



Weiss Associates

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TRANSMITTAL

TO: Scott Seery
COMPANY: ACDEH

DATE: 7/14
PROJECT #: 81-1227

FROM: Steve L.

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ENCLOSED PLEASE FIND: Vapor SSTL Calc's.

VIA:

- Fax
- 1st Class Mail
- Overnight Delivery
- UPS (Surface)
- Courier

FAX:

of pages: 3
(including this cover)

Hard Copy to follow

AS:

- Per our phone call
- You requested
- Is required
- We believe you may be interested

FOR:

- Your information
- Return to you
- Your action
- Your review & comments

COMMENTS: Scott:

We ran straight vapor calc's for SSTL's for soils at 2 ft and 4 ft. The calc. ~~includes a slab~~; the SSTL's don't change much between 2 ft and 4 ft. because the slab is much lower in permeability. Please give me a call if you have questions.

Please call (510) 450-6000 if there are any problems with transmission.

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SSTL For Benzene in Vapor at 2 Feet Below Ground Surface

Site Specific RBCA Tier 2 Analysis, Former Shell Service Station, WIC#204-6652-1106, 15275 Washington Avenue, San Leandro, CA.

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Soil Specific Parameters		
ASTM 95	ρ_s	1.7 Bulk Density(g/cm ³) or (kg/L)
Site Specific	θ_m	0.21 Air Content (w/v)
Site Specific	θ_{crack}	0.21 Air Content in foundation cracks(w/v)
Site Specific	θ_w	0.04 Water Content (w/v)
Site Specific	θ_{wcrack}	0.04 Water Content in foundation cracks(w/v)
Site Specific	θ_t	0.25 Porosity (w/v)
Actual	d	61 Depth to (location of) vapor sample (cm) - 2 foot depth
Diffusivity Parameters		
ASTM 95	H	0.22 Henry's Constant for Benzene
ASTM 95	D^{air}	9.30E-02 Air Diffusion Coefficient (cm ² /s)
ASTM 95	D^{wat}	1.10E-05 Water Diffusion Coefficient (cm ² /s)
Calculated	D^{eff}	0.0082337 Effective Diffusion Coefficient soil (cm ² /s)
Calculated	D^{eff}_{crack}	0.0082337 Effective Diffusion Coefficient through foundation cracks (cm ² /s)
Prediction of Flux From Benzene Concentration in Soil Vapor		
Iterative Calc	$C_{v,max}$	6.029 SSTL Benzene Concentration in Vapor (ug/m ³)
Calculated	F_{max}	8.14E-07 Maximum Diffusive Vapor Flux Predicted by Benzene Concentration in Soil Vapor (ug/cm ² -sec)
Indoor Air Concentration		
ASTM 95	Lb	200 Enclosed Space Volume/Infiltration Area Ratio (cm)
ASTM 95	$ER_{sp-indoor}$	0.00014 Enclosed Space Air Exchange Rate (sec ⁻¹)
ASTM 95	L_{crack}	15 Enclosed Space Foundation Thickness (cm)
ASTM 95	n	0.01 Areal Fraction of Cracks in Foundation (cm ² /cm ²)
Calculated	C_{indoor}	1.138E-08 Enclosed Space Air Concentration (ug/cm ³)
Dose		
ASTM 95	$IR_{sp-indoor}$	15 Daily Indoor Inhalation Rate (m ³ /day)
ASTM 95	EF	350 Exposure Frequency (days/year)
ASTM 95	ED	30 Exposure Duration (years)
Calculated	Dose	178.85 Dose (mg)
Risk		
CAL EPA	SF _i	0.1 California Cancer Slope Factor for Benzene (kg-day/mg)
ASTM 95	BW	70 Body Weight (kg)
ASTM 95	AT _c	70 Averaging Time for Carcinogens (years)
Calculated	Risk	1.00E-05 Risk (positives/population)

Formulas

$$D_i^{eff} = D^{air} \frac{\theta_m^{3.33}}{\theta_T^2} + D^{wat} \frac{1}{H} \frac{\theta_w^{3.33}}{\theta_T^2}$$

$$D_{crack}^{eff} = D^{air} \frac{\theta_{crack}^{3.33}}{\theta_T^2} + D^{wat} \frac{1}{H} \frac{\theta_{wcrack}^{3.33}}{\theta_T^2}$$

$$F_{max} = D_i^{eff} \frac{C_{v,max}}{d}$$

$$C_{indoor} = \frac{\left[\frac{F_{max}}{ER_{sp-indoor} \times L_b} \right]}{\left[1 + \left(\frac{D_i^{eff}/d}{ER_{sp-indoor} L_b} \right) + \left(\frac{D_i^{eff}/d}{(D_{crack}^{eff}/L_{crack})^n} \right) \right]}$$

$$Dose = C_{indoor} \times IR_{sp-indoor} \times EF \times ED$$

$$Risk = \frac{Dose \times SF_i}{BW \times AT}$$

Notes:

ASTM 95 = American Society for Testing and Materials, 1995. Standard Guide for Risk Based Corrective Action Applied at Petroleum Release Sites, E 1739-95.

Calculations: Effective diffusivity, diffusive vapor flux, enclosed space air concentration, dose and risk calculations from ASTM 95 guidance. Formulas presented above. Maximum allowable vapor concentration calculated by iteration to achieve acceptable risk level.

SSTL For Benzene in Vapor at 4 Feet Below Ground Surface

Site Specific RBCA Tier 2 Analysis, Former Shell Service Station, WIC#204-6852-1108, 15275 Washington Avenue, San Leandro, CA.

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Soil Specific Parameters	
ASTM 95	ρ_s 1.7 Bulk Density(g/cm ³) or (kg/L)
Site Specific	θ_{as} 0.21 Air Content (v/v)
Site Specific	θ_{crack} 0.21 Air Content in foundation cracks(v/v)
Site Specific	θ_{ws} 0.04 Water Content (v/v)
Site Specific	θ_{wcrack} 0.04 Water Content in foundation cracks(v/v)
Site Specific	θ_t 0.25 Porosity (v/v)
Actual	d 122 Depth to (location of) vapor sample (cm) - 4 feet depth

Diffusivity Parameters	
ASTM 95	H 0.22 Henry's Constant for Benzene
ASTM 95	D^{air} 9.30E-02 Air Diffusion Coefficient (cm ² /s)
ASTM 95	D^{wat} 1.10E-05 Water Diffusion Coefficient (cm ² /s)
Calculated	D^{eff}_s 0.00823368 Effective Diffusion Coefficient soil (cm ² /s)
Calculated	D^{eff}_{crack} 0.00823368 Effective Diffusion Coefficient through foundation cracks (cm ² /s)

Prediction of Flux From Benzene Concentration in Soil Vapor

Iterative Calc	$C_{v,max}$ 4.23E-07 SSTL Benzene Concentration in Vapor (ug/m ³)
Calculated	F_{max} 4.23E-07 Maximum Diffusive Vapor Flux Predicted by Benzene Concentration in Soil Vapor (ug/cm ² -sec)

Indoor Air Concentration

ASTM 95	L_b 200 Enclosed Space Volume/Infiltration Area Ratio (cm)
ASTM 95	$ER_{air-indoor}$ 0.00014 Enclosed Space Air Exchange Rate (sec ⁻¹)
ASTM 95	L_{crack} 15 Enclosed Space Foundation Thickness (cm)
ASTM 95	n 0.01 Areal Fraction of Cracks in Foundation (cm ² /cm ²)
Calculated	C_{indoor} 1.1355E-06 Enclosed Space Air Concentration (ug/cm ³)

Dose

ASTM 95	$IR_{air-indoor}$ 15 Daily Indoor Inhalation Rate (m ³ /day)
ASTM 95	EF 350 Exposure Frequency (days/year)
ASTM 95	ED 30 Exposure Duration (years)
Calculated	$Dose$ 178.838176 Dose (mg)

Risk

CAL EPA	SF_1 0.1 California Cancer Slope Factor for Benzene (kg-day/mg)
ASTM 95	BW 70 Body Weight (kg)
ASTM 95	AT_c 70 Averaging Time for Carcinogens (years)
Calculated	$Risk$ 1.00E-05 Risk (positives/population)

residential

Formulas

$$D_r^{eff} = D^{air} \frac{\theta_{as}^{3.33}}{\theta_T^2} + D^{wat} \frac{1}{H} \frac{\theta_{wT}^{3.33}}{\theta_T^2}$$

$$D_{crack}^{eff} = D^{air} \frac{\theta_{crack}^{3.33}}{\theta_T^2} + D^{wat} \frac{1}{H} \frac{\theta_{wcrack}^{3.33}}{\theta_T^2}$$

$$F_{max} = D_s^{eff} \frac{C_{v,max}}{d}$$

$$C_{indoor} = \frac{\left[\frac{F_{max}}{ER_{air-indoor} \times L_b} \right]}{\left[1 + \left(\frac{D_r^{eff}/d}{ER_{air-indoor} L_b} \right) + \left(\frac{D_{crack}^{eff}/d}{(D_{crack}^{eff}/L_{crack})^2} \right) \right]}$$

$$Dose = C_{indoor} \times IR_{air-indoor} \times EF \times ED$$

$$Risk = \frac{Dose \times SF_1}{BW \times AT}$$

Notes:

ASTM 95 = American Society for Testing and Materials, 1995. Standard Guide for Risk Based Corrective Action Applied at Petroleum Release Sites, E 1739-95.

Calculations: Effective diffusivity, diffusive vapor flux, enclosed space air concentration, dose and risk calculations from ASTM 95 guidance. Formulas presented above. Maximum allowable vapor concentration calculated by iteration to achieve acceptable risk level.