



GeoStrategies Inc.
 Environmental Consulting,
 Engineering and Geologic Services

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Letter of Transmittal

Date: 11/30/92

From: ROBERT MALLORY
 To: MR. DENNIS BYRNE
ACHCSA
80 SWAN WAY # 200
OAKLAND, CA. 94621

Project No: 7927
 Subject: CONT. SITE ASSESSMENT - 3RD qtr. '92
ARCO 55th 2169
889 W. GRAND AVE.
OAKLAND, CA. 94601

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Comments:

CC: MR. MICHAEL WHELAN, ARCO PRODUCTS CO.
MR. H.C. WINSOR, ARCO PRODUCTS CO.
MR. RICHARD HIETT, RWQCB - S.F. REGION

Robert C. Mallory
 (Signed)

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GeoStrategies Inc.

92-031-1 (11-92)

**CONTINUING SITE ASSESSMENT/QUARTERLY
MONITORING REPORT - Third Quarter 1992**

ARCO Service Station No. 2169
889 West Grand Avenue
Oakland, California

792705-4

November 24, 1992



GeoStrategies Inc.

2140 WEST WINTON AVENUE
HAYWARD, CALIFORNIA 94545

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November 24, 1992

ARCO Products Company
P.O. Box 5811
San Mateo, California 94402

Attn: Mr. Michael Whelan

Re: CONTINUING SITE ASSESSMENT/QUARTERLY
MONITORING REPORT - Third Quarter 1992
ARCO Service Station No. 2169
889 West Grand Avenue
Oakland, California

Gentlemen:

INTRODUCTION

This Continuing Site Assessment/Quarterly Monitoring Report was prepared by GeoStrategies Inc. (GSI) and presents field activities and ground-water sampling results for the above referenced location (Plate 1). On June 8, 1992 four exploratory soil borings were drilled and completed as recovery well AR-2 and vapor extraction wells AV-1 through AV-3. Well locations are shown on Plate 2. A vapor extraction test was performed on June 11, 1992. Step/drawdown and constant-rate aquifer tests were performed on July 15 and 16, 1992. These tests were performed to evaluate air and groundwater flow characteristics in the unsaturated and saturated zones beneath the site. Quarterly monitoring and sampling of site wells were conducted by the ARCO contractor on July 17, 1992. Field work was performed to comply with current State of California Water Resources Control Board (SWRCB) and local agency guidelines. GSI Field Methods and Procedures were presented in the GSI Work Plan dated October 29, 1991.

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SITE BACKGROUND

On May 14, 1991, GSI drilled five exploratory soil borings (A-A through A-E), as documented in a GSI Preliminary Tank Replacement Report dated July 1, 1991. Four soil borings were drilled adjacent to the underground storage tank (UST) complex (A-B through A-E) and one soil boring (A-A) was drilled in the proposed UST complex location. Total Petroleum Hydrocarbons calculated as Gasoline (TPH-Gasoline) and as Diesel (TPH-Diesel) and Benzene, Toluene, Ethylbenzene, and Xylenes (BTEX) were detected in soil samples from each boring collected from 5.5 to 11.0 feet below grade. In addition, a well adjacent to the existing USTs was properly abandoned.

In February and March 1992, the underground storage tanks at the site were removed and replaced. The former tank complex was composed of four steel tanks: one 12,000 gallon tank (unleaded), one 8,000 gallon tank (regular), and two 6,000 gallon tanks (diesel and super unleaded). The present tank complex is composed of four double wall fiberglass 10,000 gallon tanks containing unleaded gasoline and diesel products. The location of the former and present tank complexes are shown on Plate 2. Soil sample analytical results from the former tank complex confirmed results from previous soil boring samples that petroleum hydrocarbons had impacted soil in the tank complex vicinity to a depth of 12 feet below grade. Soil sample results from product line trenching revealed a TPH-Diesel concentration of 450 ppm in the vicinity of the diesel dispenser on the westernmost island. This area was overexcavated and resampled at a depth of 7 feet below ground surface. Results of the second sample identified TPH-Diesel at a concentration of 54 ppm. TPH-Gasoline and benzene were reported at levels of less than or equal to 120 ppm and 0.36 ppm, respectively, from the remaining trench samples. An Underground Storage Tank Removal and Soil Sampling Report documenting the tank removal and soil sampling analytical results was issued by ROUX Associates (ROUX) on July 14, 1992.

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Between March 16 and 25, 1992 five exploratory soil borings were drilled and completed as recovery well AR-1 and ground-water monitoring wells A-1 through A-4. TPH-Gasoline was detected in the soil sample from a depth of 10.0-feet in Boring A-1 at a concentration of 2.2 parts per million (ppm). Benzene was identified in samples from depths of 4.5-feet and 10.0-feet in Boring A-1 at concentrations of 0.024 ppm and 0.13 ppm, respectively. Results of this investigation are presented in the GSI Well Installation Report dated June 30, 1992.

Quarterly ground-water monitoring and sampling of site wells began in April, 1992. Ground-water samples are currently analyzed for TPH-Gasoline according to EPA Method 8015 (Modified) and BTEX according to EPA Method 8020.

WELL INSTALLATION FIELD ACTIVITIES

Four on-site exploratory borings were drilled on June 8, 1992, using a truck-mounted, hollow-stem auger drilling rig. Borings AV-1 through AV-3 and AR-2 were drilled to total depths ranging from 14.5 to 30.5 feet below grade. Soil samples were collected at five-foot intervals using a modified California split-spoon sampler fitted with stainless steel sample tube liners. A GSI geologist observed the drilling, described the soil samples using the Unified Soil Classification System (ASTM D 2488-84) and Munsell Soil Color Chart, and prepared a lithologic log for each boring. Exploratory boring logs are presented in Appendix A.

Soil Sampling

An Organic Vapor Monitor (OVM) photoionization detector was used to perform head-space analysis on soils from each sampled interval, as a reconnaissance - level test for the presence of Volatile Organic Compounds (VOCs) in the soil. Head-space analysis results are presented on each boring log in Appendix A.

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Soil samples retained for chemical analyses were collected in clean stainless steel liners and sealed on both ends with aluminum foil and plastic end caps. Samples were labeled, entered onto a Chain-of-Custody form, and transported in a cooler with blue ice to Sequoia Analytical (Sequoia), a State-certified environmental laboratory located in Redwood City, California.

Recovery Well Installation

Boring AR-2 was drilled using 10-inch-diameter hollow-stem augers to a depth of 30.5 feet below existing ground surface. This boring was drilled through a 12-inch-diameter conductor casing installed to a depth of 10-feet below grade in the new tank complex. Native material was used to backfill the boring from 28.5 to 30.5 feet below grade during well construction. Recovery well AR-2 was constructed using 4-inch-diameter Schedule 40 PVC well casing and carbon steel 0.020-inch continuous wrap well screen. The well screen extends from 8.5 to 28.5 feet below grade. Lonestar #2/12 graded sand was placed in the annular space across the entire screened interval and extends 1.0-foot above the top of the well screen. A one-foot thick bentonite seal was placed above the sandpack and then hydrated with clean water. A neat cement seal was placed from the top of the bentonite to 4.0-foot below ground surface. The well was completed in an underground vault box, set in the concrete slab of the new tank complex, and a waterproof locking well cap and lock was placed on the well casing.

Vapor Extraction Well Installation

Borings AV-1 through AV-3 were installed using 8-inch-diameter hollow-stem augers to a depth of 14.5 feet below grade. Bentonite was placed in the lower 0.5 feet of Borings AV-1 through AV-3 as a bottom seal. The vapor extraction wells were constructed using 2-inch-diameter Schedule 40 PVC blank well casing and 0.020-inch factory slotted well screen. Well screen extends from [REDACTED] to [REDACTED]. Lonestar #2/12 graded sand was placed across the entire screened interval and extends one-half-foot above the top of the well screen. A one-half-foot thick bentonite seal was placed above the sandpack and then hydrated with clean water. A neat cement seal was placed from the top of the bentonite to approximately 1.0-foot below ground surface. A waterproof underground vault box, set in concrete, was installed over the top of each well and a waterproof locking well cap and lock were placed on the well casings. Well completion details are presented with the Exploratory Boring Logs in Appendix A.

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Soil Chemical Analytical Results

Soil samples were analyzed for Total Petroleum Hydrocarbons calculated as Gasoline (TPH-Gasoline) and as Diesel (TPH-Diesel) according to EPA Method 8015 (Modified) and Benzene, Toluene, Ethylbenzene, and Xylenes (BTEX) according to EPA Method 8020. Chemical analyses were performed by Sequoia in Redwood City, California.

Soil chemical analytical data are summarized in Table 1. Six soil samples from Borings AV-1 through AV-3, collected at depths ranging between 6.5 and 12 feet below grade, were selected for chemical analysis. Soil samples from Boring AR-2 were not analyzed due to fill material being encountered from ground surface to first encountered water. TPH-Gasoline was detected in the soil sample from Boring AV-2 at a depth of 6.5, at a concentration of 1.8 parts per million (ppm). Benzene was identified in soil samples collected at a depth of 6.5 feet from Borings AV-1 through AV-3 at concentrations of 0.15 ppm, 0.31 ppm, and 0.037 ppm, respectively. TPH-Gasoline was detected in each sample collected from depths of 11.5 to 12 feet from Borings AV-1 through AV-3 at concentrations of 12 ppm, 1,500 ppm, and 110 ppm, respectively. Benzene was reported in these samples at concentrations of 0.81 ppm, 21 ppm, and 2.4 ppm, respectively. TPH-Diesel was reported as not detected (ND) in each soil sample analyzed. The Sequoia chemical analytical report and Chain-of-Custody form are presented in Appendix B.

HYDROGEOLOGIC CONDITIONS

Regional Setting

The site is located in Oakland, California at the base of the Berkeley Hills approximately 1/2-mile east of the San Francisco Bay. The site is situated on alluvial-fan deposits of the Temescal Formation comprised of interfingering lenses of clayey gravel, sandy silty clay, and sand-clay-silt mixtures (Radbruch, D.H., 1957). Local topography suggests ground-water flows to the west toward San Francisco Bay.

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Local Setting

Based on exploratory boring data from previous investigations, the local subsurface lithology appears to consist of clay, sand, silt, and minor gravel to the total depth explored of 30.5 feet below ground surface. Borings AV-1 through AV-3 sampled subsurface lithology to a depth of 14.5 feet below ground surface and Boring AR-2 encountered fill material to a depth of 15 feet and native material to the total depth explored of 30.5 feet. Clay was observed in borings AV-1 through AV-3 from ground surface to between 10.5 (AV-2) and 13.5 (AV-1) feet below grade. The clay was underlain by sand, clayey and silty sand, and silt to the total depths of the borings. Boring AR-2 encountered interbedded sand, clayey sand, and sandy silt from 15 feet to the total depth explored of 30.5 feet. Cross-sections have been prepared from site boring logs and are presented on Plates 3 and 4. Groundwater was first encountered in Borings AV-1 through AV-3 at a depth of 12-feet below grade and in Boring AR-2 at a depth 15-feet below grade. Water-levels stabilized after completion of Well AR-2 at a depth of 13 feet below grade. This rise in the water-level in AR-2 indicates semi-confined to confined aquifer conditions.

VAPOR EXTRACTION TEST FIELD ACTIVITIES

An eight hour vapor extraction test was performed on June 11, 1992, utilizing vapor extraction well AV-2 and an Internal Combustion (IC) engine to create a vacuum on the extraction well and combust extracted vapors. Vapor extraction wells AV-1 and AV-3 were used to monitor vacuum pressure changes during the test using a manometer. Vacuum pressure and flow rate from the extraction well were measured and recorded on an approximate hourly basis throughout the test. Air stream concentrations from the extraction well before and after combustion (i.e. influent and effluent vapor concentration readings) were also monitored utilizing an infrared (IR) detector and recorded. Influent and effluent air stream samples were collected near the end of the test, entered on a Chain-of-Custody form and transported to Sequoia. Air samples were analyzed for TPH-Gasoline and BTEX according to EPA Methods 8015 (Modified) and 8020, respectively.

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Vadose Zone Lithology

Based on exploratory borings drilled at the site, the unsaturated zone appears to be composed primarily of clay to a depth of approximately 8 feet and sand, silty and clayey sand, and silt to the static ground-water surface of approximately 12 to 13.5 feet below grade.

Results

Vacuum pressure, flow rate, and influent concentration data from the extraction well were recorded during the test and are presented in Table 2. Vacuum pressure in extraction well AV-2 ranged from 76.7 to 119.8-inches of water. Vacuum pressure results for the observation wells are presented in Table 3. Pressure changes recorded at the end of the test from the observation wells ranged from 0.14 to 1.4 inches of water. Vacuum pressure recorded at the end of the test have been used to construct a Vacuum Pressure Map (Plate 5). Based the Vacuum Pressure Map the estimated radius of influence is 50-feet from the extraction well. Flow rate from the extraction well ranged from 10.8 to 23.8 cubic feet per minute (cfm) and appeared to stabilize at approximately 22 cfm three hours into the test.

Influent vapor concentrations were recorded on an hourly basis during the eight hour test (Table 2). These data exceeded the maximum range of 14,000 parts per million (ppm) of the IR detector during each hour of the test. Concentrations measured by the IR detector are calibrated to Hexane and should not be considered a quantitative measure of TPH-Gasoline or BTEX.

The results of laboratory chemical analysis of the influent and effluent air samples are summarized in Table 4. TPH-Gasoline and benzene were identified in the effluent air sample at concentrations of 13 parts per million vapor (ppmv) and 1.9 ppmv, respectively. TPH-Gasoline and benzene were detected in the influent sample at concentrations of 24,000 ppmv and 1,300 ppmv, respectively. The air sample laboratory analytical report and Chain-of-Custody Form are presented in Appendix C.

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AQUIFER TEST FIELD ACTIVITIES

A 4-hour step-drawdown test and a 24-hour constant-rate test were performed utilizing recovery well AR-1 on July 15 and 16, 1992. The tests were performed to assess the feasibility of utilizing recovery well AR-1 to achieve hydrodynamic control of groundwater for extraction of petroleum hydrocarbons from the first encountered water-bearing zone. Recovery well AR-1 was installed to extract groundwater from the shallow aquifer zone beneath the site and to assess aquifer parameters for potential recovery system design.

Water-level measurements were obtained from recovery wells AR-1 and AR-2 and monitoring wells A-1 through A-4 prior to conducting the test to establish baseline data (Plate 6). Pressure transducers connected to a Hermit SE2000 data logger were installed in recovery well AR-1 and two selected observation wells (A-1 and A-4) to monitor water-level changes during the tests. Water-level changes in Wells A-2, A-3 and AR-2 were measured with an electronic interface probe at various time intervals throughout the duration of the tests.

AQUIFER TEST RESULTS

Data collected during the 4-hour step-drawdown and 24-hour constant-rate test were evaluated and used to calculate specific aquifer parameters; Transmissivity (T) and Storativity (S). Additional aquifer and well characteristics evaluated include observed radius of influence and well efficiency.

Step-Drawdown Test

Well AR-1 was pumped at various discharge rates to establish an optimum long-term discharge rate for the 24-hour constant-rate test. The step-drawdown test consisted of three steps: for durations of 60, 120, and 140 minutes, respectively. The discharge rates for step one and two were 2.0 and 4.0 gallons per minutes (gpm). Step three was the recovery step. An evaluation of the step-drawdown test data from a time versus drawdown plot (Appendix D) indicated that a pumping rate of 3 gpm should be used for the constant-rate test.

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Constant-Rate Test

Recovery well AR-1 was pumped for a total of 1340 minutes at a constant discharge rate of 1340 gpd. Maximum observed drawdown in the pumping well was 6.289 feet. Maximum observed drawdowns in the pumping well and observation wells are summarized in Table 5. Water-level data were collected and recorded as the pumping well recovered to greater than 90% of the total recorded drawdown in Well AR-1.

Time versus drawdown data were plotted for observation Wells A-1, A-2, A-3, A-4 and AR-2. Transmissivity (T) and Storativity (S) values were calculated from these field data plots using the Jacob Straight-line Method (Cooper & Jacob, 1946). Calculated transmissivity values from the field plots using the Jacob Method ranged from 1970 gallons per day per foot (gpd/ft) to 6600 gpd/ft. Storativity values ranged from 1.95×10^{-4} to 9.2×10^{-4} . Storativity values appear to be consistent with an aquifer that is semi-confined to confined. Jacob Method transmissivity and storativity data results are summarized in Table 5. Field Data Plots are presented in Appendix E.

To evaluate the potential effects of leakage into [redacted] GSI used Graphical Well Analysis Package (GWAP) software to analyze test data using the Theis Method (Hantush and Jacob, 1955). Data plots generated utilizing GWAP are presented in Appendix F. Transmissivity values calculated using the Theis Method for Wells A-1, A-2, A-3, A-4 and AR-2 ranged from 1765 gpd/ft to 5574 gpd/ft. Storativity values for these wells ranged from 1.87×10^{-4} to 1.1×10^{-3} . These results appear consistent with Jacob Method values. Theis Method of transmissivity and storativity results are summarized in Table 5.

Approximately 4,620 gallons of groundwater were pumped during the aquifer tests. Groundwater was disposed of by Balch Petroleum.

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Well Influence

Data collected from the observation wells during the 24-hour constant-rate aquifer test were used to construct a water-level map after 1340 minutes of pumping from recovery well AR-1 at 3.0 gpm (Plate 7). Drawdown was observed in each observation well ranging between 0.29 and 0.83 feet. The observed radius of influence appeared to be greater than 160 feet from the pumping well for the constant-rate test. The cone of depression created by pumping recovery well AR-1 did not equilibrate during the constant-rate test, indicating that pumping for a longer time duration may produce greater influence.

Well Efficiency

The well efficiency was calculated using step and constant rate drawdown data as described by Todd (1980). A graph of the Specific Capacity (S_w/Q) vs. Well Discharge (Q) is included in Appendix G. Well efficiency was calculated to be approximately 36% at a flow rate of 3 gpm. Calculations of the well efficiency are presented in Appendix G.

CURRENT QUARTER SAMPLING RESULTS

Depth to water-level measurements were obtained on May 20 and June 16, 1992 and prior to sampling on July 17, 1992 from each monitoring and recovery well. Static ground-water levels were measured from the surveyed top of the well box and recorded to the nearest ± 0.01 foot. Water-level data were referenced to Mean Sea Level (MSL) datum and used to construct potentiometric maps presented on Plates 8, 9, and 10 for each measurement date, respectively. Shallow ground-water flows north to northwest at approximate hydraulic gradients of 0.002, 0.004, and 0.003, respectively.

Each well was checked for the presence of floating product. Floating product was not observed in any well for each measurement date. Depth to groundwater and floating product measurements for May 20 and June 16, 1992 are presented in the attached EMCON Associates (EMCON) ground-water monitoring reports (Appendix H). Depth to groundwater and floating product measurements for July 17, 1992 are summarized in the attached EMCON ground-water sampling report (Appendix I). Current and historical water-level data and floating product measurements are summarized in Table 6.

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Ground-water samples were collected on July 17, 1992. Samples were analyzed for TPH-Gasoline according to EPA Method 8015 (Modified) and BTEX according to EPA Method 8020. The ground-water samples were analyzed by Sequoia. A table of current chemical analytical data is included in the EMCON report in Appendix I. Current chemical analytical data have also been added to the Historical Groundwater Quality Database presented in Table 7. Chemical isoconcentration maps for TPH-Gasoline and benzene are presented on Plates 11 and 12, respectively.

SUMMARY

The results of this investigation are summarized below:

- o Four exploratory soil borings were drilled on June 8, 1992 and completed as vapor extraction wells AV-1 through AV-3 and recovery well AR-2.
- o Lithology of the borings consists primarily of clay underlain by interbedded sand and silt to the maximum depth explored of 14.5 feet for Wells AV-1 through AV-3 and 30.5 feet for Well AR-2.
- o TPH-Gasoline was identified in soil samples from Borings AV-1, AV-2 and AV-3 from the interval of 11.5 to 12-feet below grade at concentrations ranging between 12 ppm and 1500 ppm. TPH-Gasoline was also identified in the 6.5-foot sample from Boring AV-2 at a concentration of 1.8 ppm. Benzene was detected in each soil sample analyzed at concentrations ranging between 0.037 ppm and 21 ppm.
- o Ground water-levels were initially encountered at depths between 12.0 and 15.0 feet below grade. The water-level in Well AR-2 stabilized at a depth of 13 feet below grade.
- o A vapor extraction test was performed on June 11, 1992 utilizing the newly installed vapor wells and an IC engine.
- o Based on the 50 feet radius of influence of vacuum pressure, a flow rate of 20 cfm, and an influent concentration 24,000 ppmv, the test indicates that vapor extraction is a feasible remedial option.

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- o The observed radius of influence, based on the results of the aquifer test, appears to be approximately 160 feet.
- o Based on aquifer test results it appears that a pump and treat system is a feasible option for remediating groundwater.
- o Potentiometric data collected for the months of May, June, and July indicate that groundwater flows north and northwest at calculated hydraulic gradients ranging from 0.002 to 0.004.
- o Floating product was not observed in any wells.
- o TPH-Gasoline was identified in ground-water samples from Wells A-1, AR-1, and AR-2 at concentrations ranging between 150 ppb and 44,000 ppb. Benzene was detected in Wells A-1, AR-1, and AR-2 at concentrations ranging between 6.6 ppb and 4,300 ppb. TPH-Gasoline and benzene were reported as ND for Wells A-2 through A-4.

CONCLUSIONS

The distribution of petroleum hydrocarbons in soil and ground-water for this site have been reviewed. Based on these data, petroleum hydrocarbons in soil appear to be limited to the capillary fringe above groundwater and in the area adjacent to the former UST complex. Concentration levels appear to decrease with distance from the former UST complex. Hydrocarbon contamination has been identified in groundwater in the area beneath the former and present UST complexes and the west corner of the ARCO station property.

The observed radius of influence, stabilized flow rate and petroleum hydrocarbon concentrations resulting from the vapor extraction test indicate that vapor extraction is a feasible method of remediating petroleum hydrocarbons contamination in soil beneath the site. Results of the aquifer test indicate that a groundwater extraction remediation system is feasible for treatment of the petroleum hydrocarbon plume beneath the site. The observed radius of influence and flow rate appear to be sufficient to affect hydrodynamic control of the known hydrocarbon plume.



GeoStrategies Inc.
 Environmental Consulting,
 Engineering and Geologic Services

9110 3793

9207-1 11:00

Letter of Transmittal

Date: 11/30/92

From: ROBERT MALLORY
 To: MR. DENNIS BYRNE
ACHCSA
80 SWAN WAY #200
OAKLAND, CA. 94621

Project No: 7927
 Subject: CONT. SITE ASSESSMENT - 3RD qtr. '92
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Robert C. Mallory
 (Signed)



GeoStrategies Inc.

CONFIDENTIAL

**CONTINUING SITE ASSESSMENT/QUARTERLY
MONITORING REPORT - Third Quarter 1992**

ARCO Service Station No. 2169
889 West Grand Avenue
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Page 2

SITE BACKGROUND

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In February and March 1992, the underground storage tanks at the site were removed and replaced. The former tank complex was composed of four steel tanks: one 12,000 gallon tank (unleaded), one 8,000 gallon tank (regular), and two 6,000 gallon tanks (diesel and super unleaded). The present tank complex is composed of four double wall fiberglass 10,000 gallon tanks containing unleaded gasoline and diesel products. The location of the former and present tank complexes are shown on Plate 2. Soil sample analytical results from the former tank complex confirmed results from previous soil boring samples that petroleum hydrocarbons had impacted soil in the tank complex vicinity to a depth of 12 feet below grade. Soil sample results from product line trenching revealed a TPH-Diesel concentration of 450 ppm in the vicinity of the diesel dispenser on the westernmost island. This area was overexcavated and resampled at a depth of 7 feet below ground surface. Results of the second sample identified TPH-Diesel at a concentration of 54 ppm. TPH-Gasoline and benzene were reported at levels of less than or equal to 120 ppm and 0.36 ppm, respectively, from the remaining trench samples. An Underground Storage Tank Removal and Soil Sampling Report documenting the tank removal and soil sampling analytical results was issued by ROUX Associates (ROUX) on July 14, 1992.

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Soil samples retained for chemical analyses were collected in clean stainless steel liners and sealed on both ends with aluminum foil and plastic end caps. Samples were labeled, entered onto a Chain-of-Custody form, and transported in a cooler with blue ice to Sequoia Analytical (Sequoia), a State-certified environmental laboratory located in Redwood City, California.

Recovery Well Installation

Boring AR-2 was drilled using 10-inch-diameter hollow-stem augers to a depth of 30.5 feet below existing ground surface. This boring was drilled through a 12-inch-diameter conductor casing installed to a depth of 10-feet below grade in the new tank complex. Native material was used to backfill the boring from 28.5 to 30.5 feet below grade during well construction. Recovery well AR-2 was constructed using 4-inch-diameter Schedule 40 PVC well casing and carbon steel 0.020-inch continuous wrap well screen. ~~The well screen extends from 8.5 to 28.5 feet below grade.~~ Lonestar #2/12 graded sand was placed in the annular space across the entire screened interval and extends 1.0-foot above the top of the well screen. A one-foot thick bentonite seal was placed above the sandpack and then hydrated with clean water. A neat cement seal was placed from the top of the bentonite to ~~1.0-foot~~ below ground surface. The well was completed in an underground vault box, set in the concrete slab of the new tank complex, and a waterproof locking well cap and lock was placed on the well casing.

Vapor Extraction Well Installation

Borings AV-1 through AV-3 were installed using 8-inch-diameter hollow-stem augers to a depth of 14.5 feet below grade. Bentonite was placed in the lower 0.5 feet of Borings AV-1 through AV-3 as a bottom seal. The vapor extraction wells were constructed using 2-inch-diameter Schedule 40 PVC blank well casing and 0.020-inch factory slotted well screen. ~~Well screen extends from~~ Lonestar #2/12 graded sand was placed across the entire screened interval and extends one-half-foot above the top of the well screen. A one-half-foot thick bentonite seal was placed above the sandpack and then hydrated with clean water. A neat cement seal was placed from the top of the bentonite to approximately 1.0-foot below ground surface. A waterproof underground vault box, set in concrete, was installed over the top of each well and a waterproof locking well cap and lock were placed on the well casings. Well completion details are presented with the Exploratory Boring Logs in Appendix A.

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Soil Chemical Analytical Results

Soil samples were analyzed for Total Petroleum Hydrocarbons calculated as Gasoline (TPH-Gasoline) and as Diesel (TPH-Diesel) according to EPA Method 8015 (Modified) and Benzene, Toluene, Ethylbenzene, and Xylenes (BTEX) according to EPA Method 8020. Chemical analyses were performed by Sequoia in Redwood City, California.

Soil chemical analytical data are summarized in Table 1. Six soil samples from Borings AV-1 through AV-3, collected at depths ranging between 6.5 and 12 feet below grade, were selected for chemical analysis. Soil samples from Boring AR-2 were not analyzed due to fill material being encountered from ground surface to first encountered water. TPH-Gasoline was detected in the soil sample from Boring AV-2 at a depth of 6.5, at a concentration of 1.8 parts per million (ppm). Benzene was identified in soil samples collected at a depth of 6.5 feet from Borings AV-1 through AV-3 at concentrations of 0.15 ppm, 0.31 ppm, and 0.037 ppm, respectively. TPH-Gasoline was detected in each sample collected from depths of 11.5 to 12 feet from Borings AV-1 through AV-3 at concentrations of 12 ppm, 1,500 ppm, and 110 ppm, respectively. Benzene was reported in these samples at concentrations of 0.81 ppm, 21 ppm, and 2.4 ppm, respectively. TPH-Diesel was reported as not detected (ND) in each soil sample analyzed. The Sequoia chemical analytical report and Chain-of-Custody form are presented in Appendix B.

HYDROGEOLOGIC CONDITIONS

Regional Setting

The site is located in Oakland, California at the base of the Berkeley Hills approximately 1/2-mile east of the San Francisco Bay. The site is situated on alluvial-fan deposits of the Temescal Formation comprised of interfingering lenses of clayey gravel, sandy silty clay, and sand-clay-silt mixtures (Radbruch, D.H., 1957). Local topography suggests ground-water flows to the west toward San Francisco Bay.

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Local Setting

Based on exploratory boring data from previous investigations, the local subsurface lithology appears to consist of clay, sand, silt, and minor gravel to the total depth explored of 30.5 feet below ground surface. Borings AV-1 through AV-3 sampled subsurface lithology to a depth of 14.5 feet below ground surface and Boring AR-2 encountered fill material to a depth of 15 feet and native material to the total depth explored of 30.5 feet. Clay was observed in borings AV-1 through AV-3 from ground surface to between 10.5 (AV-2) and 13.5 (AV-1) feet below grade. The clay was underlain by sand, clayey and silty sand, and silt to the total depths of the borings. Boring AR-2 encountered interbedded sand, clayey sand, and sandy silt from 15 feet to the total depth explored of 30.5 feet. Cross-sections have been prepared from site boring logs and are presented on Plates 3 and 4. Groundwater was first encountered in Borings AV-1 through AV-3 at a depth of 12-feet below grade and in Boring AR-2 at a depth 15-feet below grade. Water-levels stabilized after completion of Well AR-2 at a depth of 13 feet below grade. This rise in the water-level in AR-2 indicates semi-confined to confined aquifer conditions.

VAPOR EXTRACTION TEST FIELD ACTIVITIES

An eight hour vapor extraction test was performed on June 11, 1992, utilizing vapor extraction well AV-2 and an Internal Combustion (IC) engine to create a vacuum on the extraction well and combust extracted vapors. Vapor extraction wells AV-1 and AV-3 were used to monitor vacuum pressure changes during the test using a manometer. Vacuum pressure and flow rate from the extraction well were measured and recorded on an approximate hourly basis throughout the test. Air stream concentrations from the extraction well before and after combustion (i.e. influent and effluent vapor concentration readings) were also monitored utilizing an infrared (IR) detector and recorded. Influent and effluent air stream samples were collected near the end of the test, entered on a Chain-of-Custody form and transported to Sequoia. Air samples were analyzed for TPH-Gasoline and BTEX according to EPA Methods 8015 (Modified) and 8020, respectively.

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Vadose Zone Lithology

Based on exploratory borings drilled at the site, the unsaturated zone appears to be composed primarily of clay to a depth of approximately 8 feet and sand, silty and clayey sand, and silt to the static ground-water surface of approximately 12 to 13.5 feet below grade.

Results

Vacuum pressure, flow rate, and influent concentration data from the extraction well were recorded during the test and are presented in Table 2. Vacuum pressure in extraction well AV-2 ranged from 76.7 to 119.8-inches of water. Vacuum pressure results for the observation wells are presented in Table 3. Pressure changes recorded at the end of the test from the observation wells ranged from 0.14 to 1.4 inches of water. Vacuum pressure recorded at the end of the test have been used to construct a Vacuum Pressure Map (Plate 5). Based the Vacuum Pressure Map the estimated radius of influence is 50-feet from the extraction well. Flow rate from the extraction well ranged from 10.8 to 23.8 cubic feet per minute (cfm) and appeared to stabilize at approximately 22 cfm three hours into the test.

Influent vapor concentrations were recorded on an hourly basis during the eight hour test (Table 2). These data exceeded the maximum range of 14,000 parts per million (ppm) of the IR detector during each hour of the test. Concentrations measured by the IR detector are calibrated to Hexane and should not be considered a quantitative measure of TPH-Gasoline or BTEX.

The results of laboratory chemical analysis of the influent and effluent air samples are summarized in Table 4. TPH-Gasoline and benzene were identified in the effluent air sample at concentrations of 13 parts per million vapor (ppmv) and 1.9 ppmv, respectively. TPH-Gasoline and benzene were detected in the influent sample at concentrations of 24,000 ppmv and 1,300 ppmv, respectively. The air sample laboratory analytical report and Chain-of-Custody Form are presented in Appendix C.

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AQUIFER TEST FIELD ACTIVITIES

A 4-hour step-drawdown test and a 24-hour constant-rate test were performed utilizing recovery well AR-1 on July 15 and 16, 1992. The tests were performed to assess the feasibility of utilizing recovery well AR-1 to achieve hydrodynamic control of groundwater for extraction of petroleum hydrocarbons from the first encountered water-bearing zone. Recovery well AR-1 was installed to extract groundwater from the shallow aquifer zone beneath the site and to assess aquifer parameters for potential recovery system design.

Water-level measurements were obtained from recovery wells AR-1 and AR-2 and monitoring wells A-1 through A-4 prior to conducting the test to establish baseline data (Plate 6). Pressure transducers connected to a Hermit SE2000 data logger were installed in recovery well AR-1 and two selected observation wells (A-1 and A-4) to monitor water-level changes during the tests. Water-level changes in Wells A-2, A-3 and AR-2 were measured with an electronic interface probe at various time intervals throughout the duration of the tests.

AQUIFER TEST RESULTS

Data collected during the 4-hour step-drawdown and 24-hour constant-rate test were evaluated and used to calculate specific aquifer parameters; Transmissivity (T) and Storativity (S). Additional aquifer and well characteristics evaluated include observed radius of influence and well efficiency.

Step-Drawdown Test

Well AR-1 was pumped at various discharge rates to establish an optimum long-term discharge rate for the 24-hour constant-rate test. The step-drawdown test consisted of three steps: for durations of 60, 120, and 140 minutes, respectively. The discharge rates for step one and two were 2.0 and 4.0 gallons per minutes (gpm). Step three was the recovery step. An evaluation of the step-drawdown test data from a time versus drawdown plot (Appendix D) indicated that a pumping rate of 3 gpm should be used for the constant-rate test.

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Constant-Rate Test

Recovery well AR-1 was pumped for a total of 1340 minutes at a constant discharge rate of 50 gpm. Maximum observed drawdown in the pumping well was 5.289 feet. Maximum observed drawdowns in the pumping well and observation wells are summarized in Table 5. Water-level data were collected and recorded as the pumping well recovered to greater than 90% of the total recorded drawdown in Well AR-1.

Time versus drawdown data were plotted for observation Wells A-1, A-2, A-3, A-4 and AR-2. Transmissivity (T) and Storativity (S) values were calculated from these field data plots using the Jacob Straight-line Method (Cooper & Jacob, 1946). Calculated transmissivity values from the field plots using the Jacob Method ranged from 1970 gallons per day per foot (gpd/ft) to 6600 gpd/ft. Storativity values ranged from 1.95×10^{-4} to 9.2×10^{-4} . Storativity values appear to be consistent with an aquifer that is semi-confined to confined. Jacob Method transmissivity and storativity data results are summarized in Table 5. Field Data Plots are presented in Appendix E.

To evaluate the potential effects of leakage into ~~confined aquifer~~, GSI used Graphical Well Analysis Package (GWAP) software to analyze test data using the Theis Method (Hantush and Jacob, 1955). Data plots generated utilizing GWAP are presented in Appendix F. Transmissivity values calculated using the Theis Method for Wells A-1, A-2, A-3, A-4 and AR-2 ranged from 1265 gpd/ft to 5574 gpd/ft. Storativity values for these wells ranged from 1.87×10^{-4} to 1.1×10^{-3} . These results appear consistent with Jacob Method values. Theis Method of transmissivity and storativity results are summarized in Table 5.

Approximately 4,620 gallons of groundwater were pumped during the aquifer tests. Groundwater was disposed of by Balch Petroleum.

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Well Influence

Data collected from the observation wells during the 24-hour constant-rate aquifer test were used to construct a water-level map after 1340 minutes of pumping from recovery well AR-1 at 3.0 gpm (Plate 7). Drawdown was observed in each observation well ranging between 0.29 and 0.83 feet. The observed radius of influence appeared to be greater than 160 feet from the pumping well for the constant-rate test. The cone of depression created by pumping recovery well AR-1 did not equilibrate during the constant-rate test, indicating that pumping for a longer time duration may produce greater influence.

Well Efficiency

The well efficiency was calculated using step and constant rate drawdown data as described by Todd (1980). A graph of the Specific Capacity (S_w/Q) vs. Well Discharge (Q) is included in Appendix G. Well efficiency was calculated to be approximately 36% at a flow rate of 3 gpm. Calculations of the well efficiency are presented in Appendix G.

CURRENT QUARTER SAMPLING RESULTS

Depth to water-level measurements were obtained on May 20 and June 16, 1992 and prior to sampling on July 17, 1992 from each monitoring and recovery well. Static ground-water levels were measured from the surveyed top of the well box and recorded to the nearest ± 0.01 foot. Water-level data were referenced to Mean Sea Level (MSL) datum and used to construct potentiometric maps presented on Plates 8, 9, and 10 for each measurement date, respectively. Shallow ground-water flows north to northwest at approximate hydraulic gradients of 0.002, 0.004, and 0.003, respectively.

Each well was checked for the presence of floating product. Floating product was not observed in any well for each measurement date. Depth to groundwater and floating product measurements for May 20 and June 16, 1992 are presented in the attached EMCON Associates (EMCON) ground-water monitoring reports (Appendix H). Depth to groundwater and floating product measurements for July 17, 1992 are summarized in the attached EMCON ground-water sampling report (Appendix I). Current and historical water-level data and floating product measurements are summarized in Table 6.

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Ground-water samples were collected on July 17, 1992. Samples were analyzed for TPH-Gasoline according to EPA Method 8015 (Modified) and BTEX according to EPA Method 8020. The ground-water samples were analyzed by Sequoia. A table of current chemical analytical data is included in the EMCON report in Appendix I. Current chemical analytical data have also been added to the Historical Groundwater Quality Database presented in Table 7. Chemical isoconcentration maps for TPH-Gasoline and benzene are presented on Plates 11 and 12, respectively.

SUMMARY

The results of this investigation are summarized below:

- o Four exploratory soil borings were drilled on June 8, 1992 and completed as vapor extraction wells AV-1 through AV-3 and recovery well AR-2.
- o Lithology of the borings consists primarily of clay underlain by interbedded sand and silt to the maximum depth explored of 14.5 feet for Wells AV-1 through AV-3 and 30.5 feet for Well AR-2.
- o TPH-Gasoline was identified in soil samples from Borings AV-1, AV-2 and AV-3 from the interval of 11.5 to 12-feet below grade at concentrations ranging between 12 ppm and 1500 ppm. TPH-Gasoline was also identified in the 6.5-foot sample from Boring AV-2 at a concentration of 1.8 ppm. Benzene was detected in each soil sample analyzed at concentrations ranging between 0.037 ppm and 21 ppm.
- o Ground water-levels were initially encountered at depths between 12.0 and 15.0 feet below grade. The water-level in Well AR-2 stabilized at a depth of 13 feet below grade.
- o A vapor extraction test was performed on June 11, 1992 utilizing the newly installed vapor wells and an IC engine.
- o Based on the 50 feet radius of influence of vacuum pressure, a flow rate of 20 cfm, and an influent concentration 24,000 ppmv, the test indicates that vapor extraction is a feasible remedial option.

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- o The observed radius of influence, based on the results of the aquifer test, appears to be approximately 160 feet.
- o Based on aquifer test results it appears that a pump and treat system is a feasible option for remediating groundwater.
- o Potentiometric data collected for the months of May, June, and July indicate that groundwater flows north and northwest at calculated hydraulic gradients ranging from 0.002 to 0.004.
- o Floating product was not observed in any wells.
- o TPH-Gasoline was identified in ground-water samples from Wells A-1, AR-1, and AR-2 at concentrations ranging between 150 ppb and 44,000 ppb. Benzene was detected in Wells A-1, AR-1, and AR-2 at concentrations ranging between 6.6 ppb and 4,300 ppb. TPH-Gasoline and benzene were reported as ND for Wells A-2 through A-4.

CONCLUSIONS

The distribution of petroleum hydrocarbons in soil and ground-water for this site have been reviewed. Based on these data, petroleum hydrocarbons in soil appear to be limited to the capillary fringe above groundwater and in the area adjacent to the former UST complex. Concentration levels appear to decrease with distance from the former UST complex. Hydrocarbon contamination has been identified in groundwater in the area beneath the former and present UST complexes and the west corner of the ARCO station property.

The observed radius of influence, stabilized flow rate and petroleum hydrocarbon concentrations resulting from the vapor extraction test indicate that vapor extraction is a feasible method of remediating petroleum hydrocarbons contamination in soil beneath the site. Results of the aquifer test indicate that a groundwater extraction remediation system is feasible for treatment of the petroleum hydrocarbon plume beneath the site. The observed radius of influence and flow rate appear to be sufficient to affect hydrodynamic control of the known hydrocarbon plume.

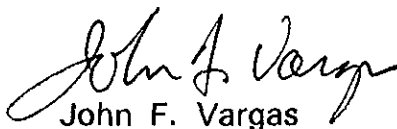
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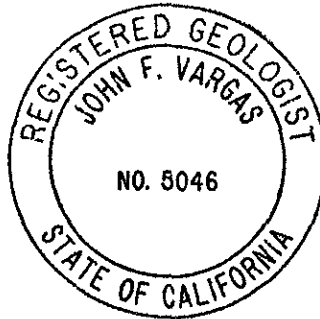
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If you have any questions, please call.

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RCM/JFV/rmt

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|----------|--|
| Table 1. | Soil Analyses Data |
| Table 2. | Vacuum Pressure Results for Well AV-2 |
| Table 3. | Vacuum Pressure Data for the Observation Wells |
| Table 4. | Air Analyses Data |
| Table 5. | Constant Rate Aquifer Test Results |
| Table 6. | Historical Water-level Data |
| Table 7. | Historical Ground-water Quality Database |

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Plate 1.	Vicinity Map
Plate 2.	Site Plan
Plate 3.	Cross-section A - A'
Plate 4.	Cross-section B - B'
Plate 5.	Vacuum Pressure Map
Plate 6.	Water Level Map Prior To Pumping Well AR-1
Plate 7.	Water Level Map After Pumping Well AR-1
Plate 8.	Potentiometric Map - May 20, 1992
Plate 9.	Potentiometric Map - June 16, 1992
Plate 10.	Potentiometric Map - July 17, 1992
Plate 11.	TPH-G Isoconcentration Map
Plate 12.	Benzene Isoconcentration Map
Appendix A:	Exploratory Boring Logs and Well Construction Details
Appendix B:	Soil Chemical Analytical Report and Chain-of-Custody Form
Appendix C:	Air Chemical Analytical Report and Chain-of-Custody Form
Appendix D:	Time vs. Drawdown
Appendix E:	Field Data Plots: Jacob Method
Appendix F:	GWAP Data Plots: Theis Method
Appendix G:	Well Efficiency Calculation
Appendix H:	EMCON Ground-water Monitoring Reports
Appendix I:	EMCON Ground-water Sampling Report

QC Review: JLP

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TABLES

TABLE 1

SOIL ANALYSES DATA

SAMPLE I.D.	SAMPLE DATE	ANALYZED DATE	TPH-G (PPM)	BENZENE (PPM)	TOLUENE (PPM)	ETHYLBENZENE (PPM)	XYLENES (PPM)	TPH-D (PPM)
AV-1-6.5	08-Jun-92	11-Jun-92	<1.0	0.15	0.019	0.014	0.062	<1.0
AV-1-12	08-Jun-92	11-Jun-92	12	0.81	1.3	0.27	1.5	<1.0
AV-2-6.5	08-Jun-92	11-Jun-92	1.8	0.31	0.15	0.036	0.21	<1.0
AV-2-11.5	08-Jun-92	11-Jun-92	1500	21	84	27	170	<1.0
AV-3-6.5	08-Jun-92	11-Jun-92	<1.0	0.037	0.0050	0.018	0.028	<1.0
AV-3-11.5	08-Jun-92	11-Jun-92	110	2.4	4.6	1.9	10	<1.0

TPH-G = Total Petroleum Hydrocarbons calculated as Gasoline

TPH-D = Total Petroleum Hydrocarbons calculated as Diesel

PPM = Parts Per Million

- Notes: 1. All data shown as <x are reported as ND (none detected).
 2. The last number of the sample I.D. corresponds to the depth the sample was collected.

TABLE 2

VACUUM PRESSURE RESULTS FOR WELL AV-2

TIME (minutes since start-up)	INFLUENT CONCENTRATION (PPM)	VACUUM PRESSURE AT WELL HEAD (inches of water)	FLOWRATE (cubic feet/min.)
0	>14,000	119.8	10.8
60	>14,000	80.1	17.1
120	>14,000	79.3	19.4
180	>14,000	79.8	22.8
240	>14,000	80.6	23.2
300	>14,000	76.7	21.6
315	>14,000	85.8	17.5
360	>14,000	85.1	21.1
420	>14,000	84.7	21.4
480	>14,000	87.6	22.4

PPM = Parts Per Million

Note: 1. Influent concentrations were measured using an infrared detector.

TABLE 3

VACUUM PRESSURE DATA FOR THE OBSERVATION WELLS

WELL NO.	TIME (minutes since start-up)	VACUUM PRESSURE (inches of water)
AV-1	18	0.20
	38	0.23
	66	0.10
	124	0.15
	184	0.10
	244	0.13
	324	0.05
	362	0.10
	423	0.16
482	0.14	
AV-3	20	0.91
	40	1.00
	68	1.10
	126	1.30
	186	1.30
	247	1.40
	326	1.22
	364	1.30
	423	1.40
484	1.40	

TABLE 4

AIR ANALYSES DATA							
SAMPLE I.D.	SAMPLE DATE	ANALYZED DATE	TPH-G (PPMV)	BENZENE (PPMV)	TOLUENE (PPMV)	ETHYLBENZENE (PPMV)	XYLENES (PPMV)
INFLUENT	11-Jun-92	12-Jun-92	24,000	1,300	1,200	85	350
EFFLUENT	11-Jun-92	12-Jun-92	13	1.9	0.29	0.10	0.51

TPH-G - Total Petroleum Hydrocarbons calculated as Gasoline
PPMV = Parts Per Million Vapor

Notes: 1. All data shown as <x are reported as ND (none detected).

TABLE 5

 =====
 CONSTANT-RATE AQUIFER TEST RESULTS
 =====

WELL NO.	PUMP RATE (GPM)	PUMPING DURATION (MINS.)	MAXIMUM DRAWDOWN (FT)	THEIS		JACOB	
				T (GPD/FT)	S	T (GPD/FT)	S
A-1	----	----	0.83	1763	5.3E-04	1970	4.7E-04
A-2	----	----	0.35	3683	1.1E-03	5110	5.1E-04
A-3	----	----	0.29	4637	1.08E-03	5142	9.2E-04
A-4	----	----	0.64	2925	1.87E-04	3330	1.95E-04
AR-1	3	1340	8.29	N/A	N/A	N/A	N/A
AR-2	----	----	0.41	5574	2.62E-04	6600	2.04E-04

T = Transmissivity

S = Specific Yield

GPD/FT = Gallons per Day per Foot

N/A = Not Applicable

TABLE 6

HISTORICAL WATER-LEVEL DATA					
MONITORING DATE	WELL NUMBER	DEPTH TO WATER (FT)	WELL ELEVATION (FT)	STATIC WATER ELEVATION (FT)	FLOATING PRODUCT THICKNESS (FT)
03-Apr-92	A-1	10.35	14.75	4.40	0.00
20-May-92	A-1	11.66	14.75	3.09	0.00
16-Jun-92	A-1	11.95	14.75	2.80	0.00
17-Jul-92	A-1	12.23	14.75	2.52	0.00
03-Apr-92	A-2	10.97	15.16	4.19	0.00
20-May-92	A-2	12.17	15.16	2.99	0.00
16-Jun-92	A-2	12.43	15.16	2.73	0.00
17-Jul-92	A-2	12.64	15.16	2.52	0.00
03-Apr-92	A-3	11.70	16.38	4.68	0.00
20-May-92	A-3	13.00	16.38	3.38	0.00
16-Jun-92	A-3	13.46	16.38	2.92	0.00
17-Jul-92	A-3	13.45	16.38	2.93	0.00
03-Apr-92	A-4	10.84	15.89	5.05	0.00
20-May-92	A-4	12.13	15.89	3.76	0.00
16-Jun-92	A-4	12.33	15.89	3.56	0.00
17-Jul-92	A-4	12.60	15.89	3.29	0.00
03-Apr-92	AR-1	11.07	15.71	4.64	0.00
20-May-92	AR-1	12.37	15.71	3.34	0.00
16-Jun-92	AR-1	12.47	15.71	3.24	0.00
17-Jul-92	AR-1	13.00	15.71	2.71	0.00
17-Jul-92	AR-2	13.14	15.79	2.65	0.00

- Notes: 1. Static water elevations referenced to Mean Sea Level (MSL).
 2. Well elevations and depths-to-water referenced to top of well box.
 3. Well AR-2 has not been referenced to MSL.

TABLE 7

HISTORICAL GROUND-WATER QUALITY DATABASE

WELL NO.	SAMPLE DATE	ANALYZED DATE	TPH-G (PPB)	BENZENE (PPB)	TOLUENE (PPB)	ETHYLBENZENE (PPB)	XYLENES (PPB)	TPH-DIESEL (PPB)
A-1	03-Apr-92	10-Apr-92	34000	6200	3900	410	3100	6100
A-1	17-Jul-92	21-Jul-92	5600	3000	500	<100	<100	N/A
A-2	03-Apr-92	10-Apr-92	<30	<0.30	<0.30	<0.30	<0.30	<50
A-2	17-Jul-92	21-Jul-92	<50	<0.50	<0.50	<0.50	<0.50	N/A
A-3	03-Apr-92	10-Apr-92	200	0.79	0.65	4.4	<0.30	130
A-3	17-Jul-92	21-Jul-92	<50	<0.50	<0.50	1.3	2.3	N/A
A-4	03-Apr-92	10-Apr-92	35	<0.30	<0.30	<0.30	<0.30	85
A-4	17-Jul-92	21-Jul-92	<50	<0.50	<0.50	<0.50	<0.50	N/A
AR-1	03-Apr-92	10-Apr-92	17000	310	1400	320	3000	12000
AR-1	17-Jul-92	21-Jul-92	44000	9100	1800	1800	10000	N/A
AR-2	17-Jul-92	21-Jul-92	150	6.6	24	6.6	39	N/A

CURRENT REGIONAL WATER QUALITY CONTROL BOARD MAXIMUM CONTAMINANT LEVELS

Benzene 1. ppb Xylenes 1750. ppb Ethylbenzene 680. ppb

CURRENT DHS ACTION LEVELS

Toluene 100.0 ppb

TPH-G = Total Petroleum Hydrocarbons calculated as Gasoline

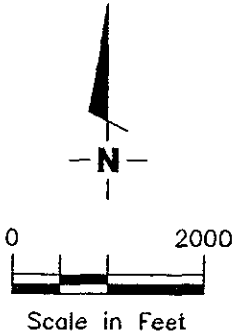
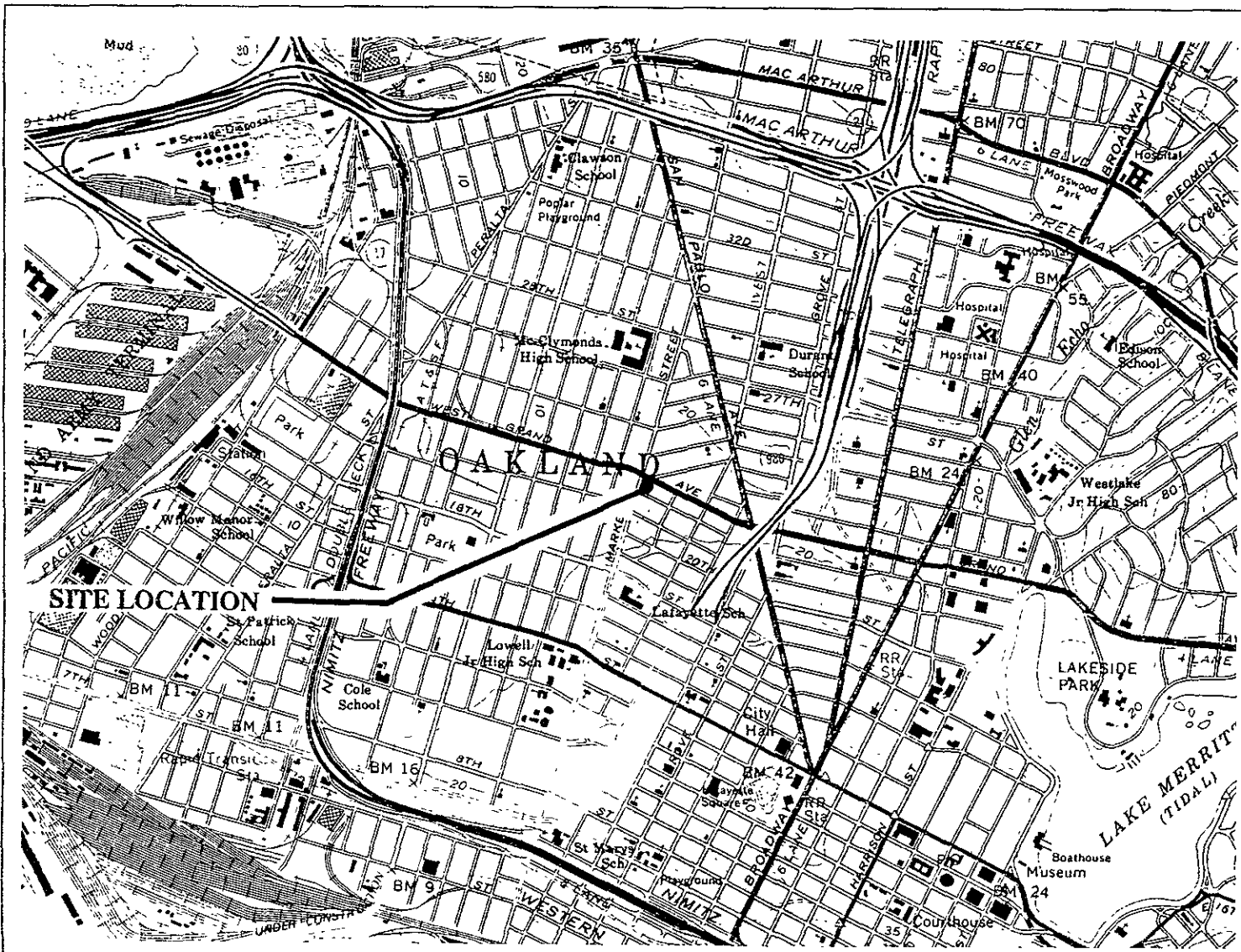
PPB = Parts Per Billion

N/A = Not Analyzed

- Notes: 1. DHS Action levels and MCL's are subject to change pending State of California review.
2. All data shown as <X are reported as ND (none detected).

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ILLUSTRATIONS



Base Map: USGS Topographic Map



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VICINITY MAP
 ARCO Service Station #2169
 889 West Grand Avenue
 Oakland, California

PLATE

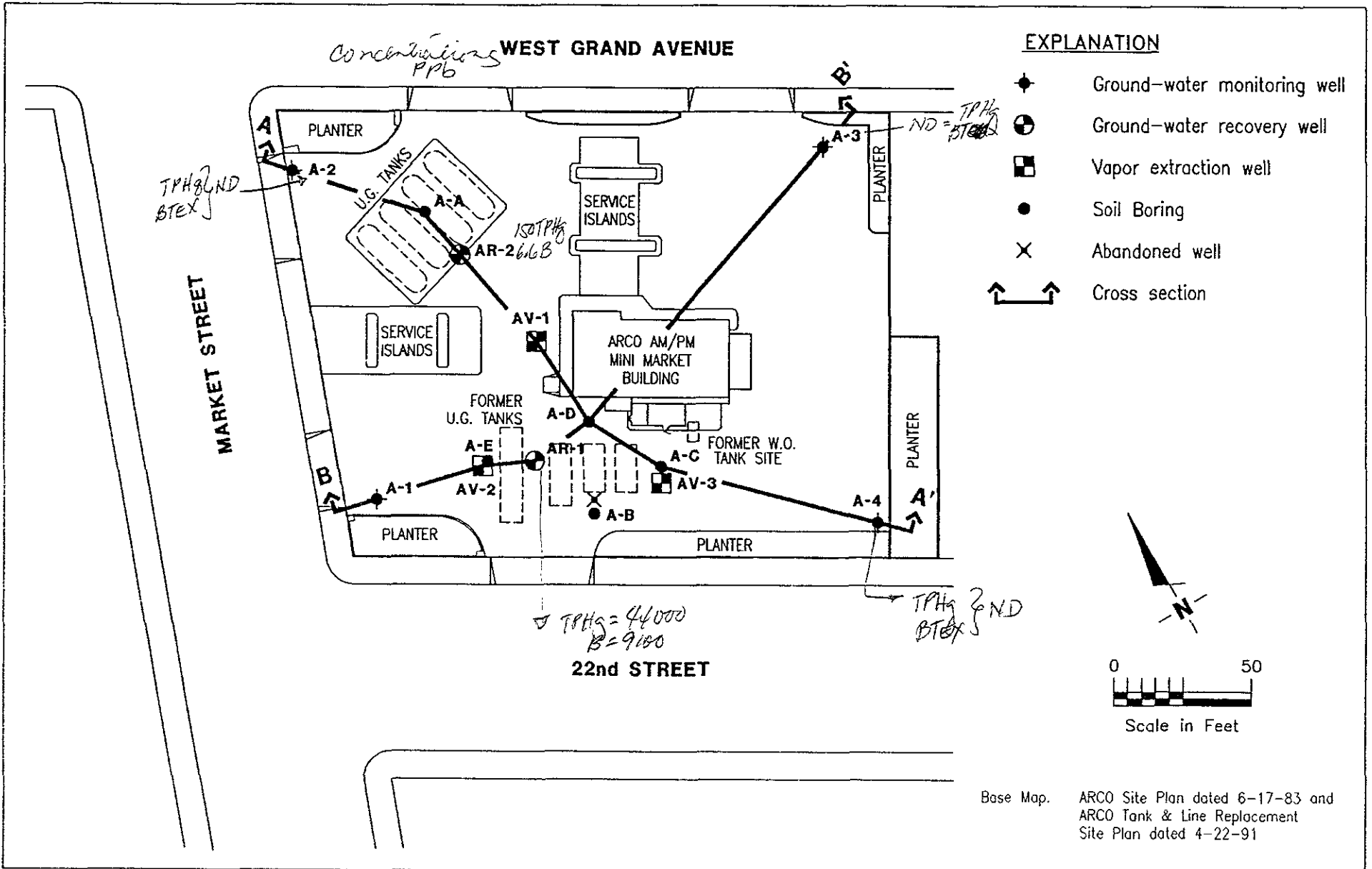
1

JOB NUMBER
 7927

REVIEWED BY

DATE
 5/91

REVISED DATE



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SITE PLAN
 ARCO Service Station #2169
 889 West Grand Avenue
 Oakland, California

PLATE

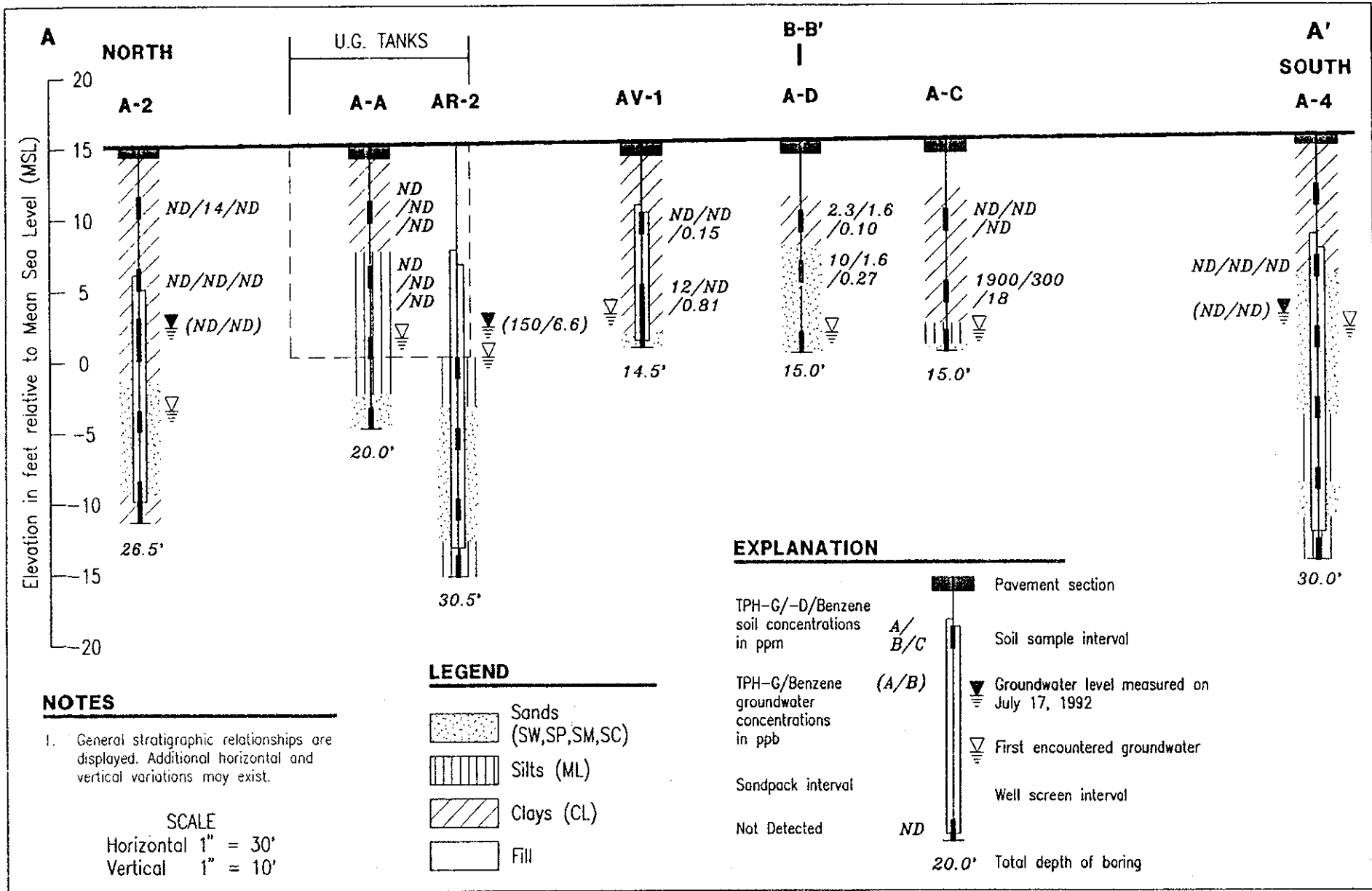
2

JOB NUMBER
792705-4

REVIEWED BY
ncm

DATE
8/92

REVISED DATE
11/92



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CROSS SECTION A-A'
 ARCO Service Station #2169
 889 West Grand Avenue
 Oakland, California

PLATE

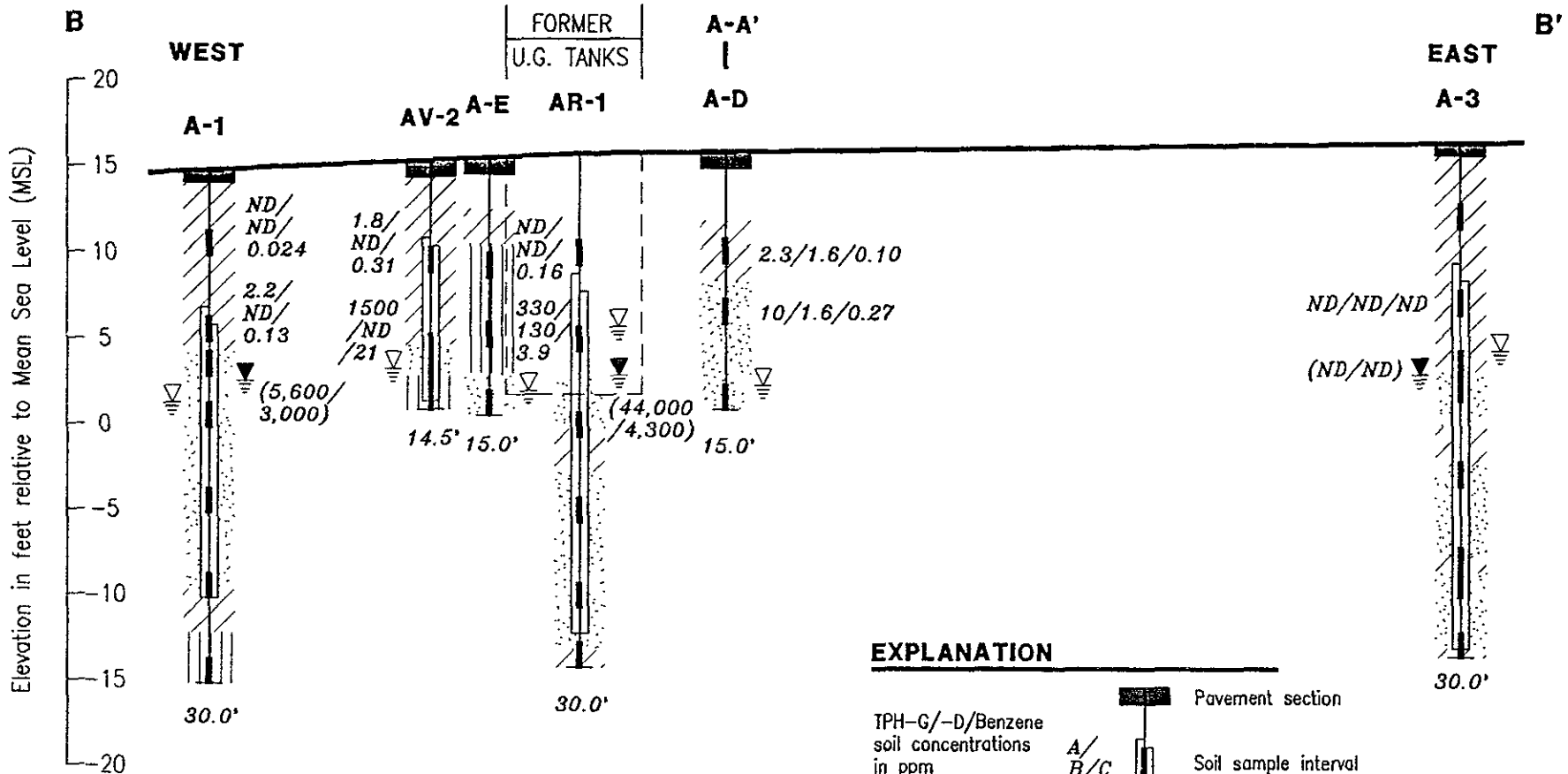
3

JOB NUMBER
 792705-4

REVIEWED BY
 REM

DATE
 8/92

REVISED DATE
 11/92



EXPLANATION

- TPH-G/-D/Benzene soil concentrations in ppm A/B/C
- TPH-G/Benzene groundwater concentrations in ppb (A/B)
- Sandpack interval
- Not Detected ND
- Pavement section
- Soil sample interval
- Groundwater level measured on July 17, 1992
- First encountered groundwater
- Well screen interval
- 20.0' Total depth of boring

LEGEND

- Sands and Gravels (SW,SP,SM,SC,GW)
- Silts (ML)
- Clays (CL)
- Fill

NOTES

1. General stratigraphic relationships are displayed. Additional horizontal and vertical variations may exist.

SCALE
 Horizontal 1" = 30'
 Vertical 1" = 10'



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CROSS SECTION B-B'
 ARCO Service Station #2169
 889 West Grand Avenue
 Oakland, California

PLATE

4

JOB NUMBER
 792705-4

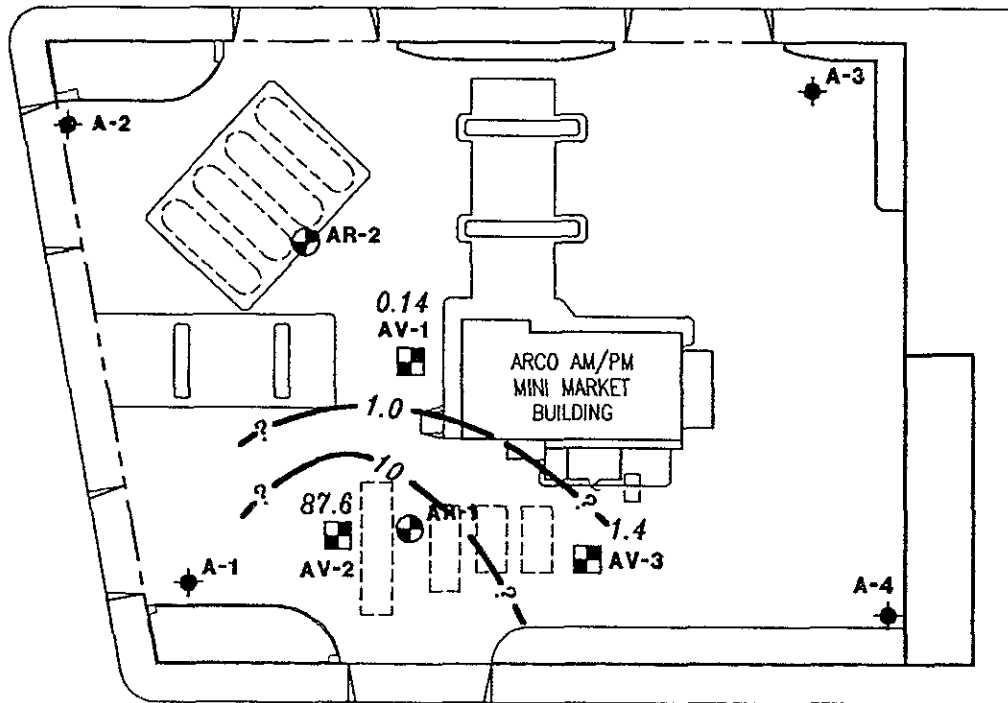
REVIEWED BY
 RCM

DATE
 8/92

REVISED DATE

WEST GRAND AVENUE

MARKET STREET

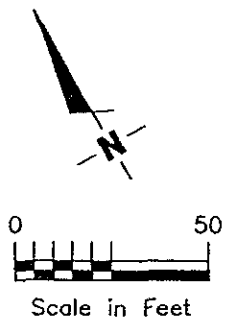


EXPLANATION

- ◆ Ground-water monitoring well
- ⊕ Ground-water recovery well
- ⊞ Vapor extraction well
- 0.1 — Vacuum pressure contour, in inches of water, relative to atmospheric pressure.
- 0.1 Vacuum pressure, in inches of water, relative to atmospheric pressure measured on June 11, 1992

22nd STREET

Base Map: ARCO Site Plan dated 6-17-83 and
ARCO Tank & Line Replacement
Site Plan dated 4-22-91



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VACUUM PRESSURE MAP
ARCO Service Station #2169
889 West Grand Avenue
Oakland, California

PLATE

5

JOB NUMBER
792705-4

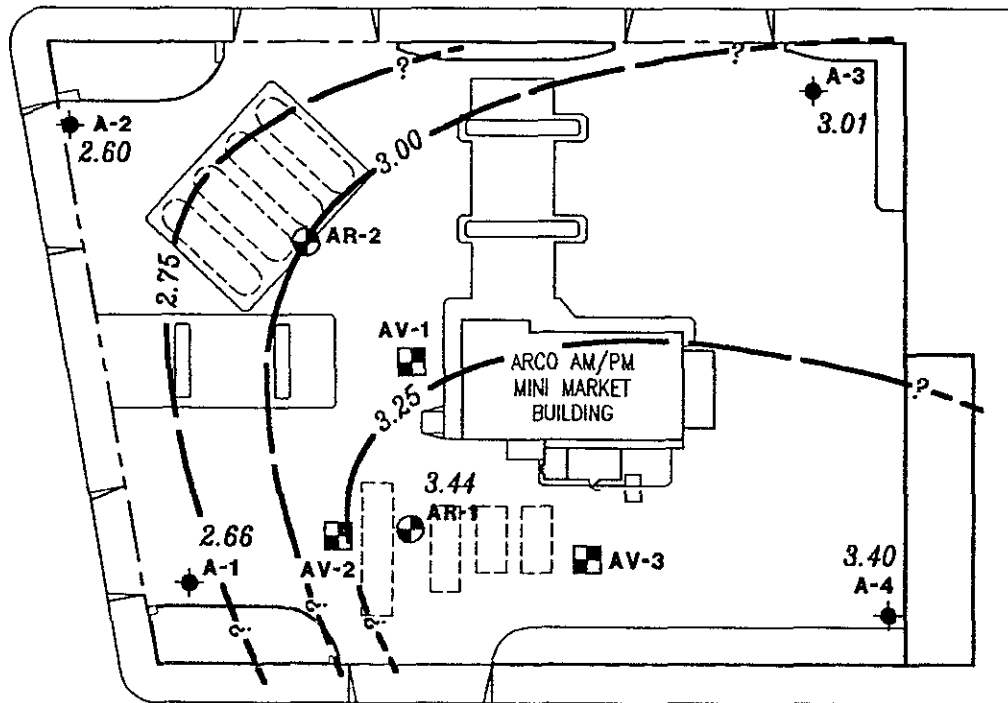
REVIEWED BY
Acem

DATE
8/92

REVISED DATE

WEST GRAND AVENUE

MARKET STREET



22nd STREET

EXPLANATION

- ◆ Ground-water monitoring well
- ⊕ Ground-water recovery well
- ⊞ Vapor extraction well
- - - 99.99 Ground-water elevation contour. Approximate Gradient = 0.004
- 99.99 Ground-water elevation in feet referenced to Mean Sea Level (MSL) measured on July 15, 1992

NOTES: 1. Contours may be influenced by irrigation practices and/or site construction activities.



Scale in Feet

Base Map: ARCO Site Plan dated 6-17-83 and
ARCO Tank & Line Replacement
Site Plan dated 4-22-91



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WATER LEVEL MAP PRIOR TO PUMPING WELL AR-1
ARCO Service Station #2169
889 West Grand Avenue
Oakland, California

PLATE

6

JOB NUMBER
792705-4

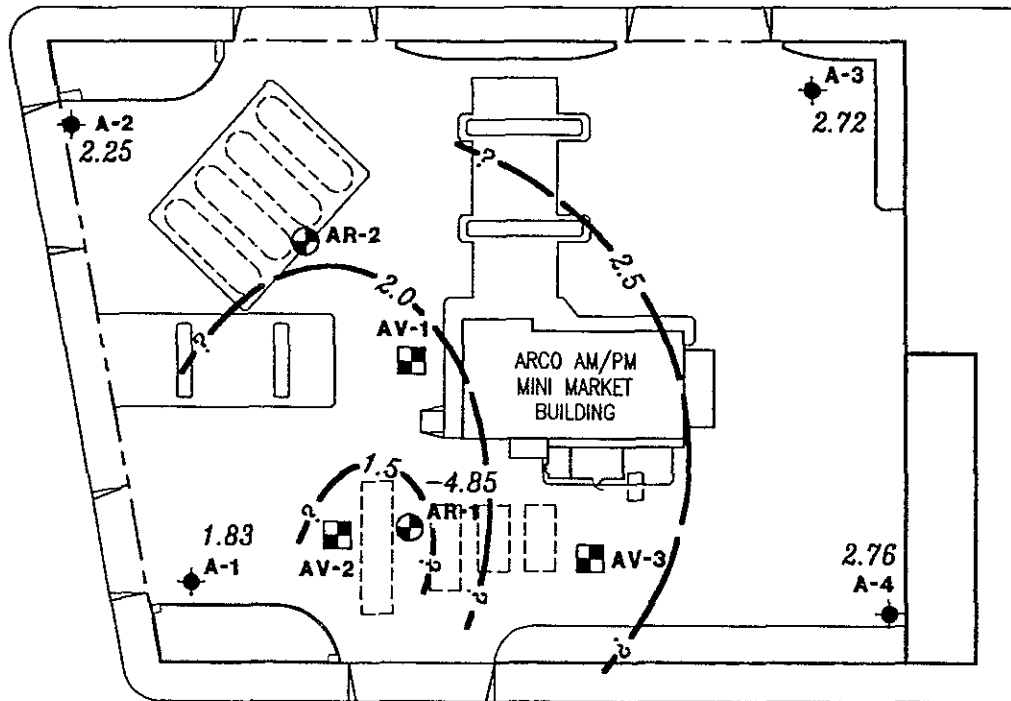
REVIEWED BY
mem

DATE
8/92

REVISED DATE

WEST GRAND AVENUE

MARKET STREET



EXPLANATION

- ◆ Ground-water monitoring well
- ⊕ Ground-water recovery well
- ⊞ Vapor extraction well
- 99.99 — Ground-water elevation contour.
- 99.99 Ground-water elevation in feet referenced to Mean Sea Level (MSL) measured on July 16, 1992

NOTES: 1. Contours may be influenced by irrigation practices and/or site construction activities.



Base Map: ARCO Site Plan dated 6-17-83 and ARCO Tank & Line Replacement Site Plan dated 4-22-91

22nd STREET



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WATER LEVEL MAP AFTER PUMPING WELL AR-1
 ARCO Service Station #2169
 889 West Grand Avenue
 Oakland, California

PLATE

7

JOB NUMBER
792705-4

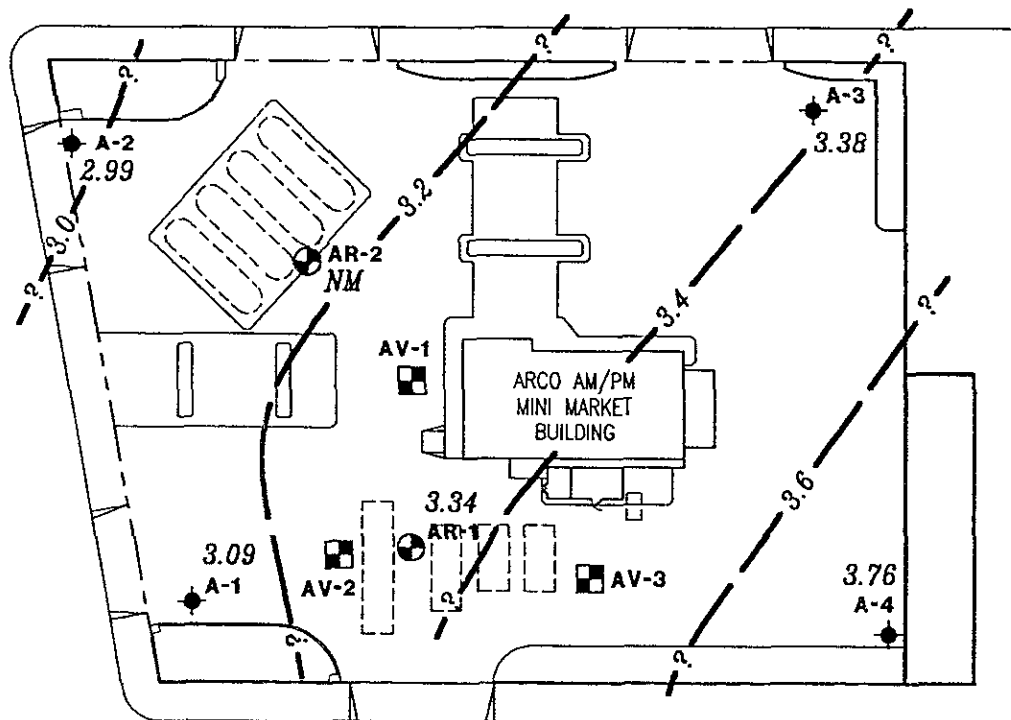
REVIEWED BY
mem

DATE
8/92

REVISED DATE

WEST GRAND AVENUE

MARKET STREET



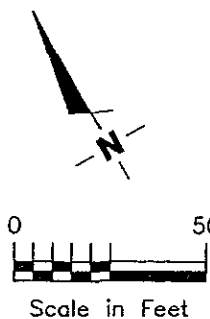
EXPLANATION

- ◆ Ground-water monitoring well
- ⊕ Ground-water recovery well
- ⊞ Vapor extraction well
- - 99.99 Ground-water elevation contour. Approximate Gradient = 0.002
- 99.99 Ground-water elevation in feet referenced to Mean Sea Level (MSL) measured on May 20, 1992
- NM Not Measured

NOTES: 1. Contours may be influenced by irrigation practices and/or site construction activities.

22nd STREET

Base Map. ARCO Site Plan dated 6-17-83 and
ARCO Tank & Line Replacement
Site Plan dated 4-22-91



GeoStrategies Inc.

POTENTIOMETRIC MAP (MAY 20, 1992)
ARCO Service Station #2169
889 West Grand Avenue
Oakland, California

PLATE

8

JOB NUMBER
792705-4

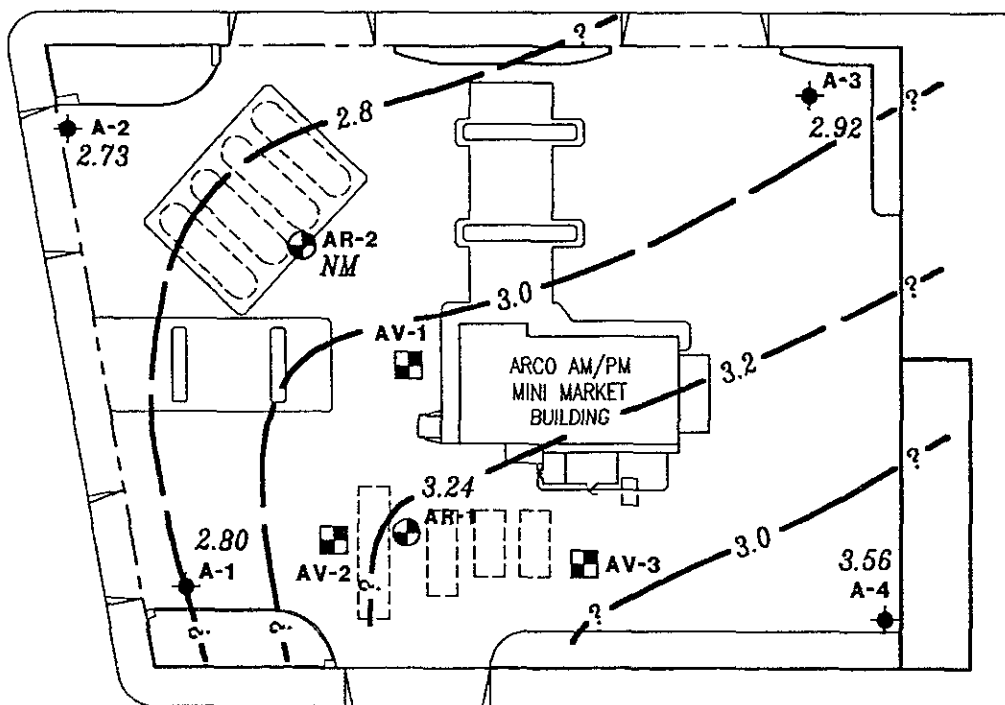
REVIEWED BY
ncm

DATE
8/92

REVISED DATE
11/92

WEST GRAND AVENUE

MARKET STREET



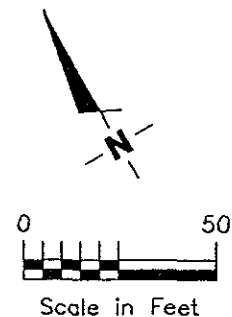
EXPLANATION

- ◆ Ground-water monitoring well
- ⊕ Ground-water recovery well
- ⊞ Vapor extraction well
- - - 99.99 Ground-water elevation contour. Approximate Gradient = 0.004
- 99.99 Ground-water elevation in feet referenced to Mean Sea Level (MSL) measured on June 16, 1992
- NM Not Measured

NOTES: 1. Contours may be influenced by irrigation practices and/or site construction activities.

22nd STREET

Base Map ARCO Site Plan dated 6-17-83 and ARCO Tank & Line Replacement Site Plan dated 4-22-91



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POTENTIOMETRIC MAP (JUNE 16, 1992)
 ARCO Service Station #2169
 889 West Grand Avenue
 Oakland, California

PLATE

9

JOB NUMBER
792705-4

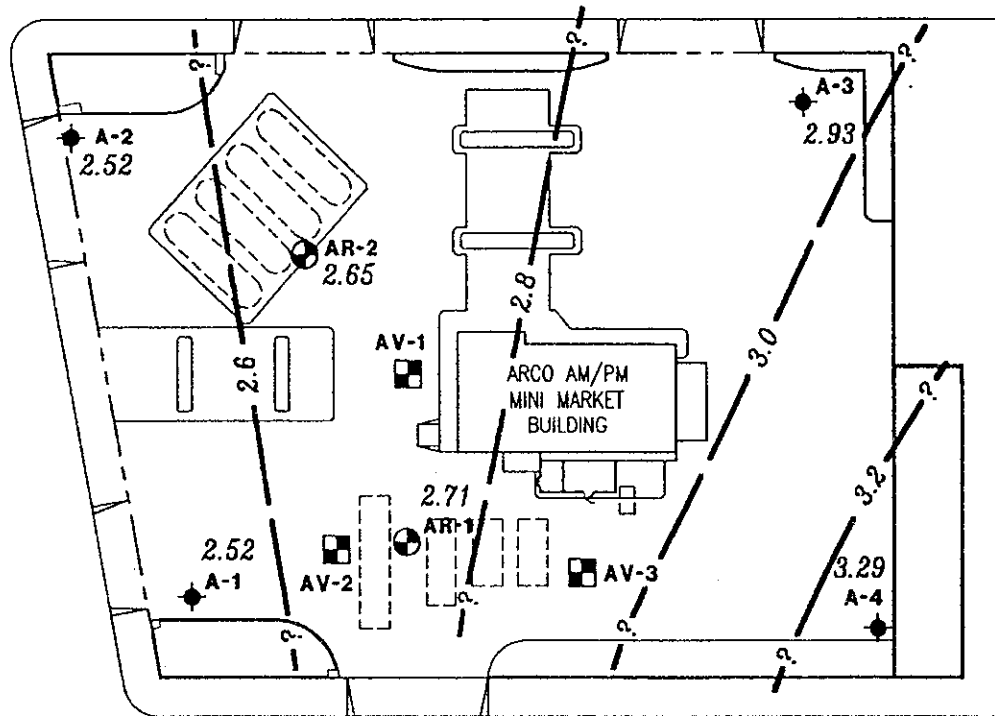
REVIEWED BY
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DATE
8/92

REVISED DATE
11/92

WEST GRAND AVENUE

MARKET STREET



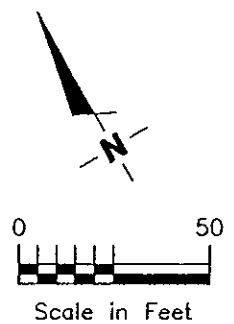
EXPLANATION

- ◆ Ground-water monitoring well
- ⊕ Ground-water recovery well
- Vapor extraction well
- - - 99.99 Ground-water elevation contour. Approximate Gradient = 0.003
- 99.99 Ground-water elevation in feet referenced to Mean Sea Level (MSL) measured on July 17, 1992

NOTES: 1. Contours may be influenced by irrigation practices and/or site construction activities.

22nd STREET

Base Map: ARCO Site Plan dated 6-17-83 and
ARCO Tank & Line Replacement
Site Plan dated 4-22-91



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POTENTIOMETRIC MAP (JULY 17, 1992)
ARCO Service Station #2169
889 West Grand Avenue
Oakland, California

PLATE

10

JOB NUMBER
792705-4

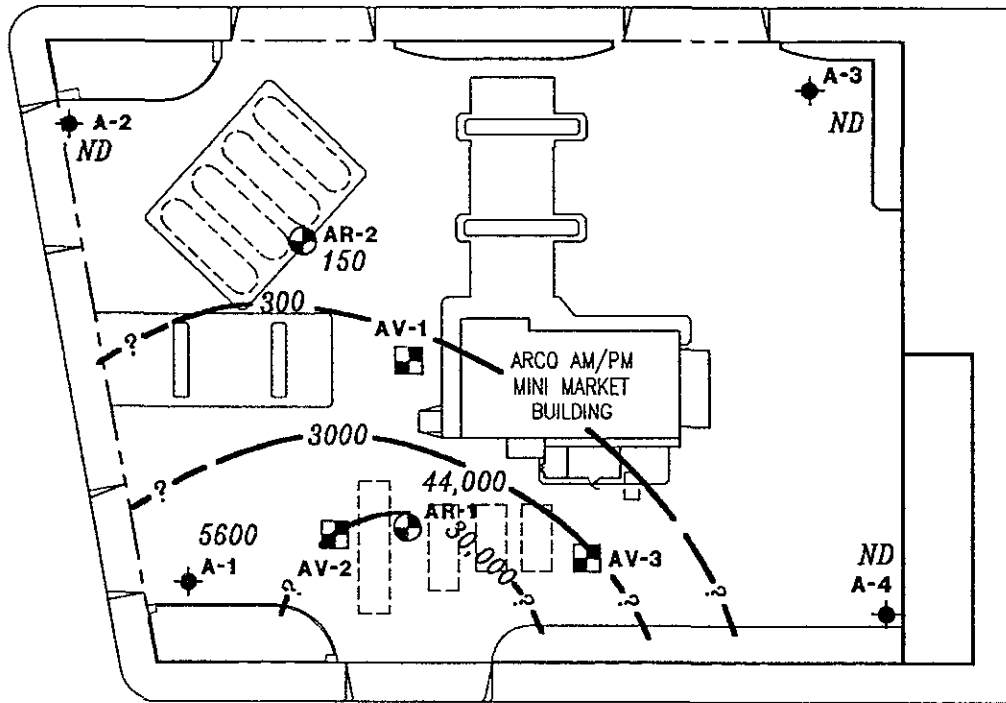
REVIEWED BY
ACM

DATE
8/92

REVISED DATE
11/92

WEST GRAND AVENUE

MARKET STREET



EXPLANATION

- ◆ Ground-water monitoring well
- ⊕ Ground-water recovery well
- ⊞ Vapor extraction well
- 5.00 --- TPH-G isoconcentration contour
- 5.0 TPH-G (Total Petroleum Hydrocarbons calculated as Gasoline) concentration in ppb sampled on July 17, 1992
- ND Not Detected (See laboratory reports for detection limits)



Base Map ARCO Site Plan dated 6-17-83 and
 ARCO Tank & Line Replacement
 Site Plan dated 4-22-91

22nd STREET



GeoStrategies Inc.

TPH-G ISOCONCENTRATION MAP
 ARCO Service Station #2169
 889 West Grand Avenue
 Oakland, California

PLATE

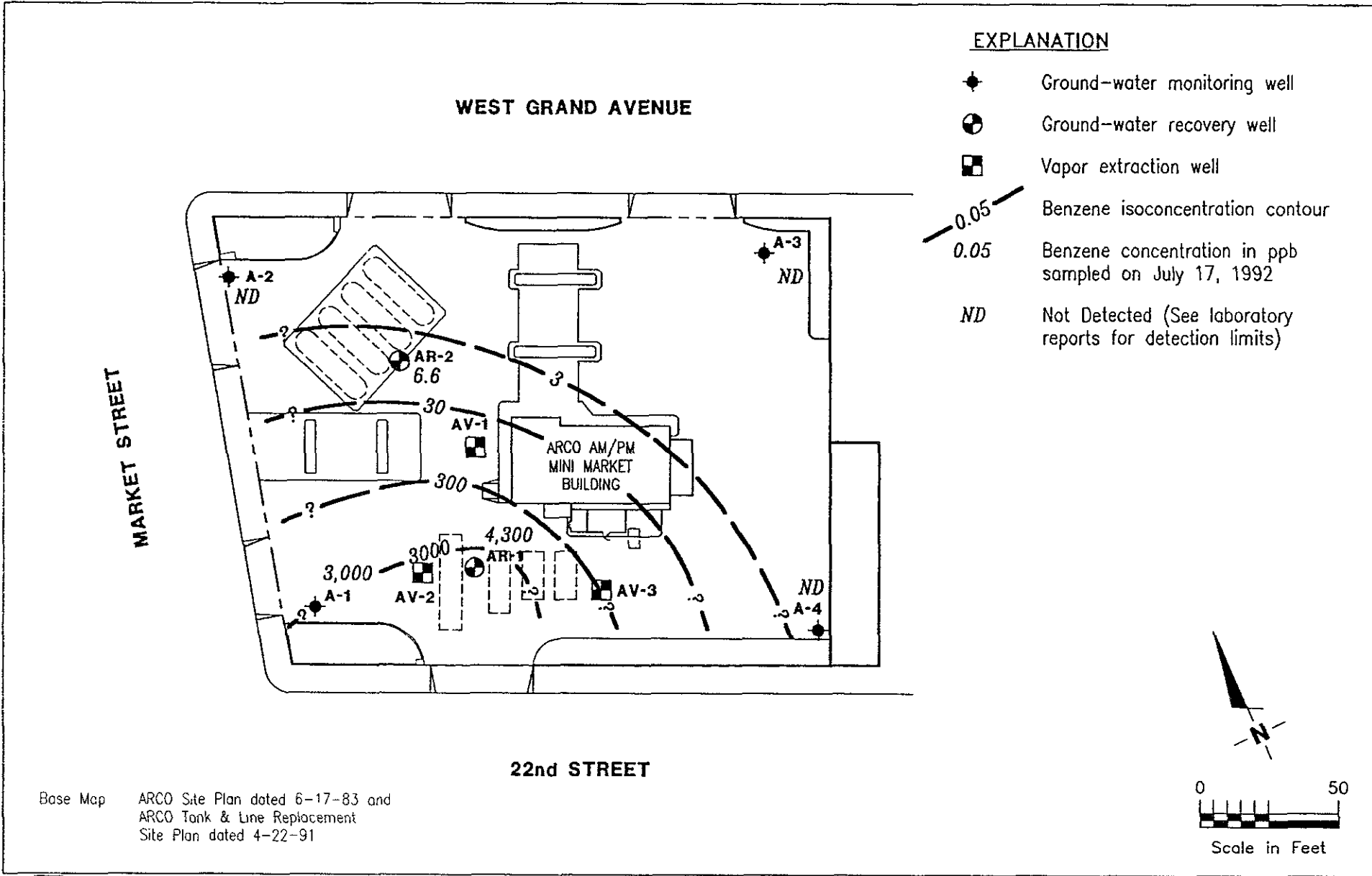
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JOB NUMBER
 792705-4

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 ACM

DATE
 8/92

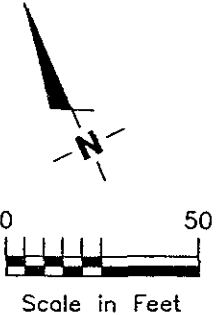
REVISED DATE
 11/92



EXPLANATION

- ◆ Ground-water monitoring well
- ⊕ Ground-water recovery well
- ⊠ Vapor extraction well
- 0.05- Benzene isoconcentration contour
- 0.05 Benzene concentration in ppb sampled on July 17, 1992
- ND Not Detected (See laboratory reports for detection limits)

Base Map ARCO Site Plan dated 6-17-83 and
 ARCO Tank & Line Replacement
 Site Plan dated 4-22-91



GeoStrategies Inc.

BENZENE ISOCONCENTRATION MAP
 ARCO Service Station #2169
 889 West Grand Avenue
 Oakland, California

PLATE

12

JOB NUMBER
 792705-4

REVIEWED BY
pcm

DATE
 8/92

REVISED DATE
 11/92

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APPENDIX A
EXPLORATORY BORING LOGS
AND
WELL CONSTRUCTION DETAILS

MAJOR DIVISIONS					TYPICAL NAMES
COARSE-GRAINED SOILS MORE THAN HALF IS COARSER THAN NO. 200 SIEVE	GRAVELS MORE THAN HALF COARSE FRACTION IS LARGER THAN NO. 4 SIEVE SIZE	CLEAN GRAVELS WITH LITTLE OR NO FINES	GW		WELL GRADED GRAVELS WITH OR WITHOUT SAND, LITTLE OR NO FINES
			GP		POORLY GRADED GRAVELS WITH OR WITHOUT SAND, LITTLE OR NO FINES
		GRAVELS WITH OVER 15% FINES	GM		SILTY GRAVELS, SILTY GRAVELS WITH SAND
			GC		CLAYEY GRAVELS, CLAYEY GRAVELS WITH SAND
	SANDS MORE THAN HALF COARSE FRACTION IS SMALLER THAN NO. 4 SIEVE SIZE	CLEAN SANDS WITH LITTLE OR NO FINES	SW		WELL GRADED SANDS WITH OR WITHOUT GRAVEL, LITTLE OR NO FINES
			SP		POORLY GRADED SANDS WITH OR WITHOUT GRAVEL, LITTLE OR NO FINES
		SANDS WITH OVER 15% FINES	SM		SILTY SANDS WITH OR WITHOUT GRAVEL
			SC		CLAYEY SANDS WITH OR WITHOUT GRAVEL
FINE-GRAINED SOILS MORE THAN HALF IS FINER THAN NO. 200 SIEVE	SILTS AND CLAYS LIQUID LIMIT 50% OR LESS	ML		INORGANIC SILTS AND VERY FINE SANDS, ROCK FLOUR, SILTS WITH SANDS AND GRAVELS	
		CL		INORGANIC CLAYS OF LOW TO MEDIUM PLASTICITY, CLAYS WITH SANDS AND GRAVELS, LEAN CLAYS	
		OL		ORGANIC SILTS OR CLAYS OF LOW PLASTICITY	
	SILTS AND CLAYS LIQUID LIMIT GREATER THAN 50%	MH		INORGANIC SILTS, MICACEOUS OR DIATOMACEOUS, FINE SANDY OR SILTY SOILS, ELASTIC SILTS	
		CH		INORGANIC CLAYS OF HIGH PLASTICITY, FAT CLAYS	
		OH		ORGANIC SILTS OR CLAYS OF MEDIUM TO HIGH PLASTICITY	
HIGHLY ORGANIC SOILS		PT		PEAT AND OTHER HIGHLY ORGANIC SOILS	

- LL - Liquid Limit (%)
- PI - Plastic Index (%)
- PID - Volatile Vapors in ppm
- MA - Particle Size Analysis
- 2.5 YR 6/2 - Soil Color according to Munsell Soil Color Charts (1975 Edition)
- 5 GY 5/2 - GSA Rock Color Chart

- No Soil Sample Recovered
- "Undisturbed" Sample
- Bulk or Classification Sample
- First Encountered Ground Water Level
- Piezometric Ground Water Level
- Penetration - Sample drive hammer weight - 140 pounds falling 30 inches. Blows required to drive sampler 1 foot are indicated on the logs



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Unified Soil Classification - ASTM D 2488-85
and Key to Test Data

Field location of boring: (See Plate 2)	Project No.: 792705	Date: 6/8/92	Boring No:
	Client: ARCO Products Company SS #2169	AR-2	
	Location: 889 W. Grand Avenue		
	City: Oakland	Sheet 1	
	Logged by: RCM	Driller: W. Hazmat	of 2

Drilling method: Hollow Stem Auger	Top of Box Elevation:	Datum:
Hole diameter: 10 - inches		

PID (ppm)	Blows/ft.* or Pressure (psf)	Type of Sample	Sample Number	Depth (ft.)	Sample	Well Detail	Soil Group Symbol (USCS)	Water Level		Time	Date	Description
								15.0'				
				1								Conductor casing to 10.5 feet.
				2								FILL - pea gravel to 15 feet.
				3								
				4								
				5								
				6								
				7								
				8								
				9								
				10								
				11								
				12								
				13								
				14								
				15								
		S&H	AR-2	16								SANDY SILT (ML) - yellowish brown (10 YR 5/4); very stiff; moist; 70% silt; 30% fine to coarse sand; trace gravel; greenish gray (5 GY 5/1) discoloration in rootholes.
0	31		16.5	17								
				18								
				19								
				20								

Remarks: * Converted to equivalent standard penetration blows/ft.

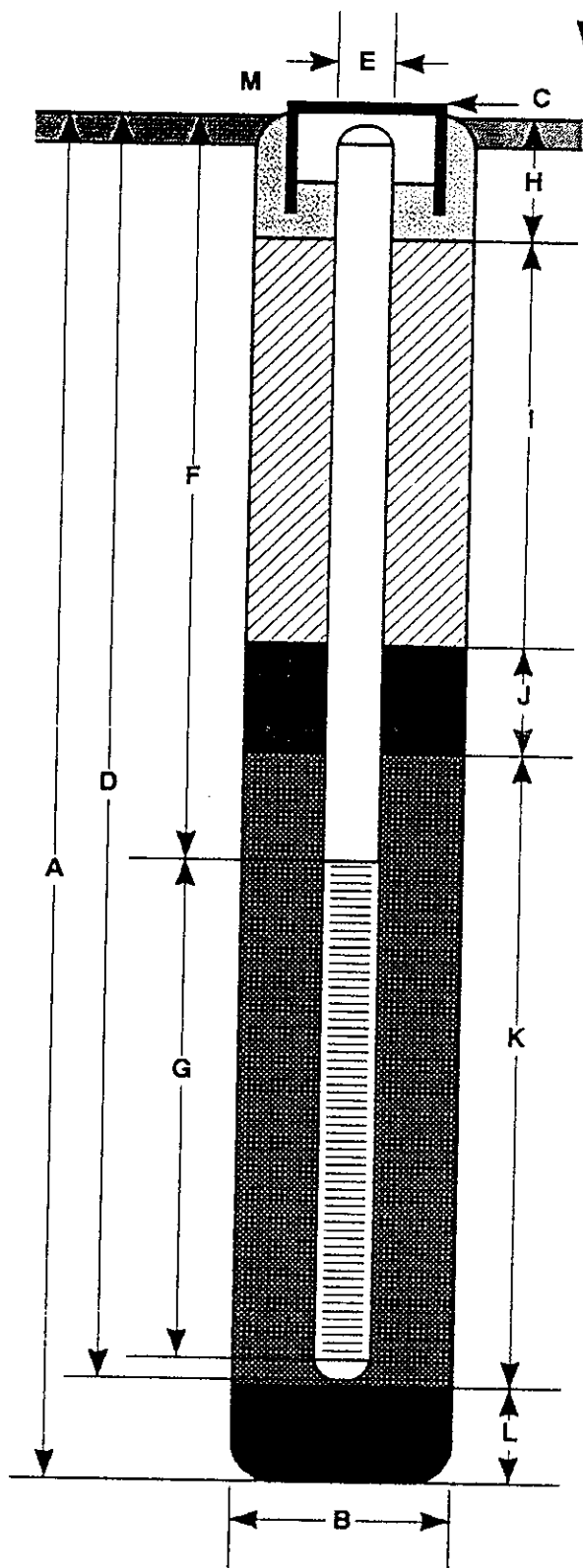
Field location of boring: (See Plate 2)	Project No.: 792705	Date: 6/8/92	Boring No:
	Client: ARCO Products Co. SS #2169	AR-2	
	Location: 889 W. Grand Avenue		
	City: Oakland, California	Sheet 2	
	Logged by: RCM	Driller: W. Hazmat	of 2

Drilling method: Hollow Stem Auger	Casing installation data:	
Hole diameter: 10 - inches	Top of Box Elevation:	Datum:

PID (ppm)	Blows/ft.* or Pressure (psi)	Type of Sample	Sample Number	Depth (ft.)	Sample	Well Detail	Soil Group Symbol (USCS)	Water Level				Description
								Time				
		S&H	AR-2	21.0			[Soil Profile Diagram]					SAND with GRAVEL (SW) - brown (10 YR 4/3); dense; saturated; 60% fine to coarse sand; 40% angular to sub-rounded, fine to medium gravel.
0	40			22								
				23								
				24								
		S&H	AR-2	26.5			[Soil Profile Diagram]					CLAYEY SAND (SC) - dark greenish gray (5 GY 4/1); dense; saturated; 80% fine to medium sand; 20% clay. SAND (SP) - dark greenish gray (5 GY 4/1); dense; saturated; 100% fine sand.
0	35			27								
				28								
				29								
		S&H	AR-2	30.0			[Soil Profile Diagram]					SILT with SAND (ML) - dark greenish gray (5 GY 4/1); hard; damp; 80% silt; 20% fine to coarse sand.
0	32			31								
				32								
				33								
				34								
				35								
				36								
				37								
				38								
				39								
				40								

Remarks:

WELL CONSTRUCTION DETAIL



- A Total Depth of Boring 30.5 ft.
- B Diameter of Boring 10 in.
Drilling Method Hollow Stem Auger
- C Top of Box Elevation _____ ft.
 Referenced to Mean Sea Level
 Referenced to Project Datum
- D Casing Length 28.5 ft.
Material Sch. 40 PVC & Carbon Steel
- E Casing Diameter 4 in.
- F Depth to Top Perforations 8.5 ft.
- G Perforated Length 20.0 ft.
Perforated Interval from 8.5 to 28.5 ft.
Perforation Type Continuous Wrap
Perforation Size 0.020 in.
- H Surface Seal from 0 to 1.0 ft.
Seal Material Concrete
- I Backfill from 1.0 to 6.5 ft.
Backfill Material Neat Cement
- J Seal from 6.5 to 7.5 ft.
Seal Material Bentonite
- K Gravel Pack from 7.5 to 28.5 ft.
Pack Material Lonestar #2/12 Graded Sand
- L Bottom Seal 2 ft.
Seal Material Native Material
- M Waterproof vault box with waterproof locking cap and lock.

Note: Depths measured from initial ground surface.



GeoStrategies Inc.

Well Construction Detail

WELL NO.

AR-2

JOB NUMBER
792705-4

REVIEWED BY PG/CEG
[Signature]

DATE
6/92

REVISED DATE

REVISED DATE

Field location of boring: (See Plate 2)

Project No.: 792705 Date: 6/8/92 Boring No: AV-1

Client: ARCO Products Co. SS #2169

Location: 889 W. Grand Avenue

City: Oakland, California

Logged by: RCM Driller: W. Hazmat Sheet 1 of 1

Casing installation data:

Drilling method: Hollow Stem Auger

Hole diameter: 8-inches

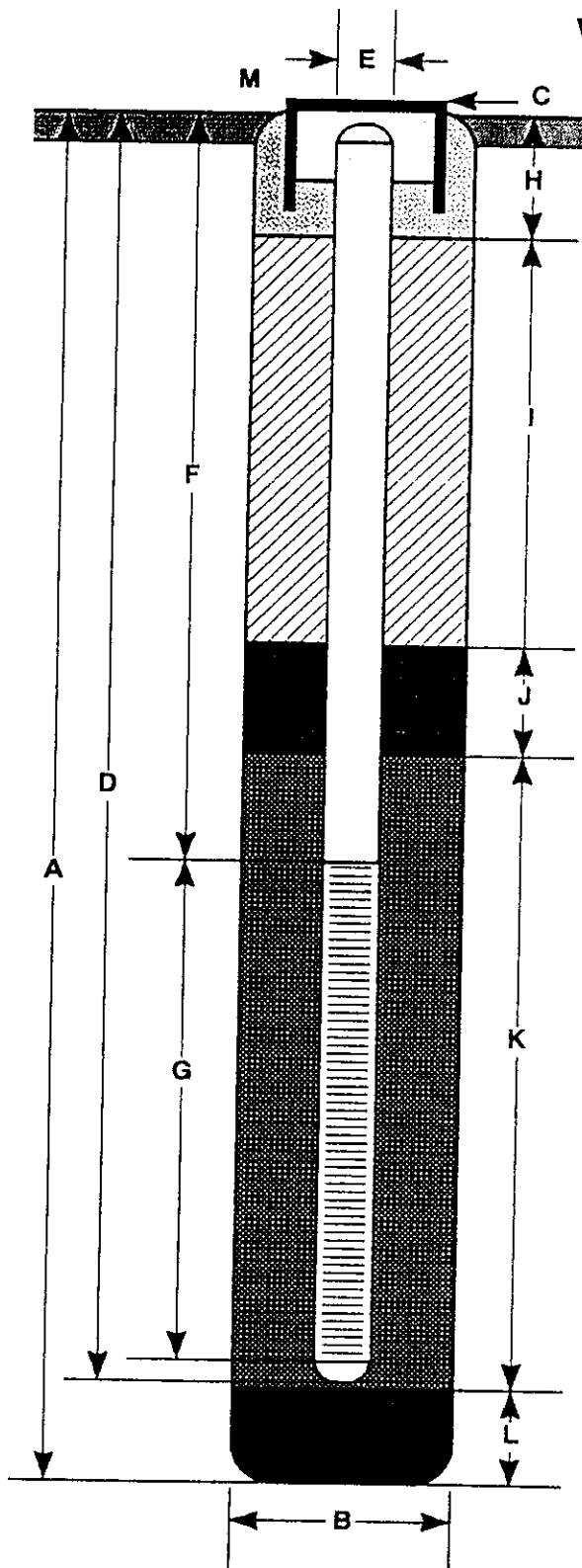
Top of Box Elevation: Datum:

PIG (ppm)	Blows/ft. or Pressure (psi)	Type of Sample	Sample Number	Depth (ft.)	Sample	Well Detail	Soil Group Symbol (USCS)	Water Level	12.0'	Time	14:35	Date	6/8/92
-----------	-----------------------------	----------------	---------------	-------------	--------	-------------	--------------------------	-------------	-------	------	-------	------	--------

								Description					
				1				PAVEMENT SECTION - 1.0 feet.					
				2				CLAY (CL) - black (10 YR 2/1); medium stiff; damp; 90 % clay; 10% fine sand.					
				3									
				4									
		S&H		5				COLOR CHANGE to dark grayish brown (2.5 Y 4/2); very stiff; iron oxide staining in rootholes at 5.0 feet.					
444	22		AV-1	6									
			6.5	7									
				8									
				9									
		S&H		10									
2146	21		AV-1	11				Minor greenish gray (5 GY 5/1) discoloration; moist at 11.5 feet.					
		S&H		12				Saturated at 12.0 feet.					
1062	22			13									
		S&H	AV-1	14									
1875	29		14.0	15				CLAYEY SAND (SC) - light yellowish brown (2.5 Y 6/4); dense; saturated, 75% fine to medium sand, 25% clay; greenish gray (5 GY 5/1) discoloration in rootholes.					
				16									
				17				Bottom of boring at 14.5 feet.					
				18				6/8/92.					
				19									
				20									

Remarks: * Converted to equivalent standard penetration blows/ft.

WELL CONSTRUCTION DETAIL



- A Total Depth of Boring 14.5 ft.
- B Diameter of Boring 8 in.
Drilling Method Hollow Stem Auger
- C Top of Box Elevation _____ ft.
 Referenced to Mean Sea Level
 Referenced to Project Datum
- D Casing Length 14 ft.
Material Schedule 40 PVC
- E Casing Diameter 2 in.
- F Depth to Top Perforations 5 ft.
- G Perforated Length 9 ft.
Perforated Interval from 5 to 14 ft.
Perforation Type Factory Slotted
Perforation Size 0.020 in.
- H Surface Seal from 0 to 1.0 ft.
Seal Material Concrete
- I Backfill from 1.0 to 4.0 ft.
Backfill Material Neat Cement
- J Seal from 4.0 to 4.5 ft.
Seal Material Bentonite
- K Gravel Pack from 4.5 to 14.0 ft.
Pack Material Lonestar #2/12 Graded Sand
- L Bottom Seal 0.5 ft.
Seal Material Bentonite
- M Waterproof vault box with waterproof locking cap and lock.

Note: Depths measured from initial ground surface.



GeoStrategies Inc.

Well Construction Detail

WELL NO.

AV-1

JOB NUMBER
792705-4

REVIEWED BY PG/CEG
[Signature]

DATE
6/92

REVISED DATE

REVISED DATE

Field location of boring:

(See Plate 2)

Project No.: 792705	Date: 6/8/92	Boring No. AV-2
Client: ARCO Products Co. SS #2169	Location: 889 W. Grand Avenue	
City: Oakland, California	Logged by: RCM	Driller: W. Hazmat
Casing installation data:		Sheet 1 of 1

Drilling method: Hollow Stem Auger

Hole diameter: 8-inches

Top of Box Elevation:	Datum:
Water Level: 12.0'	
Time: 15:40	
Date: 6/8/92	

Description

PAVEMENT SECTION - 1.0 feet.

CLAY (CL) - very dark gray (10 YR 3/1); medium stiff; damp; 90 % clay; 5% fine sand; brick fragments.

COLOR CHANGE to pale olive (5 Y 6/3); trace fine gravel at 5.0 feet.

SAND with GRAVEL (SW) - yellowish brown (10 YR 5/4); medium dense, saturated; 80% fine to medium sand; 20% fine gravel.

SANDY SILT (ML) - brown (10 YR 5/3); very stiff; saturated; 70% silt; 30% fine sand.

Bottom of boring at 14.5 feet.
6/8/92.

PID (ppm)	Blows/ft.* or Pressure (psf)	Type of Sample	Sample Number	Depth (ft.)	Sample	Well Detail	Soil Group Symbol (USCS)
				1			
				2			
				3			
				4			
		S&H		5			
114	33		AV-2 6.5	6			
				7			
				8			
				9			
		S&H		10			
896	24		AV-2 11.5	11			
		S&H		12			
702	18		AV-2 14.0	13			
		S&H		14			
655	31			15			
				16			
				17			
				18			
				19			
				20			

Remarks: * Converted to equivalent standard penetration blows/ft.



GeoStrategies Inc.

Log of Boring

BORING NO.

AV-2

JOB NUMBER
792705

REVIEWED BY RG/CEG

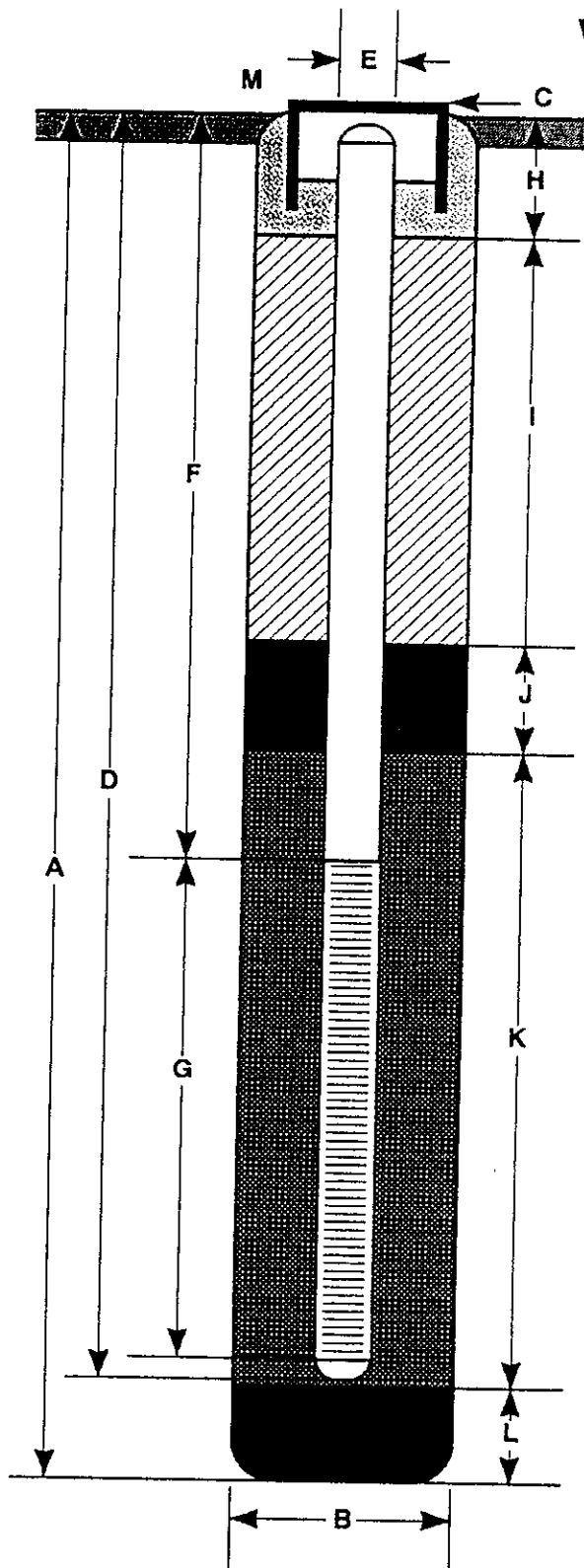
gw

DATE
6/92

REVISED DATE

REVISED DATE

WELL CONSTRUCTION DETAIL



- A Total Depth of Boring _____ 14.5 ft.
- B Diameter of Boring _____ 8 in.
Drilling Method _____ Hollow Stem Auger
- C Top of Box Elevation _____ ft.
 Referenced to Mean Sea Level
 Referenced to Project Datum
- D Casing Length _____ 14 ft.
Material _____ Schedule 40 PVC
- E Casing Diameter _____ 2 in.
- F Depth to Top Perforations _____ 5 ft.
- G Perforated Length _____ 9 ft.
Perforated Interv _____
Perforation Type _____ Factory Slotted
Perforation Size _____ 0.020 in.
- H Surface Seal from _____ 0 to _____ 1.0 ft.
Seal Material _____ Concrete
- I Backfill from _____ 1.0 to _____ 4.0 ft.
Backfill Material _____ Neat Cement
- J Seal from _____ 4.0 to _____ 4.5 ft.
Seal Material _____ Bentonite
- K Gravel Pack from _____ 4.5 to _____ 14.0 ft.
Pack Material _____ Lonestar #2/12 Graded Sand
- L Bottom Seal _____ 0.5 ft.
Seal Material _____ Bentonite
- M _____ Waterproof vault box with waterproof locking cap and lock.

Note: Depths measured from initial ground surface.



GeoStrategies Inc.

Well Construction Detail

WELL NO. _____

JOB NUMBER
792705-4

REVIEWED BY FG/CEG
FG

DATE
6/92

REVISED DATE

REVISED DATE

Field location of boring:

(See Plate 2)

Project No.: 792705	Date: 6/8/92	Boring No: AV-3
Client: ARCO Products Co. SS #2169	Location: 889 W. Grand Avenue	
City: Oakland, California		Sheet 1
Logged by: RCM	Driller: W. Hazmat	of 1

Drilling method: Hollow Stem Auger

Hole diameter: 8-inches

Top of Box Elevation: Datum:

PID (ppm)	Blows/ft.* or Pressure (psi)	Type of Sample	Sample Number	Depth (ft.)	Sample	Well Detail	Soil Group Symbol (USCS)	Water Level		Time	Date	Description
								12.0'				
				1								PAVEMENT SECTION - 1.0 feet.
				2								CLAY (CL) - very dark gray (10 YR 3/1); medium stiff; damp; 95 % clay; 5% fine sand.
				3								
				4								
		S&H		5								COLOR CHANGE to light olive brown (2.5 Y 5/4); minor white nodules at 5.0 feet.
186	12		AV-3 6.5	6								
				7								
				8								
				9								
		S&H		10								
765	18		AV-3 11.5	11								Minor greenish gray (5 GY 5/1) discoloration; moist at 11.5 feet.
		S&H		12								
435	20			13								SILTY SAND (SM) - greenish gray (5 GY 5/1); medium dense, saturated; 65% fine to coarse sand; 35% silt.
		S&H	AV-3	14								SANDY SILT (ML) - yellowish brown (10 YR 5/4); very stiff, saturated; 70% silt; 30% fine sand.
275	19		14.0	14								
				15								
				16								Bottom of boring at 14.5 feet. 6/8/92.
				17								
				18								
				19								
				20								

Remarks: * Converted to equivalent standard penetration blows/ft.



GeoStrategies Inc.

Log of Boring

BORING NO.

AV-3

JOB NUMBER
792705

REVIEWED BY RG/CEG

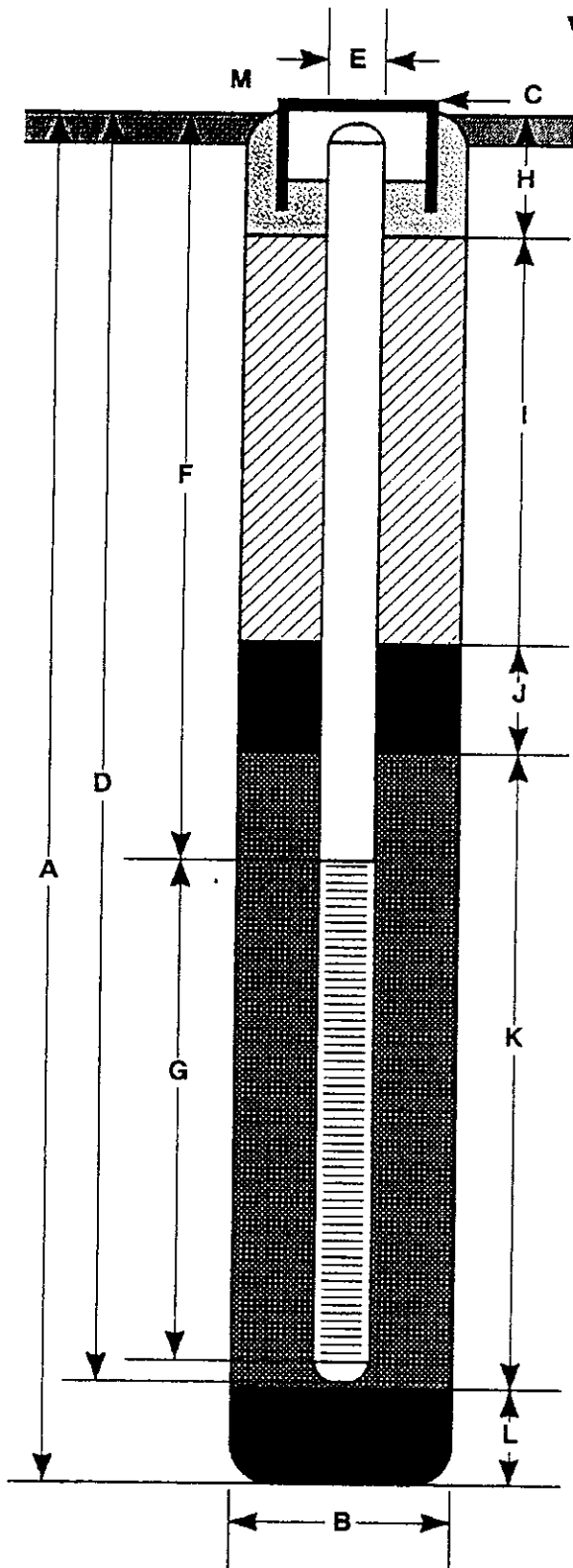
RG

DATE
6/92

REVISED DATE

REVISED DATE

WELL CONSTRUCTION DETAIL



- A Total Depth of Boring 14.5 ft.
- B Diameter of Boring 8 in.
Drilling Method Hollow Stem Auger
- C Top of Box Elevation _____ ft.
 Referenced to Mean Sea Level
 Referenced to Project Datum
- D Casing Length 14 ft.
Material Schedule 40 PVC
- E Casing Diameter 2 in.
- F Depth to Top Perforations 5.0 ft.
- G Perforated Length 9.0 ft.
Perforated Interval from 5 to 14 ft.
Perforation Type Factory Slotted
Perforation Size 0.020 in.
- H Surface Seal from 0 to 1.0 ft.
Seal Material Concrete
- I Backfill from 1.0 to 4.0 ft.
Backfill Material Neat Cement
- J Seal from 4.0 to 4.5 ft.
Seal Material Bentonite
- K Gravel Pack from 4.5 to 14.0 ft.
Pack Material Lonestar #2/12 Graded Sand
- L Bottom Seal 0.5 ft.
Seal Material Bentonite
- M Waterproof vault box with waterproof locking cap and lock.

Note: Depths measured from initial ground surface.



GeoStrategies Inc.

Well Construction Detail

WELL NO.

AV-3

JOB NUMBER
792705-4

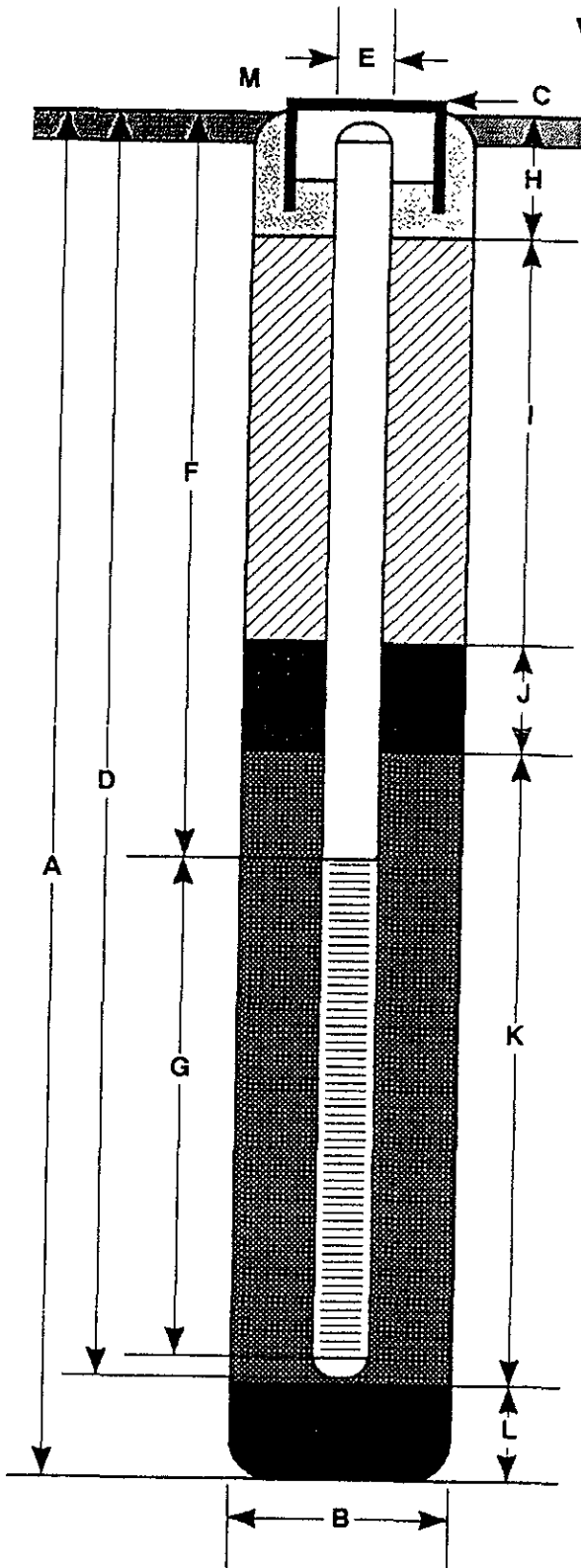
REVIEWED BY *RG/CEG*

DATE
6/92

REVISED DATE

REVISED DATE

WELL CONSTRUCTION DETAIL



- A Total Depth of Boring 30.5 ft.
- B Diameter of Boring 10 in.
Drilling Method Hollow Stem Auger
- C Top of Box Elevation _____ ft.
 Referenced to Mean Sea Level
 Referenced to Project Datum
- D Casing Length 28.5 ft.
Material Sch. 40 PVC & Carbon Steel
- E Casing Diameter 4 in.
- F Depth to Top Perforations 8.5 ft.
- G Perforated Length 20.0 ft.
Perforated Interval from 8.5 to 28.5 ft.
Perforation Type Continuous Wrap
Perforation Size 0.020 in.
- H Surface Seal from 0 to 1.0 ft.
Seal Material Concrete
- I Backfill from 1.0 to 6.5 ft.
Backfill Material Neat Cement
- J Seal from 6.5 to 7.5 ft.
Seal Material Bentonite
- K Gravel Pack from 7.5 to 28.5 ft.
Pack Material Lonestar #2/12 Graded Sand
- L Bottom Seal 2 ft.
Seal Material Native Material
- M Waterproof vault box with waterproof locking cap and lock.

Note: Depths measured from initial ground surface.



GeoStrategies Inc.

Well Construction Detail

WELL NO.

AR-2

JOB NUMBER
792705-4

REVIEWED BY RG/CEG
rg

DATE
6/92

REVISED DATE

REVISED DATE

Field location of boring:

(See Plate 2)

Project No.: 792705	Date: 6/8/92	Boring No: AV-1
Client: ARCO Products Co. SS #2169	Location: 889 W. Grand Avenue	
City: Oakland, California	Logged by: RCM	Driller: W. Hazmat
Casing installation data:		Sheet 1 of 1

Drilling method: **Hollow Stem Auger**

Hole diameter: **8-inches**

Top of Box Elevation:		Datum:	
Water Level	12.0'		
Time	14:35		
Date	6/8/92		

PIU (ppm)	Blows/ft. or Pressure (ps)	Type of Sample	Sample Number	Depth (ft.)	Sample	Well Detail	Soil Group Symbol (USCS)	Description
				1				PAVEMENT SECTION - 1.0 feet.
				2				CLAY (CL) - black (10 YR 2/1); medium stiff; damp; 90 % clay; 10% fine sand.
				3				
				4				
		S&H		5				COLOR CHANGE to dark grayish brown (2.5 Y 4/2); very stiff; iron oxide staining in rootholes at 5.0 feet.
444	22		AV-1 6.5	6				
				7				
				8				
				9				
		S&H		10				
2146	21		AV-1 11.5	11				Minor greenish gray (5 GY 5/1) discoloration; moist at 11.5 feet.
		S&H		12				Saturated at 12.0 feet.
1062	22			13				
		S&H	AV-1	14				
1875	29		14.0	14				CLAYEY SAND (SC) - light yellowish brown (2.5 Y 6/4); dense; saturated, 75% fine to medium sand, 25% clay; greenish gray (5 GY 5/1) discoloration in rootholes.
				15				
				16				
				17				Bottom of boring at 14.5 feet. 6/8/92.
				18				
				19				
				20				

Remarks: * Converted to equivalent standard penetration blows/ft.



GeoStrategies Inc.

Log of Boring

BORING NO.

AV-1

JOB NUMBER
792705

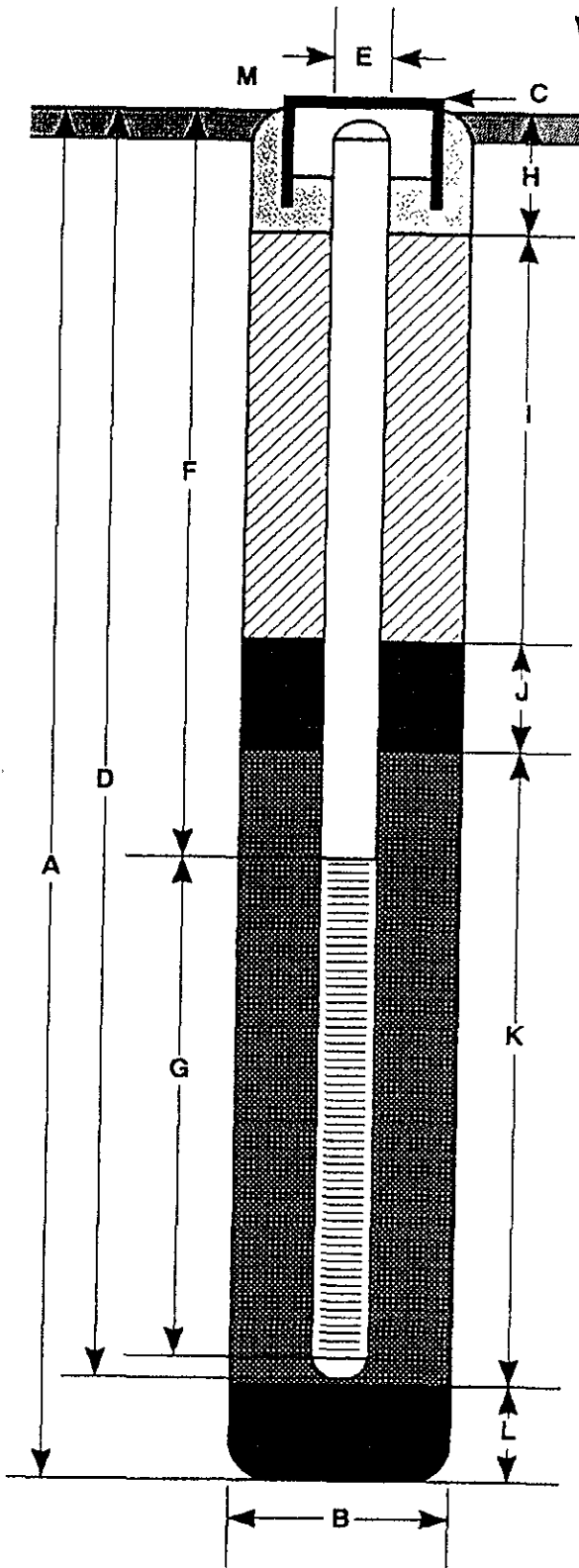
REVIEWED BY RG/CEG

DATE
6/92

REVISED DATE

REVISED DATE

WELL CONSTRUCTION DETAIL



- A Total Depth of Boring _____ 14.5 ft.
- B Diameter of Boring _____ 8 in.
Drilling Method _____ Hollow Stem Auger
- C Top of Box Elevation _____ ft.
 Referenced to Mean Sea Level
 Referenced to Project Datum
- D Casing Length _____ 14 ft.
Material _____ Schedule 40 PVC
- E Casing Diameter _____ 2 in.
- F Depth to Top Perforations _____ 5 ft.
- G Perforated Length _____ 9 ft.
Perforated Interval from _____ 5 to _____ 14 ft.
Perforation Type _____ Factory Slotted
Perforation Size _____ 0.020 in.
- H Surface Seal from _____ 0 to _____ 1.0 ft.
Seal Material _____ Concrete
- I Backfill from _____ 1.0 to _____ 4.0 ft.
Backfill Material _____ Neat Cement
- J Seal from _____ 4.0 to _____ 4.5 ft.
Seal Material _____ Bentonite
- K Gravel Pack from _____ 4.5 to _____ 14.0 ft.
Pack Material _____ Lonestar #2/12 Graded Sand
- L Bottom Seal _____ 0.5 ft.
Seal Material _____ Bentonite
- M _____ Waterproof vault box with waterproof locking cap and lock.

Note: Depths measured from initial ground surface.



GeoStrategies Inc.

Well Construction Detail

WELL NO.

AV-1

JOB NUMBER
792705-4

REVIEWED BY RG/CEG

DATE
6/92

REVISED DATE

REVISED DATE

Field location of boring:

(See Plate 2)

Project No.: 792705	Date: 6/8/92	Boring No. AV-2
Client: ARCO Products Co. SS #2169	Location: 889 W. Grand Avenue	
City: Oakland, California	Logged by: RCM	Driller: W. Hazmat
Casing installation data:		Sheet 1 of 1

Drilling method: Hollow Stem Auger

Hole diameter: 8-inches

Top of Box Elevation:		Datum:	
Water Level	12.0'		
Time	15:40		
Date	6/8/92		

PID (ppm)	Blows/ft * or Pressure (psf)	Type of Sample	Sample Number	Depth (ft.)	Sample	Well Detail	Soil Group Symbol (USCS)	Description
				1				PAVEMENT SECTION - 1.0 feet.
				2				CLAY (CL) - very dark gray (10 YR 3/1); medium stiff; damp; 90 % clay; 5% fine sand; brick fragments.
				3				
				4				
		S&H		5				COLOR CHANGE to pale olive (5 Y 6/3); trace fine gravel at 5.0 feet.
114	33		AV-2 6.5	6				
				7				
				8				
				9				
		S&H		10				
896	24		AV-2 11.5	11				
		S&H		12				SAND with GRAVEL (SW) - yellowish brown (10 YR 5/4); medium dense, saturated; 80% fine to medium sand; 20% fine gravel.
702	18			13				SANDY SILT (ML) - brown (10 YR 5/3); very stiff; saturated; 70% silt; 30% fine sand.
		S&H	AV-2 14.0	14				
655	31			15				
				16				Bottom of boring at 14.5 feet. 6/8/92.
				17				
				18				
				19				
				20				

Remarks: * Converted to equivalent standard penetration blows/ft.



GeoStrategies Inc.

Log of Boring

BORING NO.

AV-2

JOB NUMBER
792705

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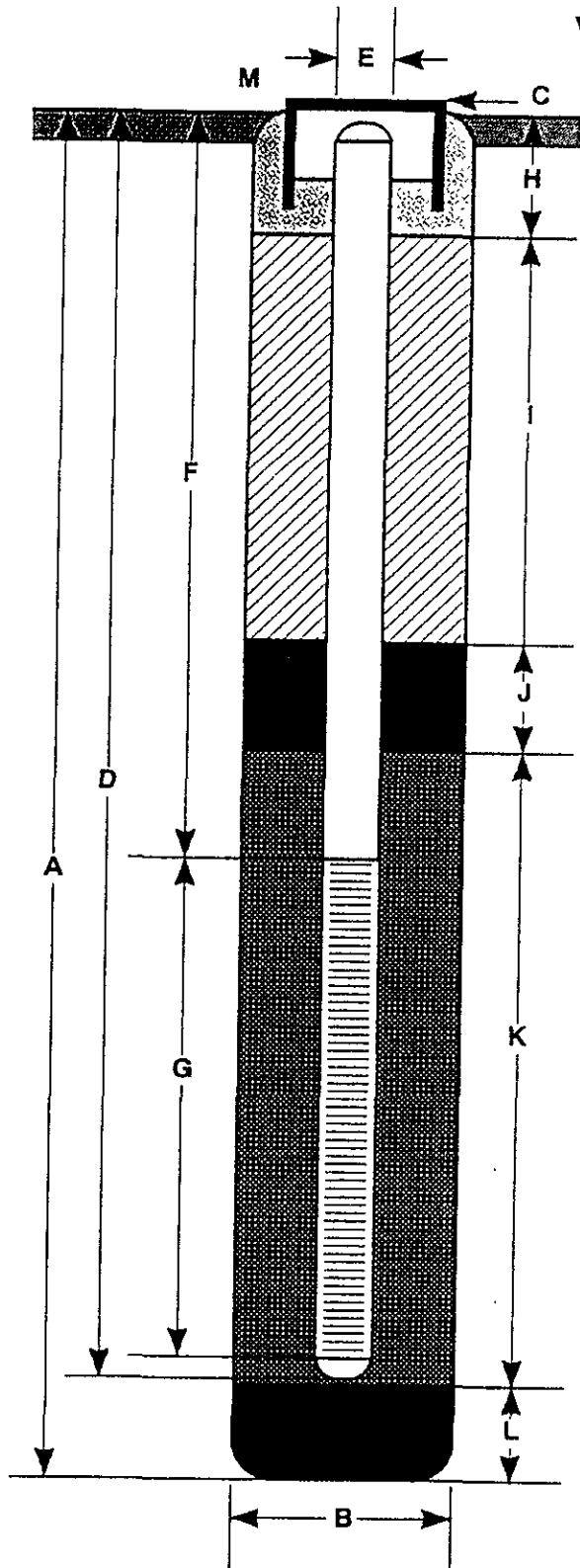
rg

DATE
6/92

REVISED DATE

REVISED DATE

WELL CONSTRUCTION DETAIL



- A Total Depth of Boring 14.5 ft.
- B Diameter of Boring 8 in.
Drilling Method Hollow Stem Auger
- C Top of Box Elevation _____ ft.
 Referenced to Mean Sea Level
 Referenced to Project Datum
- D Casing Length 14 ft.
Material Schedule 40 PVC
- E Casing Diameter 2 in.
- F Depth to Top Perforations 5 ft.
- G Perforated Length 9 ft.
Perforated Interval [REDACTED]
Perforation Type Factory Slotted
Perforation Size 0.020 in.
- H Surface Seal from 0 to 1.0 ft.
Seal Material Concrete
- I Backfill from 1.0 to 4.0 ft.
Backfill Material Neat Cement
- J Seal from 4.0 to 4.5 ft.
Seal Material Bentonite
- K Gravel Pack from 4.5 to 14.0 ft.
Pack Material Lonestar #2/12 Graded Sand
- L Bottom Seal 0.5 ft.
Seal Material Bentonite
- M Waterproof vault box with waterproof locking cap and lock.

Note: Depths measured from initial ground surface.



GeoStrategies Inc.

Well Construction Detail

WELL NO. [REDACTED]

JOB NUMBER
792705-4

REVIEWED BY RG/CEG

DATE
6/92

REVISED DATE

REVISED DATE

Field location of boring: (See Plate 2)	Project No.: 792705	Date: 6/8/92	Boring No: AV-3
	Client: ARCO Products Co. SS #2169		
	Location: 889 W. Grand Avenue		Sheet 1
	City: Oakland, California		of 1
	Logged by: RCM	Driller: W. Hazmat	

Drilling method: Hollow Stem Auger
 Hole diameter: 8-inches
 Casing installation data:

Top of Box Elevation:	Datum:
Water Level: 12.0'	
Time: 14:30	
Date: 6/8/92	

PID (ppm)	Blows/ft. or Pressure (psi)	Type of Sample	Sample Number	Depth (ft.)	Sample	Well Detail	Soil Group Symbol (USCS)	Description
				1				PAVEMENT SECTION - 1.0 feet.
				2				CLAY (CL) - very dark gray (10 YR 3/1); medium stiff; damp; 95 % clay; 5% fine sand.
				3				
				4				
		S&H		5				COLOR CHANGE to light olive brown (2.5 Y 5/4); minor white nodules at 5.0 feet.
186	12		AV-3 6.5	6				
				7				
				8				
				9				
		S&H		10				
765	18		AV-3 11.5	11				Minor greenish gray (5 GY 5/1) discoloration; moist at 11.5 feet.
		S&H		12				
435	20			13				SILTY SAND (SM) - greenish gray (5 GY 5/1); medium dense, saturated; 65% fine to coarse sand; 35% silt.
		S&H	AV-3 14.0	14				SANDY SILT (ML) - yellowish brown (10 YR 5/4); very stiff; saturated; 70% silt; 30% fine sand.
275	19			15				
				16				Bottom of boring at 14.5 feet. 6/8/92.
				17				
				18				
				19				
				20				

Remarks: * Converted to equivalent standard penetration blows/ft.



GeoStrategies Inc.

Log of Boring

BORING NO.

AV-3

JOB NUMBER
792705

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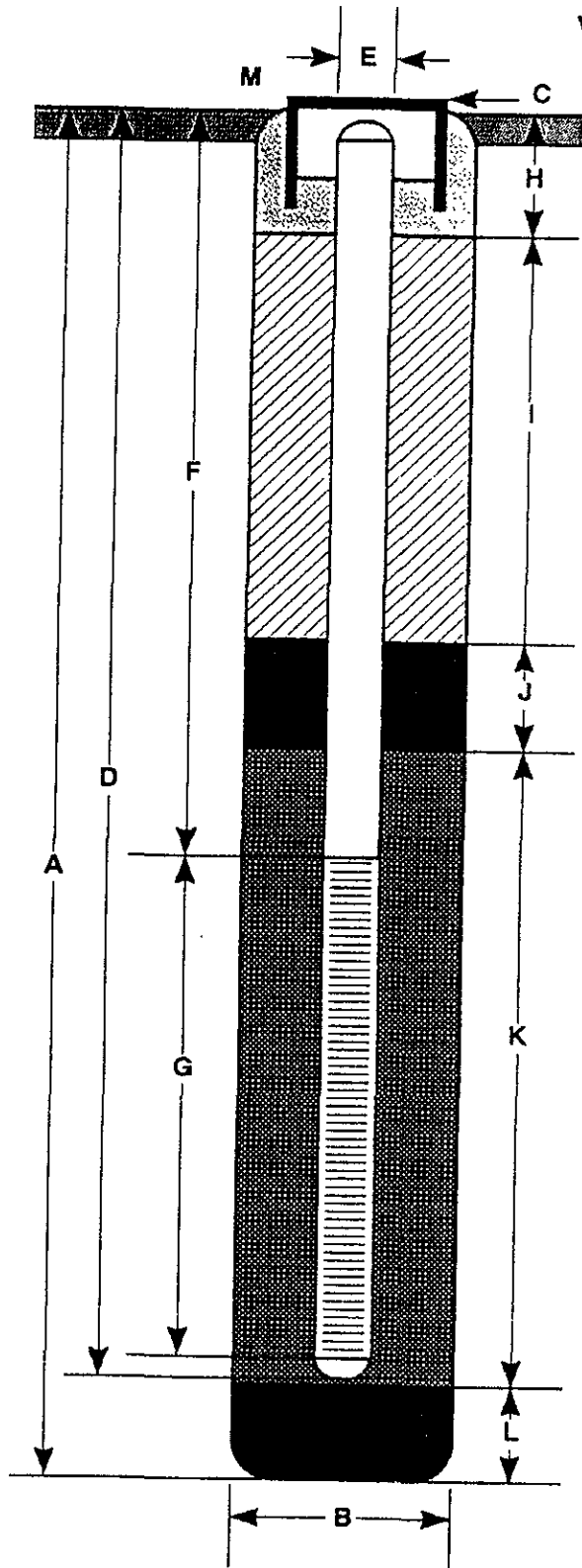
RG

DATE
6/92

REVISED DATE

REVISED DATE

WELL CONSTRUCTION DETAIL



- A Total Depth of Boring _____ 14.5 ft.
- B Diameter of Boring _____ 8 in.
Drilling Method _____ Hollow Stem Auger
- C Top of Box Elevation _____ ft.
 Referenced to Mean Sea Level
 Referenced to Project Datum
- D Casing Length _____ 14 ft.
Material _____ Schedule 40 PVC
- E Casing Diameter _____ 2 in.
- F Depth to Top Perforations _____ 5.0 ft.
- G Perforated Length _____ 9.0 ft.
Perforated Interval from _____ 5 to _____ 14 ft.
Perforation Type _____ Factory Slotted
Perforation Size _____ 0.020 in.
- H Surface Seal from _____ 0 to _____ 1.0 ft.
Seal Material _____ Concrete
- I Backfill from _____ 1.0 to _____ 4.0 ft.
Backfill Material _____ Neat Cement
- J Seal from _____ 4.0 to _____ 4.5 ft.
Seal Material _____ Bentonite
- K Gravel Pack from _____ 4.5 to _____ 14.0 ft.
Pack Material _____ Lonestar #2/12 Graded Sand
- L Bottom Seal _____ 0.5 ft.
Seal Material _____ Bentonite
- M _____ Waterproof vault box with waterproof locking cap and lock.

Note: Depths measured from initial ground surface.



GeoStrategies Inc.

Well Construction Detail

WELL NO.

AV-3

JOB NUMBER
792705-4

REVIEWED BY PG/CEG
gmv

DATE
6/92

REVISED DATE

REVISED DATE

GeoStrategies Inc.

APPENDIX B
SOIL CHEMICAL ANALYTICAL REPORT
AND
CHAIN-OF-CUSTODY FORM



SEQUOIA ANALYTICAL

680 Chesapeake Drive • Redwood City, CA 94063
(415) 364-9600 • FAX (415) 364-9233

RECEIVED
RECEIVED

APR 11 1992

Gettler Ryan
2150 W. Winton Avenue
Hayward, CA 94545
Attention: John Vargas

GETTLER-RYAN, INC.
GENERAL CONTRACTORS

Project: Arco 2169, Oakland

Enclosed are the results from 6 soil samples received at Sequoia Analytical on April 9, 1992. The requested analyses are listed below:

SAMPLE #	SAMPLE DESCRIPTION	DATE OF COLLECTION	TEST METHOD
2061686	Soil, AV-1-6.5	6/8/92	EPA 3550/8015 EPA 5030/8015/8020
2061687	Soil, AV-1-11.5	6/8/92	EPA 3550/8015 EPA 5030/8015/8020
2061688	Soil, AV-2-6.5	6/8/92	EPA 3550/8015 EPA 5030/8015/8020
2061689	Soil, AV-2-11.5	6/8/92	EPA 3550/8015 EPA 5030/8015/8020
2061690	Soil, AV-3-6.5	6/8/92	EPA 3550/8015 EPA 5030/8015/8020
2061691	Soil, AV-3-11.5	6/8/92	EPA 3550/8015 EPA 5030/8015/8020

Please contact me if you have any questions. In the meantime, thank you for the opportunity to work with you on this project.

Very truly yours,

SEQUOIA ANALYTICAL

Nokowhat D. Herrera
Project Manager



SEQUOIA ANALYTICAL

680 Chesapeake Drive • Redwood City, CA 94063
(415) 364-9600 • FAX (415) 364-9233

Gettler Ryan
2150 W. Winton Avenue
Hayward, CA 94545
Attention: John Vargas

Client Project ID: Arco 2169, Oakland
Matrix Descript: Soil
Analysis Method: EPA 3550/8015
First Sample #: 206-1686

Sampled: Jun 8, 1992
Received: Jun 9, 1992
Extracted: Jun 11, 1992
Analyzed: Jun 11, 1992
Amended: Jun 22, 1992

TOTAL PETROLEUM FUEL HYDROCARBONS (EPA 8015)

Sample Number	Sample Description	High B.P. Hydrocarbons mg/kg (ppm)
206-1686	AV-1-6.5	N.D.
206-1687	AV-1-11.5	N.D.
206-1688	AV-2-6.5	N.D.
206-1689	AV-2-11.5	N.D.
206-1690	AV-3-6.5	N.D.
206-1691	AV-3-11.5	N.D.

Detection Limits:

1.0

High Boiling Point Hydrocarbons are quantitated against a diesel fuel standard.
Analytes reported as N.D. were not present above the stated limit of detection.

SEQUOIA ANALYTICAL


Nokowhat D. Herrera
Project Manager

Please Note:

Samples 2061687, 89 & 91 appear to contain gasoline.



SEQUOIA ANALYTICAL

680 Chesapeake Drive • Redwood City, CA 94063
(415) 364-9600 • FAX (415) 364-9233

Gettler Ryan
2150 W. Winton Avenue
Hayward, CA 94545
Attention: John Vargas

Client Project ID: Arco 2169, Oakland

QC Sample Group: 2061686 - 91

Amended: Jun 22, 1992

QUALITY CONTROL DATA REPORT

ANALYTE	Diesel
----------------	--------

Method: EPA 8015
 Analyst: R.Lee
 Reporting Units: mg/kg
 Date Analyzed: Jun 11, 1992
 QC Sample #: DBLK061192

Sample Conc.: N.D.

Spike Conc. Added: 15

Conc. Matrix Spike: 11

Matrix Spike % Recovery: 73

Conc. Matrix Spike Dup.: 12

Matrix Spike Duplicate % Recovery: 80

Relative % Difference: 8.7

Quality Assurance Statement: All standard operating procedures and quality control requirements have been met.

SEQUOIA ANALYTICAL

Christine Middleton
 Nokowhat D. Herrera
 Project Manager

% Recovery:	$\frac{\text{Conc. of M.S.} - \text{Conc. of Sample}}{\text{Spike Conc. Added}} \times 100$
Relative % Difference:	$\frac{\text{Conc. of M.S.} - \text{Conc. of M.S.D.}}{(\text{Conc. of M.S.} + \text{Conc. of M.S.D.}) / 2} \times 100$



SEQUOIA ANALYTICAL

680 Chesapeake Drive • Redwood City, CA 94063
(415) 364-9600 • FAX (415) 364-9233

Gettler Ryan	Client Project ID: Arco 2169, Oakland	Sampled: Jun 8, 1992
2150 W. Winton Avenue	Matrix Descript: Soil	Received: Jun 9, 1992
Hayward, CA 94545	Analysis Method: EPA 5030/8015/8020	Analyzed: Jun 11, 1992
Attention: John Vargas	First Sample #: 206-1686	Amended: Jun 22, 1992

TOTAL PETROLEUM FUEL HYDROCARBONS with BTEX DISTINCTION (EPA 8015/8020)

Sample Number	Sample Description	Low/Medium B.P.	Benzene mg/kg (ppm)	Toluene mg/kg (ppm)	Ethyl Benzene mg/kg (ppm)	Xylenes mg/kg (ppm)
		Hydrocarbons mg/kg (ppm)				
206-1686	AV-1-6.5	N.D.	0.15	0.019	0.014	0.062
206-1687	AV-1-11.5	12	0.81	1.3	0.27	1.5
206-1688	AV-2-6.5	1.8	0.31	0.15	0.036	0.21
206-1689	AV-2-11.5	1,500	21	84	27	170
206-1690	AV-3-6.5	N.D.	0.037	N.D.	0.018	0.028
206-1691	AV-3-11.5	110	2.4	4.6	1.9	10

Detection Limits:	1.0	0.0050	0.0050	0.0050	0.0050
-------------------	-----	--------	--------	--------	--------

Low to Medium Boiling Point Hydrocarbons are quantitated against a gasoline standard.
Analytes reported as N.D. were not present above the stated limit of detection.

SEQUOIA ANALYTICAL

Christin Middleton
Nokowhat D. Herrera
Project Manager

Please Note: The above samples appear to contain gasoline.



SEQUOIA ANALYTICAL

680 Chesapeake Drive • Redwood City, CA 94063
(415) 364-9600 • FAX (415) 364-9233

Gettler Ryan
2150 W. Winton Avenue
Hayward, CA 94545
Attention: John Vargas

Client Project ID: Arco 2169, Oakland

QC Sample Group: 2061686 - 91

Amended: Jun 22, 1992

QUALITY CONTROL DATA REPORT

ANALYTE	Benzene	Toluene	Ethyl Benzene	Xylenes
---------	---------	---------	---------------	---------

Method:	EPA 8020	EPA 8020	EPA 8020	EPA 8020
Analyst:	L.Laikhman	L.Laikhman	L.Laikhman	L.Laikhman
Reporting Units:	mg/kg	mg/kg	mg/kg	mg/kg
Date Analyzed:	Jun 11, 1992	Jun 11, 1992	Jun 11, 1992	Jun 11, 1992
QC Sample #:	GBLK061192	GBLK061192	GBLK061192	GBLK061192

Sample Conc.:	N.D.	N.D.	N.D.	N.D.
Spike Conc. Added:	0.20	0.20	0.20	0.60
Conc. Matrix Spike:	0.23	0.22	0.22	0.66
Matrix Spike % Recovery:	115	110	110	110
Conc. Matrix Spike Dup.:	0.24	0.24	0.23	0.70
Matrix Spike Duplicate % Recovery:	120	120	115	117
Relative % Difference:	4.3	8.7	4.4	5.8

Quality Assurance Statement: All standard operating procedures and quality control requirements have been met.

SEQUOIA ANALYTICAL

Christen Middleton
Nokowhat D. Herrera
Project Manager

% Recovery:	$\frac{\text{Conc. of M.S.} - \text{Conc. of Sample}}{\text{Spike Conc. Added}} \times 100$
Relative % Difference:	$\frac{\text{Conc. of M.S.} - \text{Conc. of M.S.D.}}{(\text{Conc. of M.S.} + \text{Conc. of M.S.D.}) / 2} \times 100$

ARCO Facility no. 2169	City (Facility) OAKLAND	Project manager (Consultant) JOHN VARGAS	Laboratory name SEQUOIA
ARCO engineer MICHAEL WHELAN	Telephone no. (ARCO)	Telephone no. (Consultant) (510) 352-4800	Contract number 07-073
Consultant name GeoSTRATEGIES INC.		Address (Consultant) 2150 W. WINTON AVE, HAYWARD	Method of shipment COURIER
		Fax no. (Consultant) (510) 783-1089	Special detection Limit/reporting

Sample I.D.	Lab no.	Container no.	Matrix			Preservation		Sampling date	Sampling time	BTEX EPA 8020	BTEX/TPH EPA 1602/8020/8015	TPH Modified 8015 Gas Diesel	Oil and Grease 413.1 413.2	TPH EPA 418.1/SM503E	EPA 601/8010	EPA 624/8240	EPA 625/8270	TCLP Metals VOA VDA	Semi Metals EPA 60107000 TLIC STLC	Lead Org./DHS Lead EPA 7420/7421						
			Soil	Water	Other	Ice	Acid																			
AV-1-6.5		1	X			X		6/8/92	14:00	X	X															
AV-1-11.5		1	X			X		6/8/92	14:15	X	X															
AV-2-6.5		1	X			X		6/8/92	15:15	X	X															
AV-2-11.5		1	X			X		6/8/92	15:30	X	X															
AV-3-6.5		1	X			X		6/8/92	16:20	X	X															
AV-3-11.5		1	X			X		6/8/92	16:30	X	X															

Special detection Limit/reporting	LOWEST POSSIBLE
Special QA/QC	NORMAL
Remarks	
Lab number	
Turnaround time	
Priority Rush 1 Business Day	<input type="checkbox"/>
Rush 2 Business Days	<input type="checkbox"/>
Expedited 5 Business Days	<input type="checkbox"/>
Standard 10 Business Days	<input checked="" type="checkbox"/>

Condition of sample: good		Temperature received: cool	
Relinquished by sampler <i>Michael Whelan</i>	Date 6/9/92 Time 15:26	Received by <i>Clark V. Elly</i>	Date 6-9-92 Time 5:26
Relinquished by <i>Clark V. Elly</i>	Date 6-9-92 Time 4:00	Received by laboratory <i>[Signature]</i>	Date 6-9 Time 1600

GeoStrategies Inc.

APPENDIX C
AIR CHEMICAL ANALYTICAL REPORT
AND
CHAIN-OF-CUSTODY FORM



SEQUOIA ANALYTICAL

680 Chesapeake Drive • Redwood City, CA 94063
(415) 364-9600 • FAX (415) 364-9233

Gettler Ryan
2150 W. Winton Avenue
Hayward, CA 94545
Attention: Barry McCoy

Project: 9927.06, Arco 2169, Oakland

Enclosed are the results from 2 special matrix samples received at Sequoia Analytical on June 11, 1992. The requested analyses are listed below:

SAMPLE #	SAMPLE DESCRIPTION	DATE OF COLLECTION	TEST METHOD
2061972	Air, Influent	5/29/92	EPA 5030/8015/8020
2061973	Air, Effluent	5/29/92	EPA 5030/8015/8020

Please contact me if you have any questions. In the meantime, thank you for the opportunity to work with you on this project.

Very truly yours,

SEQUOIA ANALYTICAL

Nokowhat D. Herrera
Project Manager

927-A



SEQUOIA ANALYTICAL

680 Chesapeake Drive • Redwood City, CA 94063
(415) 364-9600 • FAX (415) 364-9233

Gettler Ryan
2150 W. Winton Avenue
Hayward, CA 94545
Attention: Barry McCoy

Client Project ID: 9927.06, Arco 2169, Oakland
Matrix Descript: Air
Analysis Method: EPA 5030/8015/8020
First Sample #: 206-1972

Sampled: Jun 11, 1992
Received: Jun 11, 1992
Analyzed: 6/11-12/92
Reported: Jun 15, 1992

TOTAL PETROLEUM FUEL HYDROCARBONS with BTEX DISTINCTION (EPA 8015/8020)

Sample Number	Sample Description	Low/Medium B.P. Hydrocarbons ppmv	Benzene ppmv	Toluene ppmv	Ethyl Benzene ppmv	Xylenes ppmv
206-1972	Influent	24,000	1,300	1,200	85	350
206-1973	Effluent	13	1.9	0.29	0.10	0.51

Detection Limits:

2.3

0.019

0.016

0.014

0.014

Low to Medium Boiling Point Hydrocarbons are quantitated against a gasoline fuel standard.
Analytes reported as N.D. were not present above the stated limit of detection.

SEQUOIA ANALYTICAL

Christina Herrera
Nokowhat D. Herrera
Project Manager

Please Note:

A molecular weight of 65 was used to calculate ppmv for TPH-G.



SEQUOIA ANALYTICAL

680 Chesapeake Drive • Redwood City, CA 94063
(415) 364-9600 • FAX (415) 364-9233

Gettler Ryan

Client Project ID: 9927.06, Arco 2169, Oakland

2150 W. Winton Avenue

Hayward, CA 94545

Attention: Barry McCoy

QC Sample Group: 206-1972

Reported: Jun 15, 1992

QUALITY CONTROL DATA REPORT

ANALYTE	Benzene	Toluene	Ethyl Benzene	Xylenes
---------	---------	---------	---------------	---------

Method:	EPA 8020	EPA 8020	EPA 8020	EPA 8020
Analyst:	M.Nipp	M.Nipp	M.Nipp	M.Nipp
Reporting Units:	µg/L	µg/L	µg/L	µg/L
Date Analyzed:	Jun 12, 1992	Jun 12, 1992	Jun 12, 1992	Jun 12, 1992
QC Sample #:	GBLK061292	GBLK061292	GBLK061292	GBLK061292

Sample Conc.:	N.D.	N.D.	N.D.	N.D.
Spike Conc. Added:	10	10	10	30
Conc. Matrix Spike:	8.8	8.8	8.9	27
Matrix Spike % Recovery:	88	88	8.7	90
Conc. Matrix Spike Dup.:	8.6	8.6	8.7	26
Matrix Spike Duplicate % Recovery:	86	86	87	87
Relative % Difference:	2.3	2.3	2.3	3.8

Quality Assurance Statement: All standard operating procedures and quality control requirements have been met.

SEQUOIA ANALYTICAL

Christine Medeiros
Nokowhat D. Herrera
Project Manager

% Recovery:	$\frac{\text{Conc. of M.S.} - \text{Conc. of Sample}}{\text{Spike Conc. Added}} \times 100$
Relative % Difference:	$\frac{\text{Conc. of M.S.} - \text{Conc. of M.S.D.}}{(\text{Conc. of M.S.} + \text{Conc. of M.S.D.}) / 2} \times 100$



SEQUOIA ANALYTICAL

680 Chesapeake Drive • Redwood City, CA 94063
(415) 364-9600 • FAX (415) 364-9233

Gettler Ryan
2150 W. Winton Avenue
Hayward, CA 94545
Attention: Barry McCoy

Client Project ID: 9927.06, Arco 2169, Oakland

QC Sample Group: 206-1973

Reported: Jun 15, 1992

QUALITY CONTROL DATA REPORT

ANALYTE	Benzene	Toluene	Ethyl Benzene	Xylenes
---------	---------	---------	---------------	---------

Method:	EPA 8020	EPA 8020	EPA 8020	EPA 8020
Analyst:	M.Nipp	M.Nipp	M.Nipp	M.Nipp
Reporting Units:	µg/L	µg/L	µg/L	µg/L
Date Analyzed:	Jun 11, 1992	Jun 11, 1992	Jun 11, 1992	Jun 11, 1992
QC Sample #:	GBLK061192	GBLK061192	GBLK061192	GBLK061192

Sample Conc.:	N.D.	N.D.	N.D.	N.D.
Spike Conc. Added:	10	10	10	30
Conc. Matrix Spike:	10	11	11	33
Matrix Spike % Recovery:	100	110	110	110
Conc. Matrix Spike Dup.:	9.9	10	11	32
Matrix Spike Duplicate % Recovery:	99	100	110	107
Relative % Difference:	1.0	9.5	0.0	3.1

Quality Assurance Statement: All standard operating procedures and quality control requirements have been met.

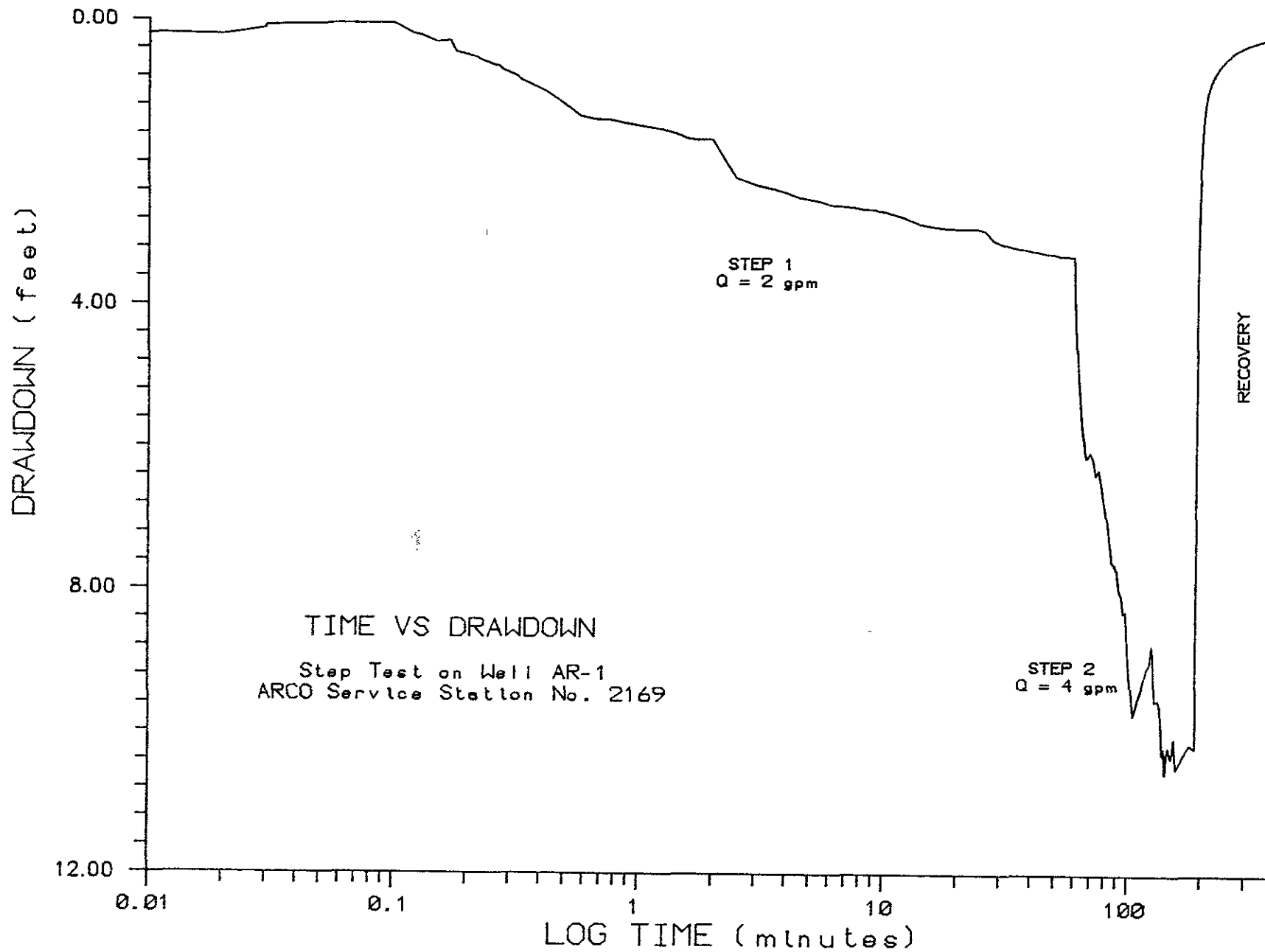
SEQUOIA ANALYTICAL

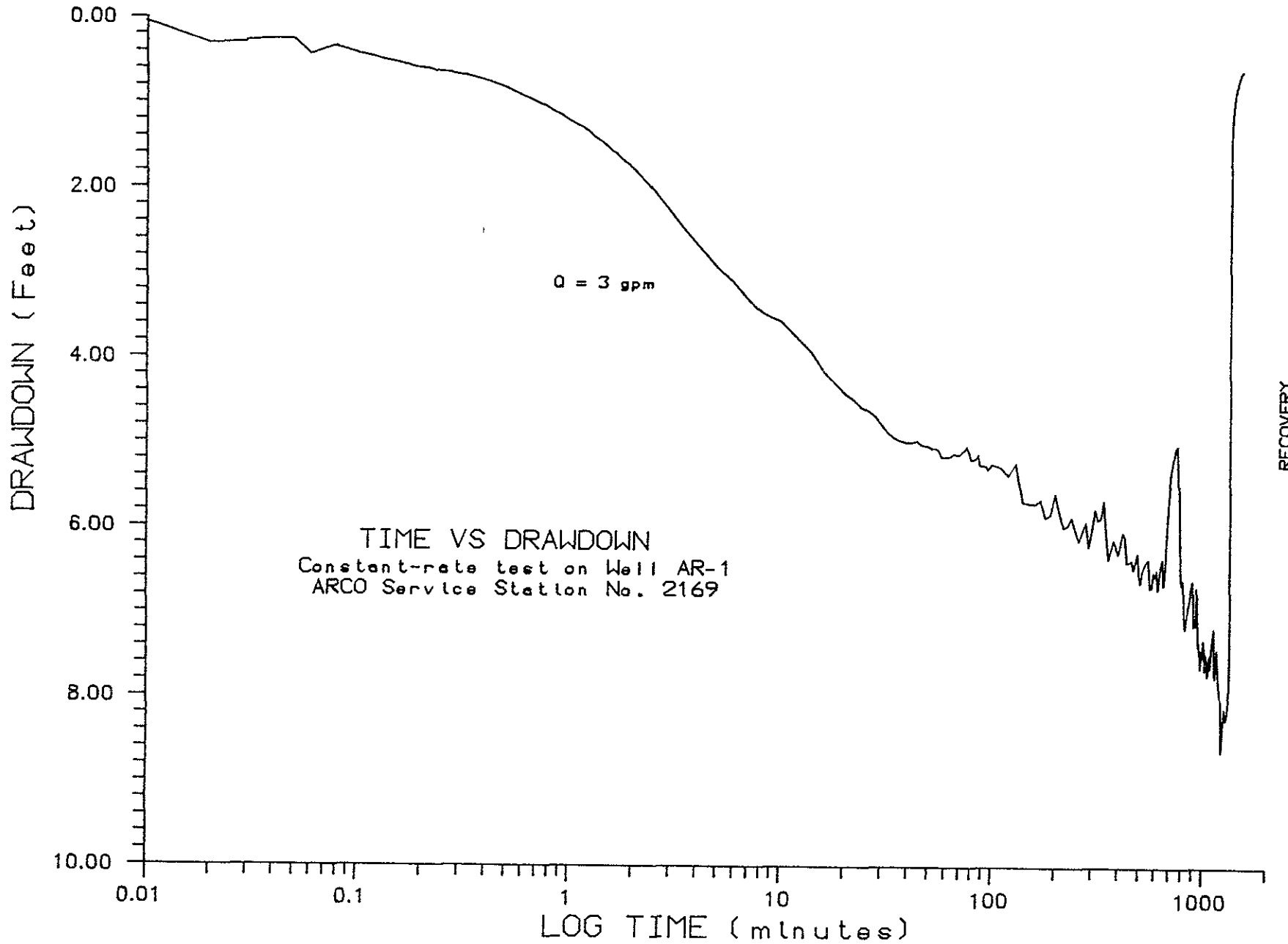
Christen Maddison
Nokowhat D. Herrera
Project Manager

% Recovery:	$\frac{\text{Conc. of M.S.} - \text{Conc. of Sample}}{\text{Spike Conc. Added}} \times 100$
Relative % Difference:	$\frac{\text{Conc. of M.S.} - \text{Conc. of M.S.D.}}{(\text{Conc. of M.S.} + \text{Conc. of M.S.D.}) / 2} \times 100$

GeoStrategies Inc.

APPENDIX D
TIME VS. DRAWDOWN



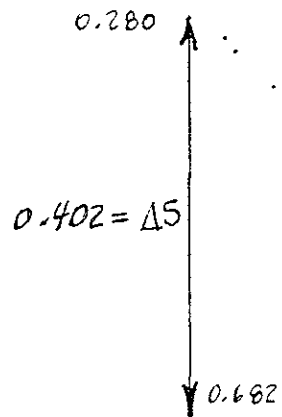


GeoStrategies Inc.

APPENDIX E
FIELD DATA PLOTS: JACOB METHOD

Constant rate

A-1



$$T = \frac{264 (Q)}{\Delta S}$$

$$T = \frac{264 (3)}{0.402}$$

$$T = 1.97 \times 10^3$$

$$S_y = \frac{0.3 (T) t_0}{r^2}$$

$$S_y = \frac{0.3 (1.9 \times 10^3) 0.0029}{50^2}$$

$$S_y = 4.75 \times 10^{-4}$$

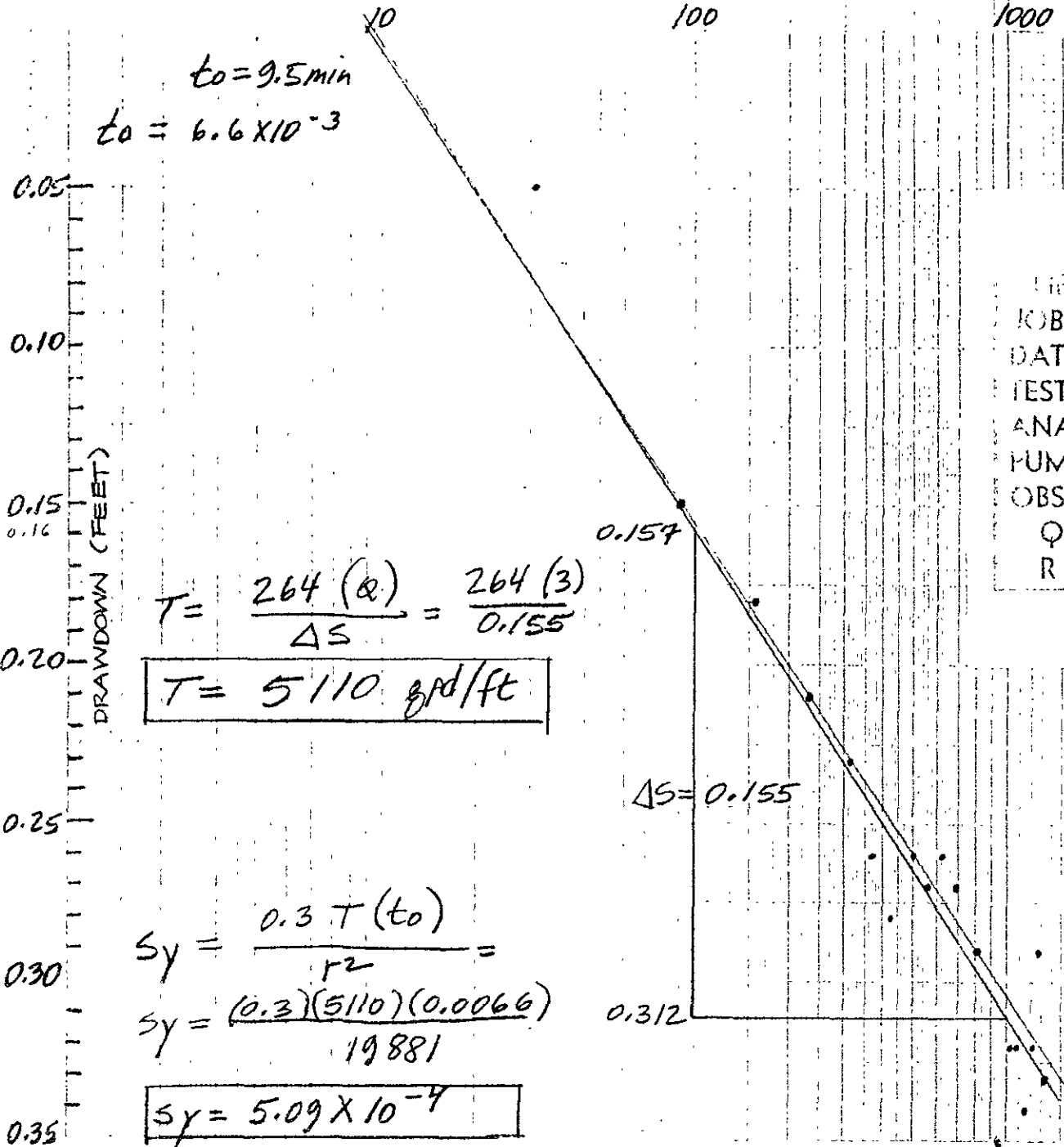
CLIENT	ARCO
JOB NO.	7927
DATE	15 July, 92
TEST NO.	Constant
ANALYSIS	Jacob
PUMP. WELL	AR-1
CBS. WELL	A-1
Q =	3 gpm
R =	50 feet

Well A-2

TIME (minute)

100

1000



$t_0 = 9.5 \text{ min}$
 $t_0 = 6.6 \times 10^{-3}$

CLIENT	ARCO
JOB NO.	7927
DATE	7-15 & 16-92
TEST NO.	Constant
ANALYSIS	JACOB
PUMP. WELL	AR-1
OBS. WELL	A-2
Q =	3 gpm
R =	141 feet

$$T = \frac{264 (Q)}{\Delta s} = \frac{264 (3)}{0.155}$$

$$T = 5110 \text{ gpd/ft}$$

$$s_y = \frac{0.3 T (t_0)}{r^2}$$

$$s_y = \frac{(0.3)(5110)(0.0066)}{19881}$$

$$s_y = 5.09 \times 10^{-4}$$

constant • WELL A-3

Time (minutes)

DRAWDOWN (feet)

DRAWDOWN (feet)

$t_0 = 22 \text{ min}$
 $t_0 = 0.015 \text{ day}$

10 100 1000

$AS = 0.154$

$T = \frac{264(Q)}{AS}$

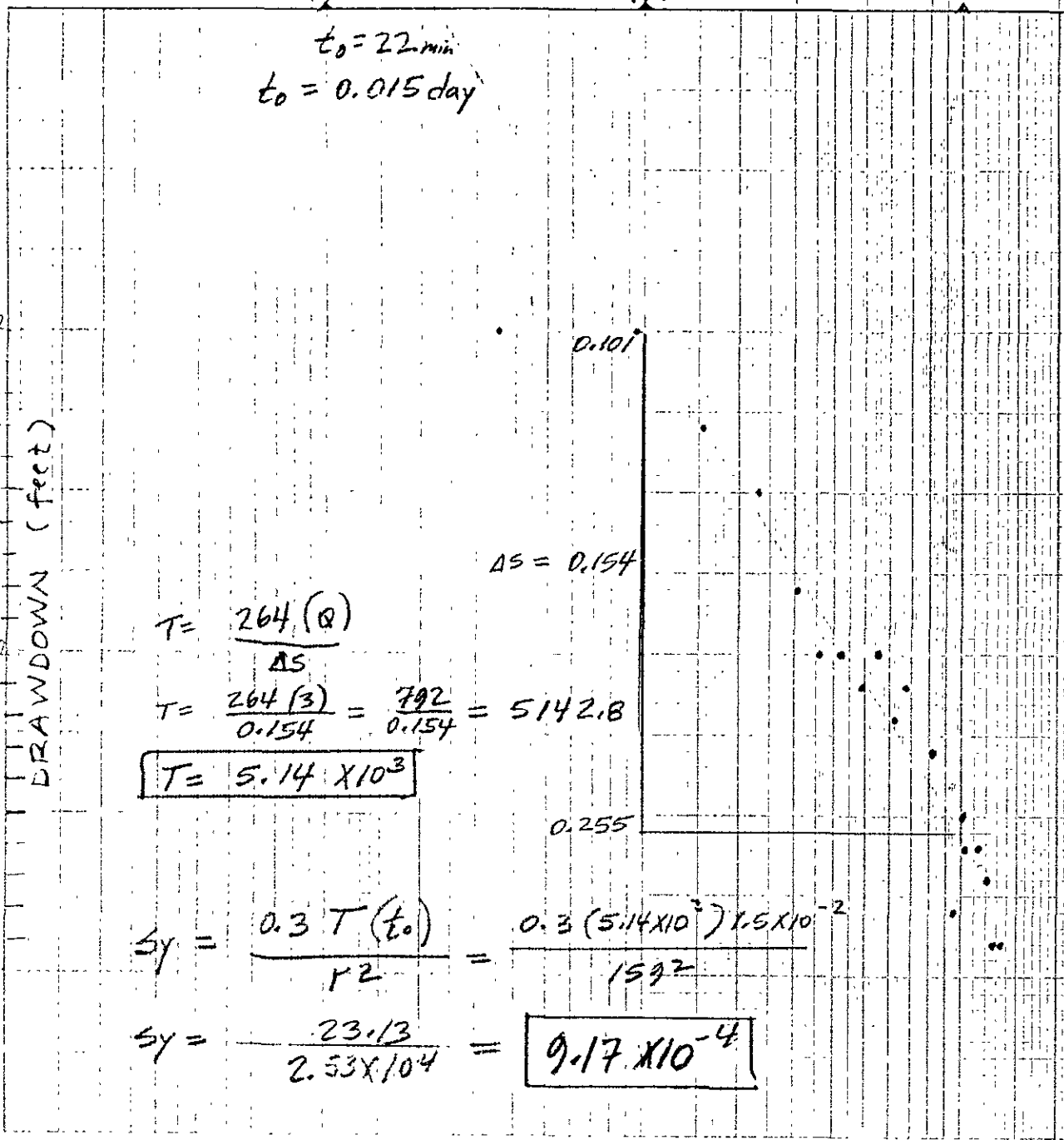
$T = \frac{264(3)}{0.154} = \frac{792}{0.154} = 5142.8$

$T = 5.14 \times 10^3$

$s_y = \frac{0.3 T(t_0)}{r^2} = \frac{0.3 (5.14 \times 10^3) 1.5 \times 10^{-2}}{159^2}$

$s_y = \frac{23.13}{2.53 \times 10^4} = 9.17 \times 10^{-4}$

ARCO
 7927
 7-15&16-92
 constant
 Jacob
 AR-1
 A-3
 3 ppm
 159 feet

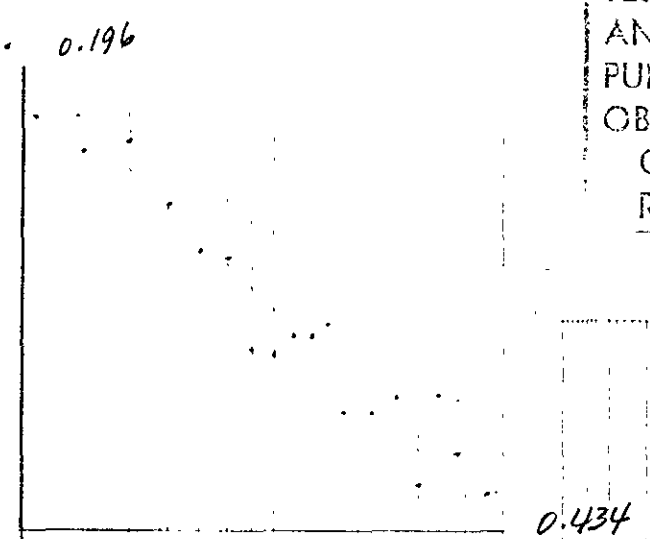


1/4 of constant rate

$t_0 = 7.6 \text{ min}$
 $t_0 = 3.2 \times 10^{-3}$

0 15 30 45 60 75 90 105 120 135 150 165 180 195 210 225 240

1
1.5
2
3
4
5
6
7



$\Delta s = .434 - .196$
 $\Delta s = 0.238$

$T = \frac{264Q}{\Delta s}$

$T = \frac{264(3)}{0.238}$

$T = 3.33 \times 10^3 \text{ gpd/ft.}$

$Sy = \frac{0.3 T (t_0)}{r^2}$

$Sy = \frac{0.3 (3.33 \times 10^3) 3.2 \times 10^{-3}}{128^2}$

$Sy = \frac{3.19}{16384}$

$Sy = 1.95 \times 10^{-4}$

CLIENT	ARCO
JOB NO.	7927
DATE	15 July 92
TEST NO.	Constan
ANALYSIS	Jacob
PUMP. WELL	AR-1
OBS. WELL	A-4
Q =	3 gpm
R =	128 feet

7927

AR-2

0.10
0.20
0.30
0.40
0.50

1.0 min = t_0
 6.9×10^{-4} days = t_0

$$T = \frac{264 Q}{\Delta S}$$

$$T = \frac{264 (3)}{0.12}$$

$$T = 6600 \text{ gpd/ft.}$$

$$S_y = \frac{0.3 T (t_0)}{r^2}$$

$$S_y = \frac{0.3 (6600) (6.9 \times 10^{-4})}{82^2}$$

$$S_y = \frac{1.37}{6724}$$

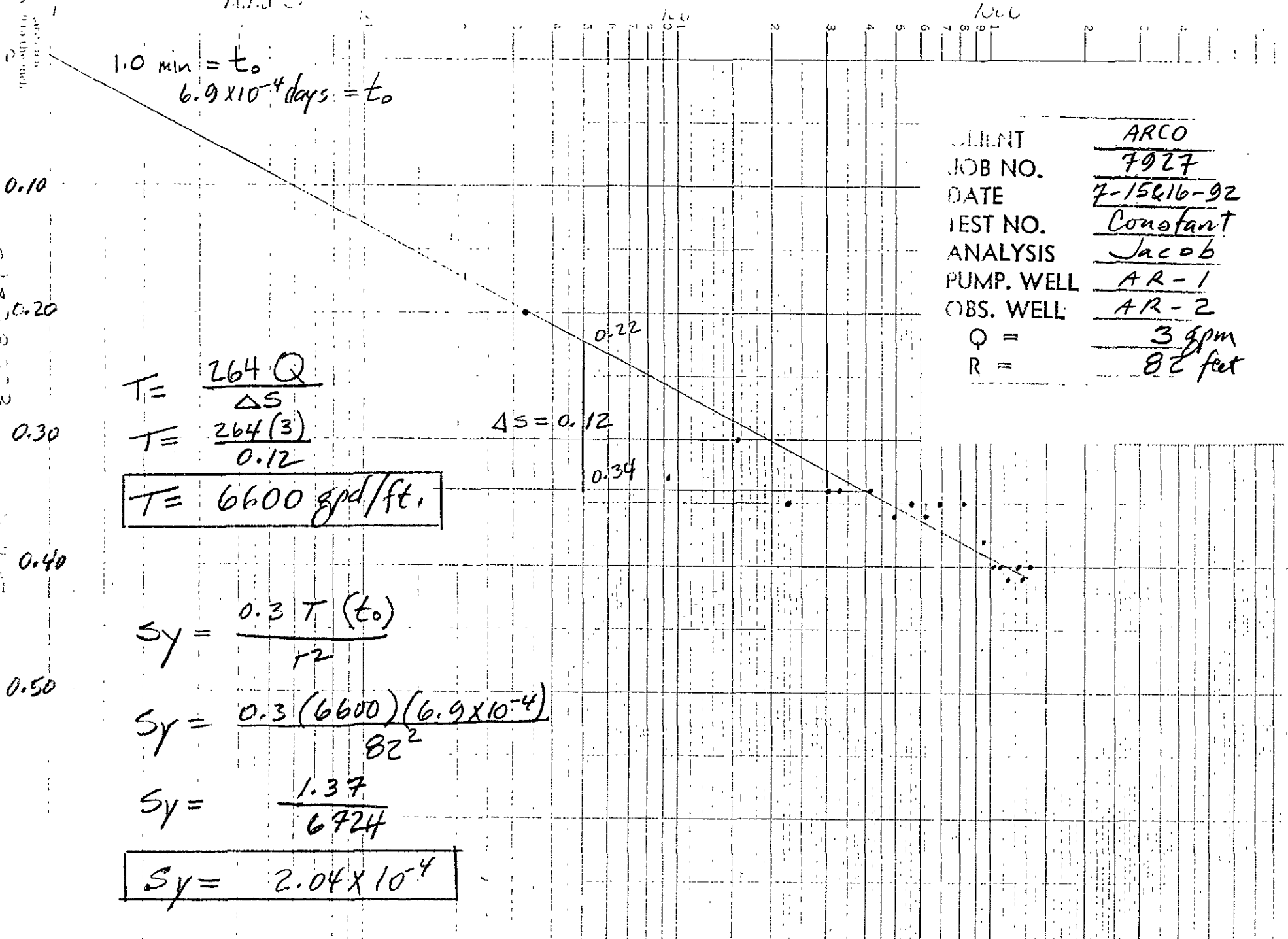
$$S_y = 2.04 \times 10^{-4}$$

$\Delta S = 0.12$

0.22

0.34

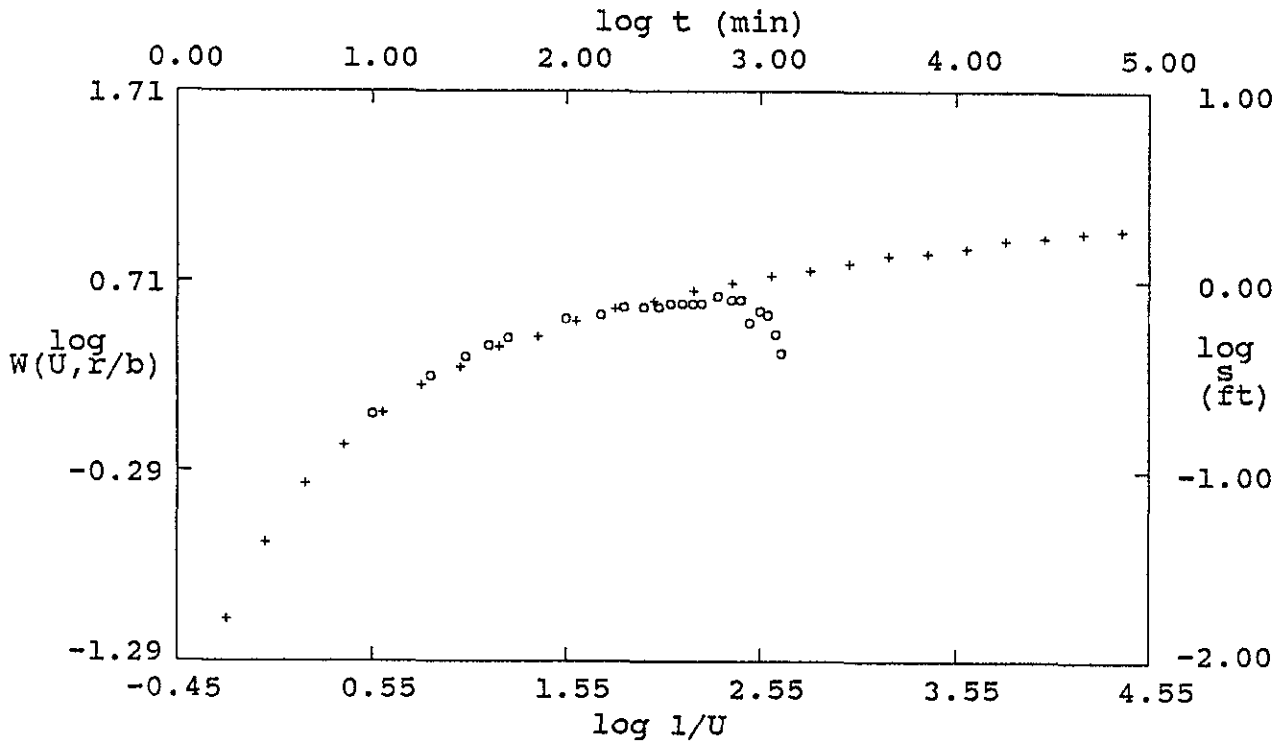
CLIENT	ARCO
JOB NO.	7927
DATE	7-15&16-92
TEST NO.	Constant
ANALYSIS	Jacob
PUMP. WELL	AR-1
OBS. WELL	AR-2
Q =	3 gpm
R =	82 feet



GeoStrategies Inc.

APPENDIX F
GWAP DATA PLOTS: THEIS METHOD

Well A-1



o - Data

+ - Type Curve

Confined Leaky: $r/B = \text{Theis}$

SOLUTION

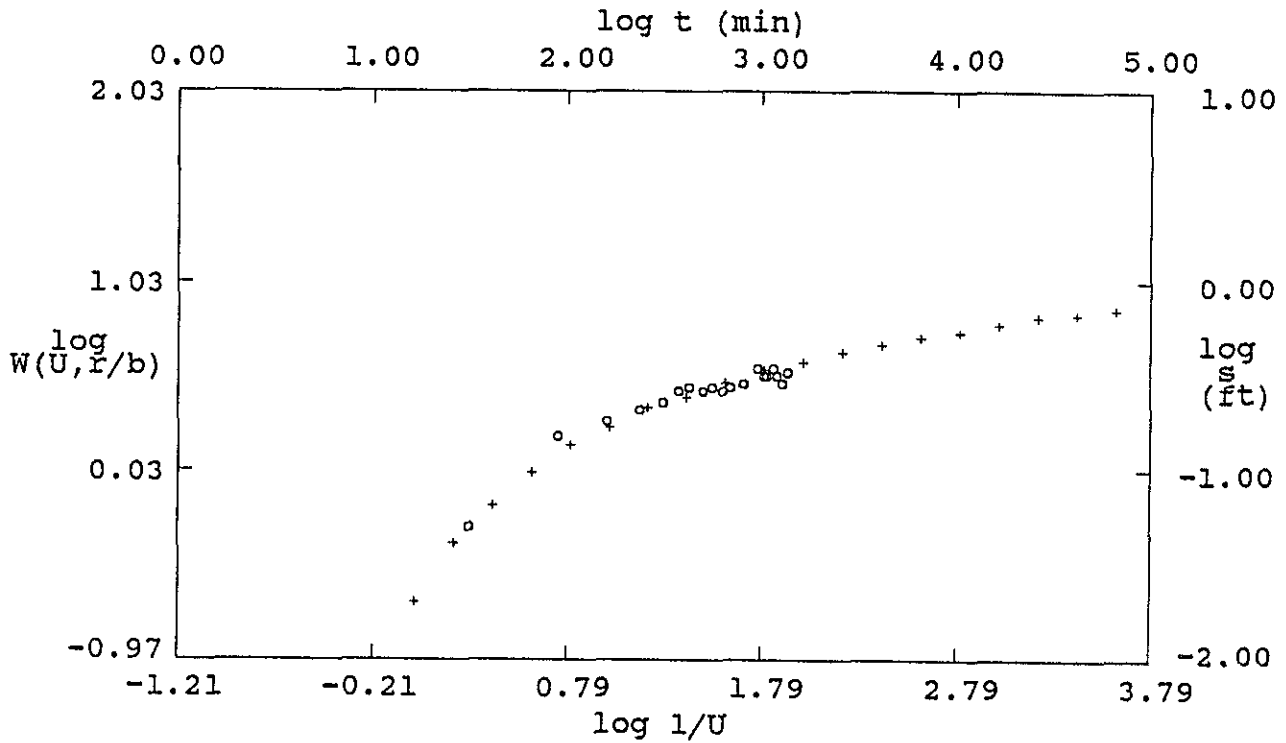
Transmissivity = $1.763\text{E}+0003$ gpd/ft

Aquifer Thick. = $1.500\text{E}+0001$ ft

Hydraulic Cond. = $1.175\text{E}+0002$ gpd/sq ft

Storativity = $5.301\text{E}-0004$

Well A-2



o - Data

+ - Type Curve

Confined Leaky: $r/B = \text{Theis}$

SOLUTION

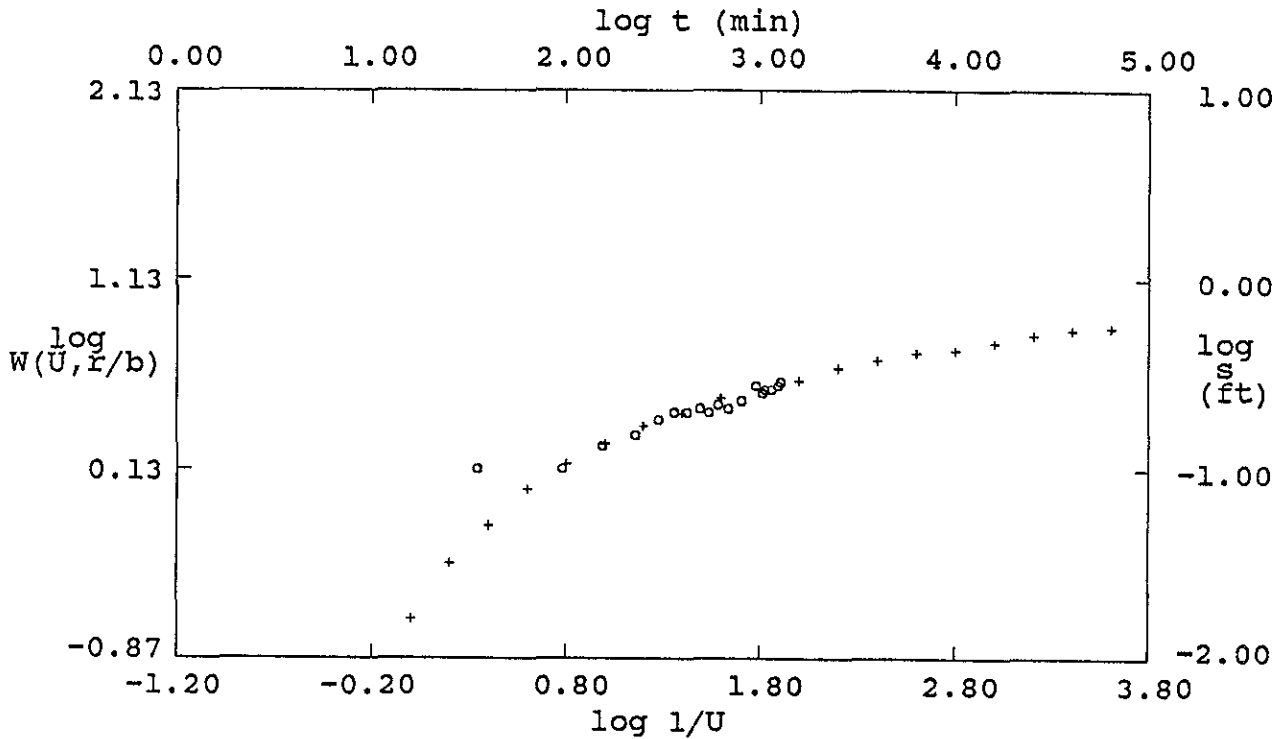
Transmissivity = $3.683\text{E}+0003$ gpd/ft

Aquifer Thick. = $1.500\text{E}+0001$ ft

Hydraulic Cond. = $2.455\text{E}+0002$ gpd/sq ft

Storativity = $1.116\text{E}-0003$

Well A-3



o - Data

+ - Type Curve

Confined Leaky: $r/B = \text{Theis}$

SOLUTION

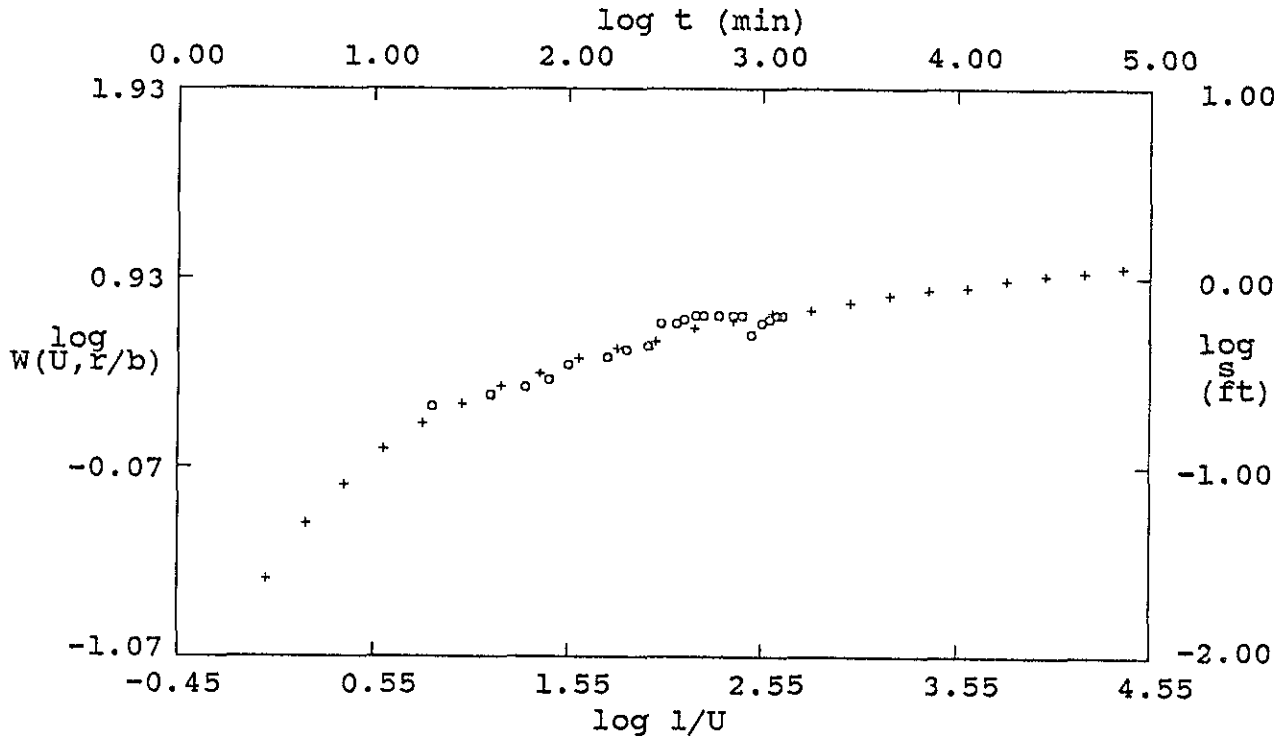
Transmissivity = $4.637E+0003$ gpd/ft

Aquifer Thick. = $1.500E+0001$ ft

Hydraulic Cond. = $3.091E+0002$ gpd/sq ft

Storativity = $1.080E-0003$

Well A-4



o - Data

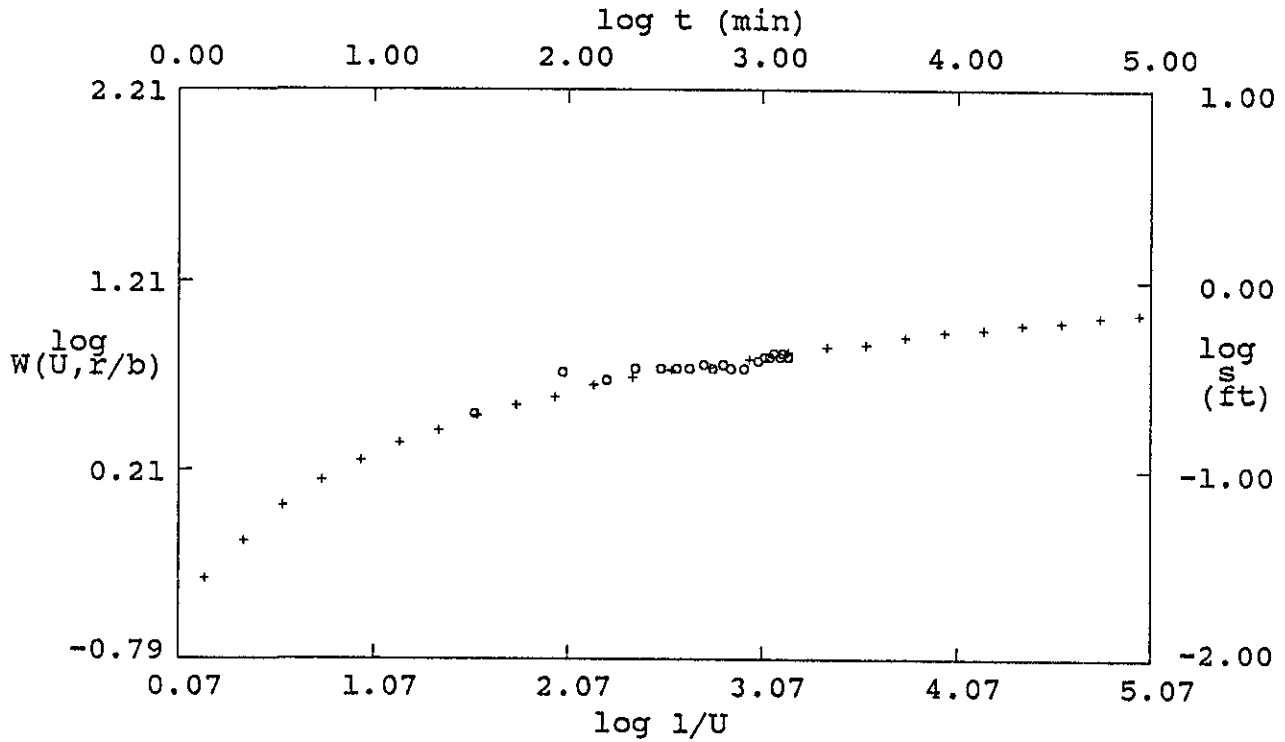
+ - Type Curve

Confined Leaky: $r/B = \text{Theis}$

SOLUTION

Transmissivity = $2.925E+0003$ gpd/ft
 Aquifer Thick. = $1.500E+0001$ ft
 Hydraulic Cond. = $1.950E+0002$ gpd/sq ft
 Storativity = $1.869E-0004$

Well AR-2



o - Data

+ - Type Curve

Confined Leaky: $r/B = \text{Theis}$

SOLUTION

Transmissivity = $5.574E+0003$ gpd/ft

Aquifer Thick. = $1.500E+0001$ ft

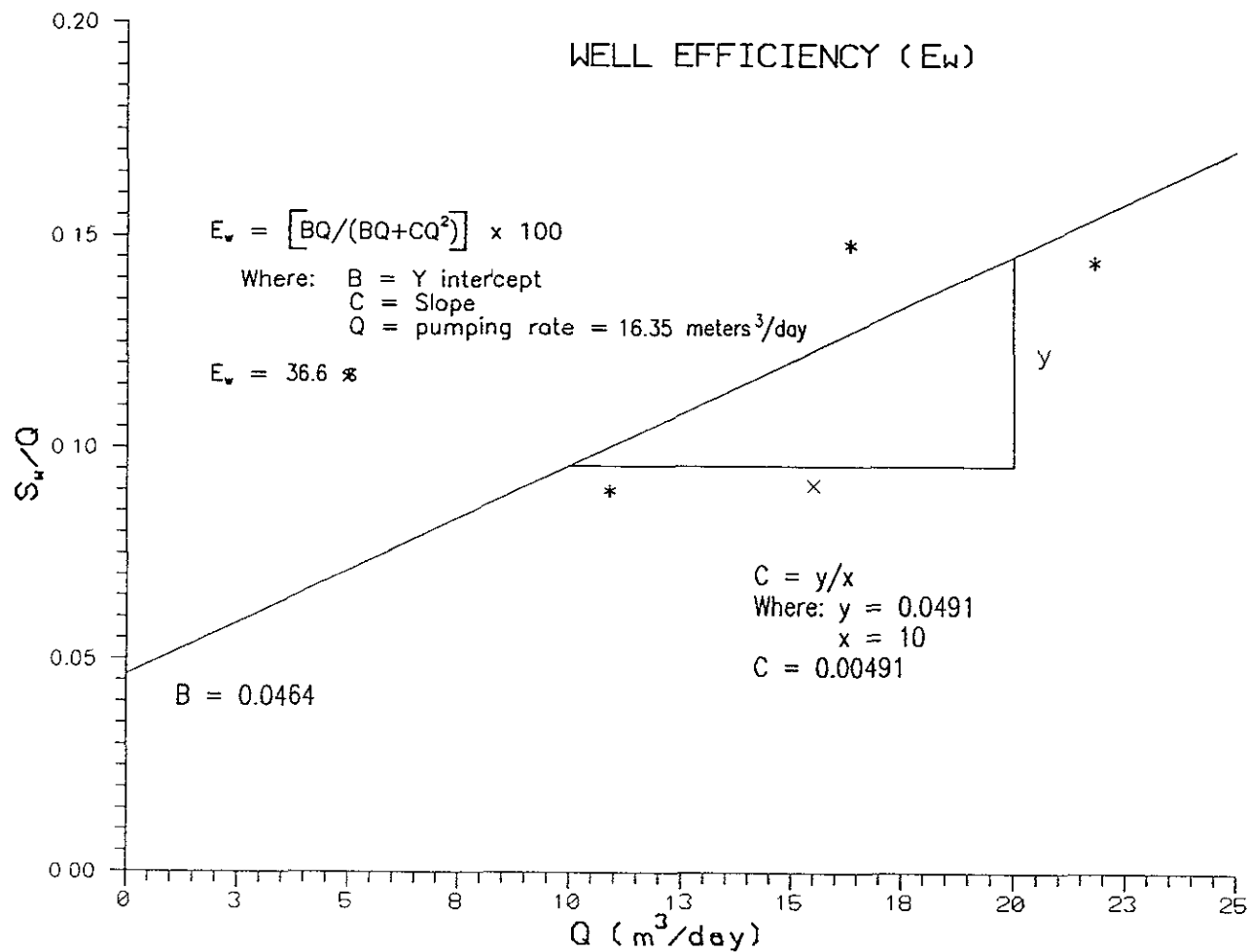
Hydraulic Cond. = $3.716E+0002$ gpd/sq ft

Storativity = $2.621E-0004$

GeoStrategies Inc.

APPENDIX G
WELL EFFICIENCY CALCULATION

WELL EFFICIENCY (E_w)



GeoStrategies Inc.

WELL EFFICIENCY GRAPH
 ARCO Service Station #2169
 889 West Grand Avenue
 Oakland, California

PLATE

JOB NUMBER
792705-4

REVIEWED BY
ACM

DATE
9/92

REVISED DATE
11/92



RECEIVED

JUN 25 1992

GeoStrategies Inc.

Date June 18, 1992
Project G70-52.01

To:
Mr. John Vargas
GeoStrategies Inc.
2140 West Winton Avenue
Hayward, California 94545

We are enclosing:

Copies	Description
<u>1</u>	<u>Depth To Water/Floating Product Survey Results</u>
<u> </u>	<u>June 1992 monthly water level survey, ARCO</u>
<u> </u>	<u>station 2169, 889 West Grand Ave. Oakland, CA.</u>

For your: X Information Sent by: X Mail

Comments:

Monthly water level data for the above mentioned site are attached. Please call if you have any questions: (408) 453-2266.

Jim Butera JB

Reviewed by:



Robert C Porter
Robert Porter, Senior Project
Engineer



**FIELD REPORT
DEPTH TO WATER / FLOATING PRODUCT SURVEY**

PROJECT # : G70-52.01

STATION ADDRESS : 889 West Grand Ave, Oakland, CA

DATE : 6-16-99

ARCO STATION # : 2169

FIELD TECHNICIAN : J. Williams

DAY : _____

DTW Order	WELL ID	Well Box Seal	Well Lid Secure	Gasket	Lock	Locking Well Cap	FIRST DEPTH TO WATER (feet)	SECOND DEPTH TO WATER (feet)	DEPTH TO FLOATING PRODUCT (feet)	FLOATING PRODUCT THICKNESS (feet)	WELL TOTAL DEPTH (feet)	COMMENTS
1	A-1	OK	OK	OK	2268	10K	11.95	11.95	ND	ND	24.35	NEED NEW LOCK
2	A-2	↓	↓	↓	2268	↓	12.43	12.44	ND	ND	25.20	-
3	A-3	↓	↓	↓	2268	↓	13.26	13.26	ND	ND	29.10	-
4	A-4	↓	↓	↓	2268	↓	12.33	12.33	ND	ND	28.00	-
5	AR-1	↓	↓	↓	2262	↓	12.47	12.48	ND	ND	27.70	-



EMCON
ASSOCIATES

Consultants in Wastes
Management and
Environmental Control

RECEIVED

MAY 27 1992

GeoStrategies Inc.

Date May 21, 1992
Project G70-52.01

To:

Mr. John Vargas
GeoStrategies Inc.
2140 West Winton Avenue
Hayward, California 94545

We are enclosing:

Copies	Description
<u>1</u>	<u>Depth To Water/Floating Product Survey Results</u>
	<u>May 1992 monthly water level survey, ARCO</u>
	<u>station 2169, 889 West Grand Ave. Oakland, CA.</u>

For your: X Information Sent by: X Mail

Comments:

Monthly water level data for the above mentioned site are attached. Please call if you have any questions: (408) 453-2266.

Reviewed by:



Jim Butera

Robert Porter

Robert Porter, Senior Project
Engineer

927-A



FIELD REPORT
DEPTH TO WATER / FLOATING PRODUCT SURVEY

PROJECT # : G70-52.01

STATION ADDRESS : 889 West Grand Ave, Oakland, CA

DATE : 5-22-92

ARCO STATION # : 2169

FIELD TECHNICIAN : M. Kuntz / J. DeFera

DAY : Wednesday

DTW Order	WELL ID	Well Box Seal	Well Lid Secure	Gasket	Lock	Locking Well Cap	FIRST DEPTH TO WATER (feet)	SECOND DEPTH TO WATER (feet)	DEPTH TO FLOATING PRODUCT (feet)	FLOATING PRODUCT THICKNESS (feet)	WELL TOTAL DEPTH (feet)	COMMENTS
1	A-1	OK	yes	yes	2268	yes	11.66	11.66	NA	ND	24.35	→
2	A-2	OK	yes	yes	2268	yes	12.17	12.18	ND	ND	25.15	-
3	A-3	OK	yes	yes	2268	yes	13.00	13.00	ND	ND	29.1	-
4	A-4	OK	yes	yes	2268	yes	12.13	12.14	ND	ND	27.90	-
5	AR#1	OK	yes	yes	2268	yes	12.37	12.37	ND	ND	27.74	-

GeoStrategies Inc.

APPENDIX I
EMCON GROUND-WATER SAMPLING REPORT



EMCON
ASSOCIATES

Consultants in Wastes
Management and
Environmental Control

RECEIVED

OCT 14 1992

GeoStrategies Inc.

Date August 10, 1992
Project G70-23.01

To:
Mr. John Vargas
GeoStrategies, Inc.
2140 West Winton Avenue
Hayward, California 94545

We are enclosing:

Copies	Description
<u>1</u>	<u>Depth To Water / Floating Product Survey Results</u>
<u>3</u>	<u>Summary of Groundwater Monitoring Data</u>
<u>1</u>	<u>Certified Analytical Reports with Chain-of-Custody</u>
<u>6</u>	<u>Water Sample Field Data Sheets</u>

For your: X Information Sent by: X Mail

Comments:

Enclosed are the data from the third quarter 1992 monitoring event at ARCO service station 2169, 889 West Grand Avenue, Oakland, CA. Groundwater monitoring is conducted consistent with applicable regulatory guidelines. Please call if you have any questions: (408) 453-2266.

Reviewed by:



Jim Butera JB.

Robert Porter
Robert Porter, Senior Project
Engineer.

FIELD REPORT
DEPTH TO WATER / FLOATING PRODUCT SURVEY

PROJECT # : G70-52.01

STATION ADDRESS : 889 West Grand Ave, Oakland, CA

DATE : 7-17-92

ARCO STATION # : 2169

FIELD TECHNICIAN : JW/RS

DAY : Friday

DTW Order	WELL ID	Well Box Seal	Well Lid Secure	Gasket	Lock	Locking Well Cap	FIRST DEPTH TO WATER (feet)	SECOND DEPTH TO WATER (feet)	DEPTH TO FLOATING PRODUCT (feet)	FLOATING PRODUCT THICKNESS (feet)	WELL TOTAL DEPTH (feet)	COMMENTS
1	A-1	Yes	Yes	Yes	2268	Yes	12.23	12.23	N.D	N.D	24.39	-
2	A-2	Yes	Yes	Yes	2268	Yes	12.64	12.64	N.D	N.D	25.17	-
3	A-3	Yes	Yes	Yes	2268	Yes	13.45	13.45	N.D	N.D	29.15	-
4	A-4	Yes	Yes	Yes	2268	Yes	12.60	12.60	N.D	N.D	27.95	-
5	AR-1	Yes	Yes	Yes	2268	Yes	13.00	13.00	N.D	N.D	27.75	-
6	AR-2	Yes	Yes	Yes	NO	Yes	13.14	13.14	N.D	N.D	29.2	-

SURVEY POINTS ARE TOP OF WELL BOXES

Summary of Groundwater Monitoring Data
 Third Quarter 1992
 ARCO Service Station 2169
 889 West Grand Avenue, Oakland, California
 micrograms per liter ($\mu\text{g/l}$) and milligrams per liter (mg/l)

Well ID and Sample Depth	Sampling Date	Depth To Water (feet)	Floating Product Thickness (feet)	TPH ¹ as Gasoline ($\mu\text{g/l}$)	Benzene ($\mu\text{g/l}$)	Toluene ($\mu\text{g/l}$)	Ethyl- benzene ($\mu\text{g/l}$)	Total Xylenes ($\mu\text{g/l}$)
A-1(24)	07/17/92	12.23	ND. ²	5,600.	3,000.	500.	<0.5	<0.5
A-2(25)	07/17/92	12.64	ND	<50.	<0.5	<0.5	<0.5	<0.5
A-3(29)	07/17/92	13.45	ND	<50.	<0.5	<0.5	1.3	2.3
A-4(27)	07/17/92	12.60	ND	<50.	<0.5	<0.5	<0.5	<0.5
AR-1(27)	07/17/92	13.00	ND	44,000.	4,300.	9,100.	1,800.	10,000.
AR-2(29)	07/17/92	13.14	ND	150.	6.6	24.	6.6	39.

1. TPH. = Total petroleum hydrocarbons
 2. ND. = Not detected



SEQUOIA ANALYTICAL

680 Chesapeake Drive • Redwood City, CA 94063
(415) 364-9600 • FAX (415) 364-9233

Emcon Associates
1938 Junction Avenue
San Jose, CA 95131
Attention: Jim Butera

Project: Arco 2169

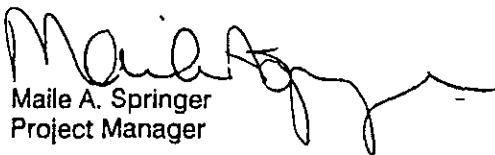
Enclosed are the results from 6 water samples received at Sequoia Analytical on July 17, 1992. The requested analyses are listed below:

SAMPLE #	SAMPLE DESCRIPTION	DATE OF COLLECTION	TEST METHOD
2072776	Water, A-1, (24)	7/17/92	EPA 5030/8015/8020
2072777	Water, A-2, (25)	7/17/92	EPA 5030/8015/8020
2072778	Water, A-3, (29)	7/17/92	EPA 5030/8015/8020
2072779	Water, A-4, (27)	7/17/92	EPA 5030/8015/8020
2072780	Water, AR-1, (27)	7/17/92	EPA 5030/8015/8020
2072781	Water, AR-2, (29)	7/17/92	EPA 5030/8015/8020

Please contact me if you have any questions. In the meantime, thank you for the opportunity to work with you on this project.

Very truly yours,

SEQUOIA ANALYTICAL


Maile A. Springer
Project Manager



SEQUOIA ANALYTICAL

680 Chesapeake Drive • Redwood City, CA 94063
(415) 364-9600 • FAX (415) 364-9233

Emcon Associates	Client Project ID: Arco 2169	Sampled: Jul 17, 1992
1938 Junction Avenue	Sample Matrix: Water	Received: Jul 17, 1992
San Jose, CA 95131	Analysis Method: EPA 5030/8015/8020	Reported: Jul 30, 1992
Attention: Jim Butera	First Sample #: 207-2776	

TOTAL PURGEABLE PETROLEUM HYDROCARBONS with BTEX DISTINCTION

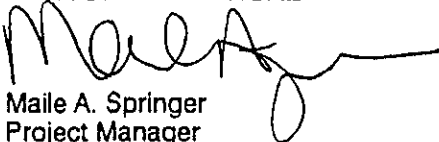
Analyte	Reporting Limit µg/L	Sample I.D. 207-2776 A-1, (24)	Sample I.D. 207-2777 A-2, (25)	Sample I.D. 207-2778 A-3, (29)	Sample I.D. 207-2779 A-4, (27)	Sample I.D. 207-2780 AR-1, (27)	Sample I.D. 207-2781 AR-2, (29)
Purgeable Hydrocarbons	50	5,600	N.D.	N.D.	N.D.	44,000	150
Benzene	0.50	3,000	N.D.	N.D.	N.D.	4,300	6.6
Toluene	0.50	500	N.D.	N.D.	N.D.	9,100	24
Ethyl Benzene	0.50	N.D.	N.D.	1.3	N.D.	1,800	6.6
Total Xylenes	0.50	N.D.	N.D.	2.3	N.D.	10,000	39
Chromatogram Pattern:		Gas	--	Gas	--	Gas	Gas

Quality Control Data

Report Limit Multiplication Factor:	200	1.0	1.0	1.0	400	1.0
Date Analyzed:	7/21/92	7/21/92	7/21/92	7/21/92	7/21/92	7/21/92
Instrument Identification:	GCHP-3	GCHP-3	GCHP-3	GCHP-3	GCHP-3	GCHP-3
Surrogate Recovery, %: (QC Limits = 70-130%)	104	91	106	101	113	114

Purgeable Hydrocarbons are quantitated against a fresh gasoline standard.
Analytes reported as N.D. were not detected above the stated reporting limit.

SEQUOIA ANALYTICAL


Maile A. Springer
Project Manager



SEQUOIA ANALYTICAL

680 Chesapeake Drive • Redwood City, CA 94063
(415) 364-9600 • FAX (415) 364-9233

Emcon Associates
1938 Junction Avenue
San Jose, CA 95131
Attention: Jim Butera

Client Project ID: Arco 2169

QC Sample Group: 2072776 - 81

Reported: Jul 30, 1992

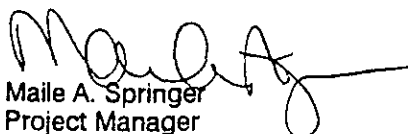
QUALITY CONTROL DATA REPORT

ANALYTE	Benzene	Toluene	Ethyl Benzene	Xylenes
---------	---------	---------	---------------	---------

Method:	EPA 8020	EPA 8020	EPA 8020	EPA 8020
Analyst:	M.Nipp	M.Nipp	M.Nipp	M.Nipp
Reporting Units:	µg/L	µg/L	µg/L	µg/L
Date Analyzed:	Jul 21, 1992	Jul 21, 1992	Jul 21, 1992	Jul 21, 1992
QC Sample #:	GBLK072192	GBLK072192	GBLK072192	GBLK072192
Sample Conc.:	N.D.	N.D.	N.D.	N.D.
Spike Conc. Added:	10	10	10	30
Conc. Matrix Spike:	10	10	10	30
Matrix Spike % Recovery:	100	100	100	100
Conc. Matrix Spike Dup.:	10	10	10	30
Matrix Spike Duplicate % Recovery:	100	100	100	100
Relative % Difference:	0.0	0.0	0.0	0.0

Quality Assurance Statement: All standard operating procedures and quality control requirements have been met.

SEQUOIA ANALYTICAL


Maile A. Springer
Project Manager

% Recovery:	$\frac{\text{Conc. of M.S.} - \text{Conc. of Sample}}{\text{Spike Conc. Added}} \times 100$
Relative % Difference:	$\frac{\text{Conc. of M.S.} - \text{Conc. of M.S.D.}}{(\text{Conc. of M.S.} + \text{Conc. of M.S.D.}) / 2} \times 100$



WATER SAMPLE FIELD DATA SHEET

Rev. 2, 5/91

PROJECT NO: G70-52.01
PURGED BY: J Williams
SAMPLED BY: J Williams

SAMPLE ID: A-2
CLIENT NAME: ARCO 2169
LOCATION: Oakland CA

TYPE: Ground Water Surface Water _____ Treatment Effluent _____ Other _____
CASING DIAMETER (Inches): 2 _____ 3 4 _____ 4.5 _____ 6 _____ Other _____

CASING ELEVATION (feet/MSL): NR VOLUME IN CASING (gal.): 4.52
DEPTH TO WATER (feet): 12.23 CALCULATED PURGE (gal.): 22.62
DEPTH OF WELL (feet): 24.39 ACTUAL PURGE VOL (gal.): 23.0

DATE PURGED: 07-17-97 Start (2400 Hr) 12:24 End (2400 Hr) 12:40
DATE SAMPLED: 07-17-97 Start (2400 Hr) 12:43 End (2400 Hr) 12:44

TIME (2400 Hr)	VOLUME (gal.)	pH (units)	E.C. (µmhos/cm @ 25° C)	TEMPERATURE (°F)	COLOR (visual)	TURBIDITY (visual)
<u>1231</u>	<u>4.5</u>	<u>6.55</u>	<u>1573</u>	<u>80.0</u>	<u>GRAY</u>	<u>HEAVY</u>
<u>1234</u>	<u>9.0</u>	<u>6.99</u>	<u>1444</u>	<u>76.7</u>	<u>L</u>	<u>L</u>
<u>1235</u>	<u>13.5</u>	<u>7.01</u>	<u>1433</u>	<u>75.7</u>	<u>L</u>	<u>L</u>
<u>1237</u>	<u>18.0</u>	<u>7.07</u>	<u>1423</u>	<u>75.4</u>	<u>L</u>	<u>L</u>
<u>12:40</u>	<u>23.0</u>	<u>7.04</u>	<u>1434</u>	<u>75.0</u>	<u>L</u>	<u>L</u>

D. O. (ppm): NR ODOR: -STRONG NR NR
(COBALT 0 - 100) (NTU 0 - 200)

FIELD QC SAMPLES COLLECTED AT THIS WELL (i.e. FB-1, XDUP-1): NR

PURGING EQUIPMENT			SAMPLING EQUIPMENT		
<input checked="" type="checkbox"/> 2" Bladder Pump	<input type="checkbox"/> Bailer (Teflon®)	<input type="checkbox"/> 2" Bladder Pump	<input checked="" type="checkbox"/> Bailer (Teflon®)	<input type="checkbox"/> DDL Sampler	<input type="checkbox"/> Bailer (Stainless Steel)
<input type="checkbox"/> Centrifugal Pump	<input type="checkbox"/> Bailer (PVC)	<input type="checkbox"/> Dipper	<input type="checkbox"/> Submersible Pump	<input type="checkbox"/> Well Wizard™	<input type="checkbox"/> Dedicated
<input type="checkbox"/> Submersible Pump	<input type="checkbox"/> Bailer (Stainless Steel)	<input type="checkbox"/> Other: _____	<input type="checkbox"/> Other: _____		
<input type="checkbox"/> Well Wizard™	<input type="checkbox"/> Dedicated				

WELL INTEGRITY: OK LOCK #: 2268

REMARKS: _____

Meter Calibration: Date: 7-17-97 Time: _____ Meter Serial #: _____ Temperature °F: 84.3
(EC 1000 103111000) (DI _____) (pH 7 7081700) (pH 10 999110100) (pH 4 4.001)
Location of previous calibration: A-1

Signature: Joe Williams Reviewed By: JB Page 1 of 1



EMCON ASSOCIATES

WATER SAMPLE FIELD DATA SHEET

Rev. 2, 5/91

PROJECT NO: G70.52.01

SAMPLE ID: A.2

PURGED BY: J. Williams

CLIENT NAME: ARCO 2169

SAMPLED BY: J. Williams

LOCATION: BAKLAND

TYPE: Ground Water Surface Water Treatment Effluent Other

CASING DIAMETER (Inches): 2 3 4 4.5 6 Other

CASING ELEVATION (feet/MSL): <u>12A</u>	VOLUME IN CASING (gal.): <u>4.67</u>
DEPTH TO WATER (feet): <u>12.64</u>	CALCULATED PURGE (gal.): <u>23.36</u>
DEPTH OF WELL (feet): <u>25.17</u>	ACTUAL PURGE VOL (gal.): <u>24.0</u>

DATE PURGED: <u>7-17-92</u>	Start (2400 Hr) <u>13:00</u>	End (2400 Hr) <u>13:08</u>
DATE SAMPLED: <u>7-17-92</u>	Start (2400 Hr) <u>13:10</u>	End (2400 Hr) <u>13:12</u>

TIME (2400 Hr)	VOLUME (gal.)	pH (units)	E.C. (umhos/cm @ 25° C)	TEMPERATURE (°F)	COLOR (visual)	TURBIDITY (visual)
<u>1303</u>	<u>4.75</u>	<u>7.11</u>	<u>1044</u>	<u>74.6</u>	<u>BROWN</u>	<u>HAZY</u>
<u>1305</u>	<u>9.50</u>	<u>7.04</u>	<u>1089</u>	<u>72.2</u>	<u>L</u>	<u>L</u>
<u>1306</u>	<u>14.25</u>	<u>7.05</u>	<u>1094</u>	<u>71.7</u>	<u>L</u>	<u>L</u>
<u>1307</u>	<u>19.0</u>	<u>7.07</u>	<u>1088</u>	<u>70.6</u>	<u>L</u>	<u>L</u>
<u>1308</u>	<u>23.75</u>	<u>7.10</u>	<u>1097</u>	<u>70.9</u>	<u>L</u>	<u>L</u>

D. O. (ppm): ND ODOR: None NR NR
(COBALT 0 - 100) (NTU 0 - 200)

FIELD QC SAMPLES COLLECTED AT THIS WELL (i.e. FB-1, XDUP-1): NR

PURGING EQUIPMENT

SAMPLING EQUIPMENT

- | | | | |
|--|---|--|--|
| <input type="checkbox"/> 2" Bladder Pump | <input type="checkbox"/> Bailor (Teflon®) | <input type="checkbox"/> 2" Bladder Pump | <input checked="" type="checkbox"/> Bailor (Teflon®) |
| <input checked="" type="checkbox"/> Centrifugal Pump | <input type="checkbox"/> Bailor (PVC) | <input type="checkbox"/> DDL Sampler | <input type="checkbox"/> Bailor (Stainless Steel) |
| <input type="checkbox"/> Submersible Pump | <input type="checkbox"/> Bailor (Stainless Steel) | <input type="checkbox"/> Dipper | <input type="checkbox"/> Submersible Pump |
| <input type="checkbox"/> Well Wizard™ | <input type="checkbox"/> Dedicated | <input type="checkbox"/> Well Wizard™ | <input type="checkbox"/> Dedicated |
| Other: <u>SACUZZI pump</u> | | Other: | |

WELL INTEGRITY: OK LOCK #: 2768

REMARKS: _____

Meter Calibration: Date: _____ Time: _____ Meter Serial #: _____ Temperature °F: _____
(EC 1000 _____ / _____) (DI _____) (pH 7 _____ / _____) (pH 10 _____ / _____) (pH 4 _____ / _____)

Location of previous calibration: 1A-1

Signature: J. Williams Reviewed By: JB Page 2 of 6



EMCON ASSOCIATES

WATER SAMPLE FIELD DATA SHEET

Rev. 2, 5/91

PROJECT NO: G70-5201
PURGED BY: J. Williams
SAMPLED BY: J. Williams

SAMPLE ID: A-3
CLIENT NAME: Acco 2169
LOCATION: OAKLAND

TYPE: Ground Water Surface Water _____ Treatment Effluent _____ Other _____
CASING DIAMETER (Inches): 2 _____ 3 4 _____ 4.5 _____ 6 _____ Other _____

CASING ELEVATION (feet/MSL): N.A. VOLUME IN CASING (gal.): 5.8
DEPTH TO WATER (feet): 13.45 CALCULATED PURGE (gal.): 29.2
DEPTH OF WELL (feet): 29.15 ACTUAL PURGE VOL (gal.): 30

DATE PURGED: 7-17-92 Start (2400 Hr) 1328 End (2400 Hr) 1336
DATE SAMPLED: 7-17-92 Start (2400 Hr) 1337 End (2400 Hr) 1338

TIME (2400 Hr)	VOLUME (gal.)	pH (units)	E.C. (µmhos/cm @ 25° C)	TEMPERATURE (°F)	COLOR (visual)	TURBIDITY (visual)
<u>1331</u>	<u>6</u>	<u>7.85</u>	<u>946</u>	<u>70.9</u>	<u>GRKY</u>	<u>HEAVY</u>
<u>1332</u>	<u>12</u>	<u>7.85</u>	<u>978</u>	<u>69.9</u>	<u>L</u>	<u>L</u>
<u>1334</u>	<u>18</u>	<u>7.78</u>	<u>995</u>	<u>69.6</u>	<u>L</u>	<u>L</u>
<u>1335</u>	<u>24</u>	<u>7.75</u>	<u>991</u>	<u>69.7</u>	<u>L</u>	<u>L</u>
<u>1336</u>	<u>30</u>	<u>7.76</u>	<u>991</u>	<u>69.9</u>	<u>L</u>	<u>L</u>

D. O. (ppm): NI ODOR: Slight _____
(COBALT 0-100) (NTU 0-200)

FIELD QC SAMPLES COLLECTED AT THIS WELL (i.e. FB-1, XDUP-1): ND

PURGING EQUIPMENT

SAMPLING EQUIPMENT

- | | | | |
|--|---|--|--|
| <input type="checkbox"/> 2" Bladder Pump | <input type="checkbox"/> Bailor (Teflon®) | <input type="checkbox"/> 2" Bladder Pump | <input checked="" type="checkbox"/> Bailor (Teflon®) |
| <input checked="" type="checkbox"/> Centrifugal Pump | <input type="checkbox"/> Bailor (PVC) | <input type="checkbox"/> DDL Sampler | <input type="checkbox"/> Bailor (Stainless Steel) |
| <input type="checkbox"/> Submersible Pump | <input type="checkbox"/> Bailor (Stainless Steel) | <input type="checkbox"/> Dipper | <input type="checkbox"/> Submersible Pump |
| <input type="checkbox"/> Well Wizard™ | <input type="checkbox"/> Dedicated | <input type="checkbox"/> Well Wizard™ | <input type="checkbox"/> Dedicated |
| Other: <u>Jaeger</u> | | Other: | |

WELL INTEGRITY: OK LOCK #: 2268

REMARKS: _____

Meter Calibration: Date: _____ Time: _____ Meter Serial #: _____ Temperature °F: _____
(EC 1000 _____ / _____) (DI _____) (pH 7 _____ / _____) (pH 10 _____ / _____) (pH 4 _____ / _____)

Location of previous calibration: #-1

Signature: [Signature] Reviewed By: JB Page 3 of 4



WATER SAMPLE FIELD DATA SHEET

Rev. 2, 5/91

PROJECT NO: G70-52-01
PURGED BY: J. Williams
SAMPLED BY: J. Williams

SAMPLE ID: A.4
CLIENT NAME: Arco 2169
LOCATION: OAKLAND CA

TYPE: Ground Water Surface Water _____ Treatment Effluent _____ Other _____
CASING DIAMETER (inches): 2 _____ 3 4 _____ 4.5 _____ 6 _____ Other _____

CASING ELEVATION (feet/MSL): NA VOLUME IN CASING (gal.): 5.7
DEPTH TO WATER (feet): 12.60 CALCULATED PURGE (gal.): 28.5
DEPTH OF WELL (feet): 27.95 ACTUAL PURGE VOL (gal.): 30

DATE PURGED: 7-17-92 Start (2400 Hr) 1345 End (2400 Hr) 1359
DATE SAMPLED: 7-17-97 Start (2400 Hr) 1400 End (2400 Hr) 1402

TIME (2400 Hr)	VOLUME (gal.)	pH (units)	EC. (umhos/cm @ 25° C)	TEMPERATURE (°F)	COLOR (visual)	TURBIDITY (visual)
<u>1352</u>	<u>6</u>	<u>7.67</u>	<u>918</u>	<u>69.9</u>	<u>GRAU</u>	<u>H2NUV</u>
<u>1353</u>	<u>12</u>	<u>7.67</u>	<u>929</u>	<u>71.1</u>	<u>L</u>	<u>L</u>
<u>1356</u>	<u>18</u>	<u>7.51</u>	<u>932</u>	<u>70.1</u>	<u>L</u>	<u>L</u>
<u>1358</u>	<u>24</u>	<u>7.70</u>	<u>879</u>	<u>71.8</u>	<u>L</u>	<u>L</u>
<u>1359</u>	<u>30</u>	<u>7.76</u>	<u>907</u>	<u>71.0</u>	<u>L</u>	<u>L</u>

D. O. (ppm): NR ODOR: NOISE COLOR: NR TURBIDITY: NR
(COBALT 0 - 100) (NTU 0 - 200)

FIELD QC SAMPLES COLLECTED AT THIS WELL (i.e. FB-1, XDUP-1): NR

PURGING EQUIPMENT

SAMPLING EQUIPMENT

- | | | | |
|--|---|--|--|
| <input type="checkbox"/> 2" Bladder Pump | <input type="checkbox"/> Bailer (Teflon®) | <input type="checkbox"/> 2" Bladder Pump | <input checked="" type="checkbox"/> Bailer (Teflon®) |
| <input checked="" type="checkbox"/> Centrifugal Pump | <input type="checkbox"/> Bailer (PVC) | <input type="checkbox"/> DDL Sampler | <input type="checkbox"/> Bailer (Stainless Steel) |
| <input type="checkbox"/> Submersible Pump | <input type="checkbox"/> Bailer (Stainless Steel) | <input type="checkbox"/> Dipper | <input type="checkbox"/> Submersible Pump |
| <input type="checkbox"/> Well Wizard™ | <input type="checkbox"/> Dedicated | <input type="checkbox"/> Well Wizard™ | <input type="checkbox"/> Dedicated |
| Other: _____ | | Other: _____ | |

WELL INTEGRITY: OK LOCK #: 2268

REMARKS: _____

Meter Calibration: Date: _____ Time: _____ Meter Serial #: _____ Temperature °F: _____
(EC 1000 _____ / _____) (DI _____) (pH 7 _____ / _____) (pH 10 _____ / _____) (pH 4 _____ / _____)
Location of previous calibration: A-1

Signature: [Signature] Reviewed By: JB Page 4 of 6



WATER SAMPLE FIELD DATA SHEET

Rev. 2, 5/91

PROJECT NO: G7052.01
PURGED BY: J. Williams
SAMPLED BY: J. Williams

SAMPLE ID: AR-1
CLIENT NAME: Acce 2169
LOCATION: OAKLAND CA

TYPE: Ground Water Surface Water _____ Treatment Effluent _____ Other _____
CASING DIAMETER (inches): 2 _____ 3 _____ 4 _____ 4.5 _____ 6 Other _____

CASING ELEVATION (feet/MSL): NA VOLUME IN CASING (gal.): 21.6
DEPTH TO WATER (feet): 13.0 CALCULATED PURGE (gal.): 2108.2
DEPTH OF WELL (feet): 27.75 ACTUAL PURGE VOL (gal.): 110

DATE PURGED: 7-17-92 Start (2400 Hr) 1418 End (2400 Hr) 1443
DATE SAMPLED: 7-17-92 Start (2400 Hr) 1444 End (2400 Hr) 1447

TIME (2400 Hr)	VOLUME (gal.)	pH (units)	EC. (umhos/cm @ 25° C)	TEMPERATURE (°F)	COLOR (visual)	TURBIDITY (visual)
<u>1421</u>	<u>22</u>	<u>7.45</u>	<u>1048</u>	<u>71.0</u>	<u>GRAY</u>	<u>118/104</u>
<u>1427</u>	<u>44</u>	<u>7.47</u>	<u>1011</u>	<u>71.5</u>	<u>2</u>	<u>1</u>
<u>1434</u>	<u>66</u>	<u>7.44</u>	<u>973</u>	<u>73.4</u>	<u>2</u>	<u>2</u>
<u>1438</u>	<u>88</u>	<u>7.43</u>	<u>1010</u>	<u>71.5</u>	<u>2</u>	<u>1</u>
<u>1443</u>	<u>110</u>	<u>7.50</u>	<u>1029</u>	<u>69.8</u>	<u>2</u>	<u>1</u>

D. O. (ppm): NL ODOR: STRONG (COBALT 0 - 100) NL (NTU 0 - 200) NR

FIELD QC SAMPLES COLLECTED AT THIS WELL (i.e. FB-1, XDUP-1): NR

PURGING EQUIPMENT

SAMPLING EQUIPMENT

- | | | | |
|--|---|--|--|
| <input type="checkbox"/> 2" Bladder Pump | <input type="checkbox"/> Bailer (Teflon®) | <input type="checkbox"/> 2" Bladder Pump | <input checked="" type="checkbox"/> Bailer (Teflon®) |
| <input checked="" type="checkbox"/> Centrifugal Pump | <input type="checkbox"/> Bailer (PVC) | <input type="checkbox"/> DDL Sampler | <input type="checkbox"/> Bailer (Stainless Steel) |
| <input type="checkbox"/> Submersible Pump | <input type="checkbox"/> Bailer (Stainless Steel) | <input type="checkbox"/> Dipper | <input type="checkbox"/> Submersible Pump |
| <input type="checkbox"/> Well Wizard™ | <input type="checkbox"/> Dedicated | <input type="checkbox"/> Well Wizard™ | <input type="checkbox"/> Dedicated |
| Other: _____ | | Other: _____ | |

WELL INTEGRITY: OK LOCK #: 2265

REMARKS: _____

Meter Calibration: Date: _____ Time: _____ Meter Serial #: _____ Temperature °F: _____
(EC 1000 _____ / _____) (DI _____) (pH 7 _____ / _____) (pH 10 _____ / _____) (pH 4 _____ / _____)
Location of previous calibration: AR-1

Signature: J. Williams Reviewed By: JB Page 5 of 6



EMCON ASSOCIATES

WATER SAMPLE FIELD DATA SHEET

Rev. 2, 5/91

PROJECT NO: G 70-5201

SAMPLE ID: AR-2

PURGED BY: J. Williams

CLIENT NAME: Acc 2169

SAMPLED BY: J. Williams

LOCATION: OAKLAND CA

TYPE: Ground Water Surface Water _____ Treatment Effluent _____ Other _____

CASING DIAMETER (Inches): 2 _____ 3 _____ 4 4.5 _____ 6 _____ Other _____

CASING ELEVATION (feet/MSL): <u>NA</u>	VOLUME IN CASING (gal.): <u>10.5</u>
DEPTH TO WATER (feet): <u>13.14</u>	CALCULATED PURGE (gal.): <u>52.6</u>
DEPTH OF WELL (feet): <u>29.2</u>	ACTUAL PURGE VOL (gal.): <u>53</u>

DATE PURGED: <u>7.17.92</u>	Start (2400 Hr) <u>1505</u>	End (2400 Hr) <u>1521</u>
DATE SAMPLED: <u>7.17-92</u>	Start (2400 Hr) <u>1524</u>	End (2400 Hr) <u>1526</u>

TIME (2400 Hr)	VOLUME (gal.)	pH (units)	EC. (umhos/cm @ 25° C)	TEMPERATURE (°F)	COLOR (visual)	TURBIDITY (visual)
<u>15:05</u>	<u>10.5</u>	<u>7.63</u>	<u>985</u>	<u>73.5</u>	<u>GRAY</u>	<u>HEAVY</u>
<u>1511</u>	<u>21.0</u>	<u>7.17</u>	<u>1024</u>	<u>70.5</u>	<u>"</u>	<u>"</u>
<u>1514</u>	<u>31.5</u>	<u>7.05</u>	<u>1184</u>	<u>69.5</u>	<u>"</u>	<u>"</u>
<u>1519</u>	<u>42.0</u>	<u>7.01</u>	<u>1189</u>	<u>69.6</u>	<u>"</u>	<u>"</u>
<u>1521</u>	<u>52.5</u>	<u>7.01</u>	<u>1190</u>	<u>70.7</u>	<u>"</u>	<u>"</u>

D. O. (ppm): NR ODOR: Slight NR (COBALT 0 - 100) NR (NTU 0 - 200)

FIELD QC SAMPLES COLLECTED AT THIS WELL (i.e. FB-1, XDUP-1): NR

PURGING EQUIPMENT

SAMPLING EQUIPMENT

- | | | | |
|--|---|--|--|
| <input checked="" type="checkbox"/> 2" Bladder Pump | <input type="checkbox"/> Bailer (Teflon®) | <input type="checkbox"/> 2" Bladder Pump | <input checked="" type="checkbox"/> Bailer (Teflon®) |
| <input checked="" type="checkbox"/> Centrifugal Pump | <input type="checkbox"/> Bailer (PVC) | <input type="checkbox"/> DDL Sampler | <input type="checkbox"/> Bailer (Stainless Steel) |
| <input type="checkbox"/> Submersible Pump | <input type="checkbox"/> Bailer (Stainless Steel) | <input type="checkbox"/> Dipper | <input type="checkbox"/> Submersible Pump |
| <input type="checkbox"/> Well Wizard™ | <input type="checkbox"/> Dedicated | <input type="checkbox"/> Well Wizard™ | <input type="checkbox"/> Dedicated |
| Other: _____ | | Other: _____ | |

WELL INTEGRITY: OK LOCK #: NO LOCK

REMARKS: _____

Meter Calibration: Date: _____ Time: _____ Meter Serial #: _____ Temperature °F: _____
 (EC 1000 _____ / _____) (DI _____) (pH 7 _____ / _____) (pH 10 _____ / _____) (pH 4 _____ / _____)
 Location of previous calibration: ITC

Signature: [Signature] Reviewed By: JB Page 6 of 6