A Report Prepared for

Gerber Products Company 445 State Street Freemont, Michigan 49412

PHASE III SITE INVESTIGATION ADDENDUM FORMER GERBER PRODUCTS FACILITY OAKLAND, CALIFORNIA

HLA Job No. 19459,001.02

bу

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#### 1.0 INTRODUCTION

This report presents the results of Harding Lawson Associates (HLA) Phase III site investigation of soil and ground-water conditions at the former Gerber Products Company (Gerber) facility in Oakland, California.

The purpose of this investigation has been to: 1) further evaluate the great and vertical extent of total petroleum hydrocarbons (TPH) and benzene, toluene, ethylbenzene, and xylenes (BTEX) previously detected in the unsaturated soils in the vicinity of the former Chevron service station area of the property; and 2) characterize the areal extent of dissolved TPH and BTEX in ground water of the uppermost aquifer downgradient of the former Chevron service station area.

#### 2.0 BACKGROUND

The project site is in the southeastern portion of Oakland, California, approximately 1-mile east of the Nimitz Freeway, U.S. Interstate 880. San Francisco Bay is approximately 2 miles southwest of the site and the Oakland hills are about 2 miles east of the site. The surrounding topography is generally flat with the surface elevation of the site approximately 20 feet above mean sea level.

#### 2.1 Site Description

The former Gerber food processing facility is located at the northwest corner of San Leandro Street and 98th Avenue in Oakland, California (Plate 1). Land use in the area is primarily industrial with retail businesses and multi-family housing. The former Gerber facility consisted of offices, warehouses, and buildings where food was processed. The remaining 20 acres of the site were reported to consist of concrete and asphalt-covered parking or storage areas.

Prior to Gerber's acquisition of the property, the northeastern corner of the site (Plate 1) was occupied by Chevron and Shell Oil Company retail service stations. The site is presently occupied by several light industrial operations that include Environmental Sampling Supply Company, a construction contractor group, and a plastics recycling center. During HLA's site visit on August 3, 1989, a truck and car were being overhauled underneath the canopy area (Plate 1), and automotive fluids and/or degreasing agents were observed leaking onto the pavement beneath them. The remaining areas of the site continue to exist as office space, vacant buildings, and concrete- and asphalt-covered pavement.

A former gasoline service station located in the immediate vicinity of the site at 9801 San Leandro Street has been identified as having soil and ground-water impacts

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resulting from gasoline contamination. The 9801 San Leandro Street site is at the corner of 98th Avenue and San Leandro Street, across 98th Avenue from Monitoring Well MW-5 at the northeast corner of the Gerber facility (Plate I). Review of California Regional Water Quality Control Board - San Francisco Bay Area (RWQCB) documentation indicates the 9801 San Leandro Street property was a former Thrifty gasoline service station and that the property was purchased by the City of Oakland as part of the City's 98th Avenue street widening project. The City of Oakland is reportedly in the process of addressing soil and ground-water remediation activities at the subject property.

#### 2.2 Previous Investigations

Previous site investigations at the former Gerber facility by Beta Associates (1987) and Groundwater Technology, Inc. (1988), as described in the reports provided for our review dated May 29, 1987, and November 17, 1988, respectively, were performed to evaluate the presence (or absence) of potential contamination in areas identified as suspect during an initial property inspection. As shown on Plate 1, a total of 15 soil borings (DH-1 through DH-11, MW-5, MW-6, MW-7 and MW-8) were previously drilled at the site to characterize soil conditions, and 7 of those borings (DH-1, DH-2, DH-4 and MW-5 through MW-8) were converted into monitoring wells (MW-1, MW-2, and MW-4 through MW-8, respectively) for characterization of ground-water conditions in the uppermost aquifer.

Analytical laboratory results for soil and ground-water samples collected from the previous borings and monitoring wells (Tables 1 and 2, respectively), indicate the presence of aromatic volatile organic compounds and TPH in soil samples collected from DH-8, MW-5, MW-6, and MW-8, and in ground-water samples collected from

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Wells MW-2, MW-5, MW-6, and MW-8. In addition, chlorinated volatile organic compounds were detected in ground-water samples collected from Monitoring Wells MW-1 and MW-7.

The aromatic volatile organic compounds detected at the site include BTEX, which are common dissolved components of gasoline. The BTEX and TPH constituents detected in ground-water samples collected from Wells MW-2, MW-5, MW-6, and MW-8 appear to be related to operations of the former Chevron service station that occupied the northeastern corner of the site prior to Gerber's acquisition of the property. and/or the migration of these constituents onto the Gerber facility from the former Thrifty gasoline service station. Additionally, elevated concentrations of TPH and benzene, toluene, and xylenes were detected in the soil sample collected from Boring DH-8 and appear to indicate an on-site source of contamination in the area occupied by the former Chevron service station. Results of a ground-penetrating radar survey conducted by Groundwater Technology, Inc. (1988), did not indicate the presence of underground fuel storage tanks in the area occupied by the former Chevron and Shell Oil service stations, suggesting that the tanks had previously been removed.

The chlorinated volatile organic compounds detected at the site,

1,1-dichloroethane (DCA); 1,1-dichloroethene (DCE); and 1,1,1-trichloroethane

(TCA), were reported in ground-water samples collected from Monitoring Wells MW-1 and MW-7.

#### 2.3 Regional Geology and Hydrogeology

The former Gerber facility is located on the San Leandro alluvial fan which is situated between San Francisco Bay and the Oakland foothills. The fan soils consist of Quaternary Age unconsolidated channel and floodplain sediments deposited by San

Leandro Creek, which is currently located 1-mile south of the site. These sediments were derived primarily from erosion of older marine rocks in the foothills and consist of coarse sand and gravel along former stream channels and of silt and clay on the associated floodplain.

The San Leandro alluvial fan consists of interlayered deposits of low-permeability clay (aquitards) and permeable sand and gravel (aquifers). The low-permeability clay materials function as confining layers for the deeper confined aquifer systems in the area, and also comprise shallow-aquifer zones. An industrial well located at the former Gerber Products facility is completed in a deeper confined aquifer zone of the area (in contrast to the shallow uppermost aquifer zone that is the subject of this investigation); the well is reported to extend to a depth of 602 feet below ground surface and is screened between 160 to 225 feet. Ground-water use from the deeper confined aquifers in the area is reported to be limited to industrial purposes (Groundwater Technology, Inc., 1988).

#### 3.0 FIELD INVESTIGATION

HLA's field investigation of site conditions at the former Gerber facility was conducted between August 3 and November 4, 1989. The scope of our services included drilling eight borings (two of which were completed as monitoring wells) and collecting soil samples from them for chemical analysis; installing and developing two groundwater monitoring wells; measuring water levels and collecting ground-water samples from each monitoring well at the site (9 wells); conducting a series of aquifer slug tests; and arranging a survey to provide reference elevations at each monitoring well location.

#### 3.1 Soil Sampling Program

To further evaluate the areal and vertical distribution of TPH and BTEX concentrations in soil of the vadose zone in the vicinity of DH-8, six soil borings, designated SB-1 through SB-6, were drilled at the locations shown on Plate 2 and soil samples were collected from them and submitted for chemical analysis. The soil borings were drilled using truck-mounted hollow-stem auger drilling equipment. An HLA geologist was present during drilling operations to coordinate activities, perform health and safety monitoring, collect soil samples, and record subsurface conditions. The soils in each boring were classified according to the Unified Soil Classification System (USCS). The lithologic logs of the soil borings and a key to the USCS are presented in Appendix A.

Undisturbed soil samples were collected from each boring at depths of approximately 5, 10, and 15 feet below ground surface (bgs). An organic vapor analyzer was used to screen soil samples for the presence of volatile organic compounds. Samples were also checked for other evidence of contamination, such as soil discoloration, petroleum and chemical odors, and the presence of liquid phase chemicals. Following

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collection and field screening, all soil sample tubes were sealed with foil-lined and taped plastic end caps. On the basis of field screening, 17 soil samples from the 6 soil borings were selected for chemical analysis. The soil samples selected for chemical analysis were stored on blue ice until delivery to Curtis & Tompkins, Ltd., a California state-certified laboratory in Berkeley, California. Chain of custody records were initiated in the field and maintained until samples were relinquished to the analytical laboratory.

To prevent potential cross contamination between borings, all downhole equipment was steam cleaned prior to use for drilling each boring. All soil sampling equipment was also cleaned with an Alconox wash and deionized water rinse prior to the collection of each soil sample. All soil sampling procedures were conducted in accordance with HLA QA/QC procedures, which meet or exceed all state and local requirements.

#### 3.2 Monitoring Well Installation and Development

To further evaluate the areal extent of TPH and BTEX concentrations in the uppermost aquifer beneath the site, two additional monitoring wells, designated MW-9 and MW-10, were installed at locations shown on Plate 1. Drilling was performed on August 4, 1989, by Spectrum Drilling, Inc., of Stockton, California using a Mobile B-53 hollow-stem auger drill rig. An HLA geologist was present to coordinate drilling activities and monitoring well installation. Drilling operations, lithologic logging, and the collection and screening of soil samples from the borings drilled for well installation were performed in accordance with the procedures described in Section 3.1.

Monitoring wells were constructed with flush-threaded 4-inch-diameter,

Schedule 40 PVC well casing and screen. Prior to removal of the auger sections,

factory-slotted 0.010-inch well screen with a bottom cap was placed at the bottom of

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#### 3.3 Ground-Water Sampling Program

On August 8, 1989, water-level measurements were obtained and ground-water samples were collected from the nine monitoring wells at the site (MW-1, MW-2, and MW-4 through MW-10). Ground-water samples were collected using a stainless steel bailer and decanted into 40-milliliter (ml) vials. The wells were purged of a minimum of three well volumes by hand bailing or with a centrifugal pump prior to sampling. The purged water was contained in 55 gallon drums and stored at the site. Water quality parameters (pH, electrical conductivity, temperature, and clarity) were also monitored during purging of the wells.

All water-level and sampling equipment was steam cleaned before use in each well to minimize cross contamination. Following collection, ground-water samples were stored on blue ice until delivery to Curtis & Tompkins, Ltd., for chemical analysis. A field blank consisting of deionized water was poured though a stainless steel bailer into a 40 ml vial and was stored with the samples. Chain of custody records were initiated in the field and maintained until samples were relinquished to the laboratory.

#### 3.4 Analytical Program

Soil samples submitted for chemical analysis were analyzed for TPH calibrated as gasoline by EPA Test Method 8015 (modified) and for BTEX by EPA Test Method 8020 using purge and trap extraction by EPA Test Method 5030. Ground-water samples submitted for chemical analysis were analyzed for volatile organics using EPA Test Method 624 and for TPH calibrated as gasoline by EPA Test Method 8015 (Modified) using purge and trap extraction method EPA 5030. All samples were analyzed by Curtis & Tompkins, Ltd.

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## 3.5 Slug Testing Program

On September 25, 1989, a series of slug tests was performed in Monitoring Wells MW-2, MW-5, MW-6 and MW-8 to estimate the transmissivity and hydraulic conductivity of the uppermost aquifer that underlies the site. The slug tests were performed in accordance with a method presented by Bouwer and Rice (1976) and Bouwer (1989) for determining the hydraulic conductivity of unconfined aquifers with completely or partially penetrating wells.

The hydraulic conductivity of the uppermost aquifer in the vicinity of each well tested was calculated from the rate of rise of the water level in the well after a certain volume of water was suddenly removed. Simulation of water removal during the subject tests was achieved by completely submerging a weighted 6-foot-long PVC slug (with a displacement volume of 0.036 cubic foot), allowing the water level in the well to reach equilibrium, and then quickly removing the slug. The resulting rate of rise of the water level in the well (recovery) was measured until the water level returned to static conditions. Water-level changes were measured using an In-Situ Inc. pressure transducer and Hermit model SE1000B data logger. Prior to the beginning and end of each slug test performed, calibration of the pressure transducer was checked using a steel measuring tape. The slug testing procedure was duplicated in each well to assess confirmation of the test data.

#### 4.0 RESULTS OF FIELD INVESTIGATION

#### 4.1 Soil and Ground-Water Conditions

Lithologic data obtained during drilling at the site revealed a general sequence of silty to sandy clay underlain by clayey sand underlain by sandy clay. The sand unit and the clay above the sand comprise the uppermost aquifer at the site. Boring logs are presented in Appendix A.

The uppermost soil at the site consists of predominantly stiff silty to sandy clay with occasional lenses of sand. These soils extend to approximately 16 feet bgs and are wet to saturated below approximately 11 feet bgs. From approximately 16 to 21 feet bgs, the soil consists of dense, saturated, clayey fine-grained sand. At Monitoring Well MW-10, the sand grades into a poorly graded sand with some fine gravel from 20 to 21 feet bgs. These sands and the saturated portion of the clay overlying these sands comprise the uppermost aquifer. The soil underlying this water-bearing sand unit is comprised of soft to stiff sandy clay. This clay unit is present at approximately 20 feet bgs at Monitoring Well MW-9. The clay unit functions as the lower confining layer (aquitard) for the uppermost aquifer.

The uppermost aquifer at the site occurs primarily from 11 to 21 feet bgs and is generally under semiconfined conditions. Water-level data and chemical data suggest that the water-bearing sand and saturated portion of the upper clay act as an unconfined unit. Hydraulically, however, the upper clay behaves as a confining layer for the semiconfined sand aquifer.

Water-level measurements from monitoring wells at the site have been obtained on four dates from April 1987 to August 1989 and are presented in Table 3. The depth to water measurements were used to calculate ground-water elevations in feet above mean sea level. Ground-water elevations from August 8, 1989, have been used to

construct the potentiometric contour map presented on Plate 3. As shown, the localized direction of ground-water flow is toward the west. The hydraulic gradient across the site ranges from approximately 0.001 to 0.002 foot/foot.

#### 4.2 Slug Test Results

Water-level data from the slug tests performed in Monitoring Wells MW-2, MW-5, MW-6, and MW-8 are illustrated as semilog plots of the change in water level versus time on Plates B1 through B6 presented in Appendix B, and were analyzed to derive values of transmissivity and hydraulic conductivity for the uppermost aquifer at the site according to Bouwer and Rice (1976), and Bouwer (1989). Analysis of the slug test data was based upon the thickness of the clayey sand zone identified in the uppermost aquifer (approximately 16 to 21 feet bgs) to derive hydraulic parameters. Calculation Sheets of the analyses are presented in Appendix B. The effect of the rate of rise of the water level in each well attributed to drainage of the gravel pack was also eliminated by ignoring the early data points of the semilog plots and using the second straight line portion in the data plot for the calculation of aquifer parameters.

A summary of the slug test results are presented in Table 4. Analysis of the semilog plots resulted in transmissivity and hydraulic conductivity values that ranged from 53 to 288 square feet per day (ft<sup>2</sup>/day), and 15 to 72 feet per day (ft/day), respectively.

In conclusion, consistent values of transmissivity and hydraulic conductivity have been derived from the slug tests performed at the site. The geometric mean transmissivity and hydraulic conductivity values of 136 ft<sup>2</sup>/day and 32 ft/day, respectively, are considered representative of the uppermost aquifer at the site. On the basis of the hydraulic gradients (0.001 to 0.002), the geometric mean hydraulic

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conductivity value obtained from the slug tests, and an estimated porosity of 30 percent for the clayey sand materials that comprise the uppermost aquifer, the horizontal velocity of ground-water flow in the uppermost aquifer ranges from about 0.1 to 0.2 ft/day.

#### 4.3 Soil Sampling Results

The laboratory analytical reports of soil samples submitted for chemical analysis from each boring are presented in Appendix C, and Table 5 presents a summary of the analytical results. In general, analytical results for the soil samples suggest that the distribution of chemicals detected in the soils from the vicinity of the former Chevron service station area can be characterized into three horizontal layers.

Soil samples collected from depths ranging between 5 to 6.5 feet bgs did not contain detectable concentrations of TPH calibrated as gasoline or of BTEX, with exception of TPH detected at 2 milligrams per kilogram (mg/kg) in the 5-foot sample from MW-8, toluene detected at 30 micrograms per kilogram (µg/kg) in the 6- to 6.5-foot sample from Boring SB-1, and benzene detected at 47 µg/kg in the 5- to 5.5-foot sample from Boring SB-5. The zone from the approximate depth 5 to 10.5 feet bgs contains TPH to accentrations ranging from 34 to 470 mg/kg from Borings SB-1 to 36-6. TPH was also detected at 5 mg/kg in the 10-foot sample from MW-8. Maximum BTEX concentrations in these samples were 3,300 µg/kg for benzame, 1,400 µg/kg for toluene, 8,200 µg/kg for ethylbenzene and 22,000 µg/kg for total xylenes. Soil samples collected between the depths of 15 to 16 feet bgs did not contain detectable concentrations of TPH or BTEX except in the vicinity of Borings SB-2 and SB-6. The 15.5- to 16-foot sample from Boring SB-2 had concentrations of TPH at 140 mg/kg, and BTEX at 670, 790, 1,300, and 4,900 µg/kg, respectively. The 15- to

15.5-foot sample from Boring SB-6 had BTEX concentrations of 33, 34, 5.5, and 26  $\mu$ g/kg, respectively.

TPH and BTEX were not detected in the 6- to 6.5-foot and 12- to 12.5-foot soil samples from Borings MW-9 and MW-10. These borings (completed as monitoring wells) were drilled southwest of the former Chevron service station area.

#### 4.4 Ground-Water Sampling Results

The laboratory analytical reports for ground-water samples collected during the current investigation and submitted for chemical analysis are presented in Appendix D. Table 2 presents a summary of the chemical parameters and concentrations detected in ground-water samples from each monitoring well sampled during the present investigation, and also includes the chemical data reported from the two previous investigations conducted at the site (Beta. 1987; Groundwater Technology, 1988).

Chemical results of the August 8, 1989, ground-water sampling event conducted by HLA indicate that chlorinated volatile organic compounds, TPH calibrated to gasoline, and the parameters BTEX were detected in samples collected from monitoring wells at the site. One or more chlorinated volatile organic compounds were detected in Wells MW-1, MW-7, and MW-9. The compounds DCE, DCA, and TCA were detected in Well MW-1 at 47, 9, and 21  $\mu$ g/l, respectively. Concentrations detected in MW-7 were 39, 8, and 13  $\mu$ g/l for DCE, DCA, and TCA, respectively. DCE was also detected at a concentration of 3  $\mu$ g/l in Well MW-9.

TPH and BTEX compounds were detected in monitoring Wells MW-2, MW-5, MW-6, and MW-8 at the northeast corner of the site. TPH concentrations in Wells MW-2, MW-6, and MW-8 were 1.1, 1.0, and 77 milligrams per liter (mg/l), respectively. Benzene concentrations ranged from 48 to 1,900 µg/l, and toluene,

ethylbenzene, and total xylene concentrations ranged from 8 to 820  $\mu$ g/l, 15 to 1,000  $\mu$ g/l, and 55 to 3,600  $\mu$ g/l, respectively.

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#### 5.0 DISCUSSION OF CHEMICAL RESULTS

#### 5.1 Soil Conditions

Chemical results for soil samples collected from the former Chevron service station area in the northeast corner of the subject property indicate that elevated concentrations of TPH and BTEX have been detected in a zone ranging from approximately 9 to 10.5 feet bgs... The distribution of TPH concentrations detected in all soil samples collected during the present and former investigations are shown on Plate 4. The concentrations of TPH detected in all samples collected between the depths of 9 and 10.5 feet bgs ranged from 5 to 10.17 mg/hg.

Similarly, concentrations of BTEX constituents detected in soil samples from the depths of 9 to 10.5 feet bgs have ranged from: 140 to 3,300 µg/kg; 200 to 2.00 µg/kg. 270 to 8,200 µg/kg; and 430 to 108,092 µg/kg, respectively. Additionally, elevated levels of TPH and BTEX have been detected in a soil sample collected from the depth of 15.5 to 16 feet bgs from boring SB-2 at concentrations of 140 mg/kg and 670, 790, 1,300, and 4,900 µg/kg, respectively. The distribution of chemical concentrations detected in soil samples from the former Chevron service station area correlate closely with the former locations of underground gasoline storage tanks, fuel conveyance lines, and service station pump islands identified on facility layout plans of the former Chevron service station. Because the predominant depth of soil contamination present in the borings sampled ranged from 9 to 10.5 feet bgs, it appears likely that former underground gasoline storage tanks in the subject area of the site were responsible for the TPH and BTEX soil concentrations detected.

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#### 5.2 Ground-Water Conditions

Analytical results for ground-water samples collected from monitoring wells at the site indicate that: 1) the areal extent of TPH and BTEX contamination appears to be limited to an area in the vicinity and downgradient of the former Chevron service station, and 2) the distribution and concentrations of the parameters DCE, DCA, and TCA detected in Wells MW-1 and MW-7 appear to indicate the presence of an impact associated with the former Shell Oil Company service station area and/or the potential migration of these parameters to the subject locations from an off-site source.

Chemical results of the TPH and BTEX analyses of ground-water samples collected at the site indicate that these parameters were detected in Wells MW-2, MW-5, MW-6, and MW-8 only. On the basis of the distribution of TPH and BTEX concentrations detected at the site, it appears that the areal extent of TPH and BTEX ground-water contamination is represented by the distribution of benzene concentrations in ground water, and is limited to the area shown on Plate 5. The source(s) responsible for the TPH and BTEX ground-water contamination identified at the site appears to be the TPH contaminated soils in the vicinity of the former Chevron service station.

Chemical results of ground-water samples collected from Wells MW-1 and MW-7 indicate that the parameters DCE, DCA, and TCA were detected in these two wells. DCE, DCA, and TCA belong to a group of compounds classified as chlorinated volatile organics and appear to represent a separate type of ground-water contamination at the site with respect to the TPH and BTEX contamination previously described. On the basis of site history information that has identified a former Shell Oil Company service station that previously occupied the subject area, it seems probable that the chlorinated volatile organic compounds detected at the site are the result of operations of

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the former Shell Oil Company service station and/or the migration of these compounds from an off-site (upgradient) source.

#### 6.0 REFERENCES

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  Gerber Products Facility, 9401 San Leandro Street, Oakland, California, May 29.
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- Bouwer, H. and Rice, R.C., 1976. A Slug Test for Determining Hydraulic Conductivity of Unconfined Aquifers with Completely or Partially Penetrating Wells. Water Resources Research, Vol. 12, No. 3, June.
- Groundwater Technology, Inc., 1988. Subsurface Hydrocarbon Investigation, Gerber Products Company, 9401 San Leandro Street, Oakland, California, November 17.

Table 1. Summary of Previous Chemical Results from Soil Samples

WELL NUMBER	SAMPLING DATE	DEPTH (FEET)	TPH (GASOLINE) mg/kg	BENZENE ug/kg	TOLUENE ug/kg	ETHYL BENZENE Ug/kg	XYLENES, TOTAL ug/kg	DIESEL mg/kg	MOTOR OIL mg/kg
Source	e: Groundwater	Technology,	Inc., 1988	3		·	· · · · · ·		<del></del>
MW-5	18-May-88	5	ND(1)	ND(0.5)	ND(0.5)	ND(0.5)	ND(0.5)	NT	NT
	18-May-88	10	160	ND(0.5)	ND(0.5)	3000	7000	NT	NT
	18-May-88	15	ND(1)	ND(0.5)	ND(0.5)	ND(0.5)	ND(0.5)	NT	NT
MW-6	18-May-88	5	ND(1)	ND(0.5)	ND(5)	ND(5)	ND(5)	NT	NT
	18-May-88	10	310	ND(0.5)	2000	4000	18000	NT	NŤ
MW-7	18-May-88	5	ND(1)	ND(0.5)	ND(5)	ND(5)	ND(5)	NT	нT
	18-May-88	10	ND(1)	ND(0.5)	ND(5)	ND(5)	ND(5)	NT	ИŤ
B-WM	19-May-88	5	2	ND(0.5)	ND(5)	ND(5)	ND(5)	NT	NT
	19-May-88	10	5	ND(0.5)	ND(5)	ND(5)	ND(5)	NT	NT
Sourc	e: Beta Associ	ates, 1987							
MW-1	18-Apr-87	3	NT	ND(10)	ND(10)	ND (10)	ND(20)	NT	NT
MW-2	18-Apr-87	3	NT	ND(10)	ND(10)	ND(10)	ND (20)	NT	NT
DH-3	18-Apr-87	2.5	NT	ND(10)	ND(10)	ND(10)	ND(20)	ΝТ -	МŢ
MW-4	18-Apr-87	10.5	NT	ND(10)	ND(10)	NT	ND(10)	ND	ND
DH-5	18-Apr-87	5	NT	ND(10)	ND(10)	ND(10)	ND(20)	NT	NT
DH-6 .	18-Apr-87	10.5	NT	ND(10)	ND(10)	NT	ND(10)	ND	NĎ
DH-7	18-Apr-87	3.5	ND(1)	ND(10)	ND(10)	ти	ND(10)	TK	Тĸ
DH-8	18-Apr-87	10	1017	1063	9997	NT	108092	ND(1)	240
DH-9	18-Apr-87	1	NT	ND(10)	ND(10)	ND(10)	ND(20)	TK	нт
DH-10	18-Apr-87	t	NT	NT	нT	NT	HT	NT	NT
DH-11	18-Apr-87	1	NT	ND(10)	ND(10)	NT	ND(10)	NT	380

mg/kg: milligrams per kilogram (equivalent to parts per million)
ug/kg: micrograms per kilogram (equivalent to parts per billion)
ND: Not detected; Limit of detection indicated in parenthesis

NT: Not Tested

Total Petroleum Hydrocarbons (TPH) by EPA Method 8015 Benzene, Toluene, Ethyl Benzene, Total Xylenes by EPA Method 8020 Extraction by EPA Method 5030, Purge and Trap

Table 2. Summary of Chemical Results from Ground-water Samples

		TPH			ETHYL	XYLENES,	OTHER	DETECTABLE V	OLATILE COMP	POUNDS
WELL	SAMPLING	(GASOLINE)	BENZENE	TOLUENE	BENZENE	TOTAL	1,1-DCE	1,1-DCA	1,1,1-TCA	1,2-DCA
NUMBER	DATE	mg/l	ug/l	ug/l	ug/l	ug/l	ug/l	ug/l	ug/l	ug/l
MV-1	18-Apr-87	NT	ND(0.5)	ND(0.5)	ND(0.5)	ND(0.5)	61	9.5	93.1	0.5
	03-Jun-88	NT	ND(5)	ND(5)	ND(5)	ND(5)	ND(5)	8	40	ND(5)
	08-Aug-89	ND(0.05)	ND(1)	ND(1)	ND(1)	ND(1)	47	9	21	ND(1)
MW-S	18-Apr-87	NT	76.9	121	93.4	477	ND(0.2)	ND(0.5)	ND(0.5)	ND(0.5)
	03-Jun-88	NT	64	18	48	60	ND(5)	ND(5)	ND(5)	ND(5)
2	08-Aug-89	1.1	48	9	33	55	ND(1)	ND(1)	ND(1)	ND(1)
MW-4	18-Apr-87	NT	ND(0.5)	ND(0.5)	ND(0.5)	ND(0.5)	ND(0.2)	ND(0.5)	ND(0.5)	ND(0.5)
	03-Jun-88	NT	ND(5)	ND(5)	ND(5)	ND(5)	ND(5)	ND(5)	ND(5)	ND(5)
	08-Aug-89	ND(0.05)	ND(1)	ND(1)	ND(1)	ND(1)	ND(1)	ND(1)	ND(1)	ND(1)
MW-5	03-Jun-88	NT	93	ND(5)	100	ND(5)	ND(5)	ND(5)	ND(5)	ND(5)
	08-Aug-89	ND(0.05)	49	8	15	63	ND(1)	ND(1)	ND(1)	ND(1)
MW-6	88-nut-88	NT	110	140	35	210	ND(5)	ND(5)	ND(5)	ND(5)
	08-Aug-89	1.0	45	- 8	15	74	ND(1)	ND(1)	ND(1)	ND(1)
MW-7	03-Jun-88	NT	ND(5)	ND(5)	ND(5)	ND(5)	25	5	18	ND(5)
	08-Aug-89	ND(0.05)	ND(1)	ND(1)	ND(1)	ND(1)	39	8	13	ND(1)
MW-8	88-Jun-88	NT	2300	2000	950	4100	ND(5)	ND(5)	ND(5)	ND(5)
	08-Aug-89	77	1900	820	1000	3600	ND(1)	ND(1)	ND(1)	ND(1)
MW-9	08-Aug-89	ND(0.05)	ND(1)	ND(1)	NO(1)	ND(1)	3	ND(1)	ND(1)	ND(1)
MV-10	08-Aug-89	ND(0.05)	ND(1)	ND(1)	ND(1)	ND(1)	ND(1)	ND(1)	ND(1)	ND(1)
Field	03-Jun-88	NT	ND(5)	ND(5)	ND(5)	ND(5)	ND(5)	ND(5)	ND(5)	ND(5)
Blank	08-Aug-89	ND(0.05)	ND(1)	ND(T)	ND(1)	ND(1)	ND(1)	ND(1)	ND(1)	ND(1)

mg/t: milligrams per liter (equivalent to parts per million)

ug/l: micrograms per liter (equivalent to parts per billion)

NT: Not Tested

ND: Not detected; Limit of detection indicated in parenthesis

1,1-DCE: 1,1-Dichloroethene

1,1-DCA: 1,1-Dichloroethane

1,1,1-TCA: 1,1,1-Trichloroethane

1,2-DCA: 1,2-Dichloroethane

Volatile Organics in Water by EPA Method 624
Total Petroleum Hydrocarbons (TPH) as Gasoline
in Aqueous Solutions by EPA Method 8015 (Modified)
Extraction by EPA Method 5030, Purge and Trap

April 18, 1987 Results from Beta Associates (1987) June 3, 1988 Results from Groundwater Technology (1988) August 8, 1989 Results from Curtis & Tompkins, Ltd.

Table 3. Water-Level Elevations

WELL NUMBER	<b>M</b> √-1	HW-2	мы-4	MW-5	MW-6	MW-7	MW-8	MW-9	MW-10
Top of Casing Elevation	18.05	18.42	18.74	18.96	18.71	18.05	18.97	17.66	18.36
DATE	DEPTH	TO WATER	(FEET)	FROM TOP	OF CASI	NG			
20-Apr-87	10.28	10.38	NA	10.84	NA	HA	NA	NA	NA
22-Jul-88	10.48	10.71	11.43	10.86	11.00	10.39	11.04	NM	NM
04-Aug-89	10.41	NM	NM	10.63	10.91	MM	10.95	NM	NM
08-Aug-89	10.40	10.56	11.19	10.77	10.89	10.27	10.98	10.11	10.53
DATE	GROUND	-WATER E	LEVATION	(FEET)	ABOVE ME	AN SEA LI	EVEL		
20-Apr-87	7.77	8.04	NA	8.12	NA	NA	NA	NA	NA
	7.57	7.71	7.31	8.10	7.71	7.66	7.93	NM	NM
22 · Jul · 88						1424	9 00	4114	
22 · Jul · 88 04 · Aug · 89	7.64	NM	MM	8.33	7.80	NM	8.02	NM	NM

NA: Not Applicable, Monitoring Well Not Yet Installed

NM: Not Measured

Table 4. Results of Siug Tests

Well Number	Test Number	Aquifer Thickness (feet)	Hydraulic Conductivity (ft/day)	Transmissivity (ft <sup>2</sup> /day)
MW-2	l	4.0	64.4	258
	2	4.0	72.0	288
1411 -	•	5.0	27.4	7 ****
MW-5	1	5.0	27.4	137
	2	5.0	22.5	113
MW-6	1	4.0	48.5	194
	2	4.0	41,5	166
	÷	4.0	41,5	100
MW-8	1	4.0	15.1	60
	2	4.0	13.2	53
	-		-3.2	
Geometric	Mean		32.2	136

Note: Analysis of slug test performed using method of Bouwer and Rice (1976) and Bouwer (1989).

Table 5. Summary of Chemical Results from Soil Samples

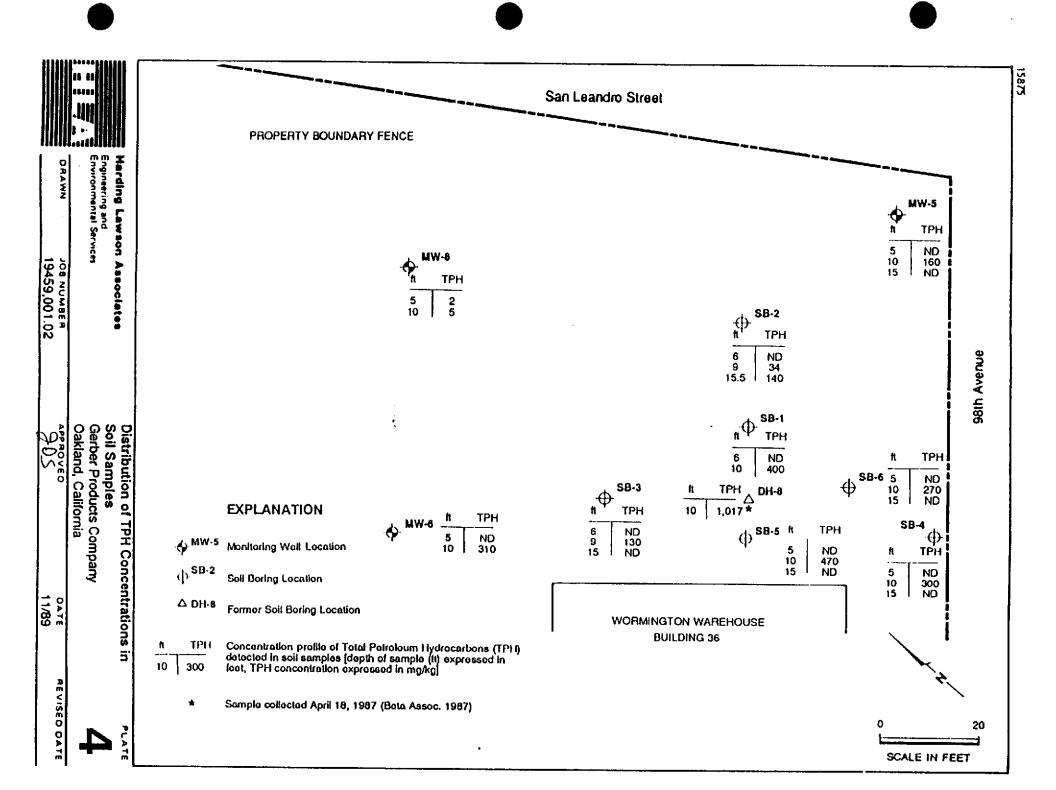
WELL NUMBER	SAMPLING DATE	DEPTH (FEET)	TPH (GASOLINE) mg/kg	BENZENE Ug/kg	TOLUENE ug/kg	BENZENE ug/kg	TOTAL ug/kg
		``	· · · · · · · · · · · · · · · · · · ·				
\$8-1 /	03-Aug-89	6-6.5	ND(10)	ND(5)	30	ND(5)	ND(5)
	03-Aug-89	19-10.5	460	1900	1400	4100	11000
SB - 2	03-Aug-89	6-6.5	ND(10)	ND(5)	ND(5)	ND(5)	ND(5)
	03-Aug-89	9-9.5	34	140	200	270	430
	03-Aug-89	15.5-16	-140 -	670	790	1300	4900
<b>58</b> -3	03-Aug-89	6-6.5	ND(10)	ND(5)	ND(5)	ND(5)	ND(5)
	03-Aug-89	9-9.5 ·	130	900	ND(100)	1500	3400
	03-Aug-89	15-15.5	ND(10)	ND(5)	ND(5)	ND(5)	ND(5)
S8-4 +	03-Aug-89	5.5.5	ND(10)	ND(5)	ND(5)	ND(5)	ND(5)
	03-Aug-89	10-10.5	300	3300	420	8200	12000
	03-Aug-89	15-15.5	ND(10)	ND(5)	ND(5)	ND(5)	ND(5)
\$8·5	03 · Aug · 89	5-5.5	ND(10)	47	ND(5)	ND(5)	ND(5)
	03-Aug-89	10-10.5	470	1960	580	7200	22000
	03-Aug-89	15-15.5	ND(10)	ND(5)	ND(5)	ND(S)	ND(5)
<b>\$8</b> *6 a	05-Oct-89	5-5.5	ND(10)	18	23	8.0	27
	05-Oct-89	10-10.5	270	2000	900	1600	3800
	05-Oct-89	15-15.5	ND(10)	33	34	5.5	26
MW-9	04-Aug-89	6-6.5	ND(10)	ND(5)	ND(5)	ND(5)	ND(5)
	04-Aug-89	12-12.5	ND(10)	ND (5)	ND(5)	ND(5)	ND(5)
MW-10	04 - Aug - 89	6-6.5	ND(10)	ND(5)	ND(5)	ND(5)	ND(5)
	04-Aug-89	12-12.5	ND(10)	ND(5)	ND(5)	ND(5)	ND(5)

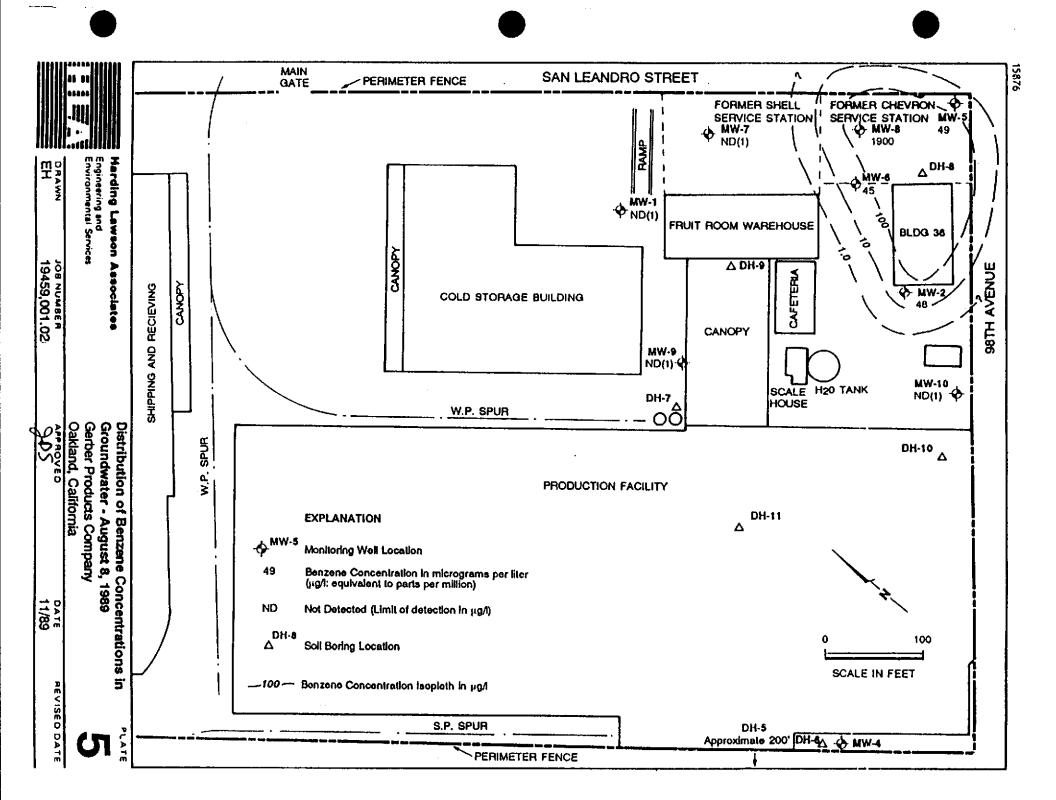
mg/kg: milligrams per kilogram (equivalent to parts per million)
ug/kg: micrograms per kilogram (equivalent to parts per billion)
ND: Not detected; Limit of detection indicated in parenthesis

Total Petroleum Hydrocarbons (TPH) by EPA Method 8015 Benzene, Toluene, Ethyl Benzene, Total Xylenes by EPA Method 8020 Extraction by EPA Method 5030, Purge and Trap

Analyses performed by Curtis & Tompkins, Ltd.

15704





# Appendix A

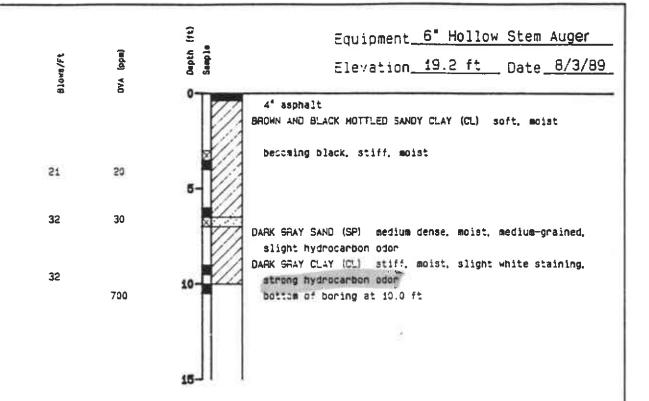
BORING LOGS AND WELL COMPLETION DETAILS

# Appendix A

# BORING LOGS AND WELL COMPLETION DETAILS

# LIST OF ILLUSTRATIONS

Plate A-1	Log of Boring SB-1
Plate A-2	Log of Boring SB-2
Plate A-3	Log of Boring SB-3
Plate A-4	Log of Boring SB-4
Plate A-5	Log of Boring SB-5
Plate A-6	Log of Boring SB-6
Plate A-7	Log of Boring and Well Completion Detail MW-9
Plate A-8	Log of Boring and Well Completion Detail MW-10
Plate A-9	Unified Soil Classification Chart





**Harding Lawson Associates** 

Engineering and **Environmental Services**  Log of Boring

Gerber Products Company Oakland, California

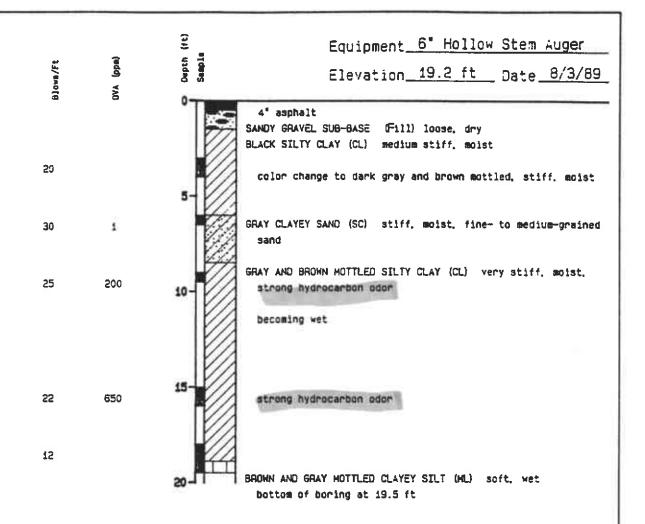
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1505°

DATE 11/89

JOB NUMBER



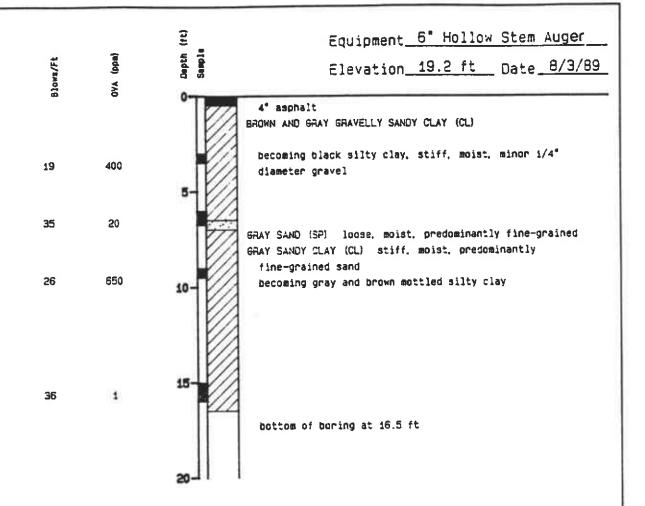


Engineering and Environmental Services Log of Boring

Gerber Products Company Oakland, California A-2

DRAWN JOB NUMBER 19459, 001.02 3PS

DATE 11/89 REVISED DATE





Engineering and Environmental Services

Log of Boring

Gerber Products Company Oakland, California

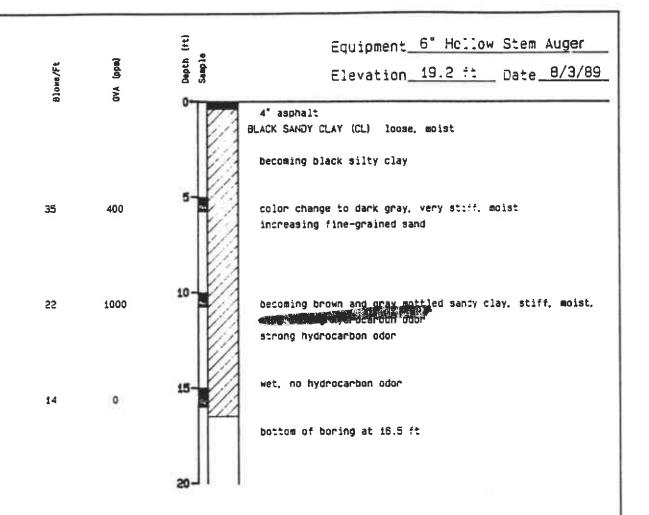
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DATE 11/89 REVISED DATE

PLATE

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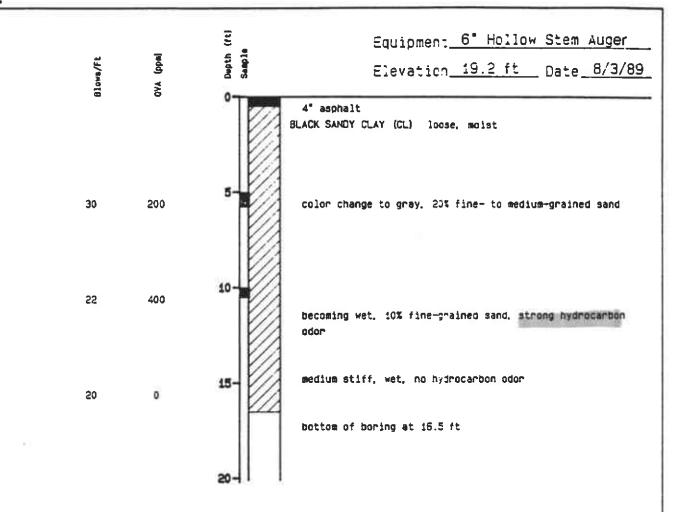


Engineering and **Environmental Services**  Log of Boring

Gerber Products Company Oakland, California

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Engineering and Environmental Services Log of Boring
Gerber Products Company
Oakland, California

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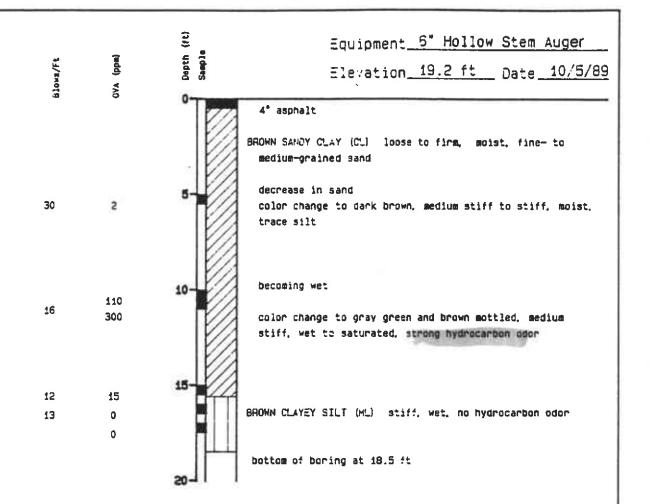
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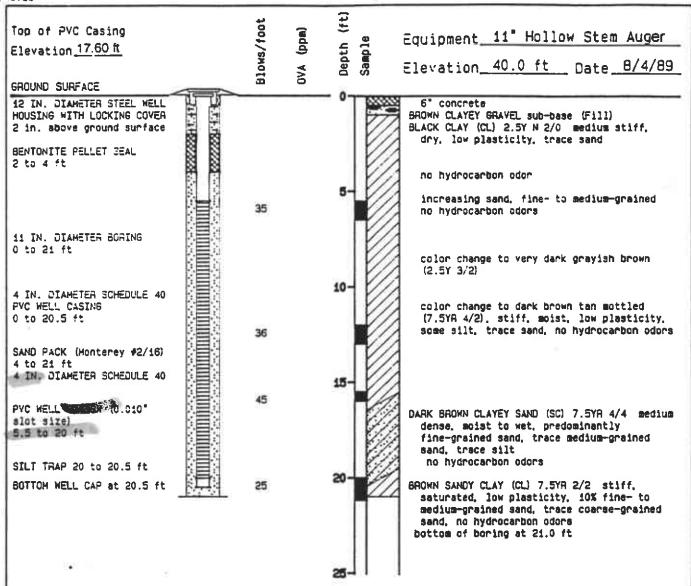


Engineering and Environmental Services Log of Boring Special Gerber Products Company Oakland, California

**A-6** 

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DATE 11/89 REVISED DATE





Engineering and **Environmental Services**  Log of Boring and Well Completion Detail

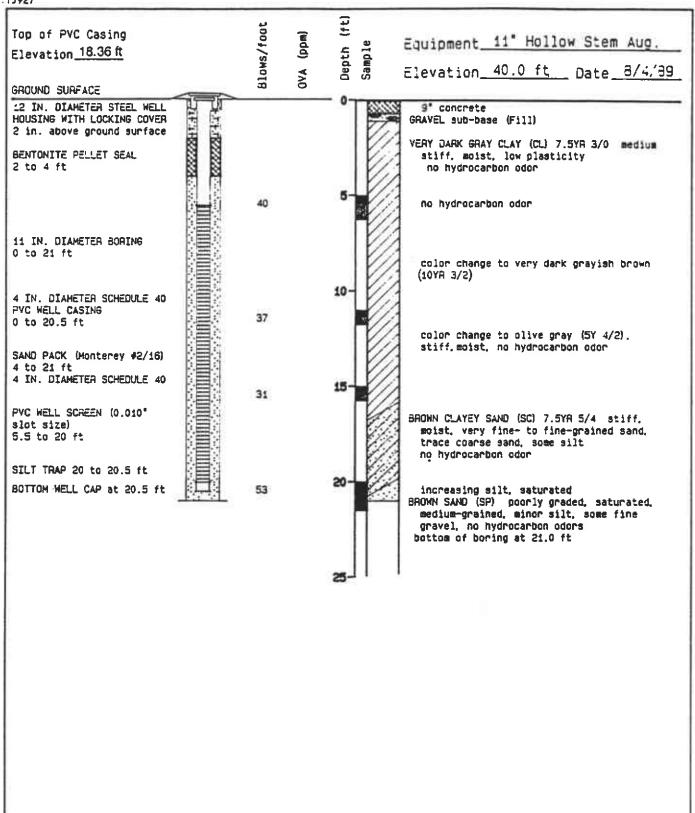
Gerber Products Company Oakland, California

JOB NUMBER

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DATE 11/89 REVISED DATE





Engineering and **Environmental Services**  Log of Boring and Well Completion Detail NOG-10 -Gerber Products Company

Oakland, California

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DATE 11/89 REVISED DATE

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	MAJOR DIV	/ISIONS			TYPICAL NAMES
COARSE—GRAINED SOILS MORE THAN HALF IS COARSER THAN NO. 200 SIEVE	GRAVELS  MORE THAN HALF COARSE FRACTION IS LARGER THAN NO. 4 SIEVE SIZE	CLEAN GRAVELS WITH	GW	S	WELL GRADED GRAVELS WITH OR WITHOUT SAND, LITTLE OR NO FINES
		LITTLE OR NO FINES	GP	É	POORLY GRADED GRAVELS WITH OR WITHOUT SAND, LITTLE OR NO FINES
		GRAVELS WITH OVER 12% FINES	GM		SILTY GRAVELS, SILTY GRAVELS WITH SAND
			GC	77	CLAYEY GRAVELS, CLAYEY GRAVELS WITH SAND
AN HA	SANDS  MORE THAN HALF COARSE FRACTION IS SMALLER THAN NO. 4 SIEVE SIZE	CLEAN SANDS WITH LITTLE OR NO FINES	sw		WELL GRADED SANDS WITH OR WITHOUT GRAVEL, LITTLE OR NO FINES
ARE TH			SP		POORLY GRADED SANDS WITH OR WITHOUT GRAVEL, LITTLE OR NO FINES
COV		SANDS WITH OVER 12% FINES	SM		SILTY SANDS WITH OR WITHOUT GRAVEL
			sc		CLAYEY SANDS WITH OR WITHOUT GRAVEL
FINE—GRAINED SOILS MORE THAN HALF IS FINER THAN NO. 200 SIEVE	SILTS AND CLAYS LIQUID LIMIT 50% OR LESS		ML		INORGANIC SILTS AND VERY FINE SANDS, ROCK FLOUR, SILTS WITH SANDS AND GRAVELS
			CL		INORGANIC CLAYS OF LOW TO MEDIUM PLASTICITY, CLAYS WITH SANDS AND GRAVELS, LEAN CLAYS
			OL		ORGANIC SILTS OR CLAYS OF LOW PLASTICITY
	SILTS AND CLAYS LIQUID LIMIT GREATER THAN 50%		мн		INORGANIC SILTS, MICACEOUS OR DIATOMACIOUS, FINE SANDY OR SILTY SOILS, ELASTIC SILTS
			СН		INORGANIC CLAYS OF HIGH PLASTICITY, FAT CLAYS
			он		ORGANIC SILTS OR CLAYS OF MEDIUM TO HIGH PLASTICITY
	HIGHLY ORGA	NIC SOILS	Pt	<b>=</b> :	PEAT AND OTHER HIGHLY ORGANIC SOILS

### UNIFIED SOIL CLASSIFICATION - ASTM D2487-85

"Undisturbed" Sample

Bulk or Classification Sample

Blows/foot: Number of blows from a 140 pound hammer dropped 30 inches required to advance the sampler one foot

OVA (ppm); Headspace concentration of volatile organic compounds from 4 ounces of soil palced in an 8 ounce glass jar for 10 minutes

#### KEY TO TEST DATA



Harding Lawson Associates Engineers and Geoscientists

Unified Soil Classification Chart Gerber Products Company Oakland, California

**A-9** 

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Appendix C

LABORATORY ANALYTICAL REPORTS FOR SOIL SAMPLES
SOIL SAMPLE IDENTIFICATION KEY

ample Number (Client ID)	Boring/Well Number	Depth (feet)
89080301	SB-1	6-6.5
89080302	SB-1	10-10.5
89080303	SB-2	6-6.5
89080304	SB-2	9-9.5
89080305	SB-2	15.5-16
89080306	SB-3	6-6.5
89080307	SB+3	9-9.5
89080308	SB-3	15-15.5
89080309	SB-4	5-5.5
89080310	SB-4	10-10.5
89080311	SB-4	15-15.5
89080312	SB-5	5-5.5
89080313	SB-5	10-10.5
89080314	SB-5	15-15.5
89100502	SB-6	5-5.5
89100503	SB-6	10-10.5
89100504	SB-6	15-15.5
89084001	MW-10	6-6.5
89084002	MW-10	12-12.5
89084003	MW-9	6-6.5
89084004	MW-9	12-12.5

# Appendix C LABORATORY ANALYTICAL REPORTS FOR SOIL SAMPLES

## Calculation Sheet 2. Stug Test of Well MW-8 (continued)

Test 1

Rising Head Test (Slug removed from well) Fully Penetrating Well

HYDRAULIC CONDUCTIVITY (K)

$$K = \frac{r_c^2 \ln(R_e/r_w)}{2L} \frac{1}{t} \ln \frac{v_0}{v_t}$$

where:  $y_0 = zero time y-axis intercept of linear portion of recovery data$ 

$$y_0 = 0.31$$
 feet

 $y_t = y_{-axis}$  intercept at time (t) of linear portion of recovery data

$$y_t = 0.15$$
 feet

t = <u>50</u> seconds

$$K = \frac{(0.193^2 (2.21))}{2(4)} \frac{1}{50} \text{ in } \frac{0.31}{0.15}$$

 $K = 1.5 \times 10^{-1}$  feet/second

 $K = 9.0 \times 10^{-3}$  Teet/minute

K = 12.9 feet/day

 $K = 4.5 \times 10^{-3}$  tentimeters/second

#### Calculation Sheet 1 . Slug Test of Well MW-8

Tests 1 and 2

Rising Head Test (Slug removed from well) Fully Penetrating Well

Method of Analysis: Bouwer and Rice (1976)

- H Hydraulic head above bottom of well screen
  (equals saturated thickness of aquifer)

  7 feet
- L Length of well screen through which water enters/exits well 4 [eet
- r Radius of well casing 0.086 feet
- r<sub>w</sub> Radius of weilbore 0.313 feet
- r<sub>c</sub> Effective radius of well casing (including porosity of gravel pack) 0.193 feet

$$r_C = [r^2 + \phi(r_w^2 - r^2)]^{1/2}$$

Calculation of In Re/rw:

$$\ln R_e/r_w = \frac{\frac{1}{1.1} + \frac{C}{L/r_w}}{\ln(H/r_w)}$$

where: R<sub>e</sub> = Effective radial distance in which the head change is dissipated

C = dimensionless parameter which is a function of L/r<sub>w</sub>, determined from analog model studies conducted by Bouwer and Rice (1976)

$$C = 1.25$$
 (unitless)

$$\ln R_e/r_w = \frac{1}{\ln(\frac{7}{0.313})} + \frac{1.25}{4.0.313}$$

$$\ln R_e/r_w = -2.21$$

Calculation Sheet 2 Slug Test of Well MW-6 (continued) Test 1

Rising Head Test (Slug removed from well) Fully Penetrating Well

HYDRAULIC CONDUCTIVITY (K)

$$K = \frac{r_c^2 \ln(R_e/r_w)}{2L} \frac{1}{t} \ln \frac{v_o}{v_t}$$

where:  $y_0 = z$  ero time y-axis intercept of linear portion of recovery data

$$y_0 = 0.34$$
 feet

 $y_t = y_t$  y-axis intercept at time (t) of linear portion of recovery data

$$y_t = 0.042$$
 feet

t = 40 seconds

$$K = \frac{0.202^{2}(2.35)}{2(4)} \frac{1}{40} \text{ In } \frac{0.34}{0.042}$$

$$K = 6.3 \times 10^{-4}$$
 feet/second

$$K = 3.8 \times 10^{-2}$$
 feet/minute

$$K = 54.1$$
 feet/day

$$K = 1.9 \times 10^{-2}$$
 centimeters/second

# Calculation Sheet 3. Slug Test of Well MW-6 (continued) Test 2

Rising Head Test (Slug removed from well) Fully Penetrating Well

HYDRAULIC CONDUCTIVITY (K)

$$K = \frac{r_c^2 \ln(R_e/r_w)}{2L} \frac{1}{t} \ln \frac{v_o}{v_t}$$

where: y<sub>0</sub> = zero time y-axis intercept of linear portion of recovery data

$$y_0 = 0.27$$
 feet

y<sub>t</sub> = y-axis intercept at time (t) of linear portion of recovery data

$$y_t = 0.067$$
 feet

$$K = \frac{0.202}{2(-4)} \frac{(-2.35)}{40}$$
 In  $\frac{0.27}{0.047}$ 

 $K = 5.2 \times 10^{-4}$  feet/second

 $K = 3.1 \times 10^{-2}$  feet/minute

K = 45.3 feet/day

 $K = 1.6 \times 10^{-2}$  centimeters/second

### Calculation Sheet 1. Slug Test of Well MW-6

Tests 1 and 2

Rising Head Test (Slug removed from well) Fully Penetrating Well

Method of Analysis: Bouwer and Rice (1976)

- H Hydraulic head above bottom of well screen
  (equals saturated thickness of aquifer) \_\_\_\_\_ 9 \_\_\_ feet
- L Length of well screen through which water enters/exits well \_\_\_\_\_4 feet
- r Radius of well casing 0.086 feet
- r<sub>w</sub> Radius of wellbore 0.313 feet
- φ Porosity of gravel pack (assumed) 0.37 unitless

$$r_C = [r^2 + \phi(r_w^2 - r^2)]^{1/2}$$

Calculation of In Re/rw:

$$\ln R_e/r_w = \frac{1}{\ln(H/r_w)} + \frac{C}{L/r_w}$$

- where: R<sub>e</sub> = Effective radial distance in which the head change is dissipated
  - C = dimensionless parameter which is a function of L/r<sub>w</sub>, determined from analog model studies conducted by Bouwer and Rice (1976)

$$\ln R_e/r_w = \frac{1}{\ln(-9.0.313)} + \frac{1.25}{4.0.313}$$

$$\ln R_e/r_w = \frac{2.35}{1.00}$$

# Calculation Sheet 3. Slug Test of Well MW-5 (continued) Test 2

Rising Head Test (Slug removed from well) Fully Penetrating Well

HYDRAULIC CONDUCTIVITY (K)

$$K = \frac{r_c^2 \ln(R_e/r_w)}{2L} \frac{1}{t} \ln \frac{v_o}{y_t}$$

where:  $y_0 = z$  ero time y-axis intercept of linear portion of recovery data

$$y_0 = 0.47$$
 feet

 $y_t = y$ -axis intercept at time (t) of linear portion of recovery data

$$y_t = 0.17$$
 feet

t = 40 seconds

$$K = \frac{(0.163^2 (2.43))}{2(.5)} \frac{1}{40} \text{ In } \frac{0.47}{0.17}$$

 $K = 1.6 \times 10^{-4}$  feet/second

K =9.8 X 10<sup>-2</sup> feet/minute

K = 13.8 feet/day

 $K = 5.0 \times 10^{-3}$  centimeters/second

# Calculation Sheet 2 . Slug Test of Well MW-5 (continued) Test 1

Rising Head Test (Slug removed from well) Fully Penetrating Well

HYDRAULIC CONDUCTIVITY (K) -

$$K = \frac{rc^2 \ln(R_e/r_w)}{2L} \frac{1}{t} \ln \frac{v_0}{y_t}$$

where: y<sub>0</sub> = zero time y-axis intercept of linear portion of recovery data

$$y_0 = 0.48$$
 feet

 $y_t = y_{-axis}$  intercept at time (t) of linear portion of recovery data

$$y_t = 0.13$$
 feet

t = <u>40</u> seconds

$$K = \frac{(0.163)^2 \cdot (2.43)}{2(5)} \quad \frac{1}{40} \quad \text{in} \quad \frac{0.48}{0.13}$$

 $K = 2.1 \times 10^{-4}$  feet/second

 $K = 1.3 \times 10^{-2}$  feet/minute

K = 18.2 feet/day

 $K = 6.4 \times 10^{-3}$  centimeters/second

Calculation Sheet 1 . Slug Test of Well MN-5

Tests 1 and 2

Rising Head Test (Slug removed from well) Fully Penetrating Well

Method of Analysis: Bouwer and Rice (1976)

Н Hydraulic head above bottom of well screen (equals saturated thickness of aquifer)

10 fect

Length of well screen through which water enters/exits well

feet

Radius of well casing

0.086 feet

Radius of wellbore ۲w

0.313 feet

φ Porosity of gravel pack (assumed) 0.21 unitless

Effective radius of well casing ۲<sub>C</sub> (including porosity of gravel pack)

\_0.163\_\_ feet

$$r_c = [r^2 + \phi(r_w^2 - r^2)]^{1/2}$$

Calculation of In Re/rw:

$$\ln R_e/r_w = \frac{1}{\ln(H/r_w)} + \frac{C}{L/r_w}$$

where:  $R_e =$ Effective radial distance in which the head change is dissipated

> C = dimensionless parameter which is a function of L/rw, determined from analog model studies conducted by Bouwer and Rice (1976)

$$\ln R_e/r_w = \frac{1}{\ln(\frac{10}{0.313})} + \frac{1.5}{5.0.313}$$

$$\ln R_e/r_w = \frac{2.43}{}$$

# Calculation Sheet 3. Slug Test of Well MM-2 (continued) Test 2

\_\_\_

Rising Head Test (Slug removed from well) Fully Penetrating Well

HYDRAULIC CONDUCTIVITY (K)

$$K = \frac{r_c^2 \ln(R_e/r_w)}{2L} \quad \frac{1}{t} \quad \text{in} \quad \frac{v_0}{y_t}$$

where:  $y_0 = z$  ero time y-axis intercept of linear portion of recovery data

$$y_0 = 0.50$$
 feet

y<sub>t</sub> = y-axis intercept at time (t) of linear portion of recovery data

$$y_t = 0.050$$
 feet

t = <u>40</u> - seconds

$$K = \frac{(0.161)^2}{2(4.0)} \frac{(2.35)}{40}$$
 in  $\frac{0.50}{0.050}$ 

$$K = 4.4 \times 10^{-1}$$
 feet/second

$$K = 2.6 \times 10^{-2}$$
 feet/minute

$$K = 37.9$$
 feet/day

$$K = 1.3 \times 10^{-2}$$
 centimeters/second

## Calculation Sheet 2. Slug Test of Well <u>MW-2</u> (continued) Test 1

Rising Head Test (Slug removed from well) Fully Penetrating Well

HYDRAULIC CONDUCTIVITY (K)

$$K = \frac{r_c^2 \ln(R_e/r_w)}{2L} \frac{1}{t} \ln \frac{y_0}{y_t}$$

where:  $y_0 =$  zero time y-axis intercept of linear portion of recovery data

$$y_0 = 0.41$$
 feet

 $y_t = y_{-axis}$  intercept at time (t) of linear portion of recovery data

$$y_t = 0.051$$
 feet

t = 40 seconds

$$K = \frac{0.160^2 (2.35)}{2(4.0)} \frac{1}{40} \text{ in } \frac{0.41}{0.051}$$

 $K = 4.0 \times 10^{-4} \text{ feet/second}$ 

 $K = 2.4 \times 10^{-2} \text{ feet/minute}$ 

K = 34.3 feet/day

 $K = 1.2 \times 10^{-2}$  centimeters/second

### Calculation Sheet 1. Slug Test of Well MW-2

Tests 1 and 2

Rising Head Test (Slug removed from well) Fully Penetrating Well

Method of Analysis: Bouwer and Rice (1976)

- H Hydraulic head above bottom of well screen (equals saturated thickness of aquifer) 9.0 feet
- L Length of well screen through which water enters/exits well 4.0 feet
- r Radius of well casing 0.086 feet
- rw Radius of wellbore 0.333 feet
- φ Porosity of gravel pack (assumed) 0.18 unitless
- r<sub>c</sub> Effective radius of well casing (including porosity of gravel pack) 0.161 feet

$$r_C = [r^2 + \phi(r_w^2 + r^2)]^{1/2}$$

Calculation of In Re/rw:

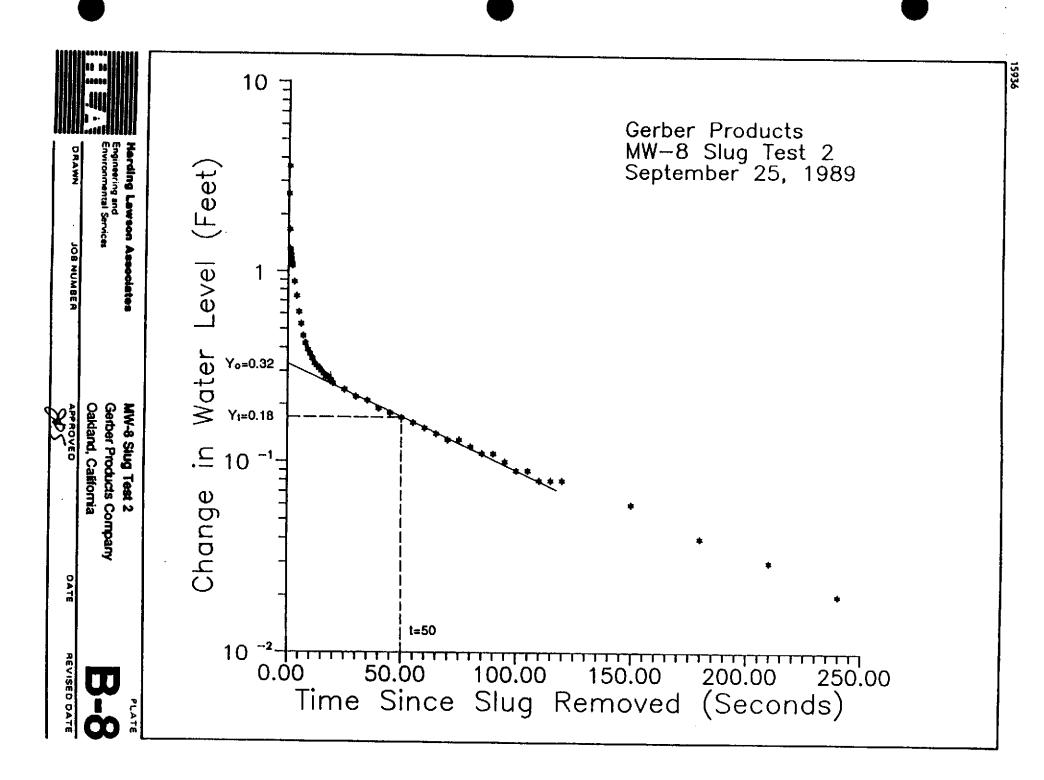
$$\ln R_e/r_w = \frac{1}{\ln(H/r_w)} + \frac{C}{L/r_w}$$

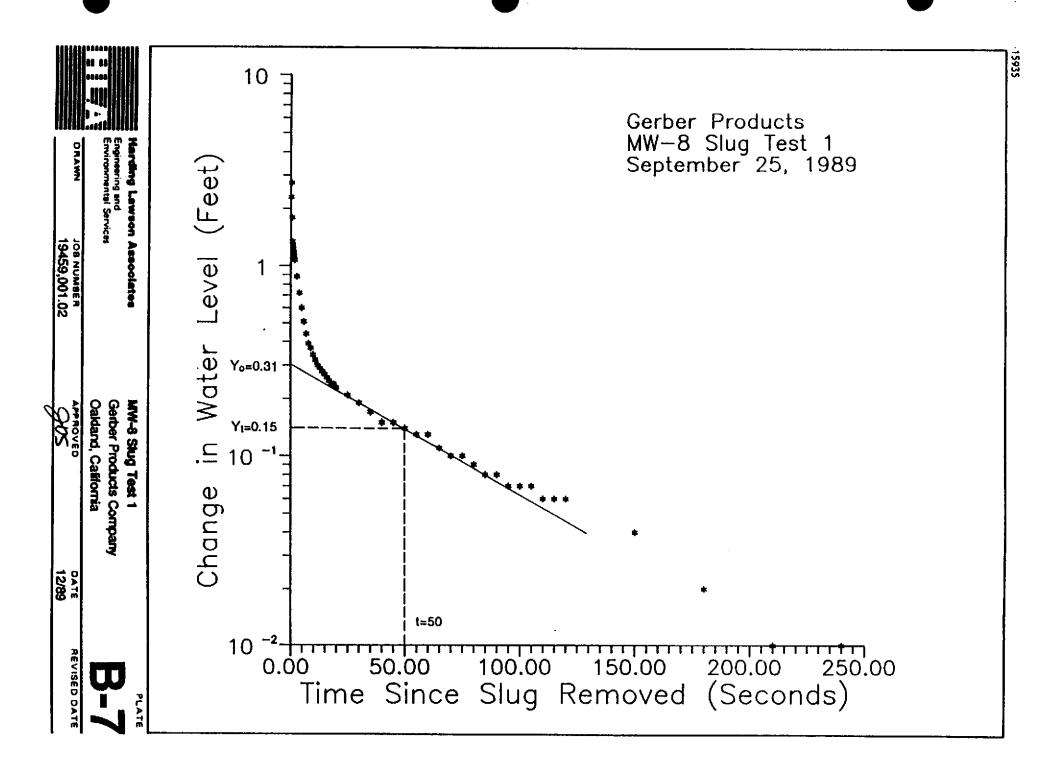
- where: R<sub>e</sub> = Effective radial distance in which the head change is dissipated
  - C = dimensionless parameter which is a function of L/r<sub>w</sub>, determined from analog model studies conducted by Bouwer and Rice (1976)

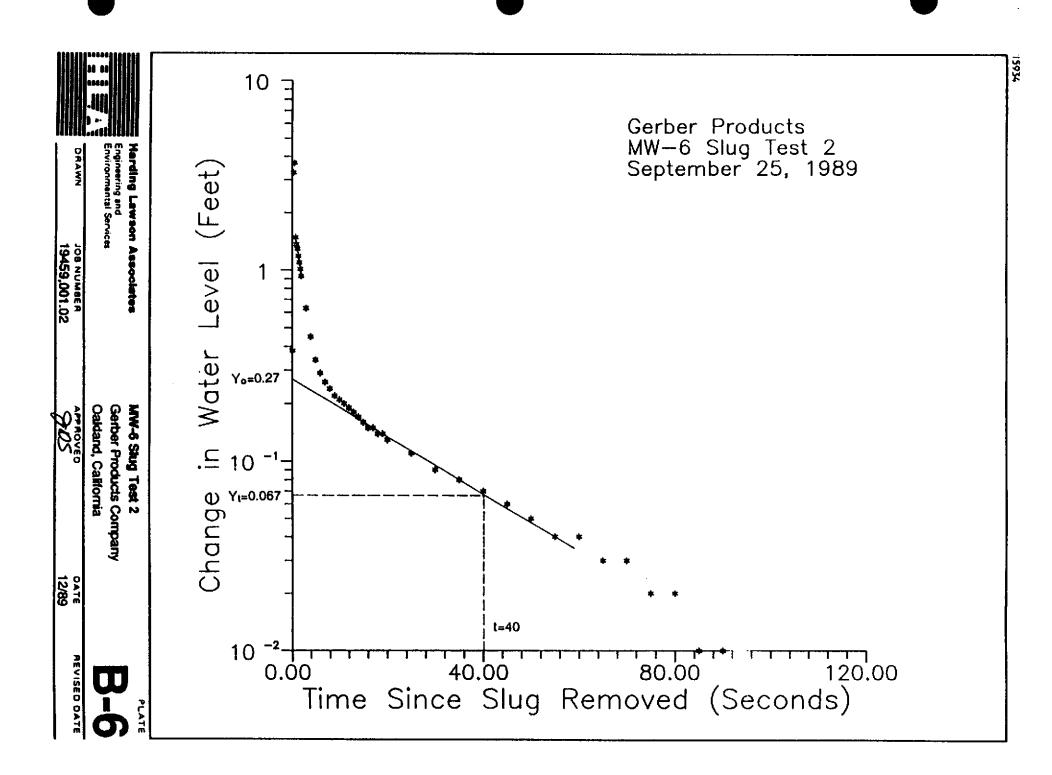
$$C = 1.9$$
 (unitless)

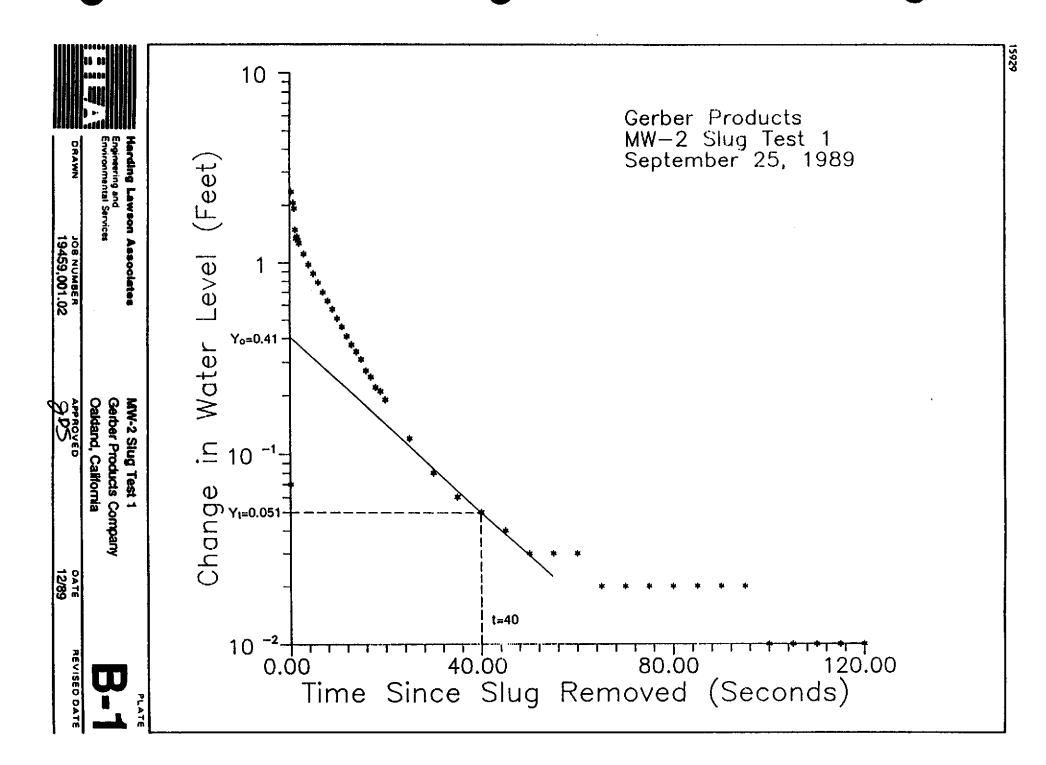
$$\ln R_e/r_w = \frac{1.1}{\ln(9.333)} + \frac{1.9}{4.0.333}$$

$$\ln R_e/r_w = \frac{2.35}{}$$

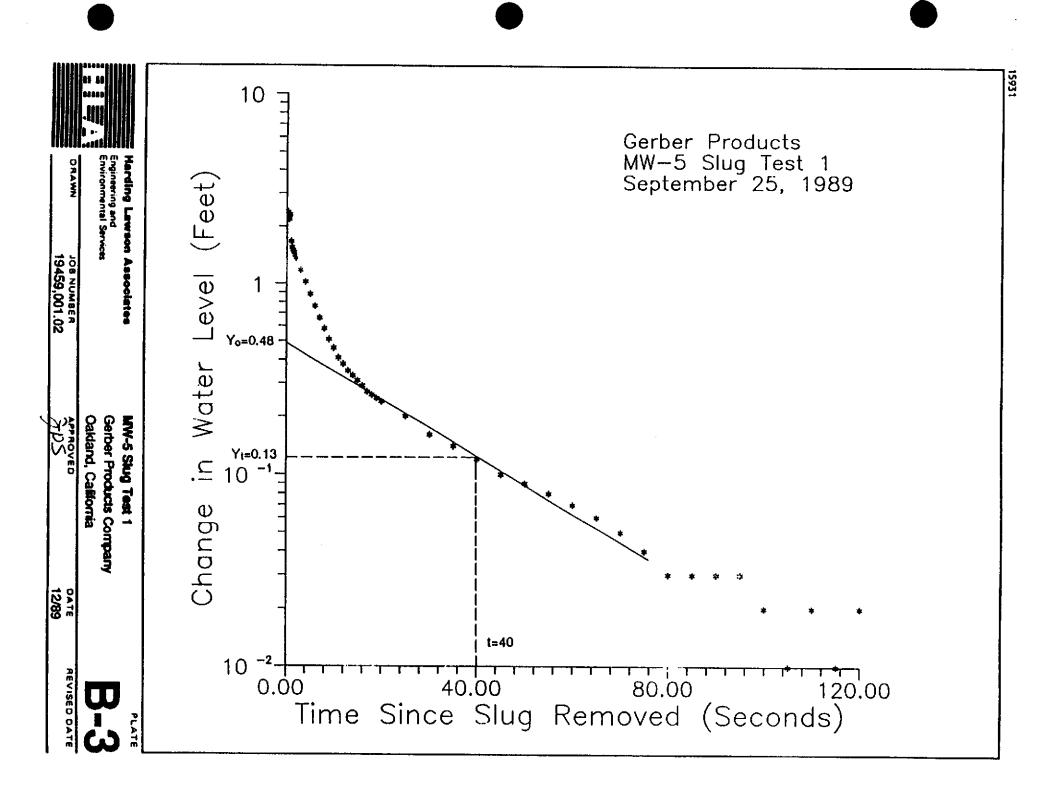


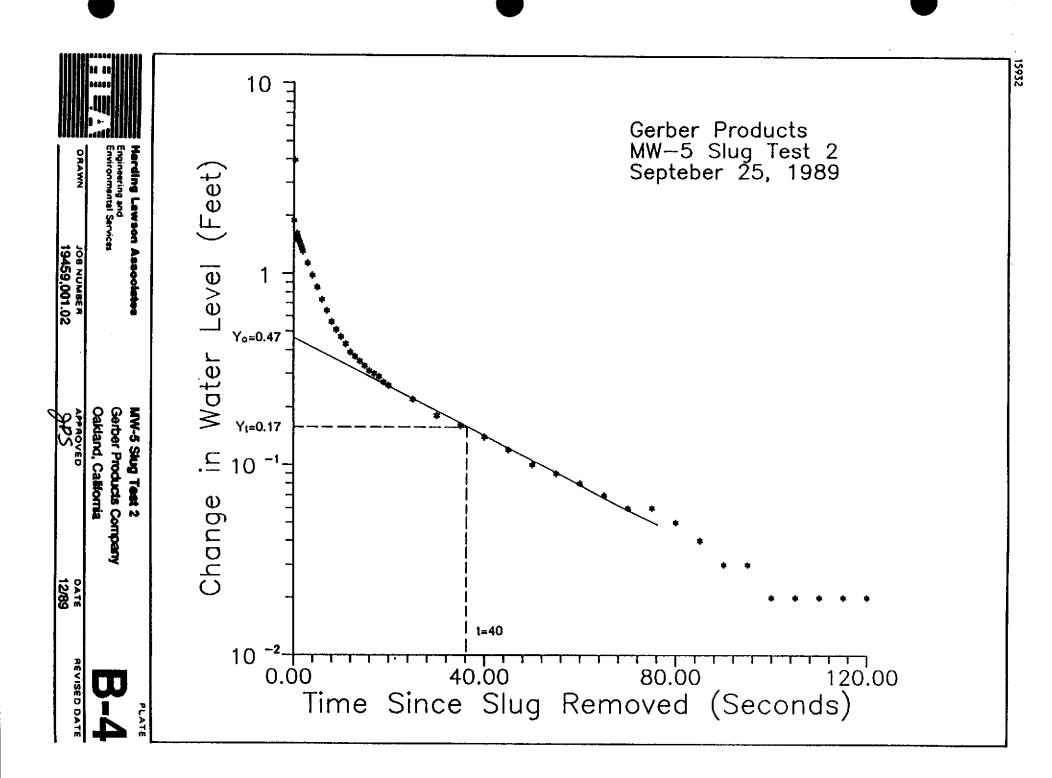


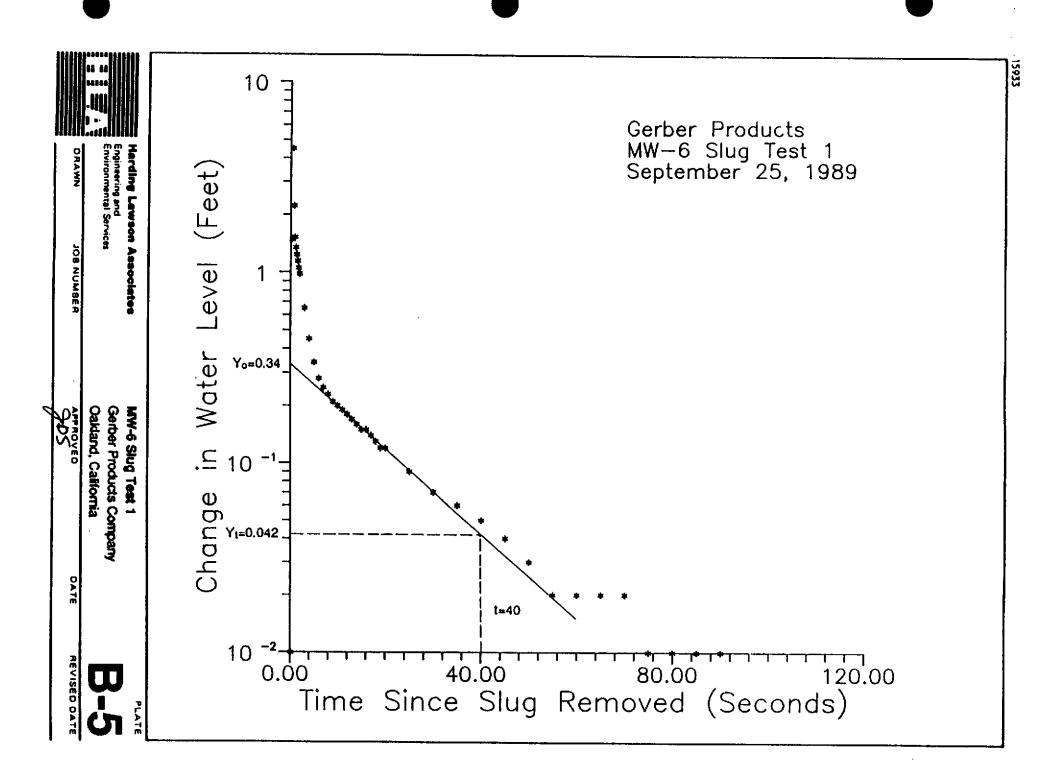




10 Gerber Products MW-2 Slug Test 2 September 25, 1989 Level (Feet) 19459,001.02 Yo=0.50 Water MW-2 Slug Test 2
Gerber Products Company .⊑ 10 DATE 12/89 1=40 10 120.00 REVISED DATE 40.00 0.00 00.08 Time Since Slug Removed (Seconds)







Appendix B
SLUG TEST DATA

#### Appendix B

#### SLUG TEST DATA

### LIST OF ILLUSTRATIONS

Plate B-I	MW-2 Slug Test 1
Plate B-2	MW-2 Slug Test 2
Plate B-3	MW-5 Slug Test I
Plate B-4	MW-5 Slug Test 2
Plate B-5	MW-6 Slug Test 1
Plate B-6	MW-6 Slug Test 2
Plate B-7	MW-8 Slug Test 1
Plate B-8	MW-8 Slug Test 2

## Curtis & Tompkins, Ltd., Analytical Laboratories, Since 1878

2323 Fifth Street, Berkeley, CA 9471O, Phone (415) 486-0900

DATE RECEIVED: 08/04/89 DATE REPORTED: 08/15/89

PAGE 1 OF 2

LAB NUMBER: 17953

CLIENT: HARDING LAWSON ASSOCIATES

REPORT ON: 14 SOIL SAMPLES

JOB #: 19459,001.02 LOCATION: GERBER

RESULTS: SEE ATTACHED

Laboratory Director



LABORATORY NUMBER: 17953

CLIENT: HARDING LAWSON ASSOCIATES

JOB NUMBER: 19459,001.02

JOB LOCATION: GERBER

. **.** 

DATE RECEIVED: 08/04/89 DATE ANALYZED: 08/09/89 DATE REPORTED: 08/15/89

PAGE 2 OF 2

Total Volatile Hydrocarbons (TVH) by EPA 8015 Benzene, Toluene, Ethyl Benzene, Xylenes by EPA 602/8020 Extraction by EPA 5030 Purge and Trap

LAB ID	CLIENT ID	TVH AS GASOLINE (mg/Kg)	BENZENE (ug/Kg)	TOLUENE	ETHYL BENZENE (ug/Kg)	TOTAL XYLENES (ug/Kg)
17953-1 17953-2 17953-3 17953-4 17953-5 17953-6 17953-7 17953-8 17953-1 17953-1 17953-1 17953-1	89080311 89080312 89080313	ND(10) 400 ND(10) 34 140 ND(10) 130 ND(10) ND(10) ND(10) ND(10) ND(10) ND(10) ND(10)	ND(5) 1,900 ND(5) 140 670 ND(5) 900 ND(5) ND(5) 3,300 ND(5) 47 1,900 ND(5)	30 1,400 ND(5) 200 790 ND(5) ND(5) ND(5) 420 ND(5) ND(5) ND(5) ND(5)	ND(5) 4,100 ND(5) 270 1,300 ND(5) 1,500 ND(5) ND(5) 8,200 ND(5) ND(5) 7,200 ND(5)	ND(5) 11,000 ND(5) 430 4,900 ND(5) 3,400 ND(5) ND(5) 12,000 ND(5) ND(5) ND(5) ND(5)

ND = None Detected; Limit of detection is indicated in parentheses.

### QA/QC SUMMARY

%RPD	8	
*RECOVERY	103	



### Curtis & Tompkins, Ltd., Analytical Laboratories, Since 1878

2323 Fifth Street, Berkeley, CA 94710. Phone (415) 486-0900

LABORATORY NUMBER: 17958

CLIENT: HARDING LAWSON ASSOCIATES

JOB NUMBER: 19459,001.02 JOB NAME: GERBER PRODUCTS DATE RECEIVED: 08/04/89
DATE ANALYZED: 08/07/89

DATE REPORTED: 08/16/89

Total Volatile Hydrocarbons (TVH) by EPA 8015
Benzene, Toluene, Ethyl Benzene, Xylenes by EPA 602/8020
Extraction by EPA 5030 Purge and Trap

LAB ID	CLIENT ID	TVH AS GASOLINE (mg/Kg)	BENZENE (ug/Kg)	TOLUENE	ETHYL BENZENE (ug/Kg)	TOTAL XYLENES (ug/Kg)
17958-1	89084001	ND(10)	ND(5)	ND(5)	ND(5)	ND(5)
17958-2	89084002	ND(10)	ND(5)	ND(5)	ND(5)	ND(5)
17958-3	89084003	ND(10)	ND(5)	ND(5)	ND(5)	ND(5)
17958-4	89084004	ND(10)	ND(5)	ND(5)	ND(5)	ND(5)

ND = None Detected; Limit of detection is indicated in parentheses.

#### QA/QC SUMMARY

%RPD	<1	
*RECOVERY	96	

LABORATORY DIRECTOR

Wilmington

Los Angeles



## Curtis & Tompkins, Ltd., Analytical Laboratories, Since 1878

2323 Fifth Street, Berkeley, CA 9471O. Phone (415) 486-0900

DATE RECEIVED: 10/05/89 DATE REPORTED: 10/17/89

PAGE 1 OF 2

LAB NUMBER: 18434

CLIENT: HARDING LAWSON ASSOCIATES

REPORT ON: 3 SOIL SAMPLES

JOB #: 19459,001.02 LOCATION: GERBER

RESULTS: SEE ATTACHED

Wilmington Los Angeles



LABORATORY NUMBER: 18434

CLIENT: HARDING LAWSON ASSOCIATES

JOB NUMBER: 19459,001.02 JOB LOCATION: GERBER DATE RECEIVED: 10/05/89
DATE ANALYZED: 10/16/89
DATE REPORTED: 10/17/89

PAGE 2 OF 2

Total Volatile Hydrocarbons (TVH) by EPA 8015 Benzene, Toluene, Ethyl Benzene, Xylenes by EPA 602/8020 Extraction by EPA 5030 Purge and Trap

LAB ID	CLIENT ID	TVH AS GASOLINE (mg/Kg)	BENZENE (ug/Kg)	TOLUENE (ug/Kg)	ETHYL BENZENE (ug/Kg)	TOTAL XYLENES (ug/Kg)
18434-1	89100502	ND(10)	18	23	8.0	27
18434-2	89100503 .	270	2,000	900	1,600	3,800
18434-3	89100504	ND(10)	33	34	5.5	26

ND = None Detected; Limit of detection is indicated in parentheses.

#### QA/QC SUMMARY

%RPD	<1	
*RECOVERY	87	
******		



.ng L. .m A 200 Rush Landing Road P.O. Box 6107 Novato, California 94948 415/892-0821 Telecopy: 415/892-1586 stes

# CHAIN THE CUSTODY FORM

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# CHAIN OF CUSTODY FORM

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Telecopy: 415/892-1586

### CHAIN OF CUSTODY FORM

Samplers: G. LIEBERMAN

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ANALYSIS REQUESTED

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# CHAIN OF CUSTODY FORM

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#### Appendix D

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LABORATORY ANALYTICAL RESULTS FOR GROUND-WATER SAMPLES

Appendix D

LABORATORY ANALYTICAL REPORTS FOR GROUND-WATER SAMPLES
GROUND-WATER SAMPLE IDENTIFICATION KEY

Sample ID	Monitoring Well Number
MW010808	MW-1
MW020808	MW-2
MW030808	Field Blank
MW040808	MW-4
MW050808	MW-5
MW060808	MW-6
MW070808	MW-7
MW080808	MW-8
MW090808	MW-9
MW100808	MW-10

DATE RECEIVED: 08/08/89 DATE REPORTED: 08/30/89

PAGE 1 OF 12

LAB NUMBER: 17977

CLIENT: HARDING LAWSON ASSOCIATES

REPORT ON: 10 WATER SAMPLES

JOB #: 19459,001.02

LOCATION: GERBER PRODUCTS

RESULTS: SEE ATTACHED

NOTE: All samples were originally analyzed and quantified on 8/9/89. Samples were subsequently reanalyzed to achieve lower detection limits at the request of the client. Quantifications from the first analysis, which was closer to the sampling event, have generally been reported and are marked with an asterisk (\*). Surrogate recoveries from both sets of analyses are reported.

Laboratory Director

Wilmington

Los Angeles



CLIENT: HARDING LAWSON ASSOCIATES

JOB #: 19459,001.02 SAMPLE ID: MW020808

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DATE RECEIVED: 08/08/89 ANALYSIS 1 (\*) 08/09/89 ANALYSIS 2 08/23/89 DATE REPORTED: 08/30/89

PAGE 2 OF 12

### EPA METHOD 624: VOLATILE ORGANICS IN WATER

COMPOUND	Resu ug/			Detection Limit ug/L
chloromethane	ND			_ <u>.</u>
bromomethane	ND			
vinyl chloride	ND			2
chloroethane	ND			2
methylene chloride	ND			1
trichlorofluoromethane	ND			2 2 2 1 1
1,1-dichloroethene	ND			1
1,1-dichloroethane	ND			1
trans-1,2-dichloroethene	ND			1
chloroform	ND			i
1,2-dichloroethane	ND			1
1,1,1-trichloroethane	ND			i
carbon tetrachloride	ND			1
bromodichloromethane.	ND			1
1,2-dichloropropane	ND			i
cis-1,3-dichloropropene	ND			1
trichloroethylene	ND			1
dibromochloromethane	ND			1
1,1,2-trichloroethane	ND			1
benzene	RD	48	+	1
trans-1,3-dichloropropene	ND	70	_	1
2-chloroethylvinyl ether	ND			2
bromoform	ND			<u>2</u> 1
1,1,2,2-tetrachloroethane				÷
tetrachloroethylene	ND			±
toluene	ND	_		Ţ
chlorobenzene	3.00	9	#	Ţ
ethyl benzene	ND	33		Ţ
ecuya Denzene		33	ন	1

acetone	ND	2
carbon disulfide	ND	1
2-butanone	,	Ţ
	ND	2
vinyl acetate	ND	2
2-hexanone	ND	2
4-methyl-2-pentanone	ND	2
styrene	ND	1
total xylenes	55 *	ī
QA/QC SUMMARY: SURROGATE RECOVERIES		
1,2-Dichloroethane-d4	109%	96%
Toluene-d8	101%	103%
· · · · · · · · · · · · · · · · · · ·		
Bromofluorobenzene	95%	90%



CLIENT: HARDING LAWSON ASSOCIATES

JOB #: 19459.001.02

SAMPLE ID: MWO50808

DATE RECEIVED: 08/08/89 DATE ANALYZED: 08/09/89 DATE REPORTED: 08/16/89

PAGE 3 OF 12

#### EPA METHOD 624: VOLATILE ORGANICS IN WATER

COMPOUND	Result ug/L	Detection Limit ug/L
chloromethane	ND	10
bromomethane	ND	10
vinyl chloride	ND	10
chloroethane	ND	10
methylene chloride	ND	
trichlorofluoromethane	ND	ξ
1,1-dichloroethene	ND	5
1,1-dichloroethane	ND	5
trans-1,2-dichloroethene	ND	5
chloroform	ND	<u> </u>
1,2-dichloroethane	ND	5
1,1,1-trichloroethane	ND	5
carbon tetrachloride	ND	. 5
bromodichloromethane -	ND	5555555555555555555
1,2-dichloropropane	ND	5
cis-1,3-dichloropropene	ND	5
trichloroethylene	ND	٠ ۲
dibromochloromethane	ND	<u> </u>
1,1,2-trichloroethane	ND	<del>~</del> <del>~</del>
benzene	49	5
trans-1,3-dichloropropene	ND	ے ج
2-chloroethylvinyl ether	ND	10
bromoform	ND	5
1,1,2,2-tetrachloroethane	ND	5
tetrachloroethylene	ND	5
toluene	8	5
chlorobenzene	ND	10 5 5 5 5 5
ethyl benzene	15	J 5
		<b>.</b>

acetone	ND	10
carbon disulfide	ND	5
2-butanone	ND	10
vinyl acetate	ND	10
2-hexanone	ND	10
4-methyl-2-pentanone	ND	10
styrene	ND	5
total xylenes	63	5

QA/QC SUMMARY: SURROGATE RECOVERIES	
1,2-Dichloroethane-d4	106%
Toluene-d8	99%
Bromofluorobenzene	96%



CLIENT: HARDING LAWSON ASSOCIATES

JOB #: 19459,001.02 SAMPLE ID: MW080808 DATE RECEIVED: 08/08/89 ANALYSIS 1 (\*) 08/09/89 ANALYSIS 2 08/23/89 DATE REPORTED: 08/30/89

PAGE 4 OF 12 EPA METHOD 624: VOLATILE ORGANICS IN WATER

COMPOUND	Result ug/L	Detection Limit ug/L
chloromethane	ND	2
bromomethane	ND	2
vinyl chloride	ND	2
chloroethane	ND	2
methylene chloride	ND	2 2 1
trichlorofluoromethane	ND	ī
1,1-dichloroethene	ND	ī
1,1-dichloroethane	ND	ī
trans-1,2-dichloroethene	ND	1
chloroform	ND	1
1,2-dichloroethane	ND	1
1,1,1-trichloroethane	ND	1
carbon tetrachloride	ND	1
bromodichloromethane ·	ND	1
1,2-dichloropropane	ND	1
cis-1,3-dichloropropene	ND	1
trichloroethylene	ND	1
dibromochloromethane	ND	1
1,1,2-trichloroethane	ND	1
benzene	1,900 *	1
trans-1,3-dichloropropene	ND	1
2-chloroethylvinyl ether	ND	2
bromoform	ND	1
1,1,2,2-tetrachloroethane	ND	1
tetrachloroethylene	ND	1
toluene	820 *	1
chlorobenzene	ND	1
ethyl benzene	1,000 *	1

acetone carbon disulfide 2-butanone vinyl acetate 2-hexanone 4-methyl-2-pentanone styrene total xylenes	ND ND ND ND ND ND ND ND 3,600 *	2 1 2 2 2 2 2 1	
QA/QC SUMMARY: SURROGATE RECOVERIES 1,2-Dichloroethane-d4 Toluene-d8 Bromofluorobenzene	102% 99% 104%	104% 88% 92%	



CLIENT: HARDING LAWSON ASSOCIATES

JOB #: 19459,001.02 SAMPLE ID: MW060808

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DATE RECEIVED: 08/08/89 ANALYSIS 1 (\*) 08/09/89 ANALYSIS 2 08/23/89 DATE REPORTED: 08/30/89

PAGE 5 OF 12

#### EPA METHOD 624: VOLATILE ORGANICS IN WATER

COMPOUND	Result ug/L	Detection Limit ug/L
chloromethane	ND	
bromomethane	ND	2
vinyl chloride	ND	2 2 2 2
chloroethane	ND	2
methylene chloride	ND	1
trichlorofluoromethane	ND	ī
1,1-dichloroethene	ND	ī
1,1-dichloroethane	ND	ī
trans-1,2-dichloroethene	ND	ī
chloroform	ND	ĩ
1,2-dichloroethane	ND	ī
1,1,1-trichloroethane	ND	1
carbon tetrachloride	ND	ī
bromodichloromethane -	ND	1
1,2-dichloropropane	ND	1
cis-1,3-dichloropropene	ND	1
trichloroethylene	ND	1
dibromochloromethane	ND	1
1,1,2-trichloroethane	ND	1
benzene	45 *	1
trans-1,3-dichloropropene	ND	1
2-chloroethylvinyl ether	ND	2
bromoform	ND	1
1,1,2,2-tetrachloroethane	ND	1
tetrachloroethylene	ND	1
toluene	8 *	1
chlorobenzene	ND	ī
ethyl benzene	15 *	1

acetone carbon disulfide 2-butanone vinyl acetate 2-hexanone 4-methyl-2-pentanone styrene total xylenes	ND ND ND ND ND ND ND	2 1 2 2 2 2 2 1 1	
QA/QC SUMMARY: SURROGATE RECOVERIES 1,2-Dichloroethane-d4 Toluene-d8 Bromofluorobenzene	108% 100% 99%	91% 100% 89%	



CLIENT: HARDING LAWSON ASSOCIATES

JOB #: 19459,001.02 SAMPLE ID: MW040808

DATE RECEIVED: 08/08/89 ANALYSIS 1 (\*) 08/09/89 ANALYSIS 2 08/22/89 DATE REPORTED: 08/30/89

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#### EPA METHOD 624: VOLATILE ORGANICS IN WATER

		<b>31</b> (
	Result	Detection
COMPOUND	ug/L	Limit
		ug/L
chloromethane	ND	Ž
bromomethane	ND	2
vinyl chloride	ND	2 2
chloroethane	ND	2
methylene chloride	ND	1
trichlorofluoromethane	ND	1
1,1-dichloroethene	ND	1
1,1-dichloroethane	ND	1
trans-1,2-dichloroethene	ND	1
chloroform	ND	1
1,2-dichloroethane	ND	1
1,1,1-trichloroethane	ND	1
carbon tetrachloride	ND	1
bromodichloromethane '	ND	1
1,2-dichloropropane	ND	1
cis-1,3-dichloropropene	ND	1
trichloroethylene	ND	1
dibromochloromethane	ND	1
1,1,2-trichloroethane	ND	1
benzene	ND	1
trans-1,3-dichloropropene	ND	1
2-chloroethylvinyl ether	ND	2
bromoform	ND	1
1,1,2,2-tetrachloroethane	ND	1
tetrachloroethylene	ND	1
toluene	ND	1
chlorobenzene	ND	1
ethyl benzene	ND	. 1
Non-Priority Hazardous Pollutant	Substances List C	ompounds
acetone	ND	2
carbon disulfide	ND	1

acetone carbon disulfide 2-butanone vinyl acetate 2-hexanone 4-methyl-2-pentanone styrene total xylenes	ND ND ND ND ND ND	2 1 2 2 2 2 1 1
QA/QC SUMMARY: SURROGATE RECOVERIES 1,2-Dichloroethane-d4 Toluene-d8 Bromofluorobenzene	106% 105% 99%	95% 108% 92%



CLIENT: HARDING LAWSON ASSOCIATES

JOB #: 19459,001.02 SAMPLE ID: MW010808

DATE RECEIVED: 08/08/89 ANALYSIS 1 (\*) 08/09/89 ANALYSIS 2 08/23/89 DATE REPORTED: 08/30/89

#### PAGE 9 OF 12 EPA METHOD 624: VOLATILE ORGANICS IN WATER

COMPOUND	Result ug/L	Detection Limit ug/L
chloromethane	ND	2
bromomethane	ND	2
vinyl chloride	ND	2
chloroethane	ND	2
methylene chloride	ND	1
trichlorofluoromethane	ND	<u></u>
1,1-dichloroethene		1
1,1-dichloroethane	47 *	1
	9 *	1
trans-1,2-dichloroethene chloroform	ND	1
· · · · · · · · · · · · · · · · · · ·	ND	1
1,2-dichloroethane	ND	1
1,1,1-trichloroethane	21 *	1
carbon tetrachloride	ND	1
bromodichloromethane-	ND	1
1,2-dichloropropane	ND	1
cis-1,3-dichloropropene	ND	1
trichloroethylene	ND	1
dibromochloromethane	ND	1
1,1,2-trichloroethane	ND	1
benzene	ND	1
trans-1,3-dichloropropene	ND	1
2-chloroethylvinyl ether	ND	2
bromoform	ND	1
1,1,2,2-tetrachloroethane	ND	1
tetrachloroethylene	ND	1
toluene	ND	1
chlorobenzene	ND	ī
ethyl benzene	ND	ī
Non-Priority Hazardous Pollutant	Substances List Co	ompounds

acetone carbon disulfide 2-butanone vinyl acetate 2-hexanone 4-methyl-2-pentanone styrene total xylenes	ND ND ND ND ND ND ND	2 1 2 2 2 2 1 1	
QA/QC SUMMARY: SURROGATE RECOVERIES 1,2-Dichloroethane-d4 Toluene-d8 Bromofluorobenzene	109% 103% 98%	98% 107% 88%	



CLIENT: HARDING LAWSON ASSOCIATES

JOB #: 19459,001.02 SAMPLE ID: MW100808

Bromofluorobenzene

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DATE RECEIVED: 08/08/89 ANALYSIS 1 (\*) 08/09/89 ANALYSIS 2 08/23/89 DATE REPORTED: 08/30/89

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102%

90%

#### EPA METHOD 624: VOLATILE ORGANICS IN WATER

	Result	Detection
COMPOUND	ug/L	Limit
- 1 1 t		ug/L
chloromethane	ND	2
bromomethane	ND	2
vinyl chloride	ND	2
chloroethane	ND	2
methylene chloride	ND	1
trichlorofluoromethane	ND	1
1,1-dichloroethene	ND	1
1,1-dichloroethane	ND	1
trans-1,2-dichloroethene	ND	1
chloroform	ND	1
1,2-dichloroethane	ND	1
1,1,1-trichloroethane	ND	1
carbon tetrachloride	ND	1
bromodichloromethane '	ND	1
1,2-dichloropropane	ND	1
cis-1,3-dichloropropene	ND	1
trichloroethylene	ND	1
dibromochloromethane	ND	1
1,1,2-trichloroethane	ND	1
benzene	ND	1
trans-1,3-dichloropropene	ND	1
2-chloroethylvinyl ether	ND	2
bromoform	ND	2 1
1,1,2,2-tetrachloroethane	ND	1
tetrachloroethylene	ND	1
toluene	ND	1
chlorobenzene	ND	1
ethyl benzene	ND	<u></u>
Non-Priority Hazardous Pollutant Sub	ostances List C	ompounds
acetone	ND	2
carbon disulfide	ND	ī
2-butanone	ND	2
vinyl acetate	ND	
2-hexanone	ND	2
4-methyl-2-pentanone	ND	2 2 2 1
styrene	ND	ī
total xylenes	ND	ī
QA/QC SUMMARY: SURROGATE RECOVERIES	<del>-</del>	_
1,2-Dichloroethane-d4	111%	93%
Toluene-d8	103%	103%
Bromofluorobonzono	1034	1034



LABORATORY NUMBER: 17977

CLIENT: HARDING LAWSON ASSOCIATES

JOB #: 19459.001.02

JOB NAME: GERBER PRODUCTS

DATE RECEIVED: 08/08/89

DATE ANALYZED: 08/10/89

DATE REPORTED: 08/28/89

PAGE 12 OF 12

Total Volatile Hydrocarbons as Gasoline in Aqueous Solutions EPA 8015 (Modified)
Extraction Method: EPA 5030 (Purge & Trap)

LAB ID	CLIENT ID	GASOLINE (mg/L)
17977-1 17977-2 17977-3 17977-4 17977-5 17977-6 17977-7 17977-8 17977-9 17977-10	MW020808 MW050808 MW080808 MW060808 MW030808 MW040808 MW070808 MW010808 MW090808	1.1 ND(0.05) 77 1.0 ND(0.05) ND(0.05) ND(0.05) ND(0.05) ND(0.05) ND(0.05)

ND = NONE DETECTED; LIMIT OF DETECTION IN PARENTHESES.

#### QA/QC SUMMARY

Duplicate: Relative % Difference Spike: % Recovery 113



Ha \_Lass tese ::
200 Rush Landing Road
P.O. 80x 6107
Novato, California 94948
415/892-0821
Telecopy: 415/892-1586

### CHAIN OF GUSTODY FORM

Samplers: From Bibble 31

Lab: Curt of Street Control

**ANALYSIS REQUESTED** 

Name/Location:	MASS DOLDS GERBER PROD OF: HICK DIGNAG		Pil F Fun	als (ylene carb. a 5
MATRIX #	CONTAINERS SA & PRESERV. NU	AMPLE JMBER OR DATE LAB JMBER	(Signature Required)  STATION DESCRIPTION/ NOTES	EPA 601/8010 EPA 602/8020 EPA 626/8240 EPA 625/8270 Priority Piltnt. Metals Benzene/Toluene/Xylene Total Petrol. Hydrocarb.
23 X	\$	2 0 23 23 23 9 0 2 0 2 0	10 MW- 2 S S S S S S S S S S S S S S S S S S	

	NUI	.AB MBI				I	PTI N	•	CC MT	ΓD		QA 300	•	MISCELLANEOUS	CHAIN OF CUSTODY RECORD				
7	Wk		Se	9	+	FE	ET		C	٥	T	Т	Т		RELINQUISHED BY: (Signature)	·	IVED BY: (Signatura)	DAT	E/TIME
					-							<del> </del>		NORMAL THE NAGANI	RELINQUISHED BY: (Signature)	RECE	EIVED BY: (Signature)	DAT	E/TIME
		1		1	<u>†</u>							#	_		RELINQUISHED BY: (Signature)	RECE	EIVED BY: (Signature)	DAT	E/TIME
		$\downarrow$			1							$\pm$			RELINQUISHED BY: (Signature)	RECE	EIVED BY: (Signature)	DAT	E/TIME
															METHOD OF SHIPMENT		RECEIVED FOR LAB BY: (Signature) (Signature) (Signature) (Signature) (Signature)	_	A/DIN

#### **DISTRIBUTION**

#### PHASE III SITE INVESTIGATION ADDENDUM FORMER GERBER PRODUCTS FACILITY OAKLAND, CALIFORNIA

#### February 21,1990

### COPY NO. \_(\_

		CODV NO
2 copies:	Gerber Products Company 445 State Street Freemont, Michigan 49412	1-2
	Attention: Mr. Richard M. Symes	
1 copy:	Job File	3
I copy:	QC/Bound Report File	4

NCP/JDS/bag/J11679-H

QUALITY CONTROL REVIEWER

Ronald N. Stoufer Engineering Geologist - 1206