

May 23, 2000

Susan Hugo
Alameda County Health Care Services Agency
1131 Harbor Bay Parkway, Suite 250
Alameda, California 94502-6577

Re: **First Quarter 2000 Monitoring Report**
Former Shell Service Station
2800 Telegraph Avenue
Oakland, California
Incident #97093398
Cambria Project #242-1507-002



Dear Ms. Hugo:

On behalf of Equiva Services LLC, Cambria Environmental Technology, Inc. (Cambria) is submitting this groundwater monitoring report in accordance with the reporting requirements of 23 CCR 2652d.

FIRST QUARTER 2000 ACTIVITIES

Groundwater Monitoring: Blaine Tech Services, Inc. (Blaine) of San Jose, California gauged and sampled the site wells, calculated groundwater elevations and compiled the analytical data. Cambria prepared a groundwater elevation contour map (Figure 1). Blaine's report, presenting the laboratory report and supporting field documents, is included as Attachment A.

Request for Reduction in Groundwater Sampling: Based on the low to non-detectable dissolved-phase concentrations of hydrocarbons at the site, Cambria respectfully requests the following revised groundwater sampling schedule:

- S-1: Sample annually in the first quarter;
- S-4: Sample annually in the first quarter;
- S-5: Sample annually in the first quarter;
- S-6: Sample semi-annually in the first and third quarters;
- S-8: Sample semi-annually in the first and third quarters;
- S-10: Sample annually in the first quarter; and
- SR-1: Sample annually in the first quarter.

Oakland, CA
San Ramon, CA
Sonoma, CA
Portland, OR

**Cambria
Environmental
Technology, Inc.**

1144 65th Street
Suite B
Oakland, CA 94608
Tel (510) 420-0700
Fax (510) 420-9170

ANTICIPATED SECOND QUARTER 2000 ACTIVITIES

Groundwater Monitoring: Blaine will gauge all wells and tabulate the data. If approved, Cambria will implement the above proposed schedule. Cambria will prepare a monitoring report.

CLOSING



We appreciate the opportunity to work with you on this project. Please call Stephan Bork at (510) 420-3344 if you have any questions or comments.

Sincerely,
Cambria Environmental Technology, Inc

Anni Kreml
Senior Staff Scientist

Stephan Bork, CEG, CHG.
Associate Hydrogeologist

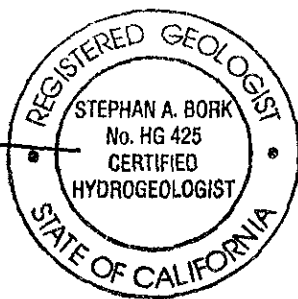
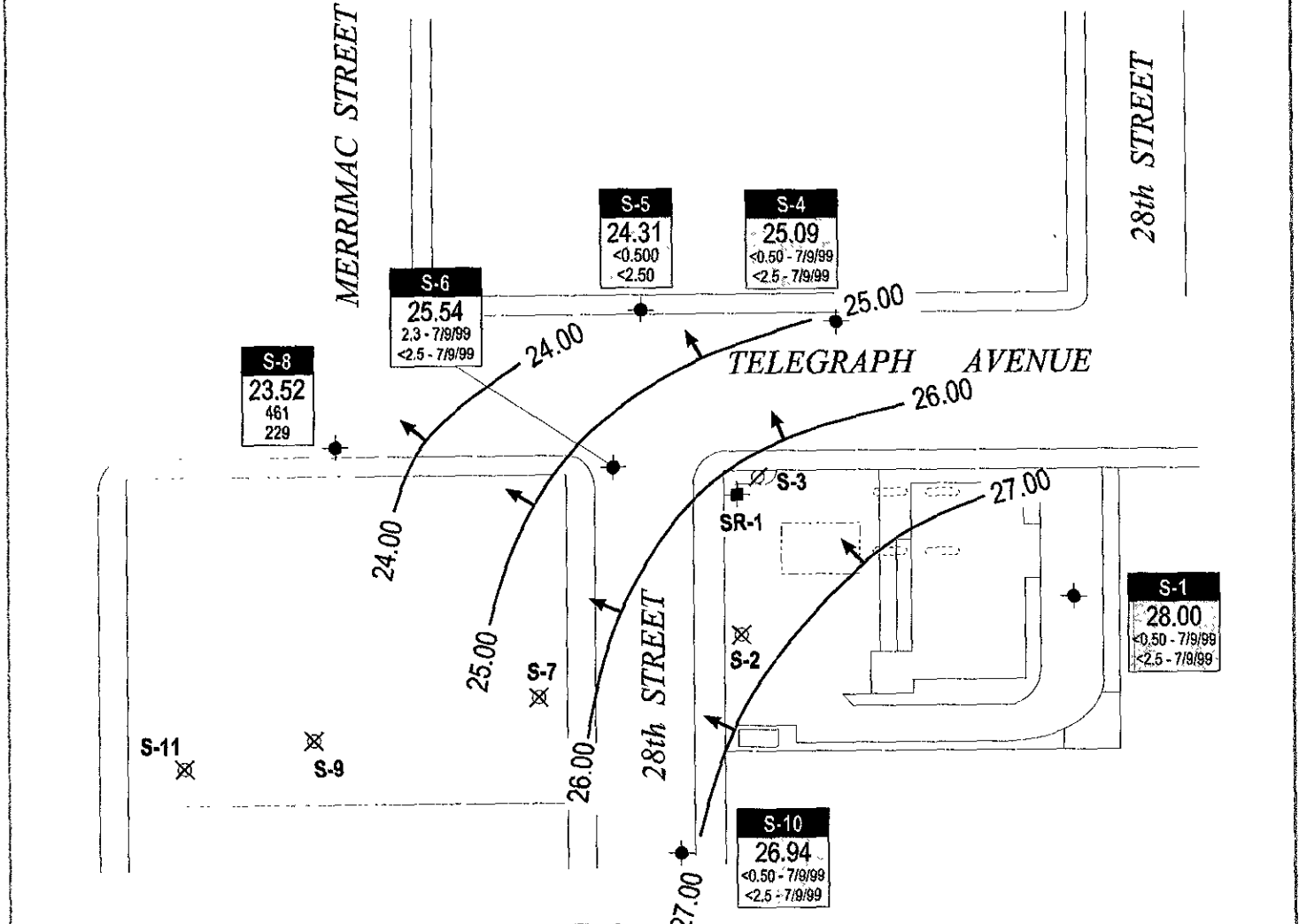


Figure: 1 - Groundwater Elevation Contour Map

Attachment: A - Blaine Groundwater Monitoring Report and Field Notes

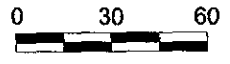
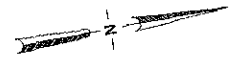
cc: Karen Petryna, Equiva Services LLC, P.O. Box 7869, Burbank, California 94510-7869
Adlai M. Karim, 2800 Telegraph Ave., Oakland, CA 94705



EXPLANATION

- S-1 ● Monitoring well location
- S-2 ✕ Destroyed monitoring well location
- S-3 ∅ Monitoring well; paved over
- SR-1 ■ Recovery well location
- Groundwater flow direction
- XX.XX Groundwater elevation contour, in feet above mean sea level (msl), approximately located; dashed where inferred

Well	Well designation
ELEV	Groundwater elevation, in feet above msl
Benzene	Benzene and MTBE concentrations are in parts per billion and are analyzed by EPA Method 8020
MTBE	



Scale (ft)

FIGURE

1

Base map taken from Weiss Associates Site Map

D:\OAKLAND\2800TELEGRAPH\FIGURES\10NGO-MP.DWG

Former Shell Service Station

2800 Telegraph Avenue
 Oakland, California
 Incident #97093398



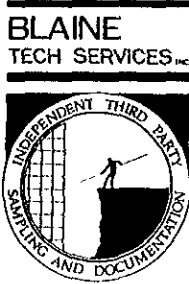
C A M B R I A

Groundwater Elevation Contour Map

March 7, 2000

ATTACHMENT A

Blaine Groundwater Monitoring Report
and Field Notes



1680 ROGERS AVENUE
SAN JOSE, CA 95112-1105
(408) 573-7771 FAX
(408) 573-0555 PHONE
CONTRACTOR'S LICENSE #746684
www.blainetech.com

May 15, 2000

Karen Petryna
Equiva Services LLC
P.O. Box 7869
Burbank, CA 91510-7869

First Quarter 2000 Groundwater Monitoring at
Former Shell Service Station
2800 Telegraph Avenue
Oakland, CA

Monitoring performed on March 7, 2000

Groundwater Monitoring Report 000307-S-1

This report covers the routine monitoring of groundwater wells at this Former Shell facility. In accordance with standard procedures that conform to Regional Water Quality Control Board requirements, routine field data collection includes depth to water, total well depth, thickness of any separate immiscible layer, water column volume, calculated purge volume (if applicable), elapsed evacuation time (if applicable), total volume of water removed (if applicable), and standard water parameter instrument readings. Sample material is collected, contained, stored, and transported to the laboratory in conformance with EPA standards. Purge water (if applicable) is, likewise, collected and transported to the Martinez Refining Company.

Basic field information is presented alongside analytical values excerpted from the laboratory report in the cumulative table of **WELL CONCENTRATIONS**. The full analytical report for the most recent samples and the field data sheets are attached to this report.

At a minimum, Blaine Tech Services, Inc. field personnel are certified on completion of a forty hour Hazardous Materials and Emergency Response training course per 29 CFR 1910.120. Field personnel are also enrolled in annual eight hour refresher courses.

Blaine Tech Services, Inc. conducts sampling and documentation assignments of this type as an independent third party. In order to avoid compromising the objectivity necessary for the proper and disinterested performance of this work, Blaine Tech Services, Inc. concentrates on objective data collection and does not participate in the interpretation of analytical results, the definition of geological or hydrological conditions, the formulation of recommendations, or the marketing of remedial systems.

Please call if you have any questions.

Yours truly,

A handwritten signature in black ink, appearing to read "Deidre Kerwin". The signature is fluid and cursive, with a long horizontal flourish extending to the right.

Deidre Kerwin
Operations Manager

DK/jt

attachments: Cumulative Table of WELL CONCENTRATIONS
Certified Analytical Report
Field Data Sheets

cc: Anni Kreml
Cambria Environmental Technology, Inc.
1144 65th Street, Suite C
Oakland, CA 94608-2411

WELL CONCENTRATIONS
Former Shell Service Station
2800 Telegraph Avenue
Oakland, CA
Wic #204-5508-2303

Well ID	Date	TPPH (ug/L)	B (ug/L)	T (ug/L)	E (ug/L)	X (ug/L)	MTBE 8020 (ug/L)	MTBE 8260 (ug/L)	TOB (MSL)	Depth to Water (ft.)	GW Elevation (MSL)	SPH Thickness (ft.)
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S-1	5/4/92	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	35.31	9.50	25.81	NA
S-1	8/10/92	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	35.31	10.85	24.46	NA
S-1	11/9/92	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	35.31	10.34	24.97	NA
S-1	2/23/93	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	35.31	7.60	27.71	NA
S-1	6/7/93	<50	2.8	1.3	0.7	3.0	NA	NA	35.31	8.63	26.68	NA
S-1	8/13/93	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	35.31	9.20	26.11	NA
S-1	11/18/93	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	35.31	10.58	24.73	NA
S-1	2/10/94	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	35.31	8.41	26.90	NA
S-1	5/3/94	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	35.31	9.09	26.22	NA
S-1	8/1/94	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	35.31	8.81	26.50	NA
S-1	11/8/94	NA	NA	NA	NA	NA	NA	NA	35.31	9.32	25.99	NA
S-1	2/3/95	NA	NA	NA	NA	NA	NA	NA	35.31	6.98	28.33	NA
S-1	8/2/95	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	35.31	9.35	25.96	NA
S-1	2/2/96	NA	NA	NA	NA	NA	NA	NA	35.31	7.45	27.86	NA
S-1	5/4/96	NA	NA	NA	NA	NA	NA	NA	35.31	8.91	26.40	NA
S-1	8/2/96	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	35.31	9.33	25.98	NA
S-1	10/2/96	NA	NA	NA	NA	NA	NA	NA	35.31	10.11	25.20	NA
S-1	1/8/97	NA	NA	NA	NA	NA	NA	NA	35.31	7.93	27.38	NA
S-1	4/17/97	NA	NA	NA	NA	NA	NA	NA	35.31	8.94	26.37	NA
S-1	7/1/97	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	35.31	9.55	25.76	NA
S-1	10/7/97	NA	NA	NA	NA	NA	NA	NA	35.31	9.43	25.88	NA
S-1	1/7/98	NA	NA	NA	NA	NA	NA	NA	35.31	8.21	27.10	NA
S-1	4/2/98	NA	NA	NA	NA	NA	NA	NA	35.31	8.27	27.04	NA

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S-1	7/2/98	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	35.31	8.97	26.34	NA
S-1	10/1/98	NA	NA	NA	NA	NA	NA	NA	35.31	9.89	25.42	NA
S-1	1/12/99	NA	NA	NA	NA	NA	NA	NA	35.31	8.45	26.86	NA
S-1	4/19/99	NA	NA	NA	NA	NA	NA	NA	35.31	9.04	26.27	NA
S-1	7/9/99	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	35.31	9.11	26.20	NA
S-1	10/6/99	NA	NA	NA	NA	NA	NA	NA	35.31	9.00	26.31	NA
S-1	3/7/00	NA	NA	NA	NA	NA	NA	NA	35.31	7.31	28.00	NA

S-2	5/4/92	1600	190	6.0	240	54	NA	NA	33.91	9.44	24.47	NA
S-2	8/10/92	<50	4.1	<0.5	<0.5	<0.5	NA	NA	33.91	10.73	23.18	NA
S-2	9/11/92	84	19	0.7	2.2	4.3	NA	NA	33.91	NA	NA	NA
S-2	11/9/92	NA	NA	NA	NA	NA	NA	NA	33.91	10.29	23.62	NA
S-2	2/23/93	16000	1600	480	850	1800	NA	NA	33.91	9.04	24.87	NA
S-2	4/8/93	Well destroyed		NA	NA	NA	NA	NA	NA	NA	NA	NA

S-3	5/4/92	NA	NA	NA	NA	NA	NA	NA	33.56	9.22	24.34	NA
S-3	8/10/92	Well paved over		NA	NA	NA	NA	NA	NA	NA	NA	NA

S-4	5/4/92	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	34.08	9.96	24.12	NA
S-4	8/10/92	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	34.08	11.32	22.76	NA
S-4	11/9/92	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	34.08	11.29	22.79	NA
S-4	2/23/93	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	34.08	9.82	24.26	NA
S-4	6/7/93	50	9.2	5.5	3.3	14	NA	NA	34.08	10.51	23.57	NA
S-4	8/13/93	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	34.08	11.05	23.03	NA

WELL CONCENTRATIONS
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S-4	11/18/93	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	34.08	11.34	22.74	NA
S-4	2/10/94	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	34.08	9.93	24.15	NA
S-4	5/3/94	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	34.08	10.40	23.68	NA
S-4	8/1/94	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	34.08	10.68	23.40	NA
S-4	11/8/94	NA	NA	NA	NA	NA	NA	NA	34.08	9.44	24.64	NA
S-4	2/3/95	NA	NA	NA	NA	NA	NA	NA	34.08	9.18	24.90	NA
S-4	8/2/95	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	34.08	10.62	23.46	NA
S-4	2/2/96	NA	NA	NA	NA	NA	NA	NA	34.08	9.23	24.85	NA
S-4	5/4/96	NA	NA	NA	NA	NA	NA	NA	34.08	10.37	23.71	NA
S-4	8/2/96	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	34.08	10.69	23.39	NA
S-4	10/2/96	NA	NA	NA	NA	NA	NA	NA	34.08	10.96	23.12	NA
S-4	1/8/97	NA	NA	NA	NA	NA	NA	NA	34.08	9.37	24.71	NA
S-4	4/17/97	NA	NA	NA	NA	NA	NA	NA	34.08	10.25	23.83	NA
S-4	7/1/97	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	34.08	10.60	23.48	NA
S-4	10/7/97	NA	NA	NA	NA	NA	NA	NA	34.08	10.52	23.56	NA
S-4	1/7/98	NA	NA	NA	NA	NA	NA	NA	34.08	9.79	24.29	NA
S-4	4/2/98	NA	NA	NA	NA	NA	NA	NA	34.08	9.56	24.52	NA
S-4	7/2/98	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	34.08	10.51	23.57	NA
S-4	10/1/98	NA	NA	NA	NA	NA	NA	NA	34.08	11.01	23.07	NA
S-4	1/12/99	NA	NA	NA	NA	NA	NA	NA	34.08	10.53	23.55	NA
S-4	4/19/99	NA	NA	NA	NA	NA	NA	NA	34.08	9.73	24.35	NA
S-4	7/9/99	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	34.08	10.48	23.60	NA
S-4	10/6/99	NA	NA	NA	NA	NA	NA	NA	34.08	10.67	23.41	NA
S-4	3/7/00	NA	NA	NA	NA	NA	NA	NA	34.08	8.99	25.09	NA

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S-5	5/4/92	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	33.42	10.27	23.15	NA
S-5	8/10/92	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	33.42	10.68	22.74	NA
S-5	11/9/92	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	33.42	10.69	22.73	NA
S-5	2/23/93	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	33.42	9.45	23.97	NA
S-5	6/7/93	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	33.42	10.23	23.19	NA
S-5	8/13/93	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	33.42	10.58	22.84	NA
S-5	11/18/93	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	33.42	10.70	22.72	NA
S-5	2/10/94	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	33.42	9.75	23.67	NA
S-5	5/3/94	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	33.42	10.19	23.23	NA
S-5	8/1/94	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	33.42	10.30	23.12	NA
S-5	11/8/94	NA	NA	NA	NA	NA	NA	NA	33.42	9.64	23.78	NA
S-5	2/3/95	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	33.42	9.59	23.83	NA
S-5	8/2/95	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	33.42	10.23	23.90	NA
S-5	2/2/96	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	33.42	9.51	23.91	NA
S-5	5/4/96	NA	NA	NA	NA	NA	NA	NA	33.42	10.15	23.27	NA
S-5	8/2/96	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	33.42	10.30	23.12	NA
S-5	10/2/96	NA	NA	NA	NA	NA	NA	NA	33.42	10.54	22.88	NA
S-5	1/8/97	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	33.42	9.56	23.86	NA
S-5	4/17/97	NA	NA	NA	NA	NA	NA	NA	33.42	10.03	23.39	NA
S-5	7/1/97	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	33.42	10.23	23.19	NA
S-5	10/7/97	NA	NA	NA	NA	NA	NA	NA	33.42	10.25	23.17	NA
S-5	1/7/98	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	33.42	9.83	23.59	NA
S-5	4/2/98	NA	NA	NA	NA	NA	NA	NA	33.42	9.73	23.69	NA

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S-5	7/2/98	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	33.42	10.04	23.38	NA
S-5	10/1/98	NA	NA	NA	NA	NA	NA	NA	33.42	10.91	22.51	NA
S-5	1/12/99	<50.0	<0.500	<0.500	<0.500	<0.500	<2.00	NA	33.42	9.80	23.62	NA
S-5	4/19/99	NA	NA	NA	NA	NA	NA	NA	33.42	9.09	24.33	NA
S-5	7/9/99	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	33.42	10.05	23.37	NA
S-5	10/6/99	NA	NA	NA	NA	NA	NA	NA	33.42	10.30	23.12	NA
S-5	3/7/00	<50.0	<0.500	<0.500	<0.500	<0.500	<2.50	NA	33.42	9.11	24.31	NA

S-6	5/4/92	3100	640	22	23	97	NA	NA	32.59	9.42	23.17	NA
S-6	8/10/92	3400	430	27	26	120	NA	NA	32.59	10.40	22.19	NA
S-6	11/9/92	2000	320	15	15	100	NA	NA	32.59	10.16	22.43	NA
S-6	2/23/93	14000	780	180	380	1300	NA	NA	32.59	7.60	24.99	NA
S-6	6/7/93	3900	1400	56	83	210	NA	NA	32.59	8.90	23.69	NA
S-6	8/13/93	4000a	890	16	<0.5	41	NA	NA	32.59	9.39	23.20	NA
S-6	11/18/93	80	5.0	<0.5	<0.5	<0.5	NA	NA	32.59	10.32	22.27	NA
S-6	2/10/94	4100	370	23	21	90	NA	NA	32.59	8.68	23.91	NA
S-6	5/3/94	4700	550	28	85	340	NA	NA	32.59	9.20	23.39	NA
S-6	8/1/94	2900	370	11	11	43	NA	NA	32.59	8.90	23.69	NA
S-6	11/8/94	NA	NA	NA	NA	NA	NA	NA	32.59	8.32	23.69	NA
S-6	2/3/95	NA	NA	NA	NA	NA	NA	NA	32.59	8.04	23.69	NA
S-6	8/2/95	1400	160	<5	<5	<5	NA	NA	32.59	9.26	23.19	NA
S-6	2/2/96	NA	NA	NA	NA	NA	NA	NA	32.59	7.90	24.69	NA
S-6	5/4/96	NA	NA	NA	NA	NA	NA	NA	32.59	8.98	23.61	NA
S-6	8/2/96	1600	150	9.2	13	23	17	NA	32.59	9.34	23.25	NA

WELL CONCENTRATIONS
Former Shell Service Station
2800 Telegraph Avenue
Oakland, CA
Wic #204-5508-2303

Well ID	Date	TPPH (ug/L)	B (ug/L)	T (ug/L)	E (ug/L)	X (ug/L)	MTBE 8020 (ug/L)	MTBE 8260 (ug/L)	TOB (MSL)	Depth to Water (ft.)	GW Elevation (MSL)	SPH Thickness (ft.)
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S-6	10/2/96	NA	NA	NA	NA	NA	NA	NA	32.59	9.96	22.63	NA
S-6	1/8/97	NA	NA	NA	NA	NA	NA	NA	32.59	7.38	25.21	NA
S-6	4/17/97	NA	NA	NA	NA	NA	NA	NA	32.59	9.16	23.43	NA
S-6	7/1/97	<50	1.5	<0.50	<0.50	<0.50	<2.5	NA	32.59	9.60	22.99	NA
S-6	10/7/97	NA	NA	NA	NA	NA	NA	NA	32.59	9.64	22.95	NA
S-6	1/7/98	NA	NA	NA	NA	NA	NA	NA	32.59	8.34	24.25	NA
S-6	4/2/98	NA	NA	NA	NA	NA	NA	NA	32.59	7.93	24.66	NA
S-6	7/2/98	370	22	0.62	<0.50	<0.50	5.60	NA	32.59	9.85	22.74	NA
S-6	10/1/98	NA	NA	NA	NA	NA	NA	NA	32.59	10.48	22.11	NA
S-6	1/12/99	NA	NA	NA	NA	NA	NA	NA	32.59	9.63	22.96	NA
S-6	4/19/99	NA	NA	NA	NA	NA	NA	NA	32.59	9.08	23.51	NA
S-6	7/9/99	52	2.3	<0.50	<0.50	<0.50	<2.5	NA	32.59	9.33	23.26	NA
S-6	10/6/99	NA	NA	NA	NA	NA	NA	NA	32.59	9.80	22.79	NA
S-6	3/7/00	NA	NA	NA	NA	NA	NA	NA	32.59	7.05	25.54	NA

S-6 (D)	8/1/94	2600	340	8.8	7.7	33	NA	NA	32.59	NA	NA	NA
S-6 (D)	8/2/95	1400	170	<5	<5	<5	NA	NA	32.59	NA	NA	NA

S-7	5/4/92	180	1.6	<0.5	1.5	3.0	NA	NA	33.33	11.21	22.12	NA
S-7	8/10/92	190	8.0	1.4	4.7	8.5	NA	NA	33.33	12.28	21.05	NA
S-7	11/9/92	280	16	4.0	7.8	21	NA	NA	33.33	11.77	21.56	NA
S-7	2/23/93	210	13	2.2	5.4	12	NA	NA	33.33	8.86	24.47	NA
S-7	6/7/93	90	1.2	2.5	1.0	<0.5	NA	NA	33.33	10.58	22.75	NA
S-7	8/13/93	140	4.0	0.8	<0.5	0.5	NA	NA	33.33	11.34	21.99	NA

WELL CONCENTRATIONS
Former Shell Service Station
2800 Telegraph Avenue
Oakland, CA
Wic #204-5508-2303

Well ID	Date	TPPH (ug/L)	B (ug/L)	T (ug/L)	E (ug/L)	X (ug/L)	MTBE 8020 (ug/L)	MTBE 8260 (ug/L)	TOB (MSL)	Depth to Water (ft.)	GW Elevation (MSL)	SPH Thickness (ft.)
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S-7	11/18/93	440	43	4.9	0.9	4.2	NA	NA	33.33	12.00	21.33	NA
S-7	2/10/94	250a	<0.5	<0.5	1.8	<0.5	NA	NA	33.33	9.88	23.45	NA
S-7	5/3/94	130	<0.5	<0.5	<0.5	<0.5	NA	NA	33.33	10.75	22.58	NA
S-7	8/1/94	250	4.8	<0.5	<0.5	<0.5	NA	NA	33.33	11.05	22.28	NA
S-7	11/8/94	NA	NA	NA	NA	NA	NA	NA	33.33	9.64	23.69	NA
S-7	2/3/95	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	33.33	8.53	24.80	NA
S-7	8/2/95	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	33.33	11.10	22.23	NA
S-7	2/2/96	480	2.2	2.4	7.9	25	NA	NA	33.33	8.58	24.75	NA
S-7	5/4/96	NA	NA	NA	NA	NA	NA	NA	33.33	10.41	22.92	NA
S-7	8/2/96	300	20	2.2	3.8	7.9	21	11	33.33	11.18	22.15	NA
S-7	10/2/96	NA	NA	NA	NA	NA	NA	NA	33.33	12.12	21.21	NA
S-7	1/8/97	850	16	6.3	20	59	<25	NA	33.33	8.23	25.10	NA
S-7	4/17/97	NA	NA	NA	NA	NA	NA	NA	33.33	10.75	22.58	NA
S-7	7/1/97	120	2.4	<0.50	2.9	2.6	3.5	NA	33.33	11.40	21.93	NA
S-7	10/7/97	NA	NA	NA	NA	NA	NA	NA	33.33	11.50	21.83	NA
S-7	4/19/99	<50.0	<0.500	<0.500	<0.500	<0.500	<5.00	NA	33.33	9.39	23.94	NA
S-7	7/9/99	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	33.33	11.15	22.18	NA
S-7	10/6/99	216	5.04	<0.500	2.23	4.82	<5.00	NA	33.33	11.65	21.68	NA
S-7	NA	Well abandoned	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA

S-7 (D)	8/2/96	340	22	2.2	4.4	8.9	20	NA	33.33	NA	NA	NA
S-7 (D)	1/8/97	840	15	<5.0	21	63	25	NA	33.33	NA	NA	NA
S-7 (D)	7/1/97	120	2.4	<0.50	2.9	2.6	<2.5	NA	33.33	NA	NA	NA

WELL CONCENTRATIONS
Former Shell Service Station
2800 Telegraph Avenue
Oakland, CA
Wic #204-5508-2303

Well ID	Date	TPPH (ug/L)	B (ug/L)	T (ug/L)	E (ug/L)	X (ug/L)	MTBE 8020 (ug/L)	MTBE 8260 (ug/L)	TOB (MSL)	Depth to Water (ft.)	GW Elevation (MSL)	SPH Thickness (ft.)
S-8	5/4/92	1600	20	420	96	330	NA	NA	31.97	10.29	21.68	NA
S-8	8/10/92	1500	19	37	60	250	NA	NA	31.97	11.12	20.85	NA
S-8	11/9/92	710	5.7	24	28	120	NA	NA	31.97	10.71	21.26	NA
S-8	2/23/93	3800	40	54	68	260	NA	NA	31.97	6.04	25.93	NA
S-8	6/7/93	1200	13	19	65	150	NA	NA	31.97	10.06	21.91	NA
S-8	8/13/93	1300	21	23	49	250	NA	NA	31.97	10.56	21.41	NA
S-8	11/18/93	870	16	5.3	59	230	NA	NA	31.97	10.90	21.07	NA
S-8	2/10/94	2400	11	55	120	530	NA	NA	31.97	9.53	22.44	NA
S-8	5/3/94	3100	12	27	130	370	NA	NA	31.97	10.06	21.91	NA
S-8	8/1/94	1500	20	18	39	190	NA	NA	31.97	10.32	21.65	NA
S-8	11/8/94	2100	22	38	73	390	NA	NA	31.97	9.25	22.72	NA
S-8	2/3/95	4800	67	39	130	300	NA	NA	31.97	8.99	22.98	NA
S-8	5/4/95	2600	31	23	71	310	NA	NA	31.97	9.22	22.75	NA
S-8	8/2/95	1700	10	9.1	48	210	NA	NA	31.97	10.36	21.61	NA
S-8	11/2/95	1200	16	13	72	130	NA	NA	31.97	10.72	21.25	NA
S-8	2/2/96	7100	29	140	360	1300	NA	NA	31.97	8.92	23.05	NA
S-8	5/4/96	3500	13	27	110	400	<25	NA	31.97	9.86	22.11	NA
S-8	8/2/96	850	9.6	7.4	30	160	11	NA	31.97	10.30	21.67	NA
S-8	10/2/96	980	<5.0	11	13	92	<25	NA	31.97	10.71	21.26	NA
S-8	1/8/97	6400	88	48	190	500	<100	NA	31.97	8.88	23.09	NA
S-8	4/17/97	1700	23	7.4	34	50	74	NA	31.97	10.00	21.97	NA
S-8	7/1/97	140	2.8	<0.50	<0.50	0.58	<2.5	NA	31.97	10.40	21.57	NA
S-8	10/7/97	300	2.7	0.63	4.6	8.4	<2.5	NA	31.97	10.50	21.47	NA
S-8	1/7/98	110	1.2	<0.50	<0.50	1.6	<2.5	NA	31.97	9.27	22.70	NA

WELL CONCENTRATIONS
Former Shell Service Station
2800 Telegraph Avenue
Oakland, CA
Wic #204-5508-2303

Well ID	Date	TPPH (ug/L)	B (ug/L)	T (ug/L)	E (ug/L)	X (ug/L)	MTBE 8020 (ug/L)	MTBE 8260 (ug/L)	TOB (MSL)	Depth to Water (ft.)	GW Elevation (MSL)	SPH Thickness (ft.)
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S-8	4/2/98	4500	140	77	140	380	<12	NA	31.97	9.31	22.66	NA
S-8	7/2/98	330	4.2	0.79	1.7	2.3	4.8	NA	31.97	9.48	22.49	NA
S-8	10/1/98	52	0.76	<0.50	<0.50	0.70	<2.5	NA	31.97	10.08	21.89	NA
S-8	1/12/99	<50.0	<0.500	<0.500	<0.500	<0.500	<2.00	NA	31.97	10.50	21.47	NA
S-8	4/19/99	3360	29.6	24.6	137	398	<100	NA	31.97	9.45	22.52	NA
S-8	7/9/99	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	31.97	10.25	21.72	NA
S-8	10/6/99	<50.0	<0.500	<0.500	<0.500	<0.500	<5.00	NA	31.97	10.70	21.27	NA
S-8	3/7/00	16500	461	397	665	1240	229	NA	31.97	8.45	23.52	NA

S-8 (D)	2/10/94	2400	11	46	100	440	NA	NA	31.97	NA	NA	NA
S-8 (D)	5/3/94	3000	21	25	120	340	NA	NA	31.97	NA	NA	NA
S-8 (D)	11/8/94	2100	20	31	75	390	NA	NA	31.97	NA	NA	NA
S-8 (D)	2/3/95	3700	53	30	100	240	NA	NA	31.97	NA	NA	NA
S-8 (D)	5/4/95	3300	38	26	89	390	NA	NA	31.97	NA	NA	NA
S-8 (D)	8/2/95	1200	15	13	70	120	NA	NA	31.97	NA	NA	NA
S-8 (D)	2/2/96	7800	33	160	400	1500	NA	NA	31.97	NA	NA	NA
S-8 (D)	5/4/96	5100	19	37	190	690	<25	NA	31.97	NA	NA	NA
S-8 (D)	10/2/96	1300	<5.0	10	28	180	<25	NA	31.97	NA	NA	NA
S-8 (D)	4/17/97	1600	25	7.4	30	43	34	NA	31.97	NA	NA	NA
S-8 (D)	1/7/98	150	1.8	0.6	<0.50	2.2	<2.5	NA	31.97	NA	NA	NA
S-8 (D)	7/2/98	360	4.3	0.89	1.7	2.3	5.7	NA	31.97	NA	NA	NA

S-9	5/4/92	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	31.86	10.45	21.41	NA
S-9	8/10/92	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	31.86	11.52	20.34	NA

WELL CONCENTRATIONS
Former Shell Service Station
2800 Telegraph Avenue
Oakland, CA
Wic #204-5508-2303

Well ID	Date	TPPH (ug/L)	B (ug/L)	T (ug/L)	E (ug/L)	X (ug/L)	MTBE 8020 (ug/L)	MTBE 8260 (ug/L)	TOB (MSL)	Depth to Water (ft.)	GW Elevation (MSL)	SPH Thickness (ft.)
S-9	11/9/92	<50	<0.5	<0.5	<0.5	0.7	NA	NA	31.86	11.02	20.84	NA
S-9	2/23/93	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	31.86	8.00	23.86	NA
S-9	6/7/93	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	31.86	10.07	21.79	NA
S-9	8/13/93	140	<0.5	<0.5	<0.5	<0.5	NA	NA	31.86	10.92	20.94	NA
S-9	11/18/93	170	<0.5	<0.5	<0.5	<0.5	NA	NA	31.86	11.19	20.67	NA
S-9	2/10/94	140	<0.5	<0.5	<0.5	<0.5	NA	NA	31.86	9.16	22.70	NA
S-9	5/3/94	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	31.86	10.03	21.83	NA
S-9	8/1/94	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	31.86	10.52	21.34	NA
S-9	11/8/94	NA	NA	NA	NA	NA	NA	NA	31.86	9.08	22.78	NA
S-9	2/3/95	NA	NA	NA	NA	NA	NA	NA	31.86	8.37	23.49	NA
S-9	8/2/95	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	31.86	9.35	22.51	NA
S-9	2/2/96	NA	NA	NA	NA	NA	NA	NA	31.86	7.53	24.33	NA
S-9	5/4/96	NA	NA	NA	NA	NA	NA	NA	31.86	9.60	22.26	NA
S-9	8/2/96	<50	<0.50	<0.50	<0.50	<0.50	12	NA	31.86	10.46	21.40	NA
S-9	10/2/96	NA	NA	NA	NA	NA	NA	NA	31.86	10.66	21.20	NA
S-9	1/8/97	NA	NA	NA	NA	NA	NA	NA	31.86	7.20	24.66	NA
S-9	4/17/97	NA	NA	NA	NA	NA	NA	NA	31.86	9.96	21.90	NA
S-9	7/1/97	<50	<0.50	<0.50	<0.50	<0.50	3.9	NA	31.86	10.64	21.22	NA
S-9	10/7/97	NA	NA	NA	NA	NA	NA	NA	31.86	10.63	21.23	NA
S-9	4/19/99	<50.0	<0.500	<0.500	<0.500	<0.500	<5.00	NA	31.86	8.69	23.17	NA
S-9	7/9/99	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	31.86	10.45	21.41	NA
S-9	10/6/99	<50.0	<0.500	<0.500	<0.500	<0.500	<5.00	NA	31.86	10.90	20.96	NA
S-9	NA	Well abandoned	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA

WELL CONCENTRATIONS
Former Shell Service Station
2800 Telegraph Avenue
Oakland, CA
Wic #204-5508-2303

Well ID	Date	TPPH (ug/L)	B (ug/L)	T (ug/L)	E (ug/L)	X (ug/L)	MTBE 8020 (ug/L)	MTBE 8260 (ug/L)	TOB (MSL)	Depth to Water (ft.)	GW Elevation (MSL)	SPH Thickness (ft.)
S-10	5/4/92	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	32.95	8.54	24.41	NA
S-10	8/10/92	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	32.95	10.43	22.52	NA
S-10	11/9/92	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	32.95	9.14	23.81	NA
S-10	2/23/93	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	32.95	6.72	26.23	NA
S-10	6/7/93	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	32.95	8.08	24.87	NA
S-10	8/13/93	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	32.95	8.83	24.12	NA
S-10	11/18/93	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	32.95	9.46	23.49	NA
S-10	2/10/94	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	32.95	7.41	25.54	NA
S-10	5/3/94	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	32.95	8.16	24.79	NA
S-10	8/1/94	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	32.95	8.29	24.66	NA
S-10	11/8/94	NA	NA	NA	NA	NA	NA	NA	32.95	7.02	25.93	NA
S-10	2/3/95	NA	NA	NA	NA	NA	NA	NA	32.95	6.79	26.16	NA
S-10	8/2/95	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	32.95	8.30	24.65	NA
S-10	2/2/96	NA	NA	NA	NA	NA	NA	NA	32.95	6.49	26.46	NA
S-10	5/4/96	NA	NA	NA	NA	NA	NA	NA	32.95	7.55	25.40	NA
S-10	8/2/96	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	32.95	9.25	23.70	NA
S-10	10/2/96	NA	NA	NA	NA	NA	NA	NA	32.95	10.54	22.41	NA
S-10	1/8/97	NA	NA	NA	NA	NA	NA	NA	32.95	6.47	26.48	NA
S-10	4/17/97	NA	NA	NA	NA	NA	NA	NA	32.95	7.78	25.17	NA
S-10	7/1/97	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	32.95	8.83	24.12	NA
S-10	10/7/97	NA	NA	NA	NA	NA	NA	NA	32.95	8.89	24.06	NA
S-10	1/7/98	NA	NA	NA	NA	NA	NA	NA	32.95	6.97	25.98	NA
S-10	4/2/98	NA	NA	NA	NA	NA	NA	NA	32.95	6.96	25.99	NA
S-10	7/2/98	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	32.95	10.41	22.54	NA

WELL CONCENTRATIONS
Former Shell Service Station
2800 Telegraph Avenue
Oakland, CA
Wic #204-5508-2303

Well ID	Date	TPPH (ug/L)	B (ug/L)	T (ug/L)	E (ug/L)	X (ug/L)	MTBE 8020 (ug/L)	MTBE 8260 (ug/L)	TOB (MSL)	Depth to Water (ft.)	GW Elevation (MSL)	SPH Thickness (ft.)
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S-10	10/1/98	NA	NA	NA	NA	NA	NA	NA	32.95	11.03	21.92	NA
S-10	1/12/99	NA	NA	NA	NA	NA	NA	NA	32.95	10.33	22.62	NA
S-10	4/19/99	NA	NA	NA	NA	NA	NA	NA	32.95	9.72	23.23	NA
S-10	7/9/99	<50	<0.50	<0.50	<0.50	<0.50	<2.5	NA	32.95	8.98	23.97	NA
S-10	10/6/99	NA	NA	NA	NA	NA	NA	NA	32.95	9.15	23.80	NA
S-10	3/7/00	NA	NA	NA	NA	NA	NA	NA	32.95	6.01	26.94	NA

S-11	5/4/92	1500	55	32	57	190	NA	NA	30.78	9.99	20.79	NA
S-11	8/10/92	750	29	13	43	120	NA	NA	30.78	10.92	19.86	NA
S-11	11/9/92	4100	32	62	120	1100	NA	NA	30.78	10.44	20.34	NA
S-11	2/23/93	760	15	13	37	140	NA	NA	30.78	7.30	23.48	NA
S-11	6/7/93	1700	40	16	100	360	NA	NA	30.78	9.51	21.27	NA
S-11	8/13/93	60	0.9	<0.5	0.8	1.2	NA	NA	30.78	10.39	20.39	NA
S-11	11/18/93	150	7.8	1.0	9.0	12	NA	NA	30.78	10.64	20.14	NA
S-11	2/10/94	4400	53	19	160	390	NA	NA	30.78	8.50	22.28	NA
S-11	5/3/94	65	1.5	<0.5	0.53	0.59	NA	NA	30.78	9.42	21.36	NA
S-11	8/1/94	240	18	6.7	6.9	18	NA	NA	30.78	10.12	20.66	NA
S-11	11/8/94	490	14	5.2	15	47	NA	NA	30.78	8.84	21.94	NA
S-11	2/3/95	380	4.1	0.9	1.4	5.1	NA	NA	30.78	7.12	23.66	NA
S-11	5/4/95	110	1.3	<0.5	1.1	1.8	NA	NA	30.78	7.96	22.82	NA
S-11	8/2/95	230	22	11	13	35	NA	NA	30.78	9.88	20.90	NA
S-11	11/2/95	200	26	10	10	30	NA	NA	30.78	10.10	20.68	NA
S-11	2/2/96	110	2.9	1.0	2.6	6.5	NA	NA	30.78	7.33	23.45	NA
S-11	5/4/96	<50	0.70	0.54	0.82	2.6	7.5	NA	30.78	8.62	22.16	NA

WELL CONCENTRATIONS
Former Shell Service Station
2800 Telegraph Avenue
Oakland, CA
Wic #204-5508-2303

Well ID	Date	TPPH (ug/L)	B (ug/L)	T (ug/L)	E (ug/L)	X (ug/L)	MTBE 8020 (ug/L)	MTBE 8260 (ug/L)	TOB (MSL)	Depth to Water (ft.)	GW Elevation (MSL)	SPH Thickness (ft.)
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S-11	8/2/96	200	11	4.6	12	38	10	NA	30.78	9.85	20.93	NA
S-11	10/2/96	290	20	6.2	16	48	8.4	NA	30.78	11.00	19.78	NA
S-11	1/8/97	56	2.0	<0.50	1.0	5.8	5.2	NA	30.78	6.20	24.58	NA
S-11	4/17/97	<50	0.88	<0.50	<0.50	<0.50	3.2	NA	30.78	8.81	21.97	NA
S-11	7/1/97	610	50	5.9	24	110	3.1	NA	30.78	10.47	20.31	NA
S-11	10/7/97	440	43	3.0	13	110	4.9	NA	30.78	10.32	20.46	NA
S-11	4/19/99	<50.0	0.530	<0.500	<0.500	5.22	<5.00	NA	30.78	8.31	22.47	NA
S-11	7/9/99	53	2.3	<0.50	<0.50	8.5	<2.5	NA	30.78	9.19	21.59	NA
S-11	10/6/99	1210	39.1	<10.0	26.4	139	<100	NA	30.78	10.25	20.53	NA
S-11	NA	Well Abandoned	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA

S-11 (D)	6/7/93	1600	51	16	83	300	NA	NA	30.78	NA	NA	NA
S-11 (D)	8/13/93	70	2.1	<0.5	0.9	2.1	NA	NA	30.78	NA	NA	NA
S-11 (D)	10/7/97	360	39	2.0	7.2	74	4.9	NA	30.78	NA	NA	NA

SR-1	5/4/92	NA	NA	NA	NA	NA	NA	NA	NA	9.02	NA	NA
SR-1	8/10/92	NA	NA	NA	NA	NA	NA	NA	NA	10.29	NA	NA
SR-1	11/9/92	NA	NA	NA	NA	NA	NA	NA	NA	10.92	NA	NA
SR-1	2/22/93	NA	NA	NA	NA	NA	NA	NA	NA	6.64	NA	NA
SR-1	6/7/93	NA	NA	NA	NA	NA	NA	NA	NA	7.36	NA	NA
SR-1	8/13/93	NA	NA	NA	NA	NA	NA	NA	NA	7.96	NA	NA
SR-1	11/18/93	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	NA	10.02	NA	NA
SR-1	2/10/94	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
SR-1	5/3/94	NA	NA	NA	NA	NA	NA	NA	NA	8.28	NA	NA

WELL CONCENTRATIONS
Former Shell Service Station
2800 Telegraph Avenue
Oakland, CA
Wic #204-5508-2303

Well ID	Date	TPPH (ug/L)	B (ug/L)	T (ug/L)	E (ug/L)	X (ug/L)	MTBE 8020 (ug/L)	MTBE 8260 (ug/L)	TOB (MSL)	Depth to Water (ft.)	GW Elevation (MSL)	SPH Thickness (ft.)
SR-1	8/1/94	NA	NA	NA	NA	NA	NA	NA	NA	7.98	NA	NA
SR-1	11/8/94	NA	NA	NA	NA	NA	NA	NA	NA	7.75	NA	NA
SR-1	2/3/95	NA	NA	NA	NA	NA	NA	NA	NA	7.20	NA	NA
SR-1	5/4/95	NA	NA	NA	NA	NA	NA	NA	NA	4.10	NA	NA
SR-1	8/2/95	NA	NA	NA	NA	NA	NA	NA	NA	5.31	NA	NA
SR-1	11/2/95	NA	NA	NA	NA	NA	NA	NA	NA	10.62	NA	NA
SR-1	2/2/96	90	6.1	6.7	2.8	8.5	NA	NA	NA	7.30	NA	NA
SR-1	5/4/96	NA	NA	NA	NA	NA	NA	NA	NA	8.10	NA	NA
SR-1	8/2/96	NA	NA	NA	NA	NA	NA	NA	NA	8.10	NA	NA
SR-1	10/2/96	NA	NA	NA	NA	NA	NA	NA	NA	9.25	NA	NA
SR-1	1/8/97	NA	NA	NA	NA	NA	NA	NA	NA	7.18	NA	NA
SR-1	4/17/97	NA	NA	NA	NA	NA	NA	NA	NA	6.01	NA	NA
SR-1	7/1/97	NA	NA	NA	NA	NA	NA	NA	NA	8.36	NA	NA
SR-1	10/7/97	NA	NA	NA	NA	NA	NA	NA	NA	9.22	NA	NA
SR-1	1/7/98	NA	NA	NA	NA	NA	NA	NA	NA	7.45	NA	NA
SR-1	4/2/98	NA	NA	NA	NA	NA	NA	NA	NA	7.43	NA	NA
SR-1	7/2/98	NA	NA	NA	NA	NA	NA	NA	NA	9.87	NA	NA
SR-1	10/1/98	NA	NA	NA	NA	NA	NA	NA	NA	10.42	NA	NA
SR-1	1/12/99	NA	NA	NA	NA	NA	NA	NA	NA	10.24	NA	NA
SR-1	4/19/99	NA	NA	NA	NA	NA	NA	NA	NA	9.64	NA	NA
SR-1	7/9/99	NA	NA	NA	NA	NA	NA	NA	NA	8.40	NA	NA
SR-1	10/6/99	NA	NA	NA	NA	NA	NA	NA	NA	9.30	NA	NA
SR-1	3/7/00	NA	NA	NA	NA	NA	NA	NA	NA	5.25	NA	NA

WELL CONCENTRATIONS
Former Shell Service Station
2800 Telegraph Avenue
Oakland, CA
Wic #204-5508-2303

Well ID	Date	TPPH (ug/L)	B (ug/L)	T (ug/L)	E (ug/L)	X (ug/L)	MTBE 8020 (ug/L)	MTBE 8260 (ug/L)	TOB (MSL)	Depth to Water (ft.)	GW Elevation (MSL)	SPH Thickness (ft.)
SR-1 (D)	11/18/93	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	NA	NA	NA	NA

Abbreviations:

TPPH= Total petroleum hydrocarbons as gasoline by modified EPA Method 8015

BTEX = benzene, toluene, ethylbenzene, xylenes by EPA Method 8020

MTBE = methyl-tertiary-butyl ether

TOB = Top of Wellbox Elevation

SPH = Separate-Phase Hydrocarbons

GW = Groundwater

ug/L = parts per billion

msl = Mean sea level

ft = Feet

<n = Below detection limit

D = Duplicate sample

NA = Not applicable

Notes:

a = Chromatogram pattern indicated the presence of an unidentified hydrocarbon.



March 21, 2000

Nick Sudano
Blaine Tech Services (Shell)
1680 Rogers Avenue
San Jose, CA 95112

RE: Equiva 2800 Telegraph Avenue, Oakland

Dear Nick Sudano

Enclosed are the results of analyses for sample(s) received by the laboratory on March 8, 2000. If you have any questions concerning this report, please feel free to contact me.

Sincerely,

Kayvan Kimyai
Project Manager D.M.

CA ELAP Certificate Number 1210





Blaine Tech Services (Shell) 1680 Rogers Avenue San Jose, CA 95112	Project: Equiva Project Number: 2800 Telegraph Ave. Project Manager: Nick Sudano	Sampled: 3/7/00 Received: 3/8/00 Reported: 3/21/00 17:40
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ANALYTICAL REPORT FOR SAMPLES:

Sample Description	Laboratory Sample Number	Sample Matrix	Date Sampled
S-5	MJC0317-01	Water	3/7/00
S-8	MJC0317-02	Water	3/7/00



Blaine Tech Services (Shell) 1680 Rogers Avenue San Jose, CA 95112	Project: Equiva Project Number: 2800 Telegraph Ave. Project Manager: Nick Sudano	Sampled: 3/7/00 Received: 3/8/00 Reported: 3/21/00 17:40
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**Total Purgeable Hydrocarbons (C6-C12), BTEX and MTBE by DHS LUFT
Sequoia Analytical - Morgan Hill**

Analyte	Batch Number	Date Prepared	Date Analyzed	Specific Method	Reporting Limit	Result	Units	Notes*
				<u>MJC0317-01</u>				
S-5							<u>Water</u>	
Purgeable Hydrocarbons	0C20004	3/20/00	3/20/00	DHS LUFT	50.0	ND	ug/l	
Benzene	"	"	"	DHS LUFT	0.500	ND	"	
Toluene	"	"	"	DHS LUFT	0.500	ND	"	
Ethylbenzene	"	"	"	DHS LUFT	0.500	ND	"	
Xylenes (total)	"	"	"	DHS LUFT	0.500	ND	"	
Methyl tert-butyl ether	"	"	"	DHS LUFT	2.50	ND	"	
Surrogate: a,a,a-Trifluorotoluene	"	"	"	70-130		95.2	%	
				<u>MJC0317-02</u>				
S-8							<u>Water</u>	
Purgeable Hydrocarbons	0C20004	3/20/00	3/20/00	DHS LUFT	1000	16500	ug/l	P-01
Benzene	"	"	"	DHS LUFT	10.0	461	"	
Toluene	"	"	"	DHS LUFT	10.0	397	"	
Ethylbenzene	"	"	"	DHS LUFT	10.0	665	"	
Xylenes (total)	"	"	"	DHS LUFT	10.0	1240	"	
Methyl tert-butyl ether	"	"	"	DHS LUFT	50.0	229	"	
Surrogate a,a,a-Trifluorotoluene	"	"	"	70-130		113	%	



Blaine Tech Services (Shell) 1680 Rogers Avenue San Jose, CA 95112	Project: Equiva Project Number: 2800 Telegraph Ave. Project Manager: Nick Sudano	Sampled: 3/7/00 Received: 3/8/00 Reported: 3/21/00 17:40
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Total Purgeable Hydrocarbons (C6-C12), BTEX and MTBE by DHS LUFT/Quality Control
Sequoia Analytical - Morgan Hill

Analyte	Date Analyzed	Spike Level	Sample Result	QC Result	Reporting Limit Units	Recov. Limits	Recov. %	RPD Limit	RPD %	Notes*
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Batch: 0C20004 **Date Prepared: 3/20/00** **Extraction Method: EPA 5030B [P/T]**

Blank										
0C20004-BLK1										
Purgeable Hydrocarbons	3/20/00			ND	ug/l	50.0				
Benzene	"			ND	"	0.500				
Toluene	"			ND	"	0.500				
Ethylbenzene	"			ND	"	0.500				
Xylenes (total)	"			ND	"	0.500				
Methyl tert-butyl ether	"			ND	"	2.50				
Surrogate: a,a,a-Trifluorotoluene	"	10.0		10.1	"	70-130	101			

LCS										
0C20004-BS1										
Benzene	3/20/00	10.0		10.9	ug/l	70-130	109			
Toluene	"	10.0		9.88	"	70-130	98.8			
Ethylbenzene	"	10.0		9.25	"	70-130	92.5			
Xylenes (total)	"	30.0		28.3	"	70-130	94.3			
Surrogate: a,a,a-Trifluorotoluene	"	10.0		10.3	"	70-130	103			

LCS Dup										
0C20004-BSD1										
Benzene	3/20/00	10.0		11.0	ug/l	70-130	110	25	0.913	
Toluene	"	10.0		9.35	"	70-130	93.5	25	5.51	
Ethylbenzene	"	10.0		8.61	"	70-130	86.1	25	7.17	
Xylenes (total)	"	30.0		27.5	"	70-130	91.7	25	2.87	
Surrogate: a,a,a-Trifluorotoluene	"	10.0		10.4	"	70-130	104			



Blaine Tech Services (Shell) 1680 Rogers Avenue San Jose, CA 95112	Project: Equiva Project Number: 2800 Telegraph Ave. Project Manager: Nick Sudano	Sampled: 3/7/00 Received: 3/8/00 Reported: 3/21/00 17:40
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Notes and Definitions

#	Note
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- P-01 Chromatogram Pattern: Gasoline C6-C12
- DET Analyte DETECTED
- ND Analyte NOT DETECTED at or above the reporting limit
- NR Not Reported
- dry Sample results reported on a dry weight basis
- Recov. Recovery
- RPD Relative Percent Difference



BLAINE

TECH SERVICES INC.

1680 ROGERS AVENUE
SAN JOSE, CALIFORNIA 95112-1105
FAX (408) 573-7771
PHONE (408) 573-0555

CHAIN OF CUSTODY
000307-51

CLIENT
Equiva - Karen Petryna

SITE
2800 Telegraph Avenue
Oakland, CA

SAMPLE I.D.	S = SOIL W = H2O	CONTAINERS	
		TOTAL	
S-5	W	3	
S-8	W	3	

C = COMPOSITE ALL CONTAINERS

CONDUCT ANALYSIS TO DETECT					
TPH - gas, BTEX	MTBE by 8020	MTBE by 8260	TPH - diesel	Oxygenates by 8260	1,2-DCA & EDB by 8010
X					
X					

LAB SEQUOIA DHS #

ALL ANALYSES MUST MEET SPECIFICATIONS AND DETECTION LIMITS SET BY CALIFORNIA DHS AND

EPA RWQCB REGION

LIA

OTHER

SPECIAL INSTRUCTIONS

Send invoice to Equiva

Incident # 97093398

Send report to Blaine Tech Services

Attn: Ann Pember

SAMPLE I.D.	S = SOIL W = H2O	TOTAL	C = COMPOSITE ALL CONTAINERS	TPH - gas, BTEX	MTBE by 8020	MTBE by 8260	TPH - diesel	Oxygenates by 8260	1,2-DCA & EDB by 8010	ADD'L INFORMATION	STATUS	CONDITION	LAB SAMPLE #
S-5	W	3		X									
S-8	W	3		X									

8 13 04

SAMPLING COMPLETED	DATE/TIME	SAMPLING PERFORMED BY	RESULTS NEEDED NO LATER THAN
	3/7/00		

RELEASED BY	DATE	TIME	RECEIVED BY	DATE	TIME
<i>Steph White</i>	3/8/00	8:08	<i>[Signature]</i>	3/8/00	8:08

RELEASED BY	DATE	TIME	RECEIVED BY	DATE	TIME
<i>[Signature]</i>	3/8/00				

RELEASED BY	DATE	TIME	RECEIVED BY	DATE	TIME

SHIPPED VIA	DATE SENT	TIME SENT	COOLER #

EQUIVA WELL MONITORING DATA SHEET

Project #: 000307-51	Job # 204-5508-2303
Sampler: Stephm	Date: 3/7/00
Well I.D.: S5	Well Diameter: 2 (3) 4 6 8
Total Well Depth: 29.85	Depth to Water: 9.11
Depth to Free Product:	Thickness of Free Product (feet):
Referenced to: FVC (Grade)	D.O. Meter (if req'd): YSI HACH

Well Diameter	Multiplier	Well Diameter	Multiplier
2"	0.16	5"	1.02
3"	0.37	6"	1.47
4"	0.65	Other	radius ² * 0.163

Purge Method: Bailer Middleburg Electric Submersible Extraction Pump Other: _____

Sampling Method: Bailer Extraction Pump Other: Dis. Bailer

$$\frac{NO}{1 \text{ Case Volume (Gals.)}} \times \frac{\text{Purge}}{\text{Specified Volumes}} = \frac{\text{Gals.}}{\text{Calculated Volume}}$$

Time	Temp (°F)	pH	Cond.	Turbidity	Gals. Removed	Observations
920	62.3	6.5	441.3	15		Odor

Did well dewater? Yes No Gallons actually evacuated: _____

Sampling Time: 920 Sampling Date: 3/7/00

Sample I.D.: S5 Laboratory: (Sequoia) BC Other: _____

Analyzed for: (TPH-G BTEX MIBE) TPH-D Other: _____

D.O. (if req'd):	Pre-purge:	mg/L	Post-purge:	mg/L
	O.R.P. (if req'd):	Pre-purge:	mV	Post-purge:

EQUIVA WELL MONITORING DATA SHEET

Project #: 000307-S1	Job # 204-5508-2303
Sampler: Stephan	Date: 3/7/00
Well I.D.: S-7	Well Diameter: 2 <u>3</u> 4 6 8
Total Well Depth:	Depth to Water:
Depth to Free Product:	Thickness of Free Product (feet):
Referenced to: PVC Grade	D.O. Meter (if req'd): YSI HACH

Well Diameter	Multiplier	Well Diameter	Multiplier
2"	0.16	5"	1.02
3"	0.37	6"	1.47
4"	0.65	Other	radius ² * 0.163

Purge Method: Bailer
 Middleburg
 Electric Submersible
 Extraction Pump
 Other: _____

Sampling Method: Bailer
 Extraction Post
 Other: _____

_____	X	_____	=	_____
1 Case Volume (Gals.)		Specified Volumes		Gals. Calculated Volume

Time	Temp (°F)	pH	Cond.	Turbidity	Gals. Removed	Observations
Raved OVER						

Did well dewater? Yes No Gallons actually evacuated: _____

Sampling Time: _____ Sampling Date: _____

Sample I.D.: _____ Laboratory: Sequoia BC Other: _____

Analyzed for: TPH-G BTEX MTBE TPH-D Other: _____

D.O. (if req'd):	Pre-purge:	mg/L	Post-purge:	mg/L
	O.R.P. (if req'd):	Pre-purge:	mV	Post-purge:

EQUIVA WELL MONITORING DATA SHEET

Project #: 000307-51	Job # 204-5508-2303
Sampler: Stephan	Date: 3/7/00
Well I.D.: 5.8	Well Diameter: 2 (3) 4 6 8
Total Well Depth: 29.85 18.69	Depth to Water: 21 8.45
Depth to Free Product: 18	Thickness of Free Product (feet):
Referenced to: PVC (Grade)	D.O. Meter (if req'd): YSI HACH

Well Diameter	Multiplier	Well Diameter	Multiplier
2"	0.16	5"	1.02
3"	0.37	6"	1.47
4"	0.65	Other	radius ² * 0.163

Purge Method: Bailer Middleburg Electric Submersible Extraction Pump Other: _____

Sampling Method: Bailer Extraction Port Other: D.S. Bailer

$$\frac{NO}{1 \text{ Case Volume (Gals.)}} \times \frac{\text{Purge}}{\text{Specified Volumes}} = \text{Gals. Calculated Volume}$$

Time	Temp (°F)	pH	Cond.	Turbidity	Gals. Removed	Observations
1000	63.6	6.5	956.1	42		Odor

Did well dewater? Yes No

Gallons actually evacuated: _____

Sampling Time: 1000 Sampling Date: 3/7/00

Sample I.D.: 5-8 Laboratory: Sequoia BC Other: _____

Analyzed for: TPH-G BTEX MIBE TPH-D Other: _____

D.O. (if req'd):	Pre-purge:	mg/L	Post-purge:	mg/L
	O.R.P. (if req'd):	Pre-purge:	mV	Post-purge:

EQUIVA WELL MONITORING DATA SHEET

Project #: 000307-S1	Job # 204-5508-2303
Sampler: Stephan	Date: 3/7/00
Well I.D.: S-9	Well Diameter: 2 3 4 6 8
Total Well Depth:	Depth to Water:
Depth to Free Product:	Thickness of Free Product (feet):
Referenced to: FVC Grade	D.O. Meter (if req'd): YSI HACH

Well Diameter	Multiplier	Well Diameter	Multiplier
2"	0.16	5"	1.02
3"	0.37	6"	1.47
4"	0.65	Other	radius ² * 0.163

Purge Method: Bailer Middleburg Electric Submersible Extraction Pump Other: _____

Sampling Method: Bailer Extraction Port Other: _____

_____	X	_____	=	_____	Gals.
1 Case Volume (Gals.)		Specified Volumes		Calculated Volume	

Time	Temp (°F)	pH	Cond.	Turbidity	Gals. Removed	Observations
Raved OVER						

Did well dewater? Yes No Gallous actually evacuated: _____

Sampling Time: _____ Sampling Date: _____

Sample I.D.: _____ Laboratory: Sequoia BC Other: _____

Analyzed for: TPH-G BTEX MIBE TPH-D Other: _____

D.O. (if req'd):	Pre-purge:	mg/L	Post-purge:	mg/L
	O.R.P. (if req'd):	Pre-purge:	mV	Post-purge:

EQUIVA WELL MONITORING DATA SHEET

Project #: 000307-51	Job # 204-5508-2303
Sampler: Stephan	Date: 3/7/00
Well I.D.: S-11	Well Diameter: 2 3 4 6 8
Total Well Depth:	Depth to Water:
Depth to Free Product:	Thickness of Free Product (feet):
Referenced to: PVC Grade	D.O. Meter (if req'd): YSI HACH

Well Diameter	Multiplier	Well Diameter	Multiplier
2"	0.16	5"	1.02
3"	0.37	6"	1.47
4"	0.65	Other	radius ² * 0.163

Purge Method: Bailer Middleburg Electric Submersible Extraction Pump
 Other: _____

Sampling Method: Bailer Extraction Port
 Other: _____

_____	X	_____	=	_____ Gals.
1 Case Volume (Gals.)		Specified Volumes		Calculated Volume

Time	Temp (°F)	pH	Cond.	Turbidity	Gals. Removed	Observations
Paved over						

Did well devater? Yes No Gallons actually evacuated: _____

Sampling Time: _____ Sampling Date: _____

Sample I.D.: _____ Laboratory: Sequoia BC Other _____

Analyzed for: TPH-G BTEX MTBE TPH-D Other: _____

D.O. (if req'd):	Pre-purge:	mg/L	Post-purge:	mg/L
	O.R.P. (if req'd):	Pre-purge:	mV	Post-purge: