

TRANSMITTAL

TO: Ms. Eva Chu

Alameda County Health Care Serv. Agency PROJECT #: 8130.01 1131 Harbor Bay Parkway, 2nd Floor

Alameda, California 94502

DATE: October 31, 1994

SUBJECT: Quarterly Groundwater

Monitoring Report - Third Quarter 1994 and Letter Request for Closure Status for Shamrock 7499 Ford Site, Dublin Boulevard, Dublin, California.

FROM:

Barbara Sieminski Project Geologist GeoStrategies, Inc. 6747 Sierra Court, Suite G Dublin, California 94568

WE ARE SENDING YOU:

COPIES	DATED	DESCRIPTION
1	10/24/94	Quarterly Groundwater Monitoring Letter Report - Third Quarter 1994 for Shamrock Ford, 7499 Dublin Boulevard, Dublin, California
1	10/24/94	Letter Request for Closure Status for Shamrock Ford Site, 7499 Dublin Boulevard, Dublin, California

THESE ARE TRANSMITTED as checked below:

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[X] As requested	[] Approved as noted	[] Submit copies for distribution
[] For approval	[] Return for corrections	[] Return corrected prints
[] For your files		

cc: Mr. Craig Caldwell, Shamrock Ford Job File, GSI



October 24, 1994

Ms. Eva Chu Alameda County Health Care Services Agency 1131 Harbor Bay Parkway, 2nd Floor Alameda, CA 94502

Subject:

Request for Closure Status for Shamrock Ford Site, 7499 Dublin

Boulevard, Dublin, California.

Ms. Chu:

On behalf of Shamrock Ford, GeoStrategies Inc. (GSI) has prepared this letter request for the Alameda County Health Care Services Agency (ACHCSA) to assign closure status to the subject site. This request for site closure is made based upon the following information:

- Based on the chemical analytical results the soils in the vicinity of the former waste-oil tank pit have not been impacted by waste-oil related hydrocarbons or metals. The soils in the vicinity of the former gasoline tank pit have been only slightly impacted by gasoline-related hydrocarbons (2.4 parts per million [ppm] of total petroleum hydrocarbons as gasoline (TPH-G) detected in the soil sample collected from the northern wall of the tank pit above the groundwater zone).
- Groundwater samples collected from monitoring wells A-1 through A-3
 have contained nondetectable levels of TPH-G; gasoline constituents
 benzene, toluene, ethylbenzene and total xylenes (BTEX); total
 petroleum hydrocarbons as diesel (TPH-D), total petroleum
 hydrocarbons as motor oil (TPH-MO), and oil and grease (O&G) since
 their installation in December 1993. All wells contained nondetectable
 levels of hydrocarbons for four consecutive quarters.

- Concentrations of volatile organic compounds (VOCs) were nondetectable in groundwater samples collected from monitoring wells A-1 through A-3 in December 1993 and March 1994. Sampling groundwater for VOCs was discontinued after obtaining approval from ACHCSA.
- Concentrations of metals cadmium, chromium, lead, nickel and zinc in groundwater samples collected from monitoring wells A-1 through A-3 were within natural background levels in December 1993 and March and June 1994. Sampling groundwater for metals was discontinued after obtaining approval from ACHCSA.

The data supporting this request for the site closure is contained in the attached Quarterly Groundwater Monitoring Report - Third Quarter 1994 for the subject site.

If you have any questions or comments concerning this request for the site closure, please call us at (510) 551-8777.

Sincerely,

GeoStrategies Inc.

Barbara Sieminski Project Geologist

Joel Coffman Project Manager

cc: Mr. Craig Caldwell, Shamrock Ford

Attachment: Quarterly Groundwater Monitoring Report - Third Quarter

1994 for Shamrock Ford Site, 7499 Dublin Boulevard,

Dublin, California



LETTER REPORT QUARTERLY GROUNDWATER MONITORING THIRD QUARTER 1994

at Shamrock Ford 7499 Dublin Boulevard Dublin, California

613001-6

Prepared for

Shamrock Ford7499 Dublin BoulevardDublin, California 94568

Prepared by .

GeoStrategies Inc. 6747 Sierra Court Dublin, California 94568

> Barbara Sieminski Project Geologist

Stephen J. Carter

Senior Project Geologist R.G. #5577

October 24, 1994



October 24, 1994

Mr. Craig Caldwell Shamrock Ford 7499 Dublin Boulevard Dublin, California 94568

Subject:

Quarterly Groundwater Monitoring Report - Third Quarter 1994 for Shamrock Ford Site, 7499 Dublin Boulevard, Dublin,

California.

Mr. Caldwell:

As requested by Shamrock Ford, GeoStrategies Inc. (GSI) has prepared this letter report summarizing the results of the third quarter 1994 groundwater monitoring at the above-referenced site. The objectives of this quarterly groundwater monitoring are to evaluate changes in the groundwater levels and changes in concentrations of petroleum hydrocarbons in groundwater beneath the site.

SITE BACKGROUND

The subject site is located at the intersections of Dublin Boulevard and Amador Plaza Road in Dublin, California, as shown on the Vicinity Map, Figure 1. In June 1993, Gettler-Ryan Inc. (G-R) removed one 1000-gallon waste-oil underground storage tank (UST) and one 2000-gallon gasoline UST from the site. The location of the former USTs are shown on the Site Plan, Figure 2. The laboratory analytical results of soil samples collected from the tank pits indicated that the soils in the vicinity of the tank pits have not been impacted by waste-oil related hydrocarbons, and have been slightly impacted by gasoline-related hydrocarbons (2.4 parts per million [ppm] of total petroleum hydrocarbons as gasoline [TPH-G] in the sample collected from the northern wall of the gasoline tank pit).

Laboratory analytical results for a groundwater "grab" sample collected from the former waste-oil tank pit indicated 150 parts per billion (ppb) TPH-G; 3.4 ppb benzene; 6.5 ppb toluene; 2.2 ppb ethylbenzene; 11 ppb total xylenes; 8,600 ppb total petroleum hydrocarbons as motor oil (TPH-MO);

and 2,200 ppb of oil and grease (O&G). Metals Cd, Cr, Pb, Ni and Zn were detected at concentrations of 17 ppb, 460 ppb, 850 ppb, 1200 ppb, and 530 ppb, respectively. Total petroleum hydrocarbons calculated as diesel (TPH-D) concentration was reported as nondetectable, however, the reporting limit was increased to 100 ppb due to oil interference. Volatile organic compounds (VOCs) concentrations (35 compounds tested) were nondetectable (less than 2 ppb) except benzene (2.6 ppb), toluene (6.1 ppb), P,M-xylene (5.6 ppb), O-xylene (3.2 ppb), methylene chloride (4.4 ppb), and acetone (34 ppb). Laboratory analytical results for a groundwater "grab" sample collected from the former gasoline tank pit indicated 3600 ppb TPH-G; 67 ppb benzene; 40 ppb toluene; 170 ppb ethylbenzene and 540 ppb total xylenes; and 16 ppb total lead. The results of the environmental investigation related to the USTs removal are described in GSI *Underground Tank Removal Report* dated August 16, 1993.

In December 1993, three groundwater monitoring wells (A-1 through A-3) were installed at the site by GSI to evaluate the extent of petroleum hydrocarbons in soil and groundwater in the vicinity of the former USTs, and to evaluate the gradient of the shallow groundwater beneath the site. The locations of the groundwater monitoring wells are shown on Figure 2. Laboratory analytical results of the soil and groundwater samples collected during this investigation indicated that the soils and groundwater in the western, southern and southeastern vicinity of the former USTs have not been impacted by waste-oil and gasoline hydrocarbons. Concentrations of metals in soil and groundwater beneath the site appeared to be within the natural background levels. The groundwater gradient of the first encountered water-bearing zone beneath the site was interpreted to be approximately 0.004 with the flow direction to the northeast. The results of this subsurface investigation are described in GSI Initial Subsurface Investigation report dated January 26, 1994.

Quarterly groundwater monitoring and sampling of the site wells began in December 1993. Groundwater samples are currently analyzed for TPH-G, gasoline constituents benzene, toluene, ethylbenzene and xylenes (BTEX), TPH-D, TPH-MO, O&G, and metals Cd, Cr, Pb, Ni and Zn.

CURRENT QUARTER MONITORING RESULTS

Groundwater Level Measurements and Gradient Evaluation

Depth to water-level measurements were obtained in groundwater monitoring wells A-1 through A-3 on July 29, August 31, and September 30, 1994. Static groundwater levels were measured from the surveyed top of each well casing and recorded to the nearest ± 0.01 foot. Water-level data were referenced to Mean Sea Level (MSL) datum and used to construct potentiometric maps (Figures 3 through 5). The shallow groundwater hydraulic gradient was interpreted to be approximately 0.002 to 0.003 with a flow direction toward northeast.

Each well was visually inspected for the presence of floating product. Floating product was not observed in any well during this quarter. Floating product has never been observed in the monitoring wells at this site. Current and previous depth-to-groundwater and floating product measurements are summarized in Table 1, Groundwater Monitoring Data.

Chemical Analyses of Groundwater Samples

Groundwater samples were collected from groundwater monitoring wells A-1 through A-3 by G-R personnel on September 30, 1994. Samples were analyzed by Western Environmental Science and Technology of Davis, California (WEST), a State-certified laboratory (Hazardous Waste Testing Laboratory Certification #1346). The groundwater samples were analyzed for TPH-G using Modified EPA Method 8015; BTEX using EPA method 602; TPH-D and TPH-MO using Modified EPA Method 8015; and O&G using Standard Methods 5520 B,F.

The G-R groundwater sampling report is presented in Appendix A, and the WEST Laboratory Analytical Report and Chain-of-Custody record are presented in Appendix B. Laboratory analytical results for groundwater samples collected from wells A-1 through A-3 indicated nondetectable concentrations of TPH-G, BTEX, TPH-D, TPH-MO, and O&G. Current and previous analytical data for wells A-1 through A-3 are summarized in Table 2, Groundwater Quality Database. Concentrations of TPH-G and benzene



Shamrock Ford Quarterly Monitoring Report 613001-6

October 24, 1994

in groundwater are presented on Figure 6, TPH-G/Benzene Concentration Map.

DISCUSSION AND RECOMMENDATIONS

The groundwater elevation decreased an average of 1 foot in wells A-1 through A-3 between June and September 1994. The groundwater flow direction changed from the southwest during June 1994 to the northeast during the third quarter 1994.

Concentrations of TPH-G, BTEX, TPH-D, TPH-MO and O&G have remained nondetectable in samples from groundwater monitoring wells A-1 through A-3 for the fourth consecutive quarter. Therefore, GSI recommends to apply to the Alameda County Health Care Services Agency for site closure status for the site.

If you have any questions please call us at (510) 551-8777.

Attachments:

Table 1.	Groundwater	Monitoring	Data
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Table 2. Laboratory Analyses of Groundwater Samples

Figure 1. Vicinity Map

Figure 2. Site Plan

Figure 3. Potentiometric Map (July 29, 1994)

Figure 4. Potentiometric Map (August 31, 1994)

Figure 5. Potentiometric Map (September 30, 1994)

Figure 6. TPH-G/Benzene Concentration Map

Appendix A: G-R Groundwater Sampling Report

Appendix B: Laboratory Analytical Report and Chain-of-Custody Form



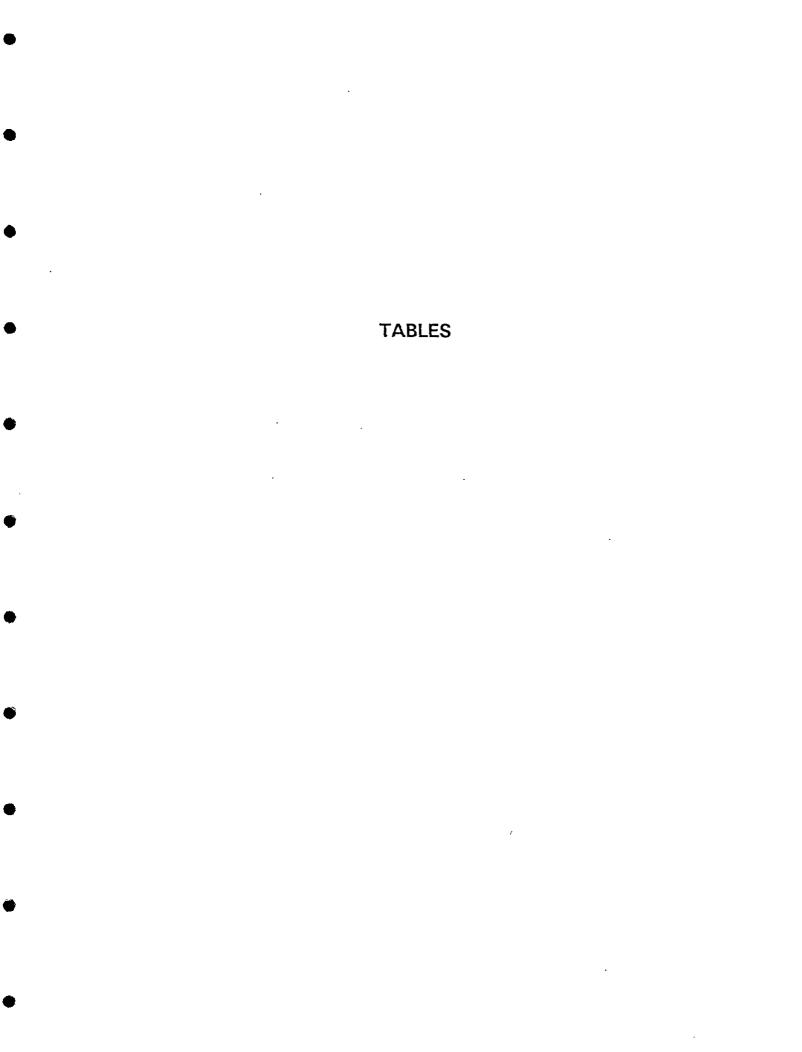


TABLE 1 GROUNDWATER MONITORING DATA Shamrock Ford Dublin, California

Monitoring Date '	Well Number	Depth to Water (ft)	Well Elevation (ft)	Static Water Elevation (ft)	Floating Product Thickness (ft)
23-Dec-93	A-1	6.27	332.88	326.61	0.00
25-Feb-94	A-1 ·	6.13	332.88	326.75	0.00
23-Mar-94	A-1	6.07	332.88	326.81	0.00
21-Apr-94	A-1	5.96	332.88	326.92	0.00
17-May-94	A-1	5.92	332.88	326.96	0.00
24-Jun-94	A-1	5.76	332.88	327.12	0.00
29-Jul-94	A-1	7.88	332.88	325.00	0.00
31-Aug-94	A-1	7.73	332.88	325.15	0.00
30-Sep-94	A-1	7.15	332,88	325.73	0.00
23-Dec-93	A-2	7.43	334.16	326.73	0.00
25-Feb-94	A-2	7.05	334.16	327.11	0.00
23-Mar-94	A-2	6.93	334.16	327.23	0.00
21-Apr-94	A-2	7.83	334.16	326.96	0.00
17-May-94	A-2	7.71	334.16	326.45	0.00
24-Jun-94	A-2	7.13	334.16	327.03	0.00
29-Jul-93	A-2	8.57	334.16	325.59	0.00
31-Aug-94	A-2	8.41	334.16	325.75	0.00
30-Sep-94	A-2	8.12	334.16	326.04	0.00
23-Dec-93	A-3	7.50	334.18 ⁷	326.68	0.00
25-Feb-94	A-3	7.19	334.18	326.99	, 0.00
23-Mar-94	A-3	7.01	334.18	327.17	0.00
21-Apr-94	A-3	7.45	334.18	326.73	0.00
17-May-94	A-3	7.29	334.18	326.89	0.00
24-Jun-94	A-3	7.18	334.18	327.00	0.00
29-Jul-94	A-3	8.22	334.18	325.96	0.00
31-Aug-94	A-3	8.18	334.18	326.00	0.00
30-Sep-94	A-3	7.93	334.18	326.25	0.00

Notes:

- 1. Static water elevations referenced to Mean Sea Level (MSL).
- 2. Well elevations and depth-to-water measured to top of casing.

TABLE 2
LABORATORY ANALYSES OF GROUNDWATER SAMPLES
Shamrock Ford
Dublin, California

SAMPLE DATE	SAMPLE POINT	TPH-G (PPB)	BENZENE (PPB)	TOLUENE (PPB)	ETHYLBENZE NE (PPB)	XYLENES (PRB)	TPH-D (PPB)	TPH-MO* (PPB)	O&G (PPB)	VOCs (PPB)	C		TETALS (F	PB) Zn	Ni
23-Dec-93	A-1	<50	<0.30	<0.30	<0.30	<0.50	< 50	<100	<1000	ND*	5.2	54	4.0	42	41
23-Mar-94	A-1	<50	< 0.30	< 0.30	< 0.30	< 0.50	< 50	<100	<1000	ND*	5.8	33	18	22	12
24-Jun-94	A-1	<50	< 0.30	< 0.30	< 0.30	< 0.50	< 50	<100	<1000	NA	4.4	25.	<3	<10	23
30-Sep-94	A-1	<50	<0.30	<0.30	< 0.30	<0.50	< 50	<100	<1000	NA	NA	NA	NA	NA	NA
23-Dec-93	A-2	<50	<0.30	<0.30	< 0.30	<0.50	< 50	<100	<1000	ND*	13	190	15	210	150
23-Mar-94	A-2	<50	< 0.30	< 0.30	< 0.30	< 0.50	<50	<100	<1000	ND*	8.3	73	5.3	46	56
24-Jun-94	, A-2	<50	<0.30	< 0.30	< 0.30	< 0.50	[°] <50	<100	<1000	NA	<4	30	<3	13	30
30-Sep-94	A-2	<50	< 0.30	<0.30	< 0.30	<0.50	< 50	<100	<1000	NA	NA	NA	NA	NA	NA
23-Dec-93	A-3	<50	<0.30	<0.30	<0.30	< 0.50	< 50	<100	<1000	ND*	5.5	51	3.5	39	32
23-Mar-94	A-3	< 50	< 0.30	< 0.30	< 0.30	< 0.50	< 50	<100	<1000	ND*	7.6	78	6.5	45	71
24-Jun-94	A-3	< 50	< 0.30	< 0.30	< 0.30	<0.50	<50	<100	<1000	NA	<4	39	4.7	26	22
30-Sep-94	A-3	<50	<0.30	<0.30	< 0.30	< 0.50	< 50	<100	<1000	NA	NA.	NA	NA.	NA	NA

Current Regional Water Quality Control Board Maximum Contaminant Levels:

Benzene 1.0 ppb, Xylenes 1750 ppb, Ethylbenzene 680 ppb, Cadmium 10 ppb, Chromium 50 ppb, Lead 50 ppb, Nickel 100 ppb, Zinc 5,000 ppb. Current Cal EPA Action Levels: Toluene 100 ppb

TPH-G = Total Petroleum Hydrocarbons calculated as Gasoline.

TPH-D = Total Petroleum Hydrocarbons calculated as Diesel.

TPH-MO = Total Petroleum Hydrocarbons calculated as Motor Oil.

O&G = Oil and Grease

VOCs = Volatile Organic Compounds.

PPB = Parts per Billion
Cd = Cadmium
Cr = Chromium

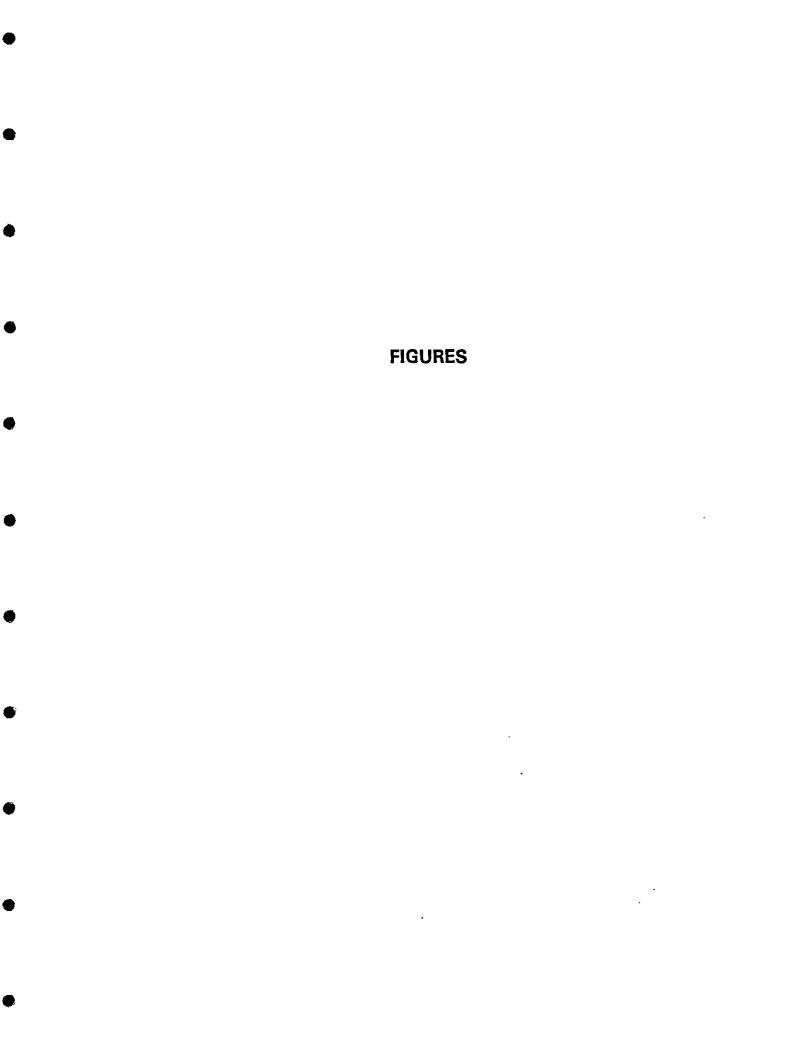
Pb = Lead Zn = Zinc

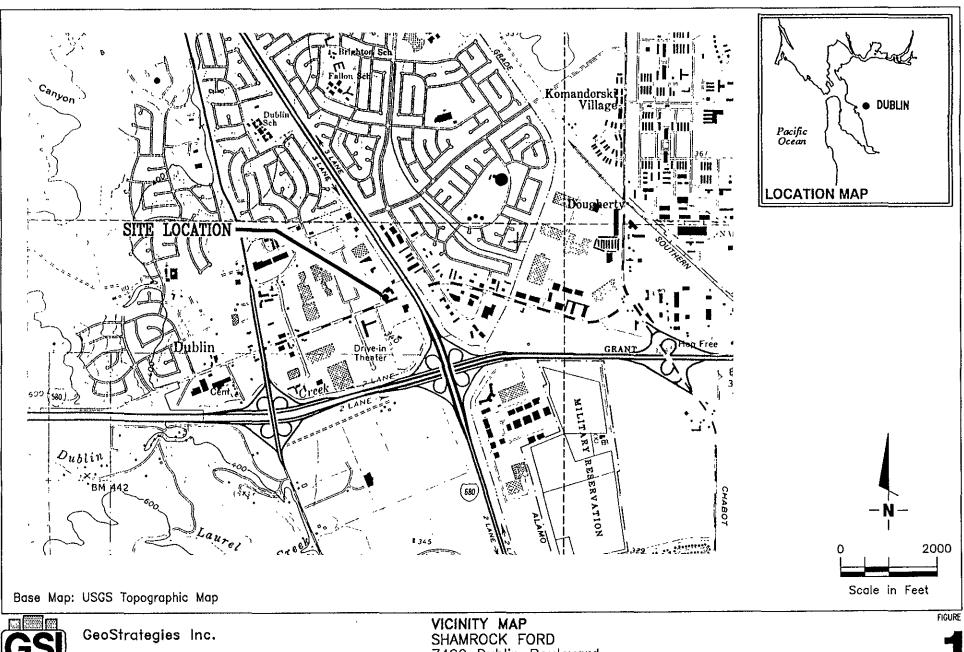
Ni = Nickel ND = Not detected

* = 38 compounds tested

NA = Not analyzed

Notes: 1. All data shown as <x are reported as ND (none detected).

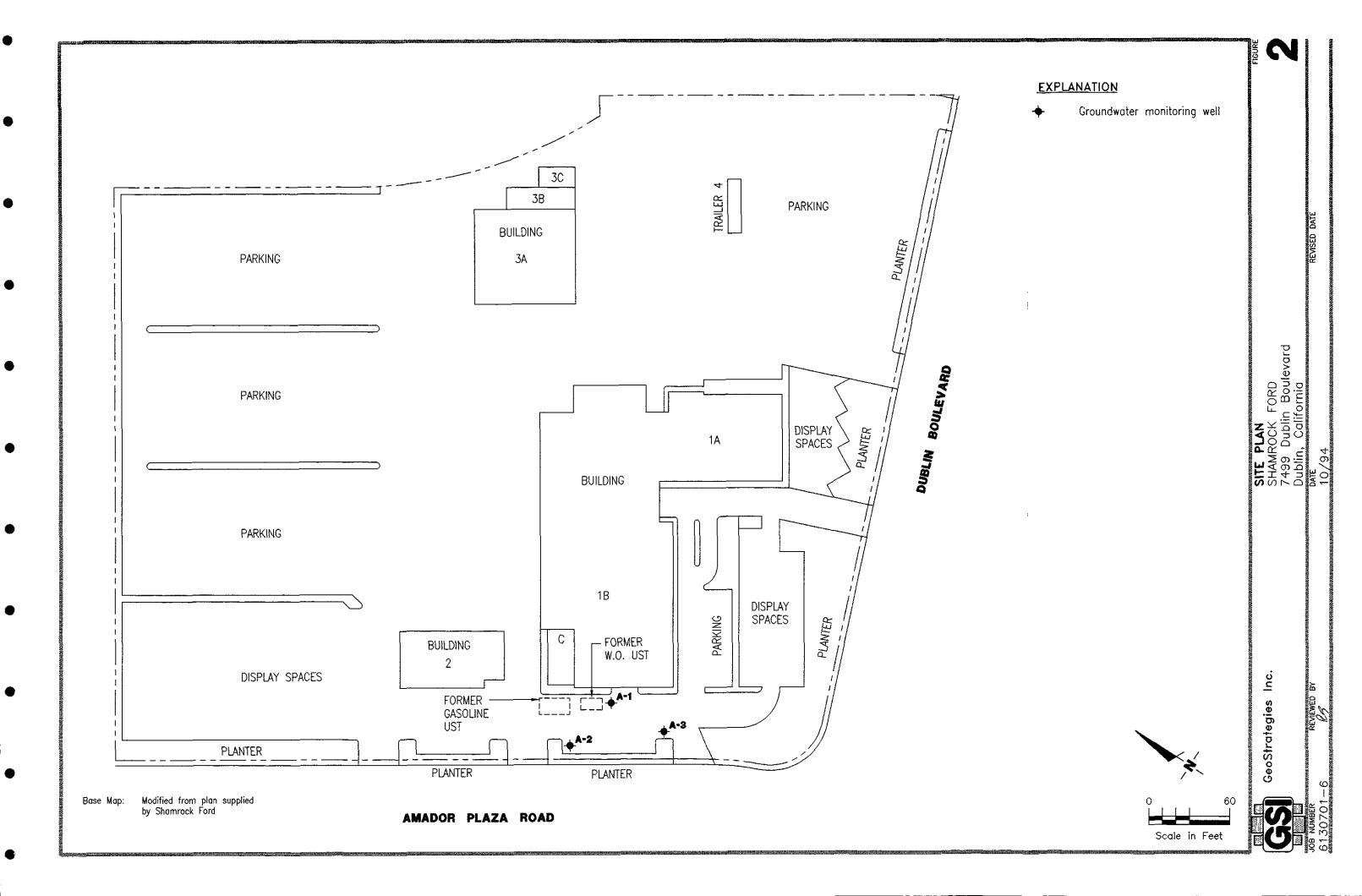


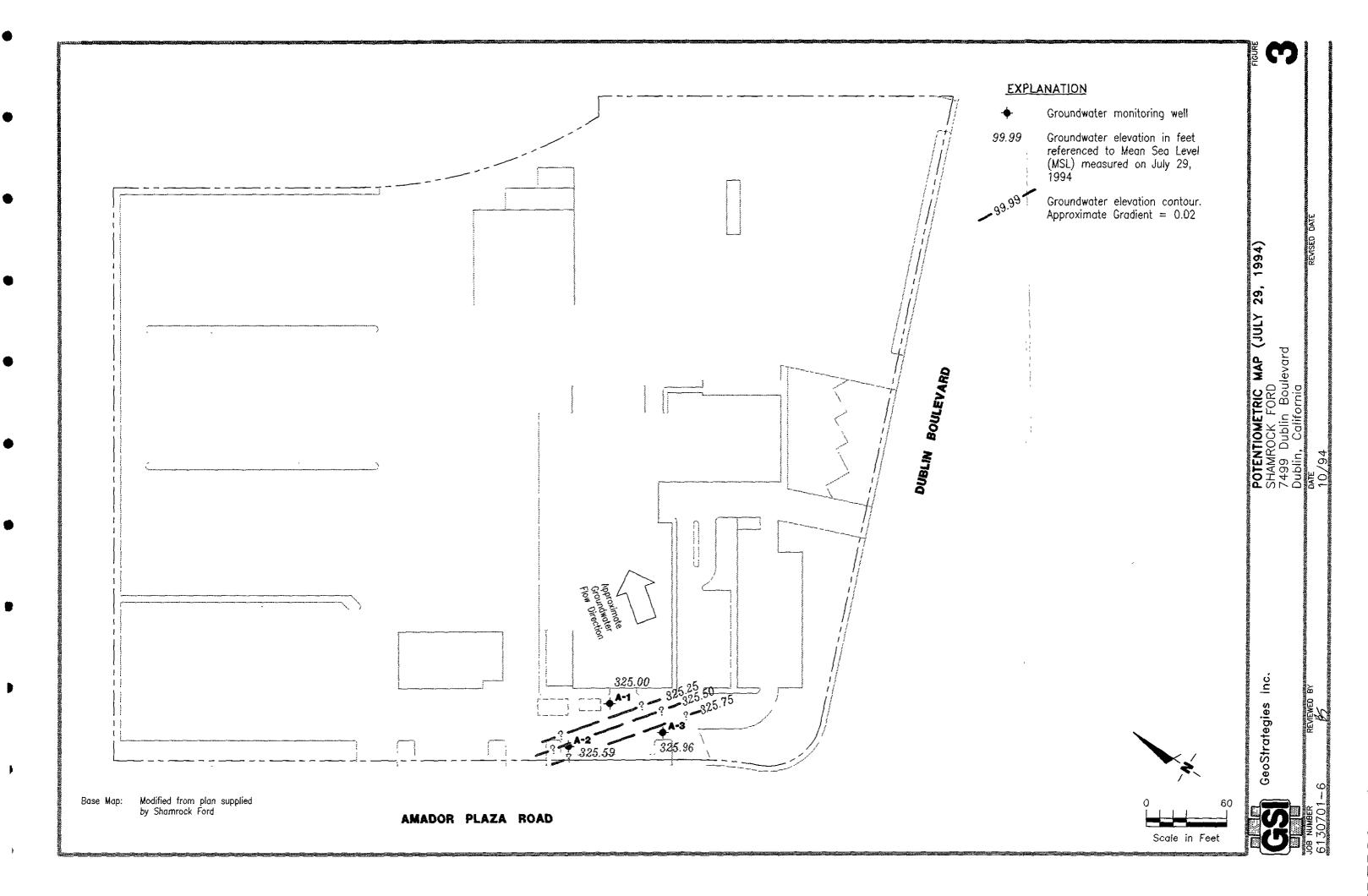


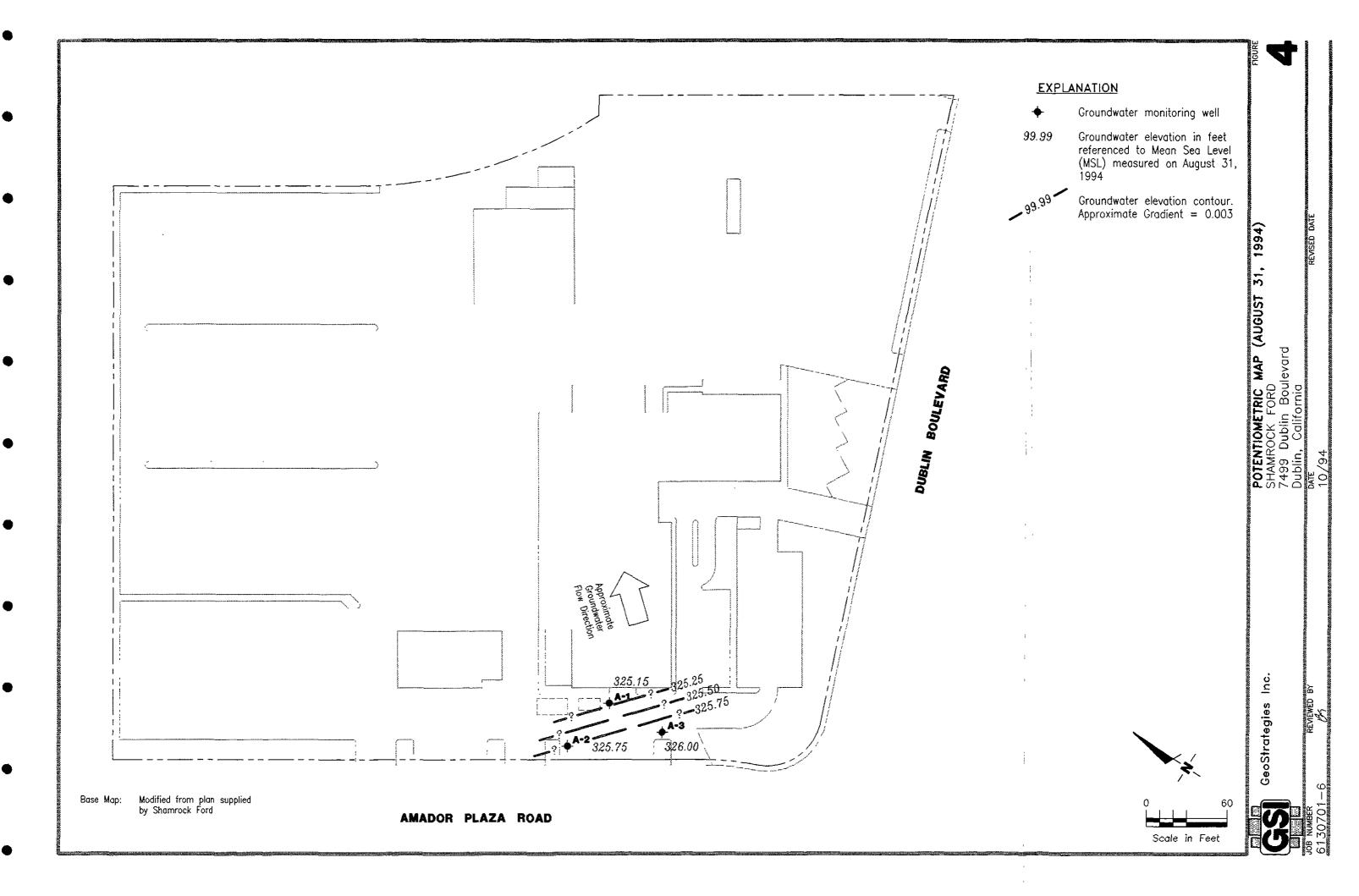
7499 Dublin Boulevard Dublin, California

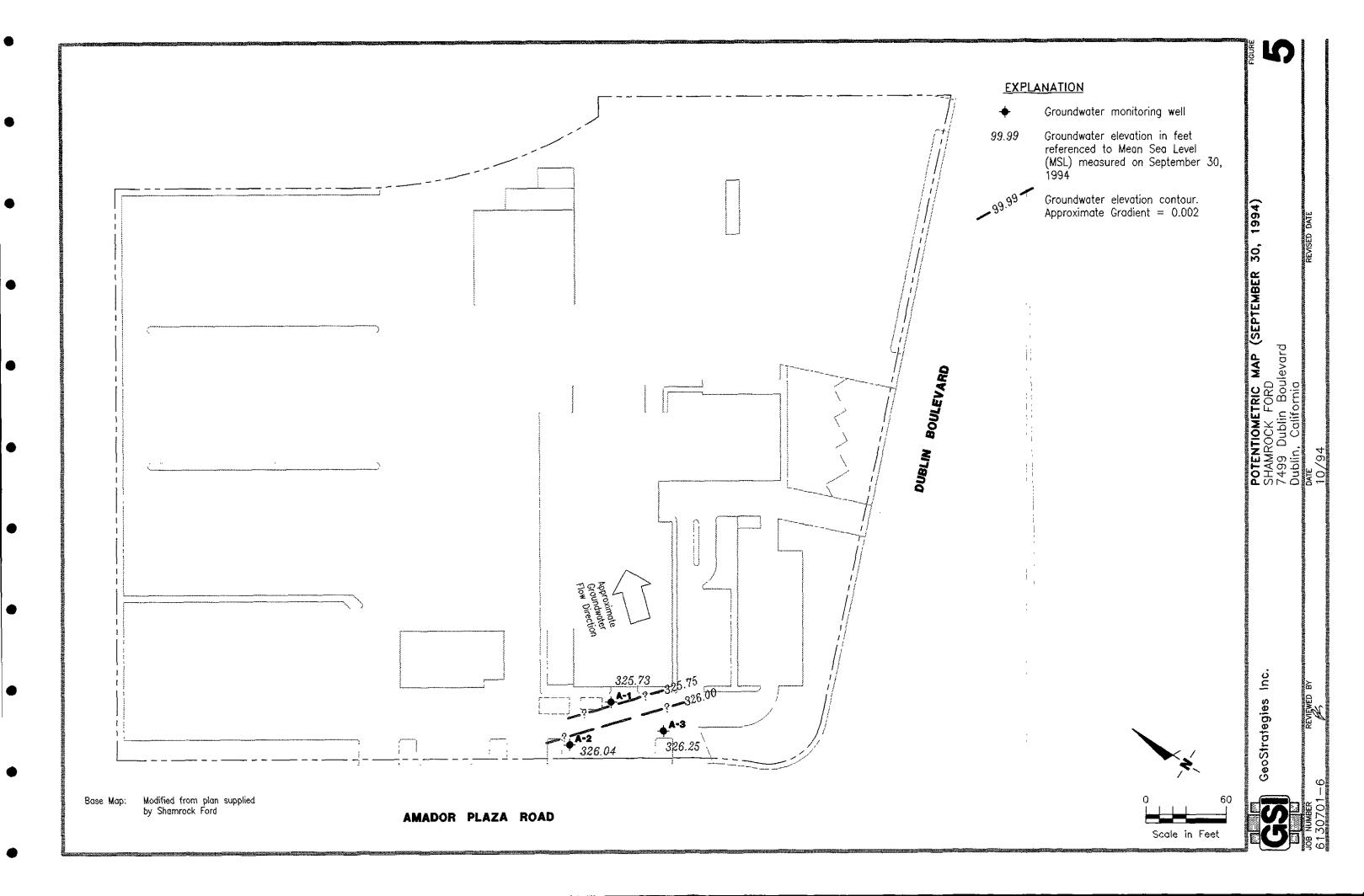
DATE 8/93 REVISED DATE

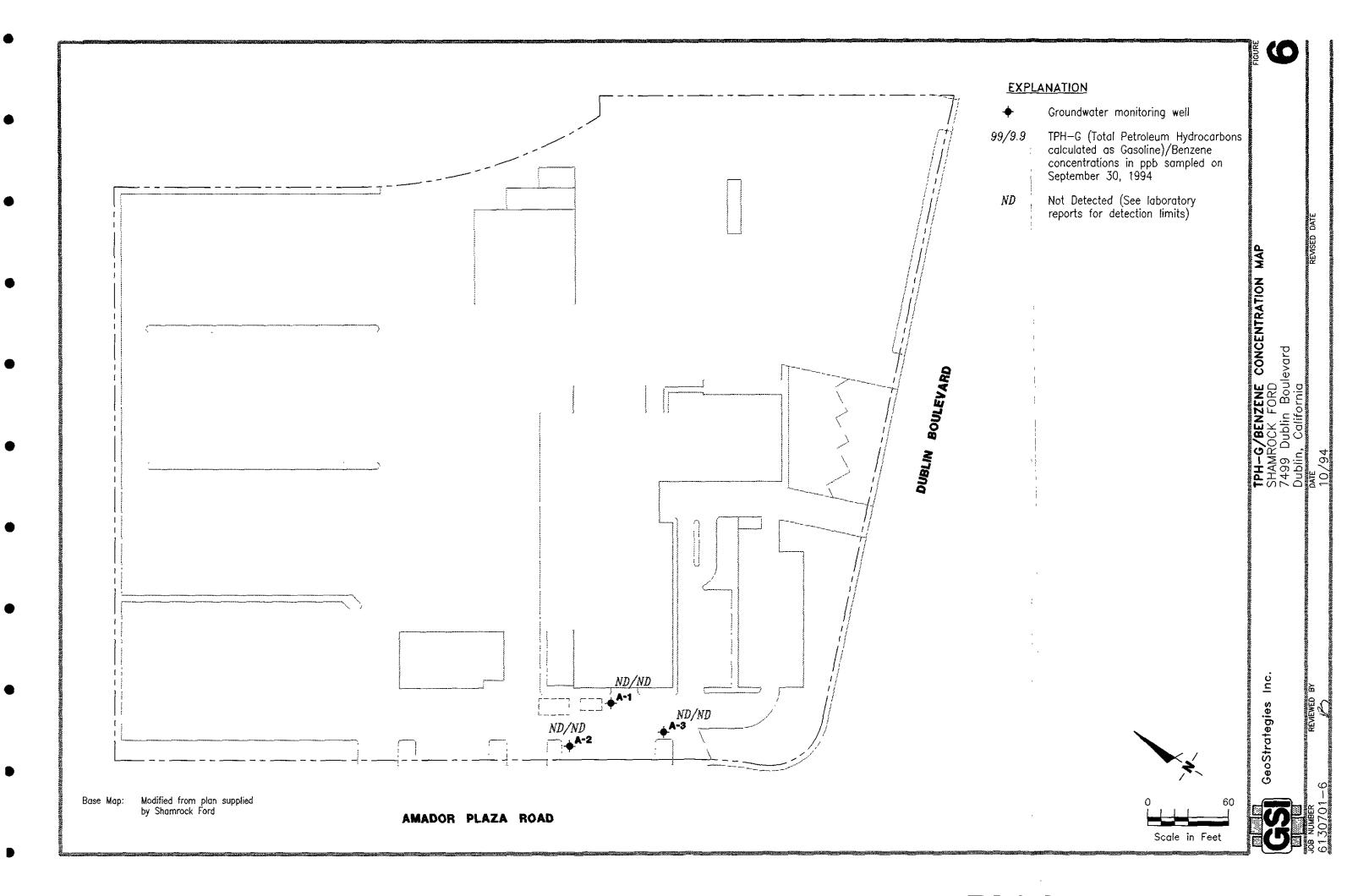
JOB NUMBER 6130 REVIEWED BY











APPENDIX A G-R GROUNDWATER SAMPLING REPORT

GEOSTRATEGIES INC.

Environmental Consultants

MONITORING WELL OBSERVATION SUMMARY SHEET

COMPANY	Shamroci	t Ford	JOB NC). <u>48/</u> 30	5,901
LOCATION	Dublin B	lvd	DAT	o. <u>48/30</u> 7-29	-94
CITY	Dublin	CA	TIM		
	•			MEASUREMENT	
WELL ID	TOTAL WELL DEPTH	DEPTH TO LIQUID	HYDROCARBON THICKNESS	POINT TOB or TOC	COMMENTS .
A-1		7.88	<u></u>	_70C	
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GEOSTRATEGIES INC.

Environmental Consultants

MONITORING WELL OBSERVATION SUMMARY SHEET .

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A-3		8,18		<i>y</i>	
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Comments:					
Sampler:	Af Ul	h-	Assistant:		•

GETTLER-RYAN INC.

General and Environmental Contractors

MONITORING WELL OBSERVATION SUMMARY SHEET

COMPANY	Shamrock	Ford	JOB NO	o. <u>8130</u>	
LOCATION	7499 L	holin Bluc	<u>/</u> DA1	9-30	94
CITY	Dablin	CA	TIM	1E	
WELL ID	TOTAL WELL DEPTH	DEPTH TO LIQUID	HYDROCARBON THICKNESS	MEASUREMENT POINT TOB or TOC	COMMENTS
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		7,44		70B	
A-2	15'	8,12	More	70C	
		8,33		70 B	
A-3	15'	7.93	Mone.	70C	•
÷ •		8.29		TOB	
	•	•			-
Comments:					
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Sempler:	fal	h-	Assistant:		· • · · · · · · · · · · · · · · · · · ·

•GETTLER-RYAN INC.

General and Environmental Contractors

WELL SAMPLING FIELD DATA SHEET

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6:11 6:13 6:15	7,03	1465 1465	69.8	1,3
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6:11 6:13 6:15 6:17 6:20 Did well dewater?_	7,03 6.98 7,00 7,03 7,02 No	1405 1405 1472 1482 1480 If yes, time	69.8 69.2 69.3 69.3 09.3	113 2.6 3.9 512 6.6
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GETTLER-RYAN INC.

General and Environmental Contractors

WELL SAMPLING FIELD DATA SHEET

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arting Time timated	7:07	Purging Flor	w Rate $\underline{\hspace{1cm}}$ $gpm. = \begin{pmatrix} Anticipated \\ Purging \\ Time \end{pmatrix}$	gpr
Purge Volume	gal. / (Rate /	Time /	
Time a	pН	Conductivity	Temperature	Volume
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7:09	7.30	1314	6812	1,3
7:09			6811	2.6
	7.30	1314		
7:09 7:11 7:13	7.30	1354 1355	6811	2.6
7:09 7:11 7:13 7:15	7.30 7.21 7.15	<u>1314</u> 1354	68.0	2.6 3.9
7:09 7:11 7:13 7:15 1:17 id well dewater?	7.30 7.21 7.15 7.14 7.15	/314 /354 /355 /350 /353 	68.1 68.0 67.8 67.8	2.6 3.9 5.2 65
7:09 7:11 7:13 7:15 2:17 id well dewater?_	7.30 7.21 7.15 7.19 7.15 No	/3/9 /359 /355 /350 /353 If yes, time	68.1 68.0 67.8 67.8 Volum	2.6 3.9 5.2 6.5
7:09 7:11 7:13 7:15 2:17 id well dewater?_	7.30 7.21 7.15 7.19 7.15 No	/3/9 /359 /355 /350 /353 If yes, time	68.1 68.0 67.8 67.8 Volum	2.6 3.9 5.2 6.5
7:09 7:11 7:13 7:15 2:17 id well dewater?_	7.30 7.21 7.15 7.19 7.15 No	/3/9 /359 /355 /350 /353 If yes, time	68.1 68.0 67.8 67.8 Volum	2.6 3.9 5.2 6.5
7:09 7:11 7:13 7:15 1:17 id well dewater?_	7.30 7.21 7.15 7.19 7.15 No	/314 /354 /355 /350 /353 	68.1 68.0 67.8 67.8 Volum	2.6 3.9 5.2 6.5

GETTLER-RYAN INC.

General and Environmental Contractors

WELL SAMPLING FIELD DATA SHEET

	am rock	n Blud	JOB # <u>&</u> DATE 9	-30-94
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npling Equipment	15 as W.			
	-			GDY
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	/ /Daaa			# · TYN11
timated Purge	gal. / FR	rging low ate	gpm. = (Anticipated Purging Time	min
Purge folume		ate /	gpm. — Purging Time Temperature)
Purge Yolume ————————————————————————————————————	рН	Conductivity	Temperature	•
Time	рН 7,3Ч	Conductivity	Temperature	Volume 1, 3 2.6
Time 6:43 6:45	pH 7,34 7,26	Conductivity 1317 1287	Temperature 67.6 68.	Volume //3
Purge /olume /	pH 7,34 7,26 7,23	Conductivity 1317 1287 1291	Temperature 67.6 68.1	Volume 1, 3 2.6
Purge folume) Time 6:43 6:45 6:47 6:49	pH 7,34 7,26 7,23 7,18	Conductivity 1317 1287 1291	Temperature 67.6 68.6 68.2	Volume 1,3 2.6 3.9
Purge folume ————————————————————————————————————	pH 7,34 7,26 7,23	Conductivity 1317 1287 1291	Temperature 67.6 68.1	Volume 1,3 2.6 3.9 5,2
Purge folume Fime 6:43 6:45 6:47 6:49 6:49	pH 7,34 7,26 7,23 7,18 7,20	Conductivity 1317 1287 1291 1299 1293	Temperature 67.6 68.1 68.1	Volume 1, 3 2.6 3.9 5, 2
Time G:43 G:45 G:47 G:47 G:47 G:51 id well dewater?_	pH 7,34 7,26 7,23 7,18 7,20 No	Conductivity 13/7 1287 1291	Temperature 67.6 68.2 68.1 Volumentations	Volume 1,3 2.6 3.9 5,2 6,5
Time G:43 G:45 G:47 G:47 G:47 G:51 id well dewater?_	pH 7,34 7,26 7,23 7,18 7,20 No	Conductivity 13/7 1287 1291	Temperature 67.6 68.2 68.1 Volumentations	Volume 1,3 2.6 3.9 5,2 6,5
Time G:43 G:45 G:47 G:47 G:47 G:51 id well dewater?_	pH 7,34 7,26 7,23 7,18 7,20 No	Conductivity 13/7 1287 1291	Temperature 67.6 68.2 68.1 Volumentations	Volume 1,3 2.6 3.9 5,2 6,5
Time G:43 G:45 G:47 G:47 G:47 G:51 id well dewater?_	pH 7,34 7,26 7,23 7,18 7,20 No	Conductivity 1317 1287 1291 1299 1293 If yes, time	Temperature 67.6 68.2 68.1 Volumentations	Volume 1,3 2.6 3.9 5,2 6,5

APPENDIX B

LABORATORY ANALYTICAL REPORT AND CHAIN-OF-CUSTODY FORM

MEST LAVBORATION

October 11, 1994 Sample Log 10412

Barbara Siemenski Gettler-Ryan Inc: 6747 Sierra Court, Suite J Dublin, CA 94568 601 I 1664

Subject: Analytical Results for 3 Water Samples

Identified as: Project # 8130.01 (Shamrock Ford)

Received: 09/30/94 Purchase Order: 8130.01

Dear Ms. Siemenski:

Analysis of the sample(s) referenced above has been completed. This report is written to confirm results communicated on October 11, 1994 and describes procedures used to analyze the samples.

Water samples were received in 40-mL glass bottles sealed with TFE septae, and in 1-L glass bottles sealed with TFE-lined caps. Each sample was received under documented chain of custody and stored at 4 degrees C until analysis was performed.

Sample(s) were analyzed using the following method(s):

"BTEX" (EPA Method 602/Purge-and-Trap)
"TPH as Gasoline" (Modified EPA Method 8015/Purge-and-Trap)
"TPH as Diesel, Motor Oil, Jet/Kerosene" (Mod. 8015/Extraction)
"Oil and Grease" (5520 B,F)

Please refer to the following table(s) for summarized analytical results and contact us at 916-753-9500 if you have questions regarding procedures or results. The chain-of-custody document is enclosed.

Approved by:

Stewart Podolsky Senior Chemist



October 11, 1994 Sample Log 10412

QC Report

Total Oil and Grease (Standard Methods 5520 B,F)

From : Project # 8130.01 (Shamrock Ford)

QC Batch KW941002

Matrix : Water

Spike and Spike Duplicate Results

Parameter	Matrix	Matrix	RPD
	Spike (%Rec)	Spike Dup. (%Rec)	%
O&G Gravimetric		sample for spiking. uplicate LCS Data.	

Laboratory Control Spike

Paramater		ory Control Spike Dup. (%Rec)	RPD %
O&G Gravimetric	90	93	3

Method Blank

Parameter	MDL(ug/L)	Measured Value(ug/L)	
O&G Gravimetric	(1000)	<1000	

Stewart Podolsky Senior Chemist



October 11, 1994 Sample Log 10412

Total Oil and Grease (Standard Methods 5520 B,F)

From : Project # 8130.01 (Shamrock Ford)

Received: 09/30/94

Matrix : Water

--all concentrations are units of ug/l--

Sample	Date Sampled	Date Analyzed	MRL	(5520 B,F) Oil and Grease
A-1	09/30/94	10/10/94	(1000)	<1000
A- 2	09/30/94	10/10/94	(1000)	<1000
A-3	09/30/94	10/10/94	(1000)	<1000

QC Batch: KW941002

tewart Podolsky



October 11, 1994 Sample Log 10412

QC Report

TPH Diesel/Motor Oil by 8015 Mod

From : Project # 8130.01 (Shamrock Ford)

QC Batch DW941005

Matrix: Water

Spike and Spike Duplicate Results

Parameter	Matrix	Matrix	RPD
	Spike (%Rec)	Spike Dup. (%Rec)	%
TPH as Diesel	Not enough sa See duplicate	ample for spiking. E LCS Data.	

Laboratory Control Spike

Parameter	Laboratory Control Spike (%Rec) Spike Dup. (%Rec)		RPD %
TPH as Diesel	92	85	8

Method Blank

Parameter	MDL(ug/L)	Measured Value(ug/L)
TPH as Diesel	(50)	<50
TPH as Motor Oil	(100)	<100

Stewart Podolsky Senior Chemist



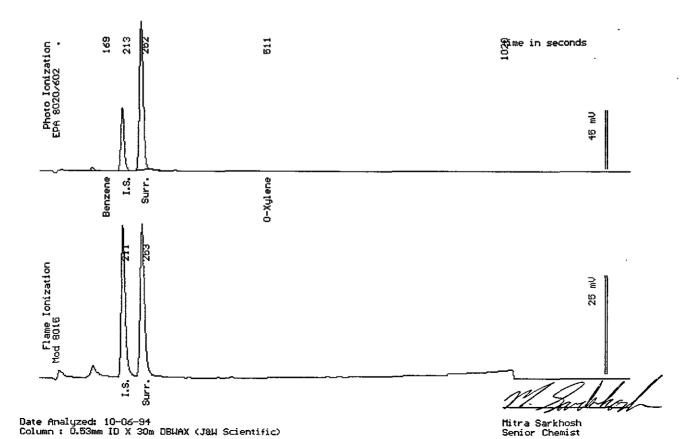
Sample: A-1

From : Project # 8130.01 (Shamrock Ford)

Sampled: 09/30/94

Dilution: 1:1 QC Batch: 2105M

Parameter	(MRL) ug/L	Measured Value ug/L
Benzene	(.30)	<.30
Toluene	(.30)	<.30
Ethylbenzene	(.30)	<.30
Total Xylenes	(.50)	<.50
TPH as Gasoline	(50)	<50
Surrogate Recover	У	102 %





Sample Log 10412

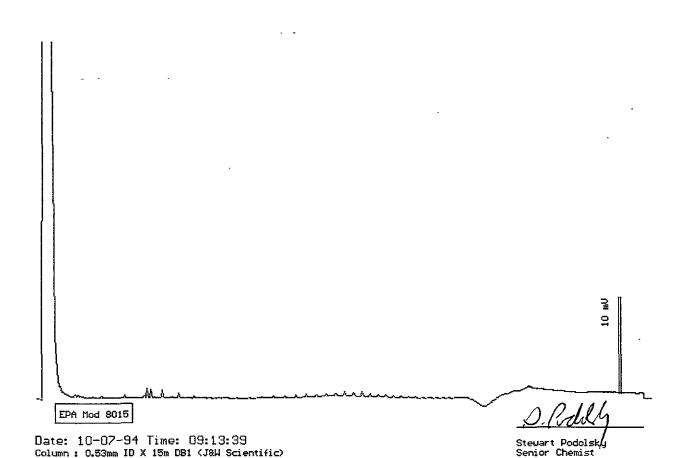
Sample: A-1

From : Project # 8130.01 (Shamrock Ford)

Sampled: 09/30/94

Extracted: 10/06/94 QC Batch: DW941005 Dilution: 1:1 Run Log: 8193F

Parameter	(MRL) ug/L	Measured Value ug/L
TPH as Diesel	(50)	<50
TPH as Motor Oil	(100)	<100





Sample Log 10412

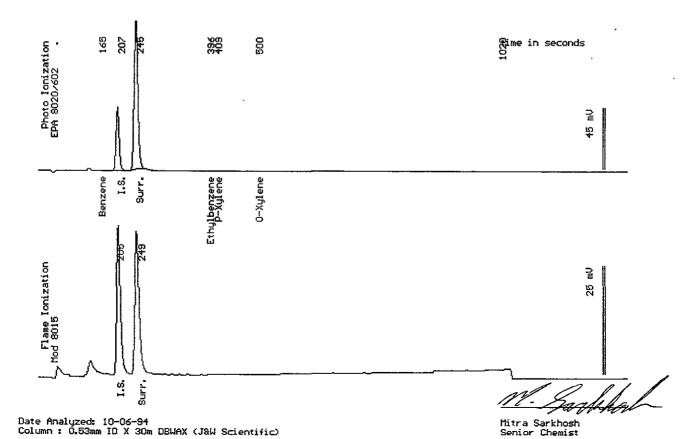
Sample: A-2

From : Project # 8130.01 (Shamrock Ford)

Sampled: 09/30/94

Dilution: 1:1 QC Batch: 2105N

Parameter	(MRL) ug/L	Measured Value ug/L
Benzene	(.30)	<.30
Toluene	(.30)	<.30
Ethylbenzene	(.30)	<.30
Total Xylenes	(.50)	<.50
TPH as Gasoline	(50)	<50
Surrogate Recovery	I	103 %





Sample: A-2

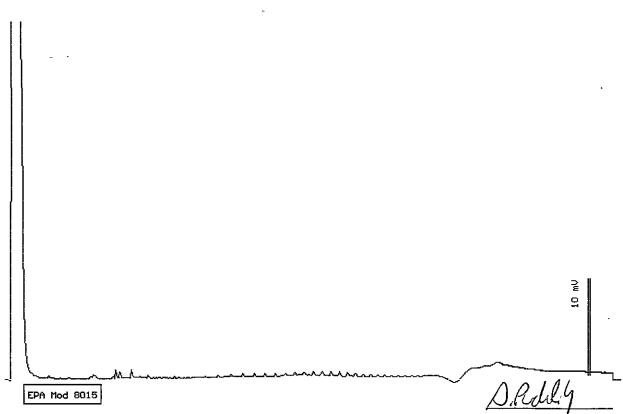
From : Project # 8130.01 (Shamrock Ford)

Sampled: 09/30/94

Extracted: 10/06/94 QC Batch: DW941005 Dilution: 1:1 Run Log: 8193F

Matrix : Water

Parameter	(MRL) ug/L	Measured Value ug/L
TPH as Diesel TPH as Motor Oil	(50) (100)	<50 <100



Date: 10-07-94 Time: 10:56:45 Column: 0.53mm ID X 15m DB1 (J&W Scientific) Stewart Podolsky Senior Chemist



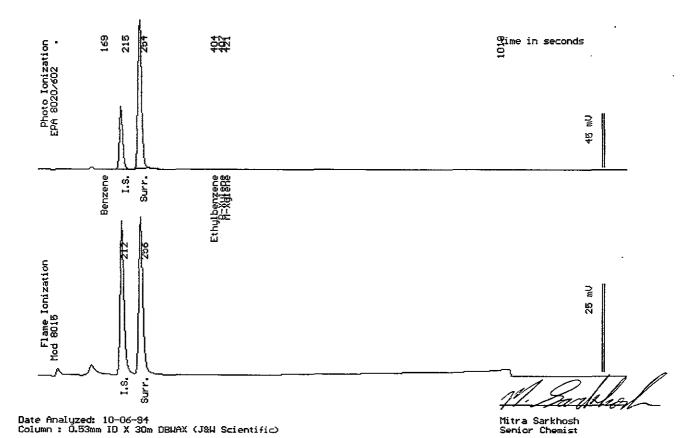
Sample: A-3

From : Project # 8130.01 (Shamrock Ford)

Sampled: 09/30/94 Dilution: 1:1

Dilution: 1:1 QC Batch: 2105N

Parameter	(MRL) ug/L	Measured Value wg/L
_	,	
Benzene	(.30)	<.30
Toluene	(.30)	<.30
Ethylbenzene	(.30)	<.30
Total Xylenes	(.50)	<.50
TPH as Gasoline	(50)	<50
Surrogate Recovery	<i>!</i>	102 %





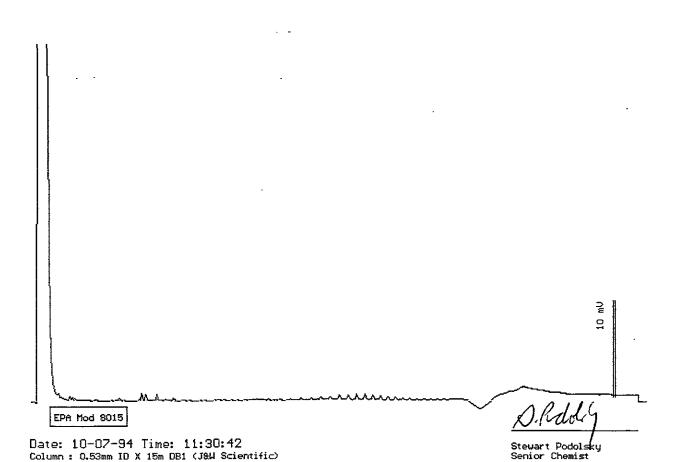
Sample: A-3

From : Project # 8130.01 (Shamrock Ford)

Sampled: 09/30/94

Extracted: 10/06/94 QC Batch: DW941005 Dilution: 1:1 Run Log: 8193F

Parameter	(MRL) ug/L	Measured Value ug/L
TPH as Diesel	(50)	<50
TPH as Motor Oil	(100)	<100





October 6, 1994 Sample Log 10412

QC Report for EPA 602 & Modified EPA 8015

From: Project # 8130.01 (Shamrock Ford)
Sample(s) Received: 09/30/94

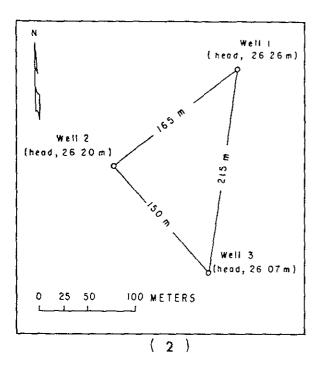
Parameter	Matrix Spike % Recovery	Matrix Spike Duplicate % Recovery	RPD *	
Benzene	98	98	0	
Ethylbenzene	99	102	3	
TPH as Gasoline	107	108	1	

^{*} RPD = Relative Percent Difference

Parameter	Method Blank		
Benzene Toluene Ethylbenzene	<0.30 ug/L <0.30 ug/L <0.30 ug/L		
Total Xylenes TPH as Gasoline	<0.50 ug/L <50 ug/L		

Mitra Sarkhosh Senior Chemist

Gettler - R		ENVIRONMENT	AL DIVISION	1609 Chair	n of Custody
COMPANY	Shamr	ock ford		JOB NO	8136,01
JOB LOCATION _	7499	Dublin Blu	vd		
CITY	Daslin	r CH		_ PHONE NO	
	Barbava	Siemenski i	DATE 9-30-94		0.01
SAMPLE ID	NO. OF CONTAINERS	SAMPLE DATE/TIM MATRIX SAMPLE			PLE CONDITION LAB ID
A-1	7	Ligard 9-3094/4	6:06 (THE Gus.	BIXE	
A-2	7	9-35-94 / 6	157 / TOH Dogs	a Motor Gul	
<i>A</i> -3	7	9-30-94/7:		Crease	
		1	SM-5520	BAR	
	**************************************				· · · · · · · · · · · · · · · · · · ·
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ESIGNATED LAB	ORATORY:	Davis CA	DHS #:		•
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DATE COMPLETED _	, -		FOREMAN	e over	-



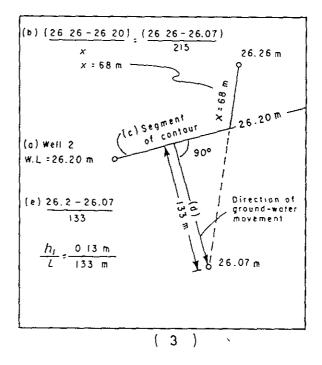
kilometer or feet per mile. A gradient of 5 m/780 m can be converted to meters per kilometer as follows:

$$\left(\frac{5 \text{ m}}{780 \text{ m}}\right) \times \left(\frac{1,000 \text{ m}}{\text{km}}\right) = 6.4 \text{ m km}^{-1}$$

Both the direction of ground-water movement and the hydraulic gradient can be determined if the following data are available for three wells located in any triangular arrangement such as that shown on sketch 2:

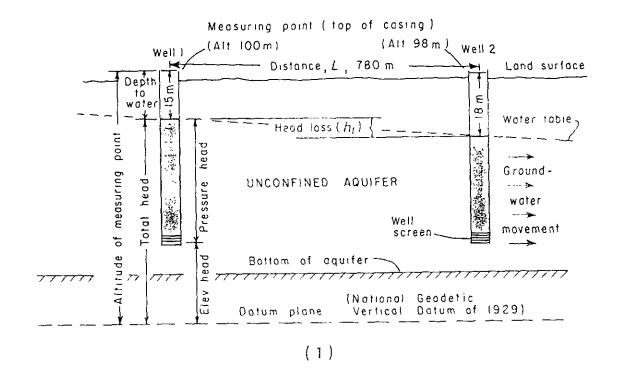
- 1. The relative geographic position of the wells.
- 2. The distance between the wells.
- 3. The total head at each well.

Steps in the solution are outlined below and illustrated in sketch 3:



- a Identify the well that has the intermediate water level (that is, neither the highest head nor the lowest head).
- b. Calculate the position between the well having the highest head and the well having the lowest head at which the head is the same as that in the intermediate well.
- c. Draw a straight line between the intermediate well and the point identified in step b as being between the well having the highest head and that having the lowest head. This line represents a segment of the water-level contour along which the total head is the same as that in the intermediate well.
- d Draw a line perpendicular to the water-level contour and through either the well with the highest head or the well with the lowest head. This line parallels the direction of ground-water movement.
- e. Divide the difference between the head of the well and that of the contour by the distance between the well and the contour. The answer is the hydraulic gradient.

HEADS AND GRADIENTS



The depth to the water table has an important effect on use of the land surface and on the development of water supplies from unconfined aquifers (1). Where the water table is at a shallow depth, the land may become "waterlogged" during wet weather and unsuitable for residential and many other uses. Where the water table is at great depth, the cost of constructing wells and pumping water for domestic needs may be prohibitively expensive.

The direction of the slope of the water table is also important because it indicates the direction of ground-water movement (1). The position and the slope of the water table (or of the potentiometric surface of a confined aquifer) is determined by measuring the position of the water level in wells from a fixed point (a measuring point) (1) (See "Measurements of Water levels and Pumping Rates,") To utilize these measurements to determine the slope of the water table, the position of the water table at each well must be determined relative to a datum plane that is common to all the wells. The datum plane most widely used is the National Geodetic Vertical Datum of 1929 (also commonly referred to as "sea level") (1).

If the depth to water in a nonflowing well is subtracted from the altitude of the measuring point, the result is the total head at the well. Total head, as defined in fluid mechanics, is composed of elevation head, pressure head, and velocity head. Because ground water moves relatively slowly, velocity head can be ignored. Therefore, the total head at an observation well involves only two components: elevation head and pressure head (1). Ground water moves in the direction of decreasing total head, which may or may not be in the direction of decreasing pressure head.

The equation for total head (h_t) is

$$h_t = z + h_D$$

where z is elevation head and is the distance from the datum plane to the point where the pressure head h_p is determined.

All other factors being constant, the rate of ground-water movement depends on the hydraulic gradient. The hydraulic gradient is the change in head per unit of distance in a given direction. If the direction is not specified, it is understood to be in the direction in which the maximum rate of decrease in head occurs.

If the movement of ground water is assumed to be in the plane of sketch 1—in other words, if it moves from well 1 to well 2—the hydraulic gradient can be calculated from the information given on the diawing. The hydraulic gradient is $h_L L$, where h_L is the head loss between wells 1 and 2 and L is the horizontal distance between them, or

$$\frac{h_1}{L} = \frac{(100 \text{ m} - 15 \text{ m}) - (98 \text{ m} - 18 \text{ m})}{780 \text{ m}} = \frac{85 \text{ m} - 80 \text{ m}}{780 \text{ m}} = \frac{5 \text{ m}}{780 \text{ m}}$$

When the hydraulic gradient is expressed in consistent units, as it is in the above example in which both the numerator and the denominator are in meters, any other consistent units of length can be substituted without changing the value of the gradient. Thus, a gradient of 5 ft/780 ft is the same as a gradient of 5 m/780 m. It is also relatively common to express hydraulic gradients in inconsistent units such as meters per