP	6.93	<37.9	<50.0	<0.50	<0.50	<0.50	<1.5	--	<0.50	--	--	--	<5.0	<250	--	--
	9/6/2012	11.29	4.45	NP	6.84	300	<50	<0.50	<0.50	<0.50	<0.50	--	<0.50	<0.50	<0.50	<0.50	<5.0	<5.0	<0.50	<0.50
	12/13/2012	11.29	3.80	NP	7.49	62	<50	<0.50	<0.50	<0.50	<0.50	--	<0.50	--	--	--	<5.0	<5.0	--	--
	MW-13	7/6/2010	11.08	4.26	NP	7	469	122	<0.50	<0.50	<0.50	<1.5	--	217	<0.50	<0.50	<0.50	199	<250	<1.0
9/20/2010		11.08	4.81	NP	6	<50.0	250 1n	<0.50	<0.50	<0.50	<1.5	--	272	--	--	--	--	<250	--	--
12/8/2010		11.08	5.02	NP	6	97.0	177 1n	<0.50	<0.50	<0.50	<1.5	--	390	--	--	--	--	<250	--	--
3/14/2011		11.08	4.32	NP	7	162	127	<0.50	<0.50	<0.50	<1.5	--	241	--	--	--	125	<250	--	--
6/2/2011		11.08	3.98	NP	7.10	89.9 T4	260 1n	<0.50	<0.50	<0.50	<1.5	--	228	--	--	--	45	<250	--	--
9/7/2011		11.08	5.74	NP	5	<50.0	167	<0.50	<0.50	<0.50	<1.5	--	207	--	--	--	--	<250	--	--
12/5/2011		11.08	5.00	NP	6	<50.0	166 1n	<0.50	<0.50	<0.50	<1.5	--	215	--	--	--	--	<250	--	--
3/6/2012		11.08	5.37	NP	6	<50.0	63.9 1n	<0.50	<0.50	<0.50	<1.5	--	110	--	--	--	39	<250	--	--
6/11/2012		11.08	5.73	NP	5	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
6/12/2012		--	--	--	--	<37.9	118 1n	<0.50	<0.50	<0.50	<1.5	--	220	--	--	--	82	<250	--	--
9/6/2012		11.08	4.14	NP	7	87	<50	<0.50	<0.50	<0.50	<0.50	--	140	<0.50	<0.50	<0.50	10	<5.0	<0.50	<0.50
12/13/2012		11.08	3.80	NP	7	<50	<50	<0.50	<0.50	<0.50	<0.50	--	130	--	--	--	14	<5.0	--	--
MW-14	6/2/2011	12.00	3.58	NP	8.42	4,180 T4	51,600	2,750	67.9	1,790	13,400	--	1.9	--	--	--	27.2	<250	--	--
	9/7/2011	12.00	3.02	NP	8.98	2,970 T4	42,600	1,050	28.1	2,990	7,300	--	<25.0	--	--	--	--	<12500	--	--
	12/5/2011	12.00	4.05	NP	7.95	3,980 T4	14,000	709	9.1	1,420	2,530	--	0.97	--	--	--	--	<250	--	--
	3/6/2012	12.00	3.94	NP	8.06	3,640 T4	16,600	959	15.0	2,330	3,830	--	<2.5	--	--	--	28.1	<1250	--	--
	6/11/2012	12.00	3.91	NP	8.09	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	6/12/2012	--	--	--	--	4,580	15,700	1,200	14.0	1,580	3,010	--	1.4	--	--	--	23.3	<250	--	--
	9/6/2012	12.00	3.35	NP	8.65	<2000	12,000	210	9.1	1,100	1,800	--	<4.0	<4.0	<4.0	<4.0	<20	<40	<4.0	<4.0
	9/11/2012	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
12/13/2012	12.00	3.26	NP	8.74	<50	10,000	72	5.8	610	780	--	<1.5	--	--	--	<7.0	<15	--	--	

TABLE 2a  
HISTORICAL GROUNDWATER GAUGING AND ANALYTICAL DATA  
76 STATION NO. 5191/5043  
449 HEGENBERGER ROAD  
OAKLAND, CALIFORNIA



Well I.D.	Date	GROUNDWATER GAUGING DATA				GROUNDWATER ANALYTICAL DATA															
		TOC Elevation (ft)	Depth to Water (ft)	LNAPL Thickness (ft)	Water Elevation* (ft)	TPHd (ug/L)	TPHg (ug/L)	Benzene (ug/L)	Toluene (ug/L)	Ethylbenzene (ug/L)	Total Xylenes (ug/L)	MTBE (SW8021B) (ug/L)	MTBE (SW8260B) (ug/L)	DIPE (ug/L)	ETBE (ug/L)	TAME (ug/L)	TBA (ug/L)	Ethanol (ug/L)	1,2-Dibromoethane (EDB) (ug/L)	1,2-Dichloroethane (ug/L)	
MW-15	6/2/2011	11.11	2.50	NP	8.61	<b>124 T4</b>	<b>357</b>	<0.50	<0.50	<0.50	<1.5	--	<b>15</b>	--	--	--	<b>6</b>	<250	--	--	
	9/7/2011	11.11	2.54	NP	8.57	<50.0	<b>412</b>	<b>6</b>	<0.50	<b>43</b>	<1.5	--	<b>128</b>	--	--	--	--	<250	--	--	
	12/5/2011	11.11	2.70	NP	8.41	<b>50.5 T4</b>	<b>201</b>	<b>7</b>	<0.50	<b>1</b>	<1.5	--	<b>142</b>	--	--	--	--	<250	--	--	
	3/6/2012	11.11	2.69	NP	8.42	<b>56.2 T4</b>	<50.0	<0.50	<0.50	<0.50	<1.5	--	<b>106</b>	--	--	--	<b>101</b>	<250	--	--	
	6/11/2012	11.11	2.84	NP	8.27	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--
	6/12/2012	--	--	--	--	<37.9	<b>74.3 1n</b>	<0.50	<0.50	<0.50	<1.5	--	<b>114</b>	--	--	--	<b>91</b>	<250	--	--	
	9/6/2012	11.11	2.24	NP	8.87	<b>64</b>	<b>59</b>	<0.50	<0.50	<0.50	<0.50	--	<b>76</b>	<0.50	<0.50	<0.50	<b>45</b>	<5.0	<0.50	<0.50	
12/13/2012	11.11	2.51	NP	8.60	<50	<50	<0.50	<0.50	<0.50	<0.50	--	<b>33</b>	--	--	--	<b>7</b>	<5.0	--	--		
MW-16	6/2/2011	10.98	3.00	NP	7.98	<b>509 T4</b>	<b>1,420 1n</b>	<b>79</b>	<0.50	<b>4</b>	<1.5	--	<b>1,200</b>	--	--	--	<b>257</b>	<250	--	--	
	9/7/2011	10.98	2.65	NP	8.33	<b>90.0 T4</b>	<b>934</b>	<0.50	<0.50	<0.50	<1.5	--	<b>1,240</b>	--	--	--	--	<250	--	--	
	12/5/2011	10.98	3.18	NP	7.80	<b>196 T4</b>	<b>948 1n</b>	<0.50	<0.50	<0.50	<1.5	--	<b>1,320</b>	--	--	--	--	<250	--	--	
	3/6/2012	10.98	2.91	NP	8.07	<b>204 T4</b>	<b>392 1n</b>	<0.50	<0.50	<0.50	<1.5	--	<b>1,090</b>	--	--	--	<b>134</b>	<250	--	--	
	6/11/2012	10.98	3.04	NP	7.94	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	
	6/12/2012	--	--	--	--	<b>48.1 T4</b>	<b>430 1n</b>	<0.50	<0.50	<0.50	<1.5	--	<b>1,100</b>	--	--	--	<b>374</b>	<250	--	--	
	9/6/2012	10.98	2.61	NP	8.37	<b>390</b>	<150	<1.5	<1.5	<1.5	<1.5	--	<b>960</b>	<1.5	<1.5	<1.5	<b>70</b>	<15	<1.5	<1.5	
12/13/2012	10.98	2.50	NP	8.48	<b>52</b>	<150	<1.5	<1.5	<1.5	<1.5	--	<b>980</b>	--	--	--	<b>55</b>	<20	--	--		
MW-17	6/2/2011	11.52	5.78	NP	5.74	<b>687 T4</b>	<b>9,130</b>	<b>2,530</b>	<b>960</b>	<b>35</b>	<b>907</b>	--	<b>1</b>	--	--	--	<b>366</b>	<250	--	--	
	9/7/2011	11.52	4.56	NP	6.96	<b>1,900 T4</b>	<b>47,200</b>	<b>9,620</b>	<b>5,510</b>	<b>1,210</b>	<b>4,510</b>	--	<25.0	--	--	--	--	<12500	--	--	
	12/5/2011	11.52	4.70	NP	6.82	<b>1,790 T4</b>	<b>17,300</b>	<b>4,720</b>	<b>511</b>	<b>238</b>	<b>747</b>	--	<2.5	--	--	--	--	<1250	--	--	
	3/6/2012	11.52	4.64	NP	6.88	<b>1,530 T4</b>	<b>1,580</b>	<b>2,090</b>	<b>24</b>	<b>39</b>	<b>166</b>	--	<b>1</b>	--	--	--	<b>481</b>	<250	--	--	
	6/11/2012	11.52	4.67	NP	6.85	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	
	6/12/2012	--	--	--	--	<b>1,090 T4</b>	<b>4,950</b>	<b>2,340</b>	<b>123</b>	<b>153</b>	<b>610</b>	--	<2.5	--	--	--	<b>411</b>	<1250	--	--	
	9/6/2012	11.52	4.39	NP	7.13	<1000	<b>18,000</b>	<b>4,300</b>	<b>170</b>	<b>370</b>	<b>1,100</b>	--	<10	<10	<10	<10	<b>300</b>	<100	<10	110	
	9/11/2012	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	--	
12/13/2012	11.52	4.20	NP	7.32	<100	<b>55,000</b>	<b>7,300</b>	<b>2,700</b>	<b>1,700</b>	<b>4,600</b>	--	<10	--	--	--	<b>300</b>	<100	--	--		

Gauging Notes:

TOS - Top of Screen  
ft - Feet  
NP - LNAPL not present  
LNAPL - Light non-aqueous phase liquid  
\* - Corrected for LNAPL if present (assumes LNAPL specific gravity = 0.75)  
-- - No information available

Analytical Notes:

< - Below laboratory's indicated reporting limit  
ug/L - micrograms/liter  
DRO- diesel range organics  
TPHd- Total petroleum hydrocarbons as diesel  
TPHg- Total petroleum hydrocarbons as gasoline  
MTBE- Methyl tertiary-butyl ether  
TBA- Tertiary-butyl alcohol

**Bold** - Above the laboratory's indicated reporting limit

1n - The TPHg result for this sample did not match the laboratory standard for gasoline. This is likely due to the presence of MTBE in the sample.  
T4- Result reported for the hydrocarbons within the method-specific range that do not match pattern of laboratory standard.

TABLE 3  
HISTORICAL SOIL ANALYTICAL RESULTS  
76 Station No. 5191/5043  
449 HEGENBERGER RD  
OAKLAND, CALIFORNIA



Sample ID	Date	Sample Depth (feet)	TPHg (mg/kg)	TPHg* (mg/kg)	DRO (mg/kg)	DRO* (mg/Kg)	Benzene (mg/kg)	Toluene (mg/kg)	Ethyl-benzene (mg/kg)	Total Xylenes (mg/kg)	MTBE (mg/kg)	TBA (mg/kg)	TAME (mg/kg)	DIPE (mg/kg)	ETBE (mg/kg)	Ethanol (mg/kg)	EDB (mg/kg)	1,2-DCA (mg/kg)	Lead (mg/kg)
P1	10/25/1991	3	3,200	NA	420	NA	33	120	110	540	NA	NA	NA	NA	NA	NA	NA	NA	NA
P2	10/25/1991	3	9,000	NA	8,400	NA	46	120	330	1,500	NA	NA	NA	NA	NA	NA	NA	NA	NA
P3	10/25/1991	3	7,100	NA	1,100	NA	48	410	220	1,200	NA	NA	NA	NA	NA	NA	NA	NA	NA
P4	10/25/1991	3	370	NA	460	NA	7.4	39	12	77	NA	NA	NA	NA	NA	NA	NA	NA	NA
MW1(2.5)	2/5/1992	2.5	14,000	NA	1,200	NA	160	680	470	2,400	NA	NA	NA	NA	NA	NA	NA	NA	NA
MW2(3.5)	2/5/1992	3.5	9,000	NA	2,400	NA	74	440	280	1,400	NA	NA	NA	NA	NA	NA	NA	NA	NA
MW2(4.5)	2/5/1992	4.5	31	NA	29	NA	2.4	0.14	3	9	NA	NA	NA	NA	NA	NA	NA	NA	NA
MW3(3)	2/5/1992	3	<1.0	NA	49	NA	<0.005	<0.005	<0.005	0.011	NA	NA	NA	NA	NA	NA	NA	NA	NA
MW3(4.5)	2/5/1992	4.5	<1.0	NA	<1.0	NA	<0.005	<0.005	<0.005	<0.005	NA	NA	NA	NA	NA	NA	NA	NA	NA
MW4(5)	8/21/1992	5	<1.0	NA	<1.0	NA	<0.005	<0.005	<0.005	0.0066	NA	NA	NA	NA	NA	NA	NA	NA	NA
MW5(6)	8/21/1992	6	340	NA	43	NA	1.1	1.2	7.8	13	NA	NA	NA	NA	NA	NA	NA	NA	NA
MW6(5)	8/21/1992	5	3.7	NA	1.2	NA	0.9	<0.005	1	0.05	NA	NA	NA	NA	NA	NA	NA	NA	NA
WO1	9/20/1994	9	<1.0	NA	NA	NA	<0.005	<0.005	<0.005	<0.005	NA	NA	NA	NA	NA	NA	NA	NA	5.0
MW9(3)	1/25/1995	3	1.7	NA	2.6	NA	0.016	<0.005	<0.005	<0.005	NA	NA	NA	NA	NA	NA	NA	NA	NA
MW10(2.5)	1/25/1995	2.5	44	NA	17	NA	2	1.5	2.3	5.4	NA	NA	NA	NA	NA	NA	NA	NA	NA
SW1	3/10/1995	8	11	NA	NA	NA	2.8	<0.005	1.6	0.067	NA	NA	NA	NA	NA	NA	NA	NA	NA
SW2	3/10/1995	8	11	NA	NA	NA	3.8	<0.005	0.79	0.034	NA	NA	NA	NA	NA	NA	NA	NA	NA
SW2(4)	3/10/1995	4	2,000	NA	140	NA	<0.005	53	42	240	NA	NA	NA	NA	NA	NA	NA	NA	NA
SW3	3/10/1995	8	1	NA	<1.0	NA	0.009	0.006	0.007	0.014	NA	NA	NA	NA	NA	NA	NA	NA	NA
SW4	3/10/1995	8	<1.0	NA	1.8	NA	<0.005	<0.005	<0.005	<0.005	NA	NA	NA	NA	NA	NA	NA	NA	NA
SW5	3/10/1995	8	<1.0	NA	1.4	NA	<0.005	<0.005	<0.005	<0.005	NA	NA	NA	NA	NA	NA	NA	NA	NA
SW6	3/10/1995	8	<1.0	NA	NA	NA	<0.005	<0.005	<0.005	<0.005	NA	NA	NA	NA	NA	NA	NA	NA	NA
SW7	3/10/1995	8	<1.0	NA	NA	NA	<0.005	<0.005	<0.005	<0.005	NA	NA	NA	NA	NA	NA	NA	NA	NA
SW8	3/10/1995	8	140	NA	NA	NA	2.6	5.3	2.7	12	NA	NA	NA	NA	NA	NA	NA	NA	NA
D1	3/24/1995	3	760	NA	46	NA	1.5	19	15	73	NA	NA	NA	NA	NA	NA	NA	NA	NA
D2	3/24/1995	3	1,200	NA	97	NA	1.6	16	22	110	NA	NA	NA	NA	NA	NA	NA	NA	NA
B1	3/28/1995	6	<1.0	NA	<1.0	NA	0.13	0.026	0.0088	0.059	NA	NA	NA	NA	NA	NA	NA	NA	NA
B2	3/28/1995	6	3.4	NA	<1.0	NA	2.8	0.041	0.19	0.28	NA	NA	NA	NA	NA	NA	NA	NA	NA
B3	3/28/1995	6	<1.0	NA	<1.0	NA	<0.005	0.01	<0.005	0.017	NA	NA	NA	NA	NA	NA	NA	NA	NA
B4	3/28/1995	6	<1.0	NA	<1.0	NA	<0.005	0.017	<0.005	0.032	NA	NA	NA	NA	NA	NA	NA	NA	NA
BD1	3/28/1995	6	<1.0	NA	<1.0	NA	0.21	0.011	0.018	0.038	NA	NA	NA	NA	NA	NA	NA	NA	NA
BD2	3/28/1995	6	12	NA	4.8	NA	2.6	0.68	0.56	1.7	NA	NA	NA	NA	NA	NA	NA	NA	NA
BD3	3/28/1995	6	<1.0	NA	<1.0	NA	0.012	0.014	0.012	0.043	NA	NA	NA	NA	NA	NA	NA	NA	NA
BD4	3/28/1995	6	<1.0	NA	<1.0	NA	<0.005	0.011	0.0072	0.037	NA	NA	NA	NA	NA	NA	NA	NA	NA
S1	3/28/1995	4	110	NA	<1.0	NA	3.5	0.61	7	13	NA	NA	NA	NA	NA	NA	NA	NA	NA
S2	3/28/1995	4	1.4	NA	9.4	NA	0.028	0.012	0.015	0.019	NA	NA	NA	NA	NA	NA	NA	NA	NA
S3	3/28/1995	4	22	NA	2.9	NA	1.2	1.2	0.65	1.9	NA	NA	NA	NA	NA	NA	NA	NA	NA
S4	3/28/1995	4	150	NA	5.8	NA	6.8	5.6	5.3	27	NA	NA	NA	NA	NA	NA	NA	NA	NA
RF1	3/31/1995	3	2,000	NA	330	NA	8.8	68	55	280	NA	NA	NA	NA	NA	NA	NA	NA	NA
RF2	3/31/1995	3	3,300	NA	230	NA	18	160	110	550	NA	NA	NA	NA	NA	NA	NA	NA	NA
SW8(6)	4/3/1995	8	<1.0	NA	<1.0	NA	0.0085	<0.005	0.0084	0.011	NA	NA	NA	NA	NA	NA	NA	NA	NA
FB1	4/3/1995	4.5	25	NA	8.6	NA	2.1	0.058	2.2	1.3	NA	NA	NA	NA	NA	NA	NA	NA	NA
FB2	4/3/1995	4.5	7.1	NA	1.6	NA	0.4	0.018	0.81	1.7	NA	NA	NA	NA	NA	NA	NA	NA	NA
FB3	4/3/1995	4.5	1.6	NA	<1.0	NA	0.028	<0.005	0.13	0.26	NA	NA	NA	NA	NA	NA	NA	NA	NA

**TABLE 3  
HISTORICAL SOIL ANALYTICAL RESULTS  
76 Station No. 5191/5043  
449 HEGENBERGER RD  
OAKLAND, CALIFORNIA**

Sample ID	Date	Sample Depth (feet)	TPHg (mg/kg)	TPHg* (mg/kg)	DRO (mg/kg)	DRO* (mg/Kg)	Benzene (mg/kg)	Toluene (mg/kg)	Ethyl-benzene (mg/kg)	Total Xylenes (mg/kg)	MTBE (mg/kg)	TBA (mg/kg)	TAME (mg/kg)	DIPE (mg/kg)	ETBE (mg/kg)	Ethanol (mg/kg)	EDB (mg/kg)	1,2-DCA (mg/kg)	Lead (mg/kg)
FB4	4/3/1995	4.5	1.4	NA	<1.0	NA	0.23	0.022	0.05	0.15	NA	NA	NA	NA	NA	NA	NA	NA	NA
FBSW1	4/3/1995	3	7.4	NA	1.3	NA	0.066	0.021	1	<0.005	NA	NA	NA	NA	NA	NA	NA	NA	NA
FBSW2	4/3/1995	3	70	NA	7.6	NA	0.11	0.096	2.1	6.7	NA	NA	NA	NA	NA	NA	NA	NA	NA
FBSW3	4/3/1995	3	2.3	NA	7.8	NA	0.012	0.01	0.018	0.012	NA	NA	NA	NA	NA	NA	NA	NA	NA
FBSW4	4/3/1995	3	9	NA	3.7	NA	0.25	0.036	0.93	0.062	NA	NA	NA	NA	NA	NA	NA	NA	NA
MW1SW1	4/5/1995	5	25	NA	2.8	NA	2.1	0.025	2.4	0.19	NA	NA	NA	NA	NA	NA	NA	NA	NA
MW1SW2	4/5/1995	5	4.2	NA	1.2	NA	0.17	0.01	0.68	0.048	NA	NA	NA	NA	NA	NA	NA	NA	NA
WE1	4/5/1995	4.5	26	NA	3.4	NA	0.31	0.3	0.59	2.6	NA	NA	NA	NA	NA	NA	NA	NA	NA
WE2	4/5/1995	4.5	2.7	NA	5.1	NA	0.0054	0.0065	0.038	0.17	NA	NA	NA	NA	NA	NA	NA	NA	NA
WE3	4/5/1995	4.5	8.2	NA	1.6	NA	0.21	0.074	1.6	0.0076	NA	NA	NA	NA	NA	NA	NA	NA	NA
FS-1	4/5/1995	4	12	NA	<1.0	NA	0.28	<0.005	1.5	0.016	NA	NA	NA	NA	NA	NA	NA	NA	NA
MW8(6)	4/21/1997	6	1.3	NA	<1.0	NA	0.0051	<0.005	0.015	0.041	<0.005	NA	NA	NA	NA	NA	NA	NA	NA
<b>Delta 2009</b>																			
B-4@6	12/17/2009	6	20.4	NA	11.4	10.1	0.046	0.18	1	4.2	0.061	0.091	<0.0029	<0.0029	<0.0029	<0.0029	<0.0029	<0.0029	NA
B-4@15	12/17/2009	15	<4.9	NA	<5.8	<5.8	0.0036	0.0069	0.011	0.049	0.0081	0.036	<0.003	<0.003	<0.003	<0.003	<0.003	<0.003	NA
B-4@20	12/17/2009	20	<4.9	NA	<5.6	<5.6	<0.003	<0.003	<0.003	<0.006	<0.003	<0.015	<0.003	<0.003	<0.003	<0.003	<0.003	<0.003	NA
B-5@8	12/17/2009	8	1,060	NA	285	269	6.2	21.6	30.9	143	<0.0029	0.079	0.068	<0.0029	<0.0029	<0.0029	<0.0029	<0.0029	NA
B-5@17.5	12/17/2009	17.5	136	NA	27.8	26.9	0.55	1.4	2.7	15.8	<0.003	0.035	<0.003	<0.003	<0.003	<0.003	<0.003	<0.003	NA
B-5@26.5	12/17/2009	26.5	1,570	NA	338	346	16.2	73.5	52.8	255	0.02	0.11	<0.0028	<0.0028	<0.0028	<0.0028	<0.0028	<0.0028	NA
B-5@32	12/17/2009	32	<4.8	NA	<5.9	<5.9	0.007	0.0087	0.0057	0.031	<0.0029	<0.015	<0.0029	<0.0029	<0.0029	<0.0029	<0.0029	<0.0029	NA
<b>Delta 2010</b>																			
MW-11@10	6/22/2010	10	NA	<0.18	NA	3.2	<0.0022	<0.0022	<0.0022	<0.0066	0.011	<0.011	<0.0022	<0.0022	<0.0022	<0.0022	<0.0022	<0.0022	6.1
MW-11@20	6/22/2010	20	NA	<0.25	NA	27.3	<0.0027	<0.0027	<0.0027	<0.0081	<0.0027	<0.013	<0.0027	<0.0027	<0.0027	<0.0027	<0.0027	<0.0027	3.4
MW-12@8	6/22/2010	8	NA	210	NA	45.7	5.2	9.1	6.7	33.3	<0.0028	0.021	<0.0028	<0.0028	<0.0028	<0.0028	<0.0028	<0.0028	8.6
MW-12@10	6/22/2010	10	NA	422	NA	73.6	4	3.5	11.0	31.4	<0.0029	<0.015	0.023	<0.0029	<0.0029	<0.0029	<0.0029	<0.0029	9.5
MW-12@20	6/22/2010	20	NA	<0.24	NA	<2.0	0.019	<0.0028	<0.0028	<0.0085	<0.0028	<0.014	<0.0028	<0.0028	<0.0028	<0.0028	<0.0028	<0.0028	6.6
MW-12A@26	6/23/2010	26	NA	6,840	NA	2,210	80.9	232	178	607	<0.0027	<0.014	<0.0027	<0.0027	<0.0027	<0.0027	<0.0027	<0.0027	13.1
MW-12A@32	6/23/2010	32	NA	943	NA	267	4.9	15.5	12.0	42.6	0.045	0.044	0.048	<0.0028	<0.0028	<0.0028	<0.0028	<0.0028	6.6
MW-12A@34	6/23/2010	34	NA	<0.22	NA	<1.9	<0.0027	0.0097	0.0074	0.033	<0.0027	<0.013	<0.0027	<0.0027	<0.0027	<0.0027	<0.0027	<0.0027	4.9
MW-13@8	6/22/2010	8	NA	<0.21	NA	<2.0	<0.0026	<0.0026	<0.0026	<0.0077	0.064	<0.013	<0.0026	<0.0026	<0.0026	<0.0026	<0.0026	<0.0026	3.6
MW-13@15	6/22/2010	15	NA	<0.24	NA	<2.0	<0.0029	<0.0029	<0.0029	<0.0087	<0.0029	<0.014	<0.0029	<0.0029	<0.0029	<0.0029	<0.0029	<0.0029	5.9
<b>Antea Group 2011</b>																			
MW-14d7	5/17/2011	7	NA	<0.23	<2.0	<2.0	<0.0027	<0.0027	<0.0027	<0.0081	<0.0027	<0.014	<0.0027	<0.0027	<0.0027	<0.36	<0.0027	<0.0027	6.6
MW-14d10	5/17/2011	10	NA	1,740	45.5 1n	45.9 1n	1.8	0.2	44	140	<0.0026	<0.013	<0.0026	<0.0026	<0.0026	<0.34	<0.0026	<0.0026	7
MW-14d13	5/17/2011	13	NA	1	<2.0	<2.0	<0.0027	<0.0027	0.037	0.066	<0.0027	<0.014	<0.0027	<0.0027	<0.0027	<0.36	<0.0027	<0.0027	6.6
MW-15d8	5/17/2011	8	NA	2.3	6.2	5.2	0.023	<0.0038	1.9	0.25	0.19	0.16	<0.0038	<0.0038	<0.0038	<0.51	<0.0038	<0.0038	7
MW-15d13	5/17/2011	13	NA	<0.23	<1.9	<1.9	<0.0028	<0.0028	<0.0028	<0.0083	0.015	0.022	<0.0028	<0.0028	<0.0028	<0.37	<0.0028	<0.0028	7
MW-16d8	5/17/2011	8	NA	<0.23	<2.0	<2.0	<0.0027	<0.0027	<0.0027	<0.0081	0.15	0.014	<0.0027	<0.0027	<0.0027	<0.36	<0.0027	<0.0027	5.7
MW-16d13	5/17/2011	13	NA	<0.23	<2.0	<2.0	<0.0028	<0.0028	<0.0028	<0.0084	<0.0028	<0.014	<0.0028	<0.0028	<0.0028	<0.37	<0.0028	<0.0028	5.5
MW-17d9	5/18/2011	9	NA	633	39.6 1n	36.7 1n	6	14.1	17.9	58	<0.0026	0.03	<0.0026	<0.0026	<0.0026	<0.35	<0.0026	<0.0026	16.3
MW-17d13	5/18/2011	13	NA	5.4	2.9 1n	2.5 1n	2.7	0.46	1.4	2.8	<0.0027	0.029	<0.0027	<0.0027	<0.0027	<0.36	<0.0027	<0.0027	6.4
B-6d9	5/18/2011	9	NA	2,490	72.0 1n	68.6 1n	26.4	73.9	58.1	230	<0.0031	<0.015	<0.0031	<0.0031	<0.0031	<0.41	<0.0031	<0.0031	10.1
B-6d14	5/18/2011	14	NA	194	258 1n	250 1n	3.6	5.1	5.1	22	<0.0025	<0.013	<0.0025	<0.0025	<0.0025	<0.33	<0.0025	<0.0025	9.2
B-6d21	5/18/2011	21	NA	7.2	<2.0	<2.0	0.67	0.86	0.25	0.94	0.036	0.014	<0.0027	<0.0027	<0.0027	<0.37	<0.0027	<0.0027	6.8
B-6d26	5/18/2011	26	NA	17	3.4 1n	2.9 1n	0.83	1.2	0.46	1.7	0.086	0.021	<0.0026	<0.0026	<0.0026	<0.34	<0.0026	<0.0026	6.6

Notes:

**TABLE 3**  
**HISTORICAL SOIL ANALYTICAL RESULTS**  
**76 Station No. 5191/5043**  
**449 HEGENBERGER RD**  
**OAKLAND, CALIFORNIA**



Sample ID	Date	Sample Depth (feet)	TPHg (mg/kg)	TPHg* (mg/kg)	DRO (mg/kg)	DRO* (mg/Kg)	Benzene (mg/kg)	Toluene (mg/kg)	Ethyl-benzene (mg/kg)	Total Xylenes (mg/kg)	MTBE (mg/kg)	TBA (mg/kg)	TAME (mg/kg)	DIPE (mg/kg)	ETBE (mg/kg)	Ethanol (mg/kg)	EDB (mg/kg)	1,2-DCA (mg/kg)	Lead (mg/kg)
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TPHg = total petroleum hydrocarbons as gasoline by EPA Method 8015  
 TPHg\* = total petroleum hydrocarbons as gasoline by CA LUFT  
 DRO = Diesel Range Organics by EPA Method 8015B  
 DRO\* = Diesel Range Organics by EPA Method 8015 Silica Gel Treated  
 BTEX = benzene, toluene, ethylbenzene, total xylenes by EPA Method 8260B  
 MTBE = methyl tertiary-butyl ether by EPA Method 8260  
 TBA = tertiary-butyl alcohol by EPA Method 8260  
 TAME = tert-amyl methyl ether by EPA Method 8260  
 DIPE = Diisopropyl ether by EPA Method 8260  
 ETBE = Ethyl-tert-butyl-ether by EPA Method 8260  
 EDB = 1,2-Dibromoethane by EPA Method 8260  
 1,2-DCA = 1,2-Dichloroethane by EPA Method 8260  
 mg/kg = milligrams per kilogram  
 NA = not applicable

**Remedial Action Plan**  
**76 Service Station No. 5191/5043**  
**449 Hegenberger Road**  
**Oakland, California**  
**Antea Group Project No. I42705191**



## ***Appendix A***

Site Details and Previous Environmental Investigations



## PREVIOUS INVESTIGATION AND SITE HISTORY SUMMARY

October 1991 - Four soil samples were collected from the product pipe trenches at depths of approximately 3 feet below ground surface (bgs) during a dispenser island modification. The product pipe trenches were subsequently excavated to the groundwater depth at 4 to 4.5 feet bgs.

February 1992 - Three monitoring wells, MW-1 through MW-3, were installed at the site to depths ranging from 13.5 to 15 feet bgs.

August 1992 - Three additional monitoring wells, MW-4 through MW-6, were installed at the site to a depth of 13.5 feet bgs.

September 1994 - One 280-gallon waste-oil UST was removed from the site. The UST was made of steel, and no apparent holes or cracks were observed in the UST. One soil sample was collected from beneath the former UST at a depth of approximately 9 feet bgs. No petroleum hydrocarbons were reported.

January 1995 - Two additional monitoring wells, MW-9 and MW-10, were installed to depths of 13 and 15 feet bgs. In addition, monitoring wells MW-4 and MW-5 were destroyed by over-drilling the wells and backfilling with neat cement.

March 1995 - Two 10,000-gallon gasoline USTs and one 10,000-gallon diesel UST were removed from the site. Groundwater was encountered in the tank cavity at a depth of approximately 8.5 feet bgs. Soil samples contained total petroleum hydrocarbons as diesel (TPHd) and benzene, and TPH as gasoline (TPHg). Approximately 125,000 gallons of groundwater were pumped from the site for remediation and properly disposed off-site. Four fuel dispenser islands and associated product piping were also removed. Based on the results of the confirmation samples, the product dispenser islands were over excavated to approximately 6 feet bgs.

March-April 1995 - During demolition activities of the former station building, soil samples were collected from two excavations, which were subsequently over excavated. Confirmation samples contained petroleum hydrocarbons. An additional area on the south side of the former station building was excavated based on photo-ionization detector (PID) readings. Two monitoring wells, MW-1 and MW-2, were destroyed in order to allow for over excavation activities to extend to an area adjacent to the dispenser islands in the southeastern quadrant of the site. The excavated areas were subsequently backfilled with clean-engineered fill.

April 1997 - Two additional monitoring wells, MW-7 and MW-8, were installed off-site to the south and east on the neighboring property to a depth of 13 feet bgs. In addition, monitoring well MW-3, which was damaged during site renovation activities, was fully drilled out and reconstructed in the same borehole.

October 2003 - Site environmental consulting responsibilities were transferred to TRC.

April 8-9, 2005 - TRC conducted a 24-hour dual phase extraction (DPE) test at the site using monitoring well MW-6. The 24-hour DPE test was only moderately successful at removing vapor-phase petroleum hydrocarbons from the subsurface; therefore, TRC recommended DPE no longer be considered a viable remedial alternative for the site.

October 2007 - Site environmental consulting responsibilities were transferred to Delta Consultants.

December 2009 - Delta advanced two borings, B-4 and B-5, to depths of 20 feet bgs and 32 feet bgs, respectively. Analytical results from the soil and groundwater samples collected from these two borings indicated that the soil and the groundwater were impacted by petroleum hydrocarbons at these locations.

June 2010 – Delta installed two 4-inch diameter monitoring/extraction wells, MW-11 and MW-12, and two 2-inch diameter monitoring wells, MW-12A and MW-13, at the site. Analytical results from the soil and groundwater samples collected from the MW-12 and MW-12A boring locations indicated that the soil and the groundwater were impacted by petroleum hydrocarbons at these locations.

May 2011 – Antea Group (formally Delta Consultants) installed four 2-inch diameter monitoring wells, MW-14 through MW-17, and advanced one soil boring, B-6, at the site. All four monitoring wells were installed with ten feet of screen from 3 feet bgs to 13 feet bgs. Analytical results of soil samples collected during the monitoring well installation reported TPHg concentrations ranging from 1.0 milligrams per kilogram (mg/kg) (MW-14d13) to 2,490 mg/kg (B-6d9), benzene concentrations ranging from 0.67 mg/kg (B-6d21) to 26.4 mg/kg (B-6d9), toluene concentrations ranging from 0.2 mg/kg (MW-14d10) to 73.9 mg/kg (B-6d9), ethylbenzene concentrations ranging from 0.037 mg/kg (MW-14d13) to 58.1 mg/kg (B-6d9), total xylenes concentrations ranging from 0.066 mg/kg (MW-14d13) to 230 mg/kg (B-6d9), methyl tertiary-butyl ether (MTBE) concentrations ranging from 0.015 mg/kg (MW-15d13) to 0.19 mg/kg (MW-15d8), tertiary-butyl alcohol (TBA) concentrations ranging from 0.014 mg/kg (MW-16d8 and B-6d21) to 0.16 mg/kg (MW-15d8), and lead concentrations ranging from 5.5 mg/kg (MW-16d13) to 16.3 mg/kg (MW-17d9). Diesel range organics (DRO) and DRO with silica gel concentrations were reported; however, all of the results did not match the laboratory standard for diesel. Concentrations of DRO ranged from 2.9 mg/kg (MW-17d13) to 258 mg/kg (B-6d14) and DRO with silica gel concentrations ranged from 2.5 mg/kg (MW-17d13) to 250 mg/kg (B-6d14).

March 2012 – Antea Group advanced five soil borings (HPB-1 through HPB-5) at the site. The borings were advanced using direct push technology. The borings were used to obtain a hydraulic profile of the substrate beneath the site. The data obtained during the investigation will be used to determine the best path forward in terms of remediation.

## **SENSITIVE RECEPTORS**

April 24, 2006, TRC completed a sensitive receptor survey for the site. According to the Department of Water Resources (DWR) records, three water supply wells are located within one-half mile of the site. The closest well is an irrigation well, reported to be, approximately 1,080 feet southeast of the site. In addition, two surface water bodies were observed within a one-half mile radius of the site. San Leandro Creek is located approximately 1,400 feet southwest of the site and flows into the San Leandro Bay. Elmhurst Creek is located approximately 2,220 feet north of the site and also flows into the San Leandro Bay.

Current Consultant: **Antea Group**

**Remedial Action Plan**  
**76 Service Station No. 5191/5043**  
**449 Hegenberger Road**  
**Oakland, California**  
**Antea Group Project No. I42705191**



## ***Appendix B***

PTS Persulfate Bench Scale Laboratory Report



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JAN 14 2013

8100 Secura Way • Santa Fe Springs, CA 90670  
Telephone (562) 347-2500 • Fax (562) 907-3610

January 9, 2013

Dennis Dettloff  
Antea Group  
11050 White Rock Road, Suite 110  
Rancho Cordova, CA 95670

Re: PTS File No: 42834  
Physical Properties Data  
Site 2705191, Oakland; I42705191

Dear Mr. Dettloff:

Please find enclosed report for pH Monitoring & Residual Persulfate Bench Scale analyses conducted upon soil and water samples received from your Site 2705191, Oakland; I42705191 project. All analyses were performed by applicable ASTM, EPA, or API methodologies in conjunction with Residual Persulfate procedures. An electronic version of the report has previously been sent to your attention via the internet. Any remnant sample material is in storage and will be retained for thirty days past completion of testing at no charge. Please note that the samples will be disposed of at that time. You may contact me regarding storage, disposal, or return of the samples.

PTS Laboratories appreciates the opportunity to be of service. If you have any questions or require additional information, please give me a call at (562) 347-2502.

Sincerely,  
PTS Laboratories

Michael Mark Brady, P.G.  
District Manager

Encl.

Project Name: Site 2705191, Oakland  
 Project Number: I42705191

PTS File No: 42834  
 Client: Antea Group

## TEST PROGRAM - 20130108

CORE ID	Depth ft.	Core Recovery ft.	ISCO Reactor Vessel Setup	pH Monitoring	Residual Persulfate Test 28 days			Notes
		Plugs:						
Date Received: 20121116								
HA-1d5	N/A	2.50	2	20	2			
MW-14	N/A	N/A						
<b>TOTALS:</b>	<b>10 cores 4 bottles</b>	<b>2.50</b>	<b>2</b>	<b>20</b>	<b>2</b>			<b>14</b>

### Laboratory Test Program Notes

Contaminant identification: \_\_\_\_\_

Standard TAT for basic analysis is 10 business days.

Reagent is OBC (Oxygen BioChem) to be provided by Redox Tech. OBC Reagent doses: 8 g/L and 15 g/L.

pH monitoring at 0hr for baseline, 4 hr, 1 day, 2 days, 4 days, 7 days, 10 days, 14 days, 21 days, and 28 days.

If the pH in either test drops to 9, Client (Antea Group) requests laboratory provide notification in order to discuss how to proceed with running the rest of the test(s).

Additional work to be billed at laboratory standard rate of \$85/hour or our standard test fee rates.

Residual persulfate TOD measurement at 28 days.

Based on specifications provided in email transmittal from N. Persaud/Antea Group 20121101

Run large ISCO reactor( 250 g : 500 mL); Use 1-L reactors to accommodate additional volume required for pH monitoring.

Residual persulfate measured by using standard back titration, FMC method or similar.

pH monitoring events may be moved to accommodate PTS Laboratories schedule D.Dettloff/Antea Group 20121129.

Composition of OBC is 80% Sodium Persulfate 20% Calcium Peroxide per D.Dettloff/Antea Group 20121130.



Client: Antea Group  
Project Name: Site 2705191, Oakland; I42705191

PTS File No: 42834  
December 3, 2012

## **TOD REACTORS SETUP LABORATORY PROCEDURE**

(ISCO – TOD Reactor Setup based on FMC Adventus procedure)

### **Purpose**

The purpose of this test is to setup reactors for conducting residual persulfate tests using OBC (Oxygen BioChem). Residual persulfate is then used to calculate Total Oxidant Demand (TOD).

### **Method Summary**

For the physical portion of the tests soil is added to glass reactor vessels. Groundwater with individual reagents (OBC) at designated ratios are added volumetrically to each reactor. The soil and reagent groundwater are manually stirred to make a slurry. Lids are placed upon the reactor vessels to minimize VOC loss. The reactors are placed on an oscillatory table and rotated at low speed (60-100 rpm) for the duration of testing. 10-20 ml aliquots of groundwater are periodically removed for measurement of pH, residual persulfate and calculation of TOD.

### **Deviations from Method**

Deviations, if any, are to be communicated to client and prior approval should be obtained before proceeding with tests.

### **Safety**

- All personnel working in the laboratory are required to follow the PTS - SFS Facility *Health, Safety, and Environment Manual* plan.
- The laboratory routinely analyzes contaminated materials (chemical and biological) where health and safety hazards can exist. Therefore this procedure should not be used unless adequate health and safety precautions are taken.
- A reference file of Material Safety Data Sheets (MSDS) is posted in the laboratory and is available to all personnel involved in these analyses.

### **Equipment and Supplies**

1000mL Reactor Vessels  
Balance – A balance sensitive to 0.01 g  
Analytical Balance sensitive to 0.1 mg  
Weighing canoes  
Graduated cylinders (250, 500 or 1000 ml)  
Stainless steel homogenizing bowl  
Magnetic stirrer and stir bars  
Stainless steel stirrer or large spoon  
Oscillatory shaker table  
10 or 20 ml pipette  
pH meter

### **Reagents and Standards**

See the Laboratory Procedure section for preparation and use of reagents.

### **Sample Collection, Preservation, and Storage**

- Sample collection is performed by the client with samples delivered to the laboratory for analyses.





- Samples are stored in Sample Refrigerator at  $4\pm 2^{\circ}\text{C}$  prior to the treatability tests.
- Water and soil samples are typically homogenized before use (homogenization may be dependant upon number of tests and sample volumes required, verify with client).
- The maximum holding time for bench scale testing is project-specific and determined by client.
- Refer to the PTS-SFS Quality Manual Section 22 Sample Management and PTS Laboratories Cooler Sample Receiving and Sample Storage SOP for additional information.

### **Quality Control**

- Due to the nature of the samples received from client and the TOD Reactors test, standards are not available. Therefore the best way to assure the equipment is operating within control is to check the calibration of equipment before use.
- Duplicate reactors may be analyzed.

### **Calibration and Standardization**

- The balances used in this analysis must have calibration checked on the day of use in the range of use.
- No other calibration or standardization is applicable to this analysis.

### **Laboratory Procedure**

Be sure to read and be familiar with all client procedure and project requirements before beginning bench test.

### **Reactor Vessel Preparation**

Contaminant free 1000 ml reactor vessels will be used for the tests.

### **Prepare Reagents**

Measure all granular reagents into labeled disposable weighing canoes. Groundwater will be measured in specified increments as each groundwater/reagent solution is mixed. Remove groundwater from refrigerator and allow to equilibrate to room temperature several hours before beginning tests.

Prepare groundwater OBC solution in designated concentrations as provided by client.

### **Sample Preparation**

Remove samples (soil and groundwater) from the refrigerator and allow to equilibrate to room temperature. Keep containers sealed to prevent the loss of VOCs. As written above, if required, the soil and groundwater are to be homogenized first. If rocks or other solid materials (gravel, lumps, and particles greater than 4 mesh) are present in soil remove them. The compositing will be conducted on the bench top as quickly as possible to minimize volatilization of COCs; however no effort will be made to exclude oxygen. The remainder of soil will be returned to refrigerator after sampling. Do not allow soil to dry. Homogenize containers of sample water to be used, using as little amount as required. The compositing will be conducted on the bench top as quickly as possible to minimize volatilization of COCs; however no effort will be made to purge oxygen. Keep remainder of sample water chilled to minimize VOC losses.

### **Reactor Vessel Preparation**

1. Refer to the Test Program for setting up the TOD Reactors and sampling requirements/schedule.
2. Place the appropriate amount of homogenized soil listed in the TOD Setup Matrix, into each labeled reactor vessel (See TOD Setup matrix for labeling scheme).
  - a. Soil and groundwater are combined in the reactors in a 1:2 soil to liquid ratio.
  - b. For a 1000 ml reactor this will be 250 grams of soil to 500 ml of groundwater.
3. Measure reagent ground water using a graduated cylinder into the reactor vessel.

4. Mix slowly by hand for ~10 seconds using a stainless steel stirrer to minimize potential VOC volatilization/loss. A slurry should be created.
5. Measure the initial pH of the groundwater in the reactor vessel.
6. Repeat step 5. at client-specified specified time intervals; 4 hrs. 1, 2, 4, 7, 10, 14, 21 and 28 days.
7. Place the cap on each reactor vessel. Monitor reactors for gas production. If gas is produced, the lids will need to be loosened to prevent reactors from breaking.
8. Place reactors on an oscillatory table and rotate at low speed (60-100 rpm) for duration of testing.
9. Repeat steps 2 through 8 for each additional reactor to be setup, starting with the lowest concentration and finishing with the highest concentration of reagents.

### **TOD Sampling**

1. After the designated time interval, remove reactor from oscillatory table and take a 10-20 ml aliquot using a pipette. The aliquot will be used for residual persulfate measurement (see Residual Persulfate by Titration Procedure).
2. If the tests have not reached the final test interval, return the reactors to the oscillatory shaker and continue rotating at low speed (60-100 rpm).
3. Repeats steps 1-2 as needed until all required time intervals have been sampled.

### **Pollution Prevention and Waste Management**

- Although test samples are submitted by the laboratory's clients, it is the laboratory's responsibility to comply with all federal, state, and local regulations governing waste management, particularly the hazardous waste identification rules and land disposal restrictions, and to protect the air, water, and land by minimizing and controlling all releases from fume hoods and bench operations. Compliance with all sewage discharge permits and regulations is also required.
- Because many of the samples PTS Laboratories analyzes may be contaminated with crude oil, refined hydrocarbons or other contaminants, it is important that all samples are safely disposed and do not violate federal, state, or local laws. It is the policy of PTS Laboratories not to violate hazardous waste or clean water discharge regulations – contact your supervisor if you have any concern regarding sample disposal.
- Refer to the PTS-SFS Quality Manual Section 22 Sample Management and PTS Laboratories Sample Disposal SOP for additional information.



## RESIDUAL PERSULFATE BY TITRATION PROCEDURE

(Based on FMC Adventus Klozur™ procedure)

### Purpose

The purpose of this test is to determine the residual persulfate in groundwater.

### Method Summary

Groundwater containing persulfate is mixed with 1 N H<sub>2</sub>SO<sub>4</sub> and 0.5 N ferrous ammonium sulfate in an Erlenmeyer flask and back titrated with 0.5 N KMnO<sub>4</sub>. The method is suitable for high pH and iron sulfate persulfate activation methods. For hydrogen peroxide and calcium peroxide activation of persulfate, 0.5 N Ce(SO<sub>4</sub>)<sub>2</sub> and a ferroin indicator must be used. Residual persulfate may then be used to calculate Total Oxidant Demand (TOD).

### Equipment needed

20 mL plastic syringe  
Nylon 0.45µm syringe filter  
10-20 mL pipette  
250 mL Erlenmeyer flask  
Stir bar / magnetic plate  
Burette  
100 mL flask

### Chemicals needed

1 N H<sub>2</sub>SO<sub>4</sub>  
0.5 N ferrous ammonium sulfate  
0.5 N KMnO<sub>4</sub> or 0.5 N Ce(SO<sub>4</sub>)<sub>2</sub>  
Ferroin indicator if using Ce(SO<sub>4</sub>)<sub>2</sub>

### Procedure

1. Remove a small aliquot of ground water with 20 mL plastic syringe, filter through 0.45µm syringe filter.
2. Pipette 10 mL of the filtered ground water solution containing persulfate into a 250 mL Erlenmeyer flask. (Note: ground water volume used may range from 2 – 20 mL depending upon concentration).
3. Add 50 mL of a 1 N H<sub>2</sub>SO<sub>4</sub> solution
4. Add exactly 40 mL of 0.5 N ferrous ammonium sulfate solution. Swirl constantly while adding.
5. Let stand for one minute
6. Titrate with 0.5 N KMnO<sub>4</sub> to a permanent pink endpoint or with 0.5 N Ce(SO<sub>4</sub>)<sub>2</sub> to a Ferroin indicator endpoint.
7. Run a blank titration on exactly 40 mL of ferrous ammonium sulfate solution, as used above, in 50 mL of 1 N H<sub>2</sub>SO<sub>4</sub>.

### Calculation

$$\text{g/L Klozur}^{\text{TM}} \text{ persulfate} = (A-B) \cdot C \cdot 119 / D$$

where:

A = mL KmnO<sub>4</sub> or Ce(SO<sub>4</sub>)<sub>2</sub> solution for titrating the blank  
B = mL KmnO<sub>4</sub> or Ce(SO<sub>4</sub>)<sub>2</sub> solution for titrating the sample  
C = normality of the KmnO<sub>4</sub> or Ce(SO<sub>4</sub>)<sub>2</sub> solution used  
D = volume of sample in mL

Project Name: Site 2705191, Oakland  
 Project Number: I42705191

PTS File No: 42834  
 Client: Antea Group

**TEST PROGRAM - MONITORING MATRIX 20130108**

REACTOR VESSEL		REACTOR TREATMENT TYPE	Monitoring Event #1	Monitoring Event #2	Monitoring Event #3	Monitoring Event #4	Monitoring Event #5	Monitoring Event #6	Monitoring Event #7	Monitoring Event #8	Monitoring Event #9	Monitoring Event #10	Notes
No.	NAME		T = 0 hour	T = 4 hrs	T = 1 day	T = 2 days	T = 4 days	T = 7 days	T = 10 days	T = 16 days	T = 21 days	T = 28 days	
1	Low OBC	28-days OBC at 8.0 g/L MW-14 Water, HA-1d5 soil	Initial pH measurement	pH monitoring	pH monitoring	pH monitoring	pH monitoring	pH monitoring	pH monitoring	pH monitoring	pH monitoring	pH monitoring, TOD test	28-days OBC@ treatment
2	High OBC	28-days OBC at 15.0 g/L MW-14 Water, HA-1d5 soil	Initial pH measurement	pH monitoring	pH monitoring	pH monitoring	pH monitoring	pH monitoring	pH monitoring	pH monitoring	pH monitoring	pH monitoring, TOD test	28-days OBC@ treatment

**Laboratory Test Program Notes**

Reagent is OBC (Oxygen BioChem) to be provided by Redox Tech. OBC Reagent doses: 8 g/L and 15 g/L.

pH monitoring at 0hr for baseline, 4 hr, 1 day, 2 days, 4 days, 7 days, 10 days, 14 days, 21 days, and 28 days.

If the pH in either test drops to 9, Client (Antea Group) requests laboratory provide notification in order to discuss how to proceed with running the rest of the test(s).

Residual persulfate TOD measurement at 28 days.

Based on specifications provided in email transmittal from N. Persaud/Antea Group 20121101

Run large ISCO reactor( 250 g : 500 mL); Use 1-L reactors to accommodate additional volume required for pH monitoring.

Residual persulfate measured by using standard back titration, FMC method or similar.

pH monitoring events may be moved to accommodate PTS Laboratories schedule D.Dettloff/Antea Group 20121129.

Composition of OBC is 80% Sodium Persulfate 20% Calcium Peroxide per D.Dettloff/Antea Group 20121130.

**Project Name:** Site 2705191, Oakland  
**Project Number:** I42705191

**PTS File No:** 42834  
**Client:** Antea Group

**TEST PROGRAM - Reagent Dosages Based on 500 ml of Groundwater 20130108**

REACTOR VESSEL		REACTOR TREATMENT TYPE	SOIL, grams	GROUNDWATER ml	TIME = 0
No.	NAME				
1	Low OBC	28-days OBC at 8.0 g/L MW-14 Water, HA-1d5 soil	250	500	OBC = 8 g/L = 4.0g/500mL
2	High OBC	28-days OBC at 15.0 g/L MW-14 Water, HA-1d5 soil	250	500	OBC = 15 g/L = 7.5g/500mL

**Laboratory Test Program Notes**

Reactor Vessels should have a small amount of headspace when filled to accommodate to oxygen gas production; lids should not be tight.

Reagent is OBC (Oxygen BioChem) to be provided by Redox Tech. OBC Reagent doses: 8 g/L and 15 g/L.

Residual persulfate TOD measurement at 28 days.

Based on specifications provided in email transmittal from N. Persaud/Antea Group 20121101

Run large ISCO reactor( 250 g : 500 mL); Use 1-L reactors to accommodate additional volume required for pH monitoring.

Residual persulfate measured by using standard back titration, FMC method or similar.

Composition of OBC is 80% Sodium Persulfate 20% Calcium Peroxide per D.Dettloff/Antea Group 20121130.

PTS File No: 42834  
Client: Antea Group

### TOD BENCH SCALE ANALYSIS SETUP

(METHOD: ISCO - PTS Laboratories, Inc.)

PROJECT NAME: Site 2705191, Oakland  
PROJECT NO: I42705191

SAMPLE ID.	VOLUME GROUNDWATER, mL	REQUIRED MASS OF OBC®, g	ACTUAL MASS OF OBC®, g	REQUIRED SOIL MASS, g	ACTUAL SOIL MASS, g
1. Low OBC	500	4.0	4.0013	250	250.15
2. High OBC	500	7.5	7.5041	250	250.03

Use 250 g soil, 500 mL H<sub>2</sub>O

Technician: JS

Date/Time: 20121210/1058

#### Low OBC (8g/L)

$$\left( \frac{8 \text{ g OBC}}{1 \text{ L H}_2\text{O}} \right) \times 0.5 \text{ L H}_2\text{O} = 4.0 \text{ g OBC}$$

#### High OBC (15g/L)

$$\left( \frac{15 \text{ g OBC}}{1 \text{ L H}_2\text{O}} \right) \times 0.5 \text{ L H}_2\text{O} = 7.5 \text{ g OBC}$$

PTS File No: 42834  
 Client: Antea Group

**Reactor Groundwater + Reagent pH T = 0 hr**

(METHODOLOGY: pH Meter)

PROJECT NAME: Site 2705191, Oakland  
 PROJECT NO: I42705191

SAMPLE ID.	DEPTH, ft.	ANALYSIS DATE	ANALYSIS TIME	ROOM TEMP. °F	SAMPLE MATRIX	pH READING
1. Low OBC	N/A	20121210	1114	73	Water	9.04
2. High OBC	N/A	20121210	1123	73	Water	9.98

**QC DATA**

**Meter Model/Type:** Corning pH Meter 240

METER CALIBRATION	Date/Time:	20121210/1003
pH Buffer Standard 4.00		4.00
pH Buffer Standard 7.00		7.00
pH Buffer Standard 10.00		10.01



PTS File No: 42834  
 Client: Antea Group

**Reactor Groundwater + Reagent pH T = 4 hr**

(METHODOLOGY: pH Meter)

PROJECT NAME: Site 2705191, Oakland  
 PROJECT NO: I42705191

SAMPLE ID.	DEPTH, ft.	ANALYSIS DATE	ANALYSIS TIME	ROOM TEMP. °F	SAMPLE MATRIX	pH READING
1. Low OBC	N/A	20121210	1515	75	Water	9.60
2. High OBC	N/A	20121210	1523	75	Water	10.03

**QC DATA**

**Meter Model/Type:** Corning pH Meter 240

<b>METER CALIBRATION</b>	<b>Date/Time:</b> 20121210/1003
pH Buffer Standard 4.00	4.00
pH Buffer Standard 7.00	7.00
pH Buffer Standard 10.00	10.01

PTS File No: 42834  
 Client: Antea Group

**Reactor Groundwater + Reagent pH T = 1 day**

(METHODOLOGY: pH Meter)

PROJECT NAME: Site 2705191, Oakland  
 PROJECT NO: I42705191

SAMPLE ID.	DEPTH, ft.	ANALYSIS DATE	ANALYSIS TIME	ROOM TEMP. °F	SAMPLE MATRIX	pH READING
1. Low OBC	N/A	20121211	1116	74	Water	8.34
2. High OBC	N/A	20121211	1116	74	Water	8.46

**QC DATA**

**Meter Model/Type:** Corning pH Meter 240

<b>METER CALIBRATION</b>	<b>Date/Time:</b> 20121211/1017
pH Buffer Standard 4.00	4.00
pH Buffer Standard 7.00	7.00
pH Buffer Standard 10.00	10.01

PTS File No: 42834  
 Client: Antea Group

**Reactor Groundwater + Reagent pH T = 2 days**

(METHODOLOGY: pH Meter)

PROJECT NAME: Site 2705191, Oakland  
 PROJECT NO: I42705191

SAMPLE ID.	DEPTH, ft.	ANALYSIS DATE	ANALYSIS TIME	ROOM TEMP. °F	SAMPLE MATRIX	pH READING
1. Low OBC	N/A	20121212	1113	75	Water	8.16
2. High OBC	N/A	20121212	1115	75	Water	8.08

**QC DATA**

**Meter Model/Type:** Corning pH Meter 240

<b>METER CALIBRATION</b>	Date/Time:	20121212/1038
pH Buffer Standard 4.00		4.00
pH Buffer Standard 7.00		7.00
pH Buffer Standard 10.00		10.01

PTS File No: 42834  
 Client: Antea Group

**Reactor Groundwater + Reagent pH T = 4 days**

(METHODOLOGY: pH Meter)

PROJECT NAME: Site 2705191, Oakland  
 PROJECT NO: I42705191

SAMPLE ID.	DEPTH, ft.	ANALYSIS DATE	ANALYSIS TIME	ROOM TEMP. °F	SAMPLE MATRIX	pH READING
1. Low OBC	N/A	20121214	1115	73	Water	8.25
2. High OBC	N/A	20121214	1118	73	Water	8.15

**QC DATA**

**Meter Model/Type:** Corning pH Meter 240

<b>METER CALIBRATION</b>	Date/Time:	20121214/1050
pH Buffer Standard 4.00		4.00
pH Buffer Standard 7.00		7.00
pH Buffer Standard 10.00		10.01

PTS File No: 42834  
 Client: Antea Group

**Reactor Groundwater + Reagent pH T = 7 days**

(METHODOLOGY: pH Meter)

PROJECT NAME: Site 2705191, Oakland  
 PROJECT NO: I42705191

SAMPLE ID.	DEPTH, ft.	ANALYSIS DATE	ANALYSIS TIME	ROOM TEMP. °F	SAMPLE MATRIX	pH READING
1. Low OBC	N/A	20121217	1115	74	Water	8.38
2. High OBC	N/A	20121217	1116	74	Water	8.00

**QC DATA**

**Meter Model/Type:** Corning pH Meter 240

METER CALIBRATION	Date/Time:	20121217/1049
pH Buffer Standard 4.00		4.00
pH Buffer Standard 7.00		7.00
pH Buffer Standard 10.00		10.01

PTS File No: 42834  
 Client: Antea Group

**Reactor Groundwater + Reagent pH T = 10 days**

(METHODOLOGY: pH Meter)

PROJECT NAME: Site 2705191, Oakland  
 PROJECT NO: I42705191

SAMPLE ID.	DEPTH, ft.	ANALYSIS DATE	ANALYSIS TIME	ROOM TEMP. °F	SAMPLE MATRIX	pH READING
1. Low OBC	N/A	20121220	1114	71	Water	8.25
2. High OBC	N/A	20121220	1116	71	Water	7.96

**QC DATA**

**Meter Model/Type:** Corning pH Meter 240

<b>METER CALIBRATION</b>	<b>Date/Time:</b> 20121220/1015
pH Buffer Standard 4.00	4.00
pH Buffer Standard 7.00	7.00
pH Buffer Standard 10.00	10.01

PTS File No: 42834  
 Client: Antea Group

**Reactor Groundwater + Reagent pH T = 16 days**

(METHODOLOGY: pH Meter)

PROJECT NAME: Site 2705191, Oakland  
 PROJECT NO: I42705191

SAMPLE ID.	DEPTH, ft.	ANALYSIS DATE	ANALYSIS TIME	ROOM TEMP. °F	SAMPLE MATRIX	pH READING
1. Low OBC	N/A	20121226	1031	71	Water	8.38
2. High OBC	N/A	20121226	1033	71	Water	7.67

**QC DATA**

**Meter Model/Type:** Corning pH Meter 240

METER CALIBRATION	Date/Time:	20121226/0929
pH Buffer Standard 4.00		4.00
pH Buffer Standard 7.00		7.00
pH Buffer Standard 10.00		10.01



PTS File No: 42834  
 Client: Antea Group

**Reactor Groundwater + Reagent pH T = 21 days**

(METHODOLOGY: pH Meter)

PROJECT NAME: Site 2705191, Oakland  
 PROJECT NO: I42705191

SAMPLE ID.	DEPTH, ft.	ANALYSIS DATE	ANALYSIS TIME	ROOM TEMP. °F	SAMPLE MATRIX	pH READING
1. Low OBC	N/A	20121231	0823	70	Water	8.33
2. High OBC	N/A	20121231	0825	70	Water	7.58

**QC DATA**

**Meter Model/Type:** Corning pH Meter 240

METER CALIBRATION	Date/Time: 20121231/0815
pH Buffer Standard 4.00	4.00
pH Buffer Standard 7.00	7.00
pH Buffer Standard 10.00	10.01

PTS File No: 42834  
 Client: Antea Group

**Reactor Groundwater + Reagent pH T = 28 days**

(METHODOLOGY: pH Meter)

PROJECT NAME: Site 2705191, Oakland  
 PROJECT NO: I42705191

SAMPLE ID.	DEPTH, ft.	ANALYSIS DATE	ANALYSIS TIME	ROOM TEMP. °F	SAMPLE MATRIX	pH READING
1. Low OBC	N/A	20130107	0755	71	Water	8.25
2. High OBC	N/A	20130107	0800	71	Water	7.51

**QC DATA**

**Meter Model/Type:** Corning pH Meter 240

METER CALIBRATION	Date/Time:	20130107/0749
pH Buffer Standard 4.00		4.00
pH Buffer Standard 7.00		7.00
pH Buffer Standard 10.00		10.01

PTS File No: 42834  
 Client: Antea Group

**PTS Laboratories**  
 Project Name: Site 2705191, Oakland  
 Project No. 142705191

**RESIDUAL PERSULFATE BY TITRATION T = 28 days**  
 (Based on FMC Adventus Klozur™ procedure)

**LABORATORY PROCEDURE**

About 50 mL 1.0N H<sub>2</sub>SO<sub>4</sub> was reacted with 40 mL 0.5N Ferrous Ammonium Sulfate and 10 mL groundwater.  
 Solution mixture is let stand for 1 minute.  
 Solution titrated with a 0.5N Ce(SO<sub>4</sub>)<sub>2</sub> solution to a ferroin indicator endpoint.  
 Final persulfate concentration determined using equation: (A-B)\*C\*119/D  
 TOD determined using equation: TOD(g/kg)= (Co - Cf) \* V / M

Sample ID	TECH. INITIALS	DATE/TIME	VOLUME OF Ce(SO <sub>4</sub> ) <sub>2</sub> FOR TITRATING BLANK mL [A]	VOLUME OF Ce(SO <sub>4</sub> ) <sub>2</sub> FOR TITRATING SAMPLE mL [B]	NORMALITY OF Ce(SO <sub>4</sub> ) <sub>2</sub> USED, N [C]	VOLUME OF SAMPLE mL [D]	INITIAL OBC® g/L	INITIAL PERSULFATE g/L	FINAL PERSULFATE g/L	VOLUME OF GROUNDWATER, L	MASS OF SOIL, g	TOD, g/Kg
1. Low OBC	JS	20130107/1126	43.85	43.79	0.5	10	8.0	6.4	0.4	0.5	250.15	12.1
2. High OBC	JS	20130107/1126	43.85	43.37	0.5	10	15.0	12.0	2.9	0.5	250.03	18.3

Initial Persulfate concentration calculated as 80% of Initial OBC® concentration based on client specified composition of OBC®

Observations or deviations from method: \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_

Lab Supervisor/PM: MMB/20130107  
 Initial/Date

# CHAIN-OF-CUSTODY / Analytical Request Document

The Chain-of-Custody is a LEGAL DOCUMENT. All relevant fields must be completed accurately.

42834

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<b>Section A</b> Required Client Information:		<b>Section B</b> Required Project Information:		<b>Section C</b> Invoice Information:	
Company: Antea Group		Report To: Dennis Dettloff		Attention: Dennis Dettloff	
Address: 1105 White Rock Road		Copy To: Ed Weyrens		Company Name: Antea Group	
Suite 110, Rancho Cordova, CA 95670		ed.weyrens@anteagroup.com		Address: 11050 White Rock Road Suite 110	
Email To: dennis.dettloff@anteagroup.com		Purchase Order No.		Rancho Cordova, CA 95671	
Phone: 916-503-1261		Client Project ID: 142705191		Regulatory Agency: Alameda County	
Requested Due Date/TAT: 10 Day (Default)		Container Order Number:		State/Location: CA/Oakland	

ITEM#	SAMPLE ID One Character per box. (A-Z, 0-9 /, -) Sample IDs must be unique	FIELD POINT NAME	MATRIX CODE (see valid codes to left)	SAMPLE TYPE (G=GRAB C=COMPI)	COLLECTED				SAMPLE TEMP AT COLLECTION	# OF CONTAINERS	Preservatives							TOD residual persulfate test	Residual Chlorine (Y/N)	Requested/Analysis/Filtered (Y/N)							
					START DATE	START TIME	END DATE	END TIME			Unpreserved	H2SO4	HNO3	HCl	NaOH	Na2S2O3	Methanol				Other						
1	HA-1d	S	SL	G	11/15/2012	11:45			10	X																	
2	MW-14		WT	G	11/15/2012	12:30			4	X																	
3																											
4																											
5																											
6																											
7																											
8																											
9																											
10																											
11																											
12																											

ADDITIONAL COMMENTS	RELINQUISHED BY/AFFILIATION	DATE	TIME	ACCEPTED BY/AFFILIATION	DATE	TIME	SAMPLE CONDITIONS			
MW-14 to be used with HA-1d	<i>[Signature]</i> Antecubay	11/15/12	15:00	<i>[Signature]</i> PTS LABS	11/16/12	1340	49.9	Y	N	Y

SAMPLER NAME AND SIGNATURE		TEMP IN C	Received on Ice (Y/N)	Custody Sealed Cooler (Y/N)	Samples Intact (Y/N)
PRINT Name of SAMPLER:	<i>Ed Weyrens</i>				
SIGNATURE of SAMPLER:	<i>[Signature]</i>	DATE Signed:	11-15-12		

*Remedial Action Plan  
76 Service Station No. 5191/5043  
449 Hegenberger Road  
Oakland, California  
Antea Group Project No. I42705191*



## ***Appendix C***

Soil Boring Logs

## BORING LOG

<b>Project No.</b> KEI-P91-1004	<b>Boring Diameter</b> 9"	<b>Logged By</b> <i>JGG</i> D.L. <i>CEG 1653</i>
	<b>Casing Diameter</b> 2"	
<b>Project Name</b> Unocal S/S #5043 449 Hegenberger Rd., Oakland	<b>Well Cover Elevation</b>	<b>Date Drilled</b> 8/21/92
<b>Boring No.</b> MW6	<b>Drilling Method</b> Hollow-stem Auger	<b>Drilling Company</b> West Hazmat

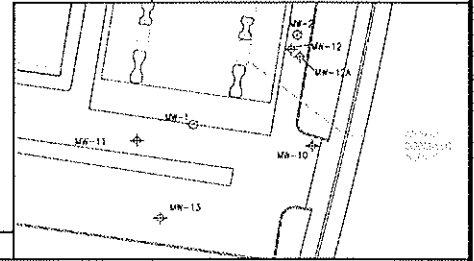
Penetration blows/6"	G. W. level	Depth (feet) Samples	Strati- graphy USCS	Description
		0		Asphalt pavement over sand and gravel base.
				Gravelly clay with sand, stiff, moist, black and olive gray, disturbed (fill).
3/4/4			CH	Clay with silt, stiff, moist, black (5Y 2.5/1) lensed with poorly graded and well graded sand.
4/5/7	▼	5	ML	Silt with very fine-grained sand, stiff, moist to wet, dark greenish gray (5GY 4/1), lensed with clayey silt between 4.5 and 5.5 feet.
3/3/4			OL	Clayey silt, stiff, moist, black (5Y 2.5/1) and very dark gray (5Y 3/1) mottled, with abundant organic matter (bay mud).
5/7/8		10	OH	Silty clay, stiff, moist, black (2.5YR 2.5/0), with abundant organic matter.
5/7/9			CH	Silty clay, stiff, moist, very dark gray (5Y 3/1), with organic matter.
				Silty clay, trace fine-grained sand, stiff, moist, dark greenish gray (5GY 4/1).
		15		TOTAL DEPTH 13.5'
		20		

# Delta Consultants

Project No: I42705191 Client: Delta/ELT  
 Logged By: Jonathan Fillingame Location: 449 Hegenberger Road, Oakland  
 Driller: Gregg Date Drilled: 6/22/2010  
 Drilling Method: Hollow Stem Auger Hole Diameter: 11"  
 Sampling Method: Direct Push Hole Depth: 20'  
 Casing Type: Sch 40 PVC Well Diameter: 4"  
 Slot Size: 0.020 Well Depth: 20'  
 Gravel Pack: #3 Monterey Sand ▽ First Water Depth: 5.5'  
 ▽ Static Water Depth: 4.5'

Well No: MW-12

Page 1 of 1



Elevation: Northing: Easting:

Well Completion	Water Level	Blow Counts	PID Reading (ppm)	Sample Identification	Depth (feet)	Recovery	Analyzed	Soil Type	LITHOLOGY / DESCRIPTION
Backfill Casing									
Neat Cement				Air-Knife	1				4" Asphalt
					2				<b>Fill (Silty SAND with Gravel)</b> ; brown, 60% fine to coarse sand, 20% silt, 20% fine to coarse gravel, chunks of asphalt, damp.
					3				<b>Lean CLAY (CL)</b> ; dark greenish grey, 95% clay, medium stiff, medium plasticity, 5% fine sand, moist.
					4				<b>Lean CLAY (CL)</b> ; dark brownish grey and black, 90% clay, stiff, medium plasticity, 5% fine sand, 5% organics/roots, moist, hydrocarbon odor.
			32.9		5				<b>Lean CLAY with Gravel (CL)</b> ; dark brownish grey, 80% clay, stiff, low plasticity, 20% fine gravel,
					6				<b>Clayey GRAVEL (GC)</b> ; dark brown, 50% fine gravel, loose, 40% clay, low plasticity, 10% fine to coarse sand, moist.
				MW-12 @8	8				
				MW-12 @10	10				<b>Lean CLAY (CL)</b> ; dark grey to black, soft, medium plasticity, wet, hydrocarbon odor.
			203		11				
					12				
					13				
					14				<b>Lean CLAY with Sand (CL)</b> ; green grey, 85% clay, stiff, medium plasticity, 15% fine to medium sand, moist.
			160		15				Color Change to Brown.
					16				<b>Fat CLAY (CH)</b> ; black, very soft, high plasticity, wet.
					17				<b>Fat CLAY (CH)</b> ; greenish grey, 90% clay, soft, high plasticity, 10% fine sand, moist.
					18				
				MW-12 @20	19				<b>Lean CLAY (CL)</b> ; brown with black spots, very stiff, medium plasticity, damp.
			335		20				
					21				
					22				

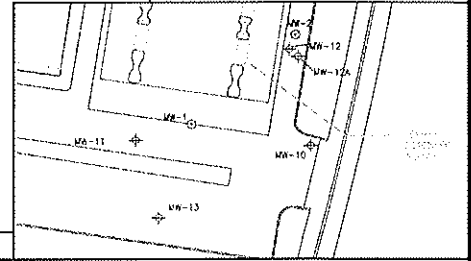


# Delta Consultants

Project No: I42705191 Client: Delta/ELT  
 Logged By: Jonathan Fillingame Location: 449 Hegenberger Road, Oakland  
 Driller: Gregg Date Drilled: 6/23/2010  
 Drilling Method: Hollow Stem Auger Hole Diameter: 8"  
 Sampling Method: Direct Push Hole Depth: 44'  
 Casing Type: Sch 40 PVC Well Diameter: 2"  
 Slot Size: 0.020 Well Depth: 34'  
 Gravel Pack: #3 Monterey Sand ▽ First Water Depth: 5.5'  
 ▽ Static Water Depth: 6'

Well No: MW-12A

Page 1 of 2



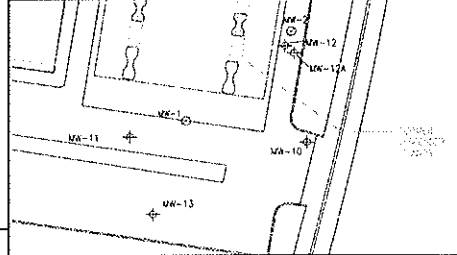
Elevation: Northing: Easting:

Well Completion		Water Level	Blow Counts	PID Reading (ppm)	Sample Identification	Depth (feet)	Recovery	Analyzed	Soil Type	LITHOLOGY / DESCRIPTION
Backfill	Casing									
Neat Cement					Air-Knife	1				4" Asphalt
						2				<b>Fill (Silty SAND with Gravel)</b> ; brown, 60% fine to coarse sand, 20% silt, 20% fine to coarse gravel, chunks of asphalt, damp.
						3				<b>Lean CLAY (CL)</b> ; dark greenish grey, 95% clay, medium stiff, medium plasticity, 5% fine sand, moist.
						4				<b>Lean CLAY (CL)</b> ; dark brownish grey and black, 90% clay, stiff, medium plasticity, 5% fine sand, 5% organics/roots, moist, hydrocarbon odor.
		▽		32.9		5				<b>Lean CLAY with Gravel (CL)</b> ; dark brownish grey, 80% clay, stiff, low plasticity, 20% fine gravel,
		▽				6				<b>Clayey GRAVEL (GC)</b> ; dark brown, 50% fine gravel, loose, 40% clay, low plasticity, 10% fine to coarse sand, moist.
						7				
						8				
				2365		9				
						10				<b>Lean CLAY (CL)</b> ; dark grey to black, soft, medium plasticity, wet, hydrocarbon odor.
						11				
						12				
				203		13				
						14				<b>Lean CLAY with Sand (CL)</b> ; green grey, 85% clay, stiff, medium plasticity, 15% fine to medium sand, moist.
						15				Color Change to Brown.
				160		16				<b>Fat CLAY (CH)</b> ; black, very soft, high plasticity, wet.
						17				<b>Fat CLAY (CH)</b> ; greenish grey, 90% clay, soft, high plasticity, 10% fine sand, moist.
						18				
						19				<b>Lean CLAY (CL)</b> ; brown with black spots, very stiff, medium plasticity, damp.
				335		20				No Recovery
						21				
						22				

# Delta Consultants

Project No: I42705191 Client: Delta/ELT  
 Logged By: Jonathan Fillingame Location: 449 Hegenberger Road, Oakland  
 Driller: Gregg Date Drilled: 6/23/2010  
 Drilling Method: Hollow Stem Auger Hole Diameter: 8"  
 Sampling Method: Direct Push Hole Depth: 44'  
 Casing Type: Sch 40 PVC Well Diameter: 2"  
 Slot Size: 0.020 Well Depth: 34'  
 Gravel Pack: #3 Monterey Sand First Water Depth: 5.5'  
 Static Water Depth: 6'

Well No: MW-12A  
 Page 2 of 2



Elevation: Northing: Easting:

Well Completion	Water Level	Blow Counts	PID Reading (ppm)	Sample Identification	Depth (feet)	Recovery	Analyzed	Soil Type	LITHOLOGY / DESCRIPTION
Neat Cement					23				No recovery
			1277	MW-12A @26	24				
					25				
					26				<b>Fat CLAY (CH)</b> ; black, soft, high plasticity, wet, hydrocarbon odor.
					27				
					28				<b>Lean CLAY (CL)</b> ; brown, greenish grey, 90% clay, stiff, medium plasticity, 10% fine to coarse sand, moist.
					29				
			3400	MW-12A @32	30				
					31				<b>Sandy Lean CLAY (CL)</b> ; brown, 70% clay, stiff, medium plasticity, 30% fine to coarse sand, moist.
					32				
			47.9	MW-12A @34	33				<b>Clayey SAND (SC)</b> ; brown, 60% fine to medium sand, loose, 40% clay, stiff, medium plasticity, wet.
					34				<b>Well Graded SAND with Clay (SW-SC)</b> ; brown, 90% fine to coarse sand, dense, 10% clay, wet.
					35				
					36				<b>Clayey SAND (SC)</b> ; brown, 60% fine to medium sand, 40% clay, wet.
					37				<b>Well Graded SAND (SW)</b> ; brown, fine to coarse, wet.
					38				<b>Well Graded SAND (SW)</b> ; brown, 90% medium to coarse sand, loose, 10% fine gravel, wet.
					39				<b>Well Graded SAND (SW)</b> ; brown, 95% fine to coarse sand, loose, 5% clay, wet.
					40				<b>Well Graded SAND (SW)</b> ; brown, 95% fine to coarse sand, loose, 5% clay, wet.
					41				<b>Well Graded SAND (SW)</b> ; brown, 95% fine to coarse sand, loose, 5% fine gravel, wet.
					42				
					43				<b>Clayey SAND (SC)</b> ; brown, 60% fine to medium sand, loose, 40% clay, wet.
					44				

Sand Caved in while Augers were removed (slough)

**Remedial Action Plan**  
**76 Service Station No. 5191/5043**  
**449 Hegenberger Road**  
**Oakland, California**  
**Antea Group Project No. I42705191**



## **Appendix D**

Regenesis ORC Advanced® Material Safety and Data Sheet

Oxygen Release Compound – Advanced (ORC *Advanced*<sup>TM</sup>)  
MATERIAL SAFETY DATA SHEET (MSDS)

Last Revised: June 24, 2010

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Section 1 - Material Identification

---

Supplier:



**REGENESIS**

1011 Calle Sombra  
San Clemente, CA 92673

Phone: 949.366.8000

Fax: 949.366.8090

E-mail: [info@regenesis.com](mailto:info@regenesis.com)

**Chemical Description:** A mixture of Calcium OxyHydroxide [CaO(OH)<sub>2</sub>] and Calcium Hydroxide [Ca(OH)<sub>2</sub>].

**Chemical Family:** Inorganic Chemical

**Trade Name:** Advanced Formula Oxygen Release Compound  
(ORC *Advanced*<sup>TM</sup>)

**Chemical Synonyms** Calcium Hydroxide Oxide; Calcium Oxide Peroxide

**Product Use:** Used to remediate contaminated soil and groundwater (environmental applications)

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Section 2 – Composition

---

<u>CAS No.</u>	<u>Chemical</u>
682334-66-3	Calcium Hydroxide Oxide [CaO(OH) <sub>2</sub> ]
1305-62-0	Calcium Hydroxide [Ca(OH) <sub>2</sub> ]
7758-11-4	Dipotassium Phosphate (HK <sub>2</sub> O <sub>4</sub> P)
7778-77-0	Monopotassium Phosphate (H <sub>2</sub> KO <sub>4</sub> P)

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**Section 3 – Physical Data**

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<b>Form:</b>	Powder
<b>Color:</b>	White to Pale Yellow
<b>Odor:</b>	Odorless
<b>Melting Point:</b>	527 °F (275 °C) – Decomposes
<b>Boiling Point:</b>	Not Applicable (NA)
<b>Flammability/Flash Point:</b>	NA
<b>Auto- Flammability:</b>	NA
<b>Vapor Pressure:</b>	NA
<b>Self-Ignition Temperature:</b>	NA
<b>Thermal Decomposition:</b>	527 °F (275 °C) – Decomposes
<b>Bulk Density:</b>	0.5 – 0.65 g/ml (Loose Method)
<b>Solubility:</b>	1.65 g/L @ 68° F (20° C) for calcium hydroxide.
<b>Viscosity:</b>	NA
<b>pH:</b>	11-13 (saturated solution)
<b>Explosion Limits % by Volume:</b>	Non-explosive
<b>Hazardous Decomposition Products:</b>	Oxygen, Hydrogen Peroxide, Steam, and Heat
<b>Hazardous Reactions:</b>	None

---

**Section 4 – Reactivity Data**

---

**Stability:** Stable under certain conditions (see below).

**Conditions to Avoid:** Heat and moisture.

**Incompatibility:** Acids, bases, salts of heavy metals, reducing agents, and flammable substances.

**Hazardous Polymerization:** Does not occur.

---

**Section 5 – Regulations**

---

**TSCA Inventory List:** Listed

**CERCLA Hazardous Substance (40 CFR Part 302)**

**Listed Substance:** No

**Unlisted Substance:** Yes

**Reportable Quantity (RQ):** 100 pounds

**Characteristic(s):** Ignitibility

**RCRA Waste Number:** D001

**SARA, Title III, Sections 302/303 (40 CFR Part 355 – Emergency Planning and Notification)**

**Extremely Hazardous Substance:** No

**SARA, Title III, Sections 311/312 (40 CFR Part 370 – Hazardous Chemical Reporting: Community Right-To-Know)**

**Hazard Category:** Immediate Health Hazard  
Fire Hazard

**Threshold Planning Quantity:** 10,000 pounds

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**Section 5 – Regulations (cont)**

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**SARA, Title III, Section 313 (40 CFR Part 372 – Toxic Chemical Release Reporting: Community Right-To-Know**

**Extremely Hazardous Substance:**

No

**WHMIS Classification:**

C

Oxidizing Material  
Poisonous and Infectious  
Material

D

Material Causing Other Toxic  
Effects –  
Eye and Skin Irritant

**Canadian Domestic Substance List:**

Not Listed

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**Section 6 – Protective Measures, Storage and Handling**

---

**Technical Protective Measures**

**Storage:**

Keep in tightly closed container. Store in dry area, protected from heat sources and direct sunlight.

**Handling:**

Clean and dry processing pipes and equipment before operation. Never return unused product to the storage container. Keep away from incompatible products. Containers and equipment used to handle this product should be used exclusively for this material. Avoid contact with water or humidity.



**Section 6 – Protective Measures, Storage and Handling (cont)**

---

**Personal Protective Equipment (PPE)**

Calcium Hydroxide

ACGIH® TLV® (2000)

5 mg/m<sup>3</sup> TWA

OSHA PEL

**Engineering Controls:**

Total dust–15 mg/m<sup>3</sup> TWA

Respirable fraction–

5 mg/m<sup>3</sup> TWA

NIOSH REL (1994)

5 mg/m<sup>3</sup>

**Respiratory Protection:**

For many conditions, no respiratory protection may be needed; however, in dusty or unknown atmospheres use a NIOSH approved dust respirator.

**Hand Protection:**

Impervious protective gloves made of nitrile, natural rubber or neoprene.

**Eye Protection:**

Use chemical safety goggles (dust proof).

**Skin Protection:**

For brief contact, few precautions other than clean clothing are needed. Full body clothing impervious to this material should be used during prolonged exposure.

**Other:**

Safety shower and eyewash stations should be present. Consultation with an industrial hygienist or safety manager for the selection of PPE suitable for working conditions is suggested.

**Industrial Hygiene:**

Avoid contact with skin and eyes.

**Protection Against Fire & Explosion:**

NA

---

**Section 7 – Hazards Identification**

---

**Emergency Overview:**

Oxidizer – Contact with combustibles may cause a fire. This material decomposes and releases oxygen in a fire. The additional oxygen may intensify the fire.

**Potential Health Effects:**

Irritating to the mucous membrane and eyes. If the product splashes in ones face and eyes, treat the eyes first. Do not dry soiled clothing close to an open flame or heat source. Any

## Regenesis - ORC Advanced MSDS

clothing that has been contaminated with this product should be submerged in water prior to drying.

- Inhalation:** High concentrations may cause slight nose and throat irritation with a cough. There is risk of sore throat and nose bleeds if one is exposed to this material for an extended period of time.
- Eye Contact:** Severe eye irritation with watering and redness. There is also the risk of serious and/or permanent eye lesions.
- Skin Contact:** Irritation may occur if one is exposed to this material for extended periods.
- Ingestion:** Irritation of the mouth and throat with nausea and vomiting.

---

### Section 8 – Measures in Case of Accidents and Fire

---

- After Spillage/Leakage/Gas Leakage:** Collect in suitable containers. Wash remainder with copious quantities of water.
- Extinguishing Media:** See next.
- Suitable:** Large quantities of water or water spray. In case of fire in close proximity, all means of extinguishing are acceptable.
- Further Information:** Self contained breathing apparatus or approved gas mask should be worn due to small particle size. Use extinguishing media appropriate for surrounding fire. Apply cooling water to sides of transport or storage vessels that are exposed to flames until the fire is extinguished. Do not approach hot vessels that contain this product.
- First Aid:** After contact with skin, wash immediately with plenty of water and soap. In case of contact with eyes, rinse immediately with plenty of water and seek medical attention. Consult an ophthalmologist in all cases.

---

### Section 8 – Measures in Case of Accidents and Fire

---

- Eye Contact:** Flush eyes with running water for 15 minutes, while keeping the eyelids wide open. Consult with an ophthalmologist in all cases.
- Inhalation:** Remove subject from dusty environment. Consult with a physician in case of respiratory symptoms.

## Regenesis - ORC Advanced MSDS

<b>Ingestion:</b>	If the victim is conscious, rinse mouth and administer fresh water. DO NOT induce vomiting. Consult a physician in all cases.
<b>Skin Contact:</b>	Wash affected skin with running water. Remove and clean clothing. Consult with a physician in case of persistent pain or redness.
<b>Special Precautions:</b>	Evacuate all non-essential personnel. Intervention should only be done by capable personnel that are trained and aware of the hazards associated with this product. When it is safe, unaffected product should be moved to safe area.
<b>Specific Hazards:</b>	<u>Oxidizing substance.</u> Oxygen released on exothermic decomposition may support combustion. Confined spaces and/or containers may be subject to increased pressure. If product comes into contact with flammables, fire or explosion may occur.

---

### Section 9 – Accidental Release Measures

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<b>Precautions:</b>	Observe the protection methods cited in Section 3. Avoid materials and products that are incompatible with product. Immediately notify the appropriate authorities in case of reportable discharge (> 100 lbs).
<b>Cleanup Methods:</b>	Collect the product with a suitable means of avoiding dust formation. All receiving equipment should be clean, vented, dry, labeled and made of material that this product is compatible with. Because of the contamination risk, the collected material should be kept in a safe isolated place. Use large quantities of water to clean the impacted area. See Section 12 for disposal methods.

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### Section 10 – Information on Toxicology

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#### Toxicity Data

<b>Acute Toxicity:</b>	Oral Route, LD <sub>50</sub> , rat, > 2,000 mg/kg (powder 50%) Dermal Route, LD <sub>50</sub> , rat, > 2,000 mg/kg (powder 50%) Inhalation, LD <sub>50</sub> , rat, > 5,000 mg/m <sup>3</sup> (powder 35%)
<b>Irritation:</b>	Rabbit (eyes), severe irritant

## Regenesis - ORC Advanced MSDS

<b>Sensitization:</b>	No data
<b>Chronic Toxicity:</b>	In vitro, no mutagenic effect (Powder 50%)
<b>Target Effects:</b>	<b>Organ</b> Eyes and respiratory passages.

---

### Section 11 – Information on Ecology

---

#### Ecology Data

	10 mg Ca(OH) <sub>2</sub> /L: pH = 9.0
	100 mg Ca(OH) <sub>2</sub> /L: pH = 10.6
<b>Acute Exotoxicity:</b>	Fishes, Cyprinus carpio, LC <sub>50</sub> , 48 hrs, 160 mg/L Crustaceans, Daphnia sp., EC <sub>50</sub> , 24 hours, 25.6 mg/L (Powder 16%)
<b>Mobility:</b>	Low Solubility and Mobility  Water – Slow Hydrolysis. Degradation Products: Calcium Hydroxide
<b>Abiotic Degradation:</b>	Water/soil – complexation/precipitation. Carbonates/sulfates present at environmental concentrations. Degradation products: carbonates/sulfates sparingly soluble
<b>Biotic Degradation:</b>	NA (inorganic compound)
<b>Potential for Bioaccumulation:</b>	NA (ionizable inorganic compound)

---

### Section 11 – Information on Ecology (cont)

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	Observed effects are related to alkaline properties of the product. Hazard for the environment is limited due to the product properties of:
<b>Comments:</b>	<ul style="list-style-type: none"><li>• No bioaccumulation</li><li>• Weak solubility and precipitation as carbonate or sulfate in an aquatic environment.</li></ul> Diluted product is rapidly neutralized at environmental pH.
<b>Further Information:</b>	NA

---

**Section 12 – Disposal Considerations**

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**Waste Disposal Method:** Consult current federal, state and local regulations regarding the proper disposal of this material and its emptied containers.

---

**Section 13 – Shipping/Transport Information**

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**D.O.T Name:** **Shipping** Oxidizing Solid, N.O.S [A mixture of Calcium OxyHydroxide [CaO(OH)<sub>2</sub>] and Calcium Hydroxide [Ca(OH)<sub>2</sub>].

**UN Number:** 1479

**Hazard Class:** 5.1

**Label(s):** 5.1 (Oxidizer)

**Packaging Group:** II

**STCC Number:** 4918717

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**Section 14 – Other Information**

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**HMIS<sup>®</sup> Rating** Health – 2 Reactivity – 1  
Flammability – 0 PPE - Required

HMIS<sup>®</sup> is a registered trademark of the National Painting and Coating Association.

**NFPA<sup>®</sup> Rating** Health – 2 Reactivity – 1  
Flammability – 0 OX

NFPA<sup>®</sup> is a registered trademark of the National Fire Protection Association.

**Reason for Issue:** Update toxicological and ecological data

---

**Section 15 – Further Information**

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**The information contained in this document is the best available to the supplier at the time of writing, but is provided without warranty of any kind. Some possible hazards have been determined by analogy to similar classes of material. The items in this document are subject to change and clarification as more information become available.**