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February 5, 2008

Mr. Jerry Wickham Alameda County Health Care Services Agency 1131 Harbor Bay Parkway, Suite 250 Alameda, California 94502-6577

Re: Site Conceptual Model and Feasibility Study/Corrective Action Plan

Former Shell Service Station 2703 Martin Luther King Jr. Way Oakland, California SAP Code 129449 Incident No. 97093397

Dear Mr. Wickham:

Conestoga-Rovers & Associates (CRA) prepared this report on behalf of Equilon Enterprises LLC dba. Shell Oil Products U.S. (Shell) for the above referenced site. Preparation of this *Site Conceptual Model* (SCM) and Feasibility Study/Corrective Action Plan (FS/CAP) was requested in a December 5, 2007 Alameda County Health Care Services Agency (ACHCSA) letter to Shell. This document was written to comply with California Code of Regulations, Title 23, Division 3, Chapter 16, Underground Storage Tank Regulations.

SITE DESCRIPTION AND BACKGROUND

The site is a former service station located on the northwest corner of Martin Luther King Jr. Way and 27th Street in a mixed commercial and residential area of Oakland, California (Figure 1). Currently, the site is occupied by Auto-Tech West and is utilized as an automotive repair shop.

A summary of previous work performed at the site and additional background information is contained in the SCM presented in Attachment A and discussed below.

SITE CONCEPTUAL MODEL

An SCM describes the relationship between the source area, transport pathways, and potential receptors. CRA developed the SCM for the subject site based on review of all available geological and analytical data. Supporting documents for the SCM include historical soil, groundwater, and soil vapor analytical tables, available boring and well logs for the site, cross sectional diagrams, sensitive receptor

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information, and a list of environmental reports for the subject site. These documents along with the SCM are presented in Appendix A. Some key findings of the SCM are listed below.

- The constituents of concern (COCs) for the site are total petroleum hydrocarbons as gasoline (TPHg), and benzene, toluene, ethylbenzene, and xylenes (BTEX). Fuel oxygenates are not considered to be COCs for the site.
- The highest gasoline constituent concentrations in soil, groundwater, and soil vapor have been detected near the former underground storage tanks (USTs), the adjacent former dispenser island, and along the western property boundary.
- Gasoline constituent concentrations in soil are defined vertically and laterally.
- Gasoline constituent concentrations in groundwater are defined vertically. Gasoline constituent concentrations in groundwater are defined horizontally except toward the northwest. Further investigation is planned. Overall BTEX concentrations have shown stable-to-decreasing trends
- BTEX concentrations in soil vapor in offsite probes are below applicable ESLs. Additional offsite soil vapor probe installations are planned.
- The site is underlain primarily by fine-grained soils. A coarser-grained lense is present at depths ranging from 10 to 25 feet below grade (fbg). Depth to groundwater has ranged from approximately 4 to 10 fbg. Groundwater flow direction ranges from west-northwest to southwest at a gradient of 0.01 to 0.02.
- Several shallow utility conduits have been identified beneath the site.
- Perched groundwater may be present in shallow utility conduits.
- No drinking water wells or surface water bodies are likely to be affected by site conditions.
- Based on the SCM analysis, there is no current link between sources-pathways-receptors for this site.

SITE GEOLOGY AND HYDROGEOLOGY

Soil Types: Cross sectional diagrams for the site are presented in the SCM in Attachment A. Soils encountered during previous subsurface investigations at the site have generally consisted of fine-grained soils (clays and silts). A coarser-grained lense may be present at approximately 10 to 25 feet below grade (fbg). The coarser-grained lense does not appear to extend beneath the site to the southeast (i.e. well boring MW-2) nor toward the southwest (i.e. borings CPT-6 and CPT-7), and it appears to thin northwest of the site (i.e. boring CPT-10). Additional non-continuous coarser-grained lenses are shown on cross sections for the site.

Groundwater Elevation and Gradient: Groundwater has been first encountered during drilling at the site at depths ranging from approximately 7 to 15 fbg. Depth to groundwater in site monitoring wells has



ranged historically from approximately 4 to 10 fbg. Based on this, groundwater may be semi-confined at the site.

Groundwater has also been encountered in shallow soil vapor probe screen intervals at the site even when no groundwater is encountered in deeper screen intervals in the same locations (i.e. SVP-3 during May 2007), and when groundwater in nearby monitoring wells is deeper. This may be indicative of perched water along preferential pathways beneath the site.

Between 2000 to 2006, groundwater flow direction varied from southwest to east. Since the installation of offsite wells MW-12 and MW-14, groundwater flow direction has varied from west-northwest to southwest at a gradient between 0.01 and 0.02.

DISTRIBUTION OF PETROLEUM HYDROCARBONS

Petroleum Hydrocarbon Distribution in Soil: Historical soil analytical data is included in the SCM in Attachment A, and total petroleum hydrocarbons as gasoline (TPHg) and benzene concentrations are shown on the cross sections presented in the SCM.

Most soil samples have been collected from below the typical static groundwater table at the site, and may be more indicative of groundwater conditions. TPHg and benzene concentrations have been highest in soil samples collected near the former USTs, the adjacent dispenser island, and along the western property boundary. TPHg and benzene are defined horizontally and vertically at the site.

Fuel oxygenates have not typically been detected in soil at the site.

Petroleum Hydrocarbon Distribution in Groundwater: Historical groundwater analytical data are included in the SCM in Attachment A, and TPHg and benzene concentrations are shown on the cross sections presented in the SCM.

Separate-phase hydrocarbons (SPH) were reported in soil borings B-1, B-5, B-6, and B-9 during the 1995 investigation. No SPH was reported during the 2000 investigation in soil boring B-19, located in the vicinity of B-6 and B-9, however.

Gasoline constituent concentrations are typically below detection limits in wells MW-1, MW-2, MW-3, and MW-12, defining these constituents northeast, southeast, south, and north, respectively, of the former USTs and dispensers. Petroleum hydrocarbon concentrations were also near or below detection limits in the grab groundwater sample collected from boring CPT-6, drilled southwest of the site during 2007.

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Benzene, toluene, ethylbenzene, and xylenes (BTEX) concentrations are typically highest in onsite well MW-5. During the fourth quarter 2007, groundwater from well MW-5 contained 7,500 micrograms per liter (μg/L) benzene. Benzene concentrations in onsite wells MW-4, MW-6, MW-7, MW-8, and V-2, located near the former USTs and along the western property boundary, ranged from 850 μg/L to 4,800 μg/L during the fourth quarter 2007. Well V-1 is screened within the clean backfill of the former UST pit, and BTEX concentrations in this well have been low since 1997. Offsite well MW-14 contained 1,600 μg/L benzene during the fourth quarter 2007, and the shallow groundwater sample from boring CPT-10, drilled northwest of the site during 2007 containing 1,600 μg/L benzene, indicated BTEX is undefined northwest of the site. Further investigation is planned.

Deeper groundwater samples were collected from depths between 31 and 37 fbg from onsite borings CPT-1 through CPT-5, and offsite boring CPT-10. Groundwater analytical results indicate significant attenuation of contaminant concentrations with depth. Based on this, no further vertical assessment is warranted.

Methyl tertiary butyl ether (MTBE) has rarely been detected in site wells. Shell ceased operation of the fuel system at the site during 1979, prior to the addition of oxygenates in their fuel. The fuel oxygenates disopropyl ether and tertiary butyl alcohol have been intermittently detected in groundwater at the site, and may be indicative of a secondary source not associated with Shell's operation of the site.

Petroleum Hydrocarbon Distribution in Soil Vapor: Historical soil vapor analytical data is included in the SCM in Attachment A.

Soil vapor samples were collected from soil borings GP-1 through GP-10 during the 2005 investigation. Several on- and offsite permanent soil vapor probes (VP-1 through VP-8) were subsequently installed during 2006 and 2007. Initial soil vapor sampling conducted during May and June 2007 from the soil probes indicated that petroleum hydrocarbon concentrations exceed applicable Environmental Screening Levels (ESLs) in soil vapor onsite. Offsite soil vapor concentrations did not exceed applicable ESLs. During October 2007, additional soil vapor samples were collected from the offsite soil vapor probes, and concentrations were lower than the initial sampling, and BTEX concentrations were still below applicable ESLs. The detection limits for TPHg in the soil vapor samples collected exceeds the November 2007 updated ESL for a residential scenario. The residential ESL for TPHg was updated to 10,000 micrograms per cubic meter (µg/m³) from 26,000 µg/m³. Quarterly monitoring of the offsite soil vapor probes is currently being conducted, and additional offsite soil vapor probe installations are planned.



TEIR I RBCA ANALYSIS

As a Tier 1 RBCA analysis, results of chemical analysis of soil, groundwater, and soil vapor samples were compared to published San Francisco Bay Regional Water Quality Control Board (RWQCB) ESLs for TPHg, and BTEX. The following tables present the maximum detected gasoline constituent concentrations in soil, and the most gasoline constituent concentrations in groundwater and soil vapor, and RWQCB ESLs (revised November 2007) for the COCs. While no drinking water wells have been identified in the vicinity of the site, ESLs were groundwater is a current or potential source of drinking water where used as a conservative comparison.

COC		Groundwater				
	Shallow Soil Concentration (a)	ESL (b)	Deep Soil Concentration (c)	ESL (d)	Groundwater Concentration (e)	ESL (b)
	mg/kg	mg/kg	mg/kg	mg/kg	µg/L	µg/L
TPHg	2,100	83	18,000	83	74,000	100
Benzene	1.8	0.044	100	0.044	7,500	1.0
Toluene	9.2	2.9	870	2.9	5,300	40
Ethylbenzene	91	3.3	370	3.3	3,000	30
Xylenes	230	2.3	2,000	2.3	20,400	2.3

Notes:

- (a) Concentrations in soil based on highest detections in shallow (less than 3 meters or 9.84 feet) soil samples.
- (b) ESLs are Table A Shallow Soil and Groundwater ESLs (Groundwater is a current or potential source of drinking water).
- (c) Concentrations in soil based on highest detections in deep (greater than 3 meters or 9.84 feet) soil samples.
- (d) ESLs are Table C Deep Soil and Groundwater ESLs (Groundwater is a current or potential source of drinking
- (e) Concentrations in groundwater based on highest detected during the fourth quarter 2007 sampling event.

Bold values exceed the ESL.



	Onsite Soil Vapor		Offsite Soil Vapor		
coc	Concentration (a)	ESLs (b)	Concentration (c)	ESLs (d)	
경기를 받고 있는데 보다. 있었음 (2012년 2월 1일	µg/m³	μg/m³	μg/m³	μg/m³	
TPHg	31,000,000	29,000	<24,000	10,000	
Benzene	760	280	<3.4	84	
Toluene	690	180,000	34	63,000	
Ethylbenzene	<690	580,000	<4.6	210,000	
Xylenes	<2,090	58,000	<22.6	21,000	

Notes:

- (a) Soil vapor concentrations based on highest detections in onsite soil vapor probes during May 2007.
- (b) ESLs are Table E-2 Shallow Soil Gas Screening Levels for Evaluation of Potential Vapor Intrusion Concerns (volatile chemicals only) Commercial/Industrial Land Use.
- (c) Concentrations in soil vapor based on highest detections in offsite soil vapor probes during October 2007.
- (d) ESLs are Table E-2 Shallow Soil Gas Screening Levels for Evaluation of Potential Vapor Intrusion Concerns (volatile chemicals only) Residential Land Use.

Bold values exceed the ESL.

Surface Soil: The highest COC concentrations detected in soil samples were found in samples collected in the vicinity of the former USTs, the adjacent former dispenser island, and along the western property boundary. TPHg, and BTEX concentrations were detected above the respective residential ESLs.

Groundwater: The highest concentrations from the fourth quarter 2007 sampling event were used for the Tier 1 RBCA analysis. TPHg and BTEX concentrations in groundwater are above the respective residential ESLs.

Soil Vapor: The highest onsite concentrations in soil vapor exceed the applicable commercial ESLs. The highest offsite concentrations in soil vapor do not exceed the applicable residential ESLs. The highest reporting limit for TPHg in offsite soil vapor samples does exceed the ESL, however.

CORRECTIVE ACTION PLAN (CAP)

Objectives

CAP cleanup objectives are based on one or more of the following criteria:

- ESLs established by the RWQCB's RBCA guidelines;
- Site Specific Target Levels established by conducting a Tier 2 RBCA evaluation;



- Current closure guidelines from the regulatory agencies, such as the California State Water Resources Control Board criteria for low-risk groundwater cases; or
- Application of Best Available Technology based on remediation system operation data that demonstrate asymptotic levels have been achieved for chemical concentrations in soil and/or groundwater.

Soil Clean-up Levels

For the purposes of this CAP, CRA assumes that the petroleum hydrocarbons detected in soil at the site may pose a risk to groundwater quality, human health, and/or the environment. Other than the Tier 1 RBCA evaluation, a detailed analysis of these potential risks has not yet been fully evaluated.

Although significant reductions in soil concentrations of COCs can be attained by various remedial alternatives, attainment of the approved soil cleanup levels may prove to be technically or economically infeasible. Thus, soil cleanup is limited to that which is technically or economically feasible.

To establish soil cleanup levels, CRA proposes using the RWQCB ESLs as the soil clean-up levels for this site. As described above, soil samples collected in the vicinity of the former USTs, the adjacent former dispenser island, and along the western property boundary exceed the respective ESLs for residential exposure.

Groundwater Clean-up Levels

According to the June 1999 East Bay Plain Groundwater Basin Beneficial Use Evaluation Report for Alameda and Contra Cost Counties, CA, groundwater in the area is an existing or probable drinking water resource, and the basin has depths ranging from 500 to over 1,000 feet. As noted in the SCM, no drinking water wells have been identified in the vicinity of the site, and impacted groundwater beneath the site appears limited to the shallow water-bearing zone.



Per the Basin Plan, however, groundwater cleanup goals will be established based on the following:

- Background concentrations of individual pollutants;
- Applicable water-quality objectives maximum contaminant levels (MCLs) to protect designated beneficial uses of the water body for drinking water;
- Concentrations which do not pose a significant risk to human health or the environment; and
- Technologic and economic feasibility.

To establish groundwater cleanup levels, CRA proposes using the RWQCB ESLs as the clean-up levels for this site. As described above, petroleum hydrocarbon concentrations exceed applicable ESLs in groundwater beneath the site.

Remedial Alternatives Discussion and Approach

The proposed remediation objectives in this CAP are based on a combination of the above criteria. The CAP objectives are to implement the most cost-effective remedial approach to protect human health, groundwater quality and other sensitive receptors. Given the specific site conditions, the specific CAP objectives are to:

- Remove hydrocarbons from the identified source areas;
- Mitigate further hydrocarbon impact to groundwater;
- Reduce potential risks to current and future site occupants;
- Continue the groundwater monitoring program to monitor water quality; and
- Establish a contingency plan to expedite or enhance remediation if necessary.

Remediation alternatives reviewed in this CAP address these five objectives. Once hydrocarbons are substantially removed or hydrocarbon levels are reduced, natural attenuation processes may remediate any residual hydrocarbons and restore the impact area(s) to background concentrations.

CRA evaluated several remedial alternatives to achieve site remedial objectives. Remedial alternatives were selected to address the TPHg and BTEX components of fuel hydrocarbons. Past and recent subsurface investigation activities indicated that elevated levels of TPHg and BTEX are present in subsurface soils and groundwater. MTBE and oxygenate concentrations have been reported near or below laboratory detection limits. The remedial technologies selected for evaluation include monitored natural attenuation, groundwater extraction, in-situ chemical oxidation, dual-phase extraction, and excavation. Each of these alternatives are discussed below and evaluated on the basis of technical feasibility and cost effectiveness.

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Remedial Alternatives

Monitored Natural Attenuation (MNA)

MNA consists of allowing hydrocarbons to biodegrade naturally and implementing a long-term groundwater monitoring plan. Decreasing concentration trends are the primary indicators of natural attenuation of hydrocarbons in groundwater. Secondary indicators such as dissolved oxygen (DO) concentrations, oxidation-reduction potential, alkalinity, and nitrate, sulfate, and ferrous iron concentrations are also used to evaluate the existence of and the potential for natural attenuation.

Feasibility and Cost-Effectiveness: MNA is typically a low-cost alternative if cleanup levels can be met within an acceptable timeframe. Given the current hydrocarbon concentrations in soil and groundwater, the timeframe to achieve cleanup levels by MNA is not reasonable.

Recommendation: CRA anticipates recommending MNA as a final remedial approach once active remediation is complete.

Groundwater Extraction (GWE)

Groundwater extraction (GWE) has historically been the most common remedial technology applied for groundwater restoration at service stations. Groundwater is extracted by down-well pumps and routed to a treatment system, such as activated carbon or an air stripper. The treatment system removes gasoline constituents from the extracted groundwater. The treated groundwater is typically discharged to the sanitary or storm sewer after treatment. GWE can also be used as an interim or temporary remediation measure. This approach can be cost effective when the majority of the source material has been removed and the extent of dissolved-phase groundwater impacts are limited. In this type of interim/temporary application, groundwater is pumped into a batch holding tank and periodically pumped into trucks for transportation to a treatment facility. Typically, 2 to 4 pore volumes are extracted to remove the remaining contaminant mass in groundwater.

In addition to dissolved-phase mass removal, GWE can provide hydraulic containment of the groundwater plume. Sufficient dewatering of the local formation can prevent contaminants from migrating with the natural groundwater flow. Source removal can only be achieved indirectly using GWE, as contaminants gradually desorb from soil (and/or residual NAPL) and enter the dissolved phase. The rate of desorption from soil is often the limiting factor for contaminant removal using GWE, especially as concentrations decline over time, and can compromise the cost-effectiveness of GWE before site cleanup goals are reached.

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Feasibility and Cost-Effectiveness: Design and installation of a GWE system would cost approximately \$150,000. This estimate is based on installation of 10 extraction wells, underground piping and utilities, a remediation compound, and treatment system. The annual GWE system operational cost is estimated at \$50,000, which includes \$10,000 for discharge of treated groundwater to the sanitary sewer. Assuming 15 years of GWE operation, the total operational cost would be \$750,000.

Annual groundwater monitoring is estimated at \$7,500. Assuming 15 years of groundwater monitoring during GWE system operation, and 3 years of groundwater monitoring following GWE to reach site cleanup goals, the total cost for groundwater monitoring is \$180,000. System demolition would cost approximately \$30,000, and the site closure request and well destructions would cost an estimated \$40,000. The total estimated cost for this alternative is \$1,150,000.

GWE would provide hydraulic control of dissolved-phase hydrocarbons, but would not directly or effectively remove source material. GWE would take a significantly long time to reach the remedial objectives, if at all.

Recommendation: Given that the primary constituents of concern are TPHg and BTEX, which are not effectively removed by GWE when source material is still present (and when mass is tied up in relatively low permeability soils), CRA does not recommend this remedial alternative.

In-Situ Chemical Oxidation (ISCO)

Injection of hydrogen peroxide can reduce hydrocarbon mass through in-situ chemical oxidation in two ways. In the presence of metals that are commonly found in the subsurface, the chemical reaction known as Fenton's Reagent produces a hydroxyl radical that is a strong oxidizer and ultimately oxidizes hydrocarbons to water and carbon dioxide. This reaction is strongly exothermic and results in increased soil and groundwater temperatures when used in-situ. Additionally, after introducing the solution into the subsurface, it also produces elevated dissolved oxygen concentrations in groundwater that can accelerate naturally occurring hydrocarbon biodegradation. The combination of chemical hydrocarbon oxidation within the treatment zone and enhanced biodegradation as dissolved oxygen migrates in groundwater away from the injection area can rapidly reduce hydrocarbon mass.

One method to apply hydrogen peroxide to a well would be to use a siphon pump and allow the hydrogen peroxide to infiltrate into the aquifer. Following the addition of the hydrogen peroxide, a slug of tap water would be added to the well to help facilitate hydrogen peroxide infiltration into the aquifer. The



amount of hydrogen peroxide and tap water added to each well would be based on the well diameter, depth to groundwater, water temperature, and soil permeability. Multiple applications are usually required. "Sentry" wells would be monitored for dissolved oxygen (DO) prior to initiating hydrogen peroxide injection to obtain background values. Once hydrogen peroxide injection is initiated, DO levels are monitored routinely in the treatment wells and sentry wells. Monitoring of bioparameters and petroleum constituent concentrations is conducted to determine the effectiveness of the hydrogen peroxide treatment.

Another method to apply hydrogen peroxide to the subsurface would be to install temporary, direct-push probes to the desired depth intervals instead of using permanent groundwater monitoring wells. The hydrogen peroxide can be injected into the probes using a pump to provide maximum infiltration of the solution into the subsurface.

Feasibility and Cost-Effectiveness: Implementation of hydrogen peroxide injection at the subject site using the direct push method would cost an estimated \$60,000. This estimate is based upon installation of 30 injection points (15 foot center spacing) and 5 observation wells. The existing monitoring wells would also be used as observation points. Each injection point would be injected with 15 gallons of a catalyst and 200 gallons of 10% H₂O₂ per event. CRA estimates up to five injection events. Each injection event is estimated to cost \$425,000.

Groundwater monitoring is estimated to cost approximately \$15,000 per year. Assuming 2.5 years of groundwater monitoring during hydrogen peroxide injection, and 2.5 years of groundwater monitoring following hydrogen peroxide injection to demonstrate that site cleanup goals will be met, the total cost for groundwater monitoring is \$75,000. The site closure request and well destructions would cost an estimated \$50,000. The total estimated cost for this alternative is \$610,000.

The effectiveness of hydrogen peroxide injection has been demonstrated in bench-scale studies and at various sites, but the reliability and costs for field applications remain uncertain when compared to other technologies. Given the soil heterogeneities at this site, which include very low permeable soils, it not likely that hydrogen peroxide could be effectively dispersed in the subsurface (hence the estimated 30 injection points, which may be an underestimate).

Recommendation: With the uncertainties regarding potential effectiveness and total overall cost, CRA does not recommend this remedial alternative.



Dual-Phase Extraction (DPE)

DPE is the process of applying high vacuum through an airtight well seal to simultaneously extract soil vapors from the vadose zone and groundwater from the saturated zone. The vacuum created by DPE can increase the groundwater yield from wells completed in low permeability formations. In addition, residual TPHg and BTEX in soil within the influence of the vacuum may be removed in the vapor phase. Groundwater extraction may provide hydraulic control of the hydrocarbon plume and reduce contaminant migration. Furthermore, extended dewatering of the saturated zone combined with vapor extraction can remediate residual hydrocarbons in the source area.

A positive displacement blower or liquid-ring pump may be used to create the higher vacuum needed to extract groundwater and soil vapors simultaneously. Alternatively, a submersible groundwater pump can be used to extract groundwater, while a blower or liquid-ring pump is used solely to extract soil vapors. The extraction device is supplemented with a soil vapor treatment (oxidizer or carbon adsorption) system. Extracted groundwater can be treated and discharged to the local sanitary sewer or storm drain with the appropriate authorization or off-hauled to a disposal facility.

Feasibility and Cost-Effectiveness: CRA conducted a DPE pilot test in date, which concluded that DPE is not technically feasible for the site conditions. Vacuum short-circuiting to the higher permeable soils occurred and the lower permeable soils did not yield sufficient air flow (<10 cubic feet per minute). Since DPE has been deemed infeasible, costing for implementation of DPE is not included.

Recommendation: DPE is not technically feasible for the site-specific hydrogeology; therefore, it is not recommended. DPE was included in this CAP to document the previous consideration of this remedial alternative.

Excavation

During excavation, contaminated soil is removed and transported to permitted off-site treatment and/or disposal facilities. In some cases, pre-treatment (via aeration, aboveground SVE, incineration, etc) of the contaminated media may be required in order to meet land disposal restrictions. Although excavation and off-site disposal alleviates the contaminant problem at the site, it does not treat the contaminant. The type of contaminant and its concentration level will impact off-site disposal requirements. The disposal of hazardous wastes is governed by the Resource Conservation and Recovery Act (RCRA) (40CFR Parts 261-265), and the U.S. Department of Transportation regulates the transport of hazardous materials (49 CFR Parts 172-179, 49 CFR Part 1387, and DOT-E 8876). Hazardous wastes must be treated to meet



either RCRA or non-RCRA treatment standards prior to land disposal. Transport and disposal of non-hazardous or special wastes are regulated by applicable California regulations.

Standard earth moving equipment (backhoes, bobcats, loaders, etc.) is typically utilized for excavation. Depending on available space, this range of equipment can excavate to a depth of approximately 20 feet. Larger earth moving equipment (excavators) can excavate slightly deeper. Entry into excavations deeper than 5 feet requires shoring per OSHA regulations. Deep excavations may require shoring to prevent collapse of the sidewalls and to prevent damage or undermining of neighboring structures, utilities, sidewalks, etc. Additionally, dewatering of the excavated area may be required depending on the groundwater elevation and recharge rates. The extent of excavation is typically estimated in advance using available soil boring data, but is ultimately directed by field personnel using field monitoring equipment such as a photo-ionization detector to screen soils by measurement of soil headspace vapor concentrations. Soil samples are collected for chemical analysis to confirm that the excavation limits are sufficient to meet soil cleanup levels.

Feasibility and Cost-Effectiveness: Implementation of excavation to a depth of 20 feet thoughout much of the western and west-central portion of the subject site is estimated to cost \$447,500. This estimate is based upon a 4-week period to complete excavation and restoration of the target area. The impacted soil is assumed to be non-hazardous waste. The estimated limits of feasible excavation are depicted in Figure 2, which equates approximately to 2,000 cubic yards or 3,000 tons. This cost includes engineering, permitting, monitoring well destruction and replacement, shoring, excavating, dewatering, stockpiling, profiling the soil for disposal, confirmatory sampling and analyses, loading, off-hauling, disposal, backfilling and compaction, site restoration, and project management and reporting.

The auto repair service would have to be closed during excavation activities, and the estimated costs of lost business are not known. The cost estimate does include well destruction and replacement since groundwater monitoring is assumed to be necessary following excavation. Groundwater monitoring is estimated to cost approximately \$7,500 per year, and would likely be necessary for 5 years at this site following excavation (mostly for off-site/downgradient groundwater monitoring). The closure request and well destructions are estimated to cost \$20,000. The total cost for this alternative is estimated to be \$505,000.

Recommendation: Through investigation and remediation activities to date, it has become apparent that there is remaining source material at this site that continues to leach into groundwater. Given the soil types and heterogeneities, excavation appears to be the only viable remedial alternative for reaching the site cleanup goals within a reasonable time. The table below presents a side-by-side comparison of the



remedial alternatives evaluated in this CAP. Excavation is the most cost-effective option. Therefore, CRA recommends implementing excavation at this site.

Remedial Alternative	MNA	GWE	ISCO	DPE	Excavation
Feasibility	Moderate	Moderate	Moderate	Poor	Good
Effectiveness	Poor	Poor	Unknown/ Poor	Poor	Good
Pilot Test Cost	NA	NA	NA	NA	NA
Design/Permit/Install Cost	NA	\$150,000	\$60,000	NA	\$447,500
Operational Duration	NA	15 years	5 events	NA	NA
Average Annual/Event Operational Cost	NA	\$50,000	\$85,000	NA	NA
Total Operational Cost	NA	\$750,000	\$425,000	NA	NA
Annual Groundwater Monitoring Cost	\$7,500	\$10,000	\$15,000	NA	\$7,500
Post-Remediation Groundwater Monitoring Duration	NA	3 years	2.5 years	NA	5 years
Total Groundwater Monitoring Duration	>50 yrs	18 years	5 years	NA	5 years
Total Groundwater Monitoring Cost	\$\$\$\$\$\$\$	\$180,000	\$75,000	NA	\$37,500
System Demo	NA	\$30,000	NA	NA	NA
Closure Request/Well Destructions	\$30,000	\$40,000	\$50,000	NA	\$20,000
Total Cost	>\$405,000	\$1,150,000	\$610,000	NA	\$505,000
Recommended Alternative					X

RECOMMENDATIONS

Based on the remedial objectives for this site, CRA recommends implementing excavation to protect future, potential receptors. Following excavation, CRA also recommends installation of a simple biosparge curtain to assist biodegradation of the downgradient dissolved-phase hydrocarbon plume. The



bio-sparge curtain would consist of a series on injection wells targeting the more permeable native soils at approximately 15 fbg, which is the most-likely migration pathway for dissolved-phase impacts. A standard air compressor would deliver air to these injection points. If ACHCSA agrees with this recommendation, then CRA will submit a Remedial Action Plan for the proposed work.

CLOSING

If you have any questions regarding the contents of this document, please call Jacquelyn L. England at (707) 933-2370.

Sincerely,

Conestoga-Rovers & Associates

Jacquelyn L. England Project Manager

Daniel N. Lescure, P.E.

Figures:

1 - Vicinity Map

2 - Proposed Excavation Limits

Attachment:

A - Site Conceptual Model

cc:

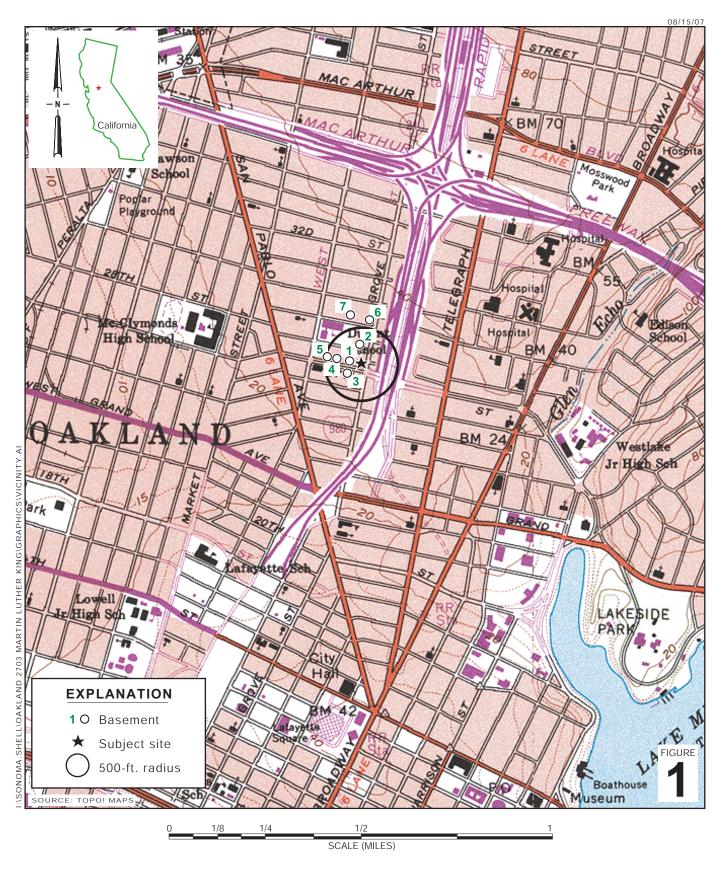
Denis Brown, Shell Oil Products US

Rodney & Janet Kwan, property owners of subject site Monique Oates, property owner at 670 27th Street in Oakland Scott Merillat, property owner at 664 27th Street in Oakland

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Conestoga-Rovers & Associates (CRA) prepared this document for use by our client and appropriate regulatory agencies. It is based partially on information available to CRA from outside sources and/or in the public domain, and partially on information supplied by CRA and its subcontractors. CRA makes no warranty or guarantee, expressed or implied, included or intended in this document, with respect to the accuracy of information obtained from these outside sources or the public domain, or any conclusions or recommendations based on information that was not independently verified by CRA. This document represents the best professional judgment of CRA. None of the work performed hereunder constitutes or shall be represented as a legal opinion of any kind or nature.

240781



Former Shell Service Station

2703 Martin Luther King Jr. Way Oakland, California



Vicinity Map

Former Shell Service Station 2703 Martin Luther King Jr Way Oakland, California



- **MW-12** Monitoring well location (2/06)
- **MW-6** Monitoring well location (1/06)
 - Monitoring well location (11/00)
- **MW-1** Monitoring well location (7/96)
- V-1 ▲ Soil vapor well location (7/96) (not used for contouring)

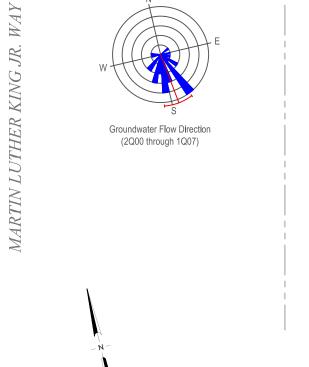


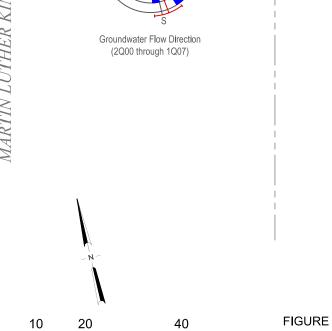
Proposed Excavation Limits Depth = 20 fbg

- -23.53 Groundwater elevation, in feet above msl
- (ND) TPHg concentration in µg/L (1,600)Benzene concentration in µg/L

Notes:

ND = Not detected NS = Not sampled





Scale (ft)

Vacant Lot 2727-29 Martin Luther King

● MW-1

21.65

(NA)

(NA)

former

dispensers

DRIVEWAY

● MW-2

19.90 (NA)

• MW-12 21.26

(ND) -(ND)

BUILDING

former

dispensers

MW-3 19.89

> $(NA)^{=}$ (NA)

A.G. W/O

AST,

former vent lines

TRENCH

▲ V-1 20:42

_ (1,300)

▲ V-2 20.40

(2,000)

(19)

Wooden Carport

anode (**) 20,40 -7 (42,000) 12 (4,900)

• MW-7 20.32

20.34 (61,000)-

(7,500)

(26,000)

(3,000)

former USTs

20.28

(7,000) (850)

● MW-4

20.30

(6,400)

(1,400)

GATE

DRIVEWAY

Basemap from Virgil Chavez Land Surveying and Alameda County Assessors Parcel Map

● MW-14

18.88

(32,000)

(1,600)

27TH STREET

Attachment A Site Conceptual Model

SITE CONCEPTUAL MODEL

Prepared by: CRA Date February 2008

Site Address:	2703 Martin Luther King Jr Way	Incident Number:	97093397
City, State:	Oakland, California	Regulatory Agency:	
	Cariana, Camorna	regulatory Agency.	Alameda County Health Care Services Agency
Item	Evaluation Criteria	Comments/Discussion	
1	Hydrocarbon Source	Comments/Discussion	
1.1	Identify/Describe Release Source	Unknown, Gasoline co	onstituents were detected in soil samples
	and Volume (if known)	collected following the tank (UST) during Octo	removal of a 2,000-gallon underground storage ober 1994. Separate-phase hydrocarbons (SPH) orings B-1, B-5 ,B-6, and B-9, drilled during 1995.
1.2	Discuss Steps Taken to Stop	1	ion was taken to stop the release as there was
	Release	tanks (USTs) were removerexcavated from 9 f	d equipment failure. The underground storage noved during 1994, and the UST pit was feet below grade (fbg) to approximately 11 fbg ckfilling with clean, imported fill material.
2	Site Characterization		The second secon
2.1	Current Site Use/Status	Martin Luther King Jr. V residential area of Oak on the property from an islands, three gasoline equipment was remove 1979, Acme West Ambinstalled a 2,000-gallon of Shell's former USTs. (ATW) in 1986, and the shop. ATW reportedly 1994, although an activ	rvice station located on the northwest corner of Way and 27th Street in a commercial and land, California. A Shell service station operated oproximately 1959 to 1979, with two dispenser USTs, and a waste oil UST. The fueling ed after Shell terminated operations at the site. In bulance Company purchased the site and a gasoline UST in the same approximate location. The property was sold to Auto-Tech West e site is currently used as an automotive repair never used the UST which was removed in we 150-gallon aboveground waste oil tank is northern-central portion of the property.
2.2	Soil Definition Status	groundwater table at the groundwater conditions highest in soil samples dispenser island, and a benzene concentration attenuation, non-detect measurements to the nation to the southwest by B-10 and	e been collected from below the typical static ne site, and may be more indicative of s. TPHg and benzene concentrations have been collected near the former USTs, the adjacent along the western property boundary. TPHg and is in soil are defined either by horizontal to concentrations, or non-detect PID north by MW-12, to the northeast by MW-1 and B-3-4 and MW-2, to the south by MW-3, to the I GP-1, and to the northwest by VP-8. Fuel ypically been detected in soil at the site.
2.3	Separate-Phase Hydrocarbon (SPH) Definition Status	investigation. No SPH	oil borings B-1, B-5, B-6, and B-9 during the 1995 was reported during the 2000 investigation in soil the vicinity of B-6 and B-9.

Itam	Evaluation Criteria	Comments/Discussion
Item		Comments/Discussion
2.4	Groundwater Definition Status	BTEX concentrations are typically below detection limits (DLs) in wells
ļ	(BTEX)	MW-1, MW-2, MW-3, and MW-12, defining these constituents
		northeast, southeast, south, and north, respectively, of the former USTs
ļ		and dispensers. BTEX concentrations were also below DLs in the grab
		gw sample collected from CPT-6, drilled southwest of the site during
		2007. BTEX concentrations are highest in onsite well MW-5. In the
		third quarter 2007, gw from well MW-5 contained 6,900 µg/L benzene.
	•	Benzene concentrations in onsite wells MW-4, MW-6, MW-7, MW-8,
		and V-2, located near the former USTs and along the western property
		boundary, ranged from 1,600 μg/L to 3,400 μg/L during the third quarter
·		2007. Well V-1 is screened within the clean backfill of the former UST
·		pit, and BTEX concentration in this well have been low since 1997.
		Offsite well MW-14 contained 1,000 µg/L benzene during the third
		quarter 2007, and the shallow gw sample from boring CPT-10, drilled
		northwest of the site during 2007, contained 1,600 μg/L benzene,
	,	indicating BTEX is undefined northwest of the site. Further investigation
		is planned.
2.4a	Vertical Groundwater Definition	Deeper groundwater samples were collected from depths between 31
	Status (BTEX)	and 37 fbg from onsite borings CPT-1 through CPT-5 and offsite boring
	, ,	CPT-10. Groundwater analytical results indicate significant attenuation
		of contaminant concentrations with depth. Based on this, no further
		vertical assessment is warranted.
2.5	BTEX Plume Stability and	BTEX concentrations in groundwater show a stable to slightly
	Concentration Trends	decreasing trend in onsite wells and in offsite well MW-14. BTEX
		concentrations have decreased several orders of magnitude in well V-1,
		installed within the clean backfill of the former UST pit.
2.6	Groundwater Definition Status	Shell ceased operation of the fuel system at the site during 1979, prior
	(MTBE)	to the addition of oxygenates in their fuel, and MTBE has rarely been
		detected in site wells. The fuel oxygenates diisopropyl ether and tertiary
		butyl alcohol have been intermittently detected in groundwater at the
		site, and may be indicative of a secondary source not associated with
	·	Shell's operation of the site. Fuel oxygenates are not considered to be
		contaminants of concern at the site.
2.7	MTBE Plume Stability and	Not applicable.
	Concentration Trends	••
2.8	Groundwater Flow Direction,	Depth to groundwater in site monitoring wells has ranged historically
	Depth Trends and Gradient	from approximately 4 to 10 fbg. Groundwater has also been
	Trends	encountered in shallow soil vapor probe screen intervals at the site even
		when no groundwater is encountered in deeper screen intervals in the
		same locations (i.e. SVP-3 during May 2007), and when groundwater in
		nearby monitoring wells is deeper. This may be indicative of perched
		water along preferential pathways. Groundwater has been first
		encountered during drilling at depths ranging from approximately 7 to 15
		fbg. Based on this, groundwater may be semi-confined at the site.
		Between 2000 to 2006, groundwater flow direction varied from
		southwest to east. Since the installation of offsite wells MW-12 and
,		MW-14, groundwater flow direction has varied from west-northwest to
1		southwest at a gradient between 0.01 and 0.02.
ı		1

Item	Evaluation Criteria	Comments/Discussion
	Stratigraphy and Hydrogeology	Comments/Discussion
2.9	Stratigraphy and Hydrogeology	Cross sectional diagrams were prepared for the site during 2003 and
		additional cross sectional diagrams were prepared during 2007. The
		site is generally underlain by fine-grained soils (clays and silts). A
		coarser-grained lense may be present at approximately 10 to 25 fbg.
		The coarser-grained lense does not appear to extend beneath the site
	·	to the southeast (see well boring log MW-2), nor to the southwest (see
		boring logs CPT-6 and CPT-7), and appears to thin northwest of the site
		(see boring log CPT-10). Additional non-continuous coarser-grained
		lenses are shown on cross sections for the site.
2.10	Preferential Pathways Analysis	Groundwater depth onsite has ranged historically from approximately 4
		to 10 fbg. Based on this, the sanitary and storm sewer systems in the
		vicinity, buried at depths ranging from 3.5 to 9 fbg, may encounter
		groundwater. Additional utility lines were identified in the northwest
		corner of the property during a geophysical survey conducted during
		2006, including a potential sewer line deeper than 4 fbg, an electrical
		line traced from the station building to the western property boundary,
-		and an unidentified utility traced from the northwest corner of the
		building to the southwest near MW-5 and toward MW-6. These utility
		corridors affect ability to perform vapor extraction as found during pilot
	<u> </u>	testing (January 2006).
2.11	Other Pertinent Issues - Soil	Several on- and offsite soil vapor probes have been installed. Initial
:	Vapor Sampling	sampling conducted during May and June 2007 indicate that gasoline
•		constituent concentrations exceed applicable ESLs in soil vapor onsite.
		Soil vapor samples collected in offsite probes do not exceed applicable
		ESLs. During October 2007, additional soil vapor samples were
		collected from the offsite soil vapor probes, and concentrations were
		lower than the intial sampling event, and still below applicable ESLs.
		Quarterly monitoring of the offsite soil vapor probes is currently being
		conducted. Additional offsite soil vapor probe installations are planned.
2.12	Other Pertinent Issues - Natural	Gasoline constituent concentrations in groundwater have been stable to
	Attenuation	slightly decreasing for several years, even though the primary sources
		(i.e. the fueling equipment and USTs) at the site have been removed.
		This may indicate that either natural biodegradation is not occurring at
		the site, or the rate of loading to groundwater from remaining impacted
		soil is equal or slightly less than the rate of natural attenuation.
		Additional indications of natural attenuation or biodegradation should be
		assessed at the site to determine which scenario is more likely.
3	Remediation Status	
3.1	Remedial Actions Taken	Oxygen releasing compounds (ORCs) were installed in wells V-1 and V-
		2 during the second quarter 2001 and removed during the fourth quarter
		2001, and in wells MW-5 and V-2 during the first quarter 2003, and
		replaced semi-annually until removal during the first quarter 2005.
		Additionally, during January 2006, a five-day dual-phase extraction
		(DPE) test was conducted using wells V-1, V-2, MW-4, MW-5, MW-6,
		MW-7, and MW-8, and a constant vacuum DPT test was conducted
		using well MW-6.
	Avec Developed at a d	-
3.2	Area Remediated	Wells V-1, V-2, MW-4, MW-5, MW-6, MW-7, and MW-8 have been
		used historically for remedial activities.

Item	Evaluation Criteria	Comments/Discussion
	Remediation Effectiveness	The DPE testing indicated the following: Low gasoline constituent concentrations in vapor detected in well V-1 indicate a lack of residual source material in the former UST pit. High gasoline constituent concentrations in vapor were detected in wells V-2, MW-5, and MW-8. Extraction flow rates varied across the site, indicating heterogeneities in the soils or preferential pathways. The highest vapor concentration areas did not yield an effective vapor extraction flow rate, and the lowest vapor concentrations areas yielded an effective vapor extraction rate. Based on these relationships, DPE is not considered feasible for the target areas of the site.
	Well and Sensitive Receptor Survey	
4.1	Designated Beneficial Water Use	According to the Basin Plan, the site is within the East Bay Plain basin. Existing beneficial uses of the East Bay Plain basin include municipal and domestic water supply, industrial service supply, industrial process supply, and agricultural water supply. The site falls within Zone A of the East Bay Plain basin, as defined in the June 1999 "East Bay Plain Groundwater Basin Beneficial Use Evaluation Report for Alameda and Contra Costa Counties, CA." Groundwater in Zone A is noted as an existing or probable drinking water resource, with a deep basin ranging from 500 to over 1,000 feet. As noted above, gasoline constituents in soil and groundwater are sufficiently defined verically.
4.2	Shallow Groundwater Use	Cambria reviewed Department of Water Resources (DWR) records during 2003, and no wells were identified within a 1/2-mile radius of the site. Cambria also completed a door-to-door survey of properties within 500-feet of the site during 2003 and within 300-feet of the site during 2006, and no wells were identified. Based on this, shallow groundwater is not used in the site vicinity.
	Deep Groundwater Use	No deep wells were identified within the 1/2-mile radius. Based on this, deep groundwater is not used in the site vicinity.
4.4	Well / Surface Water Survey Results	The nearest surface water body is Lake Merritt, located over 1/2-mile southeast of the site. No wells have been identified with a 1/2-mile radius of the site.
4.5	Likelihood of Impact to Wells	No wells have been identified with a 1/2-mile radius. Based on this, impact to wells is unlikely.
4.6	Likelihood of Impact to Surface Water	Based on the distance to the nearest surface water body and its crossgradient location, impact is unlikely.
5	Risk Assessment	
5.1	Site Conceptual Exposure Model (current and future uses)	The site is currently occupied by an automotive repair shop. The area surrounding the site is mixed commercial and residential. Future use of the parcel is assumed to be similar to current use. The automotive repair shop has open bays and threat of vapor intrusion is low.

Item	Evaluation Criteria	Comments/Discussion
5.2	Exposure Pathways	Potential exposure pathways include onsite commercial occupant inhalation of vapors from impacted soil and groundwater, dermal exposure, particle inhalation, and ingestion of impacted soil by onsite construction workers. As noted above, impact to drinking water wells and surface water bodies is considered unlikely, so direct exposure to groundwater is not considered a complete pathway. Potential vapor migration from impacted groundwater to offsite residential receptors is a complete pathway and is being monitored by vapor probes. To date, the concentrations in the offsite vapor probes are below residential ESLs for TPHg and BTEX. Monitoring and additional investigation are underway.
5.3	Human Health Risk Assessment Status	No formal risk assessment has been performed.
5.4	Ecological Risk Assessment Status	No ecological risk assessment has been performed.
5.5	Exceedances of Risk-Based Concentrations (Human Health)	Gasoline constituent concentrations in soil onsite exceed ESLs for TPHg, and BTEX. Groundwater concentrations in onsite wells MW-4, MW-5, MW-6, MW-7, MW-8, and V-2, and in offsite well MW-14 exceed ESLs for TPHg, and BTEX. Soil vapor concentrations in onsite probes VP-1, VP-2, VP-3, VP-4, and VP-6 exceed ESLs for indoor air for TPHg and benzene. None of these soil vapor probes are installed within the onsite building, however. Soil vapor concentrations in offsite probes VP-7 and VP-8 are below applicable ESLs.
5.6	Exceedances of Risk-Based Concentrations (Ecological)	No ecological risk assessment has been performed.
6 mg	Additional Recommended Data or Tasks	
	Task/Data	CRA has submitted a work plan (November 13, 2007) for additional offsite monitoring well and soil vapor probe installation to define gasoline constituents in groundwater and soil vapor offsite.
	Task/Data	CRA recommends assessing the presence of biodegraders in soil-vapors and groundwater beneath the site.
6.3	Task/Data	CRA recommends using recently released ESL guidance document and site soil vapor data to identify appropriate target cleanup goals for this site, and preparing the agency-requested corrective action plan to meet those goals.

Attachments

- 1 Site History
- 2 Historical Soil Sampling Results and Locations
- 3 Historical Groundwater Sampling Results
- 4 Available Boring and Well Logs
- 5 Cross Sectional Diagrams
- 6 Utility Maps
- 7 Historical Soil Vapor Sampling Results
- 8 Sensitive Receptor Survey/Well Location Map
- 9 List of Environmental Documents

ATTACHMENT 1

Site History

Former Shell Service Station 2703 Martin Luther King Jr. Drive Oakland, CA

PREVIOUS WORK

*## 1994 UST Removal: The 2,000-gallon UST was removed on October 11, 1994 by KTW & Associates on behalf of ATW. Two soil samples (TP-1-N and TP-2-S) were collected from beneath the tank. Chemical analysis of the soil samples identified the presence of total petroleum hydrocarbons as gasoline (TPHg) at concentrations ranging from 870 milligrams per kilogram (mg/kg) to 18,000 mg/kg. Benzene concentrations in these samples ranged from 2.9 to 100 mg/kg. The tank pit remained open until March 19, 1996 when the excavation was backfilled subsequent to over-excavation by a Shell contractor.

1995 Phase I Environmental Site Assessment (ESA): In August and September 1995, Enviros Inc. (Enviros) performed a Phase I ESA for this site. Available information collected during this ESA indicates that the subject property was occupied by residential housing prior to approximately 1959. A building permit to erect a building was obtained for Shell Oil Company in February 1959. A building permit to "close lube bays with sheet metal panels" was secured for Shell Oil Company in July 1976.

In 1979, several building permits were secured for Acme to modify existing site structures. Two building permits were secured in 1979 related to the installation of a fuel pump at the site.

During a site survey in conjunction with the Phase I ESA, an excavation was observed near the southwest corner of the service building. The excavation was covered by a blue tarp. This excavation's location is consistent with that of the 2,000-gallon UST removed in 1994 by ATW, and with a large concrete slab observed in aerial photographs taken in 1971 and 1973, and a smaller concrete slab observed in aerial photographs taken in 1981 and 1985. The larger concrete slab observed in the aerial photographs was likely covering the USTs operated by Shell, and the smaller slab was likely covering the UST operated by Acme, confirming that the same location was used for both UST complexes.

1995 Subsurface Investigation: A site assessment was performed by ACC Environmental Consultants on May 23, 1995. This included drilling nine soil borings (B-1 through B-9) using a pneumatic sampling tool in the vicinity of the excavation (which formerly housed both Shell's and Acme's USTs) and the product dispenser islands, and collecting soil and groundwater samples for chemical analysis. TPHg concentrations in soil samples ranged from <20.0 to 830 mg/kg. Benzene concentrations ranged from <1.0 to 1.8 mg/kg. Separate phase

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hydrocarbons (SPH) were identified in water samples collected from four of the soil borings (B-1, B-5, B-6, and B-9). TPHg concentrations in the non-SPH grab groundwater samples submitted for chemical analysis ranged from <50 to 89,000 micrograms per liter (μ g/l). Benzene concentrations in the grab groundwater samples ranged from <0.5 to 21,000 μ g/l.

1996 Over-Excavation: Over-excavation and back-filling of Acme's former UST excavation were performed on March 19, 1996. The excavation, originally left open to 9 fbg, was over-excavated to approximately 11 fbg. Two soil samples (TP-3-W and TP-4-E) were collected from the bottom of the over-excavated former UST area. Soil sample TP-3-W, collected from the western end of the excavation, contained 560 mg/kg TPHg, and 3.1 mg/kg benzene. Soil sample TP-4-E, collected from the eastern end of the excavation, contained 2,700 mg/kg TPHg and <3.0 mg/kg benzene. The excavation was back-filled with clean imported fill material. Soil sampling and back-filling activities are documented in Enviros' May 10, 1996 correspondence.

1996 Subsurface Investigation: In July 1996, Enviros performed additional site assessment activities. Six exploratory borings (B-10, B-11, B-12, B-13, V-1, and V-2) were drilled and sampled on July 17 and 19, 1996 using a hollow-stem auger drill rig. Borings B-11 and B-12 were completed as groundwater monitoring wells MW-1 and MW-2, and borings V-1 and V-2 were completed as soil vapor extraction wells V-1 and V-2, respectively. Soil sampling was not performed in boring V-1 due to the fact that it was installed into the back-fill material within the former UST excavation. A soil sample from below the saturated zone in boring V-2 was submitted for physical parameter analyses (porosity, permeability, fractional organic carbon content, and dry bulk density).

TPHg and benzene were not detected in soil samples collected from MW-1 (B-11), MW-2 (B-12), and B-13. TPHg was detected in soil samples collected from B-10 and V-2 at concentrations of 1.7 and 110 mg/kg, respectively. Benzene concentrations in soil samples from B-10 and V-2 were <0.0050 and 0.29 mg/kg, respectively.

Grab groundwater samples were collected from borings B-10, B-12 (MW-2), and B-13 at the depth of first encountered groundwater (approximately 8 to 11 fbg) for chemical analysis. Boring B-11 (MW-1) did not yield sufficient groundwater for grab groundwater sample collection. Monitoring wells MW-1 and MW-2 were developed and sampled on August 2, 1999 by Blaine Tech Services (Blaine) of San Jose, CA. TPHg concentrations in the groundwater samples ranged from <50 to 290,000 μg/l. Benzene concentrations ranged from <0.50 to 34,000 μg/l.

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1997 Modified Phase I ESA: In February 1997, Enviros performed a modified Phase I ESA for the subject facility. A review of aerial photographs (1952 to 1994), city directories (1967 to 1993) and Sanborn maps (1912 to 1970) did not reveal evidence of an off-site source of petroleum hydrocarbons which would have impacted groundwater onsite. The properties located north and west of the subject facility appear to have been occupied by residential houses from at least 1912 to the present. The nearest gasoline stations identified in the vicinity of the subject facility were a former Chevron station (740 27th Street at West) approximately 450 feet to the west, a former station (26th Street and Martin Luther King, Jr. Way) approximately 300 feet to the south, and a former Mobil station (554 27th Street) approximately 950 feet to the east.

2000 Sensitive Receptor Survey: In late 2000, Cambria performed a sensitive receptor survey (SRS) which attempted to identify wells and underground utility conduits. Cambria obtained utility conduit maps from the City of Oakland Engineering Department to locate and map underground utility conduits which may act as preferential pathways for contaminant migration from the site. These conduit trenches are typically back-filled with materials which are more permeable than the surrounding native soils, therefore providing a path of least resistance for petroleum hydrocarbon migration within the local groundwater. Using these maps, Cambria identified the sanitary and storm sewer systems as the only utility conduits in the site vicinity which may act as preferential pathways. All other utilities are typically buried at depths which are shallower than those of the sewer systems. Conduits identified in the area are located at depths of approximately 3.5 to 9 fbg. Therefore, the potential does exist for groundwater to flow within these conduit trenches. Groundwater depth onsite historically ranges from approximately 4.5 to 10 fbg. However, since the typical groundwater flow direction onsite has generally been to the south, it is likely that any contaminant migration within the utility conduits would be limited, since the utility conduits located to the south of the site are the shallowest of all the conduits identified adjacent to the site at depths of 3.5 to 5.5 fbg. Cambria obtained well installation and destruction records from the California Department of Water Resources (DWR) in order to identify any active water producing wells in the vicinity of the site which may be at risk to petroleum hydrocarbon impact due to contaminant migration from the subsurface of the site. DWR records did not identify any existing wells within a ½-mile radius of the site.

2000 Subsurface Investigation: In November 2000, Cambria installed three soil borings (B-17, B-18 and B-19) and three groundwater monitoring wells (MW-3, MW-4 and MW-5). Up to 2,100 mg/kg TPHg and 3.3 mg/kg benzene were reported in soil samples collected. No TPHg or benzene was detected in soil samples collected from well MW-3. Except for 0.0070 mg/kg

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detected in soil sample B-18-7.0, no methyl tertiary butyl ether (MTBE) was detected in any of the analyzed soil samples. Tertiary butyl alcohol (TBA) was detected in soil samples MW-4-5.0 and B-19-5.0 at concentrations of 0.0079 and 0.0059 mg/kg, respectively.

Grab groundwater samples were collected from borings B-17 through B-19 at first encountered groundwater for analyses during the investigation. TPHg concentrations in grab water samples collected from the borings ranged from 58,000 to 190,000 µg/l. Benzene concentrations ranged from 4,400 to 13,000 µg/l. MTBE was detected in groundwater at concentrations of 16 and 300 µg/l from B-19 and B-17, respectively, and TBA was detected at 240 µg/l in B-19 only. No SPH was observed during the investigation.

2001 Oxygen Releasing Compound (ORC) Installation: As approved by the (ACHCSA), Blaine installed ORCs in wells V-1 and V-2 during the second quarter monitoring event on May 2, 2001. ORCs were removed during the fourth quarter 2001 monitoring event. MTBE has not been detected in these two wells since the ORCs were installed.

2002 Site Investigation: In April 2002, Cambria installed borings B-20 through B-22. Groundwater was first encountered in the borings between 8.0 fbg (B-20) and 8.8 fbg (B-21 and B-22). The maximum TPHg and benzene concentrations detected in soil were 380 and 0.17 mg/kg, respectively, in the soil sample collected from 8.0 fbg in boring B-22, located behind the station building. No TPHg was detected in soil samples collected from boring B-21. No MTBE was detected in any of the analyzed soil samples collected from borings B-20, B-21, or B-22. Up to 160,000 μg/l TPHg and 18,000 μg/l benzene were reported in grab groundwater samples collected from borings B-20, B-21, and B-22. No MTBE was detected in grab groundwater samples collected from the borings. The complete report of findings was included in Cambria's June 21, 2002 Site Investigation Report. This document included recommendations for additional activities; however, a response from ACHCSA was never received.

2003 Door-to-Door Survey and Cross Sectional Diagram Preparation: During 2003, Cambria conducted a door-to-door survey of properties within 500 feet of the site. No wells were identified, but seven structures with basements were identified and mapped. Additionally, two cross sectional diagrams were prepared for the site. The complete report of findings is included in Cambria's December 16, 2003 Sensitive Receptor Survey, Geologic Cross Sections, and Fourth Quarter 2003 Groundwater Monitoring Report.

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2003 - 2005 Oxygen Releasing Compound (ORC) Installation: Although agency approval was not received, Shell proactively installed ORC in wells MW-5 and V-2 during first quarter of 2003. The ORCs were replaced on a semi-annual basis. The use of ORC was discontinued during the first quarter 2005, at Shell's request.

May 2005 Agency Meeting: Since no agency response was received to the June 2002 Site Investigation Report that contained recommendations for additional investigation, and since monitoring continued to indicate elevated concentrations of volatile constituents in groundwater, Shell authorized Cambria to prepare a work plan to investigate subsurface soil, groundwater, and soil vapor conditions along the property boundaries and at select locations on site. A new case worker was assigned to this project in early 2005, and following a meeting with the new case worker, technical comments and work plan approval were received in ACEH correspondence dated June 6, 2005. On August 15, 2005, Cambria submitted correspondence providing responses to the technical comments, notification of field work, and a request for extension for the report of findings. In correspondence dated August 19, 2005, ACEH granted the extension.

2005 Soil Vapor Investigation: From August 28 through 31, 2005, Cambria installed ten soil borings (GP-1 through GP-10). In soil, TPHg was detected from borings GP-1 at 10.0 fbg, GP-2 at 4.5 fbg, GP-3 at 5.0 and 8.5 fbg, GP-6 at 9.5 fbg, and GP-7 at 9.5 fbg at concentrations ranging from 1.5 to 3,300 mg/kg and benzene was detected from borings GP-2 at 4.5 fbg, and GP-3 at 5.0 and 8.5 fbg at concentrations ranging from 0.027 to 15 mg/kg. In groundwater, TPHg was detected in all four borings (GP-1, GP-3, GP-6, and GP-7) at concentrations ranging from 9,100 to 140,000 µg/l and benzene was also detected in all four groundwater samples at concentrations ranging from 320 to 17,000 µg/l. Soil vapor samples were collected from each boring and TPHg was detected in GP-1 through GP-10 at concentrations ranging from 350 to 71,000,000 micrograms per cubic meter (ug/m³). Benzene was detected in soil samples collected from borings GP-1 through GP-3 and GP-5 through GP-10 at concentrations ranging from <4.1 to 170,000 ug/m³. A complete discussion and presentation of these activities and findings is included in Cambria's November 15, 2005 Site Investigation Report. This report also included recommendations for performing a door-to-door survey within 300 feet of the site to confirm basement locations, building construction, and potential sources; preparing work plans for pilot testing and plume delineation. Cambria submitted the November 22, 2005 Feasibility Study Work Plan and the December 16, 2005 Plume Delineation Work Plan, which Alameda County Environmental Health (ACEH) staff approved in their December 29, 2005 correspondence.

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December 2005 – Door-to-Door Survey: Cambria conducted a door-to-door survey within 300-feet of the subject site for wells, basements, and foundation type to identify building construction and potential vapor receptors. Questionnaires were sent to 110 properties and responses for 25 properties were received as of January 13, 2006. Tabulated data and a list of properties included in the survey, and which completed surveys were received was included in our Door to Door Survey Report, Access Agreement Update, and Status/Schedule Update submittal dated January 15, 2006. Of the 25 responses received, none of the properties had basements. Three properties were denoted as vacant; nine properties contained buildings constructed with slab-on-grade foundations; three contained buildings constructed with perimeter foundations. Responses for the other 10 properties were either left blank, marked as unknown, or the response was contradictory or unclear. Regarding underground storage tanks, 17 responses were negative, four responses were marked as "unknown", and four responses were left blank. With the exception of the monitoring wells at the subject site, no wells were identified through the survey activities.

January 2006 – Subsurface Investigation: On January 3 and 4, 2006, Cambria advanced three monitoring wells (MW-6 through MW-8), one soil boring (B-23), and six soil vapor probes (VP-1 through VP-6). In soil, TPHg was detected from borings MW-6 at 10.0 and 15.5 fbg, MW-7 at 11.5 and 16.5 fbg, MW-8 at 10.5 and 19 fbg, and B-23 at 10, 15.5, and 19.5 fbg at concentrations ranging from 7.1 to 3,800 mg/kg. Benzene was detected from borings MW-6 at 19.5 fbg, MW-8 at 19.5 fbg, and B-23 at 15.5 and 19.5 fbg at concentrations ranging from 0.0090 to 33 mg/kg. The vapor probes were not installed due to saturated soil conditions. A complete discussion and presentation of these activities and findings is included in Cambria's April 14, 2006 Site Investigation Report, and First Quarter 2006 – Groundwater Monitoring Report.

January 2006 – DPE Pilot Test: Cambria conducted a five-day dual-phase extraction pilot test the week of January 16, 2006. The details and results were presented in Cambria's Pilot Test Report dated March 14, 2006. DPE was performed on wells V-1, V-2, MW-6, MW-7, MW-4, MW-5, and MW-8. On January 20, 2006, a constant vacuum DPE test was conducted on well MW-6. The report concluded 1) the absence of vapor phase concentrations (and groundwater concentrations) from well V-1 indicates that the former UST excavation does not contain residual source material; 2) high sustained and increasing vapor concentrations suggest source material is present in the vicinity of wells V-2, MW-5, and MW-8; 3) variability in extraction flow rates across the site may reflect heterogeneities in subsurface soils or may suggest preferential pathways; and 4) the extremely high effective radius of influence calculated for wells MW-5 and MW-8 during

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DPE testing on well MW-7 supports the presence of a preferential pathway in the vicinity of these wells. The data from the DPE pilot test suggests that DPE is feasible at this site. The groundwater table was effectively drawn down by DPE and moderate vapor extraction flow rates were yielded from some of the extraction points. Although DPE is deemed feasible, Cambria did not recommend implementing DPE at this site. The extraction points that yielded the highest vapor concentrations did not yield an effective vapor extraction flow rate. Conversely, low vapor concentrations were yielded from the extraction point that did yield an effective vapor extraction flow rate. Therefore, DPE is not considered feasible in the target areas at this site.

February 2006 – Install Offsite Wells MW-12 and MW-14: The December 20, 2005 Plume Delineation Work Plan proposed offsite activities including the installation of seven offsite monitoring wells and eight soil vapor probes. Based on responses from only two of the offsite property owners, Cambria completed a portion of the scope of work recommended. Monitoring wells MW-12 and MW-14 were installed at two offsite properties to 20 and 14.5 fbg, respectively. Groundwater was first encountered during drilling activities in borings MW-12 and MW-14 at 14.0 and 11.0 fbg, respectively. None of the soil samples from well MW-12 indicated the presence of any TPHg or BTEX. The 5-fbg sample from MW-14 also did not contain any reportable concentrations. TPHg was reported in the 10- and 14-fbg samples from MW-14 at concentrations of 32 and 970 mg/kg, respectively. Benzene was reported in the same two samples at concentrations of 0.0083 and 2.3 mg/kg, respectively. Fuel oxygenates were requested on the 10-fbg and 14-fbg soil samples from MW-14, and none were reported above the detection limits. These activities are documented in Cambria's May 25, 2006 Subsurface Investigation Report.

April 2006 – Survey and Site Visit: In addition to surveying the new wells, Cambria identified historical boring locations from patches on the ground surface, historical excavation edges, trenches, and other site features, and requested that they be included in the survey. Report figures since May 2006 have included the new survey data. Also, during the site visit, an inspection inside the building identified two bathrooms. A floor drain was observed in the northern-most bathroom. Standing liquid was present in the floor drain and automotive parts and cleaners were stored in this area. Thus, a sample from the floor drain was collected and submitted for analyses of volatile organic compounds (VOCs) by EPA Method 8260 and semi-volatile organic compounds (SVOCs) by EPA Method 8270. The floor drain sample was analyzed for VOCs and SVOCs. The results indicated the presence of carbon disulfide (3.69 μg/l), ethylbenzene (0.610

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 μ g/l) and toluene (0.770 μ g/l). This information was reported in Cambria's May 25, 2006 Subsurface Investigation Report.

May 2006 - Geophysical Survey: As recommended in Cambria's May 25, 2006 Subsurface Investigation Report, a geophysical study was performed on May 22, 2006. The objectives of this effort were to determine whether or not a waste oil UST was in the ground in the northwest portion of the property, and to evaluate the presence of subsurface utilities in this area that may act as preferential pathways, including the mapping of the sewer line from the floor drain found inside the northwest corner of the building during the April 19, 2006 site inspection. The results did not identify the presence of a UST on the northwest corner of the site, but did find another vent line located behind the northeast corner of the station building. A subsurface electric line was traced from the station building to the western property boundary, and an unidentified subsurface utility was traced from the northwest corner of the station building to the southwest, near MW-5 and toward MW-6. The presence of the unknown utility line in the northwest corner confirms the observations of a possible preferential pathway in this area based on the dual-phase extraction pilot test performed in January 2006. NORCAL was unable to run a line down the floor drain inside of the building due to the trap in the line, so the sewer cleanout was found on the exterior of the building. Accessing the cleanout would have resulted in damage to the cap, and the property owner would not grant permission for Cambria to open the cleanout and repair any damage. Thus, the location, direction, and depth of the sewer line in this area are still unknown. However, based on the GPR survey that was performed to try to locate a non-metallic sewer line, NORCAL concludes that the sewer line may be more than 4 feet below grade, since the GPR was unable to identify the line. This information was presented in Cambria's July 25, 2006 Status Update, Report of Geophysical Survey, and Request for Agency Meeting.

August 2006 – Agency Meeting: On August 2, 2006, a meeting between Shell and the ACEH was held to discuss results of recent activities, the status of pending activities, and an agreed upon course for proposed additional activities. During that meeting, the parties agreed to a scope of work, which was presented in Cambria's August 31, 2006 Subsurface Investigation Work Plan. The objectives detailed in that work plan were to:

- Obtain detailed lithologic information onsite and offsite by continuous sampling using electronic logging by cone penetration testing (CPT) technique in five onsite and five offsite borings labeled CPT-1 through CPT-10;
- Collect shallow soil gas samples from approximately 5 feet below grade (fbg) near offsite monitoring well MW-14 (CPT-8);

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- Obtain groundwater samples from first encountered groundwater from areas where wells have not been installed (CPT-5 through CPT-7, CPT-9, and CPT-10);
- Collect groundwater from deeper within the first aquifer at all locations from approximately 20-25 fbg, depending on the CPT log results;
- Collect groundwater samples from a deeper interval at select locations for vertical groundwater profiling (CPT-4, CPT-6, CPT-8, and CPT-9);
- Install the onsite vapor probes to allow for the future collection of soil gas samples near the western property boundary;
- Collect ambient air samples from the above-ground basement area at 664 27th Street for chemical analysis.

This scope of work was approved by the ACEH in correspondence dated September 5, 2006.

October 2006 – CPT-1 through CPT-5 and VP-1 through VP-6: Cambria installed CPT-1 through CPT-5 and VP-1 through VP-6 on the subject site. Offsite borings were not successful due to concerns about property damage (CPT-8 and CPT-9), and utility conflicts (CPT-6 and CPT-7), and lack of access agreement (CPT-10). There was a lack of adequate groundwater recharge for many of the groundwater samples attempted between 15 and 29 fbg. Groundwater sample results from between 31-37 fbg confirm significant attenuation of contaminants of at least one order of magnitude from the interval monitored by the site wells (5-20 fbg), thus nor further vertical delineation is warranted. Comparison of data from 1995, 2000, and 2006 in similar location (B-6 & B-9, B-19, and CPT-5, respectively) demonstrates attenuation of contaminant concentrations over time is occurring. The six onsite vapor probes could not be sampled due to the presence of water in some of the probes. A site inspection at the neighboring property was performed and revealed that due to significant ventilation and air exchange with outdoor ambient air, vapor sampling within the above-ground basement was no longer warranted. These activities are documented in Cambria's January 31, 2007 CPT Investigation and Vapor Probe Installation Report.

May and June 2007 CPT-6, CPT-7, and CPT-10 and VP-7 and VP-8: CRA drilled offsite borings CPT-6, CPT-7, and CPT-10 and installed offsite vapor probe pairs VP-7 and VP-8. No TPHg or benzene were detected in soil samples collected from VP-7 and VP-8, or from boring CPT-6. There was a lack of adequate groundwater recharge in the shallow groundwater sampling interval in boring CPT-6, and in both the shallow and deeper attempted intervals in boring CPT-7. Grab groundwater samples from boring CPT-10 contained 38,000 μ g/L TPHg and 1,600 μ g/L benzene at 13-17 fbg, and 640 μ g/L TPHg and 3.8 μ g/L benzene at 20-23 fbg. Soil vapor

ATTACHMENT A

Site History

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samples collected from both sampling intervals (approximately 2.5 and 4.5 fbg) in probes VP-7 and VP-8 did not contain TPHg or benzene concentrations above the residential ESLs. These activities are documented in CRA's August 27, 2007 *Plume Delineation and Soil Vapor Sampling Report*.

1996 to Present – Ongoing Groundwater Monitoring: Quarterly groundwater monitoring has been ongoing at the site since August 1996 and currently includes onsite monitoring wells MW-1 through MW-8, VP-1, and VP-2, and offsite monitoring wells MW-12 and MW-14. Fuel oxygenates are not a significant component of the groundwater plumes, although some detections of di-isopropyl ether and tertiary butyl alcohol have been observed. Overall, the groundwater flow direction is primarily to the west, with some radial components on site to the northwest and southwest. Historically, monitoring wells MW-1, MW-2, MW-3, and MW-12 have shown little or no impact from petroleum hydrocarbons. Maximum historical concentrations of TPHg and benzene have been observed in onsite monitoring well MW-5. The Third Quarter 2007 sample event (August) reported maximum concentrations of TPHg and benzene at 110,000 and 6,900 μg/l, respectively in well MW-5. Downgradient monitoring well MW-14 reported TPHg and benzene at 45,000 and 1,000 μg/l, respectively, for this same event.

ATTACHMENT 2

Historical Soil Sampling Results and Locations

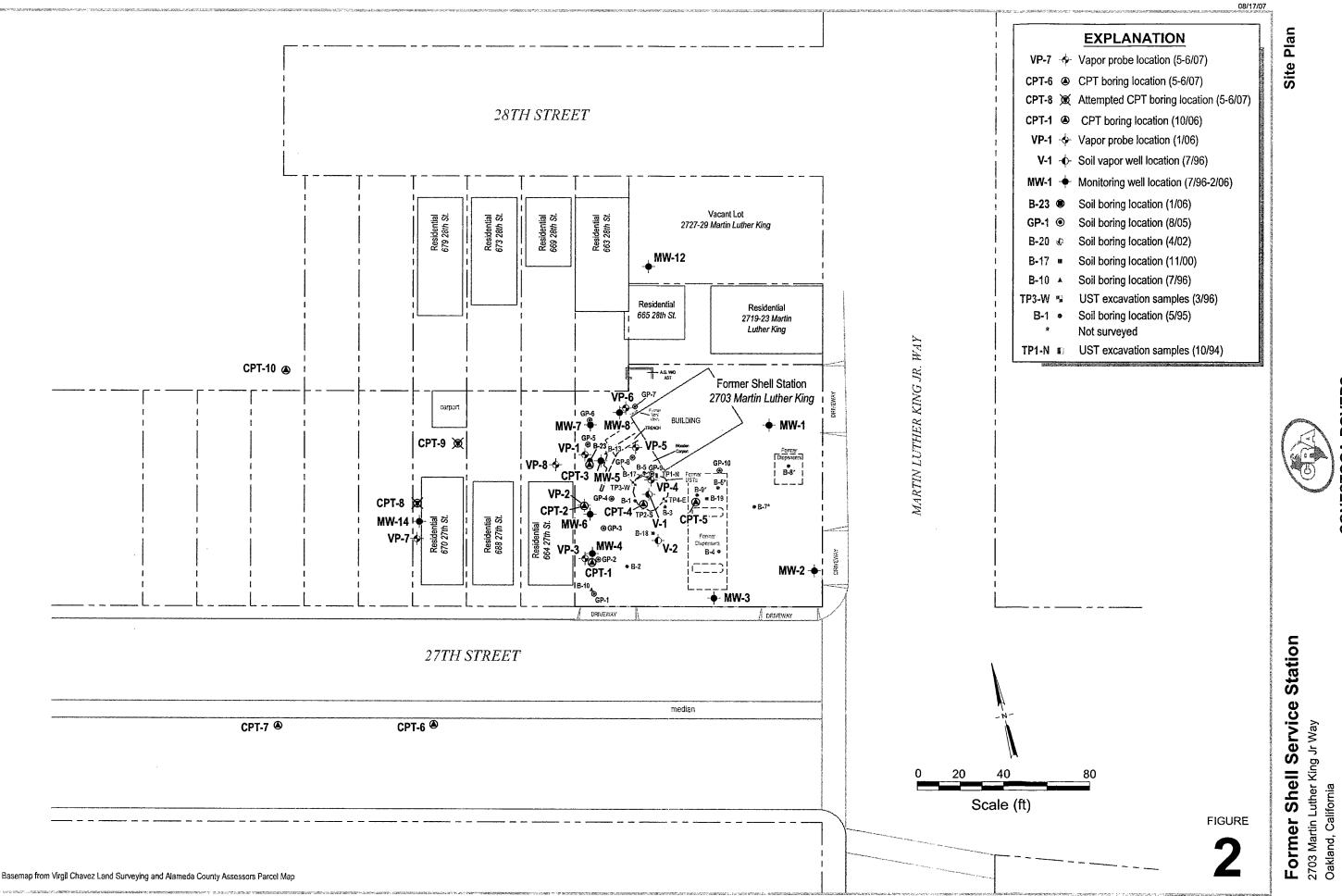


Table 1. Soil Analytical Data, Former Shell Service Station, 2703 Martin Luther King Jr. Way, Oakland, California

Depth	Date	TPHg	В	Т	E	X
(feet)	Sampled	(mg/kg)	(mg/kg)	(mg/kg)	(mg/kg)	(mg/kg)
17	17-May-07	<0.50	0.0020 a	0.0032 a	<0.0050	0.0019 a
4.5	06-Jun-07	<0.50	<0.0050	<0.0050	<0.0050	<0.010
4.5	29-May-07	<0.50	0.00096 a	0.00084 a	0.00084 a	0.0015 a
	(feet) 17 4.5	(feet) Sampled 17 17-May-07 4.5 06-Jun-07	(feet) Sampled (mg/kg) 17 17-May-07 <0.50 4.5 06-Jun-07 <0.50	(feet) Sampled (mg/kg) (mg/kg) 17 17-May-07 <0.50	(feet) Sampled (mg/kg) (mg/kg) (mg/kg) 17 17-May-07 <0.50	(feet) Sampled (mg/kg) (mg/kg) (mg/kg) (mg/kg) 17 17-May-07 <0.50

Abbreviations and Notes:

TPHg = Total petroleum hydrocarbons as gasoline, analyzed by EPA Method 8015B (M)

BTEX = Benzene, toluene, ethylbenzene, and xylenes analyzed by EPA Method 8260B

mg/kg = Milligrams per kilogram = parts per million

a = Analyte was detected at a concentration below the reporting limit and above the laboratory method detection limit. Reported value is estimated.

< x =Not detected at reporting limit x

Table 2. Soil Analytical Data, Former Shell Service Station, 2703 Martin Luther King Jr. Way, Oakland, California

Sample	Depth (fbg)	Date Sampled	TPHg (mg/kg)	B (mg/kg)	T (mg/kg)	E (mg/kg)	X (mg/kg)	MTBE (mg/kg)	TBA (mg/kg)	Lead (mg/kg)
Soil Analytical Da	ita sampled by 8	3260B, 02-28-06								
MW-12-5	5	28-Feb-06	<1.0	< 0.0050	< 0.0050	< 0.0050	< 0.0050	NA	NA	NA
MW-12-10	10	28-Feb-06	<1.0	< 0.0050	< 0.0050	< 0.0050	< 0.0050	NA	NA	NA
MW-12-15	15	28-Feb-06	<1.0	< 0.0050	< 0.0050	< 0.0050	< 0.0050	NA	NA	NA
MW-12-19.5	19.5	28-Feb-06	<1.0	<0.0050	<0.0050	< 0.0050	<0.0050	NA	NA	NA
MW-14-5	5	28-Feb-06	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	NA	NA	NA
MW-14-10	10	28-Feb-06	32	0.0083	< 0.0050	0.028	0.0055	< 0.0050	< 0.025	NA
MW-14-14	14	28-Feb-06	970	2.3	0.18	19	27	<0.15	<0.70	NA
Soil Analytical Da	ta sampled by 8	3015M/8021 or 8260B a	ıs indicated, 01-03	-06 to 01-04-06				,		
MW-6 (8260)	5 a, b	04-Jan-06	<4.9	< 0.025	< 0.025	0.025	0.044	NA	NA	17
MW-6 (8015)	10 a	04-Jan-06	290	<1.2	<1.2	3.1	3.2	NA	NA	14
MW-6 (8015)	15.5	04-Jan-06	36	< 0.62	< 0.62	0.65	2.1	NA	NA	NA
MW-6 (8260)	19.5 ^b	04-Jan-06	<1.0	0.0090	<0.0050	0.010	0.022	NA	NA ·	NA
MW-7 (8260)	5.5 b	4-Jan-06	<1.0	<0.0050	< 0.0050	<0.0050	0.013	NA	NA	11
MW-7 (8260)	11.5 a, b, c	4-Jan-06	7.1	< 0.025	< 0.025	0.19	5.2 d	NA	NA ·	8.5
MW-7 (8015)	16.5 a	4-Jan-06	340	<1.2	<1.2	7.2	<1.2	NA	NA	NA
MW-7 (8260)	19.5 ^b	4-Jan-06	<1.0	<0.0050	< 0.0050	<0.0050	0.010	NA	NA	NA
MW-8 (8260)	6.5 ^b	3-Jan-06	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	NA	NA	310
MW-8 (8015)	10.5 a, e	3-Jan-06	880	<6.2	<6.2	15	72	NA	NA	5.3
MW-8 (8015)	19.5 °	3-Jan-06	19	0.63	<0.62	<0.62	0.80	NA	NA	NA
B-23 (8260)	5 ^b	3-Jan-06	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	NA	NA	9.1
B-23 (8015)	10 a, e	3-Jan-06	520	<6.2	<6.2	12	62	NA	NA	5.4
B-23 (8015)	15.5 a, e	3-Jan-06	3,800	33	50	98	480	NA	NA	NA
B-23 (8015)	19.5 a, e	3-Jan-06	350	1.6	1.9	15	35	NA	NA	NA

Table 2. Soil Analytical Data, Former Shell Service Station, 2703 Martin Luther King Jr. Way, Oakland, California

Sample	Depth (fbg)	Date Sampled	TPHg (mg/kg)	B (mg/kg)	T (mg/kg)	E (mg/kg)	X (mg/kg)	MTBE (mg/kg)	TBA (mg/kg)	Lead (mg/kg)
Soil Analytical De	ata by 8260, san	npled 08-29-05 to 08-31	-05							
GP-1-5.0'	5.0	29-Aug-05	<1.0	< 0.0050	< 0.0050	< 0.0050	< 0.0050	NA	NA	NA
GP-1-10.0'	10.0	29-Aug-05	190*	<0.50	<0.50	<0.50	<0.50	NA	NA	NA
GP-2-4.5'	4.5	29-Aug-05	1.5	0.035	<0.0050	0.0063	<0.0050	NA	NA	NA
GP-3-5.0'	5.0	29-Aug-05	7.5	0.027	<0.0050	0.085	0.11	NA	NA	NA
GP-3-8.5'	8.5	29-Aug-05	3,300	15	2.7	91	230	NA	NA	NA
GP-4-4.5'	4.5	31-Aug-05	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	NA	NA	NA
GP-5-4.5'	4.5	30-Aug-05	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	NA	NA	NA
GP-6-5.0'	5.0	29-Aug-05	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	NA	NA	NA
GP-6-9.5'	9.5	29-Aug-05	260	<0.50	<0.50	2.1	6.8	NA	· NA	NA
GP-7-5.0'	5.0	30-Aug-05	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	NA	NA	NA
GP-7-9.5'	9.5	30-Aug-05	440	<0.50	1.8	10	59	NA	NA	NA
GP-8-4.5'	4.5	30-Aug-05	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	NA	NA	NA
GP-9-4.5'	4.5	31-Aug-05	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	NA	NA	NA
GP-10-4.5'	4.5	31-Aug-05	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	NA	NA	NA
Soil Analytical Da	nta by 2860, san	npled 4-11-02								
B-20-4.5	4.5	04-11-02	1.1	0.0075	< 0.005	< 0.005	< 0.005	<0.5	NA	NA
B-20-7.5	7.5	04-11-02	22	< 0.005	< 0.005	0.14	0.027	<0.5	NA	NA

Table 2. Soil Analytical Data, Former Shell Service Station, 2703 Martin Luther King Jr. Way, Oakland, California

Sample	Depth (fbg)	Date Sampled	TPHg (mg/kg)	B (mg/kg)	T (mg/kg)	E (mg/kg)	X (mg/kg)	MTBE (mg/kg)	TBA (mg/kg)	Lead (mg/kg)
B-21-3.0	3.0	04-11-02	<1.0	<0.005	<0.005	<0.005	<0.005	<0.5	NA	NA
B-21-8.0	8.0	04-11-02	<1.0	<0.005	<0.005	<0.005	<0.005	<0.5	NA NA	NA NA
								•		
B-22-3.0	3.0	04-11-02	<1.0	< 0.005	< 0.005	< 0.005	< 0.005	<0.5	NA	NA
B-22-8.0	3.0	04-11-02	380	0.17	0.27	6.1	31	<0.5	NA	NA
Soil Analytical Da	ata by 8260, san	npled 11-22-00								
MW-3-5.0	5.0	11-22-00	<1.0	< 0.0050	< 0.0050	< 0.0050	< 0.0050	< 0.0050	< 0.0050	NA
MW-3-10.5	10.5	11-22-00	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	<0.0050	< 0.0050	NA
MW-4-5.0	5.0	11-21-00	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	<0.0050	<0.0050	NA
MW-4-10.5	10.5	11-21-00	860	1.1	<0.20	18	66	<0.20	<2.0	NA
NOV 5 5 0	5.0	11 21 00	41.0	<0.0050	<0.0050	<0.0050	<0.0050	<0.0050	<0.0050	NT A
MW-5-5.0	5.0	11-21-00	<1.0	<0.0050	<0.0050 13	<0.0050	<0.0050 140	<0.0050 <0.20	<0.0030 <2.0	NA NA
MW-5-10.5	10.5	11-21-00	1,300	3.3	13	26	140	<0.20	<2.0	INA
B-17-5.0	5.0	11-22-00	1.3	<0.0050	<0.0050	<0.0050	<0.0050	<0.0050	< 0.0050	NA
B-17-7.0	7.0	11-22-00	2,100	0.31	0.64	18	140	< 0.050	<0.050	NA
B-18-5.0	5.0	11-22-00	1.2	<0.0050	<0.0050	<0.0050	<0.0050	<0.0050	<0.0050	NA
B-18-7.0	7.0	11-22-00	42	< 0.0050	<0.0050	0.094	<0.0050	0.0070	<0.050	NA
B-19-5.0	5.0	11-22-00	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	<0.0050	<0.0050	NA
B-19-7.0	7.0	11-22-00	2.4	0.02	<0.0050	0.025	0.023	<0.0050	<0.020	NA
2 17 7.0	7.0	22 00		0.02	101000	0.022	0.025		10.020	• • • •
Soil Analytical Da	ta by 8015/802	1 sampled 07-17-96								
TP-3-W	11.0	07-17-96	560	3.1	4.1	11	41	NA	NA	NA
TP-4-E	11.0	07-17-96	2,700	<3.00	44.0	36	210	NA	NA	NA

Table 2. Soil Analytical Data, Former Shell Service Station, 2703 Martin Luther King Jr. Way, Oakland, California

Sample	Depth (fbg)	Date Sampled	TPHg (mg/kg)	B (mg/kg)	T (mg/kg)	E (mg/kg)	X (mg/kg)	MTBE (mg/kg)	TBA (mg/kg)	Lead (mg/kg)
Soil Analytical D	ata by 8015/802	I sampled 05-23-95								
B-1-5	5.0	05-23-95	63	<0.1	<0.1	0.4	0.1	NA	NA	NA
B-2-5	5.0	05-23-95	260	0.6	<0.1	4.7	10	NA	NA	NA
B-3-6	6.0	05-23-95	150	<0.1	<0.1	0.9	0.4	NA	NA	NA
B-4-6	6.0	05-23-95	55	<0.1	<0.1	0.4	0.2	NA	NA	NA
B-5-8	8.0	05-23-95	830	1.8	9.2	12.0	33	NA	NA	NA
B-6-5	5.0	05-23-95	130	<0.1	<0.1	1.0	1.1	NA	NA	NA
B-6-10	10.0	05-23-95	390	0.3	<0.1	7.3	27	NA	NA	NA
B-7-5	5.0	05-23-95	<20	<0.1	<0.1	1.0	1.1	NA	NA	NA
B-7-10	10.0	05-23-95	53	<0.1	<0.1	0.2	0.3	. NA	NA	NA
B-8-10	10.0	05-23-95	<20	<0.1	<0.1	0.1	<0.1	NA	NA	NA
Soil Analytical D	ata by 8015/802.	I sampled 10-11-94				,				
TP-1-N	•	10-11-94	18000 ^{f, g}	100	870	370	2,000.0	NA	NA	NA
TP-2-S		10-11-94	870 ^{f, g}	2.9	2.1	19	21	NA	NA	NA

Table 2. Soil Analytical Data, Former Shell Service Station, 2703 Martin Luther King Jr. Way, Oakland, California

Sample	Depth	Date Sampled	TPHg	В	Т	Е	X	MTBE	TBA	Lead
	(fbg)		(mg/kg)							

Abbreviations and Notes:

TPHg = Total petroleum hydrocarbons as gasoline

BTEX = Benzene, toluene, ethylbenzene, and xylenes

MTBE = Methyl tertiary butyl ether

TBA = Tertiary butyl alcohol

Lead analyzed by EPA Method 3050B

fbg = Feet below grade

< x =Not detected at reporting limit x

NA = Not analyzed

a = Reporting limit raised due to high level of analyte present in sample.

b = Extracted out of hold time.

c = Internal standard out of range.

d = Estimated value. The concentration exceeded the calibration of analysis.

e = Initial analysis within holding time, but required dilution.

f = Heavier gasoline range compounds are significant (aged gasoline?).

g = Gasoline range compounds are significant; no recognizable pattern.

ATTACHMENT 3

Historical Groundwater Sampling Results

Table 2. Grab Groundwater Analytical Data, Former Shell Service Station, 2703 Martin Luther King Jr. Way, Oakland, California

Boring	Depth	Date	TPHg	В	Т	Е	X
ID	(feet)	Sampled	(µg/L)	(μg/L)	(μg/L)	(μg/L)	(μg/L)
CPT-6	13-17	17-May-07		Attempted	sample - No groundwat	ter recovery	
CPT-6-23-W	21-25	17-May-07	86	<0.50	2.4	0.38 a	1.44 a
CPT-7	10-14	17-May-07		Attempted	sample - No groundwat	er recovery	
CPT-7	18-22	17-May-07		Attempted	sample - No groundwat	er recovery	
CPT-10A	13-17	08-Jun-07	38,000	1,600	1,100	2,600	7,700
CPT-10B	20-23	08-Jun-07	640	3.8	4.9	23	110

Abbreviations and Notes:

TPHg = Total petroleum hydrocarbons as gasoline, analyzed by EPA Method 8015B (M)

BTEX = Benzene, toluene, ethylbenzene, and xylenes analyzed by EPA Method 8260B

 $[\]mu$ g/l = micrograms per liter = parts per billion

< x =Not detected at reporting limit x

a = Analyte was detected at a concentration below the reporting limit and above the laboratory method detection limit. Reported value is estimated.

Table 1. Grab Groundwater Analytical Data, Former Shell Service Station, 2703 Martin Luther King Jr. Way, Oakland, California

Sample	Depth (fbg)	Date Sampled	TPHg (μg/L)	B (µg/L)	Τ (μg/L)	E (μg/L)	X (μg/L)	MTBE (μg/L)	TBA (μg/L)
CPT groundwater sa	mples by 8260B,	sampled October 18 o	and 20, 2006						
CPT-1-35-W	35	18-Oct-06	<50	4.3	<0.50	6.1	3.0	NA	NA
CPT-2-35-W	35	20-Oct-06	2,600	180	69	55	290	NA	NA
CPT-3-35-W	35	20-Oct-06	880	45	15	45	310	NA	NA
CPT-4-37-W	37	18-Oct-06	3,200	33	150	140	570	NA	NA
CPT-5-20-W	20	18-Oct-06	25,000	1,100	200	5,300	4,100	NA	NA
CPT-5-35-W	35	18-Oct-06	220	4.0	2.6	11	44	NA	NA
Groundwater sample	s hv 8015M/802	0, sampled January 3	and 4 2006						
MW-6-W ^a	NA	04-Jan-06	59,000	6,400 ^b	890 b	2,200 b	8,100 b	NA	NA
MW-7-W ^a	NA	04-Jan-06	83,000	4,400 ^b	930 ^b	3,200 ^b	16,000 ^b	NA	NA
MW-8-W ^a	NA	03-Jan-06	49,000	1,100 b	92 ^b	480 ^b	2,700 b	NA	NA
B-23-W ^a	NA	03-Jan-06	230,000	26,000 b	700 ^b	920 ^b	110,000 ^{b,c}	NA	NA
Groundwater samples	s bv 8260B. sam	pled August 29 and 30). 2005						
GP-1-10.5'W	10.5	29-Aug-05	47,000	330	<50	680	140	NA	NA
GP-3-10'W	10.0	29-Aug-05	79,000	5,200	13,000	1,400	7,800	· NA	NA
GP-6-20'W	20.0	29-Aug-05	9,100	320	34	380	750	NA	NA
GP-7-10'W	10.0	30-Aug-05	140,000	17,000	4,600	7,600	45,000	NA	NA

Table 1. Grab Groundwater Analytical Data, Former Shell Service Station, 2703 Martin Luther King Jr. Way, Oakland, California

Sample	Depth (fbg)	Date Sampled	TPHg (μg/L)	B (μg/L)	T (μg/L)	E (μg/L)	X (μg/L)	MTBE (μg/L)	TBA (μg/L)
Groundwater sampl	es by 8260B, sam	ipled April 11, 2002							
B-20	NA	11-Apr-02	58,000	5,000	200	3,800	4,500	<200	NA
B-21	NA	11-Apr-02	160,000	18,000	9,200	5,500	29,000	<500	NA
B-22	NA	11-Apr-02	110,000	6,700	1,200	4,700	23,000	<250	NA
Groundwater sample	es by 8260B, sam	pled November 22,	2000						
B-17	NA	22-Nov-00	190,000	13,000	24,000	5,500	30,000	300	<2,000
B-18	NA	22-Nov-00	90,000	3,500	370	5,000	18,000	<20	<200
B-19	NA	22-Nov-00	58,000	4,400	740	2,200	7,300	16	240
Groundwater sample	es by 8015/8021,	sampled May 23, 19	995						
B-1	NA	23-May-95	Approximately 0.5	5-0.75 inches of N	on-aqueous phase	product			
B-2	NA	23-May-95	6,600	340	24	160	27	NA	NA
B-5	NA	23-May-95			Non-aqueous phase		ine manufactured	prior to 1984	
B-6	NA	23-May-95	Approximately 1 -	2 inches of Non-a	queous phase prod	uct			
B-7	NA	23-May-95	89,000	21,000	11,000	3,800	16,000	NA	NA
B-8	NA	23-May-95	<250	<2.5	<2.5	<2.5	<2.5	NA	NA
B-9	NA	23-May-95	Approximately 0.5	5-1.0 inches of No	n-aqueous phase pi	oduct			

Table 1. Grab Groundwater Analytical Data, Former Shell Service Station, 2703 Martin Luther King Jr. Way, Oakland, California

Sample	Depth	Date Sampled	TPHg	В	Т	Е	х	MTBE	TBA
	(fbg)		(μg/L)	(μg/L)	(μg/L)	(µg/L)	(μg/L)	(µg/L)	(µg/L)

Abbreviations and Notes:

TPHg = Total petroleum hydrocarbons as gasoline

BTEX = Benzene, toluene, ethylbenzene, and xylenes

MTBE = Methyl tertiary butyl ether

TBA = Tertiary butyl alcohol

- a- Reporting limits were raised due to high level of analyte present in the sample
- b Analyzed outside of holding time
- c Estimated value; the concentraion exceeded the calibration of analysis.

Basemap from Virgil Chavez Land Surveying and Alameda County

					1		MTBE	MTBE	1					Depth to	GW	DO
Well ID	Date	TPPH	В	Т	E	x	8020	8260	DIPE	ETBE	TAME	TBA	тос	Water	Elevation	
		(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(MSL)	(ft.)	(MSL)	(ppm)
	1. 1		<u>. </u>		 		****								<u></u>	
MW-1 (B-11)	08/02/1996	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	23.53	NA	NA	NA
MW-1 (B-11)	08/05/1996	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	NA	NA	NA	NA	23.53	8.76	14.77	NA NA
MW-1 (B-11) (D)	08/05/1996	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA.	NA	NA	NA	NA	23.53	NA	NA	NA NA
MW-1 (B-11)	10/17/1996	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	NA	NA	NA	NA	23.53	9.88	13.65	NA
MW-1 (B-11)	01/08/1997	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	NA	NA	NA	NA	23.53	6.82	16.71	NA
MW-1 (B-11)	04/07/1997	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	NA	NA	NA	NA	23.53	7.89	15.64	NA
MW-1 (B-11)	07/02/1997	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	NA	NA	NA	NA	23.53	8.71	14.82	NA
MW-1 (B-11)	10/24/1997	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	ŅA	NA	NA	NA	23.53	9.26	14.27	NA
MW-1 (B-11)	01/09/1998	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	NA	NA	NA	NA	23.53	7.94	15.59	NA
MW-1 (B-11)	04/02/1998	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	NA	NA	NA	NA	23.53	7.21	16.32	NA
MW-1 (B-11)	07/14/1998	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	NA	NA	NA	NA	23.53	7.78	15.75	NA
MW-1 (B-11)	10/01/1998	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	NA	NA	NA	NA	23.53	8.39	15.14	NA
MW-1 (B-11)	01/18/1999	<50.0	<0.500	0.785	<0.500	<0.500	2.36	NA	NA	NA	NA	NA	23.53	8.28	15.25	NA
MW-1 (B-11)	04/29/1999	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	NA	NA	NA	NA	23.53	8.41	15.12	NA
MW-1 (B-11)	08/23/1999	<50.0	<0.500	<0.500	<0.500	<0.500	<2.50	NA	NA	NA	NA	NA	23.53	8.17	15.36	NA
MW-1 (B-11)	10/06/1999	<50.0	<0.500	<0.500	<0.500	<0.500	<5.00	NA	NA	NA	NA	NA	23.53	9.37	14.16	NA
MW-1 (B-11)	01/27/2000	<50.0	<0.500	<0.500	<0.500	<0.500	<2.50	NA	NA	NA	NA	NA	23.53	7.52	16.01	NA
MW-1 (B-11)	04/18/2000	<50.0	<0.500	<0.500	<0.500	<0.500	<2.50	NA	NA	NA	NA	NA	23.53	7.66	15.87	NA
MW-1 (B-11)	07/19/2000	<50.0	<0.500	<0.500	<0.500	<0.500	<2.50	NA	NA	NA	NA	NA	23.53	7.81	15.72	NA
MW-1 (B-11)	10/24/2000	<50.0	<0.500	<0.500	<0.500	<0.500	<2.50	NA	NA	NA	NA	NA	23.53	8.33	15.20	NA
MW-1 (B-11)	01/04/2001	<50.0	<0.500	<0.500	<0.500	<0.500	<2.50	NA	NA	NA	NA	NA	23.53	8.33	15.20	NA
MW-1 (B-11)	05/03/2001	<50	<0.50	<0.50	<0.50	<0.50	NA	<5.0	NA	NA	NA	NA	23.53	7.83	15.70	NA
MW-1 (B-11)	07/09/2001	<50	<0.50	<0.50	<0.50	<0.50	NA	<5.0	NA	NA	NA	NA	23.53	8.60	14.93	NA
MVV-1	10/18/2001	<50	<0.50	<0.50	<0.50	<0.50	NA	<5.0	NA	NA	NA	NA	23.53	9.01	14.52	0.2
MW-1	01/24/2002	<50	<0.50	<0.50	<0.50	<0.50	NA	<5.0	NA	NA	NA	NA	23.53	7.68	15.85	2.1
MVV-1	04/04/2002	<50	<0.50	<0.50	<0.50	<0.50	NA	<5.0	NA	NA	NA	NA	23.53	7.38	16.15	1.1

**							MTBE	MTBE						Depth to	GW	DO
Well ID	Date	TPPH	В	Т	Ε	X	8020	8260	DIPE	ETBE	TAME	TBA	TOC	Water	Elevation	Reading
		(ug/L)	(MSL)	(ft.)	(MSL)	(ppm)										
MW-1	07/18/2002	<50	<0.50	<0.50	<0.50	<0.50	NA	<5.0	NA	NA	NA	NA	23.53	7.75	15.78	2.2
MW-1	10/21/2002	<50	<0.50	<0.50	<0.50	<0.50	NA	<5.0	NA	NA	NA	NA	29.53	8.10	21.43	1.6
MW-1	01/21/2003	<50	<0.50	<0.50	<0.50	<0.50	NA	<5.0	NA	NA	NA	NA	29.53	7.82	21.71	0.6
MW-1	04/17/2003	<50	<0.50	<0.50	<0.50	<1.0	NA	<5.0	NA	NA	NA	NA	29.53	7.76	21.77	1.7
MW-1	07/22/2003	<50	<0.50	<0.50	<0.50	<1.0	NA	<0.50	NA	NA	NA	NA	29.53	7.87	21.66	1.5
MW-1	10/20/2003	<50	<0.50	<0.50	<0.50	<1.0	NA	<0.50	NA	NA	NA	NA	29.53	8.67	20.86	0.8
MW-1	01/13/2004	<50	<0.50	<0.50	<0.50	<1.0	NA	<0.50	NA	NA	NA	NA	29.53	8.28	21.25	NA
MW-1	01/22/2004	NA	NA_	NA	29.53	8.50	21.03	1.1								
MW-1	04/01/2004	NA	29.53	7.98	21.55	NA										
MVV-1	07/13/2004	NA	29.53	8.30	21.23	NA										
MW-1	10/26/2004	NA	29.53	8.27	21.26	NA										
MW-1	01/13/2005	NA	NΑ	29.53	6.92	22.61	NA									
MW-1	04/28/2005	NA	NΑ	NA	29.53	7.18	22.35	NA								
MW-1	08/01/2005	NA	NA	NA	NA	NΑ	NA	NA	NA	NA	NA	NA	29.53	7.43	22.10	NA
MW-1	10/05/2005	NA	29.53	7.55	21.98	NA										
MW-1	01/11/2006	NA	29.54	5.35	24.19	NA										
MW-1	05/26/2006	<50.0	<0.500	<0.500	<0.500	<0.500	NA	<0.500	<0.500	<0.500	<0.500	<10.0	29.54	6.81	22.73	0.78
MW-1	08/30/2006	NA	29.54	7. 77	21.77	NA										
MW-1	11/08/2006	NA	29.54	8.39	21.15	NA										
MW-1	02/22/2007	NA	29.54	7.11	22.43	NA										
MW-1	05/29/2007	NA	29.54	7.20	22.34	NA										
MW-1	08/27/2007	NA	29.54	7.86	21.68	NA										
MW-2 (B-12)*	07/17/1996	<50	<0.50	0.69	<0.50	<0.50	<2.5	NA	NA	NA	NA	NA	22.47	NA	NA	NA
MW-2 (B-12)*	08/05/1996	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	NA	NA	NA	NA	22.47	8.35	14.12	NA
MW-2 (B-12)*	10/17/1996	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	NA	NA	NA	NA	22.47	9.32	13.15	NA

						*·····	MTBE	MTBE			Γ			Depth to	GW	DO
Well ID	Date	TPPH	В	Т	E	X	8020	8260	DIPE	ETBE	TAME	TBA	тос	Water	Elevation	Reading
		(ug/L)	(ug/L)	(ug/L)	(MSL)	(ft.)	(MSL)	(ppm)								
MW-2 (B-12) (D)*	10/17/1996	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	NA	NA	NA	NA	22.47	NA	NA	NA
MW-2 (B-12)*	01/08/1997	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	NA	NA	NA	NA	22.47	6.80	15.67	NA
MW-2 (B-12) (D)*	01/08/1997	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	NA	NA	NA	NA	22.47	NA	NA	NA
MW-2 (B-12)*	04/07/1997	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	NA	NA	NA	NA	22.47	7.81	14.66	NA
MW-2 (B-12)*	07/02/1997	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	NA	NA	NA	NA	22.47	8.27	14.20	NA
MW-2 (B-12)*	10/24/1997	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	NA	NA	NA :	NA	22.47	9.12	13.35	NA
MW-2 (B-12)*	01/09/1998	<50	<0.50	<0.50	<0.50	<0.50	6.3	NA	NA	NA	NA	NA	22.47	7.41	15.06	NA
MW-2 (B-12)*	04/02/1998	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	NA	NA	NA	NA	22.47	6.59	15.88	NA
MW-2 (B-12)*	07/14/1998	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	NA	NA	NA	NA.	22.47	7.49	14.98	NA
MW-2 (B-12)*	10/01/1998	<50	<0.50	<0.50	<0.50	0.59	<2.5	NA	NA	NA	NA	NA	22.47	8.58	13.89	NA
MW-2 (B-12)*	01/18/1999	<50.0	<0.500	0.971	<0.500	<0.500	2.47	NA	NA	NA	NA	NA	22.47	8.68	13.79	NA
MW-2 (B-12)*	04/29/1999	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	NA	NA	NA	NA	22.47	8.62	13.85	NA
MW-2 (B-12)*	08/23/1999	<50.0	<0.500	<0.500	<0.500	<0.500	<2.50	NA	NA	NA	NA	NA	22.47	7.43	15.04	NA
MW-2 (B-12)*	10/06/1999	<50.0	<0.500	<0.500	<0.500	<0.500	<5.00	NA	NA	NA	NA	NA	22.47	9.00	13.47	NA
MW-2 (B-12)*	01/27/2000	<50.0	<0.500	<0.500	<0.500	<0.500	<2.50	NA	NA	NA	NA	NA	22.47	8.15	14.32	NA
MW-2 (B-12)*	04/18/2000	<50.0	<0.500	<0.500	<0.500	<0.500	<2.50	NA	NA	NA	NA	NA	22.47	7.04	15.43	NA
MW-2 (B-12)*	07/19/2000	<50.0	<0.500	<0.500	<0.500	<0.500	<2.50	NA	NA	NA	NA	NA	22.47	7.13	15.34	NA
MW-2 (B-12)*	10/24/2000	<50.0	<0.500	<0.500	<0.500	<0.500	<2.50	NA	NA	NA	NA	NA	22.47	8.78	13.69	NA
MW-2 (B-12)*	01/04/2001	<50.0	<0.500	<0.500	<0.500	<0.500	<2.50	NA :	NA	NA	NA	NA	22.47	8.33	14.14	NA
MW-2 (B-12)*	05/03/2001	<50	<0.50	<0.50	<0.50	<0.50	NA	<5.0	NA	NA	NA	NA	22.47	7.24	15.23	NA
MW-2 (B-12)*	07/09/2001	<50	<0.50	<0.50	<0.50	<0.50	NA	<5.0	NA	NA	NA	NA	22.47	8.55	13.92	NA
MW-2	10/18/2001	<50	<0.50	<0.50	<0.50	<0.50	NA	<5.0	NA	NA	NA	NA	22.47	9.42	13.05	NA
MW-2	01/24/2002	<50	<0.50	<0.50	<0.50	<0.50	NA	<5.0	NA	NA	NA	ΝA	22.47	7.23	15.24	NA
MW-2	04/04/2002	<50	<0.50	<0.50	<0.50	<0.50	NA	<5.0	NA	NA	NA	NA	22.47	6.90	15.57	NA
MVV-2	07/18/2002	<50	<0.50	<0.50	<0.50	<0.50	NA	<5.0	NA	NA	NA	NA	22.47	7.97	14.50	NA
MW-2	10/21/2002	<50	<0.50	<0.50	<0.50	<0.50	NA	<5.0	NA	NA	NA	NA	28.47	8.62	19.85	NA

							MTBE	MTBE						Depth to	GW	DO
Well ID	Date	TPPH	В	Т	E	X	8020	8260	DIPE	ETBE	TAME	TBA	TOC	Water	Elevation	Reading
		(ug/L)	(MSL)	(ft.)	(MSL)	(ppm)										
MW-2	01/21/2003	<50	<0.50	<0.50	<0.50	<0.50	NA	<5.0	NA	NA	NA	NA	28.47	7.08	21.39	. NA
MW-2	04/17/2003	<50	<0.50	<0.50	0.98	2.5	NA	<5.0	NA	NA	NA	NA	28.47	6.94	21.53	NA
MW-2	07/22/2003	<50	<0.50	<0.50	<0.50	<1.0	NA	<0.50	NA	NA	NA	NA	28.47	8.10	20.37	NA
MW-2	10/20/2003	<50	<0.50	<0.50	<0.50	<1.0	NA	<0.50	NA	NA	NA	NA	28.47	9.09	19.38	NA
MW-2	01/13/2004	<50	<0.50	<0.50	<0.50	<1.0	NA	<0.50	NA	NA ·	NA	NA	28.47	7.28	21.19	NA
MW-2	01/22/2004	NA	28.47	8.99	19.48	2.8										
MW-2	04/01/2004	NA	28.47	6.88	21.59	NA										
MW-2	07/13/2004	NA	28.47	8.28	20.19	NA										
MW-2	10/26/2004	NA	28.47	8.43	20.04	NA										
MW-2	01/13/2005	NA	28.47	6.52	21.95	NA										
MW-2	04/28/2005	NA	28.47	6.38	22.09	NA										
MW-2	08/01/2005	NA	28.47	7.73	20.74	NA										
MW-2	10/05/2005	NA	28.47	8.47	20.00	NA										
MW-2	01/11/2006	NA	28.48	6.30	22.18	NA										
MW-2	05/26/2006	59.9	<0.500	<0.500	<0.500	<0.500	NA	<0.500	<0.500	<0.500	<0.500	<10.0	28.48	6.84	21.64	3.02
MW-2	08/30/2006	NA	28.48	8.11	20.37	NA ,										
MW-2	11/08/2006	NA	28.48	8. 61	19.87	NA										
MW-2	02/22/2007	NA	28.48	6.92	21.56	NA										
MW-2	05/29/2007	NA	28.48	7.32	21.16	NA										
MW-2	08/27/2007	NA	28.48	8.38	20.10	NA										
							= .=.									
MW-3	04/25/2001	NA	22.30	7.16	15.14	NA										
MW-3	05/03/2001	<100	<0.50	<0.50	<0.50	<0.50	NA	<5.0	NA	NA	NA	NA	22.30	7.28	15.02	NA
MW-3	07/09/2001	<50	<0.50	<0.50	<0.50	<0.50	NΑ	<5.0	NA	NA	NA	NΑ	22.30	8.45	13.85	NA
MW-3	10/18/2001	<50	<0.50	<0.50	<0.50	<0.50	NA	<5.0	NA	NA	NA	NA	22.30	9.44	12.86	NA
MW-3	01/24/2002	<50	<0.50	<0.50	<0.50	<0.50	NA	<5.0	NA	NA	NA	NA	22.30	5.88	16.42	NA

							MTBE	MTBE						Depth to	GW	DO
Well ID	Date	TPPH	В	Т	E	Х	8020	8260	DIPE	ETBE	TAME	TBA	TOC	Water	Elevation	Reading
		(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(MSL)	(ft.)	(MSL)	(ppm)
MW-3	04/04/2002	<50	<0.50	<0.50	<0.50	<0.50	NA	<5.0	NA	NA	NA	NA	22.30	6.68	15.62	NA
MW-3	07/18/2002	<50	<0.50	<0.50	<0.50	<0.50	NA	<5.0	NA	NA	NA	NA	22.30	7.63	14.67	NA
MW-3	10/21/2002	<50	<0.50	<0.50	<0.50	<0.50	NA	<5.0	NΑ	NA	NA	NA	28.30	8.56	19.74	NA
MW-3	01/21/2003	<50	<0.50	<0.50	<0.50	<0.50	NA	<5.0	NA	NA	NA	NA	28.30	6.95	21.35	NA
MW-3	04/17/2003	<50	<0.50	<0.50	<0.50	<1.0	NA	<5.0	NA	NA	NA	NA	28.30	6.77	21.53	NA
MW-3	07/22/2003	<50	<0.50	<0.50	<0.50	<1.0	NA	<0.50	NA	NA	NA	NA	28.30	7.92	20.38	NA
MW-3	10/20/2003	<50	<0.50	<0.50	<0.50	<1.0	NA	<0.50	NA	NA	NA	NA	28.30	9.12	19.18	NA
MW-3	01/13/2004	<50	<0.50	<0.50	<0.50	<1.0	NA	<0.50	NA	NA	NA	NA	28.30	7.21	21.09	NA
MW-3	01/22/2004	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	28.30	9.00	19.30	0.6
MW-3	04/01/2004	NA	NA	NA	NA	NΑ	NA	NA	NA	NA	NA	NA	28.30	6.65	21.65	NA
MW-3	07/13/2004	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	28.30	8.24	20.06	NA
MW-3	10/26/2004	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	28.30	8.50	19.80	NA
MW-3	01/13/2005	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	28.30	6.32	21.98	NA
MW-3	04/28/2005	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	28.30	6.05	22.25	NA
MW-3	08/01/2005	NA	NA	NA	NA	NA	. NA	NA	NA	NA	NA	NA	28.30	7.65	20.65	NA
MW-3	10/05/2005	NΑ	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	28.30	8.31	19.99	NA
MW-3	01/11/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	28.30	6.10	22.20	NA
MW-3	05/26/2006	<50.0	<0.500	<0.500	<0.500	<0.500	NA	<0.500	2.87	<0.500	<0.500	<10.0	28.30	6.72	21.58	1.46
MW-3	08/30/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	28.30	8.12	20.18	NA
MW-3	11/08/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	28.30	8.71	19.59	NA
MW-3	02/22/2007	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	28.30	6.78	21.52	NA
MW-3	05/29/2007	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	28.30	7.20	21.10	NA
MW-3	08/27/2007	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	28.30	8.18	20.12	NA
MW-4	04/25/2001	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	22.51	7.05	15.46	NA
MW-4	05/03/2001	8,000	3,500	24	37	350	NA	<200	NA	NA	NA	NA :	22.51	6.66	15.85	NA

				=			MTBE	MTBE			T			Depth to	GW	DO
Well ID	Date	TPPH	В	Т	E	X	8020	8260	DIPE	ETBE	TAME	TBA	TOC	Water	Elevation	Reading
		(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(MSL)	(ft.)	(MSL)	(ppm)
· · · · · · · · · · · · · · · · · · ·																
MVV-4	07/09/2001	16,000	4,100	32	890	790	NA	<200	NA	NA	NA	NA	22.51	8.28	14.23	NA
MW-4	10/18/2001	12,000	3,300	<20	430	220	NA	<200	NA	NA	NA	NA	22.51	9.40	13.11	NA
MW-4	01/24/2002	5,500	1,200	<5.0	280	240	NA	<50	NA	NA	NA	NA	22.51	5.73	16.78	NA
MVV-4	04/04/2002	2,000	350	1.4	13	7.8	NA	<10	NA	NA	NA	NA	22.51	. 5.62	16.89	NA
MVV-4	07/18/2002	3,400	440	1.3	200	98	NA	<5.0	NA	NA	NA	NA	22.51	6.94	15.57	NA
MVV-4	10/21/2002	16,000	3,100	11	1,200	970	NA	<5.0	NA	NA	NA	NA	28.51	8.04	20.47	NA
MVV-4	01/21/2003	3,600	720	3.9	110	58	NA	<25	NA	NA	NA	NA	28.51	6.10	22.41	NA
MW-4	04/17/2003	3,700	810	<5.0	140	17	NA	<50	NA	NA	NA	NA	28.51	5.97	22.54	NA
MVV-4	07/22/2003	3,700	450	<2.5	110	7.9	NA	<2.5	NA	NA	NA	NA	28.51	6.37	22.14	NA
MW-4	10/20/2003	11,000 c	2,500	<20	550	95	NA	<20	NA	NA	NA	NA	28.51	8.99	19.52	NA
MW-4	01/13/2004	6,600	1,500	<10	41	37	NA	<10	NA	NA	NA	NA	28.51	6.67	21.84	NA
MW-4	01/22/2004	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	28.51	8.80	19.71	0.3
MW-4	04/01/2004	9,500	2,100	12	170	30	NA	NA	NA	NA	NA	NA	28.51	6.28	22.23	0.1
MW-4	07/13/2004	12,000	3,600	39	160	58	NA	<25	<100	<100	<100	<250	28.51	8.20	20.31	0.1
MW-4	10/26/2004	11,000	2,800	<25	100	<50	NA	NA	NA	NA	NA	NA	28.51	8.00	20.51	0.6
MW-4	01/13/2005	12,000	2,200	14	110	43	NA	NA	NA	NA	NA	NA	28.51	6.03	22.48	0.1
MW-4	04/28/2005	8,600	2,300	27	200	49	NA	NA	NA	NA	NA	NA	28.51	5.93	22.58	3.71
MW-4	08/01/2005	11,000	3,900	57	180	47	NA	<10	<40	<40	<40	<100	28.51	6.20	22.31	NA d
MW-4	10/05/2005	9,400	3,300	45	88	33	NA	NA	NA	NA	NA	NA	28.51	8.22	20.29	2.76
MW-4	01/11/2006	3,900 f	1,700 f	14	95	78	NA	<0.50	7.4	<0.50	<0.50	32	28.51	4.25	24.26	0.6
MW-4	05/26/2006	6,730	455	1.90	56.7	44.8	NA	<0.500	4.36	<0.500	<0.500	<10.0	28.51	5.90	22.61	0.54
MW-4	08/30/2006	29,600	2,740	30.0	448	237	NA	<0.500	<0.500	<0.500	<0.500	<10.0	28.51	7.98	20.53	0.44/0.46
MW-4	11/08/2006	6,300	1,500	13	130	67	NA	NA	NA	NA	NA	NA	28.51	8.52	19.99	0.05/0.22
MW-4	02/22/2007	11,000	2,200	18	620	310	NA	NA	NA	NA	NA	NA	28.51	5.63	22.88	2.96/2.98
MW-4	05/29/2007	14,000 i,j	3,200	27	640	249.0	NA	NA	NA	NA	NA	NA	28.51	6.60	21.91	0.19/0.11
MW-4	08/27/2007	12,000 i	1,900	19 k	250	80.9 k	NA	<25	<50	<50	<50	<250	28.51	8.50	20.01	0.85/1.71

		_					MTBE	MTBE						Depth to	GW	ОО
Well ID	Date	TPPH	В	T	E	Χ	8020	8260	DIPE	ETBE	TAME	TBA	TOC	Water	Elevation	Reading
		(ug/L)	(MSL)	(ft.)	(MSL)	(ppm)										

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MW-5	04/25/2001	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	23.54	7.36	16.18	NA
MW-5	05/03/2001	160,000	12,000	20,000	3,600	23,000	NA	<500	NA	NA	NA	NA	23.54	7.77	15.77	NA
MW-5	07/09/2001	130,000	11,000	19,000	4,500	22,000	NA	<500	· NA	NA	NA	NA	23.54	9.32	14.22	NA
MW-5	10/18/2001	120,000	12,000	23,000	4,200	21,000	NA	<500	NA	NA	NA	NA	23.54	9.39	14.15	0.5
MW-5	01/24/2002	34,000	3,300	3,300	960	6,000	NA	<100	NA	NA	NA	NA	23.54	7.05	16.49	4.0
MW-5	04/04/2002	32,000	2,100	2,80 0	730	6,400	NA	<200	NA	NA	NA	NA	23.54	6.89	16.65	1.0
MW-5	07/18/2002	75,000	7,500	4,700	2,700	15,000	NA	<500	NA	NA	NA	NA	23.54	8.48	15.06	1.2
MW-5	10/21/2002	140,000	13,000	18,000	4,000	26,000	NA	<500	NA	NA	NA	NA	29.54	9.21	20.33	1.1
MW-5	01/21/2003	47,000	6,400	3,500	370	8,300	NA	<500	NA	NA	NA	NA	29.54	7.23	22.31	0.8
MW-5	04/17/2003	93,000	9,700	16,000	3,200	20,000	NA	<500	NA	NA	NA	NA	29.54	6.61	22.93	0.8
MW-5	07/22/2003	110,000	9,500	15,000	560	23,000	NA	<50	NA	NA.	NA	NA	29.54	8.68	20.86	1.2
MW-5	10/20/2003	88,000	6,600	12,000	1,900	16,000	NA	<50	NA	NA	NA	NA	29.54	9.71	19.83	0.1
MW-5	01/13/2004	4,600	460	140	<10	930	NA	<10	NA	NA	NA	NA	29.54	7.30	22.24	NA
MW-5	01/22/2004	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	29.54	9.51	20.03	0.3
MW-5	04/01/2004	70,000	7,900	11,000	2,100	17,000	NA	NA	NA	NA	NA	NA	29.54	6.80	22.74	0.1
MW-5	07/13/2004	66,000	5,900	10,000	1,900	16,000	NA	<50	<200	<200	<200	<500	29.54	9.28	20.26	0.1
MW-5	10/26/2004	6,600	670	110	7.4	2,000	NA	NA	NA	NA	NA	NA	29.54	8.75	20.79	0.8
MW-5	01/13/2005	9,500	1,300	950	360	1,900	NA	NA .	NA	NA	NA	NA	29.54	5.87	23.67	6.3
MW-5	04/28/2005	17,000	2,400	1,200	320	3,400	NA	NA	NA	NA	NA	NA	29.54	6.32	23.22	3.54
MW-5	08/01/2005	70,000	6,600	11,000	3,400	17,000	NA	<50	<200	<200	<200	<500	29.54	8.27	21.27	NA d
MW-5	10/05/2005	93,000	8,600	15,000	4,500	23,000	NA	NA	NA	NA	NA	NA	29.54	9.12	20.42	1.43
MW-5	01/11/2006	12,000	1,900	550	2,400	3,800	NA	<25	<25	<25	<25	<250	29.61	5.52	24.09	0.6
MW-5	05/26/2006	112,000	6,600	11,100	3,870	19,900 g	NA	<0.500	5.37	<0.500	<0.500	<10.0	29.61	7.02	22.59	0.45
MW-5	08/30/2006	281,000	8,050	15,400	4,770	26,800	NA	<0.500	<0.500	<0.500	60.6	<10.0	29.61	8.93	20.68	0.55/0.51
MW-5	11/08/2006	83,000	7,000	7,400	3,200	16,000	NA	NA	NA	NA	ŅA	NA	29.61	9.40	20.21	0.08/0.05

WELL CONCENTRATIONS

Former Shell Service Station 2703 Martin Luther King Jr. Way Oakland, CA

W-11 1D	D-4-	TDDU	<u> </u>	-		v	MTBE	MTBE	DIDE	FTDF	TA 845	TDA	TOO	Depth to	GW	DO
Well ID	Date	TPPH (ug/L)	B (ug/L)	T (ug/L)	E (ug/L)	X (ug/L)	8020 (ug/L)	8260 (ug/L)	DIPE (ug/L)	ETBE (ug/L)	TAME (ug/L)	TBA (ug/L)	(MSL)	Water (ft.)	Elevation (MSL)	Reading (ppm)
1		(# 3 : =/	(4.3. –/	(-3/	(9/	(-3,-)	(4.3.4.)	(-3·-/	(-3, -/	, (- <u>3</u> . –/	_ (g, -)	(-3,-)	(()	(02)	(PP-11)
MW-5	02/22/2007	35,000	9,500	13,000	5,300	23,000	NA	NA	NA	NA	NA	NA	29.61	6.87	22.74	1.17/3.17
MW-5	05/29/2007	94,000 i	6,400	9,900	4,300	22,000	NA	NA	NA	NA	NA	NA	29.61	7.85	21.76	0.08/0.19
MW-5	08/27/2007	110,000 i	6,900	11,000	4,300	22,000	NA	<100	<200	<200	<200	<1000	29.61	9.13	20.48	0.08/0.22
				· · · · · · · · · · · · · · · · · · ·												
MW-6	01/09/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	28.60	4.18	24.42	NA
MW-6	01/11/2006	150,000	9,300	1,60 0	5,100	24,000	NA ·	<2.5 f	17 f	<2.5 f	<2.5 f	51 f	28.60	4.50	24.10	3.6
MW-6	05/26/2006	67,300	6,930	870	2,440	7,590 g	NA	<5.00	10.1	<5.00	<5.00	<100	28.60	6.10	22.50	0.49
MW-6	08/30/2006	7,060	6,090	1,180	2,040	7,200	NA	<0.500	<0.500	<0.500	<0.500	<10.0	28.60	8.05	20.55	0.39/0.56
MW-6	11/08/2006	8,200	1,900	200	350	890	NA	NA	NA	NA	NA	NA	28.60	8.53	20.07	0.12/0.95
MW-6	02/22/2007	49,000	7,300	2,300	3,600	9,500	NA	NA	NA	NA	NA	NA	28.60	5.94	22.66	1.54/2.03
MW-6	05/29/2007	30,000 i,j	4,100	1,000	1,600	4,900	NA	NA	NA	NA	NA	NA	28.60	6.87	21.73	0.11/0.51
MW-6	08/27/2007	36,000 i	2,000	440	1,000	3,400	NA	<25	15 k	<50	<50	<250	28.60	8.22	20.38	0.08/0.15
								,		,						
MW-7	01/09/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	29.71	5. 50	24.21	NA
MW-7	01/11/2006	79,000	9,800	1,800	1,900	20,000	NA	<5.0 f	28 f	<5.0 f	<5.0 f	64 f	29.71	5.70	24.01	1.0
MW-7	05/26/2006	98,200	9,620	1,150	3,490	13,400 g	NA	<5.00	30.8	<5.00	<5.00	885	29.71	7.24	22.47	0.30
MW-7	08/30/2006	146,000	8,740	980	3,440	15,400	NA	<0.500	22.7	<0.500	<0.500	<10.0	29.71	9.03	20.68	0.51/0.46
MW-7	11/08/2006	61,000	6,600	880	2,800	12,000	NA	NA	NA	NA	NA	NA	29.71	9.49	20.22	0.02/0.13
MW-7	02/22/2007	50,000	3,400	910	2,200	13,000	NA	NA	NA	NA	NA	NA	29.71	7.00	22.71	0.96/2.57
MW-7	05/29/2007	26,000 i,j	2,700	320	850	3,590	NA	NA	NA	NA	NA	NA	29.71	8.01	21.70	0.09/0.15
MW-7	08/27/2007	37,000 i	3,300	240	1,300	4,060	NA	<25	20 k	<50	<50	<250	29.71	9.30	20.41	1.23/1.64
														<u> </u>		
MW-8	01/09/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	29.54	5.56	23.98	NA
MW-8	01/11/2006	32,000	2,400	180	66	5,500	NA	<0.50 f	15 f	<0.50 f	<0.50 f	35 f	29.54	5.53	24.01	0.8
MW-8	05/26/2006	24,800	423	73.0	166	2,820 g	NA ·	<0.500	2.18	<0.500	<0.500	<10.0	29.54	7.02	22.52	0.35
MW-8	08/30/2006	72,100	1,770	114	324	3,140	NA	<0.500	23.3	<0.500	<0.500	<10.0	29.54	8.81	20.73	0.51/0.50

							MTBE	MTBE						Depth to	GW	DO
Well ID	Date	TPPH	В	Т	E	X	8020	8260	DIPE	ETBE	TAME	TBA	TOC	Water	Elevation	Reading
		(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(MSL)	(ft.)	(MSL)	(ppm)
MW-8	11/08/2006	24,000	2,000	90	190	3,400	NA	NA	NA	NA	NA	NA	29.54	9.25	20.29	0.11/0.40
MW-8	02/22/2007	26,000	2,100	110	180	4,400	NA	NA	NA	NA	NA	. NA	29.54	7.08	22.46	1.37/1.71
MW-8	05/29/2007	31,000 i	2,600	99	250	3,140	NA	NA	NA	NA	NA	NA	29.54	7.81	21.73	0.05/0.49
MW-8	08/27/2007	41,000 i	3,400	110	260	3,880	NA	<20	32 k	<40	<40	<200	29.54	9.04	20.50	0.07/0.27
MW-12	05/19/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	31.16	8.42	22.74	NA
MW-12	05/26/2006	<50.0	<0.500	<0.500	<0.500	<0.500	NA	<0.500	<0.500	<0.500	<0.500	<10.0	31.16	8.44	22.72	3.88
MW-12	08/30/2006	746	<0.500	<0.500	<0.500	<0.500	NA	NA	NA	NA	NA	NA	31.16	9.54	21.62	1.75/1.81
MW-12	11/08/2006	<50	<0.50	<0.50	<0.50	<1.0	NA	NA	NA	NA	NA	NA	31.16	8.67	22.49	2.26/3.60
MW-12	02/22/2007	<50	<0.50	<1.0	<0.50	<1.0	NA	NA	NA	NA	NA :	NA	31.16	7.72	23.44	1.60/2.91
MW-12	05/29/2007	<50 i	0.49 k	<1.0	0.14 k	0.48 k	NA	NA	NA	NA	NA	NA	31.16	9.00	22.16	0.60/0.61
MW-12	08/27/2007	<50 i	<0.50	<1.0	<1.0	<1.0	NA	NA	NA	NA	NA	NA	31.16	9.90	21.26	0.47/0.24
																
MW-14	05/19/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	ΝA	NA	28.09	6.95	21.14	NA
MW-14	05/26/2006	103,000	5,280	76.7	3,930	4,800 g	NA	<5.00	49.7	<5.00	<5.00	895	28.09	7.05	21.04	3.60
MW-14	08/30/2006	10,200	1,260	12.5	1,310	1,330	NA	<0.500	<0.500	<0.500	<0.500	<10.0	28.09	9.19	18.90	3.33/3.49
MW-14	11/08/2006	29,000	4,400 h	34	2,000	1,600	NA	NA	NA	NA	NA	NA	28.09	9.80	18.29	1.16/1.40
MW-14	02/22/2007	31,000	2,600	42	2,200	1,600	NA	NA	NA	NA	NA	NA	28.09	6.70	21.39	0.59/1.11
MW-14	05/29/2007	35,000 i	1,100	14	1,800	767	NA	NA	NA	NA	NA	NA	28.09	7.89	20.20	0.08/0.08
MW-14	08/27/2007	Unable to	access we	ell :	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
MW-14	08/29/2007	45,000 i	1,000	11	870	367.8 k	NA	<10	20	<20	<20	<100	28.09	9.25	18.84	0.09/0.16
B-10 *	07/17/1996	20,000	400	<100	<100	870	<500	NA	NA	NA	NA	NA	NA	NA	NA	NA
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B-13*	07/17/1996	290,000	34,000	21,000	9,900	47,000	<2,500	NA	NA	NA	NA	NA	NA	NA	NA	NA

	<u> </u>		<u> </u>				MTBE	MTBE						Depth to	GW	DO
Well ID	Date	TPPH	В	Т	Ε	X	8020	8260	DIPE	ETBE	TAME	TBA	TOC	Water	Elevation	Reading
		(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(MSL)	(ft.)	(MSL)	(ppm)
V-1	08/02/1996	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	23.26	NA	NA	NA
V-1	08/05/1996	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA:	23.26	8.58	14.68	NA
V-1	10/17/1996	NA	NA	NA	NA	NA	NA	, NA	NA	NA	NA	NA	23.26	10.02	13.24	NA
V-1	01/16/1997	9,500	1,200	250	280	880	<50	NA	NA	NA	NA	NA	23.26	5.55	17.71	NA
V-1	04/07/1997	2,200	42	<5.0	130	15	<25	NA	NA	NA	NA	NA	23.26	7.40	15.86	- NA
V-1	07/02/1997	2,600	340	5.8	49	12	74	<4.0	NA	NA	NA	NA	23.26	8.94	14.32	NA
V-1	10/24/1997	57,000	5,200	2,300	3,600	16,000	1,900	<200	NA	NA	NA	NA	23.26	9.43	13.83	NA
V-1	01/09/1998	23,000	2,400	1,700	1,300	2,300	310	NA	NA	NA	NA	NA	23.26	6.81	16.45	NA
V-1 (D)	01/09/1998	24,000	2,500	1,800	1,400	2,400	450	NA	NA	NA	NA	NA	23.26	NA	NA	NA
V-1	04/02/1998	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	NA	NA	NA	NA	23.26	4.58	18.68	NA
V-1 (D)	04/02/1998	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	NA	NA	NA	NA	23.26	NA	NA	NA
V-1	07/14/1998	160	1.9	<0.50	4.2	<0.50	6.1	NA	NA	NA	NA	NA	23.26	7.51	15.75	NA
V-1	10/01/1998	440	18	<0.50	11	0.80	7.9	NA	NA	NA	NA _.	NA	23.26	8.49	14.77	NA
V-1	01/18/1999	697	55.7	0.839	28.2	<0.500	9.35	NA	NA	NA	NA	NA	23.26	8.59	14.67	NA
V-1	04/29/1999	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	NA	NA	NA	NA	23.26	8.69	14.57	NA
V-1	08/23/1999	457	33.4	3.59	16.3	<0.500	13.9	NA	NA	NA	NA	NA	23.26	8.99	14.27	NA
V-1	10/06/1999	714	53.7	0.740	8.69	<0.500	9.83	NA:	NA	NA	NA	NA	23.26	9.55	13.71	NA
V-1	01/27/2000	<50.0	<0.500	<0.500	<0.500	<0.500	<2.50	NA	NA	NA	NA	NA	23.26	7.19	16.07	NA
V-1	04/18/2000	<50.0	<0.500	<0.500	<0.500	<0.500	<2.50	NA	NA	NA	NA	NA	23.26	7.67	15.59	NA
V-1	07/19/2000	255	21.7	<0.500	10.2	<0.500	7.33	<1.00 a	NA	NA	NA	NA	23.26	7.53	15.73	NA
V-1	10/24/2000	200	4.05	0.566	<0.500	<0.500	7.82	NA	NA	NA	NA	NA	23.26	7.38	15.88	NA
V-1	01/04/2001	128	1.77	<0.500	<0.500	<0.500	6.40	<10.0 b	NA	NA	NA	NA	23.26	8.41	14.85	NA
V-1	05/03/2001	<50	<0.50	<0.50	<0.50	<0.50	NA	<5.0	NA	NA	NA	NA	23.26	7.20	16.06	NA
V-1	07/09/2001	110	4.4	<0.50	0.88	1.7	NA	<5.0	NA	NA	NA	NA	23.26	9.22	14.04	NA
V-1	10/18/2001	1,500	180	12	43	46	NA	<5.0	NA	NA	NA	NA	23.26	10.08	13.18	0.8
V-1	01/24/2002	210	7.1	15	4.6	32	NA	<5.0	NA	NA	NA	NA	23.26	6.44	16.82	3.5

Well ID	Date	ТРРН	В	т	E	х	MTBE 8020	MTBE 8260	DIPE	ETBE	TAME	TBA	тос	Depth to Water	GW Elevation	DO Reading
		(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(MSL)	(ft.)	(MSL)	(ppm)
	-															
V-1	04/04/2002	<50	<0.50	<0.50	<0.50	<0.50	NA	<5.0	NA	NA	NA	NA	23.26	6.18	17.08	1.0
V-1	07/18/2002	100	1.6	1.2	1.2	6.1	NA	<5.0	NA	NA	NA	NA	23.26	8.08	15.18	1.7
V-1	10/21/2002	210	1.4	<0.50	1.0	1.3	NA	<5.0	NA	NA	NA	NA	29.26	8.94	20.32	1.2
V-1	01/21/2003	61	5.2	<0.50	<0.50	<0.50	NA	<5.0	NA	NA	NA	NA	29.26	6.62	22.64	0.6
V-1	04/17/2003	<50	<0.50	<0.50	<0.50	1.2	NA	<5.0	NA	NA	NA	NA	29.26	6.00	23.26	1.3
V-1	07/22/2003	Well inacc	essible	NA	NA	NA	NA	NΑ	NA	NA	NA	NA	29.26	NA	NA	NA
V-1	10/20/2003	540	11	1.6	6.0	8.9	NA	<0.50	NA	NA	NA	NA	29.26	9.53	19.73	0.1
V-1	01/13/2004	<50	<0.50	<0.50	<0.50	<1.0	NA	<0.50	NA	NA	NA	NA	29.26	6.62	22.64	NA
V-1	01/22/2004	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	29.26	9.08	20.18	0.1
V-1	04/01/2004	<50	<0.50	<0.50	<0.50	<1.0	NA	NA	NA	NA	NA	NA	29.26	6.24	23.02	0.1
V-1	07/13/2004	120	1.8	<0.50	<0.50	<1.0	NA	<0.50	<2.0	<2.0	<2.0	<5.0	29.26	8.78	20.48	0.1
V-1	10/26/2004	<50	<0.50	<0.50	<0.50	<1.0	NA	NA	NA	NA	NA	NA	29.26	8.09	21.17	0.6
V-1	01/13/2005	<50	<0.50	<0.50	<0.50	<1.0	NA	NA	NA	NA	NA	NA	29.26	4.30	24.96	0.1
V-1	04/28/2005	<50	<0.50	<0.50	<0.50	<1.0	NA	NA	NA	NA	NA	NA	29.26	5.27	23.99	3.34
V-1	08/01/2005	54	<0.50	<0.50	<0.50	<1.0	NA	<0.50	<2.0	<2.0	<2.0	<5.0	29.26	7.77	21.49	NA d
V-1	10/05/2005	120 e	<0.50	<0.50	<0.50	<1.0	NA	NA	NA	NA	NA	NA	29.26	8.72	20.54	1.67
V-1	01/11/2006	<50	<0.50	<0.50	<0.50	<0.50	NA	<0.50	<0.50	<0.50	<0.50	<5.0	29.24	4.78	24.46	0.3
V-1	05/26/2006	<50.0	<0.500	<0.500	<0.500	1.02 g	NA	<0.500	<0.500	<0.500	<0.500	<10.0	29.24	6.61	22.63	1.94
V-1	08/30/2006	5,660	6.81	1.39	27.3	21.0	NA	<0.500	<0.500	<0.500	<0.500	<10.0	29.24	8.46	20.78	0.33/0.33
V-1	11/08/2006	1,300	3.7	1.5	5.1	6.9	NA	NA	NA	NA	NA	NA	29.24	8.95	20.29	0.05/0.11
V-1	02/22/2007	<50	<0.50	<1.0	<0.50	<1.0	NA	NA	NA	NA	NA	NA	29.24	6.17	23.07	0.76/0.99
V-1	05/29/2007	650 i	0.64	<1.0	1.2	0.95 k	NA	NA	NA	NA	NA	NA	29.24	7.21	22.03	0.69/0.74
V-1	08/27/2007	510 i, j	0.24	<1.0	<1.0	<1.0	NA	<1.0	<2.0	<2.0	<2.0	<10	29.24	8.78	20.46	0.12/0.57
V-2	08/02/1996	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	22.80	NA	NA	NA
V-2	08/05/1996	NA	NA	NA	NA	NA	NA	NA	NA	NA:	NA	NA	22.80	7.94	14.86	NA

							MTBE	MTBE						Depth to	GW	DO
Well ID	Date	TPPH	В	Т	E	χ	8020	8260	DIPE	ETBE	TAME	TBA	TOC	Water	Elevation	Reading
L	<u> </u>	(ug/L)	(MSL)	(ft.)	(MSL)	(ppm)										
V-2	10/17/1996	NA	22.80	9.30	13.50	NA										
V-2	01/08/1997	69,000	4,800	2,800	2,700	13,000	750	NA	NA	NA	NA	NA	22.80	5.82	16.98	NA
V-2	04/07/1997	90,000	4,400	1,900	3,300	14,000	<500	NA	NA	NA	NA	NA	22.80	7.10	15.70	NA
V-2 (D)	04/07/1997	77,000	4,400	2,000	3,200	14,000	<250	NA	NA	NA	NA	NA	22.80	NA	NA	NA
V-2	07/02/1997	82,000	5,500	2,700	3,500	16,000	530	<100	NA	NA	NA	NA	22.80	8.35	14.45	NA
V-2 (D)	07/02/1997	85,000	5,600	2,800	3,600	17,000	520	<100	NA	NA	NA	NA	22.80	NA	NA	NA
V-2	10/24/1997	7,300	1,100	97	230	180	91	<12	NA	NA	NA	NA	22.80	10.03	12.77	NA
V-2 (D)	10/24/1997	12,000	1,700	340	650	630	120	<20	NA	NA	NA	NA	22.80	NA	NA	NA
V-2	01/09/1998	40,000	4,100	1,500	2,500	9,000	280	NA	NA	NA	NA	NA	22.80	6.94	15.86	NA
V-2	04/02/1998	62,000	6,800	2,400	3,400	14,000	<250	NA	NA	NA	NA	NA.	22.80	5.35	17.45	NA
V-2	07/14/1998	43,000	4,700	1,100	2,500	6,600	<250	NA	NA	NA	NA	NA	22.80	6.48	16.32	NA
V-2 (D)	07/14/1998	48,000	5,100	1,300	2,600	8,100	<250	NA	NA	NA	NA	NA	22.80	NA NA	NA	NA
V-2	10/01/1998	53,000	5,200	1,800	3,200	10,000	83	NA	NA	NA	NA	NA	22.80	8.41	14.39	NA
V-2 (D)	10/01/1998	55,000	5,300	1,900	3,300	11,000	65	NA	NA	NA	NA	NA	22.80	NA	NA	NA
V-2	01/18/1999	47,100	5,800	1,960	3,450	10,200	<100	NA	NA	NA	NA	NA	22.80	8.29	14.51	NA
V-2	04/29/1999	65,000	6,100	2,800	3,200	12,000	540	NA	NA	NA	NA	NA	22.80	8.19	14.61	NA
V-2	08/23/1999	59,600	6,240	2,190	3,900	14,700	390	NA	NA	NA	NA	NA	22.80	8.44	14.36	NA
V-2	10/06/1999	63,800	4,820	1,860	2,840	11,100	<1000	NA	NA	NA	NA	NA	22.80	8.96	13.84	NA
V-2	01/27/2000	59,600	10,200	2,840	3,450	12,100	<500	NA	NA	NA	NA	NA	22.80	7.57	15.23	NA
V-2	04/18/2000	45,000	6,050	2,700	3,340	12,200	<250	NA	NA	NA	NA	NA	22.80	8.14	14.66	NA
V-2	07/19/2000	31,800	4,440	1,270	2,390	6,820	<500	NA	NA	NA	NA	NA	22.80	8.21	14.59	NA
V-2	10/24/2000	40,100	4,810	1,730	2,960	8,650	734	<10.0	NA	NA	NA	NA	22.80	8.53	14.27	NA
V-2	01/04/2001	37,500	4,510	1,390	2,710	6,880	375	NA	NA	NA	NA	NA	22.80	8.03	14.77	NA
V-2	05/03/2001	51,000	4,000	1,900	2,800	8,200	NA	<200	NA	NA	NA	NA	22.80	6 .63	16.17	NA
V-2	07/09/2001	9,600	710	190	180	1,400	NA	<25	NA	NA	NA	NA	22.80	8.75	14.05	NA
V-2	10/18/2001	20,000	2,000	540	560	6,000	NA	<50	NA	NA	NA	NA	22.80	9.60	13.20	0.4

"							MTBE	MTBE						Depth to	GW	DO
Well ID	Date	TPPH	В	Т	E	X	8020	8260	DIPE	ETBE	TAME	TBA	TOC	Water	Elevation	Reading
		(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(ug/L)	(MSL)	(ft.)	(MSL)	(ppm)
V-2	01/24/2002	36,000	2,900	870	1,700	5,900	NA	<100	NA	NA	NA	NA	22.80	5.93	16.87	4.0
V-2	04/04/2002	49,000	3,900	1,500	2,900	9,300	NA	<200	NA	NA	NA	NA	22.80	5.78	17.02	0.9
V-2	07/18/2002	50,000	3,600	1,300	2,800	9,300	NA	<200	NA	NA	NA	NA	22.80	7.58	15.22	1.3
V-2	10/21/2002	86,000	6,000	1,900	4,200	20,000	NA	<250	NA	NA	NA	NA	28.80	8.40	20.40	1.3
V-2	01/21/2003	13,000	630	200	300	2,400	NA	<25	NA	NA	NA	NA	28.80	6.52	22.28	1.2
V-2	04/17/2003	26,000	2,000	570	750	6,000	NA	<100	NA	NA	NA	NA	28.80	5.93	22.87	1.1
V-2	07/22/2003	6,800	130	34	150	440	NA	<2.5	NA	NA	NA	NA	28.80	7.96	20.84	1.4
V-2	10/20/2003	14,000	660	160	260	2,400	NA	<10	NA	NA	NA	NA	28.80	9.21	19.59	0.7
V-2	01/13/2004	20,000	1,400	410	700	4,200	NA	<13	NA	NA	NA	NA	28.80	6.90	21.90	NA
V-2	01/22/2004	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	28.80	8.50	20.30	0.1
V-2	04/01/2004	28,000	2,000	520	650	8,700	NA	NA	NA	NA	NA	NA	28.80	6.84	21.96	0.2
V-2	07/13/2004	21,000	1,900	460	1,000	4,300	NA	NA	NA	NA	NA	NA	28.80	8.28	20.52	0.1
V-2	10/26/2004	43,000	2,700	880	2,300	12,000	NA	NA	NA	NA	NA	NA	28.80	8.43	20.37	0.8
V-2	01/13/2005	23,000	1,400	330	1,800	5,800	NA	NA	NA	NA	NA	NA	28.80	6.67	22.13	0.6
V-2	04/28/2005	16,000	970	230	620	3,800	NA	NA	NA	NA	NA	NA	28.80	5.69	23.11	4.55
V-2	08/01/2005	14,000	610	190	450	3,600	NA	NA	NA	NA	NA	NA	28.80	5.25	23.55	NA d
V-2	10/05/2005	37,000	2,200	680	2,300	8,500	NA	NA	NA	NA	NA	NA	28.80	8.24	20.56	0.75
V-2	01/11/2006 f	45,000	1,900	720	3,000	13,000	NA	<25	<25	<25	<25	<250	28.81	6.60	22.21	0.4
V-2	05/26/2006	66,600	1,300	400	2,950	9,700 g	NA	<0.500	<0.500	<0.500	<0.500	<10.0	28.81	6.28	22.53	0.28
V-2	08/30/2006	7,290	2,390	750	4,680	17,000	NA	NA	NA	NA	NA	NA	28.81	8.03	20.78	0.37/0.31
V-2	11/08/2006	68,000	1,700	580	3,900	13,000	NA	NA	NA	NA	NA	NA	28.81	8.60	20.21	0.05/0.14
V-2	02/22/2007	57,000	1,300	600	4,000	15,000	NA	NA	NA	NA	NA	NA	28.81	5.88	22.93	1.23/2.50
V-2	05/29/2007	48,000 i,j	2,000	650	3,300	10,000	NA	NA	NA	NA	NA	NA	28.81	6.82	21.99	0.07/0.12
V-2	08/27/2007	55,000 i	1,600	520	2,900	8,000	NA	NA	NA	NA	NA	NA	28.81	8.22	20.59	0.22/0.48

WELL CONCENTRATIONS

Former Shell Service Station 2703 Martin Luther King Jr. Way Oakland, CA

							MTBE	MTBE						Depth to	GW	DO
Well ID	Date	TPPH	В	Т	E	X	8020	8260	DIPE	ETBE	TAME	TBA	TOC	Water	Elevation	Reading
		(ug/L)	(MSL)	(ft.)	(MSL)	(ppm)										

Abbreviations:

TPPH = Total petroleum hydrocarbons as gasoline by EPA Method 8260B; prior to May 3, 2001, analyzed by EPA Method 8015.

BTEX = Benzene, toluene, ethylbenzene, xylenes by EPA Method 8260B; prior to May 3, 2001, analyzed by EPA Method 8020.

MTBE = Methyl tertiary butyl ether

DIPE = Di-isopropyl ether, analyzed by EPA Method 8260B

ETBE = Ethyl tertiary butyl ether, analyzed by EPA Method 8260B

TAME = Tertiary amyl methyl ether, analyzed by EPA Method 8260B

TBA = Tertiary butyl alcohol, analyzed by EPA Method 8260B

TOC = Top of Casing Elevation

SPH = Separate-Phase Hydrocarbons

GW = Groundwater

DO = Dissolved Oxygen reading

n/n = Pre-purge/Post-purge DO reading

ug/L = Parts per billion

ppm = Parts per million

MSL = Mean sea level

ft. = Feet

<n = Below detection limit

(D) = Duplicate sample

NA = Not applicable

WELL CONCENTRATIONS

Former Shell Service Station 2703 Martin Luther King Jr. Way Oakland, CA

							MTBE	MTBE						Depth to	GW	DO
Well ID	Date	TPPH	В	T	E	Χ	8020	8260	DIPE	ETBE	TAME	TBA	TOC	Water	Elevation	Reading
		(ug/L)	(MSL)	(ft.)	(MSL)	(ppm)										

Notes:

- a = This sample analyzed outside of EPA recommended holding time.
- b = Due to error of Sequoia Analytical laboratories, well V-1 confirmed for MTBE by EPA Method 8260 instead of V-2.
- c = Hydrocarbon does not match pattern of laboratory's standard.
- d = Dissolved oxygen reading not taken due to meter malfunction.
- e = Quantity of unknown hydrocarbon(s) in sample based on gasoline.
- f = Sample was originally analyzed within the EPA recommended hold time. Re-analysis for dilution was performed past the recommended hold time.
- g = Analyte was detected in the associated Method Blank.
- h = Initial analysis within holding time. Reanalysis for the required dilution or confirmation was past holding time.
- i = Analyzed by EPA Method 8015B (M).
- j = The sample chromatographic pattern for TPH does not match the chromatographic pattern of the specified standard. Quantitation of the unknown hydrocarbon(s) in the sample was based upon the specified standard.
- k = Analyte was detected at a concentration below the reporting limit and above the laboratory method detection limit. Reported value is estimated.
- * = Water sample from Boring.

Site surveyed June 14, 2001 by Virgil Chavez Land Surveying of Vallejo, CA.

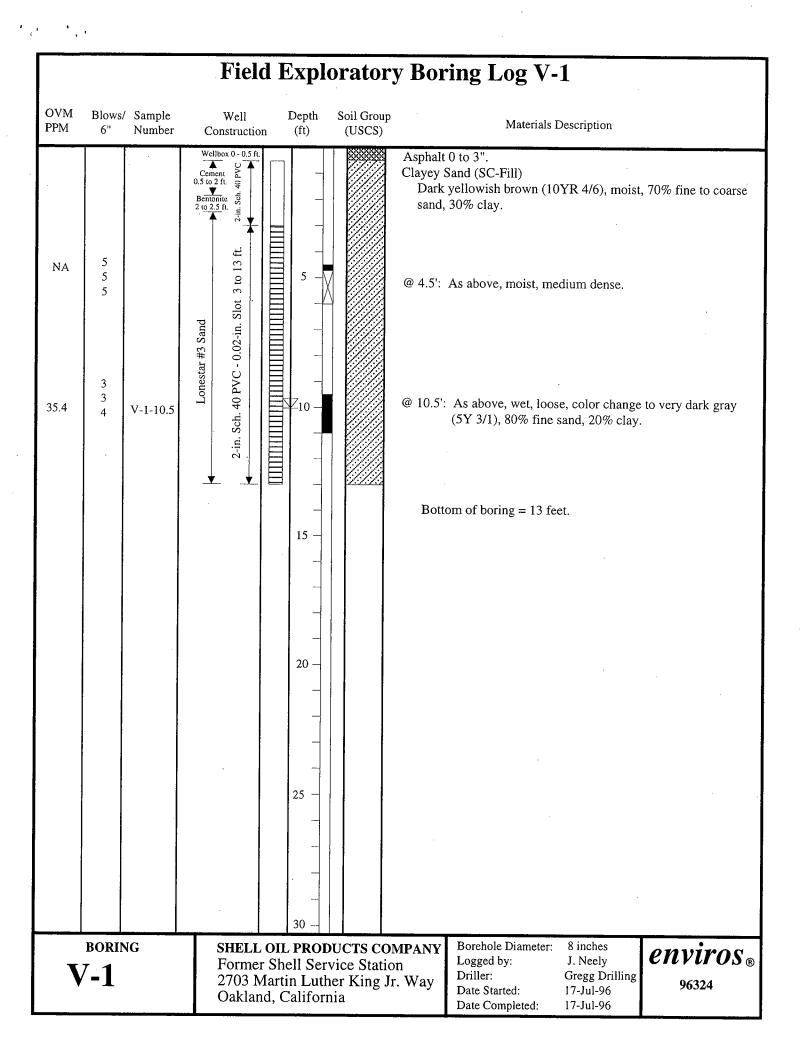
Site surveyed August 13, 2002 by Virgil Chavez Land Surveying of Vallejo, CA.

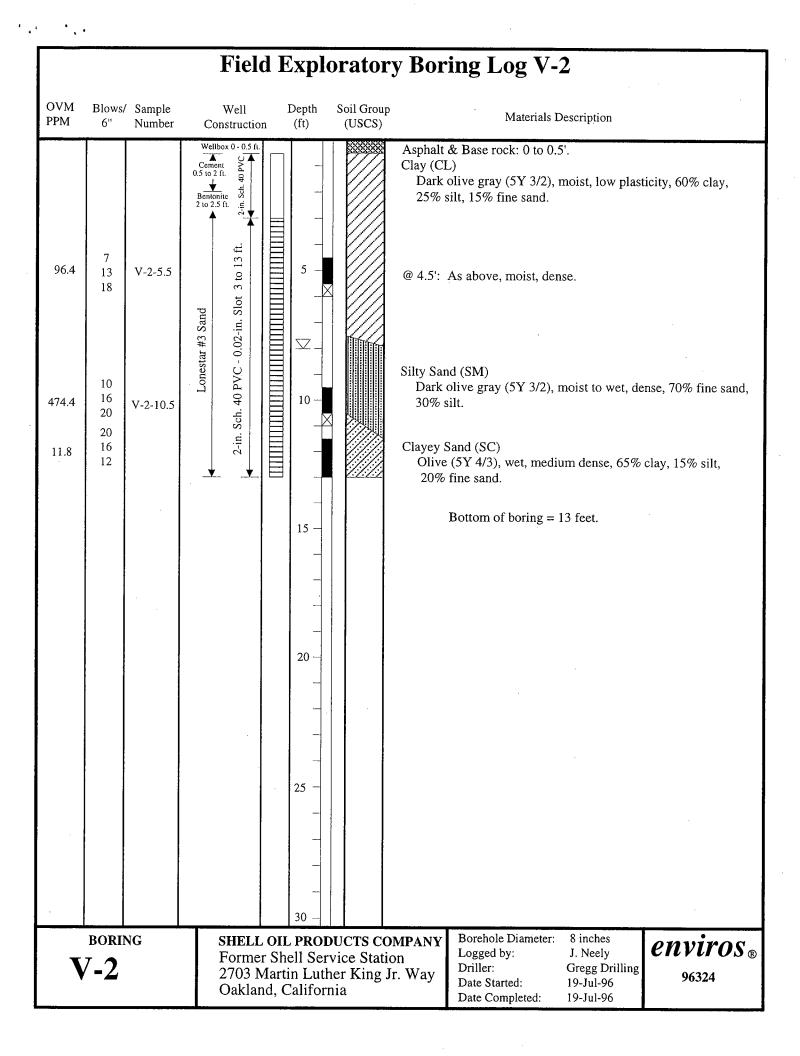
Wells MW-1 through MW-8, V-1, and V-2 surveyed on February 14, 2006 by Virgil Chavez Land Surveying of Vallejo, CA..

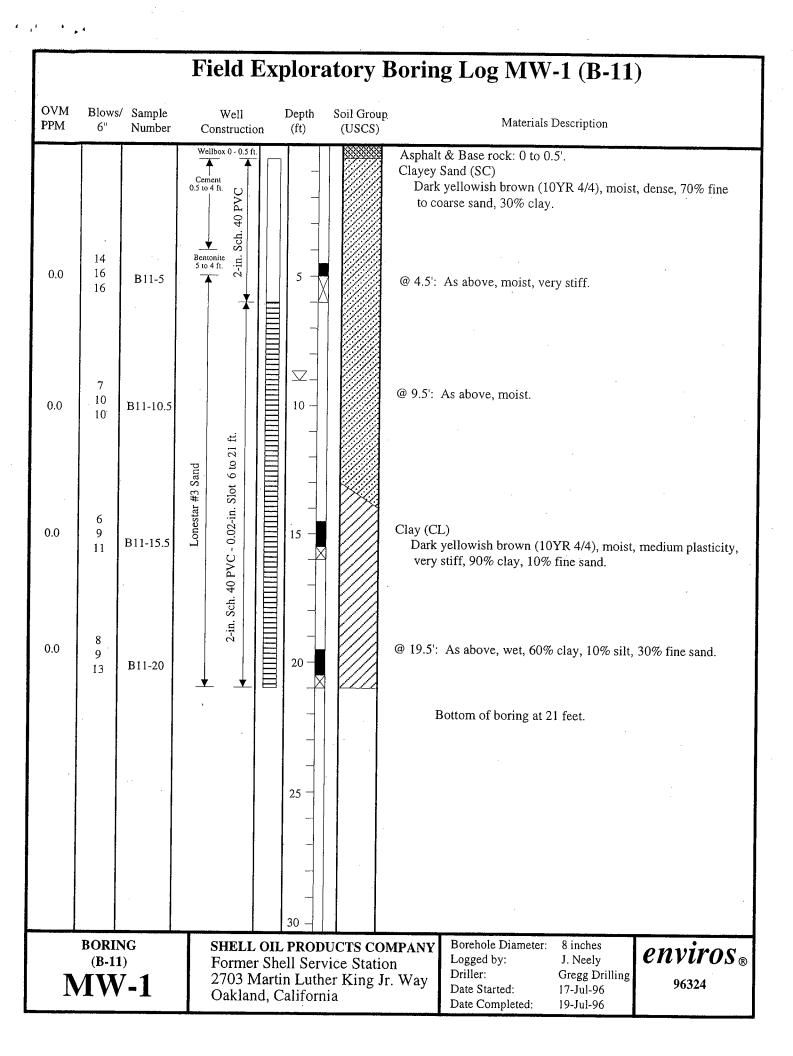
Wells MW-12 and MW-14 surveyed on April 19, 2006 by Virgil Chavez Land Surveying of Vallejo, CA..

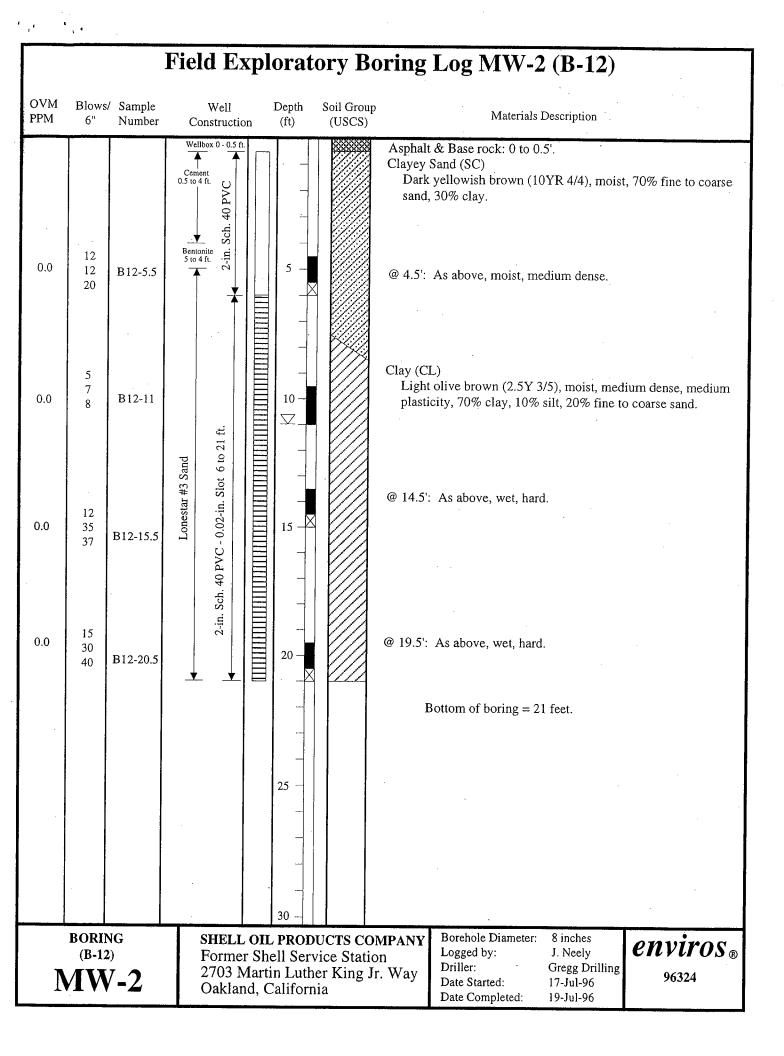
ATTACHMENT 4

Available Boring and Well Logs







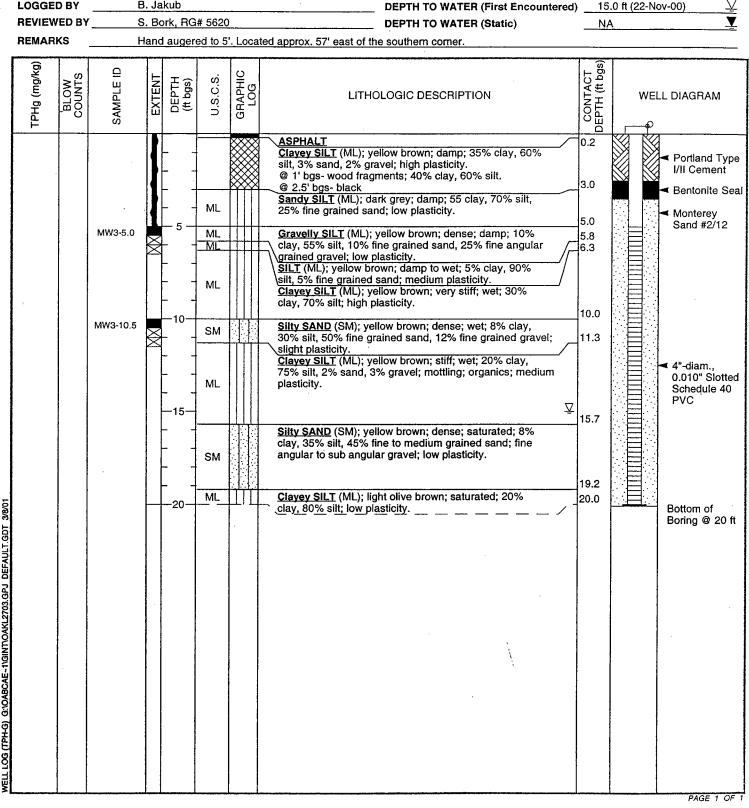






Cambria Environmental Technology, Inc. 1144 - 65th St. Oakland, CA 94608 Telephone: (510) 420-0700 Fax: (510) 420-9170

CLIENT NAME Equiva Services LLC BORING/WELL NAME MW-3 **JOB/SITE NAME** oakl2703 22-Nov-00 DRILLING STARTED DRILLING COMPLETED 22-Nov-00 LOCATION 2703 Martin Luther King, Oakland **PROJECT NUMBER** 242-0781 WELL DEVELOPMENT DATE (YIELD) NA DRILLER Gregg Drilling Not Surveyed **GROUND SURFACE ELEVATION** DRILLING METHOD Hollow-stem auger TOP OF CASING ELEVATION Not Surveyed BORING DIAMETER SCREENED INTERVAL 5 to 20 ft bgs LOGGED BY B. Jakub DEPTH TO WATER (First Encountered) ___15.0 ft (22-Nov-00) REVIEWED BY ___ S. Bork, RG# 5620 NA **DEPTH TO WATER (Static)**



BORING/WELL LOG



Cambria Environmental Technology, Inc. 1144 - 65th St. Oakland, CA 94608

Telephone: (510) 420-0700 Fax: (510) 420-9170

CLIENT NAME	Equiva Services LLC	BORING/WELL NAME MW-4
JOB/SITE NAME	oaki2703	DRILLING STARTED 21-Nov-00
LOCATION	2703 Martin Luther King, Oakland	DRILLING COMPLETED 21-Nov-00
PROJECT NUMBER	242-0781	WELL DEVELOPMENT DATE (YIELD) NA
DRILLER _	Gregg Drilling	GROUND SURFACE ELEVATION Not Surveyed
DRILLING METHOD	Hollow-stem auger	TOP OF CASING ELEVATION Not Surveyed
BORING DIAMETER	10"	SCREENED INTERVAL 5 to 20 ft bgs
LOGGED BY	B. Jakub	DEPTH TO WATER (First Encountered) NA $\overline{\Sigma}$
REVIEWED BY	S. Bork, RG# 5620	DEPTH TO WATER (Static) NA
		The state of the s

REMARKS Hand augered to 5'. Located approx. 23' north of the southern corner CONTACT DEPTH (# bgs) TPHg (mg/kg) BLOW GRAPHIC LOG DEPTH (ft bgs) EXTENT U.S.C.S. SAMPLE LITHOLOGIC DESCRIPTION WELL DIAGRAM **ASPHALT** 0.1 Clayey GRAVEL(GC); dark yellowish brown; 1.0 Portland Type moist-damp; 15% clay, 10% silt, 5% sand, 70% gravel; no I/II Cement Silty CLAY(CL); black; moist-damp; 60% clay, 40% silt; ■ Bentonite Seal high plasticity. @ 3.5' fbg- dark greenish gray. Monterey Sand #2/12 MW4-5.0 @ 5' bgs- mottled; 60% clay, 25% silt, 15% fine grained sand. 10.0 MW4-10.5 Clayey SAND (SP); olive gray/dark yellow brown; moist-wet; 25% clay, 10% silt, 65% fine grained sand; mottled; medium to high plasticity. 4"-diam., 0.010" Slotted Schedule 40 SP **PVC** @ 15' bgs- 25% clay, 10% silt, 55% sand, 10% gravel. 18.5 <u>Gravelly SILT(ML)</u>; olive brown; saturated; 10% clay, 60% silt, 5% sand, 25% gravel; low plasticity. ML 20.0 Bottom of Boring @ 20 ft WELL LOG (TPH-G) G:\OABCAE~1\GINT\OAKL2703.GPJ DEFAULT.GDT PAGE 1 OF





Cambria Environmental Technology, Inc. 1144 - 65th St. Oakland, CA 94608

Telephone: (510) 420-0700

Fax: (510) 420-9170

CLIENT NAME	Equiva Services LLC	BORING/WELL NAME MW-5	
JOB/SITE NAME	oakl2703	DRILLING STARTED 21-Nov-00	
LOCATION	2703 Martin Luther King, Oakland	DRILLING COMPLETED 21-Nov-00	
PROJECT NUMBER	242-0781	WELL DEVELOPMENT DATE (YIELD) NA	_
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION Not Surveyed	
DRILLING METHOD	Hollow-stem auger	TOP OF CASING ELEVATION Not Surveyed	
BORING DIAMETER	10"	SCREENED INTERVAL 5 to 20 ft bgs	
LOGGED BY	B. Jakub	DEPTH TO WATER (First Encountered) 10.0 ft (22-Nov-00)	$\overline{\mathbb{Q}}$
REVIEWED BY	S. Bork, RG# 5620	DEPTH TO WATER (Static) NA	Ī
DEMARKS	Hand augered to 5' Located approx 10' as	est of the car port	

CONTACT DEPTH (# bgs) TPHg (mg/kg) GRAPHIC LOG BLOW COUNTS EXTENT DEPTH (ft bgs) U.S.C.S. SAMPLE LITHOLOGIC DESCRIPTION WELL DIAGRAM 0.2 FILL brown; dense; dry; 40% silt, 10% sand, 50% 1.2 Portland Type. gravel; low plasticity.

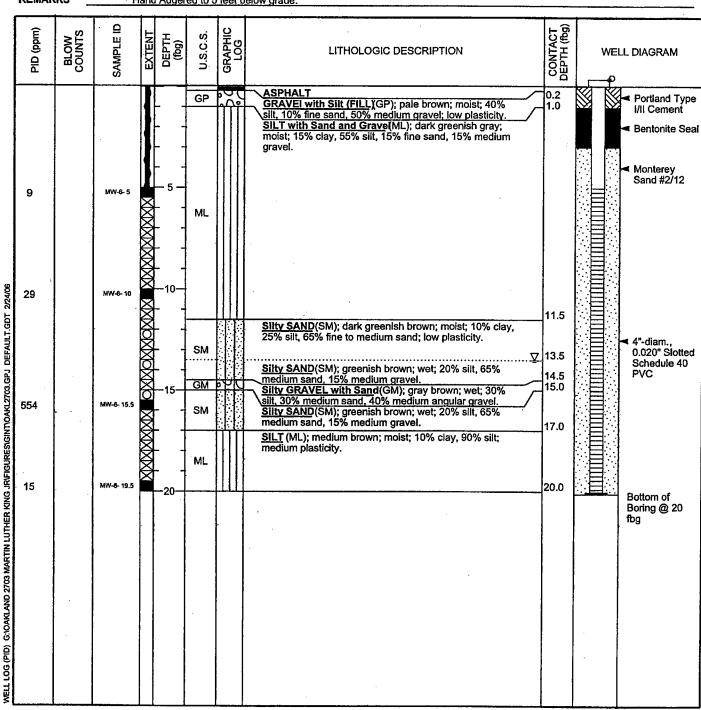
Clayey SILT (ML) very dark brown; very stiff; dry; 40% clay, 60% silt; medium plasticity. I/II Cement ML 3.0 Bentonite Seal Silty SAND (SM); very dark brown; dense; damp; 10% SM clay, 35% silt, 53% fine grained sand, 2% gravel; low Monterey 5.0 plasticity. Sand #2/12 MW5-5.0 Clayey SILT (ML); olive brown; very stiff; dry to moist; 25% clay, 50% silt, 23% sand, 2% gravel; low plasticity. ML @ 10' bgs- saturated; 40% clay, 60% silt; medium to high MW5-10.5 plasticity. 11.3 Clayey SAND(SC); dark greenish grey; very stiff; saturated; 15% clay, 13% silt, 70% fine grained sand, 2% 4"-diam., fine subangular grained gravel; low plasticity. SC 0.010" Slotted Schedule 40 **PVC** 15.0 Gravelly SILT (ML); olive brown; saturated; 10% clay, 70% silt, 5% fine grained sand, 2% fine subangulare grained gravel; low plasticity. ML @ 18.5' bgs- interbedded silt and gravelly silt; yellowish brown; saturated; 5% clay, 90% silt, 5% gravel; low 20.0 -20 WELL LOG (TPH-G) G:QABCAE~11GINT1OAKL2703.GPJ DEFAULT.GDT 3/8/01 plasticity. Bottom of Boring @ 20 ft



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BORING/WELL LOG

CLIENT NAME	Shell Oil Products US	BORING/WELL NAME MW-6
JOB/SITE NAME	2703 Martin Luther King Jr. Way	DRILLING STARTED04-Jan-06
LOCATION _	Oakland, California	DRILLING COMPLETED 04-Jan-06
PROJECT NUMBER_	247-0781-007	WELL DEVELOPMENT DATE (YIELD) NA
DRILLER _	Gregg Drilling	GROUND SURFACE ELEVATION 29.24 ft above msl
DRILLING METHOD_	Hollow-stem auger	TOP OF CASING ELEVATION 28.60 ft above msl
BORING DIAMETER_	8"	SCREENED INTERVALS 5 to 20 fbg
LOGGED BY	B. DeBoer	DEPTH TO WATER (First Encountered) 13.5 fbg (04-Jan-06)
REVIEWED BY	A. Friel, PG	DEPTH TO WATER (Static) NA
REMARKS	Hand Augered to 5 feet below grade.	





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BORING/WELL LOG

CLIENT NAME Shell Oil Products US BORING/WELL NAME MW-7 **JOB/SITE NAME** 2703 Martin Luther King Jr. Way **DRILLING STARTED** 04-Jan-06 DRILLING COMPLETED 04-Jan-06 LOCATION Oakland, California PROJECT NUMBER 247-0781-007 WELL DEVELOPMENT DATE (YIELD) NA DRILLER **Gregg Drilling GROUND SURFACE ELEVATION** 30.10 ft above msl **DRILLING METHOD** Hollow-stem auger TOP OF CASING ELEVATION 29.71 ft above msl **BORING DIAMETER** SCREENED INTERVALS 5 to 20 fbq **LOGGED BY** B. DeBoer DEPTH TO WATER (First Encountered) 12.5 fbg (04-Jan-06) **REVIEWED BY** A. Friel, PG **DEPTH TO WATER (Static)** NA REMARKS

Hand Augered to 5 feet below grade. SAMPLE ID GRAPHIC LOG CONTACT DEPTH (fbg) (mdd) BLOW EXTENT DEPTH (fbg) U.S.C.8 LITHOLOGIC DESCRIPTION WELL DIAGRAM 문 ASPHALT

GRAVEI with Silt (FILL)(GP); pale brown; moist; 40% silt, 10% fine sand, 50% medium gravel; low plasticity.

SILT (ML); dark brown to black; moist; 25% clay, 75% silt; medium plasticity. 0.2 GP ■ Portland Type 1.0 I/II Cement **Bentonite Seal** Monterey Sand #2/12 10 MW-7- 5.5 ML 11.5 DEFAULT.GDT 11 MW-7-11 5 Silty SAND with Gravel (SM); light brown; moist to wet; 15% silt, 60% medium sand, 25% medium gravel. SM 4"-diam., 13.0 0.020" Slotted GM Silty GRAVEL with Sand(GM); light brown; wet; 15% 13.5 silt, 25% medium sand, 65% medium gravel.

SILT with Gravel(ML); light brown; moist; 20% clay, 70% silt, 10% medium gravel; medium plasticity. Schedule 40 JRIFIGURESIGINTIOAKI 2703 GPJ **PVC** ML 16.0 Silty SAND with Gravel(SM); light brown with green; wet; 15% silt, 65% fine sand, 20% medium gravel. 360 MW-7- 16.5 SM 19.0 Sandy SILT(ML); medium brown; moist; 70% silt, 30% fine to medium sand; medium plasticity. ML 59 MW-7- 19 5 20.0 20 G:\OAKLAND 2703 MARTIN LUTHER KING Bottom of Boring @ 20 fbg LOG (PID)



DEFAULT.GDT 2/24/06

WELL LOG (PID) GNOAKLAND 2703 MARTIN LUTHER KING JRIFIGURESIGINTIOAKL2703.GPJ

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BORING/WELL LOG

CLIENT NAME	Shell Oil Products US	BORING/WELL NAME MW-8	
JOB/SITE NAME	2703 Martin Luther King Jr. Way	DRILLING STARTED 03-Jan-06	
LOCATION _	Oakland, California	DRILLING COMPLETED 03-Jan-06	
PROJECT NUMBER_	247-0781-007	WELL DEVELOPMENT DATE (YIELD) NA	
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION 30.10 ft above msl	
DRILLING METHOD_	Hollow-stem auger	TOP OF CASING ELEVATION 29.54 ft above msl	
BORING DIAMETER_	8"	SCREENED INTERVALS 5 to 20 fbg	
LOGGED BY	B. DeBoer	DEPTH TO WATER (First Encountered) 12.0 fbg (03-Jan-06)	\overline{Z}
REVIEWED BY	A. Friel, PG	DEPTH TO WATER (Static) NA	Ţ
REMARKS	Hand Augered to 5 feet below grade.		

CONTACT DEPTH (fbg) PID (ppm) SAMPLE ID GRAPHIC LOG BLOW COUNTS EXTENT U.S.C.S. DEPTH (fbg) LITHOLOGIC DESCRIPTION WELL DIAGRAM ASPHALT

GRAVEI with Silt (FILL)(GP); pale brown; moist; 40% silt, 10% fine sand, 50% medium gravel; low plasticity.

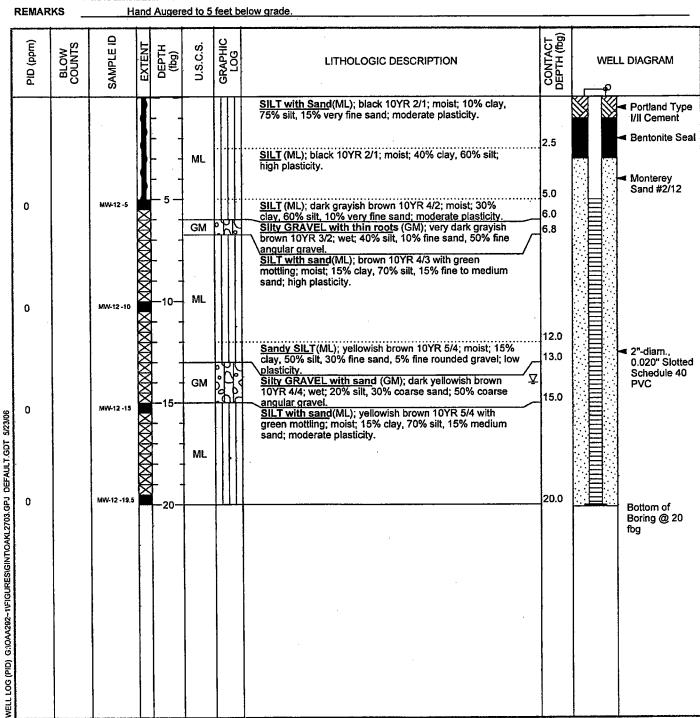
SILT (ML); greenish gray; moist; 20% clay, 70% silt, 10% fine sand; medium plasticity. 0.2 1.0 GP ■ Portland Type I/II Cement Bentonite Seal Monterey Sand #2/12 ML 0.2 MW-8- 6.5 10.0 Silty GRAVEL with Sand(GP); 15% silt, 15% fine sand, 60% medium gravel. $[\cdot \circlearrowleft]$ 37 ,0°C 立 GP 4"-diam., 0.020" Slotted 13.5 GRAVEL with Silt and Sand(GP); medium brown with green; wet; 10% silt, 30% fine sand, 60% medium gravel. SAND with Grave(SP); medium brown; wet; 80% coarse sand, 20% medium gravel. Schedule 40 14.5 SP 19.0 SILT with Sand(ML); light brown; moist; 15% clay, 70% silt, 15% medium sand; medium plasticity. ML 116 MW-8- 19.5 20.0 20 Bottom of Boring @ 20 fbg

BORING/WELL LOG



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CLIENT NAME	Shell Oil Products US	BORING/WELL NAME MW-12	
JOB/SITE NAME _	2703 Martin Luther King Jr. Way	DRILLING STARTED 28-Feb-06	
LOCATION	Oakland, California	DRILLING COMPLETED 28-Feb-06	
PROJECT NUMBER_	247-0781-010	WELL DEVELOPMENT DATE (YIELD) NA	
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION 31.60 f	ft above msl
DRILLING METHOD_	Hollow-stem auger	TOP OF CASING ELEVATION 31.16 ft above r	nsi
BORING DIAMETER_	8"	SCREENED INTERVALS 5 to 20 fbg	
LOGGED BY	B. DeBoer	DEPTH TO WATER (First Encountered) 14.0) fbg (28-Feb-06)
REVIEWED BY	A. Friel, PG	DEPTH TO WATER (Static) NA	Ţ
REMARKS	Hand Augered to 5 feet below grade.		







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CLIENT NAME	Shell Oil Products US	BORING/WELL NAME MW-14		
JOB/SITE NAME	2703 Martin Luther King Jr. Way	DRILLING STARTED 28-Feb-06		
LOCATION	Oakland, California	DRILLING COMPLETED 28-Feb-06		
PROJECT NUMBER_	247-0781-010	WELL DEVELOPMENT DATE (YIELD)	NA	
DRILLER _	Gregg Drilling	GROUND SURFACE ELEVATION 2	28.33 ft above msl	
DRILLING METHOD_	Hand-auger	TOP OF CASING ELEVATION 28.09 ft at	pove msl	
BORING DIAMETER_	4"	SCREENED INTERVALS 5 to 14.5 f	ъд	
LOGGED BY	B. DeBoer	DEPTH TO WATER (First Encountered)	11.0 fbg (28-Feb-06)	Ϋ́
REVIEWED BY	A. Friel, PG	DEPTH TO WATER (Static)	NA ·	Ţ
DEMARKS				

REVIEWED BY_	A. Frie	el, PG	DEPTH TO WATER (Static)	NA	<u> </u>
REMARKS					
PID (ppm) BLOW COUNTS	SAMPLE ID EXTENT	(fbg) U.S.C.S.	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	ELL DIAGRAM
ESIGINTOAKI.2703.GPJ DEFAULT.GDT 5/2306 + 000	MW-14 -14 [EXX	DEF CONTRACTOR OF CONTRACTOR O	CONCRETE SILT (ML); black 10YR 2/1; moist; 25% clay, 75% silt; high plasticity. SILT (ML); dark brown 10YR 3/3; dry; 40% clay, 60% silt; high plasticity. SILT with sand(ML); dark yellowish brown 10YR 4/4; dry; 25% clay, 60% silt, 15% coarse sand; high plasticity. SILT (ML); dark grayish brown 10YR 4/2; dry; 40% clay, 60% silt; high plasticity. SILT (ML); greenish gray GLEY1 5/5GY; moist; 15% clay, 95% cilt; moderate plasticity.	0.2 5.0 8.0 9.5 Z. 11.0	Portland Type I/II Cement Bentonite Seal Monterey Sand #2/12 1"-diam., 0.020" Slotted Schedule 40 PVC Bottom of Boring @ 14.5 fbg
Well log (PID) G:\OAA232-1VFIGH					

Environmental Control Associates, Inc. Pneumatic Sampler.	HNu (ppm)	SAMPLE #	Sample Interval	Depth (feet)	LOGGED PROJECT	NT: Pneumatic Sampler (1" O.D.) BY: M. Kaltreider T: 2703 Martin Luther King Jr. Wy DATE: 5/23/95
<u>Munsell Color Scale</u>				2	Si	sphalt Pavement/Baserock: gravel. andy Clay (CL), dark greenish gray, nedium plasticity, medium stiff, noist (moderate hydrocarbon odor).
(10YR - 3/2)	30	B1-5		4 6		andy Clay (CL), as above prox. 0.5 to 0.75" non-aqueous
(5Y - 3/2)	60	No Sample		— ∑ 10	pro Rei sla	oduct on water. fusal at 9', possible tank hold-down b. BOTTOM OF BORING @ 9 feet
				12		(Refusal encountered)
				— 14 <i>-</i> — 16 <i>-</i>		
				<u> </u>	-	• •
	,			20 22		
				— 24 —		÷
				— 26 <i>-</i> — 28 —		•
ACC ENVIRONMENTAL C				JOB NO: (6254-1.0	LOG OF BORING B-1
1000 ATLANTIC AVEUN ALAMEDA, CA				DATE: 6	/24/95	2703 Martin Luther King Jr. Way Oakland, California

Environmental Control Associates, Inc. Pneumatic Sampler.	HNu (ppm)	SAMPLE #	Sample Interval	Depth (feet)	LOGG PROJE	PMENT: Pneumatic Sampler (1" O.D.) ED BY: M. Kaltreider ECT: 2703 Martin Luther King Jr. Wy T DATE: 5/23/95
Munsell Color Scale		-		2		Asphalt Pavement/Baserock: gravel. Clayey Sand (SC), Olive green mottled mottled dark green with 5-10%
				4		fines, medium dense, moist (slight hydrocarbon odor).
(10YR - 3/2)	10	B2-5		•		Clayey Sand (SC) brown mottled greyish green with 45 to 50% fine
(5Y - 3/2)	40	B2-7		— 6 — <u>∑</u>		grain sand, dense, slightly plastic, saturated, hydrocarbon odor.
•				8		BOTTOM OF BORING @ 7 feet (Refusal encountered)
				10		
				 12. 		
				— 14 —		
	·			— 16 —		
				<u> </u>		
				— 20 —		
	,			22		
				24		:
				— 26 —		
				— 28 —		
				20		
ACC ENVIRONMENTAL C 1000 ATLANTIC AVEUN			J	10B NO: 6	3254-1	O LOG OF BORING B-2
ALAMEDA, CA	-			DATE: 6/	/24/95	2703 Martin Luther King Jr. Way Oakland, California

1 1/2 1

Environmental Control Associates, Inc. Pneumatic Sampler.	HNu (ppm)	SAMPLE #	Sample Interval	Depth (feet)	LOGGED I	NT: Pneumatic Sampler (1" O.D.) BY: M. Kaltreider : 2703 Martin Luther King Jr. Wy ATE: 5/23/95
Munsell Color Scale				_	sesse As	phalt Pavement/Baserock: gravel.
·				<u> </u>		
(10YR - 3/2)	10	B3-4		4 —	gre	ndy Clay (CL), Brown mottled by with 35% fine grain sand, stiff, ry plastic, moist.
(5Y - 3/2)	40	B3-6		6		
				— 8 —	///// wi	andy Clay (CL) dark olive green ith 25% fine grain sand, plastic, iff, moist, hydrocarbon odor.
				— 10 —		
		No Sample		<u> </u>	Sai en	ndy Clay (CL), as above, no water countered, refusal at 12 feet.
·					1	BOTTOM OF BORING @ 12 feet
				14 -		
				— 16 —		
				18		
·						
·				20		·
				22		
				<u> </u>		
				0.0		
	!			— 26 —	1	
				<u> </u>		
ACC ENVIRONMENTAL (1000 ATLANTIC AVEUR				JOB NO: (6254-1.0	LOG OF BORING B-3
ALAMEDA, CA	-			DATE: 6	6/24/95	2703 Martin Luther King Jr. Way Oakland, California

Environmental Control Associates, Inc. Pneumatic Sampler.	HNu (ppm)	SAMPLE #	Sample	(feet)	LOGGED PROJECT	NT: Pneumatic Sampler (1" O.D.) BY: M. Kaltreider : 2703 Martin Luther King Jr. Wy ATE: 5/23/95
Munsell Color Scale				0 -		phalt Pavement/Baserock: gravel.
				2	///// mc	ndy Clay (CL), Greyish brown ottled reddish brown with 35% fine ain sand, stiff, plastic, moist with
(10YR - 3/2)	10	B4-4		— 4 —		v roots.
(5Y - 3/2)	50	B4-6		6 —	gre sar	ndy Clay (CL) greyish green mottled by and brown with 40% fine grain ad, plastic, stiff, moist, strong
				8	hyd	drocarbon odor.
,				10 —		
		No Sample	\overline{Z}	12	Sar ref	ndy Clay (CL), as above, saturated usal at 12 feet.
				14		BOTTOM OF BORING @ 12 feet No water encountered
				— 16 —		
						ŗ
		·		— 18 <i>—</i>		
				 20 –		
				— 22 —		
				<u> </u>		<i>;</i>
				— 26 —		
				—28 —		
ACC ENVIRONMENTAL C 1000 ATLANTIC AVEUN				JOB NO: 6	5254-1.0	LOG OF BORING B-4
ALAMEDA, CA	9450)1 		DATE: 6	/24/95	2703 Martin Luther King Jr. Way Oakland, California

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Environmental Control Associates, Inc. Pneumatic Sampler.	HNu (ppm)	SAMPLE #	Sample Interval	Depth (feet)	LOGGED PROJECT	NT: Pneumatic Sampler (1" O.D.) BY: M. Kaltreider : 2703 Martin Luther King Jr. Wy ATE: 5/23/95
Munsell Color Scale (10YR - 3/2) (5Y - 3/2)	10 50	B5-5 B5-7		0246810	Sai As Sai mo gra slig Sar oli	phalt Pavement/Baserock: gravel. Indy Clay (CL), dark greenish grey ottled brown with 15% fine hin sand, stiff, very plastic, moist, ght hydrocarbon odor. Indy Clay (CL) brown mottled dark we grey with 25% very fine grain hid, slightly plastic, stiff, moist, drocarbon odor.
		No Sample		— 12 — — ½ — — 16 — — 18 —		Approximately 0.25-0.5" non-aqueous product on water. Indy Clay (CL), as above, saturated. BOTTOM OF BORING @ 15 feet
				— 20 — — 22 — — 24 — — 26 —		
ACC ENVIRONMENTAL (1000 ATLANTIC AVEUN ALAMEDA, CA	IUE, SI	JITE 110		JOB NO: 6		LOG OF BORING B-5 2703 Martin Luther King Jr. Way Oakland, California

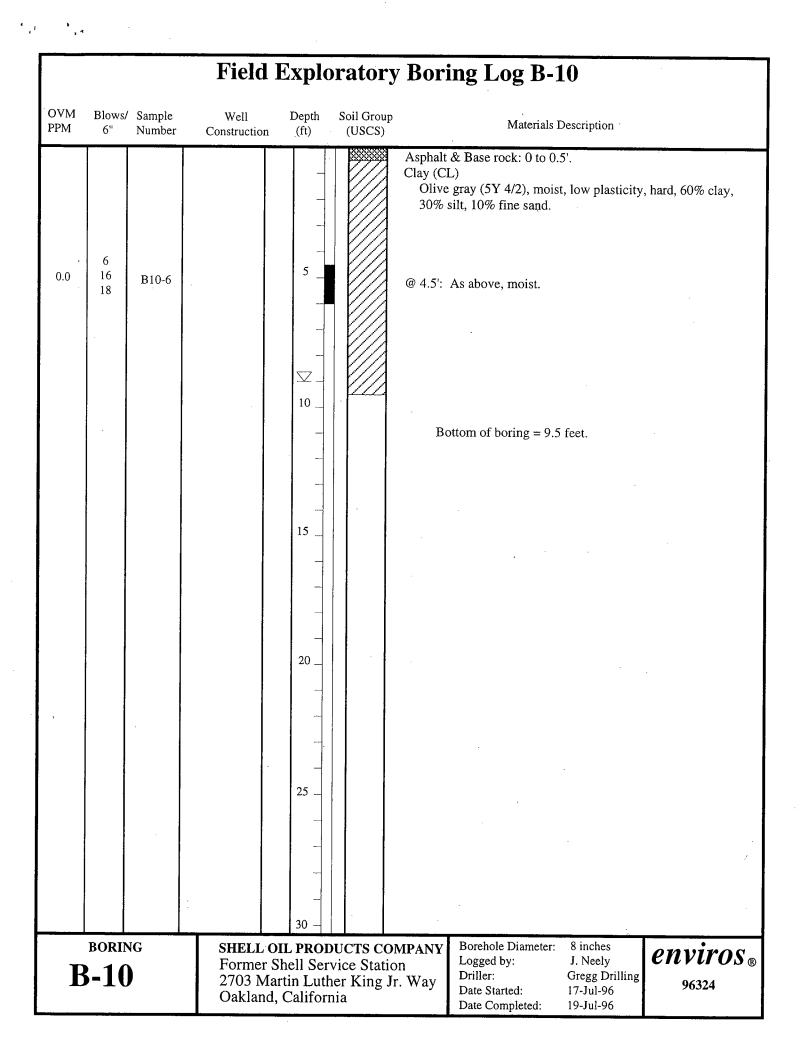
Environmental Control Associates, Inc. Pneumatic Sampler.	HNu (ppm)	SAMPLE #	Sample Interval	Depth (feet)	LOGGED PROJECT	NT: Pneumatic Sampler (1" O.D.) BY: M. Kaltreider : 2703 Martin Luther King Jr. Wy PATE: 5/23/95
Munsell Color Scale					AS	sphalt Pavement/Baserock: gravel.
				2	ге	ayey Sand (SC), olive grey mottled ddish brown with 65% fine
(10YR - 3/2)	100	B6-5		4 —	gr hy	rain sand, dense, moist, strong vdrocarbon odor.
				6 —		
				8 <i>-</i>		ayey Sand (SC) brown mottled dark ey with 70% fine grain sand,
(5Y - 3/2)	500	B6-10	-	<u> </u>	(6)	ense, very moist, strong drocarbon odor.
				— 12 —		Approximately 1-2" non-aqueous product on water.
		No	<i></i>	14 -	wit	ayey Sand (SC), Brown mottled grey th 80% fine grain sand, dense, wet,
		Sample	77)	16	SU	ong hydrocarbon odor BOTTOM OF BORING @ 15 feet
				10		
				18		
				20 -		
				22		
	:			24		
				<u> </u>		
				<u> </u>		
·						
ACC ENVIRONMENTAL (T .	JOB NO: (6254-1.0	LOG OF BORING B-6
	ATLANTIC AVEUNUE, SUITE 110 ALAMEDA, CA 94501			DATE: 6	6/24/95	2703 Martin Luther King Jr. Way Oakland, California

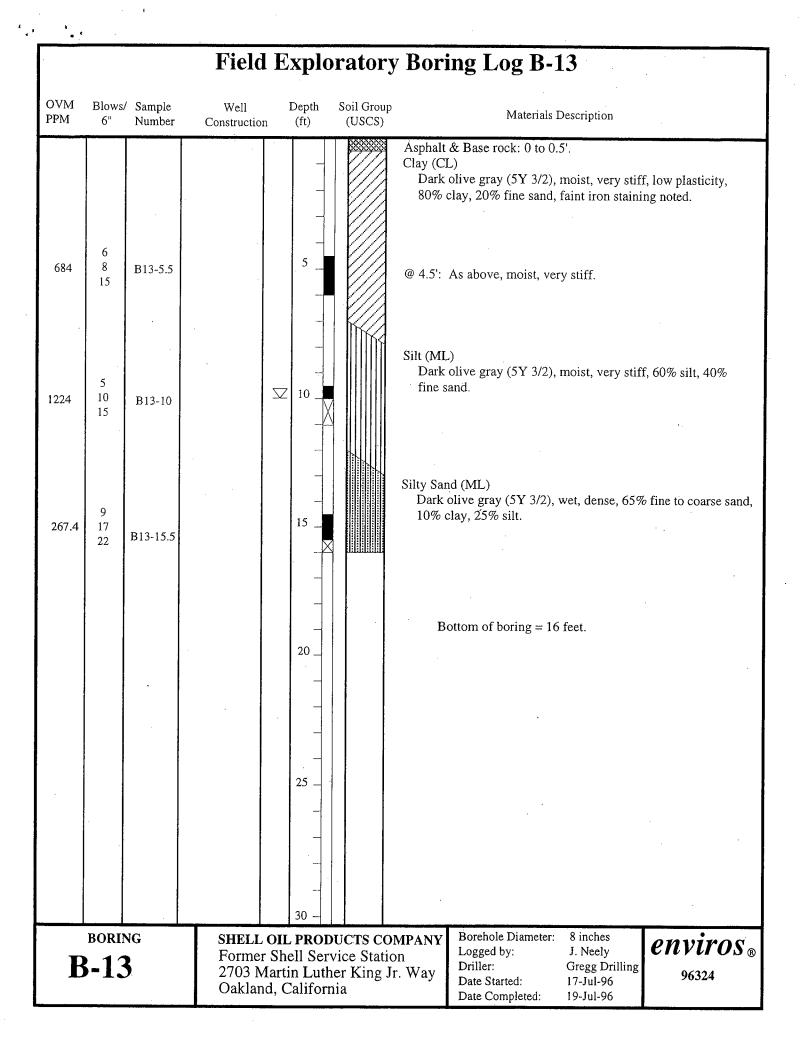
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Environmental Control Associates, Inc. Pneumatic Sampler.	HNu (ppm)	SAMPLE #	Sample	Depth	EQUIPMENT: Pneumatic Sampler (1" O.D.) LOGGED BY: M. Kaltreider PROJECT: 2703 Martin Luther King Jr. Wy START DATE: 5/23/95
Munsell Color Scale				0 -	Asphalt Pavement/Baserock: gravel.
				2	
			:		
(10YR - 3/2)	0	B7-5		4	Sand (SP) with clay, dark greyish green (5-10% fines), dense, moist.
(S are (a see a
				6 —	•
				- 8 -	
(5Y - 3/2)	20	B7-10		<u>∑</u> — 10 —	Sand (SP) brown mottled grey with 10% fines, dense, moist to wet.
				10 —	with 1070 mies, dense, moist to wet.
·				— 12 —	
		No		— 👱 –	Sand (SP), Brown mottled grey with 5% fines, dense, wet.
		Sample	77,	_	BOTTOM OF BORING @ 15 feet
				16 —	
				18	
; •					
				<u> </u>	
				22	
				— 22 —	
				<u> </u>	·
				 26	
				— 28 —	
				20	
·			$\frac{1}{1}$		
ACC ENVIRONMENTAL (,	JOB NO: 6	6254-1.0 LOG OF BORING B-7
ALAMEDA, CA				DATE: 6	2703 Martin Luther King Jr. Way /24/95 Oakland California
1000 ATLANTIC AVEUI ALAMEDA, CA				DATE: 6	2703 Martin Luther King Jr. Way 024/95 Oakland, California

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Environmental Control Associates, Inc. Pneumatic Sampler.	HNu (ppm)	SAMPLE #	Sample Interval	Depth (feet)	LOGGI PROJE	MENT: Pneumatic Sampler (1" O.D.) ED BY: M. Kaltreider CT: 2703 Martin Luther King Jr. Wy DATE: 5/23/95
Munsell Color Scale				_ 0 _	22222	Asphalt Pavement/Baserock: gravel.
				2		Sand (SP) with clay, brown mottled reddish brown, (5-10% fines),
(10YR - 3/2)	0	B8-5		4 -		dense, moist (interperted at fill).
				— 6 _. —		
(5)(2/2)				- 8 -		Clayey Sand (SC) brown mottled black
(5Y - 3/2)	0	B8-10		10 -		with 35% fines, dense, moist to wet.
				— 12 –		
		No Sample		<u>∑</u> —14 –		Sand (SP), Brown mottled grey with 5% fines, dense, wet.
		Sample		— 16 —		BOTTOM OF BORING @ 15 feet
				18		
		,		20		
				22		
				— 24 —		;
				<u> </u>		
				— 28 —		
			ı			
	ACC ENVIRONMENTAL CONSULTANTS 1000 ATLANTIC AVEUNUE, SUITE 110			JOB NO: (6254-1	
AL AME DA, CA	9450	01		DATE: 6	6/24/9	2703 Martin Luther King Jr. Way Oakland, California





BORING/WELL LOG

PAGE 1 OF 1



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DRILLER DRILLIN BORING LOGGET	E NAM ON T NUM R G MET DIAME D BY ED BY	E 0 2 BER 2 HOD H ETER 7 E	akl2 703 42-0 iregi lollo " i. Ja	0781 g Drillin w-stem kub ork, RG	Luther g auger # 5620	King, (Dakland ed approx. 28' north of B	TOP OF CASING ELEVAT SCREENED INTERVAL DEPTH TO WATER (First DEPTH TO WATER (Station	ATE (YIELD)_ VATION _ TION _ Not SuNA Encountered	NA Not Sirveyed 13.	urveyed 0 ft (22-Nov	v-00) \(\sum_{\textstyle \textstyle \textst
TPHg (mg/kg)	BLOW	SAMPLE ID	EXTENT	DEPTH (ft bgs)	U.S.C.S.	GRAPHIC LOG	· LITHC	DLOGIC DESCRIPTION		CONTACT DEPTH (ft bgs)	WEL	L DIAGRAM
		B17-5.0			ML		clay, 60% silt; mediu	ıck; damp; 5% clay, 25% si		5.0		▼ Portland Type I/II Cement Bottom of Boring @ 15 ft





Cambria Environmental Technology, Inc. 1144 - 65th St. Oakland, CA 94608 Telephone: (510) 420-0700 Fax: (510) 420-9170

CLIENT NAME JOB/SITE NAME LOCATION PROJECT NUMBER DRILLER DRILLING METHOD BORING DIAMETER LOGGED BY REVIEWED BY REMARKS	oakl27 2703 I 242-0 Gregg Hollov 7" B. Jak S. Bor Hand	Martin 781 Drillin v-stem kub k, RGi	g auger # 5620 ed to 5'	DRILLING STARTED 22-Nov-00					
TPHg (mg/kg) BLOW COUNTS	EXTENT	DEPTH (ft bgs)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESC	RIPTION	CONTACT DEPTH (ft bgs)	. WELI	L DIAGRAM
WELL LOG (TPH-G) G:JOABCAE-1/GINTJOAKL2703.GPJ DEFAULT.GDT 3/8/01 B18-2:0	×	- 5	ML		ASPHALT Clayey SILT (ML); black; very stiff; high plasticity. Sandy SILT (ML); dark grey; 5% claime grained sand; low plasticity. @7' bgs- dark olive grey Silty SAND (SM); yellow brown; we 50% fine grained sand, 12% fine grain	ay, 70% silt, 25%	3.0		Portland Type I/II Cement Bottom of Boring @ 15 ft

BORING/WELL LOG



Cambria Environmental Technology, Inc. 1144 - 65th St. Oakland, CA 94608 Telephone: (510) 420-0700 Fax: (510) 420-9170

CLIENT NAME	Equiva Services LLC	BORING/WELL NAME B-19	
JOB/SITE NAME	oak!2703	DRILLING STARTED 22-Nov-00	
LOCATION _	2703 Martin Luther King, Oakland	DRILLING COMPLETED 22-Nov-00	
PROJECT NUMBER	242-0781	WELL DEVELOPMENT DATE (YIELD) NA	
DRILLER _	Gregg Drilling	GROUND SURFACE ELEVATION Not Surveyed	
DRILLING METHOD _	Hollow-stem auger	TOP OF CASING ELEVATION Not Surveyed	
BORING DIAMETER _	7"	SCREENED INTERVAL NA	
LOGGED BY	B. Jakub	DEPTH TO WATER (First Encountered) 15.0 ft (22-Nov-00)	∇
REVIEWED BY	S. Bork, RG# 5620	DEPTH TO WATER (Static) NA	
REMARKS	Hand augored to E' Loosted approx. EO no		

Hand augered to 5'. Located approx. 50' north of MW-3. CONTACT DEPTH (# bgs) TPHg (mg/kg) SAMPLE ID GRAPHIC LOG BLOW COUNTS EXTENT U.S.C.S. DEPTH (ft bgs) LITHOLOGIC DESCRIPTION **WELL DIAGRAM** ASPHALT
Clayey SILT (ML); black; very stiff; 40% clay, 60% silt; high plasticity. 0.2 ML 3.0 Sandy SILT (ML); dark brey; 5% clay, 70% silt, 25% fine grained sand; low plasticity. ML B19-5.0 7.0 B19-7.0 Clayey SILT (ML); brown; very stiff; moist; 40% clay, 60% silt; high plasticity. ML 10.0 Portland Type <u>Silty SAND</u> (SM); yellow brown; stiff; wet; 8% clay, 30% silt, 50% fine grained sand, 12% fine grained gravel; low I/II Cement plasticity. ∇ SM 20.0 WELL LOG (TPH-G) GNOABCAE-11GINTNOAKL2703.GPJ DEFAULT.GDT 3/8/01 20 Bottom of Boring @ 20 ft



Cambria Environmental Technology, Inc. 5900 Hollis Street, Suite A Emeryville, CA 94608 Telephone: 510-420-9700 Fax: 510-420-9170

CLIENT NAME	Shell Oil Products US	BORING/WELL NAME B-23
JOB/SITE NAME	2703 Martin Luther King Jr. Way	DRILLING STARTED 03-Jan-06
LOCATION	Oakland, California	DRILLING COMPLETED 03-Jan-06
PROJECT NUMBER_	247-0781-007	WELL DEVELOPMENT DATE (YIELD) NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION Not Surveyed
DRILLING METHOD_	Hollow-stem auger	TOP OF CASING ELEVATION Not Surveyed
BORING DIAMETER_	8"	SCREENED INTERVALS NA
LOGGED BY	B. DeBoer	DEPTH TO WATER (First Encountered) 13.5 fbg (03-Jan-06)
REVIEWED BY	A. Friel, PG	DEPTH TO WATER (Static) NA
REMARKS	Hand Augered to 5 feet below grade.	· · · · · · · · · · · · · · · · · · ·

PID (ppm)	BLOW	SAMPLE ID	EXTENT	DЕРТН (fbg)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
О		B-23- 5		- 5 -	GP ML	25	ASPHALT GRAVEI with Silt (FILL)(GP); pale brown; moist; 40% silt, 10% fine sand, 50% medium gravel; low plasticity. Clayve SILT (ML); dark greenish gray; moist; 35% clay, 65% silt; moderate plasticity.	0.2 1.0	
EFAULT.GDT 2/24/08		8-23 - 10		 10 	SM	2012/2012 2012/2012 2012/2013	Sandy SILT with Gravel (ML); brown; moist; 65% silt, 20% fine sand, 15% medium gravel; moderate plasticity. Silty SAND (SM); light greenish brown; moist; 20% silt, 80% medium sand.	10.0 11.5 13.5	▼ Portland Type
JRESIGINTOAKL2703.GPJ DI SE G		B-23- 15.5		 15 	GP ML SP ML		GRAVEL with Sand (GP); light brown; wet; 30% coarse sand, 70% coarse angular gravel. Sandy SiLT with Gravel (ML); brown; moist; 65% silt, 20% fine sand, 15% medium gravel; moderate plasticity. SAND (SP); light brown; wet; 90% medium sand, 10% medium gravel. Sandy SiLT with Gravel (SM); greenish gray and brown; moist; 65% silt, 20% fine sand, 15% medium gravel; moderate plasticity.	14.0 15.0 16.0	
WELL LOG (PID) G:OAKLAND 2703 MARTIN LUTHER KING JRIFIGURES/GINTOAKL2703.GPJ DEFAULT.GDT 222408 T		8-2-1 9.5	XX					20.0	Bottom of Boring @ 20 fbg



CLIENT NAME _	Shell Oil Products US	BORING/WELL NAME	GP-1	•	
JOB/SITE NAME _	Former Shell Station	DRILLING STARTED	29-Aug-05		
LOCATION _	2703 Martin Luther King Jr. Way, Oakland, CA	DRILLING COMPLETED_	29-Aug-05		
PROJECT NUMBER_	0781	WELL DEVELOPMENT D		NA	
DRILLER _	Gregg Drilling	GROUND SURFACE ELE		Not Surveyed	
DRILLING METHOD_	Hydraulic push	TOP OF CASING ELEVAT			
BORING DIAMETER	2"	SCREENED INTERVAL	NA		
LOGGED BY	S. Lewis	DEPTH TO WATER (First		10.5 ft (29-Aug-05)	$\overline{\nabla}$
REVIEWED BY	A. Friel, PG 6452	DEPTH TO WATER (Statio		NA NA	Y
DEMARKS			-		

REVIEWED E	••• <u> </u>	4. F	rlel, PG	6452		DEPTH TO WATER (Static)	N	A
PID (ppm) BLOW	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	SOIL DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
6.4	GP-1- 4.0'V GP-1-5.0 GP-1- 10.0			ML SM	30 S S S S S S S S S S S S S S S S S S S	Silty SAND with Gravel (SM); brown (10YR 5/2); moist; 5% clay, 15% silt, 35% fine to coarse sand, 45% fine gravel. SILT (ML); very dark grayish brown (10YR 3/2); moist; 30% clay, 65% silt, 5% fine to medium sand; medium plasticity. (a) 3.5' - A vapor sample was collected from 3.5 to 4 feet below grade. (a) 5' - dark greenish gray (5GY 4/1).	0.2 0.8 0.8	■ Portland T
			-					Bottom of Boring @ 1
								PAGE 1



CLIENT NAME	Shell Oil Products US	BORING/WELL NAME GP-2
JOB/SITE NAME	Former Shell Station	DRILLING STARTED 29-Aug-05
LOCATION	2703 Martin Luther King Jr. Way, Oakland, CA	DRILLING COMPLETED 29-Aug-05
PROJECT NUMBER	0781	WELL DEVELOPMENT DATE (YIELD) NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION Not Surveyed
DRILLING METHOD_	Hand auger	TOP OF CASING ELEVATION Not Surveyed
BORING DIAMETER_	3"	SCREENED INTERVAL NA
LOGGED BY	S. Lewis	DEPTH TO WATER (First Encountered) NA
REVIEWED BY	A. Friel, PG 6452	DEPTH TO WATER (Static) NA
REMARKS		
© S	H + 6 9	F. G

REMAR	KS _									
PID (ppm)	BLOW	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	SOIL DESCRIPTION	CONTACT DEPTH (fbg)	WE	LL DIAGRAM
14.0		GP-2- 4.0℃ GP-2-4.5			SM ML		ASPHALT Silty SAND with Gravel (SM); strong brown (7.5Y 4/6); moist; 25% silt, 50% fine to coarse sand, 25% fine to coarse sand. SiLT (ML); dark greenish gray (10Y 3/1); moist; 30% clay, 65% silt, 5% fine to medium sand; medium plasticity. @ 2' - greenish black (10Y 2.5/1). @ 3' - mottled with greenish gray (5G 5/1). @ 3.5' - A vapor sample was collected from 3.5 to 4 feet below grade.	0.2 0.8 4.5		✓ Portland Type I/II Bottom of Boring @ 4.5 f
										·



BORING/WELL LOG

PAGE 1 OF

CLIENT NAME Shell Oil Products US BORING/WELL NAME GP-3 JOB/SITE NAME Former Shell Station **DRILLING STARTED** 29-Aug-05 LOCATION 2703 Martin Luther King Jr. Way, Oakland, CA DRILLING COMPLETED 29-Aug-05 **PROJECT NUMBER** 0781 WELL DEVELOPMENT DATE (YIELD) NA **DRILLER** Gregg Drilling **GROUND SURFACE ELEVATION** Not Surveyed Hydraulic push TOP OF CASING ELEVATION Not Surveyed SCREENED INTERVAL S. Lewis

DRILLING METHOD BORING DIAMETER LOGGED BY DEPTH TO WATER (First Encountered) 9.0 ft (29-Aug-05) REVIEWED BY A. Friel, PG 6452 **DEPTH TO WATER (Static)** NA **REMARKS** CONTACT DEPTH (fbg) GRAPHIC LOG (mdd) BLOW SAMPLE EXTENT DEPTH (fbg) U.S.C.S. SOIL DESCRIPTION WELL DIAGRAM 문 0.2 SM Silty SAND with Gravel (SM); yellowish brown (10YR 5/4); moist; 25% silt, 60% fine to coarse sand, 15% fine to 1,0 ML coarse gravel. SILT with Sand and Gravel (ML); dark greenish gray (10Y 3/1); moist; 30% clay, 40% silt, 15% fine to coarse sand, 15% fine gravel; low to medium plasticity.

Silty SAND (SM); dark greenish gray (10Y 3/1); moist; 20% silt, 80% fine to medium sand.

@ 3.5' - A vapor sample was collected from 3.5 to 4 feet below grade. 3.0 GP-3-SM 4.0" 5.0 678 GP-3-5.0^t Portland Type below grade.
SILT (ML); dark greenish gray (10Y 3/1); moist; 30% clay, 55% silt, 10% fine to medium sand, 5% fine gravel; 1/11 ML low to medium plasticity. 942 GP-3-8.5 ▽ 9.0 Silty SAND (SM); dark greenish gray (10Y 3/1); wet; SM 10.0 30% silt, 70% fine to medium sand. GP-3-A hydropunch sample was collected from 10 to 12 feet 10W below grade. Bottom of Boring @ 12 ft



CLIENT	NAME	S	hell	Oil Pro	oducts	us		BORING/	WELL NAME _	GP-4						
JOB/SI	re nam	E <u>F</u>	orm	er She	II Static	n ·		DRILLING	STARTED _	31-Aug-05						
LOCAT	ION	27	703	Martin	Luther	King	g .	r. Way, Oakland, CA DRILLING								
PROJE	CT NUM		781					WELL DE	VELOPMENT D	ATE (YIELD)	_NA		 			
DRILLE				g Drillir				GROUND	SURFACE ELE	VATION _	Not S	urveyed	·			
	NG MET			auger	<u> </u>				TOP OF CASING ELEVATION Not Surveyed							
	3 DIAME								D INTERVAL _				7			
LOGGE	-	.s. A		wis	6450		-	•	WATER (First				<u> </u>			
REMAR	_	<u> </u>	<u>. EU</u>	ei, PG	0452			DEPIRIT	WATER (Stati	IC)	NA	1	<u> </u>			
KEMAN		·······			,											
PID (ppm)	BLOW	SAMPLEID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC	507	SOIL DESCR	IPTION		CONTACT DEPTH (fbg)	WEI	LL DIAGRAM			
•			F		SM			ASPHALT			0.2	W/XW				
					ML			Silty SAND with Gravel (SM); p moist; 15% silt, 60% fine to coar- coarse gravel. SiLT (ML); dark greenish gray (clay, 65% silt, 5% fine to medium	se sand, 25% fin	e to 30%	1.0		✓ Portland Type I/II			
6.4		GP-4- 4.0'V GP-4-4.5'		_ <u> </u>		Ш	Ц	@ 3.5' - A vapor sample was col below grade.	ected from 3.5 t	o 4 feet	4.5		Bottom of Boring @ 4.5 ft			
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BORING/WELL LOG

PAGE 1 OF 1

LOCAT PROJE DRILLE DRILLE BORIN LOGGE	ECT NUM ER ING MET IG DIAME ED BY WED BY	E	orm 703 781 Greg and		II Station Luther	on r King	WELL DEVE GROUND SI TOP OF CAS SCREENED DEPTH TO V					
PID (ppm)	BLOW	SAMPLE ID	EXTENT	DEРТН (fbg)	U.S.C.S.	GRAPHIC LOG	SOIL DESCRIP	SOIL DESCRIPTION		WEL	L DIAGRAM	
0.0		GP-5- 4.0'V GP-5-4.5'			SM ML	300	ASPHALT Silty SAND with Gravel (SM); yello 5/4); moist; 15% silt, 60% fine to cogravel. SILT (ML); very dark grayish brow 30% clay, 65% silt, 5% fine to medi plasticity. @ 3.5' - A vapor sample was collected below grade.	oarse sand, 25% fine on (10YR 3/2); moist; ium sand, medium	0.2 1.0 4.5		■ Portland Type I/II Bottom of Boring @ 4.5 ft	
AULT.GDT 10/26/05												
WELL LOG (PID) I:\OAKQAN~1\G\NT\0781.GPJ DEFAULT.GDT 10/26/05												



CLIENT NAME

DRILLING METHOD

LOCATION

DRILLER

Cambria Environmental Technology, Inc. 270 Perkins Street Sonoma, CA 95476 Telephone: 707-935-4850

Hydraulic push

BORING/WELL LOG

PAGE 1 O

Fax: 707-935-6649 Shell Oil Products US GP-6 **BORING/WELL NAME** JOB/SITE NAME Former Shell Station **DRILLING STARTED** 29-Aug-05 DRILLING COMPLETED 30-Aug-05 2703 Martin Luther King Jr. Way, Oakland, CA PROJECT NUMBER WELL DEVELOPMENT DATE (YIELD) NA Gregg Drilling **GROUND SURFACE ELEVATION** Not Surveyed

TOP OF CASING ELEVATION Not Surveyed

BORING DIAMETER_ SCREENED INTERVAL S. Lewis DEPTH TO WATER (First Encountered) 20.0 ft (30-Aug-05) A. Friel, PG 6452 **DEPTH TO WATER (Static)** NA

LOGGED BY REVIEWED BY Y **REMARKS** CONTACT DEPTH (fbg) (mdd) GRAPHIC LOG BLOW U.S.C.S. EXTENT DEPTH (fbg) SAMPLE SOIL DESCRIPTION **WELL DIAGRAM** 윤 ASPHALT
Silty SAND with Gravel (SM); pale brown (10YR 6/3);
moist; 20% silt, 50% fine to coarse sand, 30% fine gravel.
SILT (ML); dark grayish brown (10YR 4/2); moist; 30%
clay, 65% silt, 5% fine to medium sand; medium plasticity. 0.2 SM 1:1 **GP-6-**@ 3.5' - A vapor sample was collected from 3.5 to 4 feet 4.0'V below grade. 0.0 GP-6-5.0' ML @ 5' - dark greenish gray (10Y 3/1). 10.0 0.0 GP-6-9.5 Portland Type A hydropunch sample was collected from 10 to 20 feet below grade. GP-6-⊻ 20'W Bottom of Boring @ 20 ft



BORING/WELL LOG

PAGE 1 OF

CLIENT NAME Shell Oil Products US BORING/WELL NAME GP-7 JOB/SITE NAME Former Shell Station **DRILLING STARTED** 30-Aug-05 DRILLING COMPLETED 30-Aug-05 LOCATION 2703 Martin Luther King Jr. Way, Oakland, CA **PROJECT NUMBER** WELL DEVELOPMENT DATE (YIELD) NA DRILLER Gregg Drilling **GROUND SURFACE ELEVATION** Not Surveyed TOP OF CASING ELEVATION Not Surveyed **DRILLING METHOD** Hand auger **BORING DIAMETER** SCREENED INTERVAL NA **LOGGED BY** S. Lewis DEPTH TO WATER (First Encountered) 10.0 ft (30-Aug-05) **REVIEWED BY** A. Friel, PG 6452 **DEPTH TO WATER (Static)** NA

REMARKS CONTACT DEPTH (fbg) GRAPHIC LOG (mdd) BLOW **EXTENT** U.S.C.S. DEPTH (fbg) SAMPLE SOIL DESCRIPTION WELL DIAGRAM 읊 ASPHALT
Silty SAND with Gravel (SM); pale brown (10YR 6/3);
dry to moist; 25% silt, 50% fine to coarse sand, 25% fine 0.2 SM 1.5 SiLT (ML); very dark grayish brown (10YR 3/2); moist 30% clay, 65% silt, 5% fine to medium sand; medium plasticity.

@ 3.5' - A vapor sample was collected from 3.5 to 4 feet GP-7-4.0'V Portland Type 0.0 GP-7-5.0' below grade. ML M @ 6' - dark greenish gray (10Y 3/1). 3,000 ፟⊈]10.0 5,200 GP-7-9.5 **Bottom of** Boring @ 10 ft WELL LOG (PID) I:10AKLAN~11GINT10781.GPJ DEFAULT.GDT 10/26/05



CLIENT NAME	Shell Oil Products US	BORING/WELL NAME GP-8					
JOB/SITE NAME	Former Shell Station	DRILLING STARTED					
LOCATION	2703 Martin Luther King Jr. Way, Oakland, CA	DRILLING COMPLETED 30-Aug-05					
PROJECT NUMBER_	0781	WELL DEVELOPMENT DATE (YIELD) NA					
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION Not Surveyed					
DRILLING METHOD_	Hand auger	TOP OF CASING ELEVATION Not Surveyed					
BORING DIAMETER	2"	SCREENED INTERVAL NA					
LOGGED BY	S. Lewis	DEPTH TO WATER (First Encountered) NA					
REVIEWED BY	A. Friel, PG 6452	DEPTH TO WATER (Static) NA					
REMARKS							
- 1 - 1 - 6							
MW VTS	F B SS 물이	(fbg)					

REMAR	VED BY_ RKS		<u> </u>	iel, PG	6452		DEPTH TO WATER (Static)	N/	\	¥
PID (ppm)	BLOW	SAMPLE ID	EXTENT	DEРТН (fbg)	U.S.C.S.	GRAPHIC LOG	SOIL DESCRIPTION		WELL DIAGRAM	
,			P		SM		ASPHALT Silty SAND with Gravel (SM); pale brown (10YR 6/3);	TO CONTACT 15 DEPTH (fbg)		
		CD a			ML		Silty SAND with Gravel (SM); pale brown (10YR 6/3); moist; 25% silt, 60% fine to coarse sand, 15% fine gravel. SILT (ML); very dark grayish brown (10YR 3/2); moist; 30% clay, 65% silt, 5% fine to medium sand; medium plasticity. @ 3.5' - A vapor sample was collected from 3.5 to 4 feet			✓ Portland Type I/II
1.7		GP-8- 4.0'V GP-8-4.5		1			@ 3.5' - A vapor sample was collected from 3.5 to 4 feet below grade.	4.5		Bottom of Boring @ 4.51
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CLIENT NAME			hell	Oil Pro	oducts	US		BORING/WELL NAME	GP-9					
JOB/S			er She				DRILLING STARTED	5						
LOCAT	TION	2	703	Martin	Luther	r King .	Jr. Way, Oakland, CA	DRILLING COMPLETED	5					
	ECT NUM		<u> 781</u>			····	······································	WELL DEVELOPMENT	DATE (YIELD)	.D) NA				
DRILLER Gregg Drilling														
DRILLING METHOD Hand auger TOP OF CASING ELEVATION N														
BORING DIAMETER 2" SCREENED INTERVAL LOGGED BY S. Lewis DEPTH TO WATER (First Enc														
					6452					Pred) NA $\overline{\underline{V}}$				
REMAI		<u></u>	<u>., FI</u>	<u>191, PG</u>	0452		·	DEPTH TO WATER (Stat	(IC)	NA	١	_		
INCHIA!		····			,				····					
PID (ppm)	SAMPLE ID	SAMPLE ID		U.S.C.S.	GRAPHIC LOG	SOIL DESCRIPTION			CONTACT DEPTH (fbg)	WELL DIAGRAM				
0.0		GP-9-			SM		CONCRETE Silty SAND with Gravel (SM); yellowish brown (10YR 5/4); moist; 15% silt, 60% fine to coarse sand, 25% fine gravel. @ 3.5' - A vapor sample was collected from 3.5 to 4 feet			0.4 4.5		✓ Portland Type I/II		
0.0		4.0°V GP-9-4.5					below grade.		· · · · · · · · · · · · · · · · · · ·		777.	Bottom of Boring @ 4.5 ft		
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							,·							
አ														
3DT 10/26/(
DEFAULT.										i				
T/0781.GPJ														
KLAN~11GIN					ì			·						
WELL LOG (PID) I:\OAKLAN-1\GINT\0781.GPJ DEFAULT.GDT 1025;05														
WELL LOG							·							



BORING/WELL LOG

CLIENT NAME Shell Oil Products US BORING/WELL NAME **GP-10 JOB/SITE NAME** Former Shell Station **DRILLING STARTED** 31-Aug-05 LOCATION 2703 Martin Luther King Jr. Way, Oakland, CA DRILLING COMPLETED 31-Aug-05 PROJECT NUMBER_ WELL DEVELOPMENT DATE (YIELD) NA DRILLER Gregg Drilling Not Surveyed **GROUND SURFACE ELEVATION** DRILLING METHOD Hand auger TOP OF CASING ELEVATION Not Surveyed **BORING DIAMETER** SCREENED INTERVAL **LOGGED BY** S. Lewis **DEPTH TO WATER (First Encountered)** NA REVIEWED BY A. Friel, PG 6452 **DEPTH TO WATER (Static)** NA

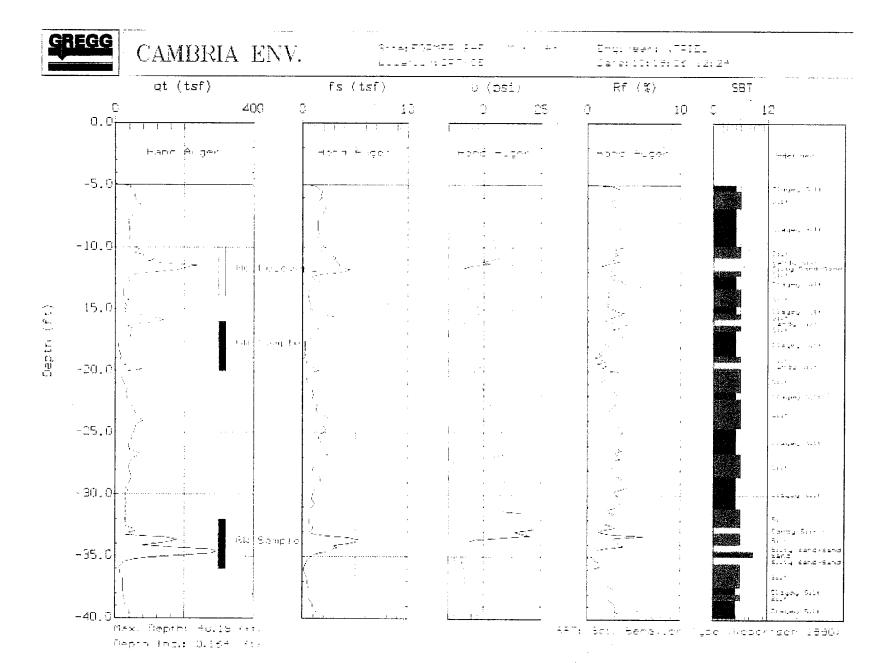
REMARKS CONTACT DEPTH (fbg) GRAPHIC LOG PID (ppm) BLOW U.S.C.S. EXTENT DEPTH (fbg) SAMPLE SOIL DESCRIPTION **WELL DIAGRAM** ASPHALT
Silty SAND with Gravel (SM); yellowish brown (10YR 5/4) moist; 15% silt, 60% fine to coarse sand, 25% fine 0.2 SM 1.0 gravel.

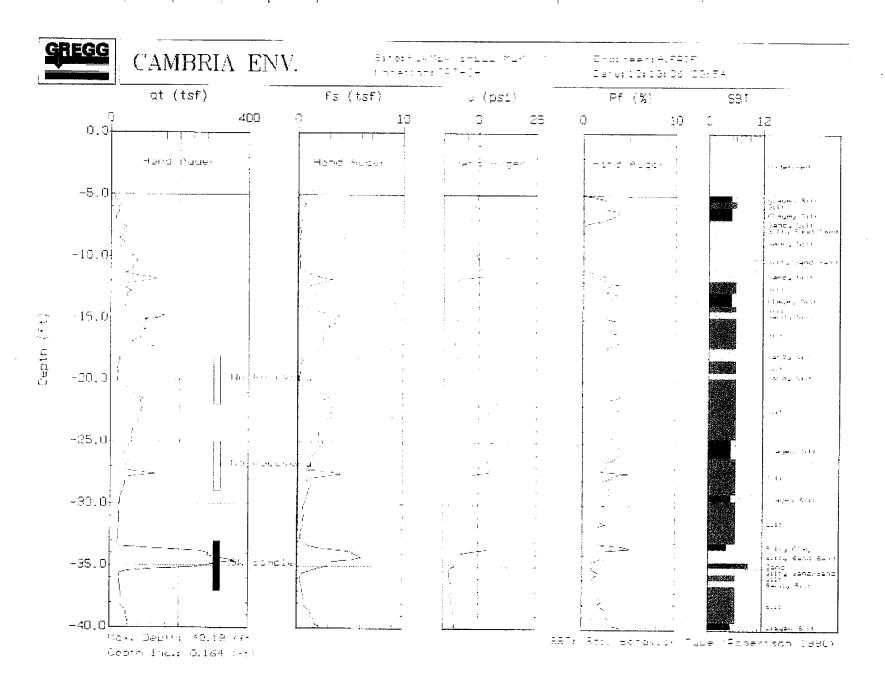
SILT (ML); dark greenish gray (10Y 3/1); moist; 30% clay, 65% silt, 56% fine sand; medium plasticity.

@ 3.5' - A vapor sample was collected from 3.5 to 4 feet Portland Type ML M GP-10-0.0 4.0°V Bottom of below grade. GP-10-Boring @ 4.5 ft 4.5'

State: ೯೭೫೯೩ - ೨೪೮೩ - ೨೯೮೩ - ೨೯೮೩ - ೨೯೮೩ - ೨೯೮೩ - ೨೯೮೩ - ೨೯೮೩ - ೨೯೮೩ - ೨೯೮೩ - ೧೯೮೩ - ೧೯೮೩ - ೧೯೮೩ - ೧೯೮೩ - ೧೯೮೩ at (tsf) fs (tsf) FF (ಇ) SBT U (psi) 400 10 0 10 0 hand Adder Mand Adjer UT04-1540 Saget fills -10.0F\ filas Salta Lara المتاريخين المعالم -15.0artes tas -20.0 -25.04 -30.04 -35.04 - 8ax. Lepth: 18.34 (4)/ 397: Paul Bena dan Type Romensage, 1990

- Booth Inc.: 6.082 (1)





RobbinDAMDA BABUL MURIUMS CAMBRIA ENV. I guneenthe will Located wilst IB Land: Luxub: 36 (10:26 qt (tsf) fs (tsf) U (psi) Rf (%) 58T Ð 400 0 10 Ũ. 25 Q 10 Ŋ. 12 0.0-Нава нидер Hibr.d ⊢ು⊈0--5.Q Sairy Slay Timete 5 D 1144 -10.0or your 140,000 Carrier Cour Service Reduction Administration (Contraction mini Slagen (d. Salen Hag Slagen (d.) -15.0i+ -- ; Service فيس يسهمك F1 . +12 -20,0 Staged with 5.210 المراجعين والمسترات State Section 19 19 Seas a Malaga tulgag unit Story Stag Store time orgin -05.04 Salva Class ية ريجيجا ٢ -30.0÷ ٠.. =٠ Salting of the Olayay Olis -35.0-6 Semble us au Clayey Sair Max. Gebih: 40.15 kttp: ABT: Bail Benevian Type Robertson (1980)

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Septo on: (.164 (+))

CAMBRIA ENV. Bines FORMER ID 트립스 성실하고 있다. Dere: 10: 20: 24 | 14: 27 qt (tsf) fs (tsf) J (psi) Rf (%) \$9T D 400 10 25 \Box 10 12 0.0tranc Augen Object Newsper Ur de Horad ~5.3 C. Bus G. Stir C. Bus G. Stir Billio G. And والمسارية -10.00astronom as 1. Causa III 1 40, -15.0 Classes offi and the following the gap Subject to the -20.0 full type of the مراكا والمواصلاة Set Le Elegan dist Making Class, -25.0 G L Gridge IJ_{i} Key mus Stitle Lieu tiba Cibabba 200 Silia Ciba -30.0 412. Side a Clay erago, elle ovāk Silv Seneskyd Samd Senesy Silv Silvy SamdySamd Silvy SamdySamd Silvy SamdySamd -35.0 5:1: -40.0[‡] Clayer site Мах. Верто: 40.18 (но RBTs, Back denovior Type (Page team (**990**) Depth Incl. 0.184 (40)

1 1



Avg. Interval: 0.328 (ft)

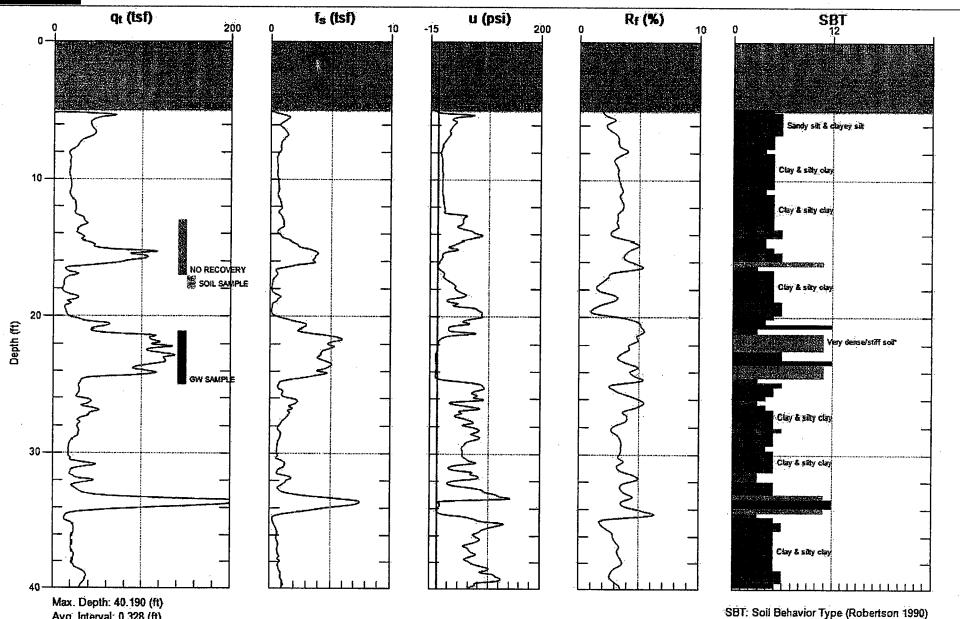
CONESTOGA-ROVERS

Site: FMR. SHELL STATION

Sounding: CPT-06

Engineer: A.FRIEL

Date: 5/17/2007 12:23





Avg. Interval: 0.328 (ft)

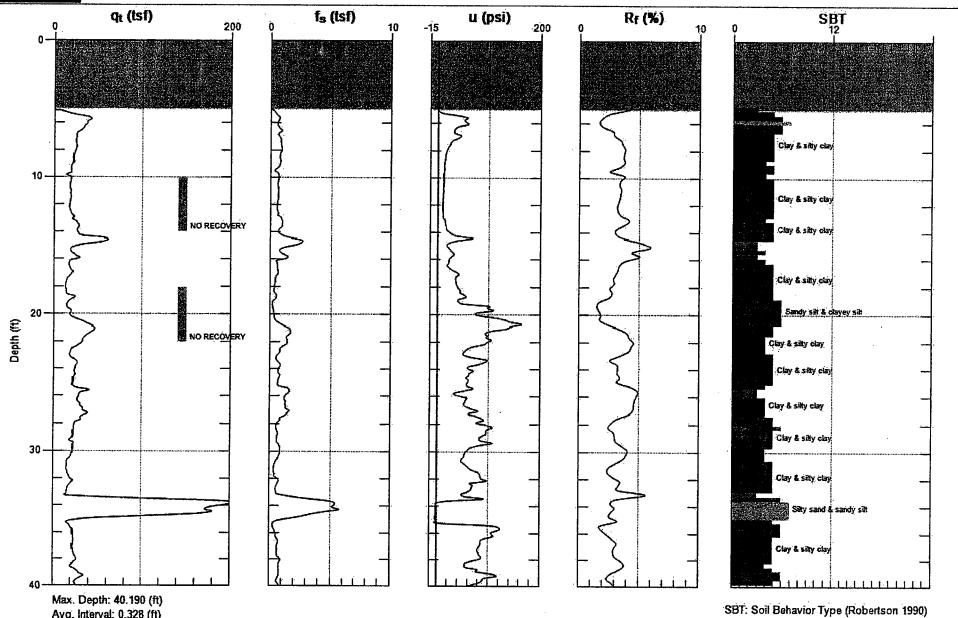
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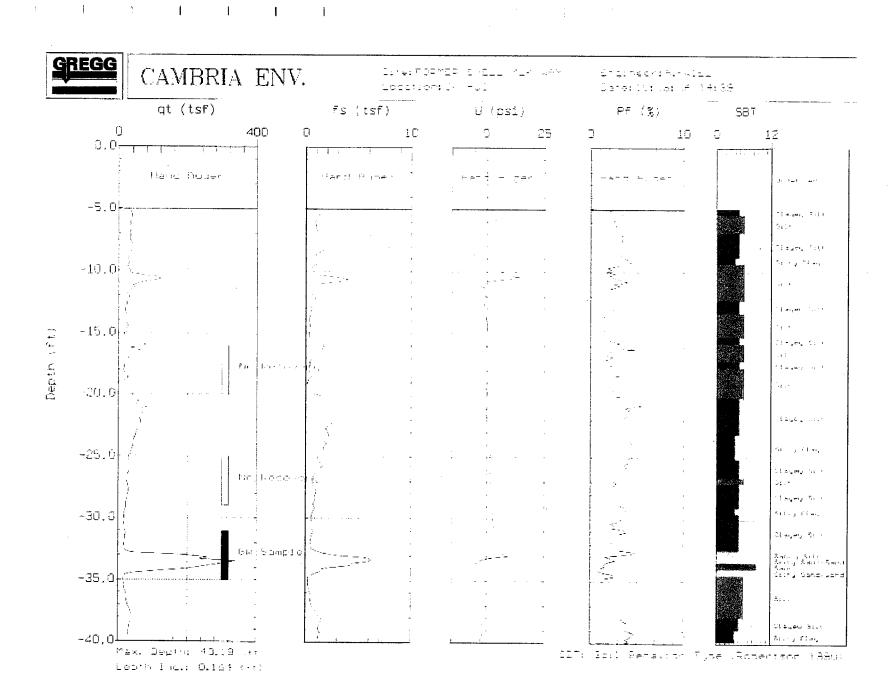
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Sounding: CPT-07

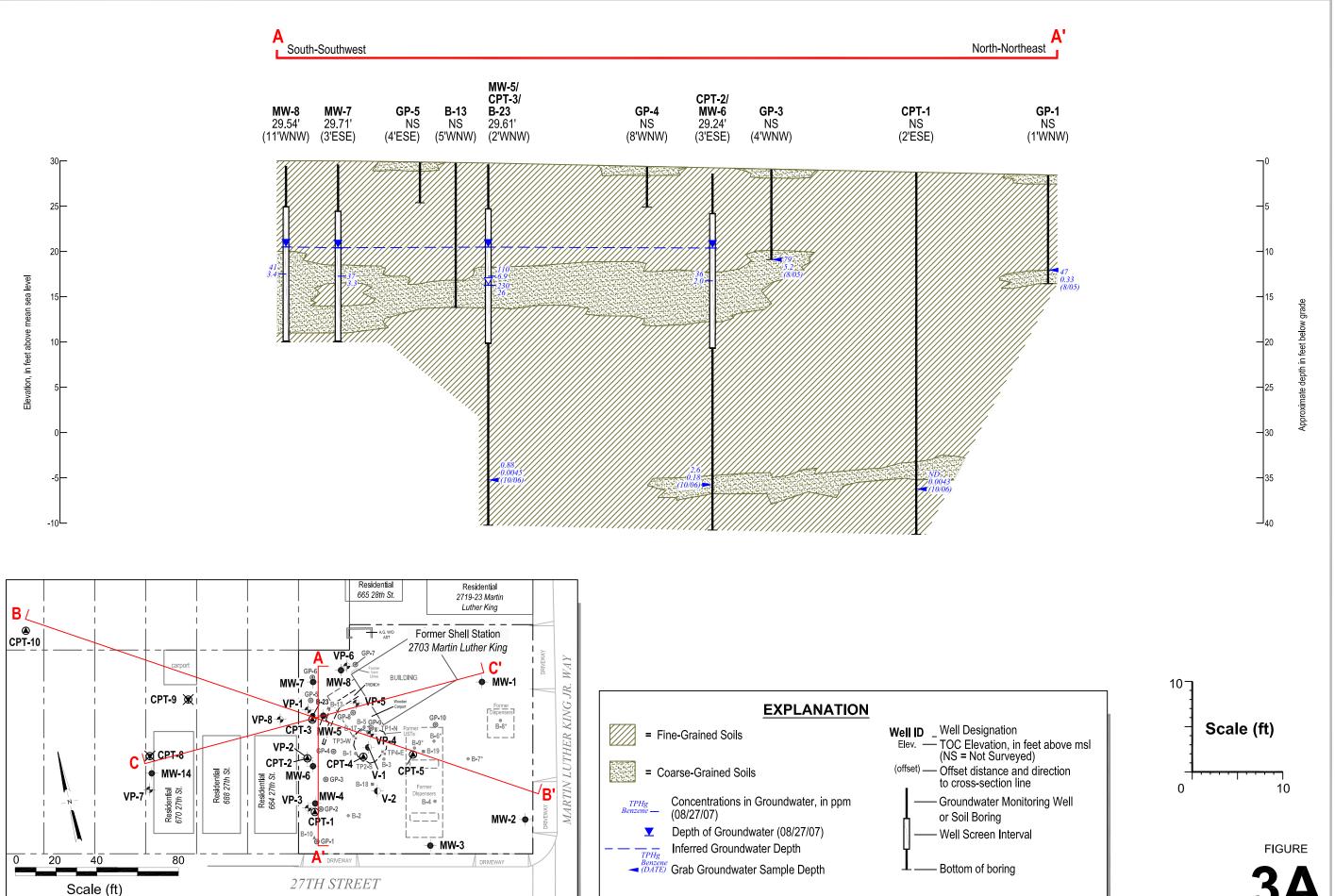
Engineer: A.FRIEL

Date: 5/17/2007 09:12





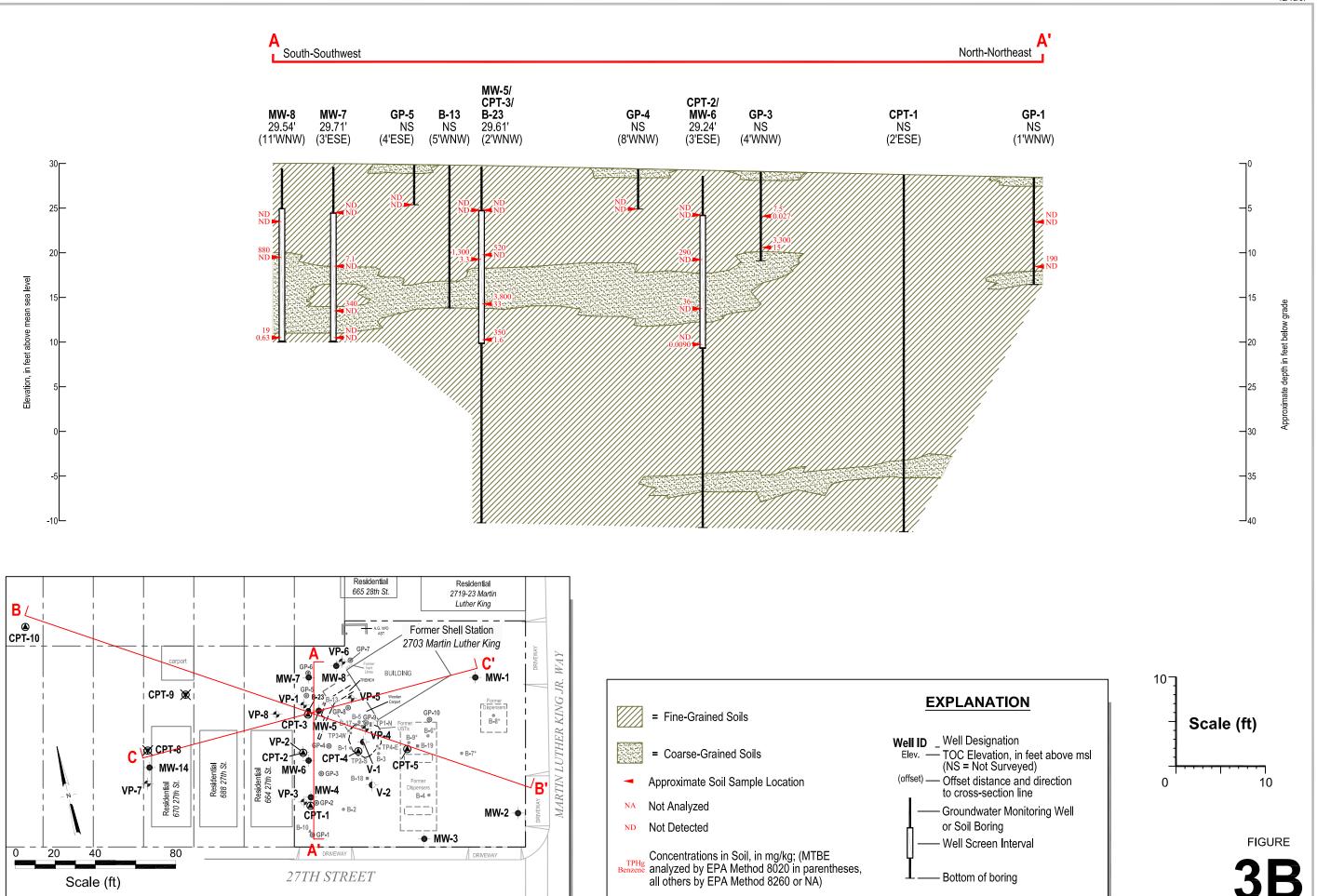
Cross Sectional Diagrams



Grab and QM Groundwater Results Section A-A' Geologic Cross

Former Shell Service Station

2703 Martin Luther King Jr. Way Oakland, California



Geologic Cross Section A-A'
- Soil Results

ONESTOGA-ROVERS

Former Shell Service Station

2703 Martin Luther King Jr. Way Oakland, California

→ (DATE) Grab Groundwater Sample Depth

TPHg Benzene (DATE)

CPT Groundwater Sampling Interval and Concentrations, in ppm (DATE)

● MW-3

27TH STREET

80

20

40

Scale (ft)

Bottom of boring

Former Shell Service Station 2703 Martin Luther King Jr. Way Oakland, California

Grab and QM Groundwater Results

80

27TH STREET

20

40

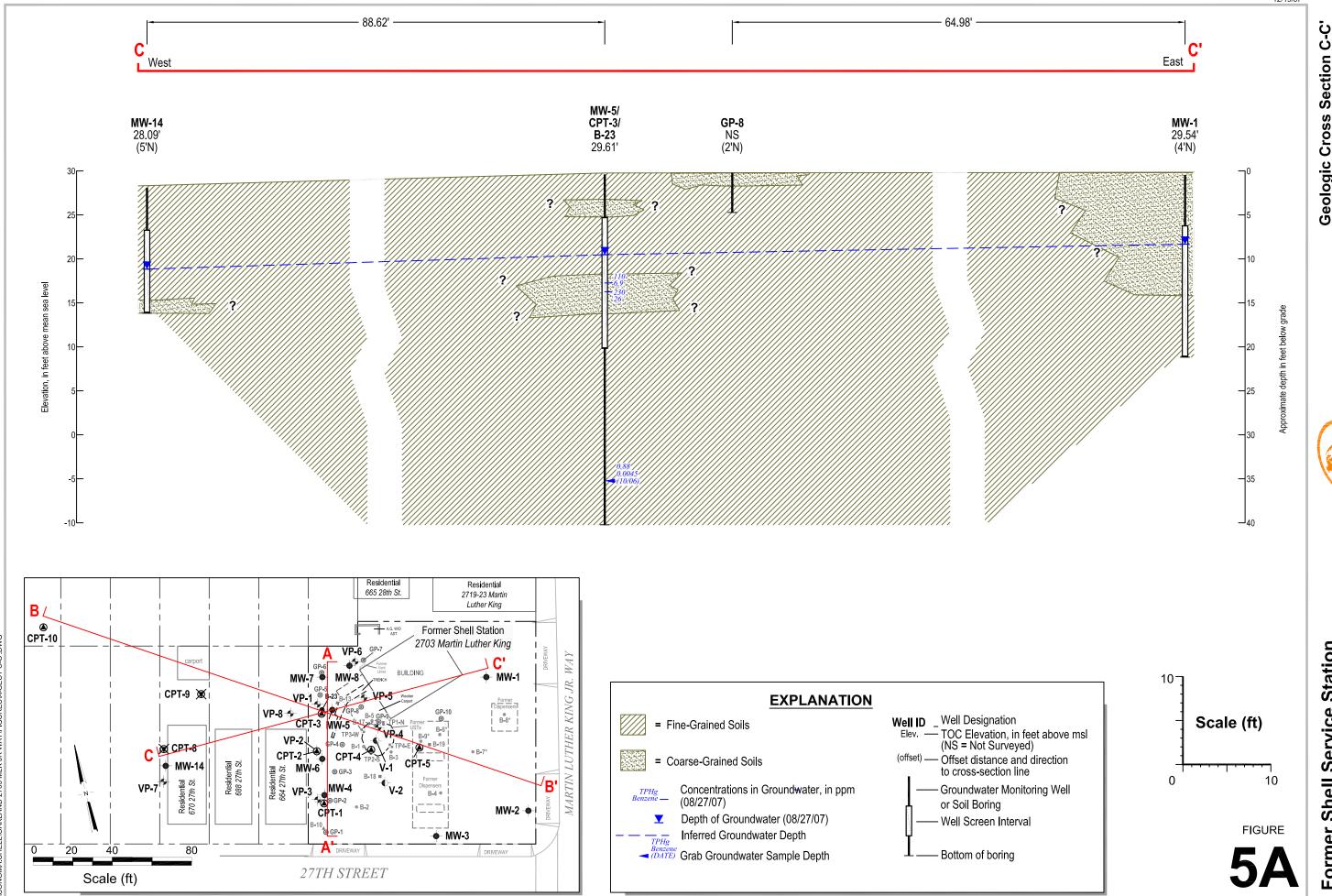
Scale (ft)

Concentrations in Soil, in mg/kg; (MTBE analyzed by EPA Method 8020 in parentheses,

all others by EPA Method 8260 or NA)

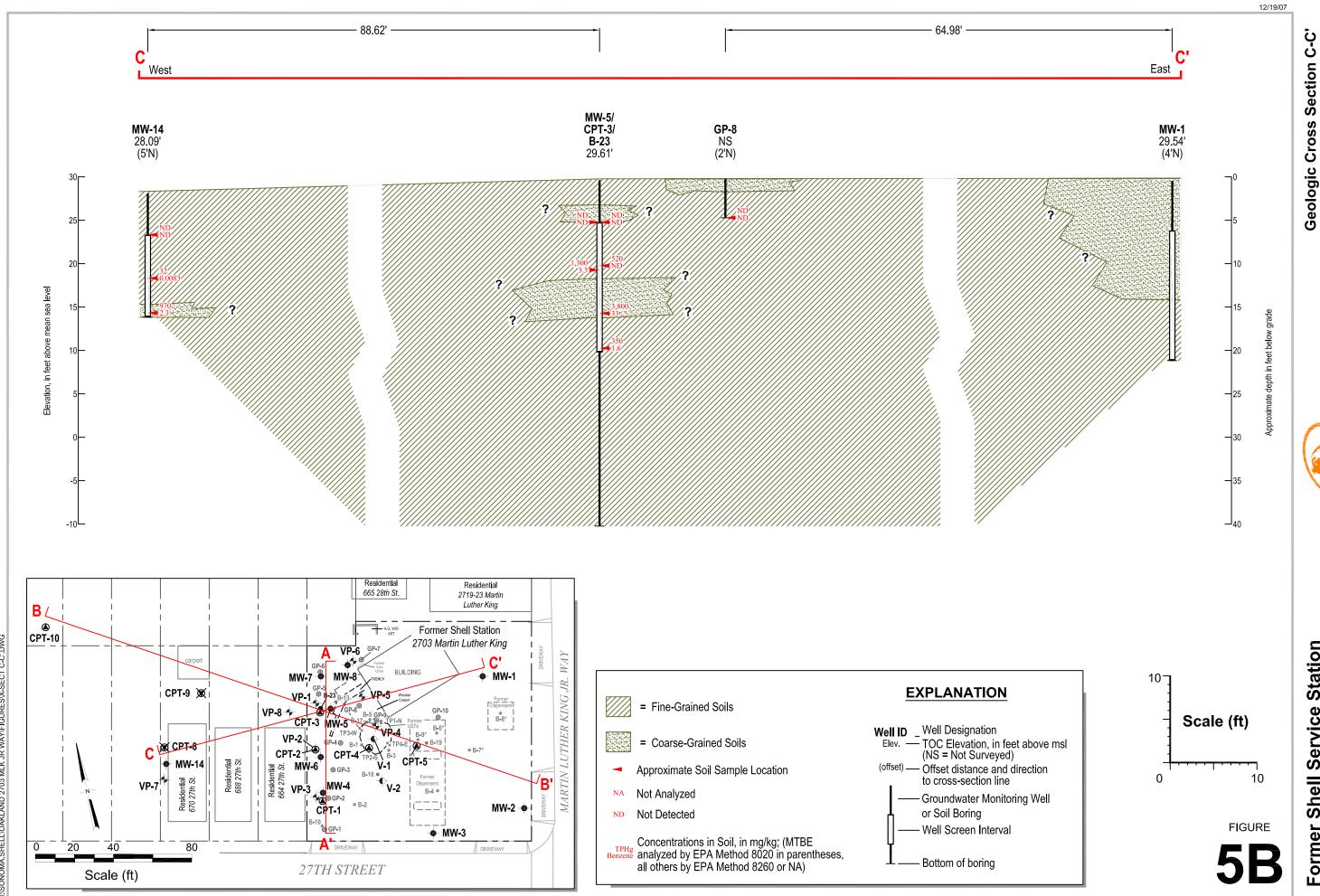
Bottom of boring

Former Shell Service Station 2703 Martin Luther King Jr. Way Oakland, California



Grab and QM Groundwater Results Section C-C' Geologic Cross

Former Shell Service Station 2703 Martin Luther King Jr. Way Oakland, California



Grab and QM Groundwater Results Geologic Cross

Former Shell Service Station

2703 Martin Luther King Jr. Way Oakland, California

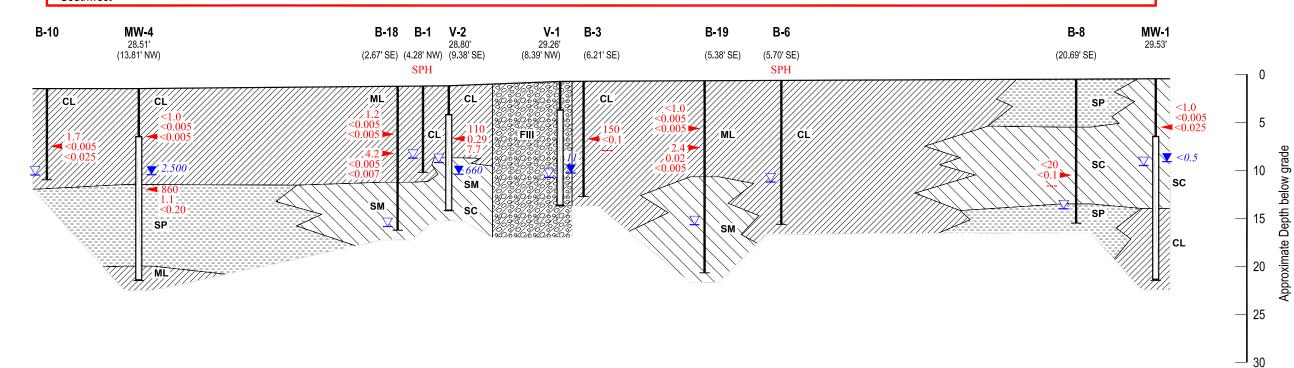
107

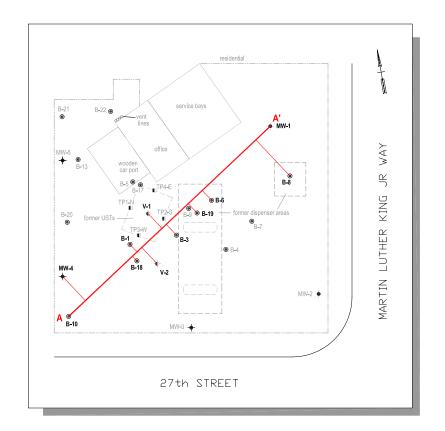
Scale (ft)

Former Shell Service Station 2703 Martin Luther King Jr. Way Oakland, California

FIGURE





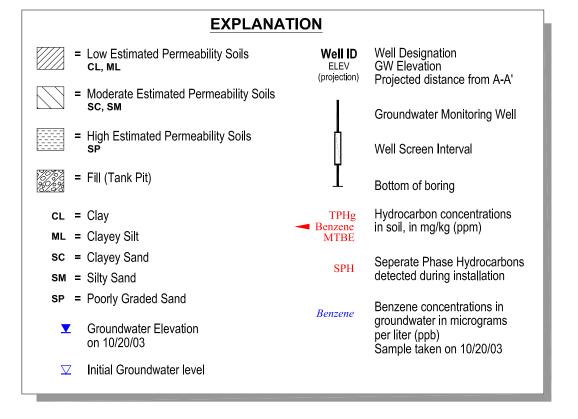


30_L

25

MSL^L

Elevation









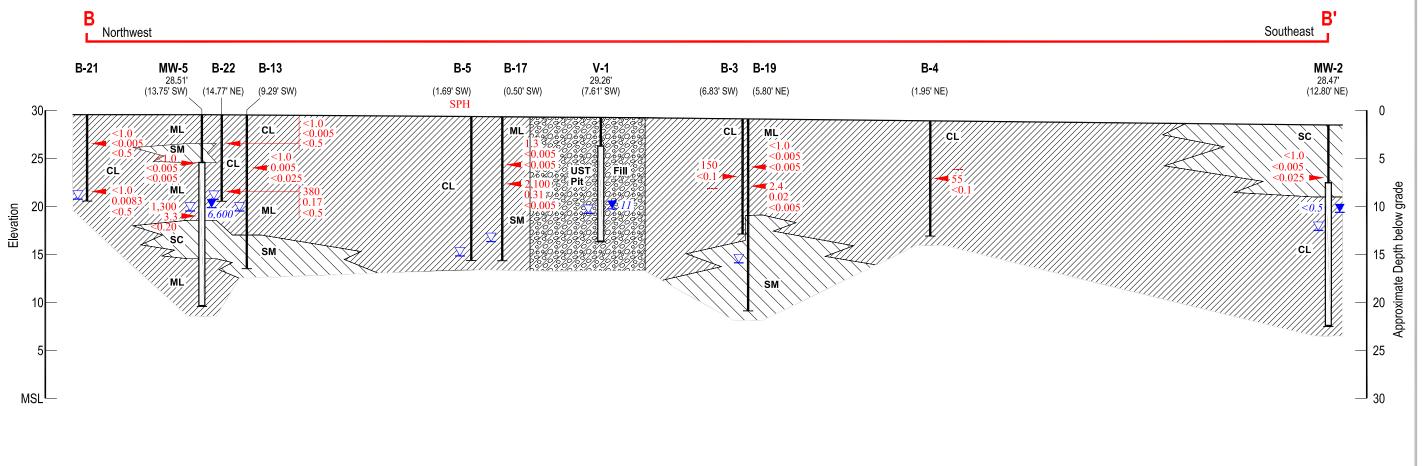
Former Shell Service Station

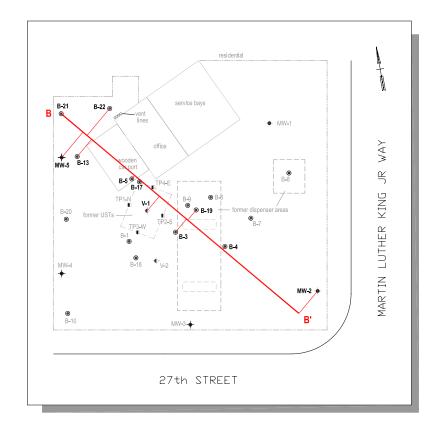
FIGURE

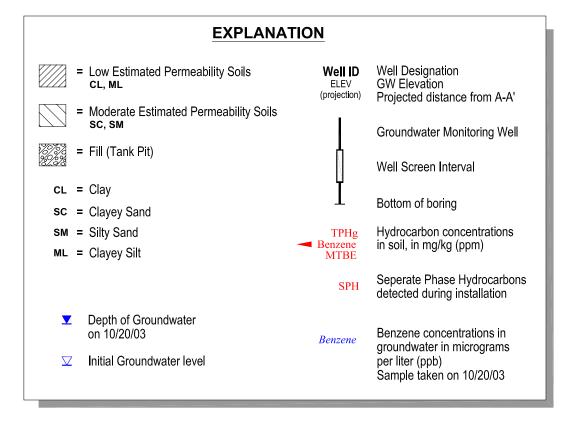
107

Scale (ft)

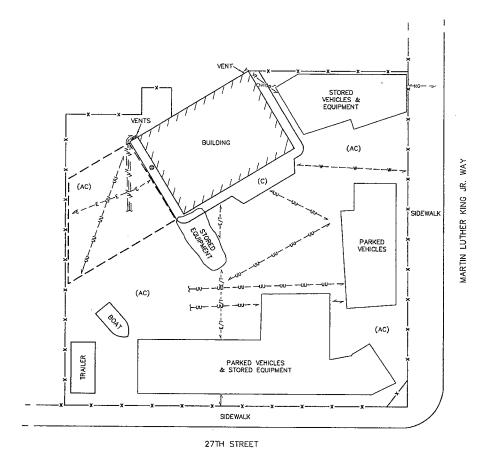
2703 Martin Luther King Jr. Way Oakland, California

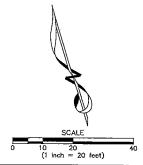






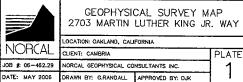
Utility Maps





	LEGEND
	LIMITS OF GPR/METAL DETECTOR SURVEY FOR POSSIBLE USTS
<u>—</u> е——	ELECTRIC LINE
—-Е/1	ELECTRIC & TELECOMMUNICATIONS LINE
	NATURAL GAS LINE
—-uu	UNDIFFERENTIATED UTILITY LINE
v	VENT LINE
vs vs	SUSPECTED VENT LINE
	WATER LINE
—х	CHAIN-LINK FENCE
0	SANITARY SEWER CLEANOUT
(AC)	ASPHALT
(c)	CONCRETE

PLATE



Historical Soil Vapor Sampling Results

Table 1. Soil Vapor Analytical Data, Former Shell Service Station, 2703 Martin Luther King Jr. Way, Oakland, California

Sample	Sample Depth	Date	TPHg	В	T	E	X	Isobutane	Butane	Propan
· ID	(fbg)	Sampled	(μg/m³)	(μg/m³)	(μg/m³)	(μg/m ³)	(μg/m ³)	(μg/m³)	(μg/m³)	(μg/m
VP-1-3	3	30-May-07	5,500,000	<510	690	<690	<2,090		·	
VP-1-5				Unable t	o sample; wa	ater in probe				
VP-2-3				Unable t	o sample; wa	iter in probe				
VP-2-5				Unable t	o sample; wa	iter in probe				
VP-3-3				Unable t	o sample; wa	ater in probe				
VP-3-5	5	30-May-07	31,000,000	760	<75	<86	<256			
VP-4-3	3	30-May-07	800,000	<79	240	<110	<320			
VP-4-5	5	30-May-07	680,000	<66	170	<90	<270			
VP-5-3				Unable t	o sample; wa	ater in probe				
VP-5-5				Unable t	o sample; wa	ater in probe				
VP-6-3	3	30-May-07	3,500,000	110	320	<55	160			
VP-6-5	5	30-May-07	1,900,000	<100	410	<140	<420			
Ambient (at site)		30-May-07	<19,000	16	16	<3.1	<9.2			
VP-7-3	3	12-Jun-07	<21,000	23	7,000	110	241			
VP-7-3	3	30-Oct-07	<19,000	<2.7	9.6	<3.6	<17.6	657.3	16.6	ND
VP-7-5	5	12-Jun-07	<21,000	23	2,100	110	230			
VP-7-5	5	30-Oct-07	<18,000	<2.5	15	<3.4	<16.4	402.4	ND	ND
VP-8-3	3	12-Jun-07	<23,000	20	9,300	120	267			
VP-8-3	3	30-Oct-07	<24,000	<3.4	34	<4.6	<22.6	395.1	7.8	NE
VP-8-3-DUP	3	30-Oct-07	<18,000	<2.6	6.5	<3.5	<17.5	366.6	ND	NE
VP-8-5	5	12-Jun-07	<22,000	33	11,000	120	278			
VP-8-5	5	30-Oct-07	<19,000	<2.6	8.5	<3.6	<17.6	468.3	5.9	NE

Table 1. Soil Vapor Analytical Data, Former Shell Service Station, 2703 Martin Luther King Jr. Way, Oakland, California

Abbreviations and Notes:

Results in bold exceed Environmental Screening Level

fbg = Feet below grade

 $\mu g/m^3 = micrograms per cubic meter$

< x =Not detected at reporting limit x

ND = Not detected

TPHg = Total petroleum hydrocarbons as gasoline by Modified EPA Method TO-3 GC/FID

BTEX = Benzene, tolunene, ethylbenzene, and xylenes by Modified EPA Method TO-15

Isobutane, butane, and propane by TPA Method TO-15

Table 4. Soil Vapor Analytical Data, Former Shell Service Station, 2703 Martin Luther King Jr. Way, Oakland, California

Sample ID	Sample Depth (fbg)	Date Sampled	TPHg (μg/L)	TPHg (μg/m³)	Β (μg/m³)	Τ (μg/m³)	Ε (μg/m³)	X (μg/m³)
GP-1-4.0	4.0	29-Aug-05	1.2	1,200	12	5.1	<5.5	9.8
GP-2-4.0	4.0	29-Aug-05	180	180,000	2,900	<22	<26	<26
GP-3-4.0	4.0	29-Aug-05	71,000	71,000,000	170,000	<2,100	<2,400	<2,400
GP-4-4.0	4.0	31-Aug-05	0.35	350	<4.1	8.9	<5.6	6.2
GP-5-4.0	4.0	30-Aug-05	3.1	3,100	5.4	5.4	<5.6	8.4
GP-6-4.0	4.0	29 - Aug-05	340	340,000	780	<22	<25	<25
GP-7-4.0	4.0	30-Aug-05	37	37,000	340	1,100	200	452
GP-8-4.0	4.0	30-Aug-05	1.6	1,600	8.4	5.0	<5.6	<5.6
GP-9-4.0	4.0	31-Aug-05	3.7	3,700	4.6	5.6	<6.0	6.9
GP-10-4.0	4.0	31-Aug-05	99	99,000	32	22	. 6.4	22
Environmental Scr SFBRWQCB, Fel		Commercial Residential	72 26	72,000 26,000	290 85	180,000 63,000	1,200,000 420,000	410,000 150,000

Abbreviations and Notes:

Results in bold exceed Environmental Screening Level

fbg = Feet below grade

 μ g/L = micrograms per liter

 $\mu g/m^3 = micrograms per cubic meter$

< x =Not detected at reporting limit x

TPHg = Total petroleum hydrocarbons as gasoline by Modified EPA Method TO-3 GC/FID

BTEX = Benzene, toluene, ethylbenzene, and xylenes by Modified EPA Method TO-14A

Sensitive Receptor Survey/Well Location Map

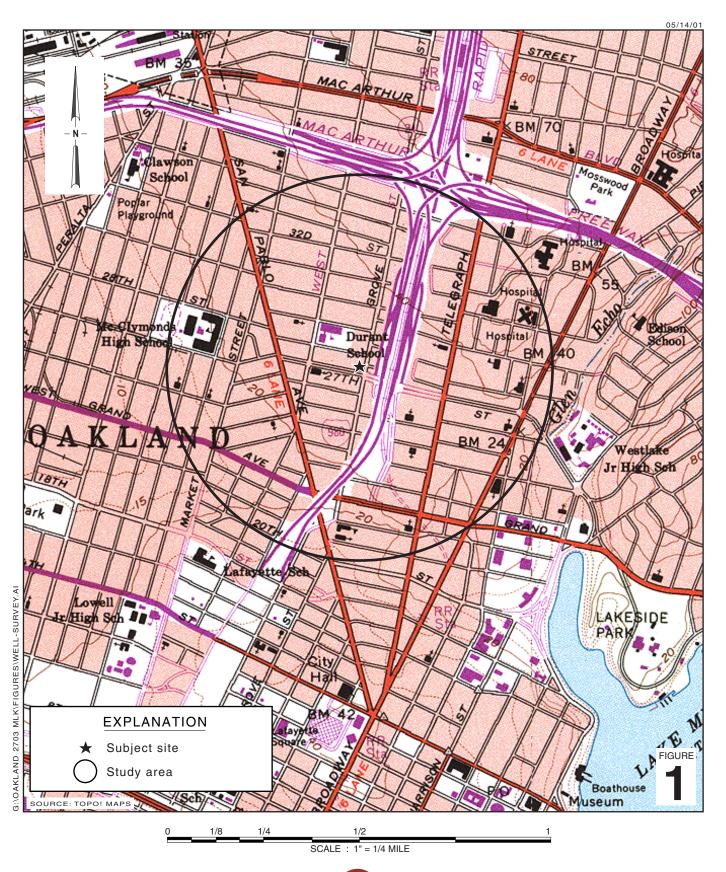
Table 1. Door-to-Door Survey Results - Former Shell Service Station, 2703 Martin Luther King Jr. Way, Oakland, California

Property Address	Basement	Basement Conditions	Foundation Type	UST's	Existing On- Site Wells	Vicinity Wells	Former On- Site Wells	Notes
2576 MLK Jr. Way	No	N/A	Slab on Grade	No	No	No	No	
2592 MLK Jr. Way	No	N/A	BLANK	No	No	Unknown	No	
2618 MLK Jr. Way	No	N/A	Unknown	No	No	Unknown	Unknown	
2624 MLK Jr. Way	No	N/A	Unknown	No	No	Unknown	Unknown	
2703 MLK Jr. Way	No	N/A	Slab on Grade	No	No	Unknown	No	Subject Site - monitoring wells exist on-site
2727 MLK Jr. Way	No	N/A	N/A	Unknown	Unknown	Unknown	Unknown	Empty lot
2760 MLK Jr. Way	No	N/A	N/A	Unknown	Unknown	Unknown	Unknown	Empty lot
2764 MLK Jr. Way	No	N/A	N/A	Unknown	Unknown	Unknown	Unknown	Empty lot
2766 MLK Jr. Way	No	N/A	Slab on Grade	No	Unknown	Unknown	Unknown	
2768 MLK Jr. Way	No	N/A	Slab on Grade	BLANK	Unknown	Unknown	Unknown	
2772 MLK Jr. Way	No	N/A	Slab on Grade	BLANK	Unknown	Unknown	Unknown	
2786 MLK Jr. Way	BLANK	BLANK	BLANK	BLANK	BLANK	BLANK	BLANK	Returned Blank Questionnaire
2827 MLK Jr. Way	No	N/A	Unknown	No	No	No	No	Answered "yes" to slab or perimeter
2831 MLK Jr. Way	No	N/A	Perimeter	No	No	Unknown	No	
553 27th Street	No	N/A	Unknown	No	No	No	No	
661 27th Street	No	N/A	Slab on Grade	No	No	Unknown	Unknown	A Phase 1 indicated a former laundry (non dry-cleaners) with no UST's
681 27th Street	No	N/A	Slab on Grade	No	No	Unknown	Unknown	A Phase 1 indicated a former laundry (non dry-cleaners) with no UST's
687 27th Street	No	N/A	BLANK	No	No	No	No	
690 27th Street	No	N/A	Perimeter	No	No	No	No	
709 27th Street	BLANK	BLANK	BLANK	BLANK	BLANK	BLANK	BLANK	Returned Blank Questionnaire
627 28th Street	No	N/A	Unknown	Unknown	Unknown	Unknown	Unknown	
628 Sycamore Street	No	N/A	Slab on Grade	No	No	No	No	
662 Sycamore Street	No	N/A	Perimeter	No	No	Unknown	Unknown	
740 26th Street	No	N/A	Slab on Grade	No	No	Unknown	Unknown	
2700 West St.	No	N/A	Unknown	No	No	Unknown	No	

Notes and Abbreviations:

N/A - Not Applicable

BLANK - No Response



Former Shell Service Station

2703 Martin Luther King Jr. Way□ Oakland, California Incident #97093397



Area Well Survey

CAMBRIA (1/2 - Mile Radius)

Table 1. Door-to-Door Survey Results, Former Shell Service Station, 2703 Martin Luther King Jr. Way, Oakland, California

	Resident	Rec'd	Well at	Basement	UST at	
	Present?	Response	Address?	at Address?	Address?	
Address		to Flyer?				Comments
721 26th Street	No	No	Unknown	Unknown	Unknown	
717 26th Street	No	No	Unknown	Unknown	Unknown	
713 26th Street	Yes	-	No	No	No	•
709 26th Street	No	No	Unknown	Unknown	Unknown	
701 26th Street	No	No	Unknown	Unknown	Unknown	
699 26th Street	No	No	Unknown	Unknown	Unknown	
691 26th Street	No	No	Unknown	Unknown	Unknown	
683 26th Street	No	No	Unknown	Unknown	Unknown	
679 26th Street	Yes	-	No	No	No	
669 26th Street	No	No	Unknown	Unknown	Unknown	
2565 Martin Luther King Jr Way	No	No	Unknown	Unknown	Unknown	
650 Sycamore Street	Yes	-	No	No	No	
658 Sycamore Street	No	No	Unknown	Unknown	Unknown	
662 Sycamore Street	No	No	Unknown	Unknown	Unknown	
670 Sycamore Street	No	No	Unknown	Unknown	Unknown	
676 Sycamore Street	No	No	Unknown	Unknown	Unknown	
678 Sycamore Street	No	No	Unknown	Unknown	Unknown	
682 Sycamore Street	No	No	Unknown	Unknown	Unknown	
686 Sycamore Street	Yes	-	No	No	No	
690 Sycamore Street	No	No	Unknown	Unknown	Unknown	
700 Sycamore Street	No	No	Unknown	Unknown	Unknown	
2627 Martin Luther King Jr Way	No	No	Unknown	Unknown	Unknown	
2619 Martin Luther King Jr Way	No	No	Unknown	Unknown	Unknown	
2611 Martin Luther King Jr Way	No	No	Unknown	Unknown	Unknown	
2601 Martin Luther King Jr Way	No	No	Unknown	Unknown	Unknown	
662 26th Street	No	No	Unknown	Unknown	Unknown	
672 26th Street	No	No	Unknown	Unknown	Unknown	
678 26th Street	No	No	Unknown	Unknown	Unknown	
686 26th Street	No	No	Unknown	Unknown	Unknown	
706 26th Street	No	Yes	No	No	Unknown	
710 26th Street	No	Yes	No	No		
714 26th Street	No	No	Unknown		Unknown	
724 26th Street	No	No	Unknown	Unknown	Unknown	
724 20th Street	No	No	Unknown	Unknown	Unknown	
732 26th Street	No	No		Unknown	Unknown	
736 26th Street	Yes		Unknown No	Unknown	Unknown	i e
740 26th Street		Yes		No	Unknown	
733 27th Street	No No	Yes	No	No	Unknown	
733 27th Street	No No	No	Unknown	Unknown	Unknown	
725 27th Street	No	No	Unknown	Unknown	Unknown	
723 27th Street		No No	Unknown	Unknown	Unknown	
719 27th Street	No No	No No	Unknown	Unknown	Unknown	
715 27th Street	No No	No No	Unknown	Unknown	Unknown	
713 27th Street 709 27th Street	No Voc	No	Unknown	Unknown	Unknown	
709 27th Street	Yes	-	No	No	No	
	Yes	Na	No	No	No	
705 27th Street	No	No	Unknown	Unknown	Unknown	
697 27th Street	No	No	Unknown	Unknown	Unknown	
691 27th Street	No	No	Unknown	Unknown	Unknown	
687 27th Street	No	No	Unknown	Unknown	Unknown	
683 27th Street	Yes	Yes	No	Yes	Unknown	
681 27th Street	No	No	Unknown	Unknown	Unknown	
661 27th Street	No	No	Unknown	Unknown	Unknown	
624 Sycamore Street	No	No	Unknown	Unknown	Unknown	

Table 1. Door-to-Door Survey Results, Former Shell Service Station, 2703 Martin Luther King Jr. Way, Oakland, California

	Resident	Rec'd	Well at	Basement	UST at	
	Present?	Response	Address?	at Address?	Address?	
Address		to Flyer?				Comments
628 Sycamore Street	No	No	Unknown	Unknown	Unknown	
2576 Martin Luther King Jr Way	No	No	Unknown	Unknown	Unknown	
2592 Martin Luther King Jr Way	No	Yes	No	No	Unknown	Vacant businesses; 2582-2592 MLF
2606 Martin Luther King Jr Way	Yes	-	Unknown	No	No	2600-2606 MLK
2610 Martin Luther King Jr Way	Yes	-	No	No	No	2608/2610 MLK
2618 Martin Luther King Jr Way	No	Yes	No	No	Unknown	2000/2010 MILIE
2624 Martin Luther King Jr Way	No	Yes	No	No	Unknown	
2718 Martin Luther King Jr Way	No	No	Unknown	Unknown	Unknown	,
2750 Martin Luther King Jr Way	No	No	Unknown	Unknown	Unknown	
2756 Martin Luther King Jr Way	Yes	-	No	No	No	
2760 Martin Luther King Jr Way	No	No	Unknown	Unknown	Unknown	
2764 Martin Luther King Jr Way	No	No	Unknown	Unknown	Unknown	
2766 Martin Luther King Jr Way	No	Yes	No	No	Unknown	
2768 Martin Luther King Jr Way	No	Yes	No	No		
2772 Martin Luther King Jr Way	No	Yes	No		Unknown	
2786 Martin Luther King Jr Way	No	No	Unknown	No	Unknown	
627 28th Street	No			Unknown	Unknown	
663 28th Street		No	Unknown	Unknown	Unknown	
2727 Martin Luther King Jr Way	No	No	Unknown	Unknown	Unknown	
	No	No	Unknown	Unknown	Unknown	
2721 Martin Luther King Jr Way	No	Yes	No.	No	Unknown	
664 27th Street	No	No	Unknown	Unknown	Unknown	
668 27th Street	No	No	Unknown	Unknown	Unknown	
670 27th Street	No	No	Unknown	Unknown	Unknown	
672 27th Street	No	No	Unknown	Unknown	Unknown	
676 27th Street	No	Yes	No	Yes	Unknown	
680 27th Street	No	Yes	No	No	Unknown	
682 27th Street	Yes	-	No	No	No	682/684 27th
688 27th Street	No	No	Unknown	Unknown	Unknown	
690 27th Street	No	No	Unknown	Unknown	Unknown	
696 27th Street	Yes	-	No	Yes	No	
700 27th Street	No	Yes	No	Yes	Unknown	
708 27th Street	Yes	-	No	No	No	
714 27th Street	No	No	Unknown	Unknown	Unknown	
2700 West Street	No	Yes	No	No	Unknown	
2212 West Street	No	No	Unknown	Unknown	Unknown	
685 28th Street	No	No	Unknown	Unknown	Unknown	
683 28th Street	No	Ņo	Unknown	Unknown	Unknown	
679 28th Street	No	No	Unknown	Unknown	Unknown	
673 28th Street	No	No	Unknown	Unknown	Unknown	
669 28th Street	No	No	Unknown	Unknown	Unknown	
837 Martin Luther King Jr Way	Yes	-	No	No	No	
833 Martin Luther King Jr Way	No	No	Unknown	Unknown	Unknown	
2831 Martin Luther King Jr Way	Yes	-	No	No	No	•
2827 Martin Luther King Jr Way	No	No	Unknown			
2823 Martin Luther King Jr Way	No	No	Unknown	Unknown	Unknown	
2821 Martin Luther King Jr Way				Unknown	Unknown	
668 28th Street	No No	No	Unknown	Unknown	Unknown	
674 28th Street	No Voc	No	Unknown	Unknown	Unknown	
	Yes	-	No	Yes	No	
682 28th Street	No	No	Unknown	Unknown	Unknown	
686 28th Street	No	No	Unknown	Unknown	Unknown	
675 29th Street	No	No	Unknown	Unknown	Unknown	
665 29th Street	No	No	Unknown	Unknown	Unknown	
2850 West Street	Yes	-	No	No	No	

Table 1. Door-to-Door Survey Results, Former Shell Service Station, 2703 Martin Luther King Jr. Way, Oakland, California

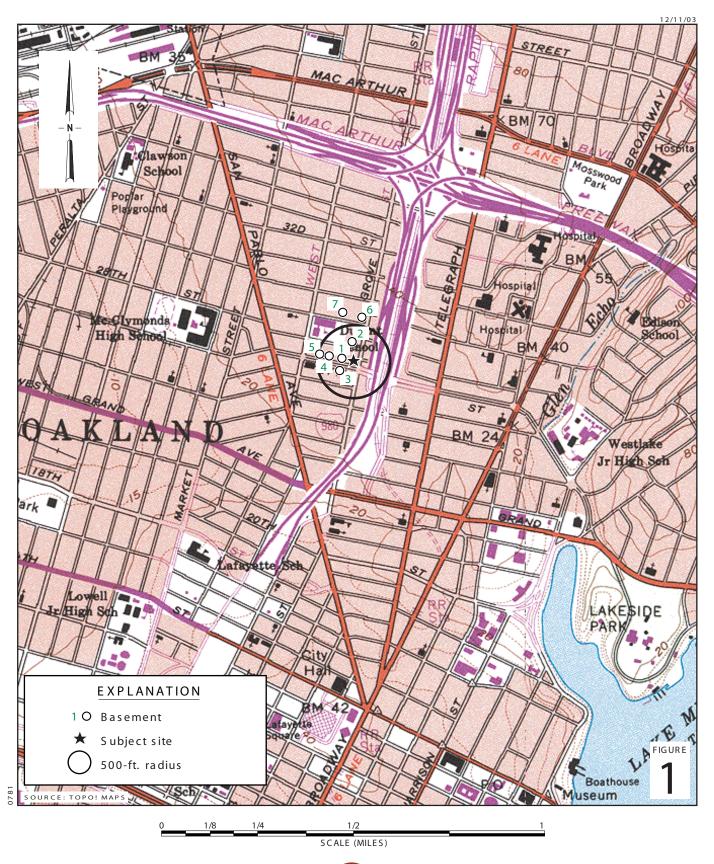
	Resident	Rec'd	Well at	Basement	UST at	
	Present?	Response	Address?	at Address?	Address?	
Address		to Flyer?		_		Comments
2903 Martin Luther King Jr Way	Yes	-	No	Yes	No	
670 29th Street	No	. No	Unknown	Unknown	Unknown	
678 29th Street	No	Yes	No	No	Unknown	
682 29th Street	No	No	Unknown	Unknown	Unknown	
686 29th Street	No	No	Unknown	Unknown	Unknown	
696 29th Street	Yes	-	No	Yes	No	
700 29th Street	No	No	Unknown	Unknown	Unknown	
630 28th Street	No	No	Unknown	Unknown	Unknown	
638 28th Street	No	No	Unknown	Unknown	Unknown	
644 28th Street	No	No	Unknown	Unknown	Unknown	
2818 Martin Luther King Jr Way	No	No	Unknown	Unknown	Unknown	Vacant home
2822 Martin Luther King Jr Way	No	No	Unknown	Unknown	Unknown	
2836 Martin Luther King Jr Way	No	No	Unknown	Unknown	Unknown	

Table 2. Basement Data, Former Shell Service Station, 2703 Martin Luther King Jr. Way, Oakland, California

Map Number	Address	Basement Floor Material	Sump Pump?	Approximate Distance from Site (feet)	Direction of Basement from Site
1	676 27th Street	Concrete	Unknown	180	W
2	674 28th Street	Earth	Unknown	240	N
3	683 27th Street	Concrete	Yes	260	sw
4	696 27th Street	Unknown	No	370	W
5	700 27th Street	Earth	Unknown	450	w
6	2903 Martin Luther King Jr Way	Earth	Unknown	580	N N
7	696 29th Street	Concrete/Earth	Yes	620	N N

Notes:

Map number corresponds to Site Vicinity/Receptor Survey Map (Figure 1)



Former Shell Service Station 2703 Martin Luther King Jr. Way Oakland, California



CAMBRIA

Site Vicinity/Receptor Survey Map

List of Environmental Documents

2703 Martin Luther King Jr. Way, Oakland, California - List of Known Environmental Documents					
Date	Title/Subject	Company			
26-Oct-94	Closure Report	KTW			
1-Jun-95	Phase II Envoronmental Site Investigation	ACC Env. Consultants			
2-Jan-96	Site Investigation Work Plan	Enviros			
10-May-96	Over-excavation & Sampling	Enviros			
30-Oct-96	Soil Boring Well Installation Report	Enviros			
16-May-01	Site Investigation Report	Cambria			
16-May-01	Subsurface Investigation Report	Cambria			
19-Dec-01	Subsurface Investigation Work Plan	Cambria			
21-Jun-02	Site Investigation Report	Cambria			
16-Dec-03	Sensitive Receptor Survey, Geologic Cross Sections and Fourth Quarter 2003 Groundwater				
	Monitoring Report	Cambria			
12-Aug-05	Response to Technical Comments, Notification of Field Work, and Request for Extension	Cambria			
15-Aug-05	Revised Response to Technical Comments, Notification of Field Work, and Request for				
	Extension	Cambria			
15-Nov-05	Site Investigation Report	Cambria			
22-Nov-05	Feasibility Study Work Plan	Cambria			
20-Dec-05	Plume Delineation Work Plan	Cambria			
20-Jan-06	Door to Door Survey Report, Access Agreement Update, and Status/Schedule Update	Cambria			
14-Mar-06	Pilot Test Report	Cambria			
14-Apr-06	Site Investigation Report, and First Quarter 2006 - Groundwater Monitoring Report	Cambria			
25-May-06	Subsurface Investigation Report	Cambria			
25-Jul-06	Status Update, Report of Geophysical Survey, and Request for Agency Meeting	Cambria			
31-Jan-07	CPT Investigation and Vapor Probe Installation Report	Cambria			
27-Aug-07	Plume Delineation and Soil Vapor Sampling Report	CRA			
13-Nov-07	Monitoring Well and Vapor Point Installation Work Plan	CRA			
Various	Groundwater Monitoring Reports - First Quarter 1997 through current	Cambria/CRA			