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SITE CONCEPTUAL MODEL

FOR

FORMER USA STATION NO. 57 10700 MACARTHUR BOULEVARD OAKLAND, CALIFORNIA

Prepared for

USA GASOLINE CORPORATION

May 6, 2005

Prepared by

ENVIRONMENTAL, INC.

3330 Cameron Park Drive, Suite 550 Cameron Park, California 95682

Project No. 2007-0057-01



May 6, 2005

Mr. Amir Gholami Alameda County Department of Environmental Health 1131 Harbor Bay Parkway, 2nd Floor Alameda, California 94502

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Project Manager

Re: Site Conceptual Model

Former USA Station No. 57 10700 MacArthur Boulevard

Oakland, California

Dear Mr. Gholami:

This Site Conceptual Model was prepared under the supervision of the undersigned.

STRATUS ENVIRONMENTE GEO

Stephen J. Cantak

Senior Project Sup

OF CALIFO Mr. Chuck Miller, USA Gasoline Corporation cc:

Mr. Ken Phares, Jay-Phares Corporation

Mr. Peter McIntyre, AEI Consultants

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1 EXECUTIVE SUMMARY

Stratus Environmental, Inc. (Stratus), on behalf of USA Gasoline Corporation (USA), has prepared the following Site Conceptual Model (SCM) for former USA Station No. 57, located at 10700 MacArthur Boulevard, Oakland, California (Figure 1). This SCM contains tables and figures that have been generated as part of assessment activities previously conducted at the site. The SCM also includes a brief description of the site, summarizes the extent of petroleum hydrocarbon impact to soil and groundwater, and identifies transport and exposure pathways. A summary of this SCM is provided in Table 1.

A total of twenty soil borings have been installed at the site, eight of which were completed as groundwater monitoring wells. Site assessment studies conducted to date have explored to a maximum depth of 44 feet below ground surface (bgs). Lithologic conditions encountered during drilling consisted of at least 10 to more than 44 feet bgs of interbedded fine-grained (silt and clay) and coarse-grained sediments (silty and clayey sand, gravelly sand, clayey gravel). A laterally continuous stratum of sandy and clayey gravel is encountered at approximately 11 to 25 feet bgs. These interbedded strata overlay deeply weathered, highly fractured, silty sandstone, siltstone, claystone, and chert (bedrock). The contact between the sediments and the underlying bedrock appears to dip toward the north at approximately 25° from horizontal.

Depth to groundwater in the monitoring wells at the site has fluctuated between approximately 7 and 21 feet bgs since the monitoring program was initiated in 1995. Groundwater fluctuations do not appear seasonally related. Since monitoring was initiated, groundwater elevations appear to generally decrease in wells S-1, S-2, and MW-5, and to generally increase in wells MW-3 and MW-7. Historically, groundwater flow has been towards the north, south, southwest, southeast and southeast, radial around wells S-1, S-2, and MW-7, and radial away from well MW-3. Groundwater flow gradients have ranged from 0.001 to 0.086.

In the vadose zone, petroleum hydrocarbon impact appears to be limited to the vicinity of the former underground storage tanks (UST's) and the former dispenser islands. Petroleum hydrocarbon impact extends vertically to groundwater. Based on available soil analytical data, and assuming no degradation, Stratus estimates that approximately 141 kilograms (311 pounds [lbs]) of total petroleum hydrocarbons as gasoline (TPHG) remain in the vadose zone.

Except in the vicinity of the southwest corner of the former UST pit (borings B-1, B-2, B-3, and MW-3), the extent of vadose zone impact appears to be adequately characterized. Impact is limited laterally to the vicinity of the former UST pit, dispensers, and product piping trench. Impact extends vertically to groundwater. At the furthest extent of excavation, impact in the former UST pit appears limited to the walls and base in the southern corner of the pit. Over-excavation was not performed beneath the former dispenser islands, but based on data from the adjacent product piping trench, impact beneath the islands is likely limited to 10 feet bgs.

Petroleum hydrocarbon impact to groundwater appears to be restricted to the vicinity of wells S-1, S-2, MW-3, and MW-7. Historical analytical data suggest a generally decreasing trend in dissolved concentrations. The highest concentrations of dissolved hydrocarbons are consistently reported in well S-2. Historical analytical data suggest that the plume configuration is stable. The estimated mass of TPHG, benzene, and methyl tertiary butyl ether (MTBE) in groundwater (based on first quarter 2005 data) is 5.5 lbs, 0.4 lbs, and 0.3 lbs, respectively.

Excavation at the time of UST removal (July and October, 1994) appears to have removed approximately 148.40 pounds of TPHG, 0.07 pounds of benzene, and 18.72 of total petroleum hydrocarbons as diesel (TPHD). Dual phase extraction (DPE) feasibility testing performed in 2004 attained groundwater extraction rates between 0.07 and 2.80 gallons per minute (gpm), achieving TPHG extraction rates up to 0.001 pounds per day (lbs/day). Soil vapor extraction rates of 86 to 87 cubic feet per minute (cfm) achieved TPHG extraction rates up to 5.16 lbs/day. These data indicated that DPE was a technically viable remedial option to address both residual hydrocarbon impact in the vadose zone and dissolved impact in the groundwater.

There do not appear to be any complete pathways at the site for exposure to hydrocarbon compounds. Redevelopment plans for the site may lead to complete exposure pathways for inhalation exposure in indoor air, and for dermal contact with impacted groundwater. The nearest identified water supply well appears to be located approximately 1,000 feet to the southwest (irrigation well). This well does not appear threatened by hydrocarbon impact for the USA site.

Based on available soil analytical data, concentrations of TPHG, TPHD, and benzene, toluene, ethylbenzene, and total xylenes (BTEX) compounds remain in the soil in the vicinity of the former UST pit and former dispensers at concentrations above current Regional Water Quality Control Board (RWQCB) Environmental Screening Levels (ESL's). It is our understanding, based on discussions with Jay-Phares Corporation, that current redevelopment plans for the site call for removal of up to 15 feet of soil in the area of the former UST pit and former dispensers, which would remove most of the soil impact. A limited area near the southern corner of the former UST pit will likely still contain residual hydrocarbons above ESL's, but over-excavation in this area could remove impacted soil above ESL's.

Based on the current groundwater monitoring analytical data, groundwater is impacted with TPHG, BTEX compounds, MTBE, tertiary butyl alcohol (TBA), and 1,2-dichloroethane (1,2-DCA) at concentrations above ESL's. Additional DPE mass removal events (approximately 30 days duration), prior to redevelopment, has been proposed for this site, which should reduce hydrocarbon concentrations significantly in both soil (vadose zone) and groundwater prior to implementation of the proposed redevelopment plans.

2 SITE DESCRIPTION

2.1 Site Description

Former USA Station 57 is situated in eastern Oakland, California, near the Oakland-San Leandro boundary. The site is currently an undeveloped, partially paved parcel situated on the western corner of the intersection of 108th Avenue and Foothills Boulevard, adjacent to Interstate 580 (Figure 1). This parcel comprises the eastern corner of the Foothills Square Shopping Center. The site is bounded to the northeast by Foothill Boulevard, and to the southeast by 108th Avenue. The southwest and northwest edges of the site are bounded by parking area associated with the adjacent shopping center (Figure 2). Photographs of the current site conditions are included in Appendix A.

The subject site previously operated as USA Gasoline Station No. 57. The former service station configuration included three 12,000-gallon gasoline and one 8,000-gallon diesel UST's and three dispenser islands. The station was closed, and the UST's, dispensers, and associated product piping were removed in July 1994. The approximate former locations of the UST's and dispenser islands are shown on Figure 3

2.2 Topography and Surface Conditions

From the subject site, topography slopes moderately toward the southwest, down the East Bay Plain toward San Francisco Bay. Immediately northeast of the site, the San Leandro Hills rise sharply out of the plain (Figure 1).

The site itself is generally flat. The ground surface remains partially paved with asphalt and concrete, except for the former UST pit and former dispenser islands. The eastern corner of the site is covered with a large stockpile (reported to be approximately 3,000 cubic yards [yd³]) of soil excavated from another area of the shopping center as part of a separate environmental investigation.

2.2.1 Drainage

The surface run-off from the site appears to flow into storm drains located in the parking area of the shopping center (Figure 2). Run-off from Foothill Boulevard and 108th Avenue is directed to storm drain catch basins by concrete roadside gutters. The nearest surface water appears to be San Leandro Creek, situated approximately 4,000 feet to the south, and Seneca Reservoir, approximately 5,000 feet to the north-northeast (Figure 1).

2.2.2 Zoning and Land Use

All properties in the immediate vicinity of the site have been developed. Single- and multiple-family dwellings are situated to the southeast (across 108th Avenue). Interstate Highway 580 is located to the northeast (across Foothill Boulevard). A retail shopping center is situated immediately to the southwest and northwest. Knowland State Arboretum and Park and Lake Chabot Municipal Golf Course are located in the San

Leandro hills northeast and east of the site, respectively. Several small urban parks are situated to the south-southeast and southeast of the site. The closest of these parks is over 3,000 feet from the site. (Figure 1). Based on the City of Oakland Planning and Zoning Department (http://www.oaklandnet.com/maproom/), the subject site and adjacent shopping center are zoned for commercial use. Properties in the vicinity of the site are zoned for commercial and residential use.

2.2.3 Meteorology Data

The climate in the vicinity of the site generally consists of mild to hot summers with infrequent precipitation, and mild winters with intermittent rainfall events and foggy conditions. A California Irrigation Management Information System (CIMIS) weather station in Union City, California (Station No 171) reported an average air temperature of 57.4 degrees Fahrenheit (°F), an average maximum temperature of 67.7 °F, an average minimum temperature of 48.0 °F, an average wind speed of 3.5 miles per hour, and an average total precipitation of 26.81 inches between May 1, 2004, and April 11, 2005 (http://www.cimis.water.ca.gov/cimis/). Meteorological conditions at the subject site should be generally similar to the data collected at the Union City weather station.

3 SUMMARY OF SITE ASSESSMENT ACTIVITIES

Assessment of petroleum hydrocarbon impact at the site was initiated in 1987. Several consultants have been involved in site characterization activities at this site. The following is a brief summary of assessment activities conducted to date. Locations of all soil borings and wells are included on Figure 3.

- Pacific Environmental Group installed two groundwater monitoring wells (S-1 and S-2) and four soil borings (A through D) in February 1987. This investigation was performed as part of a potential real estate transaction, not in response to a reported release.
- Three 12,000-gallon USTs and one 8,000-gallon UST were removed in July 1994. Soil sampling and over-excavation activities were overseen by Western Geo-Engineers. Additional excavation in the southern corner of the former UST pit was performed in October 1994 under the direction of Alton Geosciences.
- Alton Geoscience installed one groundwater monitoring well (MW-3) and six soil borings (B-1 through B-6) in February and March 1995.
- Alton Geoscience installed five groundwater monitoring wells (MW-4 through MW-8) in November 1995.
- Groundwater monitoring and sampling was initiated in 1995.

Boring logs and well construction details are presented in Appendix B, and are summarized on Table 2. Historical soil analytical data are summarized in Appendix C. Historical groundwater monitoring and chemical analytical data are included in Appendix D.

4 SUBSURFACE CONDITIONS

4.1 Geologic Conditions

4.1.1 Regional Setting

The subject site is situated on the eastern edge of the East Bay Plain, a broad, gently sloping area of sedimentary deposits on the eastern shore of San Francisco Bay. In the site vicinity, these sediments are mapped as Late Pleistocene alluvium, consisting of weakly consolidated, slightly weathered, poorly sorted, irregularly interbedded clay, silt, sand, and gravel, interpreted to be alluvial fan and fluvial deposits of the Holocene age. These alluvial fan deposits extend westward over the Alameda formation, the major basin filling unit in the area. In the immediate site vicinity, the Hayward Fault separates the sediments of the East Bay Plain from the igneous rocks (gabbros, keratophyres, and quartz keratophyres) that comprise the western portion of the adjacent San Leandro Hills (Helley and others, 1979; Figuers, 1998; Graymer, 2000).

4.1.2 Subsurface Geologic Conditions

Site assessment studies conducted to date have explored to a maximum depth of 44 feet bgs. A total of twenty soil borings were advanced, eight of which were completed as groundwater monitoring wells (S-1, S-2, and MW-3 through MW-8). Interpreted geologic relationships are illustrated on geologic cross section A-A' (Figure 4). Additional geologic cross sections constructed during previous investigations, and site plans illustrating the surface traces of those cross sections, are presented in Appendix E.

Based on boring logs from subsurface investigations, the subject site is underlain by interbedded strata consisting predominantly of unconsolidated fine-grained sediments (silt and clay) and coarse-grained sediments (silty and clayey sand, gravelly sand, and clayey gravel). These interbedded strata extend from at least 10 feet to more than 44 feet bgs. Within this unit of unconsolidated sediments, a stratum of sandy and clayey gravel is encountered at approximately 25 feet below ground surface (bgs) beneath the northern portion of the site, and at approximately 11 feet bgs beneath the southern end of site.

These interbedded strata of clay, silt, sand, and gravel overlay deeply weathered, highly fractured silty sandstone, siltstone, claystone, and chert. This sandstone, siltstone, claystone, and chert unit has been interpreted by others as bedrock, although it should be noted that the borings into this material were advanced using hollow-stem augers, and samples of the material were collected using a modified California split-spoon sampling device. Gravel-sized clasts were reported within the bedrock unit in some of the borings. Field notes from Western Geo-Engineers (1994) suggest chert is also present. The contact between the sediments and the underlying sandstone/siltstone appears to dip toward the north at an apparent angle of approximately 25° from horizontal.

4.2 Hydrogeology

Historical groundwater depth-to-water data indicate that groundwater has fluctuated between approximately 7 and 21 feet bgs in the monitoring well network since monitoring and sampling was initiated in 1995 (the initial depth-to-water reading for well MW-8 of 33.33 on November 22, 1995, appears anomalous and was not included in discussions or graphical representations of historical groundwater conditions). The greatest amount of fluctuation (12.18 feet, from 7.38 to 19.56 feet bgs) is observed in well MW-5, and the smallest amount of fluctuation (10.20 feet, from 5.88 to 16.08 feet bgs) is observed in well MW-4, indicating a smear zone approximately 10 to 12 feet thick.

Based on the historical depth-to-water data (Appendix D), the well screens in wells S-1, S-2, and MW-3 through MW-7 appear to have been submerged during some or all of the life of the wells (well construction details summarized in Table 2). Wells MW-4 and MW-5 are the only wells not constructed with some or all of the screened intervals placed within the sandstone/siltstone/claystone bedrock (lithologic logs and well construction details are included in Appendix B, and are summarized on Figure 4). While these wells may not be ideally constructed, they none the less appear to adequately monitor subsurface hydrogeologic conditions beneath the site.

As shown on the hydrographs in Appendix F, the fluctuations observed in the monitoring well network do not appear to be seasonally related. The hydrographs suggest that groundwater elevations are generally decreasing in wells S-1, S-2, and MW-5, increasing in wells MW-3 and MW-7, and are not increasing or decreasing in wells MW4 and MW-8 (there is not enough data for well MW-6 to evaluate the groundwater elevation trend in this well).

Historically, groundwater flow has been toward the north, south, southwest, southeast, radial toward wells S-1, S-2, and MW-7, and radial away from well MW-3. Groundwater gradients have ranged from 0.001 to 0.089 feet/feet. During the most recent monitoring event (January 9, 2005), groundwater was measured between 10.34 and 20.33 feet bgs, with groundwater flow radial toward wells S-1, S-2, and MW-7, and radial away from well MW-3 (Figure 5). Available historical groundwater elevation contour maps for the site are included in Appendix G.

4.3 Utilities

A utility survey performed by California Underground Utilities on April 22, 2005, identified the presence of water, sewer, and electrical lines beneath the subject site. The approximate locations of these utilities are shown on Figure 3. Burial depths of these utility lines were not identified during the survey. However, based on our experience at similar service station sites, we expect the utilities to be buried approximately 2 to 3 feet bgs. The assumed burial depths are shown on Figure 4. Based on the locations identified during the April 22, 2005, survey and the assumed burial depths, these utilities do not appear situated to act as preferential pathways for hydrocarbon plume migration.

Work performed by others has identified the presence of water, electrical, natural gas, storm drain, and telephone lines beneath the adjacent shopping center parking lot (Figure 2). The burial depths of these utilities were not identified. These utilities appear situated outside the area of soil or groundwater impact associated with the USA facility.

4.4 Extent of Petroleum Hydrocarbon Impact

4.4.1 Extent of Residual Petroleum Hydrocarbon Impact

TPHG and benzene concentrations in soil are summarized in Figures 6 and 7. Iso-concentration maps of TPHG concentrations in soil at various depths beneath the site are included in Appendix H.

Former UST Pit

Petroleum hydrocarbons have impacted soil in the vicinity of the former UST pit, and impact appears to extend to the saturated zone. Based on analytical data from soil samples collected at the furthest extent of excavation, impact remains in the western and southwestern walls of the pit (Figure 6). Samples collected at 12 to 13 feet bgs from the pit walls in this area reported up to 9.6 milligrams/kilogram (mg/Kg) of benzene and 2,400 mg/Kg of TPHG (this TPHG concentration is not shown on Figure 6; it was from a sample collected by Alton Geosciences and the sample location was not indicated in the material reviewed). As inferred from the cross-section (Figure 4), soil in this area consists of silty and clayey gravel. The base of the UST pit was excavated to depths between 15.5 and 20 feet bgs. TPHG and benzene were also reported in samples collected from the base of the UST pit (up to approximately 20 feet bgs) at concentrations up to 620 and 1.1 mg/Kg, respectively. The highest concentrations were reported in the sample collected from 20 feet bgs in the southern corner of the pit. Field notes indicate the material at this location was bedrock, described as indurated, fractured chert with claystone (Western Geo-Engineers, 1994).

Former Product Dispensers

TPHG and benzene were reported in five of the six soil samples collected beneath the former dispenser islands. These samples were collected between 3 and 3.5 feet bgs in what is inferred from the cross-section (Figure 4) as silt and clay grading into silty and clayey sand. As shown on Figure 6, the highest concentration of TPHG (1,800 mg/Kg) and benzene (0.72 mg/Kg) reported from the dispenser island samples were in sample DI-6, collected from the eastern end of the northern island. The vertical extent of impact beneath the former dispenser islands is not completely characterized.

Former Piping Trench

Hydrocarbons were reported in only one of the five soil samples collected from the former product piping trench. This sample (PI-2, between the middle and northern islands, Figure 6), collected from 3.5 feet bgs, reported TPHG at a concentration of 4,500 mg/Kg. Limited excavation in the area of this sample deepened the pit to

approximately 9 feet bgs. A confirmation sample collected at the base of this pit (PI2-0, Figure 6) reported TPHG at 15 mg/Kg and benzene at 0.02 mg/Kg. Soil conditions beneath the former piping trench are inferred to be similar to those under the former dispensers.

Soil and Well Borings

Near the former UST pit, soil samples collected from borings B-1 and MW-3 (west of the former UST pit) at depths between 9.5 and 35 feet bgs were reported to contain TPHG at concentrations up to 540 mg/Kg and benzene concentrations up to 2.6 mg/Kg. East of the former UST pit TPHG was reported in soil samples collected in boring B-2 between 16 and 26 feet bgs at concentrations of 16 to 240 mg/Kg. Benzene concentrations in these samples ranged from 0.057 to 0.96 mg/Kg. Soil analytical data from exploratory soil borings drilled adjacent to the former dispenser islands, former product line trench, and former UST pit suggest that the lateral extent of impact near the former dispenser islands and former product line trench has been adequately characterized. Soil impact south and southeast of borings B-2 and B-3 is not completely characterized. Soil impact west of borings B-1 and MW-3 is also not completely characterized. With these exceptions, impacted soil remaining in the UST pit and beneath the dispenser islands at the furthest extent of excavation appears to be adequately characterized.

The highest residual concentrations are reported in samples collected within the interbedded sedimentary strata. Near the southern corner of the UST pit, low concentrations of residual hydrocarbons have also been reported in samples collected from the claystone/siltstone, at depths up to 8 feet below the inferred contact between the sedimentary unit and the bedrock. Based on the iso-concentration maps, approximately 141 Kg of TPHG remains in the vadose zone soil (311 lbs). Mass calculations are included in Appendix H.

4.4.2 Extent of Dissolved Hydrocarbons

Free product has not been observed at this site, but a sheen has been observed in well S-2 on a sporadic basis, most recently in July 2004, at the conclusion of the DPE feasibility testing.

TPHG, BTEX compounds, MTBE, TBA, and 1,2-DCA are consistently reported in wells S-1, S-2, and MW-3. MTBE is also consistently reported in well MW-7. The highest concentrations of TPHG, benzene, MTBE, TBA, and 1,2-DCA are consistently reported in well S-2. Very low concentrations of TPHG, benzene, and MTBE have also been reported on a sporadic basis in wells MW-4, MW-5, MW-6, and MW-8. TPHG, benzene, and MTBE concentrations for the first quarter 2005 are summarized in Figure 8. Based on these data, benzene, MTBE, and 1,2-DCA are present at concentrations above their current Maximum Contaminant Levels (MCL's) of 1.0 micrograms per liter (μg/L), 13 μg/L (primary MCL), and 0.5 μg/L, respectively.

Based on plots of historical TPHG, benzene, and MTBE concentrations (Appendix F), there does appear to be a general decrease of dissolved petroleum hydrocarbons in wells

S-1, S-2, MW-3, and MW-7. TPHG and benzene concentrations in wells S-1, S-2, and MW-3 appear to show this decreasing trend. The dissolved MTBE concentrations in wells S-1 and MW-7 also appear to have a downward trend, while the MTBE concentration trend in well S-2 appears flat, and the MTBE concentration trend in well MW-3 appears to be increasing. Concentrations of 1,2-DCA in wells S-1, S-2, and MW-3 appear to be decreasing, while the TBA concentrations in these wells appears flat. Historical groundwater chemical analytical data are summarized in Appendix D. These data suggest the extent of dissolved hydrocarbon impact has been adequately characterized, and the dissolved hydrocarbon plume configuration appears relatively stable. However, the available data are not adequate to evaluate if the dissolved hydrocarbons penetrate the soil/bedrock interface to any great extent, or the extent to which fracture flow might influence dissolved hydrocarbon distribution beneath the site.

Iso-concentration contours for TPHG, benzene, and MTBE concentrations reported during the first quarter 2005 sampling event are included in Appendix I. Based on these iso-concentration contours, approximately 2,490 grams of TPHG (5.5 lbs), 169 grams of benzene, (0.4 lbs), and 158 grams of MTBE (0.3 lbs) remain in the groundwater beneath the site. While the limited number of data points makes construction of viable iso-concentration maps problematic, the overall decreasing trends in dissolved concentrations of TPHG, benzene, and MTBE suggest that the mass of dissolved hydrocarbons in the groundwater beneath the site have likely decreased since removal of the UST's and dispensers, while the lateral extent of dissolved impact appears relatively unchanged.

5 REMEDIAL ACTIONS

- Approximately 775 cubic yards of soil were reported excavated under the direction of Western Geo-Engineers after removal of UST's in 1994. Based on an arithmetic mean of concentrations reported for samples from the soil stockpile, approximately 148.40 Kg (327.17 lbs) of TPHG, 0.07 Kg (0.15 lbs) of benzene, and 18.72 Kg (41.27 lbs) of TPHD were removed with the stockpiles. Tabulated stockpile analytical data are included in Appendix C. Calculations of mass removed are included in Appendix H.
- Stratus Environmental Inc. performed a DPE test in 2004. Soil vapors and groundwater were extracted from wells S-1, S-2, MW-3, and a combination of all wells simultaneously. The test was able to achieve groundwater extraction rates between 0.07 and 2.80 gpm, and soil vapor extraction rates between 86 to 87 cfm. The induced groundwater radius of influence during the test was limited. In groundwater, hydrocarbon mass was extracted at estimated rates up to 0.001 lbs/day of TPHG, 0.00001 lbs/day of benzene, and 0.001 lbs/day of MTBE. In soil vapor, hydrocarbon mass was extracted at estimated rates up to 5.16 lbs/day of TPHG, 0.01 lbs/day of benzene, and 0.01 lbs/day of MTBE. These test data indicated that DPE was a technically viable technology to address the impact beneath the site.
- The report recommended additional DPE to further reduce hydrocarbon mass, especially in the vadose zone. Tables summarizing analytical data and field measurements from the DPE test are included in Appendix J.

6 POTENTIAL EXPOSURE PATHWAYS AND SENSITIVE RECEPTORS

An exposure pathway model for the site is presented in Figure 9. The primary potential source of exposure (leaking UST's, piping, and dispensers) were removed from the site in 1994. Potential secondary sources for exposure include residual hydrocarbons in subsurface soil and dissolved petroleum hydrocarbons in groundwater.

6.1 Potential On-site Exposure Pathways

The primary sources for exposure to gasoline and related compounds (leaking UST's, piping, and dispensers) have been removed. Secondary sources of potential exposure at this site include residual hydrocarbons in the vadose zone soil, and dissolved hydrocarbons in the groundwater. While TPHD has been reported in soil and groundwater samples, the primary compounds of concern at this site appear to be TPHG, BTEX, MTBE, TBA, and 1,2-DCA.

Exposure to the secondary sources of petroleum hydrocarbons at the site (impacted soil and groundwater beneath the site) appears limited. Potential transport mechanisms associated with these secondary sources include exposure of impacted soil to human contact (dermal contact and ingestion), volatilization of residual hydrocarbons in the vadose zone and in groundwater (inhalation), and exposure to impacted groundwater through pumping (dermal contact and ingestion).

6.1.1 Potential for Human Contact

Surface soil at the site is not impacted. There is no surface water at the site or in the immediate vicinity. Exposure of construction workers to impacted soil (or groundwater, depending on the depth of excavation and the depth to water) may be possible during planned redevelopment activities. If construction workers are properly trained for this type of work (e.g. taking precautions to properly check, and if necessary, ventilate excavations in the impacted areas; taking proper measures to monitor air quality and utilize breathing respirators where appropriate; wearing the proper clothing while working at the site; and washing prior to eating or drinking), and proper care and attention is given to safety precautions and hygiene, the risk of exposure to construction workers through dermal contact, accidental ingestion, or inhalation of volatilized hydrocarbons appears minimal. Excavation activities in the vicinity of the former USA station should be performed and supervised by HAZWOPER-trained personnel.

Dissolved hydrocarbons are present in groundwater beneath the site. However, because there are no structures at the site to restrict natural airflow, it appears unlikely that vapors from the dissolved plume will accumulate in concentrations that will become an exposure threat. As there are currently no water supply wells at the site or in the immediate vicinity, exposure to impacted groundwater appears unlikely (except as discussed above for construction workers).

6.1.2 Potential for Environmental Impact

Given the current site conditions, it appears unlikely that impact at this site could compromise other environmentally sensitive receptors (e.g. adjacent surface soil or surface water).

6.1.3 Potential Future Land Use

The site is currently zoned for commercial use (C-30). Potential redevelopment plans call for construction of a shopping center building over the area of the former UST's and dispensers. Volatilization of hydrocarbons into the building may be possible, but with proper engineering controls incorporated into the building design (e.g. vapor barrier), exposure of the customers or employees in the building is unlikely.

6.2 Off-site Receptors

6.2.1 Water Supply Wells

Well search data were included in GHH's Risk Assessment and Closure Request Report (1998). Copies of the table and figure from the GHH report are included in Appendix K. The locations and operational status of these wells has not been verified.

When radial groundwater flow is not observed at the site, groundwater flow appears to be toward the southeast. Based on the data included in Appendix K, there does not appear to be any water supply wells situated southeast of the subject site. The nearest water supply well is an irrigation well at 2455 109th Avenue, approximately 1,000 feet to the southwest. The data summarized in Appendix K suggests there are no off-site groundwater receptors likely to be impacted by dissolved hydrocarbons from the site.

6.3 Previous Risk Assessment

GHH submitted a Risk Assessment and Closure Request (1998) that included a Dominico Fate and Transport modeling of impact to the nearest groundwater receptor. This model indicated that under steady state conditions, the benzene concentration at the nearest receptor would be approximately 1.5 x 10⁻⁸ µg/L (Appendix L).

GHH's Closure Information/Proposal (2002) included a Tier 1 Risk Based Corrective Action analysis that concluded benzene concentrations in soil exceeded the limits for volatilization to indoor air, and the benzene concentrations in well S-2 exceeded the limits for groundwater ingestion.

6.4 Environmental Screening Levels

The San Francisco Bay RWQCB has developed Environmental Screening Levels (ESL's) for TPHG, BTEX compounds, MTBE, TBA, and 1,2-DCA (summarized in Appendix M). Residual concentrations of TPHG and BTEX compounds in soil beneath the site that exceed the ESL concentrations are illustrated on Figure 10. ESL tables are included in Appendix M. ESL values for shallow soil (<3 meters) were utilized for this

comparison. Soil and groundwater concentrations of TPHG, benzene, toluene, ethylbenzene, xylenes, MTBE, TBA, and 1,2-DCA were compared to ESL concentrations for both commercial and residential property usage (there are no differences in the soil ESL's for commercial and residential usage for the compounds of concern at this site).

6.4.1 Soil Impact

Based on discussions with Jay-Phares Corporation, current redevelopment plans may require the area of the former service station to be excavated to an elevation of 64 to 66 feet MSL. This might require the removal of up to 15 feet of soil. These excavation activities should remove virtually all impacted soil in the vicinity of the former dispenser island and former UST pit. As depicted in the figures included in Appendix M, small areas of residual impact will remain near the southern end of the former UST pit. If sampling performed after completion of the redevelopment grading activities confirm the presence of residual TPHG, BTEX compounds, MTBE, TBA, and 1,2-DCA in this area at concentrations above ESL's, additional limited excavation should be able to reduce these concentrations to acceptable levels.

6.4.2 Groundwater impact

Based on the most recent groundwater monitoring and sampling data, dissolved concentrations of TPHG, MTBE, TBA, and 1,2-DCA were reported above ESL values in well S-1; concentrations of TPHG, BTEX compounds, MTBE, TBA, and 1,2-DCA were reported above ESL values in well S-2; and concentrations of benzene, MTBE, TBA, and 1,2-DCA were reported above ESL values in well MW-3. None of the compounds of concern were reported in well MW-7 at concentrations above ESL values.

7 SUMMARY

- The former USA Station No. 57 was closed and the UST's, dispenser islands, and associated product piping were removed in July 1994. Approximately 775 yd³ of soil were excavated as part of the UST and dispenser removal activities. The site was not redeveloped subsequent to station closure. The site is currently zone for commercial usage.
- Site assessment activities were initiated in 1987. To date a total of twenty soil borings have been drilled at the site. Eight of the borings were converted to groundwater monitoring wells.
- Geology beneath the site consists of approximately 10 to more than 40 feet bgs of interbedded fine-grained (silt and clay) and coarse-grained sediments (silty and clayey sand, gravelly sand, and clayey gravel). A stratum of sandy and clayey gravel is encountered at approximately 11 to 25 feet bgs. This interbedded unit overlies deeply weathered, highly fractured bedrock comprised of silty sandstone, siltstone, claystone, and chert. The contact between the sediments and the underlying sandstone/siltstone appears to dip toward the north at approximately 25° from horizontal.
- Based on the depth to groundwater in the monitoring wells, the smear zone due to groundwater fluctuation is approximately 10 to 12 feet thick. Groundwater flow has been and towards the north, south, southwest, southeast, radial toward wells S-1, S-2, and MW-7, and radial away from well MW-3.
- Petroleum hydrocarbons have impacted soil in the immediate vicinity of the former UST complex and former dispenser islands. Impact extends to the saturated zone. In general, the vertical and lateral extent of the impact appears to be adequately characterized. Approximately 141 Kg (311 lbs) of TPHG remain in the vadose zone soil.
- Dissolved hydrocarbons of concern include TPHG, BTEX compounds, MTBE, TBA, and 1,2-DCA. Groundwater impact appears limited to the vicinity of wells S-1, S-2, MW-3, and MW-7, with the highest concentrations reported in well S-2.
- TPHG and benzene concentrations appear to be decreasing in wells S-1, S-2, and MW-3. MTBE concentrations appear to be decreasing in wells S-1 and MW-7, and increasing in well MW-3. Groundwater concentrations and plume configuration appear relatively stable. Approximately 2,490 grams of TPHG (5.5 lbs), 169 grams of benzene, (0.4 lbs), and 158 grams of MTBE (0.3 lbs) are remain in the groundwater beneath the site.
- Approximately 775 yd³ of soil were excavated and removed from the site. Approximately 148.40 Kg (327.17 lbs) of TPHG, 0.07 Kg (0.15 lbs), and 18.72 Kg (41.27 lbs) of TPHD were removed in this stockpiled material.

- The DPE test was successful in removing TPHG, benzene, and MTBE in both soil vapor and groundwater. The test data suggest DPE is a viable remedial alternative to remove residual hydrocarbons from the soil and groundwater beneath the site.
- There does not appear to be any complete pathway for human exposure to residual or dissolved hydrocarbons beneath the site. There does not appear to be any downgradient water supply wells.
- A very limited area of soil impacted by concentrations above ESL values will remain after proposed redevelopment grading. Dissolved concentrations of some or all of the compounds of concern are reported in wells S-1, S-2, and MW-3 at concentrations above ESL values.

8 DISCUSSION & RECOMMENDATIONS

Petroleum hydrocarbon impact has been identified in the vadose zone as well as in the groundwater. In the vadose zone, petroleum hydrocarbon impact appears to be limited to the immediate vicinity of the former UST's and the former dispenser islands. The lateral and vertical extent of vadose zone impact has been adequately characterized. Approximately 141 Kg (310 lbs) pounds of residual hydrocarbon as TPHG appears to remain in the unsaturated zone. Additional characterization of the vadose zone impact does not appear warranted at this time.

Petroleum hydrocarbon impact has also been identified in wells S-1, S-2, MW-3, and MW-7. The extent of the dissolved hydrocarbon impact appears to be adequately characterized. The dissolved concentrations and plume configuration appear stable. The estimated mass of TPHG, benzene, and MTBE in groundwater (based on first quarter 2005 data) is 5.5 lbs, 0.4 lbs, and 0.3 lbs, respectively. Additional characterization of the dissolved hydrocarbon plume does not appear warranted at this time.

Soil and groundwater impact are present beneath the site at concentrations that exceed current RWQCB ESL values. Remedial activities proposed below should reduce these concentrations.

Based on our discussions with Jay-Phares Corporation, redevelopment plans for the site may require excavation of up to 15 feet of soil to lower the grade to 64 to 66 feet MSL. These excavation activities should remove most of the residual soil impact. Soil generated during these grading activities will be screened in the field, and impacted soil will be segregated and properly disposed of off-site. The proposed excavation activities appear likely to leave a small pocket of impact above ESL values in the vicinity of the southern corner of the former UST pit. Stratus recommends this area of impact also be excavated, and soil samples collected and analyzed to confirm removal of impact to concentrations below ESL values.

Stratus has recommended a program of 30-day dual phase extraction to reduce the mass of dissolved hydrocarbons in the groundwater beneath the site (Stratus, 2004b). This program will be implemented upon approval of the proposed work by Alameda County Department of Environmental Health.

9 REFERENCES

The following documents were consulted, in whole or in part, during preparation of this report:

- Alton Geoscience, 1995, Supplementary Site Assessment Report (dated April 24, 1995).
- --, 1996, Supplementary Site Assessment Report (dated February 26, 1995).
- Figuers, S., 1998, Groundwater study and water supply history of the East Bay Plain, Alameda and Contra Costa Counties, CA: Norfleet Consultants, Livermore, California (prepared for the Friends of the San Francisco Bay Estuary, Oakland, California).
- GHH Engineering Inc., 1998, Risk Assessment and Closure Request Report (dated September 1998).
- --, 2002, Closure Information Proposal (dated April 2002).
- Graymer, M.W., 2000, Geologic map and map database of the Oakland metropolitan area, Alameda, Contra Costa, and San Francisco Counties, California: U.S. Geological Survey Miscellaneous Field Studies MF-2342, version 1, scale 1:50,000 (digital map, http://geopubs.wr.usgs.gov/map-mf/mf2342/mf2342f.pdf).
- Helley, E.J., K.R. Lajoie, W.E. Spangle, and M.L. Blair, 1979, Flatland deposits of the San Francisco Bay Region, California-their geology and engineering properties, and their importance to comprehensive planning: U.S. Geological Survey Professional Paper 943.
- Pacific Environmental Group, 1987, Preliminary Site Assessment Investigation (dated March 13, 1987).
- Stratus Environmental, Inc., 2004, Work Plan for Monitoring Well Replacement (dated January 14, 2004).
- --, 2004a, Feasibility Test Work Plan (dated March 15, 2004).
- --, 2004b, Dual Phase Extraction Test Report (dated October 15, 2004).
- --, 2005, Quarterly Groundwater Monitoring Report, First Quarter 2005 (dated April 13, 2005).
- Western Geo-Engineers, 1994, UST's Removal Soil Sampling and OverExcavation (dated October 6, 1994).

10 LIMITATIONS

This report was prepared in general accordance with accepted standards of care which existed at the time this work was performed. No other warranty, expressed or implied, is made. Conclusions and recommendations are based on field observations and data obtained from this work and previous investigations. It should be recognized that definition and evaluation of geologic conditions is a difficult and inexact art. Judgments leading to conclusions and recommendations are generally made with incomplete knowledge of the subsurface conditions present. More extensive studies may be performed to reduce uncertainties, such as additional subsurface assessment, risk-based corrective action analysis, or fate and transport modeling. This report is solely for the use and information of our client unless otherwise noted.

TABLE 1

Site Conceptual Model Summary

Former USA Service Station No. 57 10700 MacArthur Boulevard Oakland, California

ltem	Comment				
Source of Contamination	Former UST's, dispensers, and product piping.				
Chemicals of Concern	Petroleum hydrocarbons (TPHG, BTEX compounds, MTBE, TBA, and 1,2-DCA). TPHD has been reported; not a chemical of concern.				
Site Vicinity	Situated on shopping center property. Surrounding land developed for residential use, commercial use, and freeway.				
Summary of Investigations	Compliance soil samples were collected when the UST's, dispensers, and product pipe were removed in 1994. A total of twenty soil borings have been drilled. Eight of the borings were converted to groundwater monitoring wells.				
Subsurface Geology	The site is underlain by interbedded fine-grained (silt and clay) and sandy sediments (silty and clayey sand), from approximately 10 to more than 40 feet bgs. A laterally continuous stratum of sandy and clayey gravel is encountered at approximately 11 to 25 feet bgs. This interbedded unit overlies deeply weathered, highly fractured, silty sandstone and siltstone bedrock. The contact between the sediments and the underlying bedrock appears to dip toward the north at approximately 25° from horizontal.				
Groundwater flow direction and gradient	Depth to groundwater measurements have fluctuated approximately 10 to 12 feet since monitoring was initiated in 1995. Groundwater flow direction has been and towards the north, south, southwest, southeast, radial toward wells S-1, S-2, and MW-7, and radial away from MW-3. During the most recent monitoring event (January 19, 2005), groundwater was measured between 10.34 and 20.33 feet bgs. Gradients have fluctuated from 0.001 to 0.086 ft/ft.				
Maximum Concentrations in Soil	TPHG = 2,400 mg.Kg (UST pit, 10/94) TPHD = 330 mg.Kg (UST pit, 10/94) Benzene = 9.6 mg.Kg (UST pit, 9/94) Toluene = 21 mg.Kg (UST pit, 9/94) Ethylbenzene = 40 mg.Kg (UST pit, 9/94) Xylenes = 260 mg.Kg (UST pit, 9/94)				
Maximum Concentrations in Groundwater	TPHG = 160,000 μg/L (Well S-2, 7/31/98) TPHD = 7,300 μg/L (Well S-1, 4/28/98) Benzene = 5,700 μg/L (Well MW-3, 11/22/95) Toluene = 3,800 μg/L (Well S-2, 2/12/87) Ethylbenzene = 1,300 μg/L (Well S-2, 2/12/87) Xylenes = 11,000 μg/L (Well S-2, 2/12/87) MTBE = 750 μg/L (Well S-2, 11/19/02) TBA = 2,000 μg/L (Well MW-3, 8/10/04) 1,2-DCA = 270 μg/L (Well MW-3, 8/10/04)				

TABLE 1

Site Conceptual Model Summary

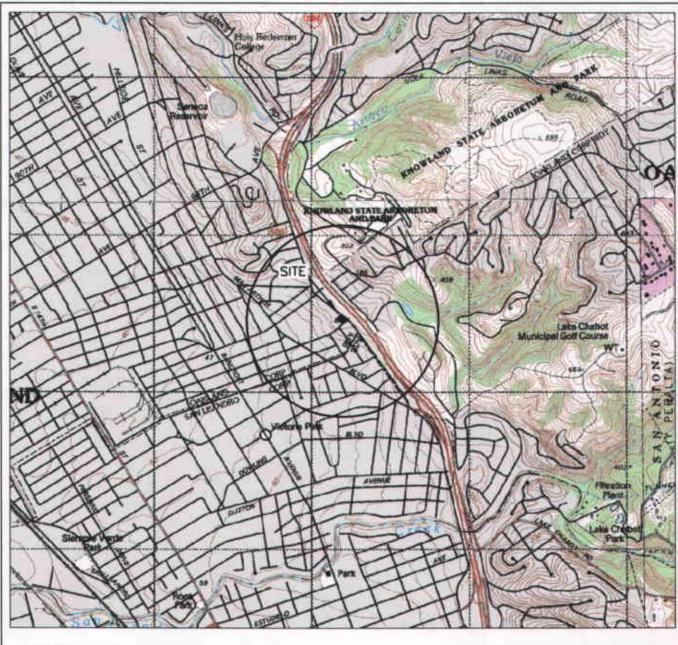
Former USA Service Station No. 57 10700 MacArthur Boulevard Oakland, California

Extent of Impact in Soil	Extent of vadose zone impact appears to be adequately characterized. Impact is limited laterally to the vicinity of the former UST pit, dispensers, and product piping trench. Impact extends vertically to groundwater (Groundwater has fluctuated between 7 and 21 feet bgs).			
Extent of Impact to Groundwater	Extent of groundwater impact appears to be adequately characterized, and limited to the vicinity of wells S-1, S-2, MW-3, and MW-7.			
Potential Sensitive Receptors	There are no water supply wells at the site. The nearest supply well is an irrigation well approximately 1,000 feet to the southwest.			
Potential Exposure Pathways	There do not appear to be any complete exposure pathways at the site at this time. Proposed redevelopment plans have the potential to create exposure pathways via volatilization to indoor air and dermal contact with impacted groundwater.			
Feasibility Studies	Testing performed in July 2004 indicated that DPE was a viable remedial alternative to remove hydrocarbon mass.			
Remedial Efforts	Approximately 775 cubic yards of soil were reported excavated from the former UST pit in 1994. During the DPE feasibility test, approximately 13.34 pounds of TPHG were removed via soil vapor extraction, and approximately 0.015 pounds of TPHG was removed via extraction of impacted groundwater.			
Next Phase of Activity	Perform additional DPE events to further reduce the TPHG mass in the groundwater and vadose zone.			

Table 2 - DRILLING AND WELL CONSTRUCTION SUMMARY

Former USA Station #57 10700 MacArthur Boulevard Oakland, California

ID	Date	Boring Dia. (inches)	Boring Depth (feet bgs)	Casing Diameter (inches)	Casing Depth (feet bgs)	Slot Size (inches)	Screen Interval (feet bgs)
Monitoring	Wells						
S-1	2/12/87	8	40	3	40	0.02	20 - 40
S-2	2/12/87	8	40	3	40	0.02	20 - 40
MW-3	2/28/95	10	44	4	44	0.02	24 -44
MW-4	11/20/95	10	40.5	4	40.5	0.02	10 - 40.5
MW-5	11/20/95	10	41	4	40	0.02	10 - 40
MW-6	11/20/95	10	40.5	4	40.5	0.02	10 - 40.5
MW-7	11/21/95	10	41	4	40	0.02	10 - 40
MW-8	11/21/95	10	35.5	4	35	0.02	10 - 35
Soil Boring	<u>(S</u>						
Α	2/12/87	8	20				
В	2/12/87	6	20				
C	2/12/87	6	20				
D	2/12/87	6	20				
B-1	2/28/95	8	46				
B-2	3/1/95	8	31				
B-3	3/1/95	8	21				
B-4	3/2/95	8	12				
B-5	3/2/95	8	12				
B-6	3/2/95	8	12				
B-7	3/2/95	. 8	12				
B-8	3/2/95	8	12				



GENERAL NOTES:
BASE MAP FROM U.S.G.S.
OAKLAND, CA
7.5 MINUTE TOPOGRAPHIC
PHOTOREVISED 1980



QUADRANGLE LOCATION



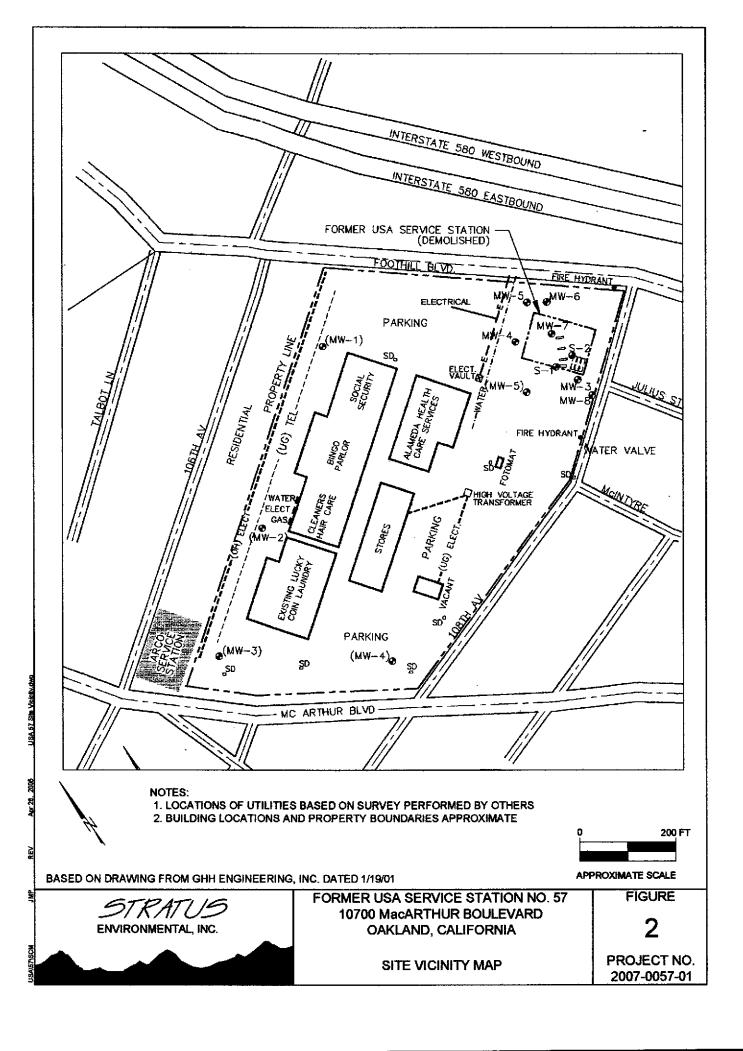
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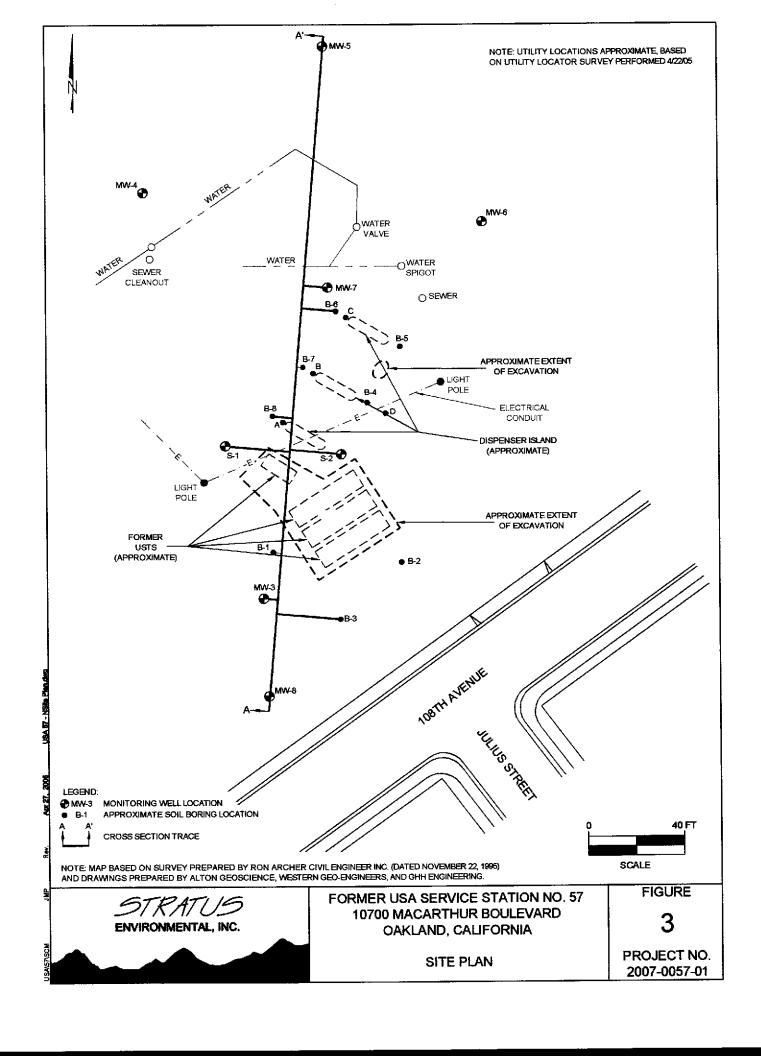
STRATUS ENVIRONMENTAL, INC.

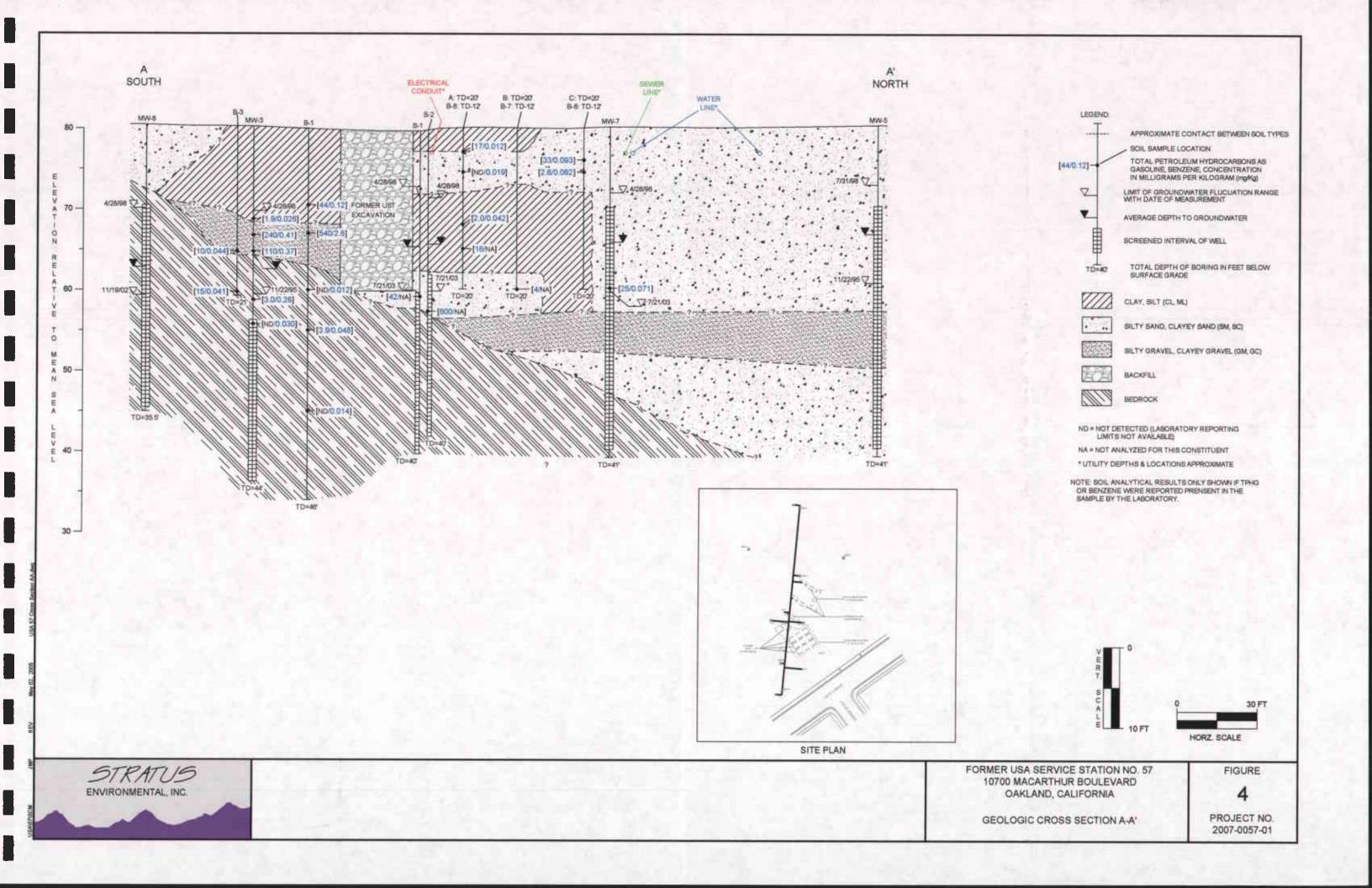
FORMER USA SERVICE STATION NO. 57 10700 MACARTHUR BOULEVARD OAKLAND, CALIFORNIA SITE LOCATION MAP FIGURE

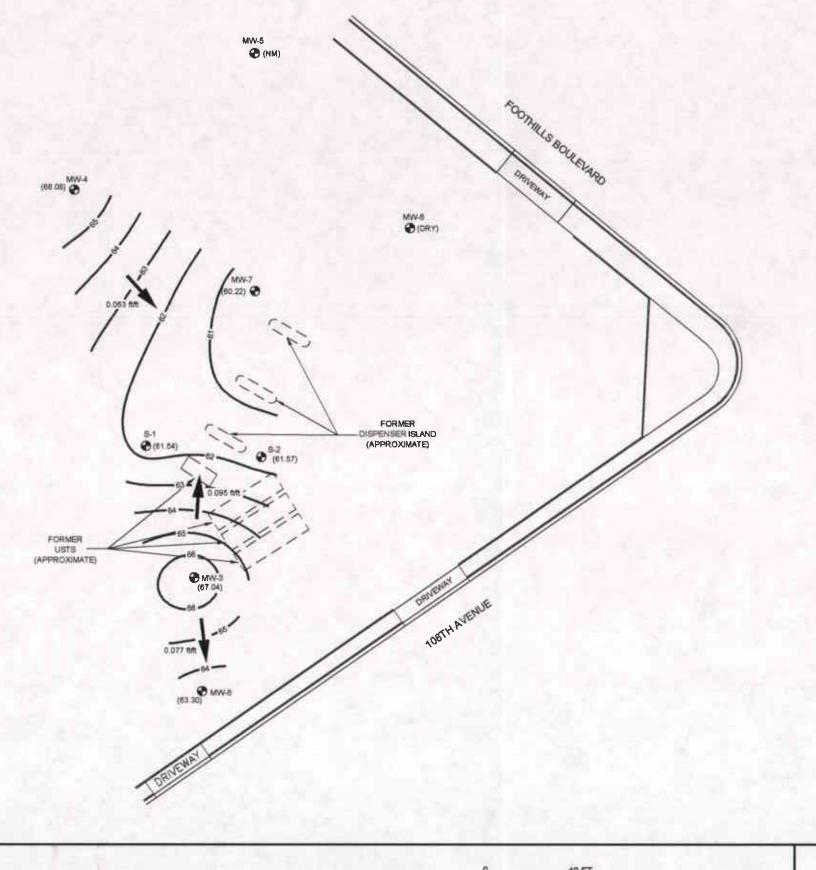
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LEGENO

MW-3 MONITORING WELL LOCATION

(61.54) GROUND WATER ELEVATION IN PEET RELATIVE TO MEAN SEA LEVEL

WATER TABLE CONTOUR IN FEET RELATIVE TO MEAN SEA LEVEL

INFERRED DIRECTION OF GROUND WATER FLOW

(NM) NOT MEASURED (WELL DAMAGED)

WELLS MEASURED: 1/19/05

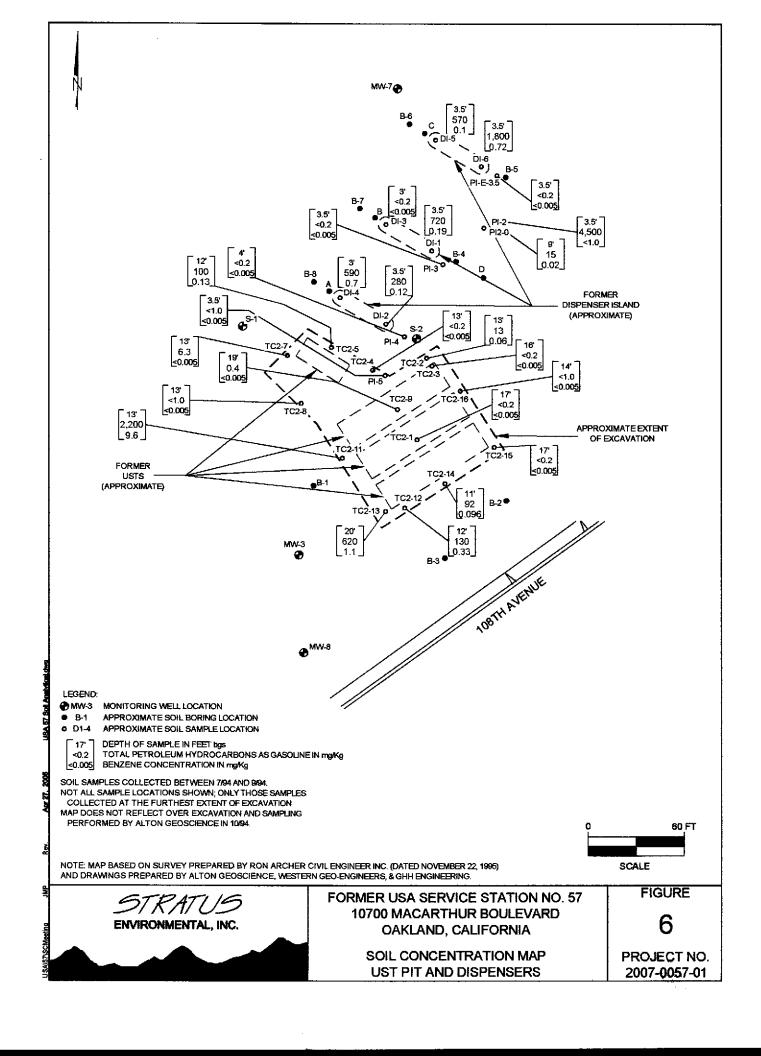
HORZ, SCALE

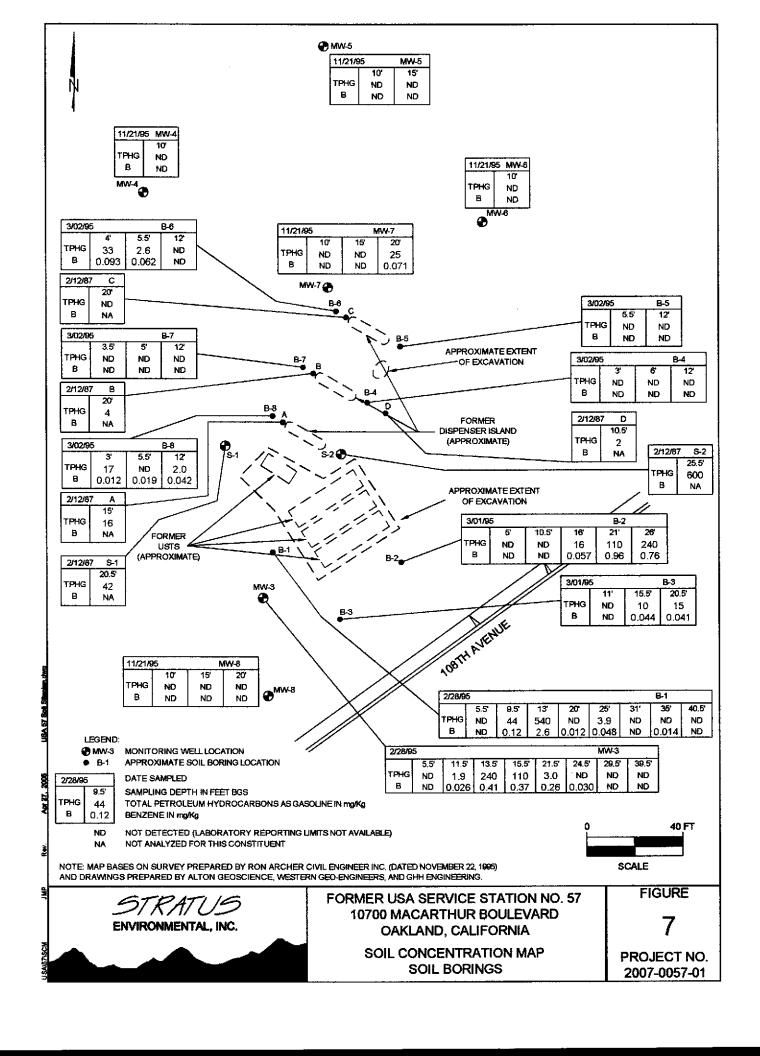
FORMER USA SERVICE STATION NO. 57 10700 MACARTHUR BOULEVARD OAKLAND, CALIFORNIA

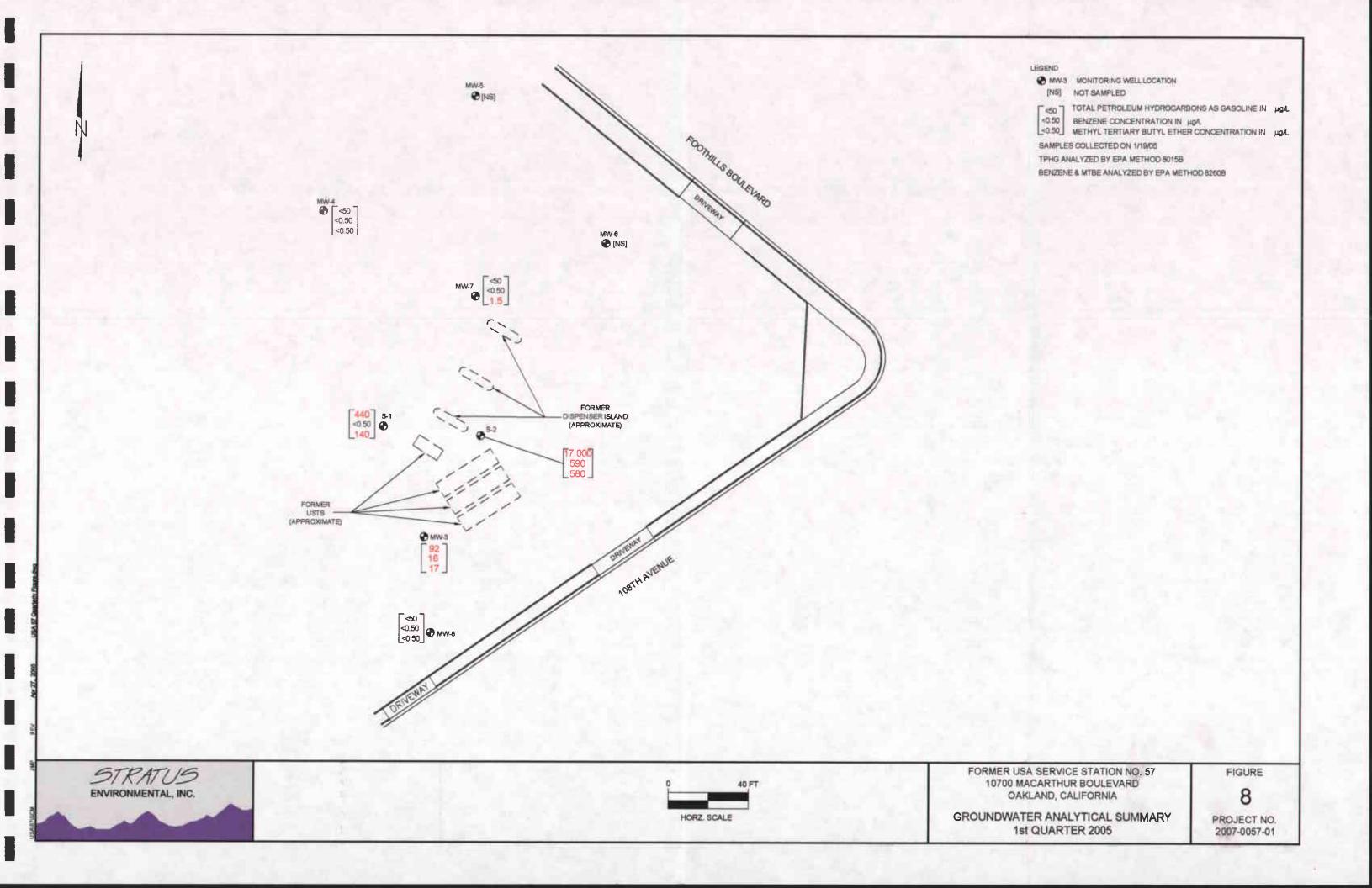
GROUNDWATER ELEVATION CONTOUR MAP 1st QUARTER 2005 FIGURE 5

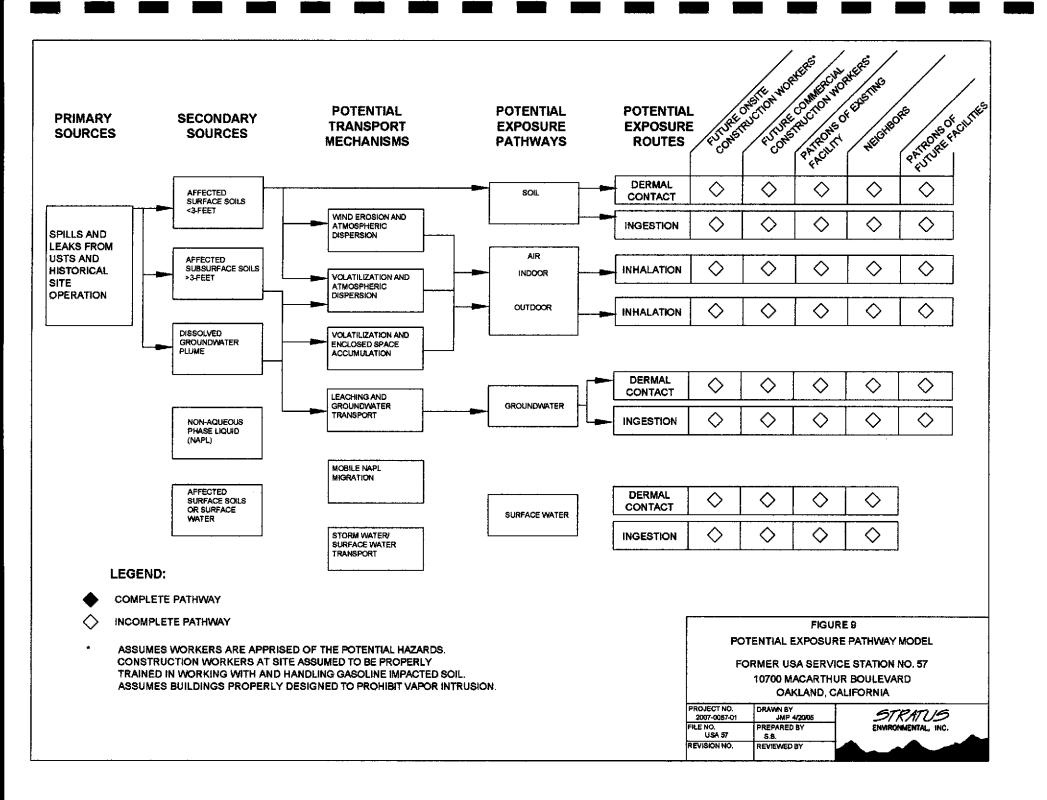
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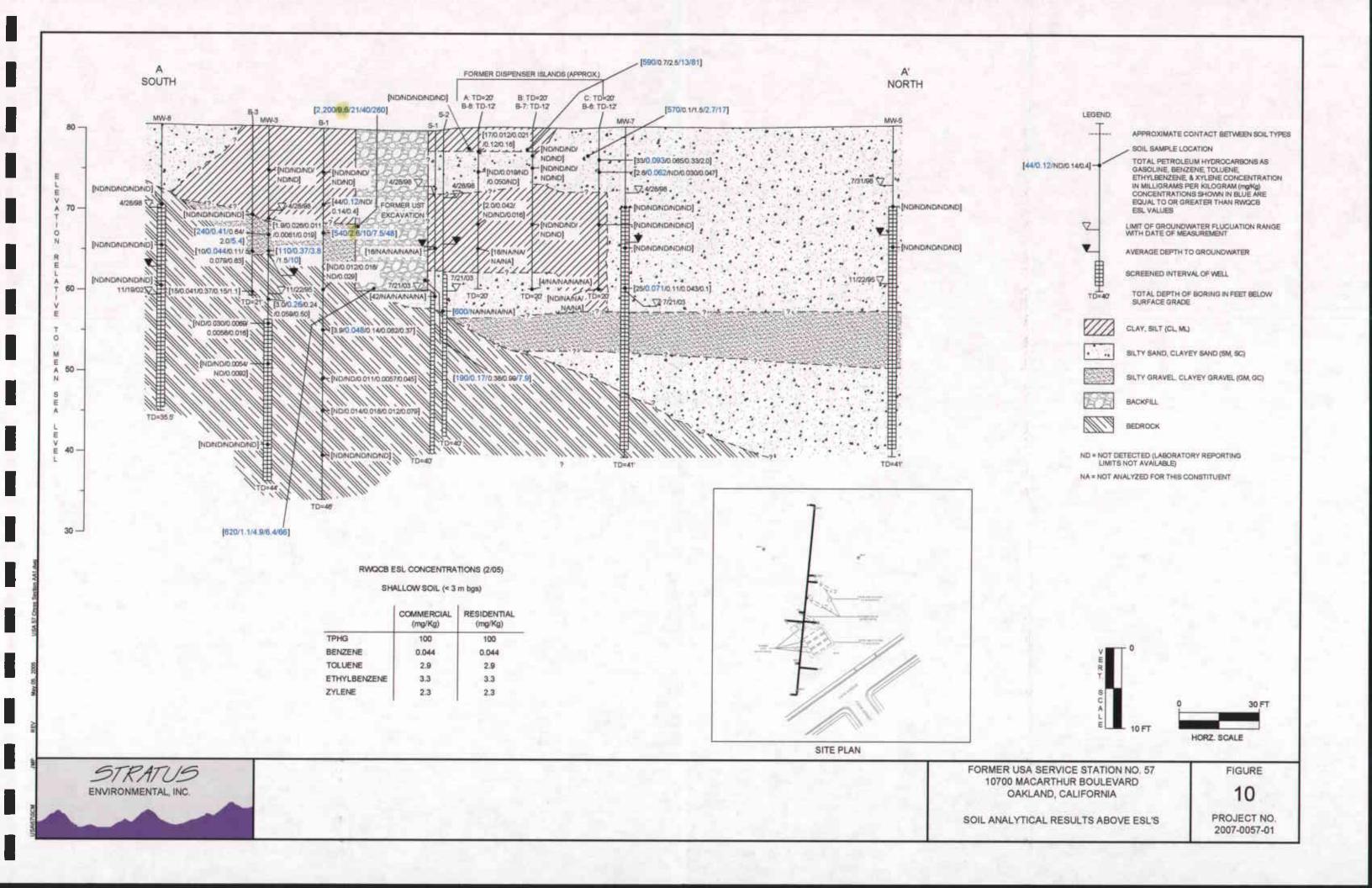
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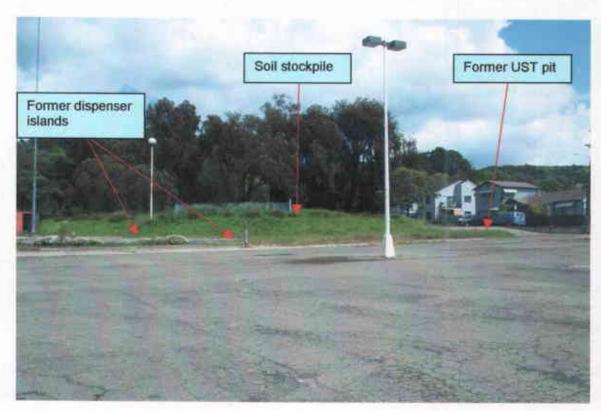




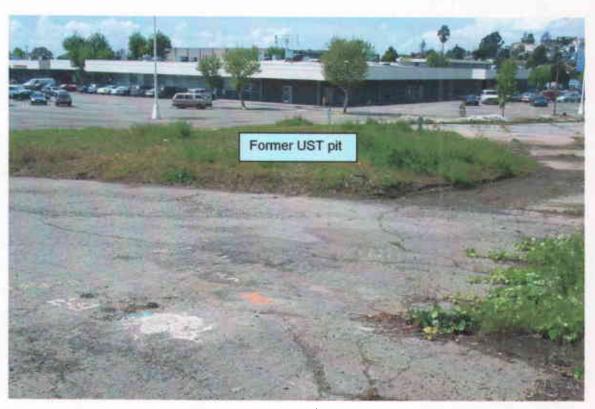




APPENDIX A PHOTOGRAPHS OF CURRENT SITE CONDITIONS



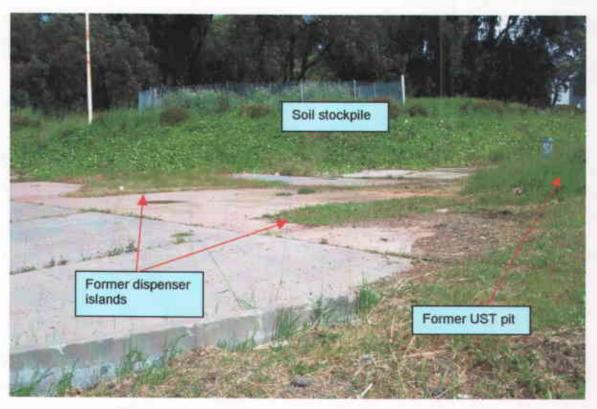
Subject site, viewed from Foothill Square parking lot (facing east).



Former UST pit, viewed from 108th Avenue (facing northwest).



Subject site, viewed from Foothill Square parking lot (facing south).



Former Dispenser islands, viewed east from parking lot.

APPENDIX B

BORING LOGS AND WELL CONSTRUCTION DETAILS

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dark grayish-brown silty sandstone; fractured

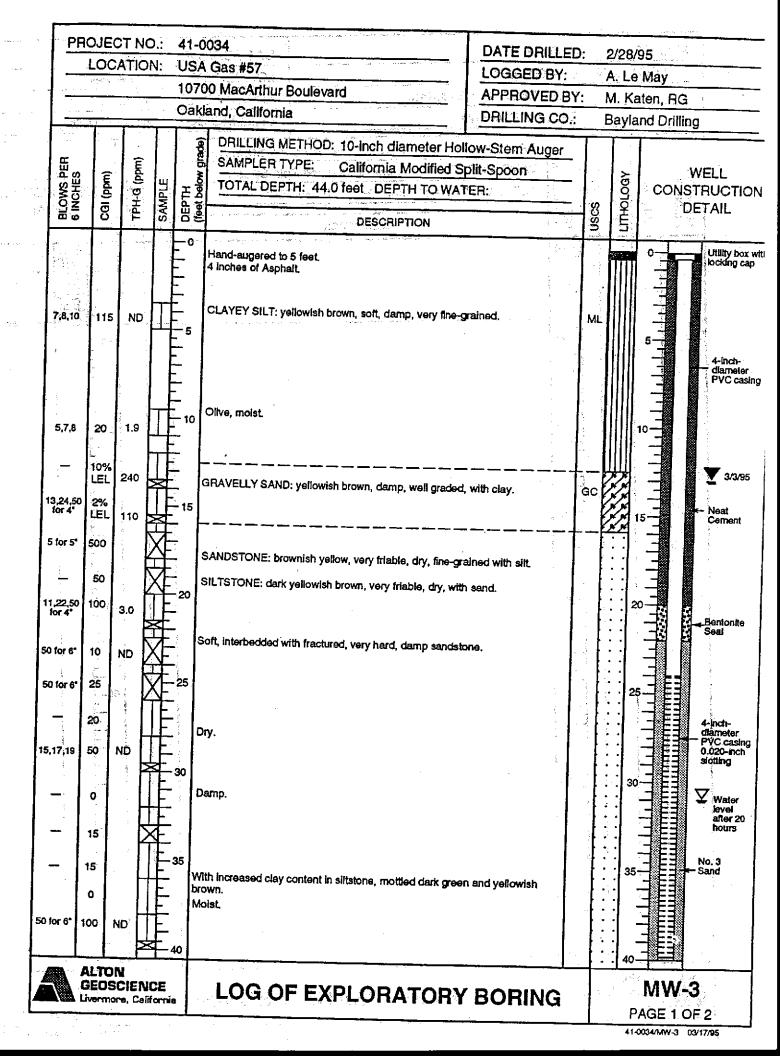
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a company of				1	Vana	And the second of the second o	NG CO.:	E	Bayla	and Drilling
	BLOWS PER 6 INCHES	CGI (ppm)	TPH-G (ppm)	SAMPLE	DEPTH (feet below grade)	DRILLING METHOD: 10-inch diameter Hollow-Stem SAMPLER TYPE: California Modified Split-Spoor TOTAL DEPTH: 44.0 feet DEPTH TO WATER: DESCRIPTION		uscs	итногосу	WELL CONSTRUCTION DETAIL
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- 1 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2			T NO		41-0 USA	034 Gas #57	DATE DRILLED		2/28/9	
					1070	O MacArthur Boulevard	LOGGED BY: APPROVED BY DRILLING CO.:	<u>':</u>		May Iten, RG Ind Drilling
	BLOWS PER 6 INCHES	CGI (ppm)	TPH-G (ppm)	SAMPLE	DEPTH (feet below grade)	DRILLING METHOD: 8-inch diameter Hollor SAMPLER TYPE: California Modified Sp TOTAL DEPTH: 46.0 feet DEPTH TO WAT	olit-Spoon	USCS USCS	LITHOLOGY	WELL CONSTRUCTION DETAIL
12	2,15,10 1,27,35	75 70% LEL 175 ALTI	ND ND ND ND ND ND ND ND ND ND ND ND ND N		- 15 - 20 - 25 - 30	Hand-augered to 4 feet. 6 inches of Concrete. SILTY CLAY: dark grey brown, soft, damp. CLAYEY SILT: dark yellowish brown, soft, damp, few single pebbles. GRAVELLY SAND: mottled dark yellow brown and greet clay. From approximately 17 feet to bottom of hole: Interbeddistitatione. SANDSTONE: light olive brown, very fractured and friable carbonate infill in fractures. SILTY CLAY (weathered bedrock): dark grayish brown, soft carbonate infill in fractures. SILTY CLAY (weathered bedrock): light olive brown, soft carbonate infill in fractures. SILTY CLAY (weathered bedrock): light olive brown, soft carbonate infill in fractures.	n, loose, damp, with ed sandstone and le with calcium soft, damp at 10 feet. le with calcium	CL ML	2	0 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -
		GEO	SCIE			LOG OF EXPLORATOR	Y BORING			B-1 PAGE 1 OF 2

PRO		T NO	,	USA 1070	Gas #57 L 0 MacArthur Boulevard	DATE DRILLE LOGGED BY: APPROVED B DRILLING CO	Y: N	A. Le И. Ka	May May aten, RG and Drilling
BLOWS PER 6 INCHES	CGI (ppm)	TPH-G (ppm)	SAMPLE	DEPTH (feet below grade)	DRILLING METHOD: 8-inch diameter Hollow-SAMPLER TYPE: California Modified Split-TOTAL DEPTH: 46.0 feet DEPTH TO WATER DESCRIPTION	-Ѕрооп	SOSN	ПТНОГОВУ	WELL CONSTRUCTION DETAIL
27.30	4	を Manager Company C	The second secon	45 	GRAVELLY CLAY (weathered bedrock): dark yellowish browell graded, with sand and pebbles to 1/4 inch.		The state of the s		→
		ON OSCIE			LOG OF EXPLORATORY	BORING	G	÷ :	B-1 PAGE 2 OF 2

41-0034/8-1 03/17/95

PRO			_			DATE DRILLE	D: 3/1/9	5
	OC.	ATIO	N:			OGGED BY:	A. Le	May
	-	<u>.1 % * * </u>				PPROVED B		iten, RG
2.2.00	<u> </u>		14	Oal	kland, California	PILLING CO.		nd Drilling
BLOWS PER 6 INCHES	CGI (ppm)	TPH-G (ppm)	SAMPLE		DRILLING METHOD: 8-Inch diameter Hollow-S SAMPLER TYPE: California Modified Split- TOTAL DEPTH: 31.0 feet DEPTH TO WATER DESCRIPTION	Spoon	USCS	WELL CONSTRUCTI DETAIL
					Hand-augered to 5 feet. 4 inches of Asphalt.			0-
,12,17 ,	60	ND	X	- - - -	CLAYEY SILT: dark yellowish brown, soft, damp, fine grain	ed, low plasticity.	ML	5-1
,16,21	80	ND		- 10 - 1	At approximately 10 feet depth includes small peobles and recover and green.	nottled dark		10 -
27,31	5% ÆL	16	,	15	SANDY CLAY: dark yellowish brown, damp, fine-grained. SANDSTONE: brownish yellow, fractured, damp, fine-graine	d with Alay	CL	- Neat Cermen Grout
	25	110	The state of the s	20	SANDY CLAY (weathered bedrock); dark yellowish brown, d fine-grained. SANDSTONE: brownish yellow, fractured, fine-grained, with staining.	emp,	2	
1,17 15 LI	0% EL	240		-25	interbedded with sandy clay. SANDY CLAY (weathered bedrock) to 25 feet, then fractured	sandstone.	2	
,13 Lf o sc:	ff			- 30 -	GRAVELLY SAND (weathered bedrock): very dark grayish br saturated, well graded.	own, loose,	30	
:				- 35		i i	35	
				-40	***	man and a second	40	
A GI		N CIEN ra, Ca			LOG OF EXPLORATORY E	BORING		B-2 PAGE 1 OF 1

41-0034/8-1 03/17/95

, —	JEC OCA	7.		USA 1070	Gas #57 Gas Athur Boulevard	DATE DRILLED LOGGED BY: APPROVED BY DRILLING CO.:	. A	1. Ka	May sten, RG
BLOWS PER 6 INCHES	CGI (ppm)	TPH-G (ppm)	SAMPLE	DEPTH (feet below grade)	DRILLING METHOD: ,8-inch diameter Hollow SAMPLER TYPE: California Modified Sp TOTAL DEPTH: 21.0 feet DEPTH TO WATE	lit-Spoon	USCS	итногову	WELL CONSTRUCTION DETAIL
5,7,10 8,10,8 28,39,43 27,46,23	o 5	15	The second secon	0 5 5 9 10 25 35 35 35 35	Hand-augered to 5 feet. 4 inches Asphalt. CLAYEY SILT: brown, soft, damp, fine-grained, with sampebbles. SANDY CLAY: very dark grayish brown, soft, damp, with a moderate amount of silt. SANDSTONE: fight yellowish brown, friable, very fracture thick layer of sandy day at 15 feet. Interbedded with gravelly day. GRAVELLY CLAY (weathered bedrock): dark olive brown with large pebbles to 0.5-inch diameter.	n small pebbles and and and and and and and and and and			0
	ALTON GEOSCIENCE LIVermore, California LOG OF EXPLORATORY BORIN								²⁰ ─ B-3 PAGE 1 OF 1

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					Gas #57	DATE DRILLED:	3/2/95	<u> </u>
	913.	1.5	34. 		O MacArthur Boulevard	LOGGED BY:	A. Le May	<u> </u>
¥ :	\$ 1				and, California	APPROVED BY: DRILLING CO.:	M. Katen, RG	-
4.43				1	Control of the Contro		Bayland Drilling	
			i.	arade)	DRILLING METHOD: 8-Inch diameter Hollo SAMPLER TYPE: California Modified Sr			,
ES E	Ê	ndd)	Ш	8	SAMPLER TYPE: California Modified Sp		≽ WE	
BLOWS PER 6 INCHES	CGI (ppm)	TPH-G (ppm)	SAMPLE	DEPTH (leet below	TOTAL DEPTH: 12.0 feet DEPTH TO WAT		SS DET	4.7
<u> </u>	ဝ	H.	Š	 	DESCRIPTION		S P DET	AIL E
in a second				上°	Hand-augered to 4 feet.		0	
			┝	<u> </u>	- 110,000	ua et militari		i
5,7,13	5	ND		F	SANDY CLAY: olive brown, soft, saturated from surface of pebbles.		or 3	- Andrews
	s. 			-, _	SAND dath collection is	1 4 4 4		and the second
7,7,8	15	ND		_5 	SAND: dark yellowish brown, loose, saturated, medium- sand, poorly graded.		5-	Neat Cement
		4 4					SP	Grout
Marie N						·		\$ \$
				 -	SANDY CLAY: clive brown, medium soft, moist, with sm	noll amount of		•
6,15,15	15	ND	1	10	pebbles.	iali amount of	10-3-11	
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	EOS	CIEN 70, Cal		.	LOG OF EXPLORATORY	BORING	B-4	
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41-0034/8-4 03/21/95

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7		ATION			Gas #57 0 MacArthur Boulevard	LOGGED BY: APPROVED BY:	A. Le	May iten, RG
i de la companya de l	5 c	3.53 (2.3			and, California	DRILLING CO.:		nd Drilling
BLOWS PER 6 INCHES	CGI (ppm)	TPH-G (ppm)	SAMPLE	DEPTH (feet below grade)	DRILLING METHOD: 8-Inch diameter Holic SAMPLER TYPE: California Modified S TOTAL DEPTH: 12.0 feet DEPTH TO WAT DESCRIPTION	plit-Spoon	иясь итноцову	WELL CONSTRUCTION DETAIL
5,7,14	15	ND.	The second secon	5 10 25 25 36 40 40 40 40 40 40 40 40 40 40 40 40 40	Hand-augered to 4 feet. 6 inches Concrete. SANDY CLAY: clive brown, very soft, damp, with small. Moist; with slit.	I pebbles.		- Neat Cement Grout
A		ON SCIE			LOG OF EXPLORATOR	Y BORING		B-5 PAGE 1 OF 1

41-0034/B-5 03/21/95

		N CIEN re, Cel			DRING		B-6 PAGE 1 0	୍ର ୍ଟ୍ର F1	
2.2.5 2.7.11 2,13.21	130	33 26 NO		10 - 15 - 30 - 35 - 35 - 35 - 35	Hand-augered to 4 feet. 6 Inches of Concrete. SANDY CLAY: green clive gray, very soft, damp, with silt and opebbles. Olive gray. SILTY CLAY: dark brown, soft, with occasional larger pebbles.				- Neat Cement Grout
BLOWS PER 6 INCHES	CGI (ppm)	TPH-G (ppm)	SAMPLE	DEPTH (faet below grade)	DRILLING METHOD: 8-inch diameter Hollow-Ste	m Auger	изся	W CONST	:
		ATIO	V ;	1070	00 MacArthur Boulevard APF	GGED BY: PROVED BY: LLING CO.:	M. K	e May aten, RG and Drilling	
 		TNC				TE DRILLED:	3/2/9	95	
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41-0034/8-6 03/21/95

	PRC	OJEC	T NO).:	41-0	034	DATE DRILLED:	 : :	3/2/9	15 (10 to 10
		LOC!	ATION	<u>v:</u>	Sec. 17.4.5	Gas #57	LOGGED BY:			May
٠					1.070	00 MacArthur Boulevard	APPROVED BY:			aten, RG
				·· ==	Oakl	land, California	DRILLING CO.:		3ayla	and Drilling
	BLOWS PER 6 INCHES	CGI (ppm)	TPH-G (ppm)	SAMPLE	DEPTH (feet below grade)	DRILLING METHOD: 8-inch diameter Hollo SAMPLER TYPE: California Modified Sp TOTAL DEPTH: 12.0 feet DEPTH TO WAT DESCRIPTION	plit-Spoon	uscs	ШНОГОВУ	WELL CONSTRUCTION DETAIL
, sie	22.5 2.7.11	130 60 10	ND ND		ارابارابارابا	Hand-augered to 5 feet. 6 inches Concrete. SANDY CLAY: dark olive gray, very soft, damp, with silpebbles. At 4.5 feet depth, dark brown, harder, increased silt cor	複樂性ない かごり	CL		5— Neat Cament Grout
	2,13,21	10	ND	The second secon	10	Dark olive gray, medium hard, damp, with slit. At 11.5 feet depth, dark brown, hard.				10 11 11 1
			2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	The second secon	15 15 					15-
	at the law		A Company of the Comp	Victorial and the second of th	25					25 1 1 1 2 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3
					30					30 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7
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41-0034/8-7 03/21/95

PRO	JEC	T NO).:_	41-0	034	ATE DRILLED:		3/2/9	5	
L	.OC/	OITA	V :	USA	Gas #57 L	OGGED BY:		A. Le	May	
		ATION: USA Gas #57 10700 MacArthur Boulevard Oakland, California DRILLING METHOD: 8-Inch diameter Hollow-Stem Auge SAMPLER TYPE: California Modified Split-Spoon TOTAL DEPTH: 12.0 feet DEPTH TO WATER: DESCRIPTION Hand-augered to 4 feet, 6 inches Concrets, SANDY CLAY: dark olive gray, very soft, damp, with some small grave peobles GRAVELLY CLAY: dark olive gray, very soft, damp, with some small grave peobles 2.0 SILTY CLAY: dark yellowish brown, hard, damp, with rare small peobles with sand. DN SCIENCE LOGGED E APPROVE DRILLING APPROVE DRILLING DRILLING BRILLING BRI	APPROVED BY:	1	Μ. Κε	ten, RG				
<u></u>				Oak	and, California	RILLING CO.:		онл 5 10 5 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	nd Drilling	
BLOWS PER 6 INCHES	CGI (ppm)	TPH-Q (ppm)	SAMPLE	DEPTH (feet below grade)	SAMPLER TYPE: California Modified Split-	Spoon	USCS	ПТНОСОВУ	CONST	ELL RUCTION TAIL
4,4,7 2,3,5	90 95 25	ND		15 10 15 20 25 30	6 inches Concrete. SANDY CLAY: dark olive gray, very soft, damp. CLAYEY SAND: dark olive gray, very soft, damp, with som pebbles. GRAVELLY CLAY: dark olive gray, very soft, saturated. SILTY CLAY: dark yellowish brown, hard, damp, with rere		CL SC CL		15 20 25 30 30 30 30 30 30 30 30 30 30 30 30 30	Neat Cement Grout
	:	;								
A						BORING			PAGE 1 0	OF 1

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<u></u> -	OCA	4OIT	1:						
		ATION: USA Gas #57 10700 MacArthur Boulevard Oakland, California DRILLING METHOD: 10-inch diameter Hollow-Stem Auger SAMPLER TYPE: California Modified Split-Spoon TOTAL DEPTH: 40.5 feet DEPTH TO WATER: 15.0 feet DESCRIPTION Hand-sugered to 5 feet. SILTY SAND: dark yellowish brown, medium dense, damp, poorly graded. SANDY SILT: dark yellowish brown, medium dense, moist, with clay, contains carbonate pebbles up to 0.13-inch diameter. SILTY SAND and GRAVEL Mixture: dark yellowish brown, medium dense, wet, with clay, with pebbles to 0.5-inch diameter. SILTY SAND and GRAVEL Mixture: strong brown, dense, damp, with pebbles to 0.5-inch diameter.			V	<u> & W</u>	/ Drilling		
				9	DRILLING METHOD: 10-inch diameter Hol	low-Stem Auger			-
## ^{**}		Ê		grac	SAMPLER TYPE: California Modified S	plit-Spoon		<u>.</u>	WELL
S PE	m)	dd) t	<u>ات</u> ا	<u>₩</u>	TOTAL DEPTH: 40.5 feet DEPTH TO WAT			P	CONSTRUCTION
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<u>m</u> o	Q .k:	F	S	0.5	DESCRIPTION				
	۷,			E	Hand-augered to 5 feet.				O Monument box with locking cap
				E '			215		- Jocking Cap
	Was			<u> </u>					Neat
			Ļ	F			SM		Cement
9,14,15	-	-		- 5	SILTY SAND: dark yellowish brown, medium dense, d	amp, poorly graded.	3 V		5
			Γ	E					4-Inch- dlameter PVC casing
			ι.	F	<u> </u>				Bentonite
				F	SANDY SII Tudork walloudsh beauty alter damp with a	المالة			Seal
8.11.14	0	ND		├ 10	SAND I SILIT dak yanowish blown, sun, damp, with t	lay.	ML		10 -
				Ė.					
				E					
		2		Ė					
18,21,34	5 -			15	SILTY SAND: dark yellowish brown, medium dense, m contains carbonate pebbles up to 0.13-inch diameter.	oist, with clay,	SM		15 E
			广	F					
	a	٠.		E.,				脚	
1 3				Ė.				17	
18,31,34	0		П	E 20	SILTY SAND and GRAVEL Mixture: dark vellowish bu	own, medium]
			-	F.					Sand
				E		.,	!	<i>y y</i>	
				Ε.		w	GC		
14,24,36	0		П	25	SILTY CLAYEY SAND and GRAVEL Mixture: strong b	rown, dense,			25-
			┸	F	damp, with peobles to 0.5-inch diameter.	. स - स			4-inch-
				<u> 200</u> 1 - 1	r which indicate the little beautiful to the contract of the c				diameter PVC casing
				E	and the second of the second o				0.020-Inch stotting
12,18,23	0		T	-30		e e e			130—E
			屵	<u></u>					
				F	·	e e e e e e e e e e e e e e e e e e e			
				E		·-		//	
0.00.00			\vdash	_ 35	A A a different and a second				35— []
9,22,31	0		ot	-	medium dense.				
				F				(I)	
				F				//	
30,50	o		 -	E 40	Ingrapped eith sentent			//	40 = = = = = = = = = = = = = = = = = = =
	. <u> </u>		斉	F	Increased an coliner	<u> </u>		22	End cap
	ALT	ON DSCIE	ĘΝ.	CE	LOG OF EXPLORATOR	RY BORING			MW-4
		more,			LOG OF EXTENSION			<u>.</u>	PAGE 1 OF 1
									41-0034/MW-4 01/05/96

		ON OSCIE more, (LOG OF EXPLORATOR	Y BORING		MW-5 PAGE 1 OF 1
10,21,32			T	40				40 End cap
5,12,21	0			35 - - - -	With lenses up to 4 inches of more gravel-rich, saturate			35
10,15,24	0		¥	30 30 	SILTY CLAYEY SANDY GRAVEL: dark yellowish brown poorly graded. SILTY SAND: dark yellowish brown, medium dense, dargravel and some clay.	mp, with	SM	30-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1
	4 3 7 7 8 W					in loses seburated		4-inch- damete PVC car 0.020-in slotting
6,9,16	_		X		No recovery, sampler saturated, gravel lense?		GM	25—
12,18,24	0			- - 20 -				20 - No. 3 - Sand
16,23,24	0	ND		—15 - - -	SILTY SAND: dark yellowish brown, medium dense, dar gravel and some clay.	mp, with it makes	SM	15 -
10,14,19	0	ND	X	- - - - - - -	graded, with occasional pebbles to 0.5-inch diameter.			
			H	 - - - - -	CLAYEY SAND: dark yellowish brown, medlum dense,	damp, poorly	sc	damete PVC cas Bentonit
7,18,21	0		Ţ		Hand-augered to 5 feet. 4 inches Asphalt. SILTY SAND: yellowish brown, medium dense, damp, f	īne-grained, poorly	SM	locking ca
BLOWS PER 6 INCHES	PID(ppm)	TPH-G (ppm)	SAMPLE	DEPTH (feet below grade)	DRILLING METHOD: 10-inch diameter Hollo SAMPLER TYPE: California Modified Sp TOTAL DEPTH: 41.0 feet DEPTH TO WATE	lit-Spoon	USCS	WELL CONSTRUCTIO DETAIL Monument box with
					and, California	DRILLING CO.:		/ Drilling
L	OCA	NOIT			Gas #57 0 MacArthur Boulevard	LOGGED BY: APPROVED BY:	A. Le M. Ka	May ten, RG
PRO	JEC.	T NO	:	41-00)34	DATE DRILLED:	11/20	

PRO				41-00		DATE DRILLED:		1/20/	
L(OCA	TION			Gas #57	LOGGED BY:			May
			-,		0 MacArthur Boulevard	APPROVED BY:			ten, RG
ļ - ; -			١.	Oakla	and, California	DRILLING CO.:	· V	& W	Drilling
BLOWS PER 6 INCHES	n)	TPH-G (ppm)	ш	DEPTH (feet below grade)	DRILLING METHOD: 10-inch diameter Hollow-Stem Auger SAMPLER TYPE: California Modified Split-Spoon TOTAL DEPTH: 40.5 feet DEPTH TO WATER: 15.0 feet				WELL CONSTRUCTION
OWS CHE	PID(ppm)	 ±	SAMPLE	PTH # Del	TOTAL DEFIN. 40.5 Teel DEFIN TO WAT	Ln. 15.0 leet	nscs	LITHOLOGY	DETAIL
11 9 11 8	PID	ТР	S. IAS	DE (fee	DESCRIPTION		Sn	Ę	
e i i ĝi i i				ابابا	Hand-augered to 5 feet.	d d			Monument box with locking cap
•									Neat Cement
10,16,21	-	4	X	, 	SILTY SAND for 2 inches: brown, dry, then SILTY SAND: dark yellowish brown, medium den some clay.	se, damp with	SM		4-inch- dlameter PVC casing
88	· · · · · · · · · · · · · · · · · · ·			- - 1 10	With gravel.		14.5		Bentonite Seal
13,25,30	• 0 :	ND	×	111					
9,18,28	0			_ _ _ 15	SILTY SAND and GRAVEL Mixture: moist, with clay.	era e e e e e e e e e e e e e e e e e e			
									No. 3
18,21,24	a			 20	Wet.				20
				_		L .			<u> </u>
9,14,19	0			25 	Gravel-rich lenses up to 4-inch thick.		GC)	25 — E 3 4-Inch-
lead A						an in the second			dlameter PVC casing 0.020-inch siotling
6,11,16	- ,		X	_ зо 	Saturated, poor recovery.	and the second second			30-1
		•	. :		As above to Gineber the	W. C.			
12,50 for 4"			\pm	35 	As above for 6 inches, damp. SILTY SANDSTONE BEDROCK: dark yellowish brown fractured and friable.	n, dry,			95-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1
12,17,17	0	·	Į ×		CLAYEY GRAVEL BEDROCK Interbedded: brown, loc includes fractured bedrock pebbles.	ose, saturated,			40————————————————————————————————————
A		ON ISCIE more, (LOG OF EXPLORATOR	RY BORING			MW-6 PAGE 1 OF 1

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		GEO	SCIE			LOG OF EXPLORATORY BORING	Ì		MW-7 PAGE 1 OF 1 41-0034/MW-7 01/05/96
	,2232	ALT	ואם		- 40	· · · ·	<u> </u>		-
12	,2232	o			- - - -	With claystone interbeds, saturated.			End cap
2:	3,50	0		X	35 1 1	SILTY SANDSTONE BEDROCK; light olive brown, very fractured, moist, very friable, with clay.			35-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1
							SM		
17,	31,32	0		\top	30	SILTY SAND: dark yellowish brown, dense, damp, with gravel and clay.			slotting
					1-1-1	: : : : : : : : : : : : : : : : : : :	ļ		dlameter PVC casing 0.020-linch
14	,19,22	>2,500			 25	CLAYEY SANDY and GRAVEL Mixture: yellowish brown, medium dense, damp, pebbles to 0.13-inch diameter.	GC		25————————————————————————————————————
: 1			:		-	<u> </u>	-		
10,	,13,20	>2,500	25		-20 - -	Slight greenish color.			20 — =
		: 1							
8.	15,23	0	N∩		15				15-
i.					<u>-</u>				
9,	15,22	0	ND		10	With clay and carbonate pebbles to 0.5-inch diameter.	SM		10
	<i>5</i>				- - -				PVC casing Bentonite Seal
6,1	1,19	0		×	5 	SILTY SAND: dark yellowish brown, medium dense, damp, fine-grained, poorly graded.			4-inch-
		2 4	e i Ass	_					Neat Cement
						Hand-augered to 5 feet.			O Monument box with locking cap
	S INC	PID(Ĕ	SAM	DEP (feet	DESCRIPTION	nscs	E	
We pen	HES	(md	G (ppm)	PE	FH ·	SAMPLER TYPE: California Modified Split-Spoon TOTAL DEPTH: 41.0 feet DEPTH TO WATER: 20.0 feet	6	ПТНОГОВУ	WELL CONSTRUCTION DETAIL
					ade)	DRILLING METHOD: 10-inch diameter Hollow-Stem Auger			
			1			0 MacArthur Boulevard APPROVED BY and, California DRILLING CO.:			aten, RG V Drilling
	L	LOCATION: US 107 Oa (mdd) 9-Hdl 1,19 O ND 5,22 O ND 5,23 O ND 1,2 1,11 1		Gas #57 LOGGED BY: 0 MacArthur Boulevard APPROVED BY			May		
	PRO	JECT	ГΝΟ		41-00	DATE DRILLED	: 1	1/21	1/95

· · · · · · · · · · · · · · · · · · ·	Gravel and clay. Compared and clay. Compared a									
L	OCATION: USA Gas #57 10700 MacArthur Boulevard Oakland, California California									
				1070	O MacArthur Boulevard					
		H.		Oakla	ınd, California	DRILLING CO.:	<u>V</u>	& W	Drilling	
					DRILLING METHOD: 10-inch diameter Hollo	ow-Stem Auger				
 #: .		Ê		grac	SAMPLER TYPE: California Modified Sp	lit-Spoon		<u>بر</u>	The second secon	1.00
'S PE	(E)	ф) (ш	∓ <u>§</u>	TOTAL DEPTH: 35.5 feet DEPTH TO WAT	ER; N/A		Σο		
INCE	ID(pi	PH	AMP	EPT leat to	DESCRIPTION	, and a	30SL	<u>¥</u>	ם ט	TAIL
E 9	<u></u>	_	(2)		DESCRIPTION				0	Monument
					Hand-augered to 5 feet.					box with
	1	· 44		-						_ Neat Cement
				5			SM		5—	
10,14,24	gravel and clay. Stil TV SANDSTONE BEDBOCK: vellowish brown, frieble, fractured, d						1.5			diameter -
				<u> </u>	7					PVC casing
300 L 73										Bentonite Seal
		i	H	10	SILTY SANDSTONE BEDROCK: yellowish brown, frial	ble, fractured, dry, very	lense		10-1 E	
50 for 3*	O,	ָ טא	尸	F	,					
				E.						
				E						
50 for 5°	_	ND	臣	15					15—E	
	10			<u> </u>						▼
,										3
				F						Sand
50 for 5°	_	ND	\boxtimes	- 20 -						
\$				<u> </u>						
				<u> </u>			-			
	,		┝	F 76					25	
50 for 6°			\boxtimes	E"I	and the second of the second o					
18/3-4-4					To appear					4-inch- diameter PVC casing:
				_	en de la companya de la companya de la companya de la companya de la companya de la companya de la companya de La companya de la co					0.020-inch slotting
25,32,50			\vdash	 	As above including 6 inches of strong brown claystone	and sand.			30-JEE	
			涔	‡						
				F						
				E						
28 50			\prod	- 35					35	End cap
28,50 for 6"	0		ř	-	,			ŀ		
				E						
				E	:					
				40		-			40	
				<u> </u>			`		MW	/- 8
									PAGE 1	
					<u> </u>					a 04/05/05

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APPENDIX C HISTORICAL SOIL ANALYTICAL DATA

TABLE OF RESULTS

	TABLE OF RESULTS	
in the second second second second second second second second second second second second second second second		
ND = None Detected	Parts per Million	
	(dry soil basis)	

Laboratory Number	Sample Identification	Date Received	Total Hydrocarbons
	Project 100-22. Oakland	.01,	
\$7-02-076-01	A 13.5-1	5' 2/17/87	16. 7
S7-02-076-02	B 18.5-2	医克里克耳 人名西西西西西西西西西西西西西西西西西西西西西西西西西西西西西西西西西西西西	n tali selah bilan 1907 dan 1964. Bilang dan 4 5 memberah bilan 1964 dan 1
\$7-02-076-03		0' 2/17/87,	recent of the first of the second second second second second second second second second second second second
57-02-076-04	D 9-10.5		
\$7-02-076-05 8 0 8 1	US-1 4512 19-20.	5' 2/17/87)
S7-02-076-06	S-1 3 19-20.	5' 2/17/87	
S7-02-076-07	S-2 24-25.5		600:
	Fill Box	e a company to the first	410: 15 (1982)
	•	Detection Limit	2.

TABLE 4

SOIL ANALYTICAL DATA FORMER USA STATION #57 10700 MacARTHUR BOULEVARD OAKLAND, CALIFORNIA

Well ID	Date	Depth (feet)	TPH G (ppm)	ТРН D (ррт)	Benzene (ppm)	Toluene (ppm)	Ethyl- benzene (ppm)	Total Xylene (ppm)
S-1	02/12/87	20.5 20.5	42 16	-	-	-		-
S-2	02/12/87	24.5	600	_	-			
B-1	02/28/95	5.5 9.5 13.0 20.0 25.0 31.0 35.0 40.5	ND 44 540 ND 3.9 ND ND ND	- 55 - - - ND	ND 0.12 2.6 0.012 0.048 ND 0.014 ND	ND ND 10 0.016 0.14 0.011 0.018 ND	ND 0.14 7.5 ND 0.062 0.0057 0.012 ND	ND 0.4 48 0.029 0.37 0.045 0.079 ND
B-2	03/01/95	5.0 10.5 16.0 21.0 26.0	ND ND 16 110 240		ND ND 0.057 0.96 0.76	ND ND 0.028 0.41 1.4	ND ND 0.029 0.33 0.85	ND ND 1.2 1.5 1.9
B-3	03/01/95	11.0 15.5 20.5	ND 10 15	1.3	ND 0.044 0.041	ND 0.11 0.37	ND 0.079 0.15	ND 0.63 1.1
B-4	03/02/95	3.0 6.0 12.0	ND ND ND	- ND	ND ND ND	ND ND ND	ND ND ND	ND ND ND
B-5	03/02/95	5.5 12.0	ND ND	- ND	ND ND	ND ND	ND ND	ND ND
B-6	03/02/95	4.0 5.5 12.0	33 2.6 ND	5.3	0.093 0.062 ND	0.065 ND ND	0.33 0.030 ND	2.0 0.047 0.022

TABLE 4 (Continued)

SOIL ANALYTICAL DATA FORMER USA STATION #57 10700 MacARTHUR BOULEVARD OAKLAND, CALIFORNIA

.Well (D	Date	Depth (feet)	TPÀ G (ppm)	TPH D (ppm)	Benzene (ppm)	Toluene (ppm)	Ethyl- benzene (ppm)	Total Xylene (ppm)
В-7	03/02/95	3.5 5.0 12.0	ND ND ND	ND - -	ND ND ND	ND ND ND	ND ND ND	ND ND ND
B-8	03/02/95	3.0 5.5 12.0	17 ND 2.0	ND -	0.012 0.019 0.042	0.021 ND ND	0.12 0.050 ND	0.16 ND 0.016
MW-3	02/28/95	5.5 11.5 13.5 15.5 21.5 24.5 29.5 39.5	ND 1.9 240 110 3.0 ND ND ND	- 12 - - - -	ND 0.026 0.41 0.37 0.26 0.030 ND ND	ND 0.011 0.64 3.8 0.24 0.0069 0.0054 ND	ND 0.0061 2.0 1.5 0.059 0.0056 ND ND	ND 0.019 5.4 10 0.50 0.016 0.0092 ND
MW-4	11/21/95	10.0	ND	5.0	ND	ND	ND	ND
MW-5	11/21/95	10.0 15.0	ND ND	5.2 4.2	ND ND	ND ND	ND ND	ND ND
MW-6	11/21/ 9 5	10.0	ND	4.4	ND	ND	ND	ND
MW-7	11/21/95	10.0 15.0 20.0	ND ND 25	4.7 4.3 8.7	ND ND 0.071	ND ND 0.11	ND ND 0.043	ND ND 0.1
MW-8	11/21/95	10.0 15.0 20.0	ND ND ND	5.5 5.1 4.5	ND ND ND	ND ND ND	ND ND ND	ND ND ND

TPH G

Total petroleum hydrocarbons in the gasoline range

TPH D

Total petroleum hydrocarbons in the diesel range

ppm

Parts per million

ND

Not detected at the method detection limit

Not measured/not analyzed

Boring locations are presented in Alton Geo Sciences' "Supplementary Site Assessment Report" which are included in Appendix C.

TABLE 5

SOIL ANALYTICAL DATA - TANK REMOVAL FORMER USA STATION #57 10700 MacARTHUR BOULEVARD OAKLAND, CALIFORNIA

CAMBO SERVICES	elajos krativaj d	100 min - 100 min	Magaziner (F	新国际部分部	W250.50				T 11	TTLC
Sample	Sample ID	Date	Depth 🐺	TPH.G	-TPH D	Benzene	Toluene	Ethyl- benzene	Total Xylene	Lead
Location		7 P 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7			(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(mgg)
		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	(feet)	(ppm)	(PPIII)		rough the second		T PASSAGE	
an digestale erestina di se	and a signature a promise meaning				>15×12×12	71D10 005)	ND(0.005)	NID(0.005)	ND(0.005)	7
Product	PI-E-3.5	07/19/94	3.5	ND(0.2)	ND(1.0)	ND(0.005) ND(1.0)	6	60	440	4
Trench	PI-2	07/19/94	3.5	4,500	ND(50)	ND(0.005)	ND(0.005)			ŝ
	PI-3	07/19/94	3.5	ND(0.2)	ND(1.0)	ND(0.005)	ND(0.005)	ND(0.005)	ND(0.005)	6
	Pi-4	07/19/94	4	ND(0.2)	ND(1.0) ND(1.0)	ND(0.005)	ND(0.005)	ND(0.005)	ND(0.005)	7
	PI-5	07/19/94 09/19/94	3.5 9	ND(1.0)	110(1.0)	0.02	0.04	0.07	0.19	
	PI2-0	09/19/94	, , , ,	15						-
Tank Field	TP1	07/19/94	12.5	-	60	ND(0.005)	0.015	0.007	0.008	-
I MIK I ICIG	TP2	07/19/94	12.5	-	230	ND(1.0)	0.79	2.2	0.7	-
	TP3	07/19/94	13	94	-	0.18	0.25	1	5.9	3
	TP4	07/19/94	13	1400	-	1.9	3.5	12	150	4
	TP5	07/19/94	13	300	-	ND(0.5)	0.74	4.8	20	3
	TP6	07/19/94	13	0.7	-	ND(0.005)	ND(0.005)		ND(0.005)	3
	TP7	07/19/94	13	ND(0.2)	-	ND(0.005)	ND(0.005)	ND(0.005)	MD(0:003)	3 .
	ma 1	00/10/04	16	ND(0.2)		ND(0.005)	ND(0.005)	ND(0.005)	ND(0.005)	-
Tank Cavity	TC-1	08/19/94 08/19/94	16	93	_	ND(1.0)	0.28	0.63	3.1	
	TC-2		17.5	2.4	l	0.008	0.02	0.02	0.11	-
	TC-3	08/19/94 08/19/94	17.5	0.7	2	ND(0.005)	5	ND(0.005)	ND(0.005)	-
	TC-4	08/19/94	17.5	190	1 [0.17	0.38	0.99	7.9	-
	TC-5 TC-6	08/19/94	18	ND(0.2)	_	ND(0.005)	ND(0.005)	ND(0.005)	ND(0.005)	
	SM-1	08/19/94	19.5	0.4		ND(0.005)	ND(0.005)	ND(0.005)	ND(0.005)	-
	TC2-1	09/27/94	417 17	ND(0.2)		ND(0.005)	ND(0.005)	ND(0.005)	ND(0.005)	
	TC2-1	09/27/94	13	13	1 -	0.06	0.019	0.026	ND(0.005)	-
	TC2-3	09/27/94	16	ND(0.2)	_	ND(0.005)	ND(0.005)	ND(0.005)	ND(0.005)	-
	TC2-4	09/27/94	13	ND(0.2)	-	ND(0.005)	ND(0.005)	ND(0.005)		-
	TC2-5	09/27/94	12	100	200	0.13	0.12	0.1	0.26	
	TC2-7	09/27/94	13	6.3	37	ND(0.005)	ND(0.005)	ND(0.005)	ND(0.005)	-
	TC2-8	09/27/94	13	ND(1.0)	16	ND(0.005)	ND(0.005)	ND(0.005)	ND(0.005)	-
	TC2-9	09/27/94	19	0.4	-	ND(0.005)		ND(0.005)		-
	TC2-11	09/27/94	13	2200	-	9.6	21	40	260	-
	TC2-12	09/27/94	12	130	-	0.33	0.29	0.66	7.9	-
	TC2-13	09/27/94	20	620	-	1.1	4.9	6.4	66	-
	TC2-14	09/27/94	11	92		0.096	0.1	0.17	1.7	-
	TC2-15	09/27/94	17	ND(0.2)	-	ND(0.005)	ND(0.005)	ND(0.005	ND(0.005] -
	TC2-16	09/27/94	14	ND(1.0)	-	ND(0.005)	ND(0.005)	(כטט.ט)מאן	כטט.ט)עאן(, -
(Alton	l l	10/94	12-13	300	330	-	-	_	-	1 -
(Alton	′ 1	10/94	12-13	510	ND	-	-	-	-	1 -
(Alton	· I	10/94	12-13	2400	ND	-	-	-	-	-
(Alton		10/94	12-13	940	ND_	 - -		+		
Diagona	DIT	09/27/94	3.5	720	_	0.19	2	9	53	-
Dispenser	DI-1 DI-2	09/27/94	3.5	280	-	0.12	0.8	4.6	33	-
Island	DI-3	09/27/94	3.3	ND(0.2)	_	ND(0.005	i	ND(0.005)ND(0.005) -
	DI-4	09/27/94	3	590	-	0.7	2.5	13	81	
	DI-5	09/27/94		570	-	0.1	1.5	2.7	17	-
	DI-6	09/27/94		1800	-	0.72	5.2	31	180	

SOIL SAMPLES BY WESTERN GEO-ENGINEERS UNLESS OTHERWISE NOTED

Total petroleum hydrocarbons in the gasoline range TPH G

Total petroleum hydrocarbons in the diesel range TPH D

Parts per million ppm

Not detected at the method detection limit ND

Not measured/not analyzed

WEGE: TABLE 1

USA PETROLEUM CORPORATION 10700 MACARIMUR BLVD., CAMLAND, CALIPORNIA

SOIL SAMPLE LABORATORY RESULTS

SAMPLE	SAMPLE	E DATE	. Ubara . Ubara	Sampling					*********	P#110							
LOCATION	ald)	SAMPLED			LAB	TPH.G	TPH,D	BENZENS	LOTHENS	ETHYL	XYLENB	TILC	STLO		PNA's	VOL .ORGAN	1.00
		Draw LLD	IN FEET	COMPANY			Dom	Ppm.	ppm	BENZENB	ppu ppu	LEAD	LEXE) E	y M8270	by 8240	a single
*******			TW PEET	er er er er er						ppm		ЪЪш	PPM	-1	ppm	** ppm	
	2 - 1				~ .							*******					Sept. 2 control
P_L TRNCHI	PI-E 3.5	07/19/94	3.5	WEGE	AEN	<0.2	<1.0	<.005	<.005						e		
P_L TRNCH	PI-2	07/19/94	3.5	WEGE	AEN	4500	<50	<1.0	6	<.005	<.005	7,					
P_L TRNCH	PI-3	07/19/94	3.5	WEGE	AEN	<0.2	<1.0	<.005	<.005	60	440	4	4		****		42.7
P_L TRNCH	PI-4	07/19/94	4	WEGE	AEN	<0.2	<1.0	< 005	<.005	<.005	<.005	5		-	*	1 - 1	EVEN ALL
P_L TRNCH	PI-S	07/19/94	3.5	WEGE	AEN	<1.0	<1.0	<.005	<.005	<.005	< .005	6			**,*	, S	Ÿ
								1.003	2.003	<.D05	<.005	7					
TMK FIELD	TP1	07/19/94	12.5	WEGE	AÉN		60	<.005	0.015						+ 5		
TNK FIELD	TP2	03/19/94	12.5	WEGE	AEN		230	<1.0	0.013	0.007	0.008				<0.2	+ 12 - 1-1	
TNK FIELD	TP3	07/19/94	13 .	WEGE	AEN	94		0.18	0.25	2.2	0.7.	1		: - : *	.0,77.	כוא	Professional
TNK FIELD	TP4	07/19/94	13	WEGE	AEN	1400		1.9		1	5.9	3					
THE FIELD	TPS	\$7/19/94	13	WEGE	AEN	300		* 5	3.5	12	150	4 .			- 2	satisficances.	ate de la
TNK FIELD	TF6	07/19/94	13	WEGE	AEI	0.7		<.005	0.74	4.8	20	3			S - 2	ND.	1 1 1
INK FIELD	TP7	27/19/94	13	WEGE	AEN	<0.2		<.005	<.005	0.006	<.005,	3		*	12	14 5 2 11 1	·
								2.003	<.005	< .005	<.005	3				ş#s (+4s −1	
TAX CAVIY	TC-1	08/19/94	16	WEGE	AEN	<0.2		<.Q05									
TRIK CAVTY	TC-2	28/19/94	16	WEGE	AZN	93		<0.01	<.005	<.065	<.005				**.	14 17 1	
TMK CAVIY	TC-3	28/19/94	17.5	WEGE	AEN	2.4	1	0.008	0.28	0.63	3.1				-	,	* -, *
THE CAVITY	TC-4 :	08/19/94	15.5	WEGE	AEN	0,7	2		0.02	0.02	0.11				1 1 -		5.04
TNK CAVTY	TC-S	C6/19/94	17	WEGE	AEN	190	•	<.005	<.005	<.005	<.005					• . •	
TNK CAVTY	TC-6	28/19/94	18	WEGE	AEN	<0.2		0.17	0,38	0.99	7.9						
TNK CAVTY	SM-1 (5/18/94	19.5	WEGE	AEN	C.4	*	<.005	<.005	< .005	< 005				5-		
					10			< .005	< .005	<.005				1.5	٠.	Jan Barrier and A	N. 37.
THE CAVITY :	TC2-1 .6	9/27/94	17	WEGE	AEN	40.2				5.1	5.27		ž		-10-5	1.5	* . • .*
INK CAVIY	rcz-z a	19/27/94	13	WEGE	AEN 370	13	1	<.005	<.005	<.005	<.005		•	٠.		1 1	ster 1 🕟 🔻
THE CAVITY 1	TC2-3 0	9/27/94	16	WEGE	AEN	<0.2		0.06	0.019	0.026	. < -005					•	
INK CAVIY 1	rcz-4 a	9/27/94	13	WEGE	AEN		1.0	9.	₹.005	<.005	. c . 005				1.23	1 1 1 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 3 2 1 1 Tab
DOX CAVIY 7	FC2-5 0	9/27/94	12	WEGE	AEN	100	***	<.005	<.005	<.005	<.005						
THE CAVITY T	C2-7 0	9/27/94		NEGE	AEN		200		0.12	0.1	0.25				·		97. T
NK CAVTY I		9/27/94		WEGE	AEN		37		∢.005	<.005	<.005		•			100	4.7
THE CAVITY I	C2-9 6:	9/27/94		WEGE	AEN		16		<.005	<-005	<.005	-				5	100
NK CAVIY TO	2-11 0	9/27/94			AEN	0.4 2200	*		<.005	< . 005	<.005 / L				-4, 1	1 14 1	13.57
NK CAVTY TO					AEN	130		9.6	21	40	260 :					V	
NK CAVTY TO					AEN	620				D.66	7.9						
MK CAVIY IC					AEN	92		1.1	4.9	6.4	66						
NK CAVTY TO						<0.2		0.096			.1.7				(·	8	*
NK CAVTY TO						<1.0					<.005				530,00		-
			•			<1.0		<.00S -	<.005	≺.005	<.005						.*
SP ISL D	I-I ÇB	/19/94	3.5 9	(EGE	Aen	720				. *	5						1.5
ESP ISL DI	[-2 ¢s	/19/94			AEN			0.19	2	9	53				1	3.1	
CSP ISL DI	-3 08	/19/94				280		0.12	0.8	4.6	33 .	•		."			
				'		<0.2		<.005	.00\$.005	c.005				3		

APPENDIX D

HISTORICAL GROUNDWATER ELEVATION AND ANALYTICAL DATA

GROUNDWATER ELEVATION AND ANALYTICAL SUMMARY
Former USA Service Station No. 57

Former USA Service Station No. 57 10700 MacArthur Blvd., Oakland, California

Well Number	Date Collected	Depth to Water (feet)	Well Elevation (ft msl)	Groundwater Elevation (ft msl)	TPHG (μg/L)	Τ ΡΉD (μg/L)	Benzene (μg/L)	Toluene (μg/L)	Ethylbenzene (µg/L)	Total Xylenes (µg/L)	MTBE (µg/L)
C 1	02/12/87						630	4.4	3.5	37	NA
S-1	03/03/95	13.10	74.74	61.64	910	5,900	260	7.6	16	14	NA
	03/03/93	12.35	/4./4	62.39	NA	NA	NA	NA	NA	NA	NA
	11/22/95	19.30	78.68	59.38	460	6,100	13	0.69	0.99	1.1	460*
	12/06/95	19.59	76.00	59.09	NA	NA	NA	NA	NA	NA	NA
	01/04/96	19.52		59.16	NA	NA	NA	NA	NA	NA	NA
	01/04/90	15.07		63.61	1,100	200	11	6	3	6	200*
	10/10/97	18.90		59.78	530	2,000	<0.5	2.1	<0.5	<2	230*
		16.79		61.89	1,800	2,000	<0.5	<0.5	1.5	10	87*
	01/20/98				-						
	04/28/98	8.37		70.31	130	7,300	1.9	3.2	<0.5	<0.5	310* 280*
	07/31/98	11.61		67.07	310	2,000	0.54	4.6	3.8	0.82	
	06/10/99	14.35		64.33	660	150	0.99	< 0.5	<0.5	2.4	80*[1]
	10/18/00	17.56		61.12	< 50	330	< 0.5	0.93	< 0.5	< 0.5	44
	03/12/02	16.29		62.39	500	< 50	2.8	4.8	0.79	4.4	63
	11/19/02	19.53		59.15	190	NA	< 0.50	< 0.50	< 0.50	< 0.50	190
	01/09/03	18.14		60.54	510	NA	1.1	< 0.50	0.52	< 0.50	11
	04/14/03	18.04		60.64	300	NA	<1.0[2]	<1.0[2]	<1.0[2]	<1.0[2]	27
	07/21/03	20.31		58.37	300	NA	< 0.50	< 0.50	< 0.50	< 0.50	11
	10/09/03	19.46		59.22	390	NA	< 0.50	< 0.50	< 0.50	< 0.50	8.8
	01/15/04	18.21	79.66	61.45	200	NA	< 0.50	< 0.50	< 0.50	< 0.50	6.0
	04/08/04	19.29		60.37	140	NA	< 0.50	< 0.50	< 0.50	< 0.50	12
	08/10/04	18.86		60.80	110	NA	4.6	< 0.50	< 0.50	0.51	73
	11/11/04	19.81		59.85	160	NA	< 0.50	< 0.50	< 0.50	< 0.50	150
	01/19/05	18.12		61.54	440	NA	< 0.50	< 0.50	1.4	< 0.50	140

TABLE 1

GROUNDWATER ELEVATION AND ANALYTICAL SUMMARY
Former USA Service Station No. 57

Well Number	Date Collected	Depth to Water (feet)	Well Elevation (ft msl)	Groundwater Elevation (ft msl)	TPHG (μg/L)	TPHD (μg/L)	Benzene (μg/L)	Toluene (μg/L)	Ethylbenzene (µg/L)	Total Xylenes (μg/L)	MTBE (μg/L)
MW-3	03/03/95	13.99	76.30	62.31	2,500	1,600	540	92	36	200	NA
	07/24/95	13.33		62.97	NA	NA	NA	NA	NA	NA	NA
	11/22/95	20.94	80.32	59.38	14,000	5,400	5,700	230	430	650	820*
	12/06/95	17.48		62.84	NA	NA	NA	NA	ΝA	NA	NA
	01/04/96	20.01		60.31	NA	NA	NA	NA	NA	NA	NA
	01/31/97	16.63		63.69	1,100	<50	130	8	5	5	NA
	10/10/97	20.62		59.70	3,400	1,100	830	4	100	<10	160*
	01/20/98	15.40		64.92	3,900	550	7.9	4.1	< 0.5	3.7	<5.0*
	04/28/98	10.51		69.81	800	1,000	82	5.2	5.7	5.4	240*
	07/31/98	13.46		66.86	2,200	610	510	7.6	16	5.27	310*
	11/02/98	17.11		63.21	4,900	1,600	220	16	13	13.7	180*
	06/10/99	15.24		65.08	1,000	120	< 0.5	< 0.5	< 0.5	1.1	120*[1]
	10/18/00	15.41		64.91	<50	<50	< 0.5	< 0.5	< 0.5	< 0.5	12
	04/08/04	13.70		66.62	<50	NA	< 0.50	< 0.50	< 0.50	< 0.50	19
	08/10/04	16.96		63.36	580	NA	19	<1.0[3]	<1.0[3]	3.3	300
	11/11/04	17.40		62.92	3,000	NA	810	<5.0[3]	43	<5.0[3]	690
	01/19/05	13.28		67.04	92	NA	18	< 0.50	0.77	< 0.50	17

GROUNDWATER ELEVATION AND ANALYTICAL SUMMARY
Former USA Service Station No. 57

Well	Date	Depth to Water	Well Elevation	Groundwater Elevation	ТРНС	TPHD	Benzene	Toluene	Ethylbenzene	Total Xylenes	MTBE
Number	Collected	(feet)	(ft msl)	(ft msl)	(μg/L)	(μg/L)	(μg/L)	(μg/L)	(μg/L)	(μg/L)	(µg/L)
		· -		•							
MW-4	11/22/95	14.99	76.42	61.43	<50	200	<0.5	1.5	< 0.5	1.7	6.4*
	12/06/95	11.21		65.21	NA	NA	NA	NA	NA	NA	NA
	01/04/96	14.62		61.80	NA	NA	NA	NA	NA	NA	NA
	01/31/97	8.18		68.24	< 50	< 50	< 0.5	2	< 0.5	2	11*
· :	10/10/97	14.14		62.28	<50	<50	< 0.5	< 0.5	< 0.5	<2	<5.0*
	01/20/98	7.05		69.37	<50	< 50	< 0.5	< 0.5	< 0.5	< 0.5	<5.0*
	04/28/98	5.88		70.54	<50	< 50	< 0.5	< 0.5	< 0.5	< 0.5	<5.0*
	07/31/98	8.40		68.02	<50	< 50	< 0.5	< 0.5	< 0.5	< 0.5	<5.0*
	11/02/98	16.08		60.34	NA	NA	NA	NA	NA	NA	NA
	06/10/99	14.81		61.61	NA	NA	NA	NA	NA	NA	NA
	10/18/00	12.71		63.71	<50	<50	< 0.5	0.59	0.82	0.53	<5.0*
	03/12/02	8.92		67.50	< 50	< 50	< 0.5	0.61	0.72	2.5	1.8
	11/19/02	13.24		-13.24	<50	NA	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50
	01/09/03	11.00		-11.00	<50	NA	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50
	04/14/03	11.03		-11.03	<50	NA	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50
	07/21/03	13.10		-13.10	<50	NA	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50
	10/09/03	13.33		-13.33	<50	NA	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50
	01/15/04	12.14		-12.14	<50	NA	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50
	04/08/04	10.76		65.66	<50	NA	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50
	08/10/04	12.62		63.80	<50	NA	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50
	11/11/04	11.93		64.49	<50	NA	< 0.50	< 0.50	<0.50	< 0.50	< 0.50
	01/19/05	10.34		66.08	<50	NA	< 0.50	< 0.50	<0.50	<0.50	<0.50

TABLE 1

GROUNDWATER ELEVATION AND ANALYTICAL SUMMARY

Well Number	Date Collected	Depth to Water (feet)	Well Elevation (ft msl)	Groundwater Elevation (ft msl)	TPHG (μg/L)	TPHD (μg/L)	Benzene (μg/L)	Toluene (µg/L)	Ethylbenzene (µg/L)	Total Xylenes (µg/L)	MTBE (μg/L)
MW-5	11/22/95	19.56	80.52	60.96	<50	280	<0.5	1.8	<0.5	3	2.2*
112 17 5	12/06/95	15.84	00.52	64.68	NA	NA	NA	NA	NA	NA	NA
	01/04/96	19.36		61.16	NA	NA	NA	NA	NA	NA	NA
	01/31/97	13.31		67.21	80	<50	< 0.5	0.6	< 0.5	2	6*
	10/10/97	17.80		62.72	< 50	<50	< 0.5	< 0.5	< 0.5	<2	<5*
	01/20/98	12.58		67.94	<50	<50	< 0.5	< 0.5	< 0.5	< 0.5	<5.0*
	04/28/98	9.45		71.07	< 50	<50	< 0.5	<0.5	< 0.5	< 0.5	<5.0*
	07/31/98	7.38		73.14	<50	<50	< 0.5	<0.5	< 0.5	<0.5	<5.0*
	11/02/98	15.98		64.54	< 50	<500	< 0.5	<0.5	< 0.5	< 0.5	<5.0*
	06/10/99	14.60		65.92	NA	NA	NA	NA	NA	NA	NA
	10/18/00	17.77		62.75	< 50	< 50	< 0.5	0.75	<0.5	0.79	28
	03/12/02	15.72		64.80	<50	< 50	< 0.5	< 0.5	<0.5	< 0.5	<5.0*
•	11/19/02	NM		NM				Well Dam	aged		
	01/09/03	NM		NM				Well Dam	aged		
	04/14/03	NM		NM				Well Dam	aged		
	07/21/03	NM		NM				Well Dam	aged		
	10/09/03	NM		NM				Well Dam	aged		
ļ	01/15/04	NM		NM				Well Dam	aged		
	04/08/04	16.80		63.72	<100	NA	< 0.50	< 0.50	<0.50	< 0.50	< 0.50
	08/10/04	18.58		61.94	89	NA	< 0.50	< 0.50	< 0.50	<0.50	< 0.50
	11/11/04	NM		NM				Well Dam	aged		
	01/19/05	NM		NM				Well Dam	aged		

GROUNDWATER ELEVATION AND ANALYTICAL SUMMARY

TABLE 1

Well Number	Date Collected	Depth to Water (feet)	Well Elevation (ft msl)	Groundwater Elevation (ft msl)	TPHG (μg/L)	TPHD (μg/L)	Benzene (µg/L)	Toluene (μg/L)	Ethylbenzene (µg/L)	Total Xylenes (µg/L)	MTBE (μg/L)
	44155/05			50.01		1.40	40 E		-0.5	1.5	£ 2*
MW-6	11/22/95	21.73	81.64	59.91	<50	140	< 0.5	1.2	<0.5	1.5	5.3*
	12/06/95	18.03		63.61	NA	NA	NA	NA	NA	NA	NA
	01/04/96	21.67		59.97	NA	NA	NA	NA	NA	NA	NA
	01/31/97	16.01		65.63	70	<50	< 0.5	2	<0.5	<1	5*
	10/10/97	20.55		61.09	80	<50	< 0.5	< 0.5	< 0.5	<2	<5*
	01/20/98	15.74		65.90	<50	<50	< 0.5	< 0.5	<0.5	<0.5	<5.0*
	04/28/98	10.78		70.86	<50	<50	< 0.5	< 0.5	<0.5	<0.5	<5.0*
	07/31/98	13.97		67.67	<50	<50	< 0.5	< 0.5	< 0.5	<0.5	<5.0*
	11/02/98	17.97		63.67	NA	NA	NA	NA	NA	NA	NA
	06/10/99	16.92		64.72	NA	NA	NA	NA	NA	NA	NA
	10/18/00	NM		ΝM				Unable to I	ocate		
	03/12/02	NM		NM				Unable to I	ocate		
	11/19/02	NM		NM				Unable to I	ocate		
	01/09/03	NM		NM				Unable to I	ocate.		
	04/14/03	NM		NM				Unable to I	ocate.		
	07/21/03	NM		NM				Unable to I	ocate		
	10/19/03	NM		NM				Unable to I	ocate		
	01/15/04	NM		NM				Unable to I	ocate		
	04/08/04	NM		NM					Not Sampled		
	08/10/04	NM		NM				Ory - Not Sa	=		
	11/11/04	17.20		64.44				Dry - Not Sa	-		
	01/19/05	NM		NM				Dry - Not Sa			

TABLE 1

GROUNDWATER ELEVATION AND ANALYTICAL SUMMARY

33 711	D-4-	Depth to	Well	Groundwater	TDUC	TRITE	**			Total	
Well	Date	Water	Elevation	Elevation	TPHG	TPHD	Benzene	Toluene	Ethylbenzene	Xylenes	MTBE
Number	Collected	(feet)	(ft msl)	(ft msl)	(μg/L)	(µg/L)	(μg/L)	(μg/L)	(μg/L)	(μg/L)	(μg/L)
MW-7	11/22/95	19.38	78.86	59.48	<50	180	<0.5	0.57	<0.5	0.62	0.73*
	12/06/95	19.72		59.14	NA	NA	NA	NA	NA	NA	NA
	01/04/96	19.76		59.10	NA	NA	NA	NA	NA	NA	NA
	01/31/97	15.25		63.61	70	<50	0.7	1	<0.5	<1	8*
	10/10/97	19.03		59.83	< 50	<50	< 0.5	< 0.5	<0.5	<2	15*
	01/20/98	17.11		61.75	<50	<50	< 0.5	<0.5	<0.5	<0.5	<5.0*
	04/28/98	8.22		70.64	<50	<50	< 0.5	< 0.5	<0.5	<0.5	9.3*
	07/31/98	11.53		67.33	<50	< 50	< 0.5	< 0.5	< 0.5	<0.5	<5.0*
	11/02/98	15.15		63.71	NA	NA	NA	NA	NA	NA	NA
	06/10/99	14.23		64.63	NA	NA	NA	NA	NA	NA	NA
	10/18/00	17.59		61.27	NA	<50	< 0.5	< 0.5	< 0.5	< 0.5	<5.0*
	03/12/02	16.54		62.32	< 50	< 50	< 0.5	< 0.5	< 0.5	< 0.5	2.9
	11/19/02	19.59		-19.59	< 50	NA	< 0.50	< 0.50	< 0.50	< 0.50	3.8
	01/09/03	18.38		-18.38	<50	NA	< 0.50	< 0.50	< 0.50	< 0.50	2.7
	04/14/03	18.17		-18.17	<50	NA	< 0.50	< 0.50	< 0.50	<0.50	< 0.50
	07/21/03	20.29		-20.29	<50	NA	< 0.50	< 0.50	< 0.50	< 0.50	1.8
	10/09/03	19.48		-19.48	<50	NA	< 0.50	< 0.50	< 0.50	< 0.50	2.9
	01/15/04	18.45	79.81	61.36	<50	NA	< 0.50	< 0.50	< 0.50	<0.50	2.6
	04/08/04	17.28		62.53	<50	NA	< 0.50	< 0.50	< 0.50	< 0.50	0.81
	08/10/04	18.85		60.96	<50	NA	< 0.50	< 0.50	< 0.50	< 0.50	2.1
	11/11/04	19.85		59.96	<50	NA	< 0.50	< 0.50	< 0.50	< 0.50	1.0
	01/19/05	19.59		60.22	<50	NA	< 0.50	< 0.50	< 0.50	< 0.50	1.5

TABLE 1
GROUNDWATER ELEVATION AND ANALYTICAL SUMMARY

		Depth to	Well	Groundwater						Total	
Well	Date	Water	Elevation	Elevation	TPHG	TPHD	Benzene	Toluene	Ethylbenzene	Xylenes	MTBE
Number	Collected	(feet)	(ft msl)	(ft msl)	(μg/L)	(µg/L)	(μg/L)	(µg/L)	(μg/L)	(µg/L)	(μg/L)
MW-8	11/22/95	33.33	79.55	46.22	<50	360	<0.5	1.3	<0.5	2.1	2.1*
17177	12/06/95	17.57	,,,,,,	61.98	NA	NA	NA	NA	NA	NA	NA
	01/04/96	20.08		59.47	NA	NA	NA	NA	NA	NA	NA
	01/31/97	18.72		60.83	80	<50	0.6	1	< 0.5	1	8*
	10/10/97	20.26		59.29	50	<50	< 0.5	< 0.5	<0.5	<2	<5*
	01/20/98	15.91		63.64	<50	<50	< 0.5	< 0.5	<0.5	< 0.5	<5.0*
	04/28/98	10.39		69.16	<50	<50	< 0.5	< 0.5	<0.5	<0.5	<5.0*
	07/31/98	12.93		66.62	<50	<50	< 0.5	< 0.5	<0.5	< 0.5	<5.0*
1	11/02/98	16.90		62.65	<50	<500	< 0.5	< 0.5	< 0.5	< 0.5	<5.0*
	06/10/99	14.98		64.57	NA	NA	NA	NA	NA	NA	NA
	10/18/00	16.27		63.28	<50	<50	< 0.5	< 0.5	1.1	6.3	8.6*
	03/12/02	14.56		64.99	<50	<50	< 0.5	0.63	0.55	1.7	0.94
	11/19/02	21.14		-21.14	< 50	NA	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50
	01/09/03	17.90		-17.90	<50	NA	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50
ļ	04/14/03	17.84		-17.84	< 50	NA	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50
	07/21/03	19.79		-19.79	<100[2]	NA	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50
	10/09/03	21.02		-21.02	<50	NA	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50
	01/15/04	18.10	80.50	62.40	<50	NA	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50
1	04/08/04	17.51		62.99	<50	NA	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50
	08/10/04	20.76		59.74	<50	NA	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50
	11/11/04	21.38		59.12	<50	NA	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50
E	01/19/05	17.20		63.30	<50	NA	< 0.50	< 0.50	<0.50	< 0.50	< 0.50
	01/1//03	17.20		05.50	-50	1471				0.20	

TABLE 1

GROUNDWATER ELEVATION AND ANALYTICAL SUMMARY

Well	Date	Depth to Water	Well Elevation	Groundwater Elevation	TPHG	TPHD	Benzene	Toluene	Ethylbenzene	Total Xylenes	мтве
Number	Collected	(feet)	(ft msl)	(ft msl)	(μg/L)	(μg/L)	(μg/L)	(μg/L)	(μg/L)	(µg/L)	(μg/L)
		- 									
Note:											
* = MTBE a	nalyzed using E	PA Method 80)20/8021B						msl = Mean sea leve	el	
MTBE = Me	thyl tert-butyl e	ther							μg/L = micrograms	per liter	
TPHD = Tot	al petroleum hyd	drocarbons as	diesel								
TPHG = Tota	al petroleum hyd	drocarbons as	gasoline						NA = Not analyzed		
TPHG analya	zed using EPA N	Method 8015B	and the remain	ning analytes using E	PA Method	8260B			NM = Not measured	1	
[1] Laborato	ry indicates the	chromatogram	does not mate	h the diesel hydrocar	bon range pa	ttern.					
[2] Reporting	g limits were inc	reased due to	sample foamin	g.							
[3] Reporting	g limits were inc	reased due to	high concentra	tions of target analyt	es.						
Monitoring v	wells surveyed b	y Morrow Sur	veying on Febr	uary 10, 2004.							
Data prior to	November 19,	2002 provided	by GHH Engi	neering.							

TABLE 2

GROUNDWATER ANALYTICAL RESULTS FOR OXYGENATES AND ADDITIONAL COMPOUNDS

Well Number	Date Collected	MTBE (μg/L)	TBA (μg/L)	DIPE (μg/L)	ETBE (µg/L)	TAME (µg/L)	1,2-DCA (μg/L)	EDB (µg/L)	Methanol (µg/L)	Ethanol (μg/L)
S-1	11/19/02	190	<10	<1.0	<1.0	<1.0	214	3.7.4		
	01/09/03	11	<5.0	<1.0	<1.0	<1.0 <1.0	NA	NA	NA	NA
	04/14/03	27	<20[2]	<2.0[2]	<2.0[2]		NA	NA	NA	NA
	07/21/03	11	<10[2]	<1.0 <1.0	<1.0 <1.0	<2.0[2]	NA	NA	NA	NA
	10/09/03	8.8	6.4	<1.0 <1.0	<1.0	<1.0	NA 11.5	NA	NA	NA
	01/15/04	6.0	10	<1.0	<1.0	<1.0	<1.0	<2.0	NA	NA
	04/08/04	12	8.5	<1.0	<1.0	<1.0	<1.0	<2.0	NA	NA
	08/10/04	73	28	<1.0	<1.0	<1.0	<1.0	<2.0	<5,000	<5,000
	11/11/04	150	14	<1.0	<1.0 <1.0	<1.0	16	<2.0	<5,000	<5,000
	01/19/05	140	14	<1.0		<1.0	7.3	<2.0	<5,000	<5,000
		110	14,	>1.0	<1.0	<1.0	3.8	<2.0	<5,000	<5,000
S-2	11/19/02	750	<200[1]	<20[1]	<20[1]	<20[1]	TA T A	N1 4		
	01/09/03	270	<100[1]	<10[1]	<10[1]	<10[1]	NA NA	NA	NA.	NA
	04/14/03	400	95	<5.0[1]	<5.0[1]	<5.0[1]	NA	NA	NA	NA
	07/21/03	410	110	<5.0[1] <5.0[1]	<5.0[1] <5.0[1]		NA	NA	NA	NA
	10/09/03	180	57	<5.0[1]	<5.0[1] <5.0[1]	<5.0[1]	NA	NA	NA	NA
	01/15/04	130	48	<4.0[1]	~ *	<5.0[1]	<5.0[1]	<20[1]	NA	NA
	04/08/04	430	130	<5.0[1]	<4.0[1]	<4.0[1]	<4.0[1]	<16[1]	NA	NA
	08/10/04	92	<100[1]	<10[1]	<5.0[1]	<5.0[1]	<5.0[1]	<20[1]	<5,000	<5,000
	11/11/04	420	<200[1]	<20[1]	<10[1]	<10[1]	74	<40[1]	<5,000	<5,000
	01/19/05	580	200[1]		<20[1]	<20[1]	<20[1]	<80[1]	<5,000	<5,000
	01.15105	300	200	<5.0[1]	<5.0[1]	<5.0[1]	8.2	<20[1]	<5,000	<5,000
MW-3	04/08/04	19	7.6	<1.0	<1.0	~1.0				
	08/10/04	300	2,000	2.2		<1.0	<1.0	<2.0	<5,000	<5.000
	11/11/04	690	1,400	<10[1]	<2.0[1]	<2.0[1]	270	<8.0[1]	<5,000	<5,000
	01/19/05	17	1,400	<1.0	<10[1]	<10[1]	140	<40[1]	<5,000	<5,000
	- 27 137 03	1 /	17	~1.0	<1.0	<1.0	1.4	<2.0	<5,000	<5,000

TABLE 2

GROUNDWATER ANALYTICAL RESULTS FOR OXYGENATES AND ADDITIONAL COMPOUNDS

Well Number	Date Collected	MTBE (μg/L)	TBA (µg/L)	DIPE (µg/L)	ETBE (μg/L)	TAME (µg/L)	1,2-DCA (μg/L)	EDB (μg/L)	Methanol (μg/L)	Ethanol (μg/L)
MW-4	11/19/02	< 0.50	<5.0	<1.0	<1.0	<1.0	NA	NTA	3.1.4	214
	01/09/03	< 0.50	<5.0	<1.0	<1.0	<1.0	NA NA	NA NA	NA	NA
	04/14/03	< 0.50	<5.0	<1.0	<1.0	<1.0	NA NA	NA	NA	NA
	07/21/03	< 0.50	<5.0	<1.0	<1.0	<1.0	NA NA	NA NA	NA NA	NA NA
	10/09/03	< 0.50	<5.0	<1.0	<1.0	<1.0	<1.0	<2.0	NA NA	NA NA
	01/15/04	< 0.50	7.8	<1.0	<1.0	<1.0	<1.0	<2.0	NA.	NA NA
	04/08/04	< 0.50	<10	<1.0	<1.0	<1.0	<1.0	<2.0		
	08/10/04	< 0.50	<10	<1.0	<1.0	<1.0	<1.0		<5,000	<5,000
	11/11/04	<0.50	<10	<1.0				<2.0	<5,000	<5.000
	01/19/05	<0.50			<1.0	<1.0	<1.0	<2.0	<5,000	<5,000
	01/19/03	~0.30	<10	<1.0	<1.0	<1.0	<1.0	<2.0	<5,000	<5,000
MW-5	11/19/02 01/09/03 04/14/03 07/21/03 10/09/03 01/15/04 04/08/04	<0.50	<10	<1.0	<1.0	Well Damaged Well Damaged Well Damaged Well Damaged Well Damaged Well Damaged	<1.0	c4 0121	~5 000	
	08/10/04 11/11/04 01/19/05	<0.50	<10	<1.0	<1.0	<1.0 <1.0 Well Damaged Well Damaged	<1.0	<4.0[2] <2.0	<5,000 <5,000	<5,000 <5,000

TABLE 2

GROUNDWATER ANALYTICAL RESULTS FOR OXYGENATES AND ADDITIONAL COMPOUNDS

Well Number	Date Collected	MTBE (μg/L)	TBA (μg/L)	DIPE (μg/L)	ETBE (µg/L)	TAME (µg/L)	1,2-DCA (μg/L)	EDB (µg/L)	Methanol (μg/L)	Ethanol (μg/L)
MW-6	11/19/02				Į	Inable to Loca	te			
	01/09/03					Inable to Loca				
	04/14/03					Jnable to Loca				
	07/21/03				-	Inable to Loca				
	10/19/03					Jnable to Loca				
	01/15/04				τ	Inable to Loca	te			
	04/08/04					structed - Not				
	08/10/04					structed - Not				
	11/11/04					structed - Not				
	01/19/05					structed - Not				
MW-7	11/19/02	3.8	<5.0	<1.0	<1.0	<1.0	NA	NA	NA	NA
	01/09/03	2.7	<5.0	<1.0	<1.0	<1.0	NA	NA	NA	NA
	04/14/03	< 0.50	<5.0	<1.0	<1.0	<1.0	NA	NA	NA	NA
	07/21/03	1.8	<5.0	<1.0	<1.0	<1.0	NA	NA	NA	NA
	10/09/03	2.9	<5.0	<1.0	<1.0	<1.0	<1.0	<2.0	NA	NA
	01/15/04	2.6	7.9	<1.0	<1.0	<1.0	<1.0	<2.0	NA	NA
	04/08/04	0.81	9.0	<1.0	<1.0	<1.0	<1.0	<2.0	<5,000	<5,000
	08/10/04	2.1	<10	<1.0	<1.0	<1.0	<1.0	<2.0	<5,000	<5,000
	11/11/04	1.0	<10	<1.0	<1.0	<1.0	<1.0	<2.0	<5,000	<5,000
	01/19/05	1.5	<10	<1.0	<1.0	<1.0	<1.0	<2.0	<5,000	<5,000

TABLE 2

GROUNDWATER ANALYTICAL RESULTS FOR OXYGENATES AND ADDITIONAL COMPOUNDS

Former USA Service Station No. 57 10700 MacArthur Blvd., Oakland, California

Well Number	Date Collected	MTBE (μg/L)	TBA (μg/L)	DIPE (µg/L)	ETBE (µg/L)	TAME (μg/L)	1,2-DCA (μg/L)	EDB (μg/L)	Methanol (μg/L)	Ethanol (µg/L)
MW-8	11/19/02	< 0.50	<5.0	<1.0	<1.0	<1.0	NA	NA.	NA	NA.
	01/09/03	< 0.50	< 5.0	<1.0	<1.0	<1.0	NA	NΛ	NA	NA
	04/14/03	< 0.50	<5.0	<1.0	<1.0	<1.0	NA	NA	NA	NA
	07/21/03	< 0.50	<10[2]	<1.0	<1.0	<1.0	NA	NA	NA	NA
	10/09/03	< 0.50	<5.0	<1.0	<1.0	<1.0	<1.0	<2.0	NA	NA
	01/15/04	< 0.50	9.9	<1.0	<1.0	<1.0	<1.0	<2.0	NA	NA
	04/08/04	< 0.50	<10	<1.0	<1.0	<1.0	<1.0	<2.0	<5,000	<5,000
	08/10/04	< 0.50	<10	<1.0	<1.0	<1.0	<1.0	< 2.0	<5,000	<5,000
	11/11/04	< 0.50	<10	<1.0	<1.0	<1.0	<1.0	<2.0	<5,000	<5,000
	01/19/05	< 0.50	<10	<1.0	<1.0	<1.0	<1.0	<2.0	<5,000	<5,000

Note:

Oxygenates analyzed using EPA Method 8260B

pg/l = micrograms per liter

NA = Not analyzed

[1] Reporting limits were increased due to high concentrations of target analytes

[2] Reporting limits were increased due to sample foaming

MTBE = Methyl tertiary butyl ether

TBA = Tertiory butyl alcohol

DIPE = Di-isopropyl ether

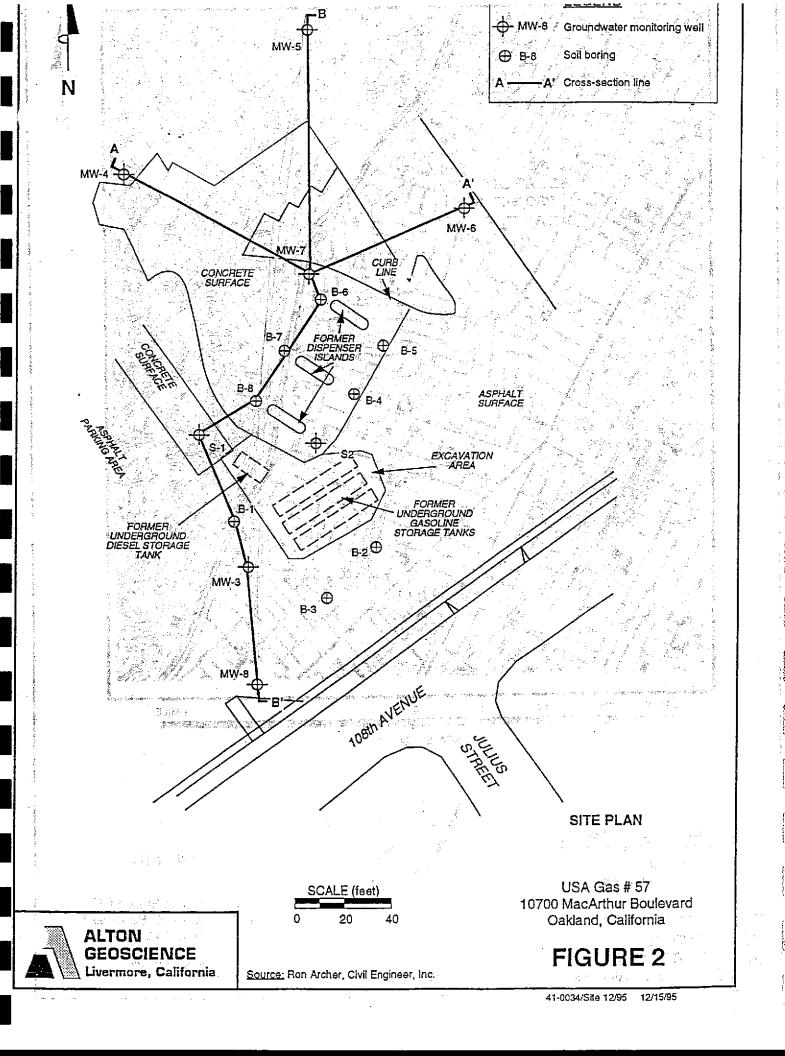
ETBE = Ethyl tertiary butyl ether

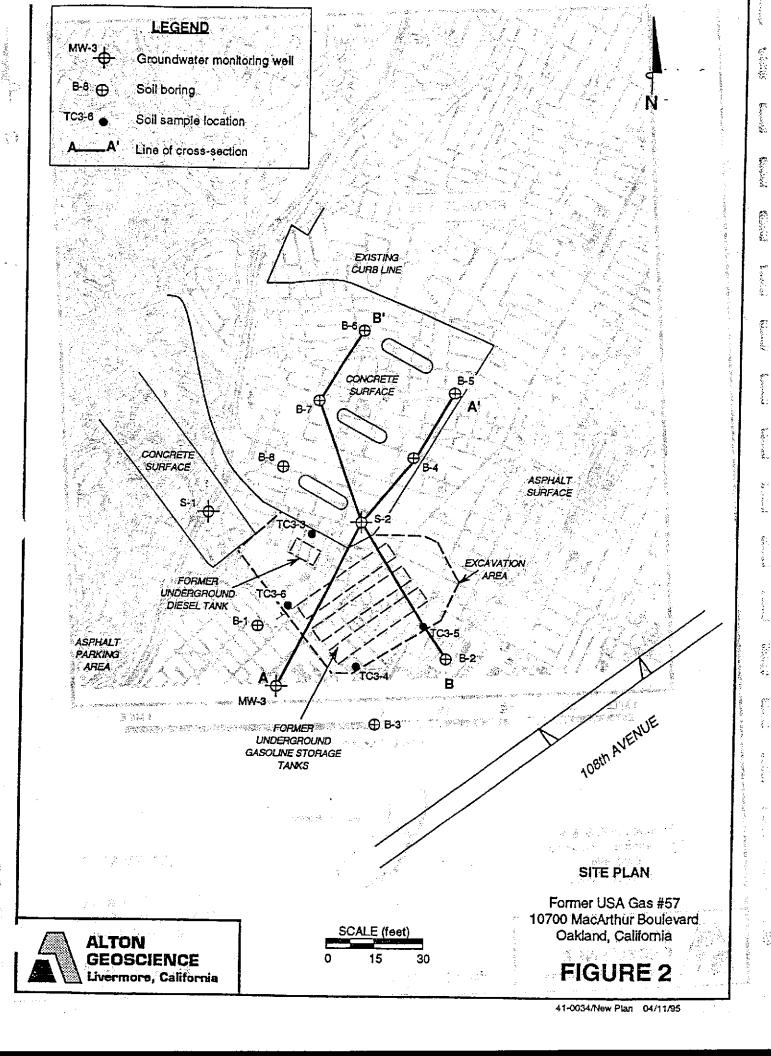
TAME = Tertiary amyl methyl other

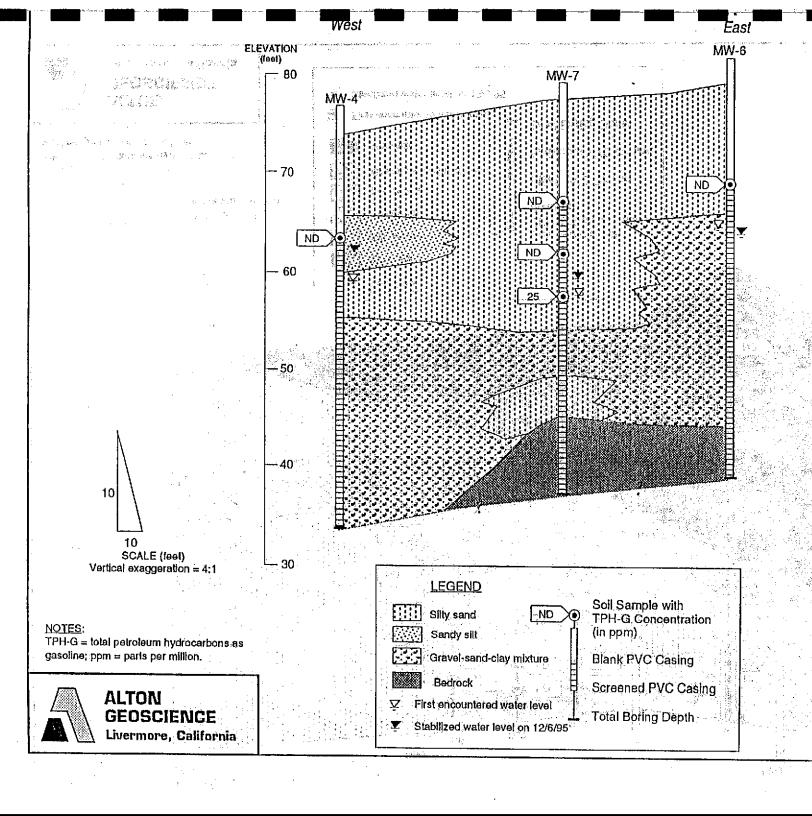
1,2-DCA = 1,2-Dichloroethane

EDB = 1,2-Dibromoethane

APPENDIX E ADDITIONAL GEOLOGIC CROSS SECTIONS





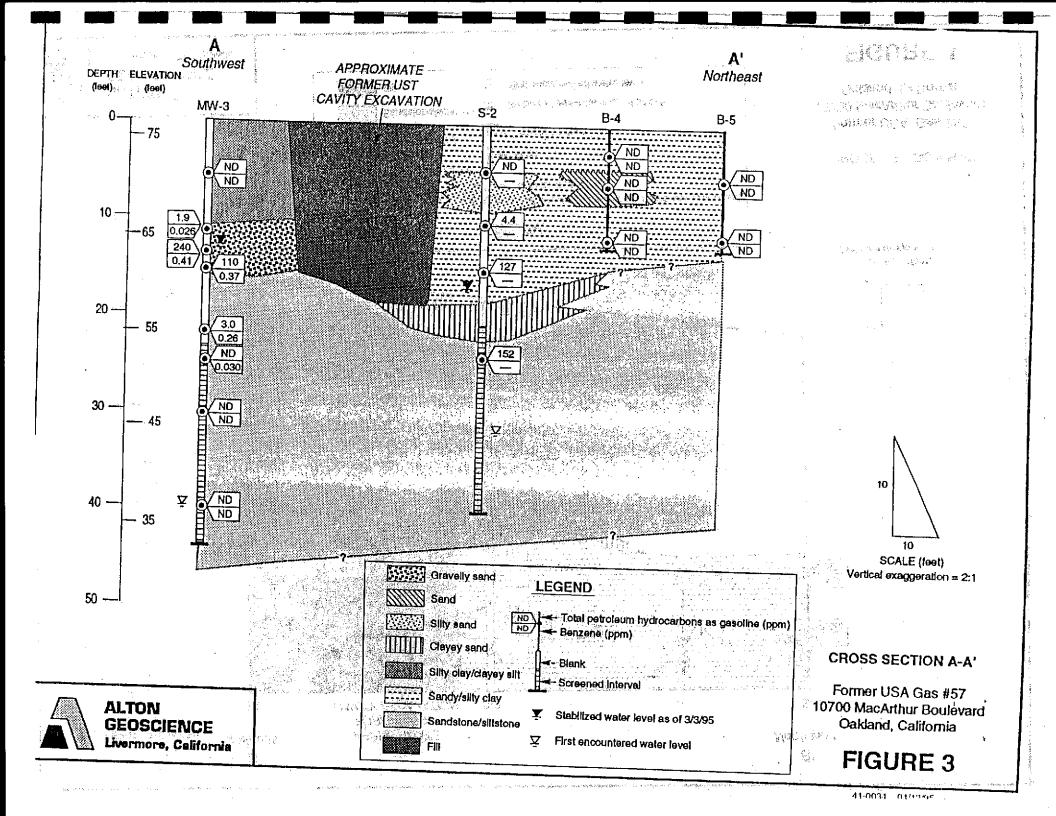


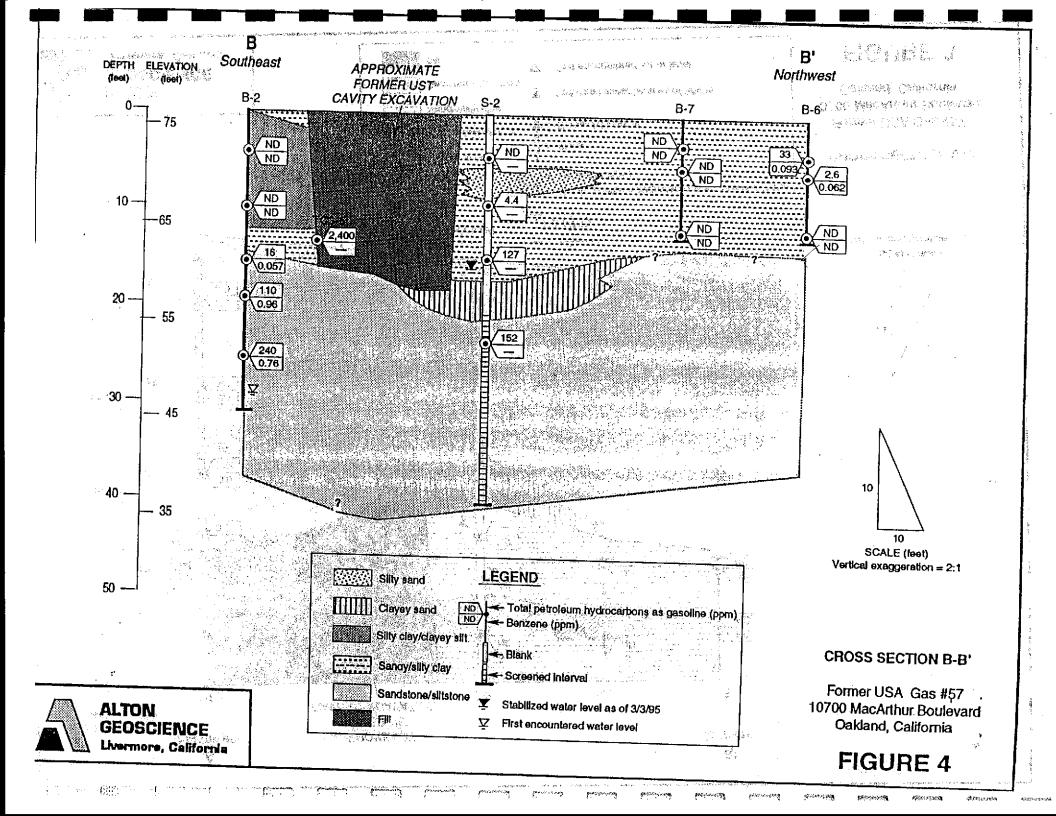
SHORE MUNICIPALITY.

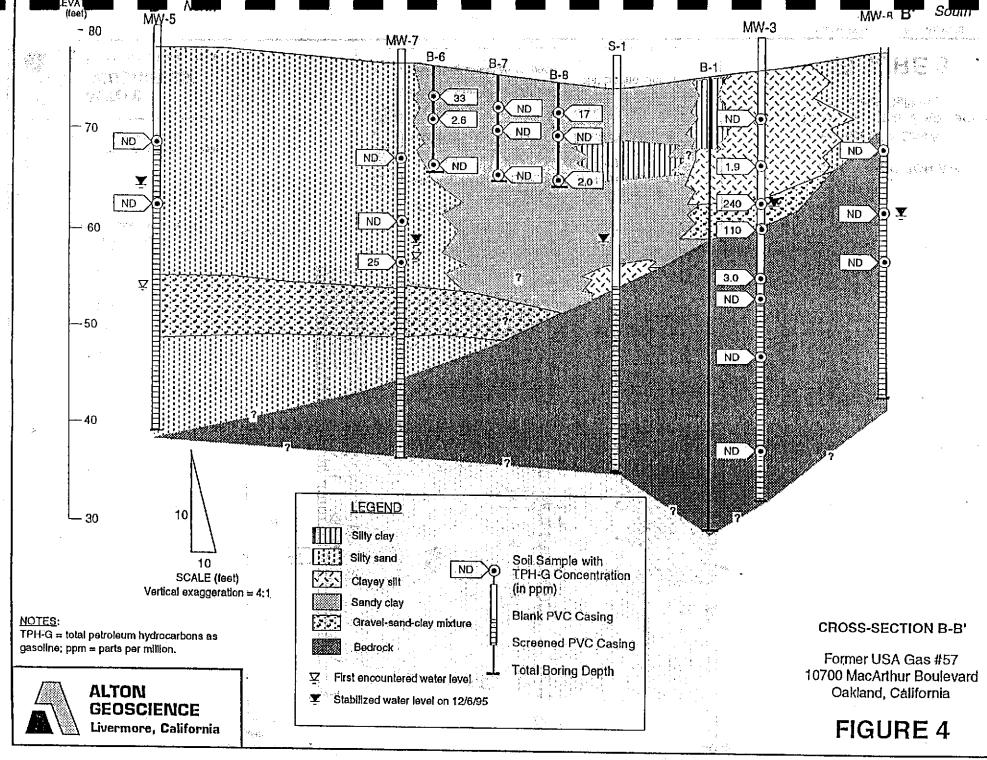
CROSS-SECTION A-A'

Former USA Gas #57 10700 MacArthur Boulevard Oakland, California

FIGURE 3

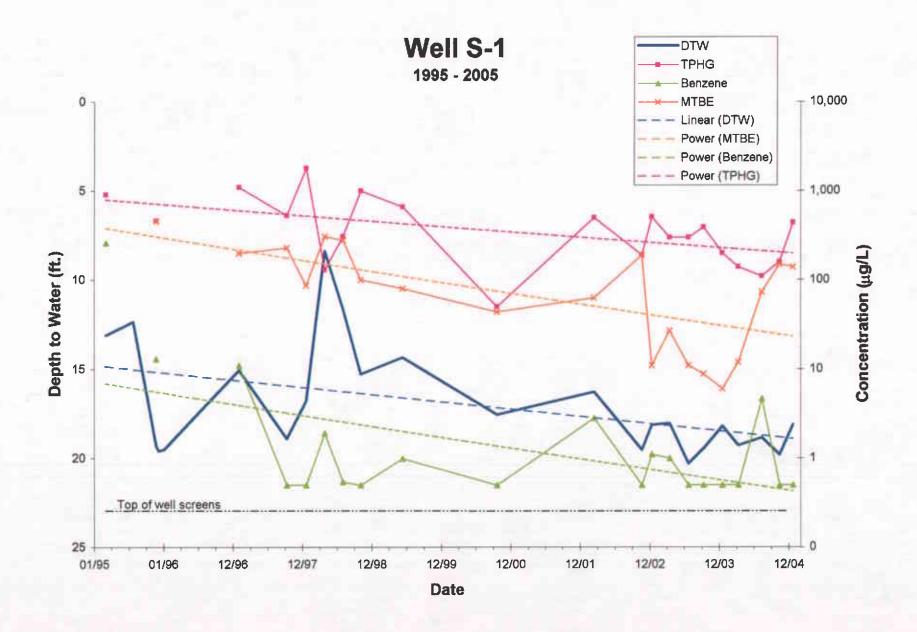


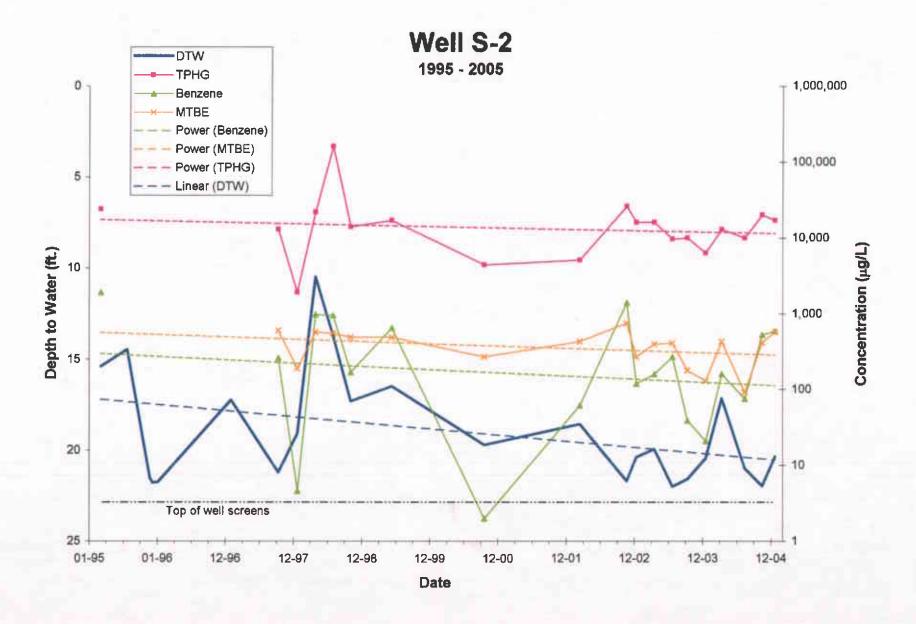


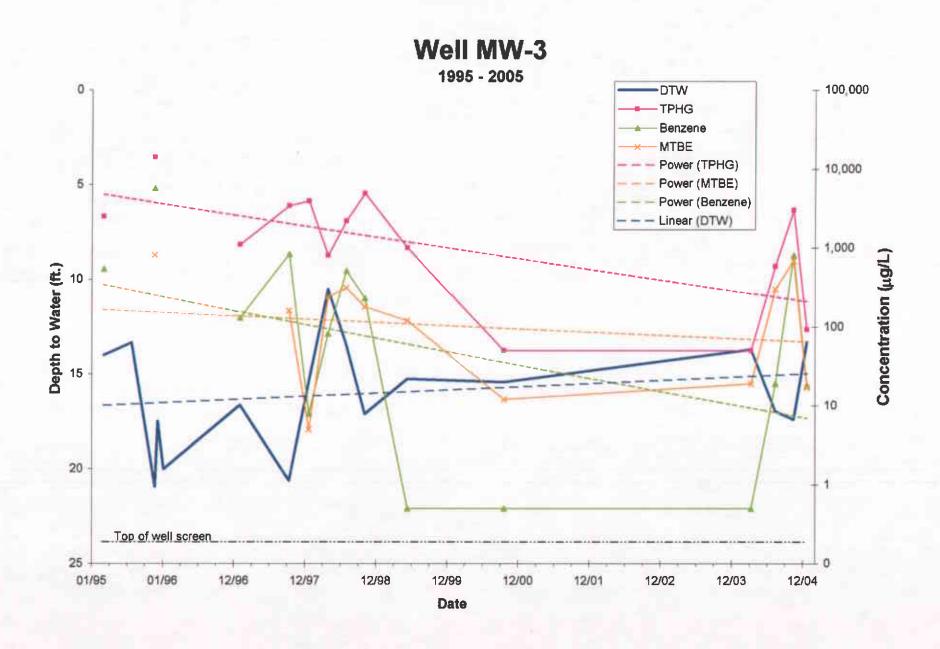


APPENDIX F

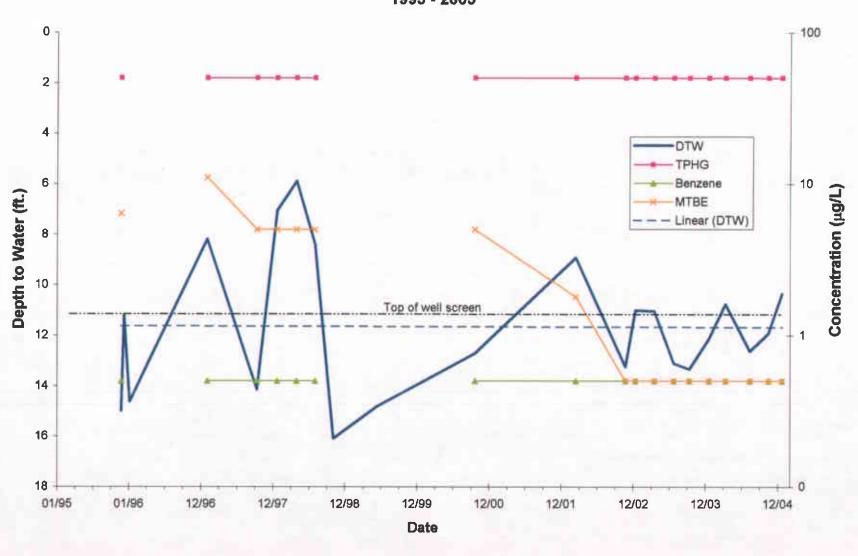
HYDROGRAPHS AND DISSOLVED CONCENTRATION PLOTS

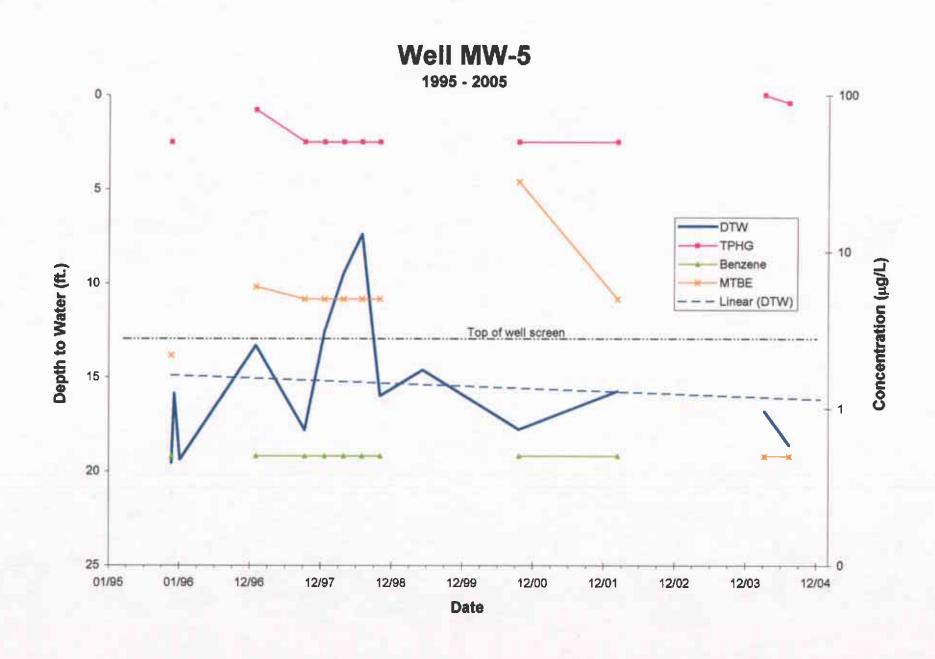






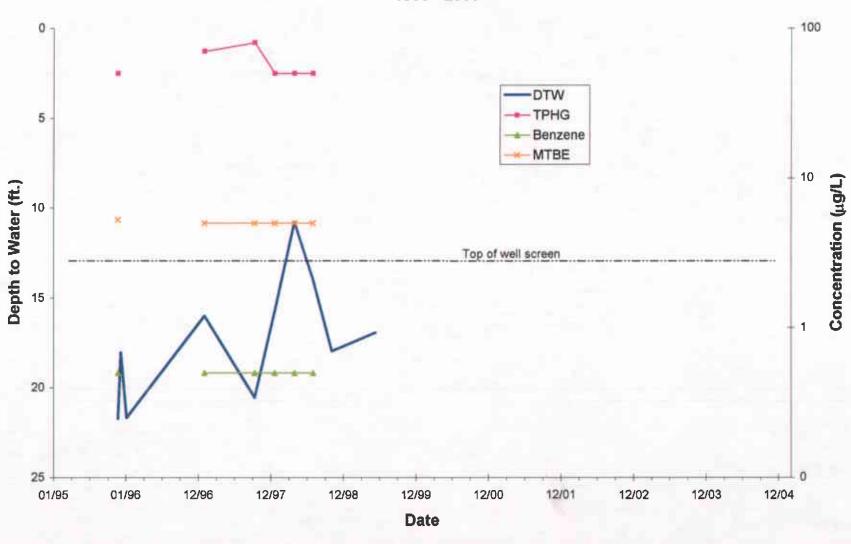
Well MW-4 1995 - 2005





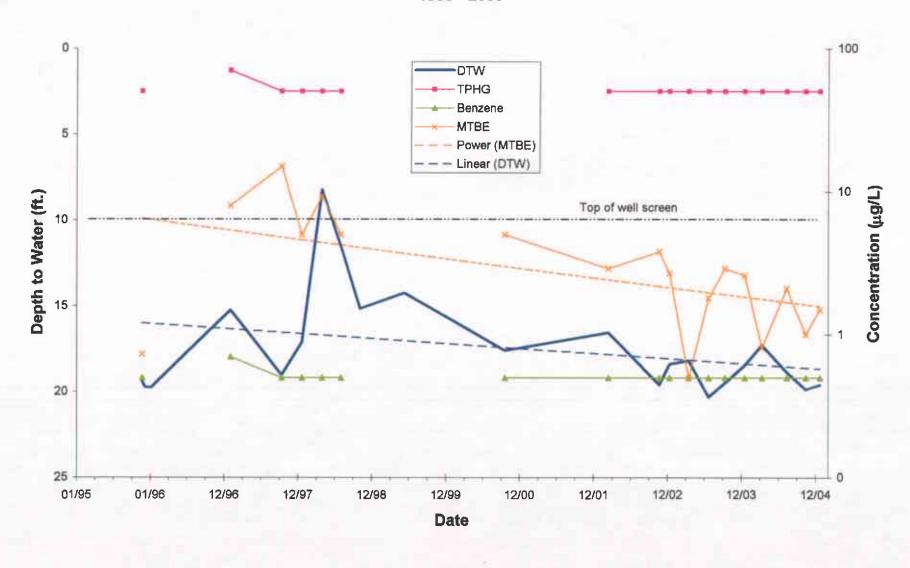
Well MW-6

1995 - 2005

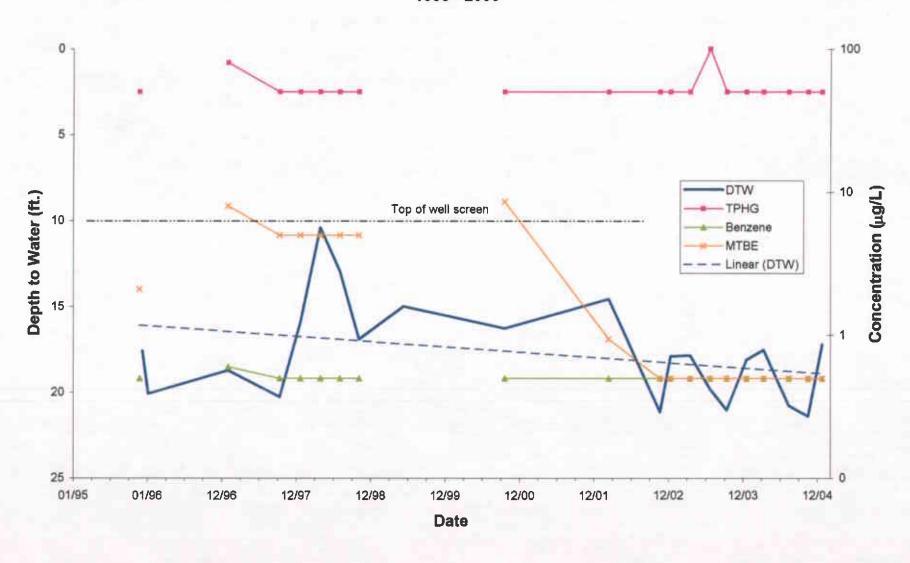


Well MW-7

1995 - 2005

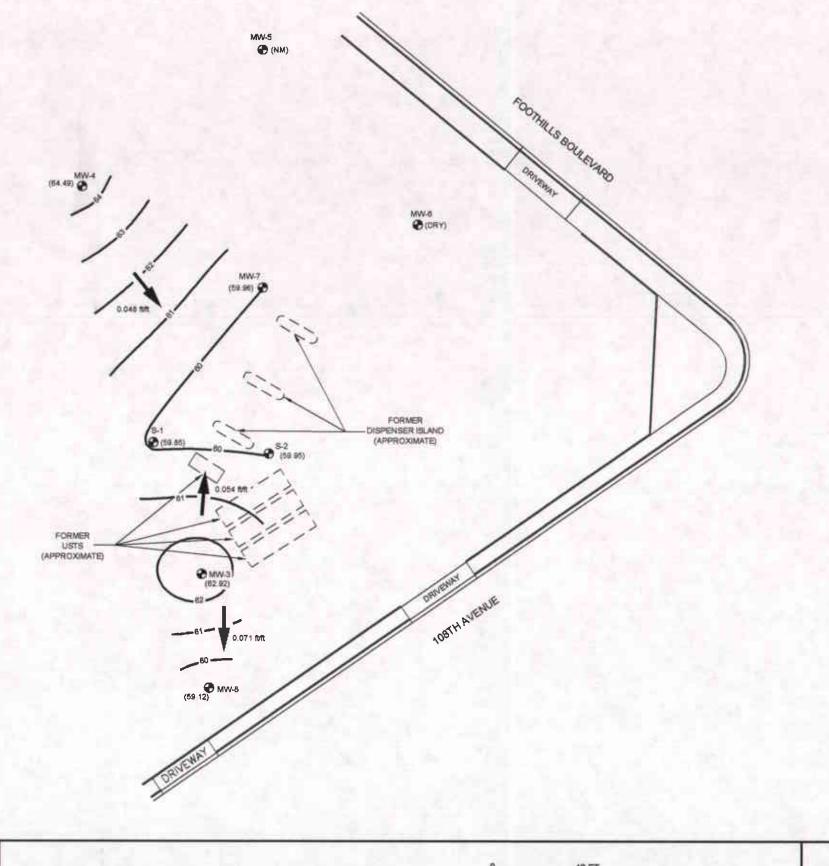


Well MW-8 1995 - 2005



APPENDIX G

HISTORICAL GROUNDWATER ELEVATION CONTOUR MAPS



LEGEND

MW-3 MONITORING WELL LOCATION

(59.86) GROUND WATER ELEVATION IN FEET RELATIVE TO MEAN SEA LEVEL

INFERRED DIRECTION OF GROUND WATER PLOW

(NM) NOT MEASURED (WELL DAMAGED)

WELLS MEASURED: 11/11/04

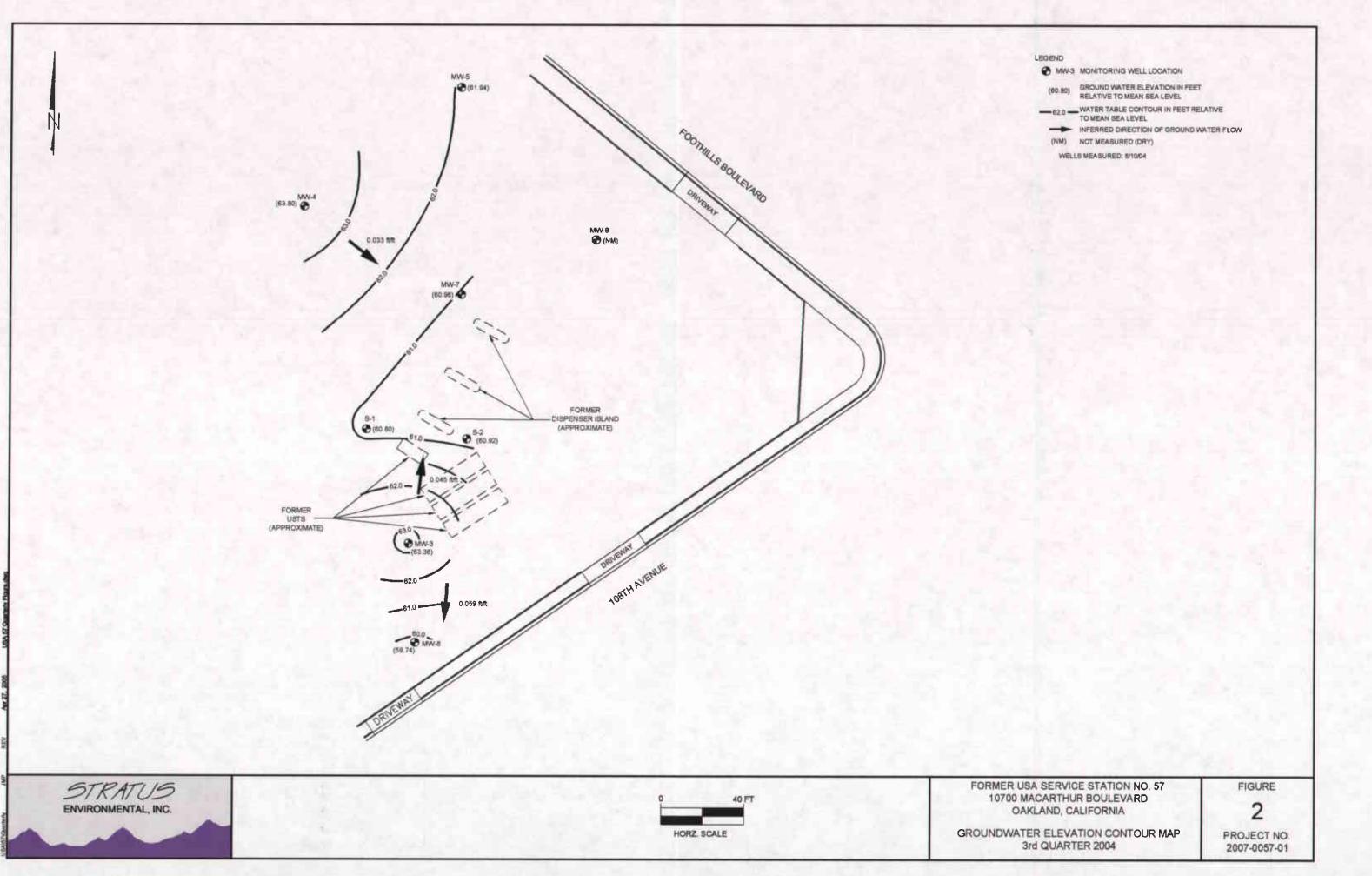
STRATUS ENVIRONMENTAL, INC.

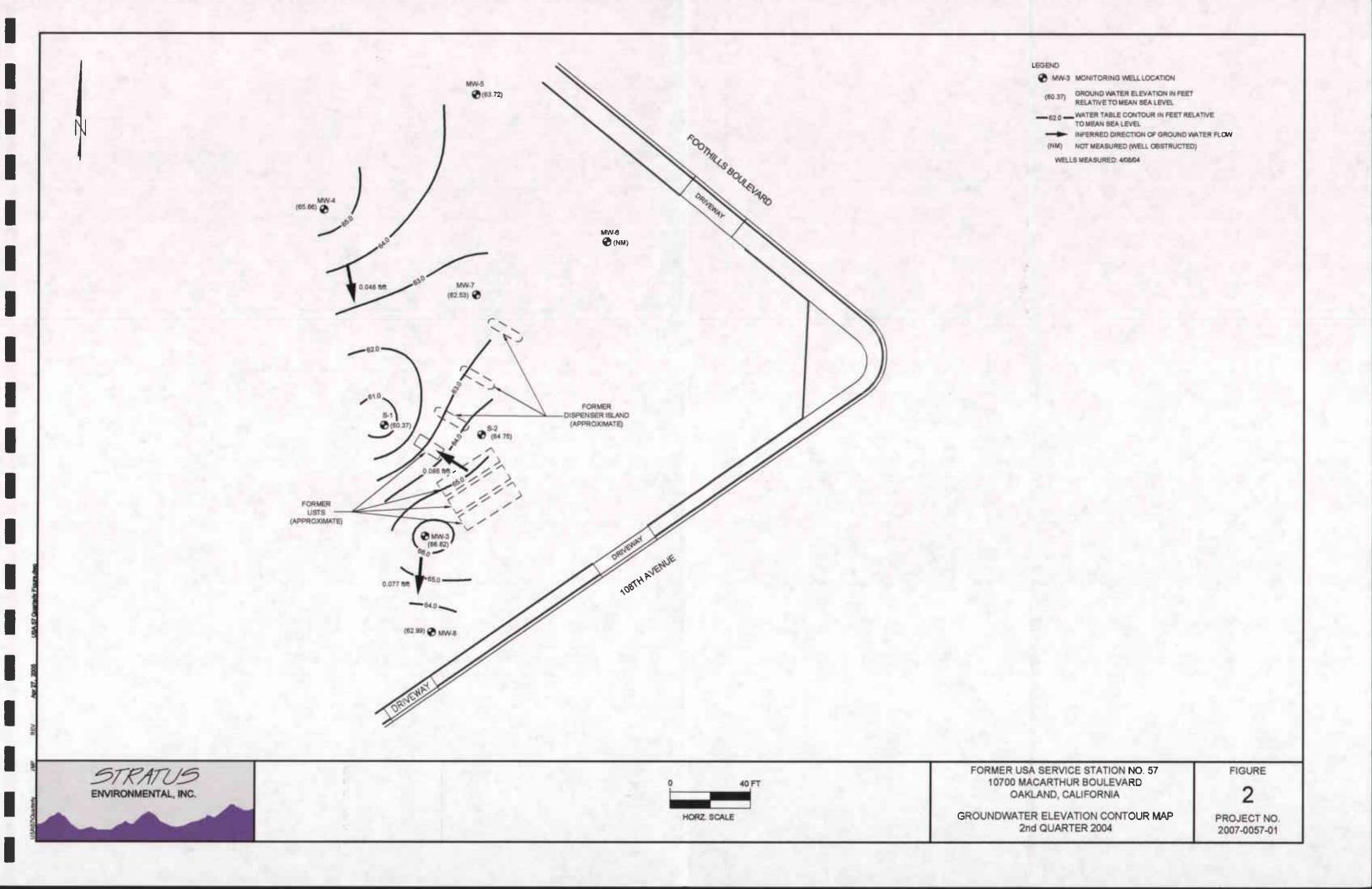


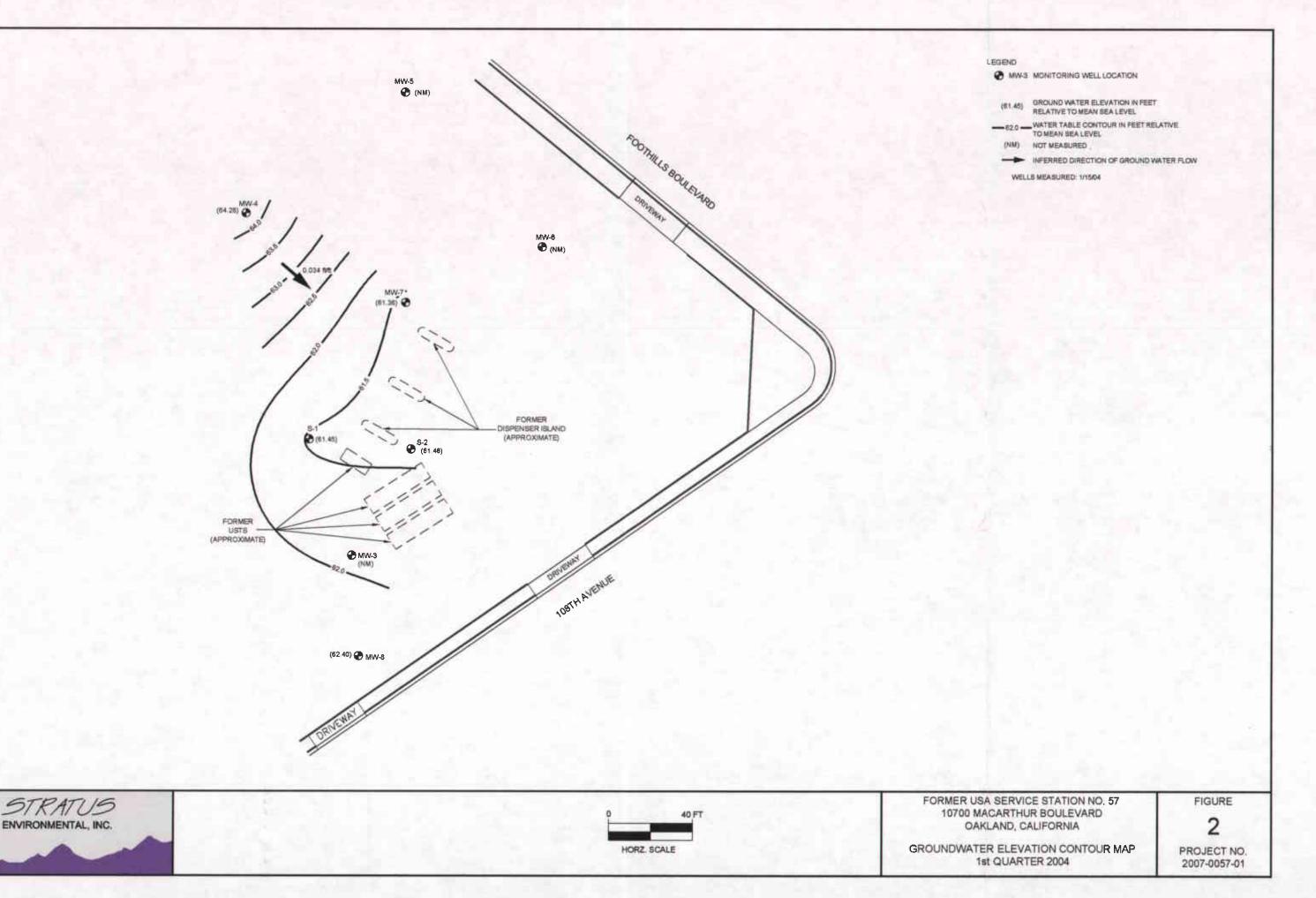
FORMER USA SERVICE STATION NO. 57 10700 MACARTHUR BOULEVARD OAKLAND, CALIFORNIA

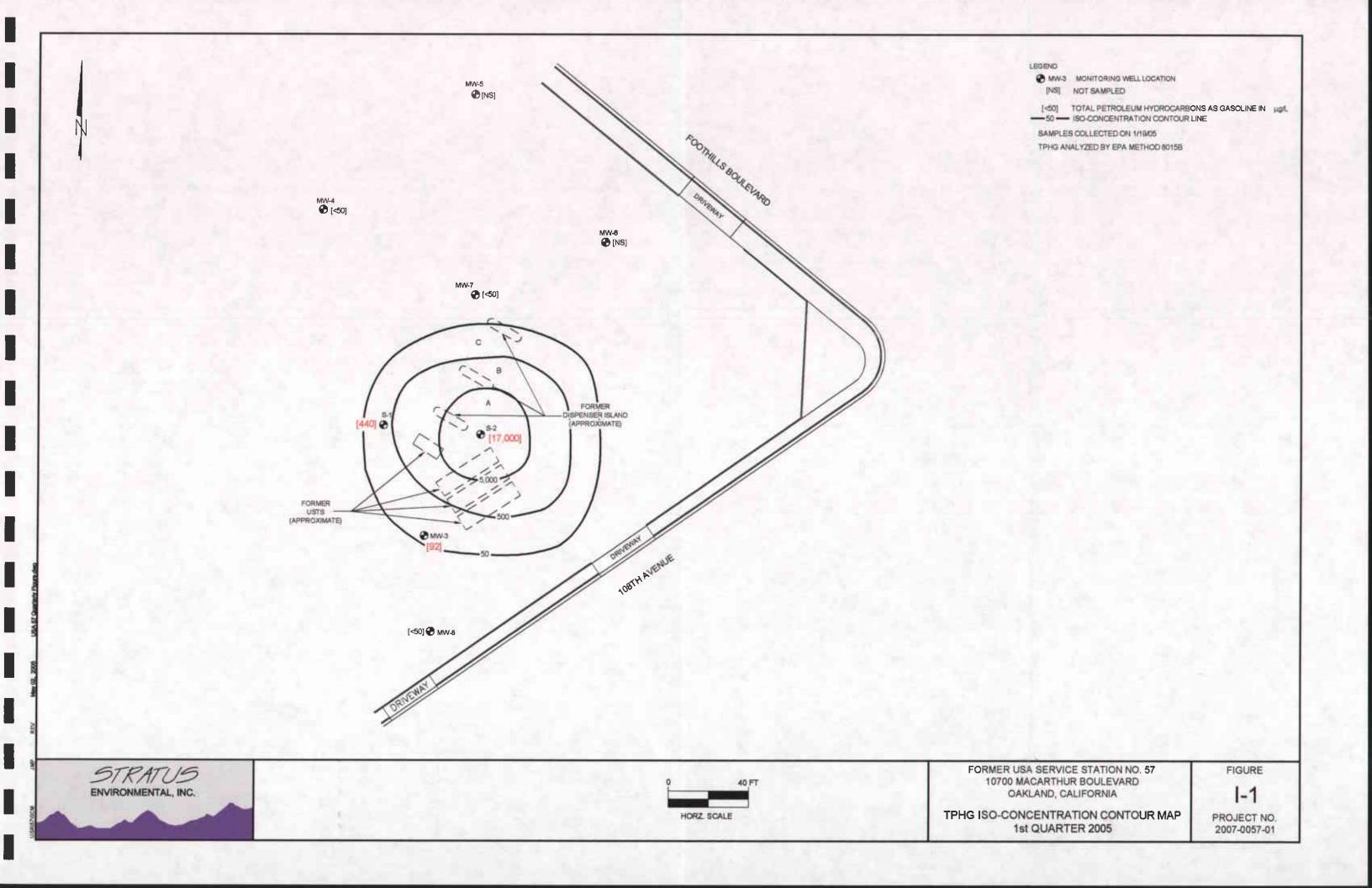
GROUNDWATER ELEVATION CONTOUR MAP 4th QUARTER 2004 FIGURE

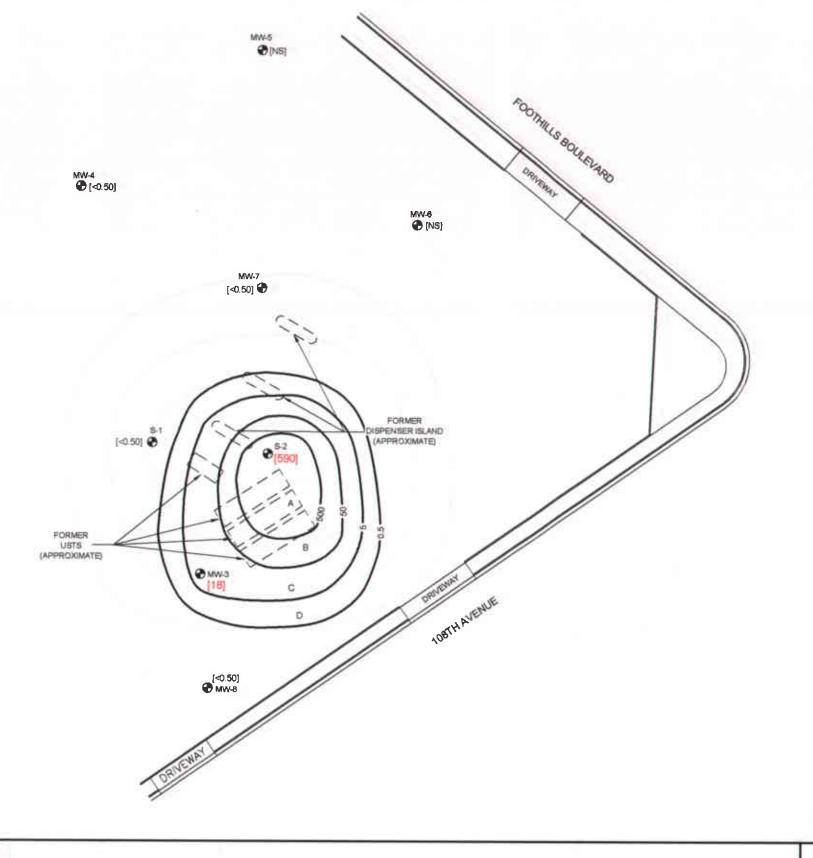
PROJECT NO. 2007-0057-01











LEGE

MW-3 MONITORING WELL LOCATION

[NS] NOT SAMPLED

[<0.50] BENZENE CONCENTRATION IN Hg/L

-50 - ISO-CONCENTRATION CONTOUR LINE

SAMPLES COLLECTED ON 1/19/05

BENZENE ANALYZED BY EPA METHOD 8260B

STRATUS ENVIRONMENTAL, INC.



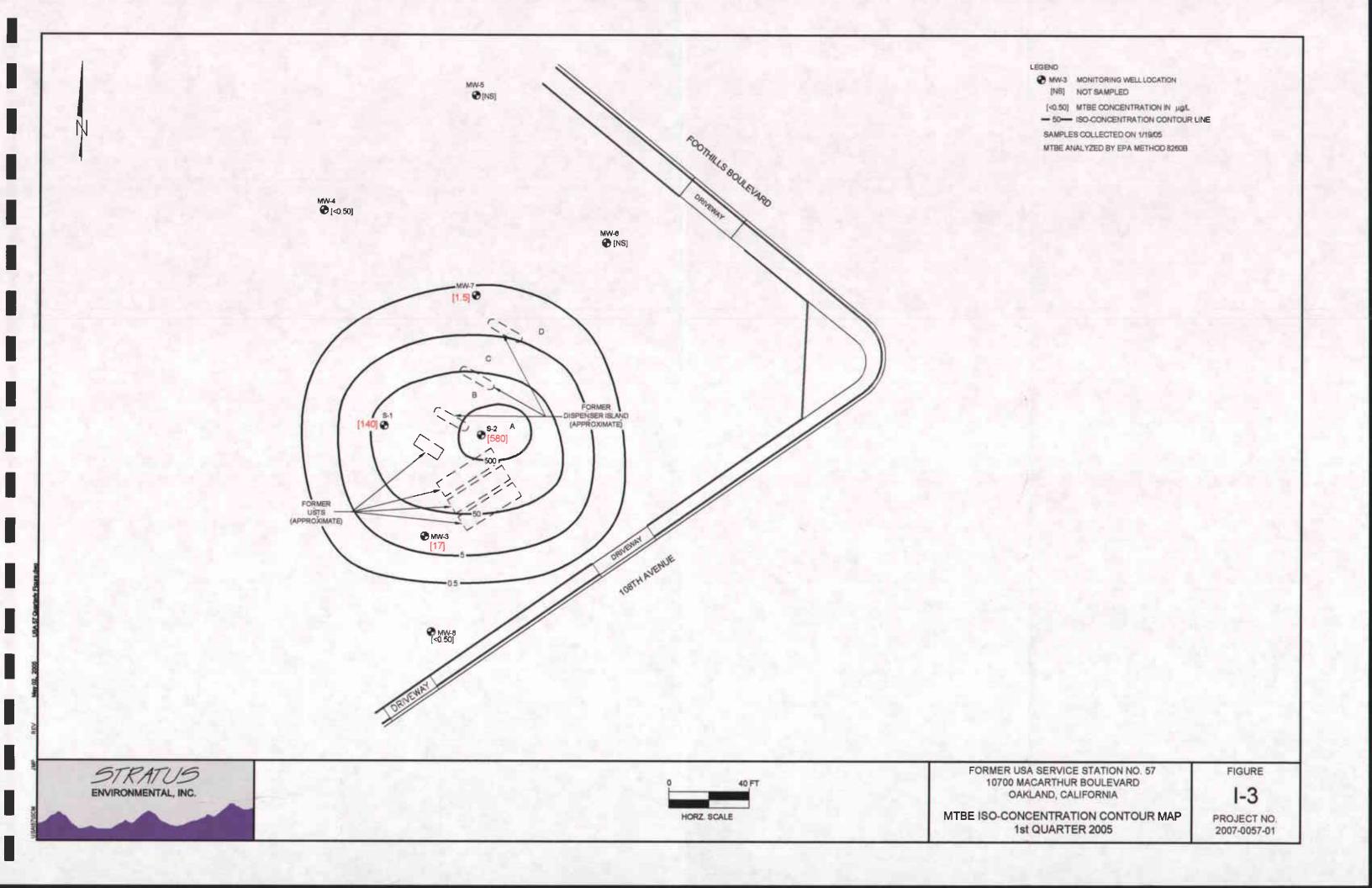
FORMER USA SERVICE STATION NO. 57 10700 MACARTHUR BOULEVARD OAKLAND, CALIFORNIA

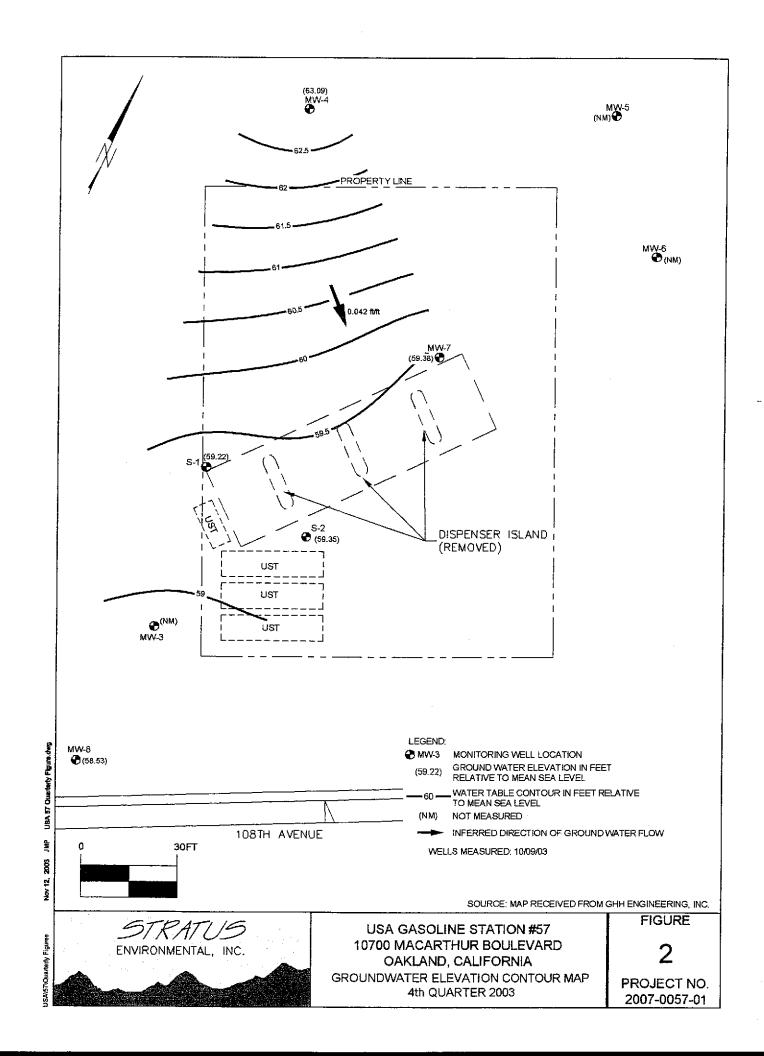
BENZENE ISO-CONCENTRATION CONTOUR
MAP 1st QUARTER 2005

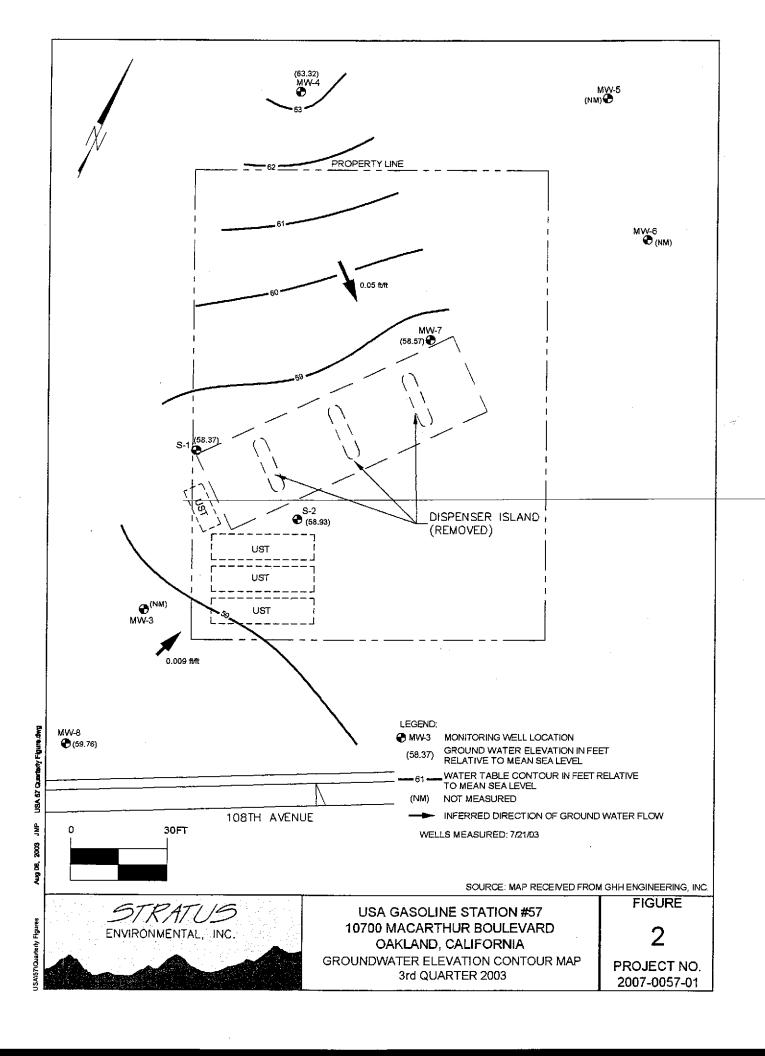
FIGURE

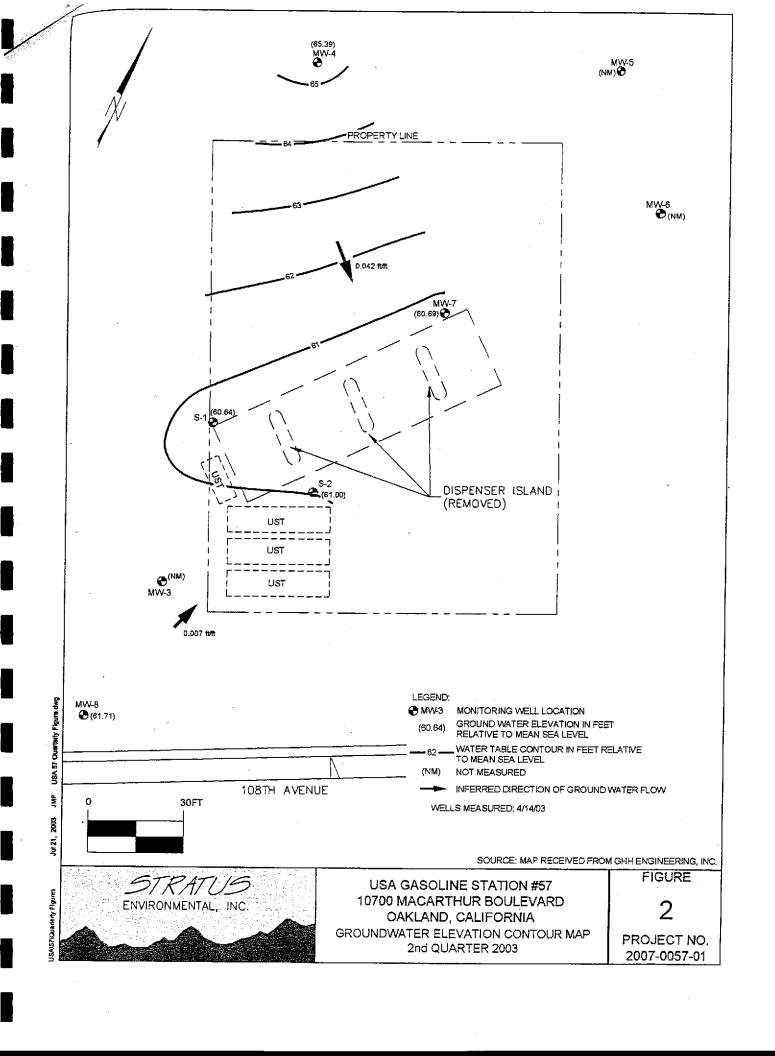
1-2

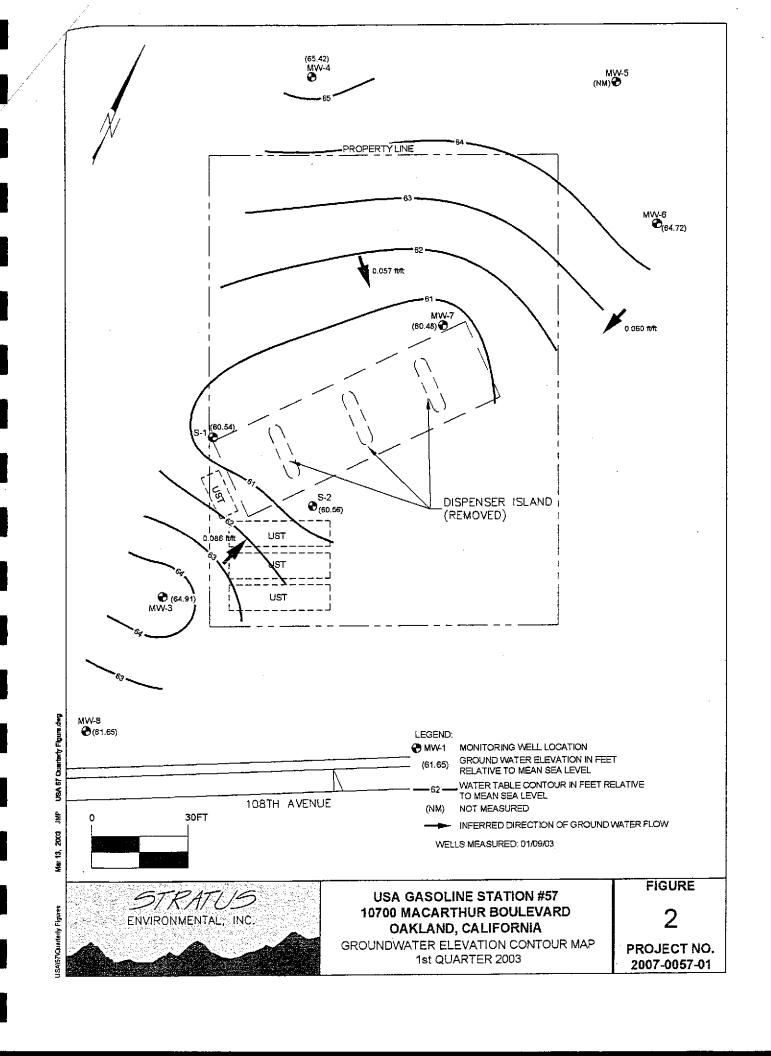
PROJECT NO. 2007-0057-01

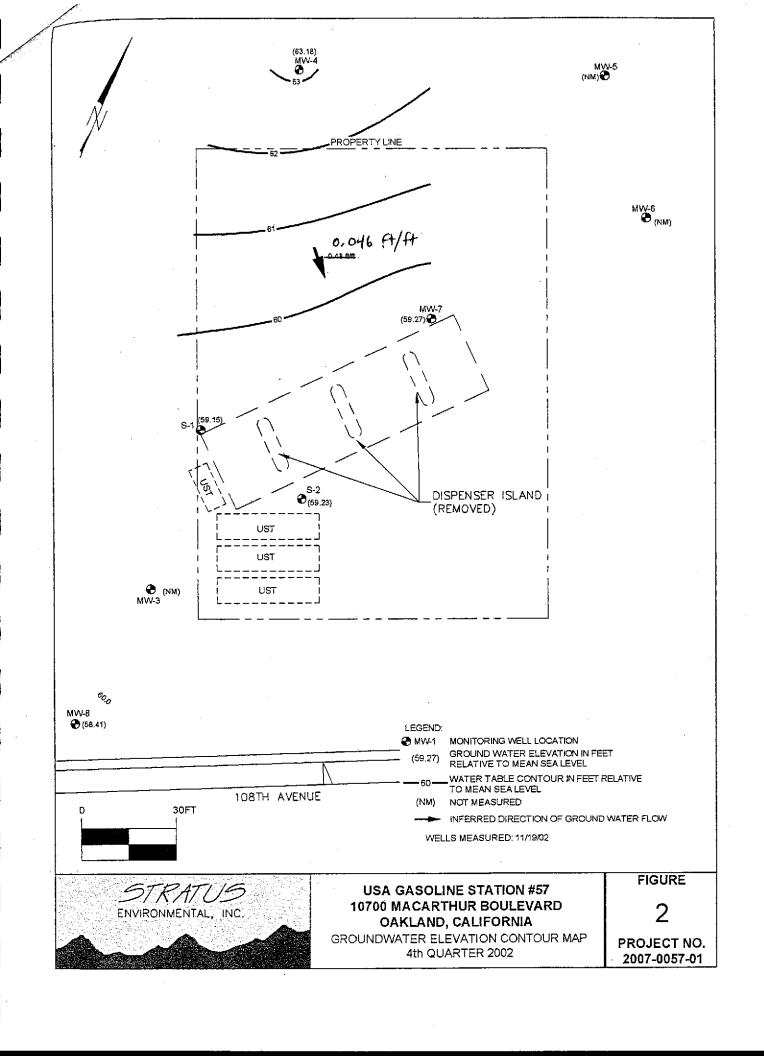


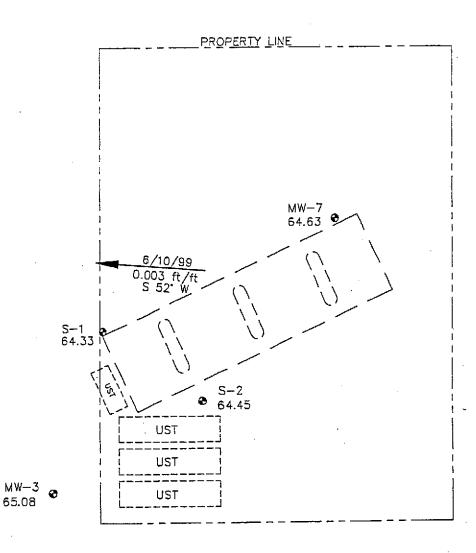












MW-6 € 64.72

MW-8 64.57

108TH AVENUE

LEGEND

MONITORING WELL LOCATION •

SCALE: 1" = 30"

USA GASOLINE STATION #57 OAKLAND, CALIFORNIA GROUNDWATER ELEVATION MAP JUNE 10, 1999

ENGINEERING, INC. 8084 Old Auburn Rd. Citrus Heights, CA 95610 (916) 723-7645

INITIAL

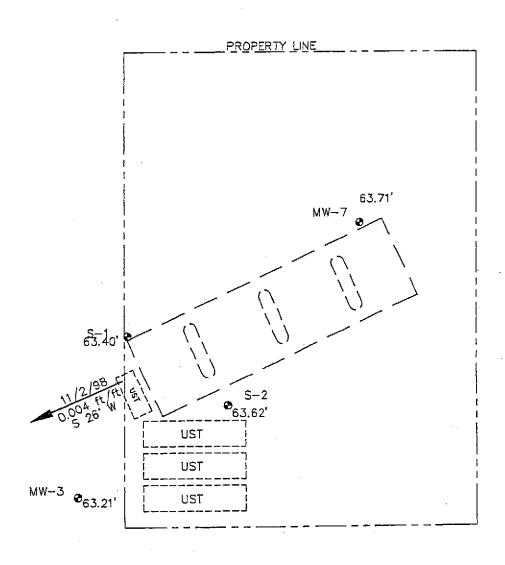
G.E.B. DATE

7/1/99

JOB # 5090

FIG. # 3 A

* NOT USED IN GRADIENT CALCULATION



MW-6 **€**63.67'

MW-8 **e**62.65'

108TH AVENUE

LEGEND

MONITORING WELL LOCATION

SCALE: 1" = 30'

* NOT USED IN GRADIENT CALCULATION

USA GASOLINE STATION #57 OAKLAND, CALIFORNIA GROUNDWATER ELEVATION MAP NOVEMBER 2, 1998

ENGINEERING, INC. 8084 Old Auburn Rd.

Citrus Heights, CA 95610 (916) 723-7645

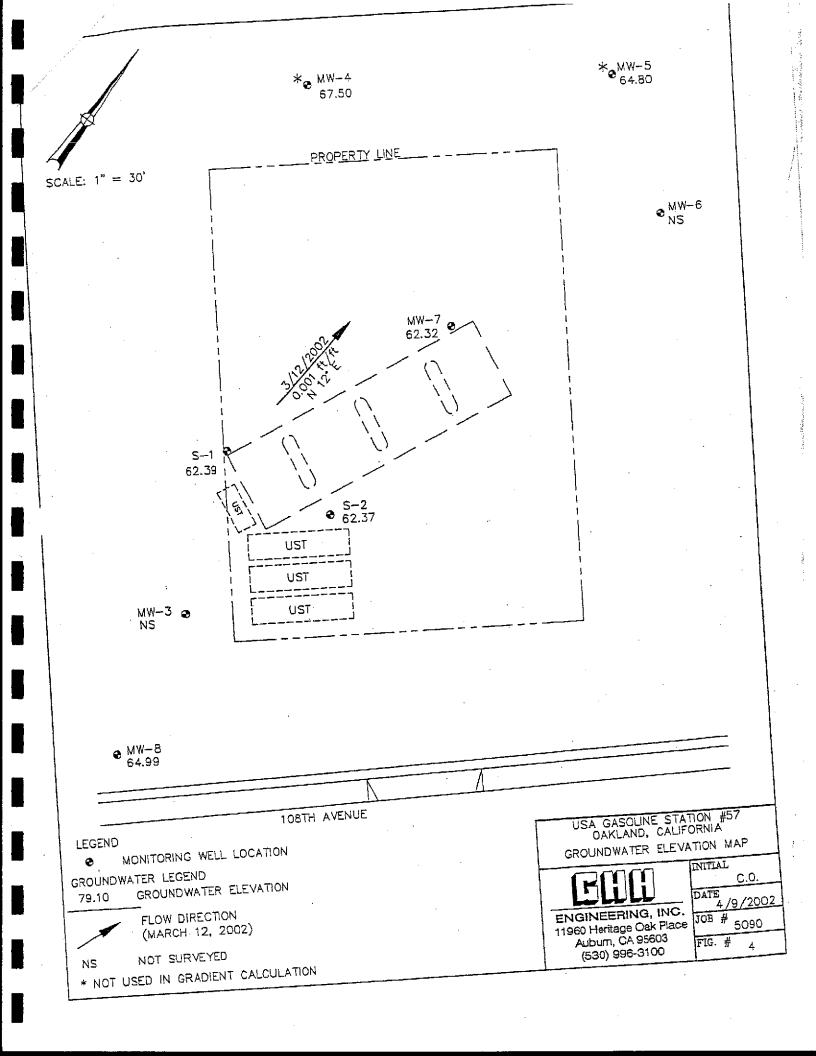
INITIAL

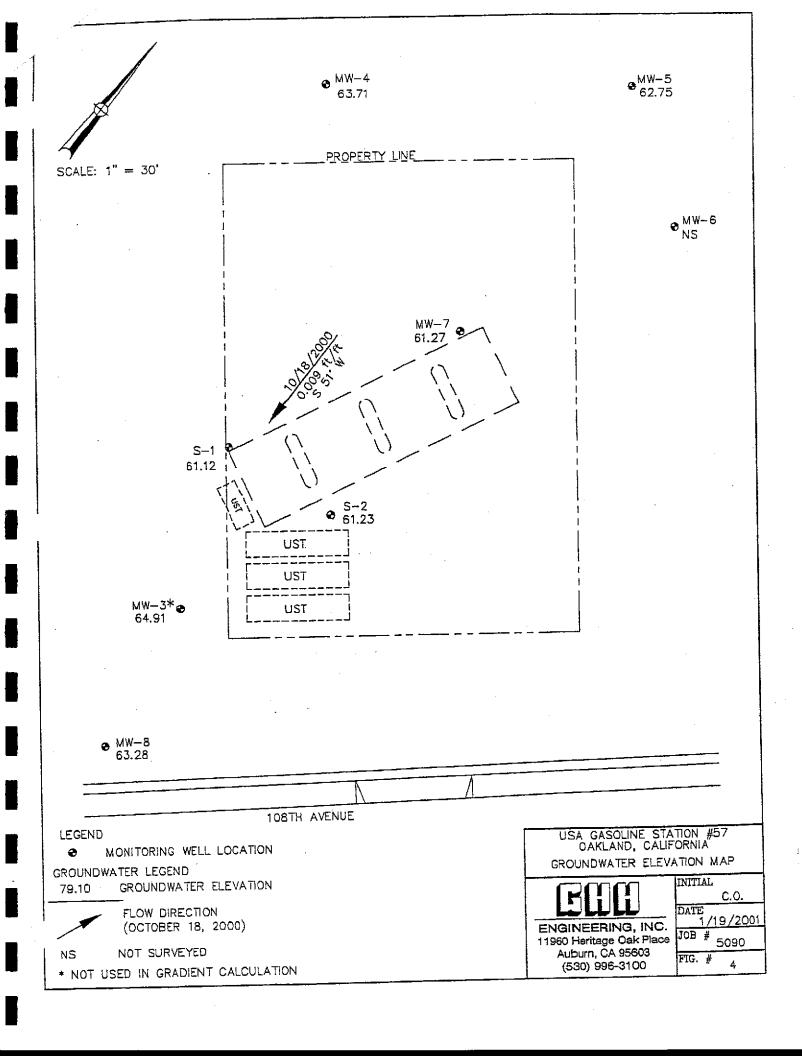
G.E.B.

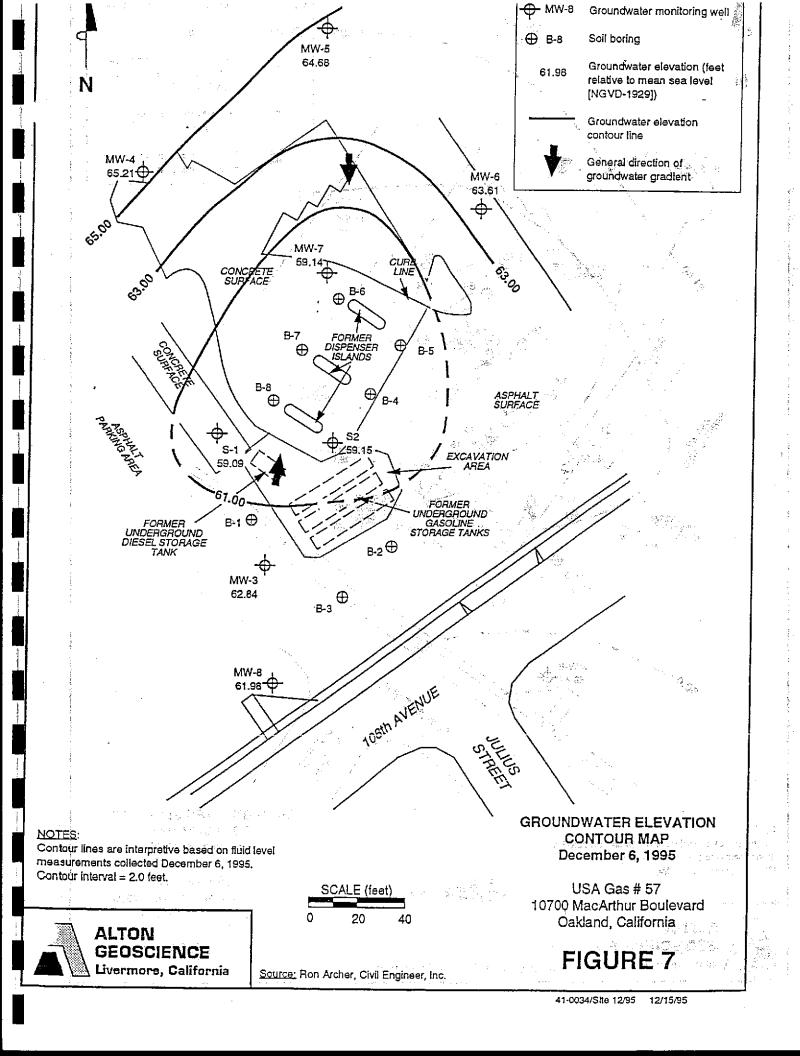
DATE 7/1/99

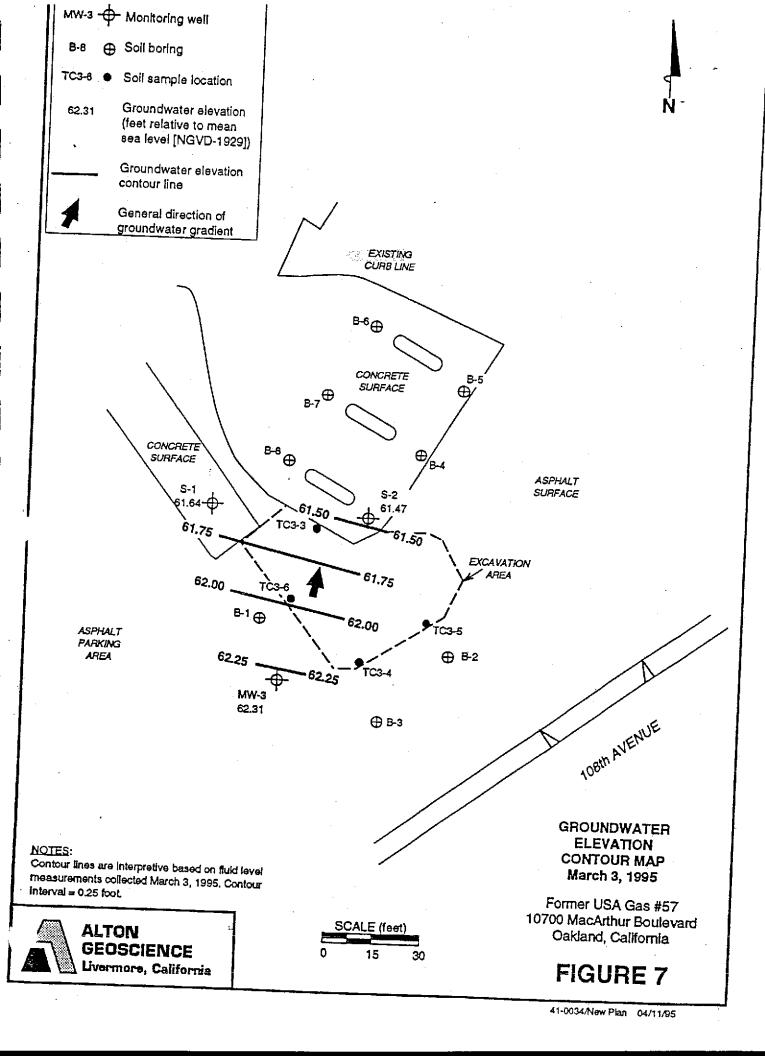
JOB # 5<u>090</u>

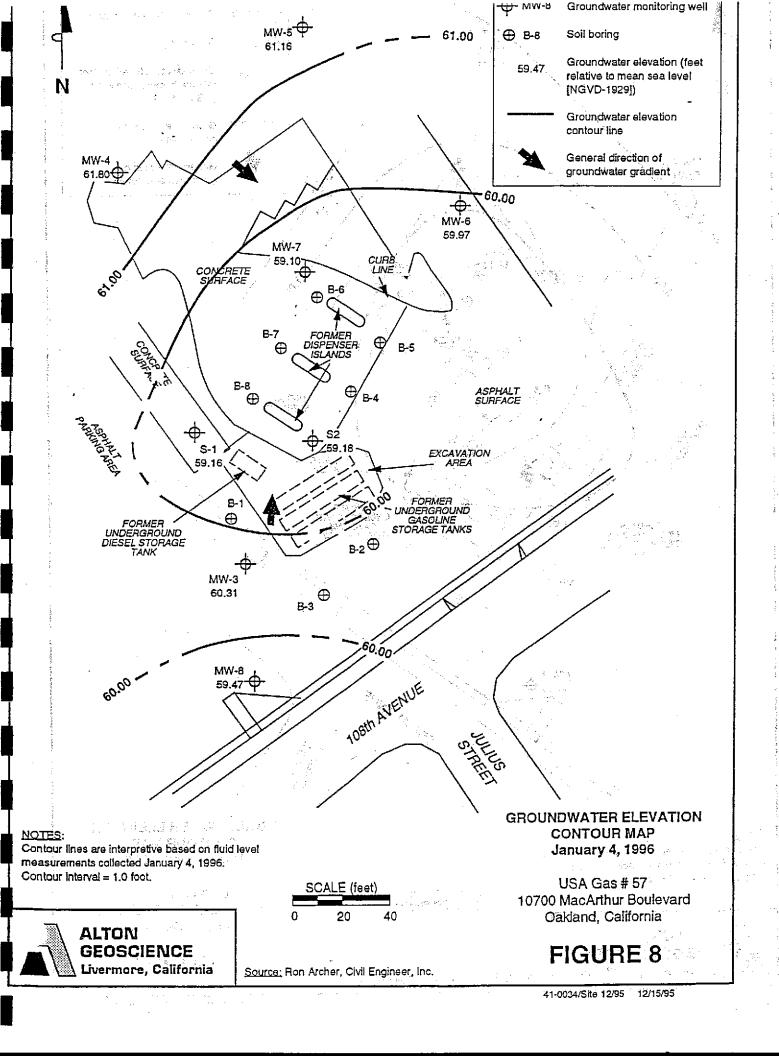
FIG. #











APPENDIX H

DEPTH DISCRETE ISO-CONCENTRATION CONTOUR MAPS FOR TPHG AND PETROLEUM HYDROCARBON MASS ESTIMATES

Former USA Station No. 57 10700 MacArthur Boulevard Oakland, California of TPHG Remaining in the Vadose Zone

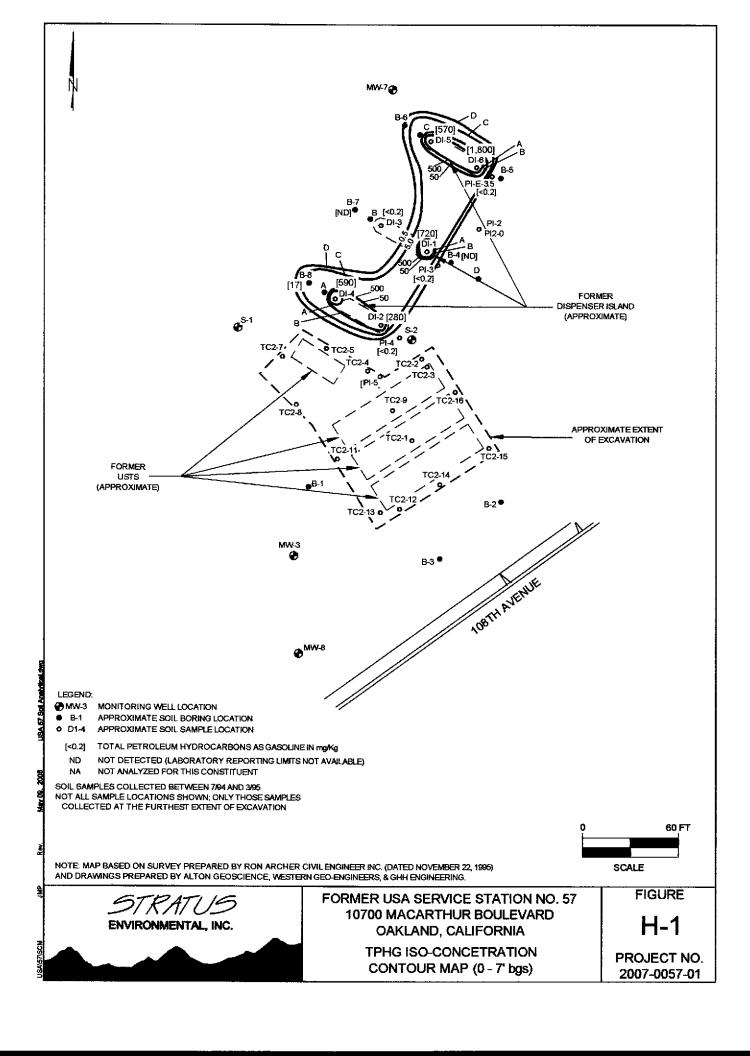
Mass of TPH	3 Remaining	in the	Vadose Zo	one

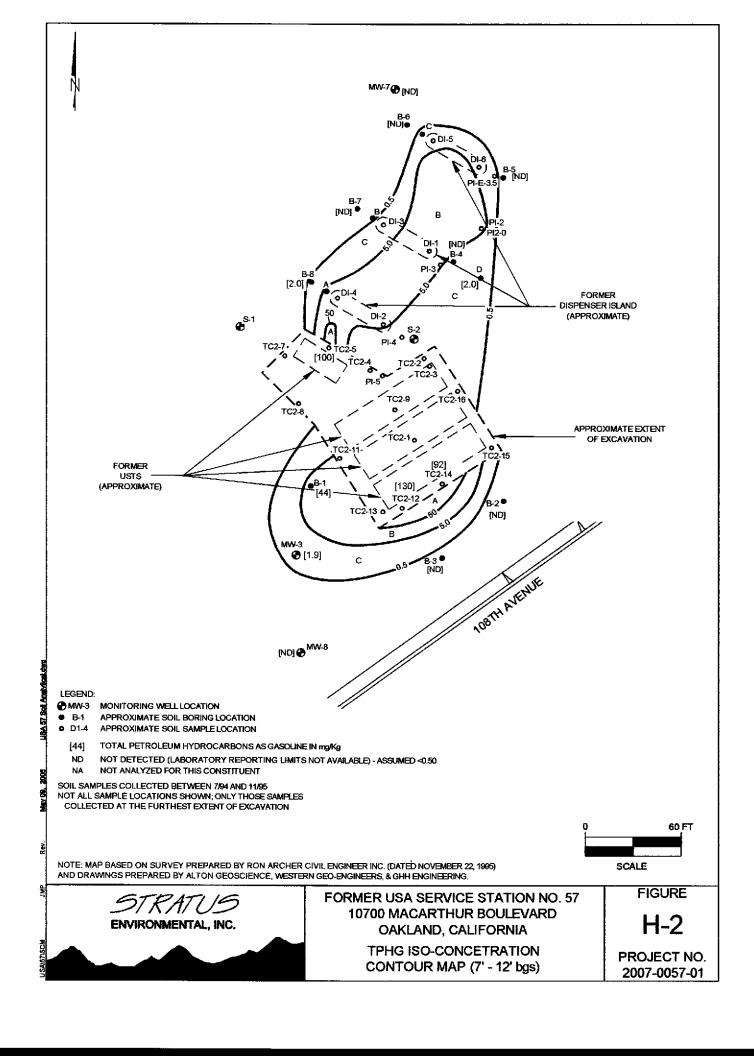
Basis	Area ID	Area sq.ft	Depth ft	Avg Conc mg/kg	Soil Volume cu.ft	Soil Density Kg/cu.ft	Soil Mass Kg	TPHG Mass Kg
H-1								
Figure 60	Α	224.13	7	500	1,568.91	36.85	57,814.33	28.91
(0 to 7	В	311.95	7	50	2,183.65	36.85	80,467.50	4.02
feet bgs)	С	1790.43	7	5	12,533.01	36.85	461,841.42	2.31
	D	634.46	7	0.5	4,441.22	36.85	163,658.96	0.08
					Mass of TPHG	from 0 - 7 feet b	gs =	35.32
H.Z								
Figure 65	Α	228.83	5	50	1,144.15	36.85	42,161.93	2.11
(7 to 12	В	4374.89	5	5	21,874.45	36.85	806,073.48	4.03
feet bgs)	С	5670.22	5	0.5	28,351.10	36.85	1,044,738.04	0.52
		<u>.</u>			Mass of TPHG	from 7 - 12 feet l	bgs =	6.66
43								
Figure 6E	Α	397	5	500	1,983.80	36.85	73,103.03	36.55
(12 to 17	В	2681.09	5	50	13,405.45	36.85	493,990.83	24.70
feet bgs)	С	10360.94	5	5	51,804.70	36.85	1,909,003.20	9.55
[<u></u>	Mass of TPHG	from 12 - 17 feet	bgs_=	70.80
H-A								
Figure 64	Α	285.34	5	500	1,426.70	36.85	52,573.90	26.29
(17 to 22	В	1250.00	5	5	6,250.00	36.85	230,312.50	1.15
feet bgs)	С	4565.62	5	0.5	22,828.10	36.85	841,215.49	0.42
					Mass of TPHG	from 17 - 22 feel	bgs =	27.86

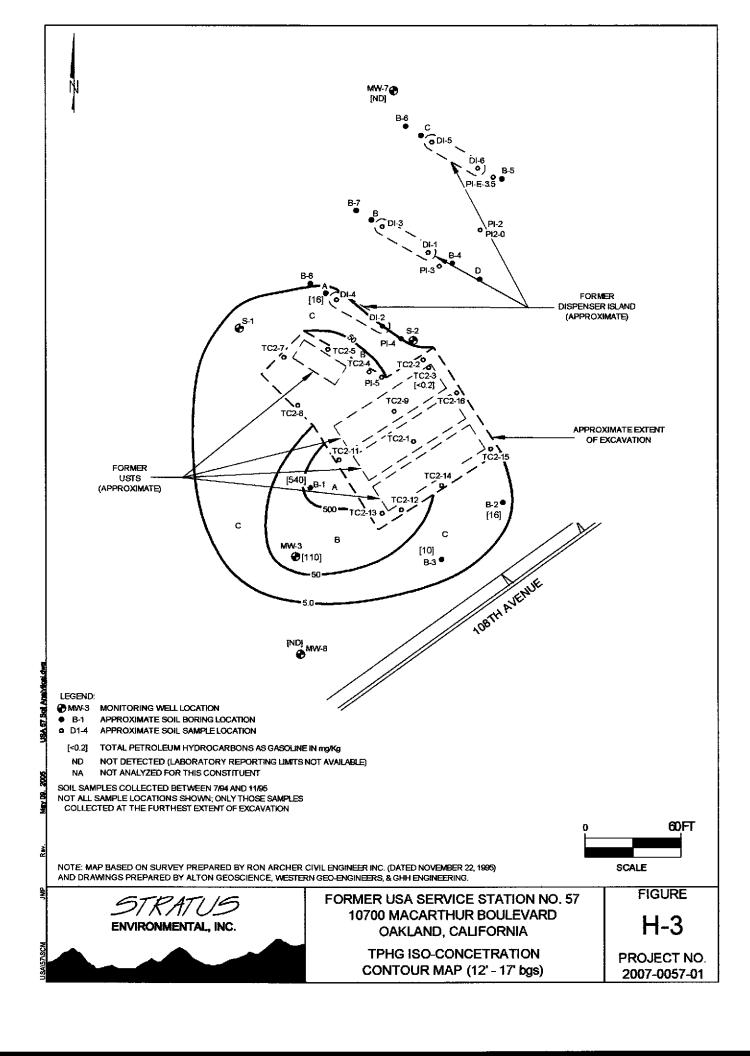
Estimated Total Mass of Petroleum Hydrocarbons in the Subsurface = 141

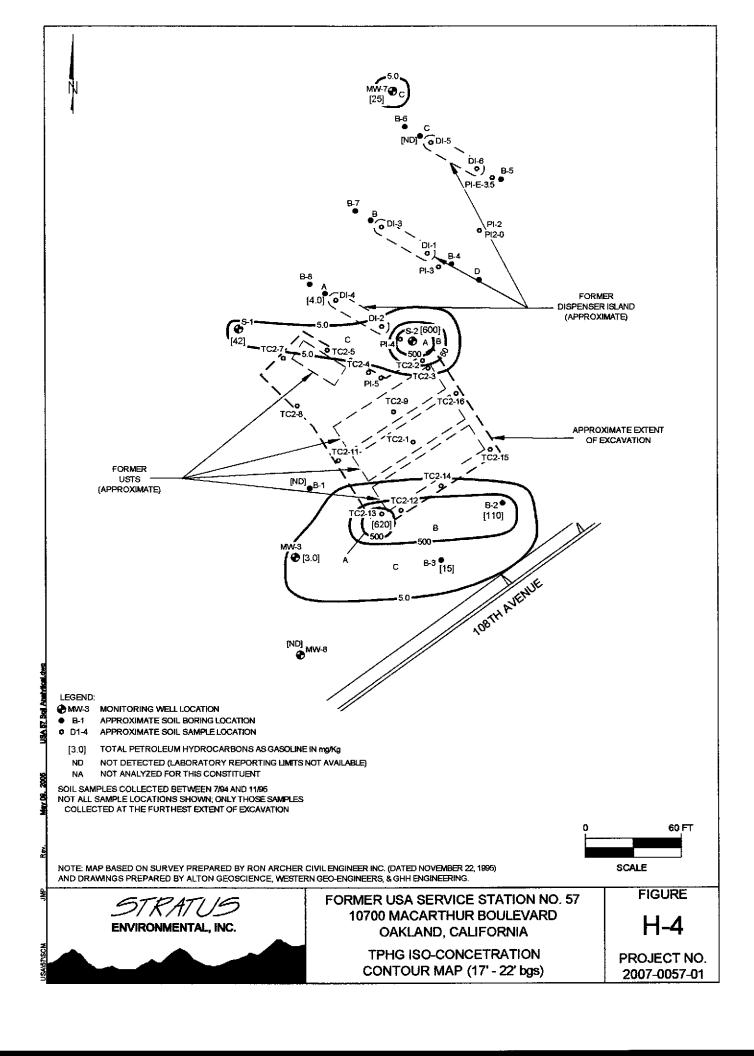
Notes:

- 1. Concentrations are assumed from the outer contour. Assumed to be uniform across area.
- 2. The average concentration is assumed to be uniform across the chosen depth of soil profile
- 3. Soil density is assumed be to 36.85 kilograms per cubic feet (Kg/cu.ft)
- 4. Soil Mass = Soil Density * Soil Volume
- 5. TPHG Mass(Kilograms) = Soil Mass (Kilograms) * Average Concentration (Avg Conc) (milligrams*10⁻⁶/Kilogram)









Former USA Station No. 57 10700 MacArthur Boulevard Oakland, California Mass of TPHG, Benzene, and TPHD in Stockpiled Soil

Basis	Avg Conc mg/kg	Soil Volume cu.ft	Soil Density Kg/cu.ft	Soil Mass Kg	Mass Kg
TPHG	192.46	20,925.00	36.85	771,086.25	148.40
Benzene	0.09	20,925.00	36.85	771,086.25	0.07
TPHD	376.40	1,350.00	36.85	49,747.50	18.72

Notes:

- 1. Average concentrations based on data from Western Geo-Sciences (1994).
- Stockpile for TPHG and benzene assumed to be 775 cubic yards.
- 3. Stockpile for TPHD assumed to be 50 cubic yards.

APPENDIX I

DISSOLVED ISO-CONCENTRATION CONTOUR MAPS AND DISSOLVED HYDROCARBON MASS ESTIMATES 1ST QUARTER 2005

Former USA Station No. 57 10700 MacArthur Boulevard Oakland, California Dissolved Hydrocarbon Mass Remaining

Basis	Area ID	Area sq.ft	Depth ft	Avg Conc μg/L	Water Volume liters	TPHG Mass grams
TPHG	Α	1670.58	27.5	5,000	390,271.17	1,951.36
Figure I-1	В	4053.93	27.5	500	947,055.52	473.53
	С	5564,06	27.5	50	1,299,843.30	64.99
		!				
			Estimated	Mass of TPHG	in groundwater =	2,489.88
					-	
Be	Α	1271.78	27.5	500	297,105.84	148.55
Figure I-2	В	1454.28	27.5	50	339,740.43	16.99
	С	2717.27	27.5	5	634,792.80	3.17
	D	2722.87	27.5	0.5	636,101.04	0.32
			Estimated M	ass of Benzene	in groundwater =	169.03
						_
MTBE	Α	812	27.5	500	189,694.71	94.85
Figure I-3	В	4682.65	27.5	50	1,093,933.43	54.70
-	С	6074.20	27.5	5	1,419,019.24	7.10
	D	8141.09	27.5	0.5	1,901,874.04	0.95
					, ,	
			Estimated	Mass of MTBE	in groundwater =	157.59

Notes:

- 1. Based on groundwater data from 1st quarter 2005.
- 2. Average concentration for area assumed equal to outer contour value.
- 3. The average concentration is assumed to be uniform vertically.
- 4. Water column = TD deepest well (44 ft bgs) average DTW (16.5 ft bgs).
- 5. Based on soil drilling observations, average porosity assumed to be 30%.
- 6. Mass (grams) = volume (ft³) * porosity * 29.31687 (L/ft³) * concentration (μ g/L) * 10-6 (g/mg).

APPENDIX J DPE TEST DATA

TABLE 1 DPE TEST USING WELL S-2

Former USA Station No. 57 10700 MacArthur Boulevard Oakland, California

		Ampl	Air	Totalizer	GW	Inf	Oper				nduced	Vacuun	n ("WC)	&/or DT\	N (feet	bgs) Data	in Obse	ervation	Wells			[
	TE	Appl			Ext Rate		Temp		S-1			MW-3		MW	4	MW			MW-7		MW	/-8
Date & Time	hh:mm	Vac "Hg	Flow cfm	gallons		ppmv	deg F	Vac	DTW	DD	Vac	DTW	DD	DTW	DD	DTW	DD	Vac	DTW	DD	DTW	DD
7/6/2004 7:00	1111,1111111	119_		42,120					18.13			15.70		12.26		18.07			18.19	<u> </u>	19.55	L
7/6/2004 8:30	,			<u>. </u>		Start	Up Test	using we	II S-2, DT	W =20.	26 feet	bgs and	DPE u	nit hour i	meter re	ading =	839.6					
7/6/2004 9:00	00:30	25.50	87	42,120		2.9	1,450	NM	NM	NM	NM	MM	NM	NM	NM	NM	NM	MM	NM	MM	NM	NM
7/6/2004 10:00	01:30	L NM	NM	42,120	 	23.0	NM	0.35	NM	МИ	NM	NM	NM	NM	NM	NM	NM	NM	NM	NM	NM	NM
7/6/2004 11:00	02:30	26.25	88	42,130	0.07	29.0	1,466	1.30	18.38	0.25	0.0	15.70	0.00	12.27	0.01	18.08	0.01	0.0	18.30	0.11	19.58	0.03
7/6/2004 11:00	03:30		87	42,200	0.33	24.0	1 444	0.50	18.58	0.45	0.0	15.69	-0.01	12.25	-0.01	18.05	-0.02	0.0	18.35	0.16	19.51	-0.04
7/7/2004 6:30	22:00			42,820		7.1	1,456	0.20	18.65	0.52	0.0	15.70	0.00	12.26	0.00	18.04	-0.03	0.0	18.38	0.19	19.55	0.00
	22:20	20.00		12,020	<u> </u>		<u> </u>	L_ 		Disc	ontinue	Test on	1 S-2	-								
7/7/2004 6:50	·							<u> </u>	50			60		13	15	1	70		70		10	00
Distance to Extra	tion Well				-				20 - 40			24 - 44	_	10 -	40.5	10	- 40		10 - 40.	5	10	- 35
Screening Interva	1	20 - 4	IO (S-2)					<u>L</u>			<u> </u>			Щ—		<u> </u>						

Notes:

TE - Time Elapsed, hours: minutes

Appl - Applied

Oper - Operating

Vac - Vacuum

DTW - depth to groundwater

" WC - Inches water column

ppmv - parts per million by volume

Temp - Temperature

deg F - degree Farenheit

Ext. - Extraction

cfm - cubic feet per minute

Inf - Influent

DD - Drawdown

GW Ext - Groundwater Extraction

PID - Photo Ionization Detector

All induced vacuum measured in observation wells were in "WC

gpm - gallons per minute

"Hg - Inches Mercury

bgs - below ground surface

TABLE 2 DPE TEST USING WELL S-1

Former USA Station No. 57 10700 MacArthur Boulevard Oakland, California

	TE	Anni	Air	Totalizer	GW	Inf	Oper			ln	duced	Vacuum	("WC)	&/or DT	W (feet	bgs) Da	ita in Ob	servati	on Wells	5		
	16	Appl			Ext Rate		Temp.		S-2			MW-3		MW	1-4	MV	V-5		MW-7		MW	/-8
Date & Time	hh:mm	Vac "Hg	Flow	gallons		ppmv	deg F	Vac	DTW	DD	Vac	DTW	DD	DTW	DD	DTW	DD	Vac	DTW	DD	DTW	DD
7/7/2004 7:05		119	Cilli	ganono	<u> </u>	1-1			Star	Up Te	st usine	Well S	-1						· · · · · · · · · · · · · · · · · · ·			
		NM	NM	42,820	NM	NM	NM	NM	NM		NM	15.70		12.26		18.07			18.38		19.55	<u> </u>
7/7/2004 7:05			 	<u> </u>	 		1,459	+7.4	30.08		NM	NM	NM	NM	NM	NM	NM	NM	NM	NM	NM	NM
7/7/2004 7:30	00:25	24.00	86	42,890	2.80	1.5	1,409	-									0.04		10.00	0.00	10.55	0.00
7/7/2004 8:00	00:55	24.00	87	42,890		0.6	1,456	+4.4	25.35	-4.73	0.0	15.70	0.00	1 - 1 - 1		 		0.0	18.38			
7/7/2004 9:00		24.00	87	42,960	0.61	0.0	1,457	+0.2	22.16	-7:92	0.0	15.70	0.00	12.25	-0.01	18.07	0.00	0.0	18.38	0.00	19.55	0.00
7/7/2004 9:05				<u> </u>		·				Disc	ontinu	e Test or	n S-1									
77772004 0.00	02.00	<u></u>							50				-	1	10	1	70		80		10	05
Distance to Extra	ction <u>We</u>	II S-1							00 10			24 - 44		10 -	40.5	10	- 40		10 - 40.	 5	10	- 35
Screening Interv	al	20 - 4	0 (S-1)						20 - 40			24 - 44	<u> </u>	10-			-10	l . <u> </u>			1	

Notes:

TE - Time Elapsed, hours: minutes

Appl - Applied

Oper - Operating

Vac - Vacuum

DTW - depth to groundwater

" WC - Inches water column

ppmv - parts per million by volume

Temp - Temperature

deg F - degree Farenheit

Ext. - Extraction

cfm - cubic feet per minute

Inf - Influent

DD - Drawdown

GW Ext - Groundwater Extraction

PID - Photo Ionization Detector

All induced vacuum measured in observation wells were in "WC

gpm - gallons per minute

"Hg - Inches Mercury

bgs - below ground surface

TABLE 3 DPE TEST USING WELL MW-3

Former USA Station No. 57 10700 MacArthur Boulevard Oakland, California

	TE	Appl	Air	Totalizer	GW	Inf	Oper				Indu	ed Vacu	um ("W	C) &/or D	TW (fee	t bgs) Da	ita in Ol	servati	on Wells			
Date & Time	1.5	Appl Vac	Flow		Ext Rate		Temp		S-1			S-2		MW		MW			MW-7		MW	/-8
Date & Tille	hh:mm	"Hg		gallons		ppmv	deg F	Vac	DTW	DD	Vac	DTW	DD	DTW	DD	DTW	DD	Vac_	DTW	DD	DTW	DD
7/7/2004 9:25				1 3	<u>, </u>	· · · · · · · · · · · · · · · · · · ·	<u> </u>		S	tart Up	Test us	ing Well	MW-3				_					
7/7/2004 9:25		NM	NM	42,960		NM	NM	NM	NM		NM	22.16		12.26		18.07		NM	18.38		19.55	NM
						0.0	1,450		NM		NM	NM		NM		NM		NM	NM	н	NM	NM
7/7/2004 10:00		24.50	87	42,960	 		<u> </u>						-1.16	<u></u>	0.00	18.06	-0.01	0.0	18.36	-0.02	19.53	-0.02
7/7/2004 10:30	01:05	25.50	87	42,960		0.0	1,447	0.0	19.38		 	21.00		ļ	-							
7/7/2004 11:30	02:05	26.00	87	42,960		0.0	1,456	0.0	19.11	-0.27	+0.2	20.91	-1.25	12.25	0.00	18.06	-0.01	0.0	18.35	-0.03	19.53	-0.02
7/7/2004 11:35	02:10					Discont	inue tes	on MV	γ-3													
<u> </u>					<u> </u>				60			60		17	0	22	0		120		5	i0
Distance to Extra			(B4111 5)	·					20 - 40			20 - 40		10 -	40.5	10 -	40		10 - 40.5		10	- 35
Screening Interva	l	24-44 ((MW-3)_								L——					<u> </u>		1			-	

Notes:

TE - Time Elapsed, hours: minutes

Appl - Applied

Oper - Operating

Vac - Vacuum

DTW - depth to groundwater

" WC - Inches water column

ppmv - parts per million by volume

Temp - Temperature

Ext. - Extraction

deg F - degree Farenheit

cfm - cubic feet per minute

Inf - Influent

DD - Drawdown

GW Ext - Groundwater Extraction

PID - Photo Ionization Detector

All induced vacuum measured in observation wells were in "WC

gpm - gallons per minute

"Hg - Inches Mercury

bgs - below ground surface

TABLE 4 COMBINED DPE TEST USING WELLS S-1, S-2, AND MW-3

Former USA Station No. 57 10700 MacArthur Boulevard Oakland, California

	TE	Appl	Air	Totalizer	GW	Inf	Oper												
Date & Time	,-	Vac	Flow	Reading	Ext Rate	PID	Temp	MV	/-4	MW	1-5	MY	V-6		MW-7			MW-8	
pate & Time	hh:mm	"Hg	cfm	gailons	gpm	ppmv	deg F	DTW	DD	DTW	DD	Vac	DTW	Vac	DTW	DD	Vac	DTW	<u>dd</u>
7/7/2004 11:35							S	art Test	on S-1,	S-2 and N	1W-3				r r	 1			
7/7/2004 11:35	0.00	NM	NM	42,960	NM	NM	NM	12.25		18.06		NM	DRY	NM	18.35		ММ	19.53	
7/8/2004 6:15	18:40	22.25	87	44,610	1.47	4.0	1,460	12.25	0.00	18.11	0.05	0.0	DRY	0.0	18.63	0.28	0.0	19.70	0.17
7/9/2004 6:00	42:25	23.00	86	46,960	0.92	2.3	1,440	12.33	80.0	18.18	0.12	0.0	DRY	0.0	18.72	0.37	0.0	20.02	0.49
7/10/2004 6:00	66:25	23.00	86	48,690	0.43	3.5	1,460	12.41	0.16	18.26	0.2	0.0	DRY	0.0	18.78	0.43	0.0	20.32	0.79
7/11/2004 6:00	90:25	21.00	86	50,760	0.38	3.2	1,456	12.41	0.16	18.27	0.21	0.0	DRY	0.0	18.81	0.46	0.0	20.58	1.05
7/12/2004 6:30		22.50	86	52,780	0.29	3.0	1,453	12.42	0.17	18.32	0.26	0.0	DRY	0.0	18.84	0.49	0.0	20.75	1.22
7/15/2004 6:00		22.50	86	58,760	0.53	4.0	1,446	12.27	0.02	18.36	0.3	0.0	DRY	0.0	18.90	0.55	0.0	21.17	1.64
7/19/2004 5:45		23.25	86	66,320	0.45	3.2	1,459	11.67	-0.58	18.23	0.17	0.0	DRY	0.0	18.98	0.63	0.0	21.50	1.97
7/22/2004 5:45		23.25	86	71,870	0.26	3.0	1,458	12.05	-0.20	18.33	0.27	0.0	DRY	0.0	19.03	0.68	0.0	21.65	2.12
7/25/2004 10:36			<u> </u>	77,720	0.23	Discontinue DPE Test. DPE unit hour meter reading = 1,297.7													
Distance to Nearest		Well	<u> </u>		<u></u>	!		1	10	1	70		110		70			50	
Screening Interval	EXIIdetion							10	- 40,5	10	- 40	10	- 40.5		10 - 40.5	5		10 - 35	

Notes:

TE - Time Elapsed, hours: minutes

Appl - Applied

Oper - Operating

Vac - Vacuum

DTW - depth to groundwater

" WC - Inches water column

ppmv - parts per million by volume

Temp - Temperature

deg F - degree Farenheit

Ext. - Extraction

cfm - cubic feet per minute

Inf - Influent

DD - Drawdown

GW Ext - Groundwater Extraction

PID - Photo Ionization Detector

All induced vacuum measured in observation wells were in "WC

gpm - gallons per minute

"Hg - Inches Mercury

bgs - below ground surface

TABLE 5 SOIL VAPOR ANALYTICAL RESULTS

Former USA Station No. 57 10700 MacArthur Boulevard Oakland, California

Sample Date	Sample Time	Sample ID	Sample Type	TPHG	Benzene	Toluene	Ethyl- benzene	Total Xylenes	МТВЕ
07/06/04	1030	Eff Air	Air	<12	<0.12	<0.12	<0.12	<0.12	<0.12
07/06/04	1032	Inf Cat Air	Air	660	2.1	0.38	1.2	1.1	1.0
07/07/04	0904	Inf Cat Air S-1	Air	<12	<0.12	<0.12	<0.12	<0.12	0.29
07/07/04	1126	Inf Cat Air MW-3	Air	<12	<0.12	<0.12	<0.12	<0.12	0.13
07/19/04	0641	Eff Air	Air	<12	<0.12	<0.12	<0.12	<0.12	<0.12
07/19/04	0644	Inf Cat Air	Air	88	0.26	<0.12	<0.12	0.19	0.25

All air sample values reported in milligrams per cubic meter (mg/m³)

Analytical Laboratory

Alpha Analytical, Inc. (ELAP #2019)

TPHG = Total petroleum hydrocarbons as gasoline

BTEX = Benzene, toluene, ethylbenzene, and total xylenes

MTBE = Methyl tertiary butyl ether

Analytical Methods

TPHG analyzed by EPA Method SW8015B/DHS LUFT Manual

BTEX and MTBE analyzed by EPA Method SW8260B

TABLE 6 GROUNDWATER ANALYTICAL RESULTS

Former USA Station No. 57 10700 MacArthur Boulevard Oakland, California

Sample Date	Sample Time	Sample 1D	Sample Type	трнс	Benzene	Toluene	Ethyl- benzene	Total Xylenes	МТВЕ	ТВА	DIPE	ЕТВЕ	TAME	Methanol	Ethanol
07/06/04	1050	S-2	Water	2200	13	1.8	10	26,9	66	170	<1.0	<1.0	<1.0	<5,000	<5,000
07/08/04	0854	Influent	Water	<100[1]	<0.50	<0.50	0.66	4.4	16	NA	NA	NA	NA	NA NA	NA
07/08/04	0905	GAC Influent	Water	110	<0.50	<0.50	<0.50	1.89	17	NA	NA	NA	NA	NA	NA
07/08/04	1030	Effluent	Water	<50	<0.50	<0.50	<0.50	<0.50	<0.50	NA	NA	NA	NA	NA	NA
07/19/04	0623	Effluent	Water	<50	<0.50	<0.50	<0.50	<0.50	<0.50	<10	<1.0	<1.0	<1.0	NA	NA
07/19/04	0630	Influent	Water	<50	<0.50	<0.50	<0.50	0.52	3.7	56	<1.0	<1.0	<1.0	NA	NA
07/27/04	1118	Effluent	Water	<50	<0.50	<0.50	<0.50	<0.50	<0.50	<10	<1.0	<1.0	<1.0	NA	NA

All water sample values reported in micrograms per liter (µg/L)

TPHG = Total petroleum hydrocarbons as gasoline

BTEX = Benzene, toluene, ethylbenzene, and total xylenes

MTBE = Methyl tertiary butyl ether

TBA = Tertiary butyl alcohol

DIPE = Di-isopropyl ether

ETBE = Ethyl tertiary butyl ether

TAME = Tertiary amyl methyl ether

NA = Not analyzed

[1] Reporting limits were increased due to sample foaming

Analytical Laboratory

Alpha Analytical , Inc. (ELAP #2019)

Analytical Methods

TPHG analyzed by EPA Method SW8015B/DHS LUFT Manual

BTEX, MTBE, TBA, DIPE, ETBE, & TAME analyzed by EPA Method SW8260B $\,$

Methanol & Ethanol analyzed by EPA Method SW8260B-DI

TABLE 7 PETROLEUM HYDROCARBON MASS EXTRACTION RATES SUMMARY

Former USA Station No. 57 10700 MacArthur Boulevard Oakland, California

	Test Well		Influe	ent Concer	itration		Soil Vapor			ntive Mass Removed
Date	ID	Flowrate		(mg/m	3)	w	ells (lbs/da	ay)	Period ¹	Total
		(cfm)	TPHG	Benzene	MTBE	TPHG	Benzene	MTBE	lbs	lbs
07/06/04	S-2	87.0	660	2.1	1.0	5.16	0.01	0.01	5.16	5.16
07/07/04	S-1	87.0	<12	<0.12	0.29	<0.09	<0.001	0.002	0.01	5.17
07/07/04	MW-3	87.0	<12	<0.12	0.13	<0.09	<0.001	0.001	0.01	5.18
07/19/04	S-1, S-2, MW-3	86.0	88	0.26	0.25	0.68	0.002	0.002	8.16	13.34
		Volume of		. ~		3.5	T		l	tive Mass
	Test Well	groundwater	Influe	nt Concen	itration		Extracted		'	Removed
Date	ID	extracted ² ,		(µg/L)			ındwater (lbs)	Period	Total
		gallons	TPHG	Benzene	MTBE	TPHG	Benzene	MTBE	lbs	lbs
									•	
07/06/04	S-2	80	2,200	13	66	0.001	0.00001	0.00004	0.001	0.001
07/08/04	S-1, S-2, MW-3	2,490	<100	<0.50	16	<0.002	<0.00001	0.0003	0.012	0.014
07/19/04	S-1, S-2, MW-3	21,710	<50	<0.50	4	< 0.01	<0.0001	0.001	0.008	0.015

Sample Calculations

Ext. Rate from = $\frac{40 \text{ cu ft x}}{\text{min}}$ = $\frac{8,400 \text{ mg}}{\text{cu meter}}$ = $\frac{16}{3593}$ mg day = $\frac{\text{x cu meter}}{35.314 \text{ cu ft}}$

= 30.21 <u>lbs/day</u>

Mass removed = concentration (μ g/L) x gallons extracted x (2.2046 x 10- 9)(lb/mg) / 0.26418 (gal/L) from groundwater

Based on average groundwater extraction rate of 0.63 gpm and the average concentrations, the mass extraction rate for is calculated using:

Mass removed from = concentration (μg/L) x average flowrate (gpm) x (2.2046 x 10-9)(lb/mg) / 0.26418 (gal/L) groundwater (lbs/day) * 60 (mins/hr)*24 (hr/day)

 $\begin{array}{lll} \text{TPHG} & = & 0.017 & \text{lbs/day} \\ \text{Benzene} & = & 0.0001 & \text{lbs/day} \\ \text{MTBE} & = & 0.0002 & \text{lbs/day} \end{array}$

For mass estimates between the sampling dates, average mass extraction rate and time elapsed (operational uptime) between the sampling events were used

² Volume estimated based on flow totalizer measurements taken on the sampling days

Figure 3

Depth to Water Variation with Time in Observation Wells - DPE Test at S-2

Former USA Station No. 57

10700 MacArthur Boulevard

Oakland, California

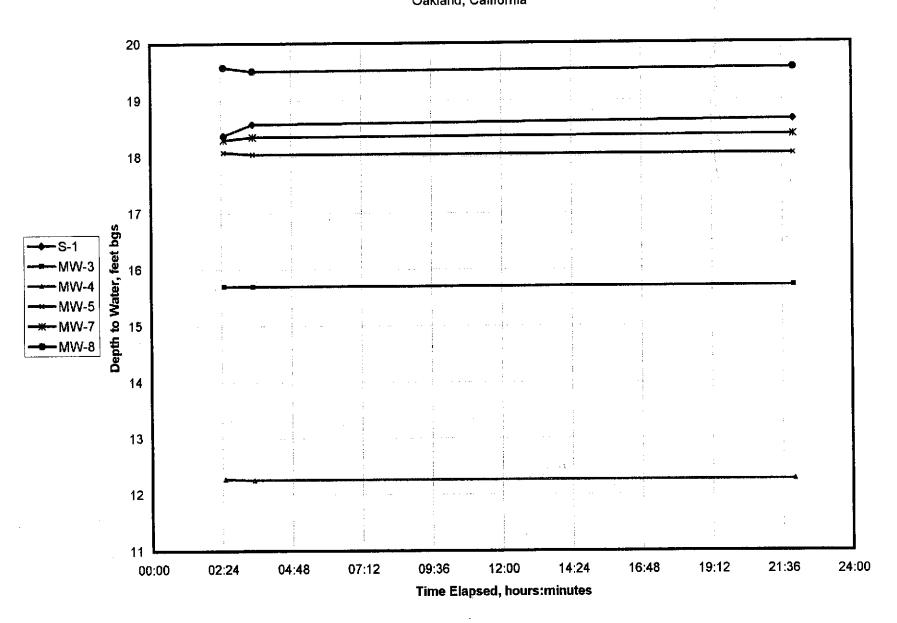


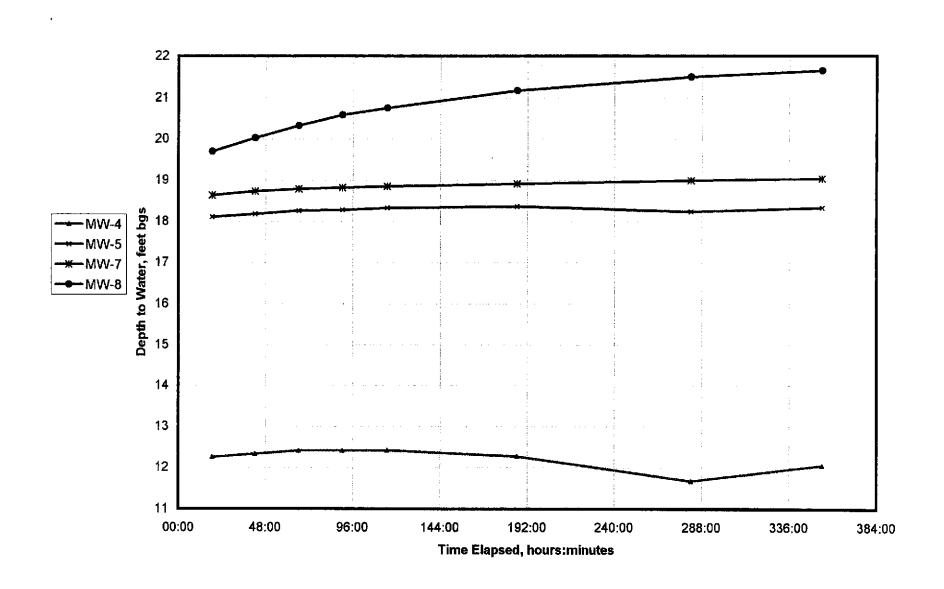
Figure 4

Depth to Water Variation with Time in Observation Wells - Combined DPE Test

Former USA Station No. 57

10700 MacArthur Boulevard

Oakland, CA



APPENDIX K WELL SURVEY DATA

TABLE 1

WELLS WITHIN 1/2-MILE RADIUS USA STATION #57 OAKLAND, CALIFORNIA

Map ID		Owner	Well Address	DWR	Year	
					100	
1 1	MW	Southland	10501 Foothills	2 S 3 W 24 E (3-5)	1987	
2	MW		10600 MacArthur	2 S 3 W 24 E 11	1992	I see the
3	MW.		106th	,	1951	28-85'
4	MW	Programme and the second	Micrella (Characha) 1 1 1 5	2 S 3 W 24 M	4.87	the first to the
5	IW	Bull 868 (22 Pt. 13 13 18 18 18 18 18 18 18 18 18 18 18 18 18	2544 109th	2 S 3 W 24 M 1	è ·	38-55
6	A	Unocal	96 MacArthur	A DESCRIPTION OF THE PROPERTY	a Sile Light for a Sile Light Sile Sile	Unknown
7	IW		377 Hollister	2 S 3 W 24 N 1	1971	35-75
8		PG&E	Sunnyside 75' SW of 104th	2 S 3 W 23 K 1	1974	120' 144' 465' 386
9	1 :	PG&E	Shaw & Stanley	2 S 3 W 24 E 2	1976	120'
10	DW		Stella & Malcolm	2 S 3 W 24 B 5	1955	55-123'
11			10700 Stella	2 S 3 W 24 B 2	1951	55'
12		The second secon	10731 Mark	2 S 3 W 24 B 1	1951	102'
13	DW		Mark	2 S 3 W 24 B 3	in taki	100' %
14		l a company of the co	10544 Stella	2 S 3 W 24 C 3		42-92'
15			Mark & Hood	2 S 3 W 24 B	1958	56-107'
16 17	ÞΨ		Malcolm & Stella	2 S W W 24	* * * * * * * * * * * * * * * * * * *	100'
18			10521 Stella	S 2 3 W 24 C	5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Unknown
19		R. Trimble	10520 Stella	2 \$ 3 W 24 C		190'
20			10550 Stella	2 S 3 W 24 C		Unknown
			10600 Stella	2 S 3 W 24 B 4	1 Tel 1 1 2	98'
	CFW	ruae -	Voltaire & 108th	2 S S W 23 J 1		105'

MW Monitoring well
DW Domestic well

CW Cathodic protection well

The state of the control of the cont

IW Irrigation well

G:\data\5090\Search.wbI

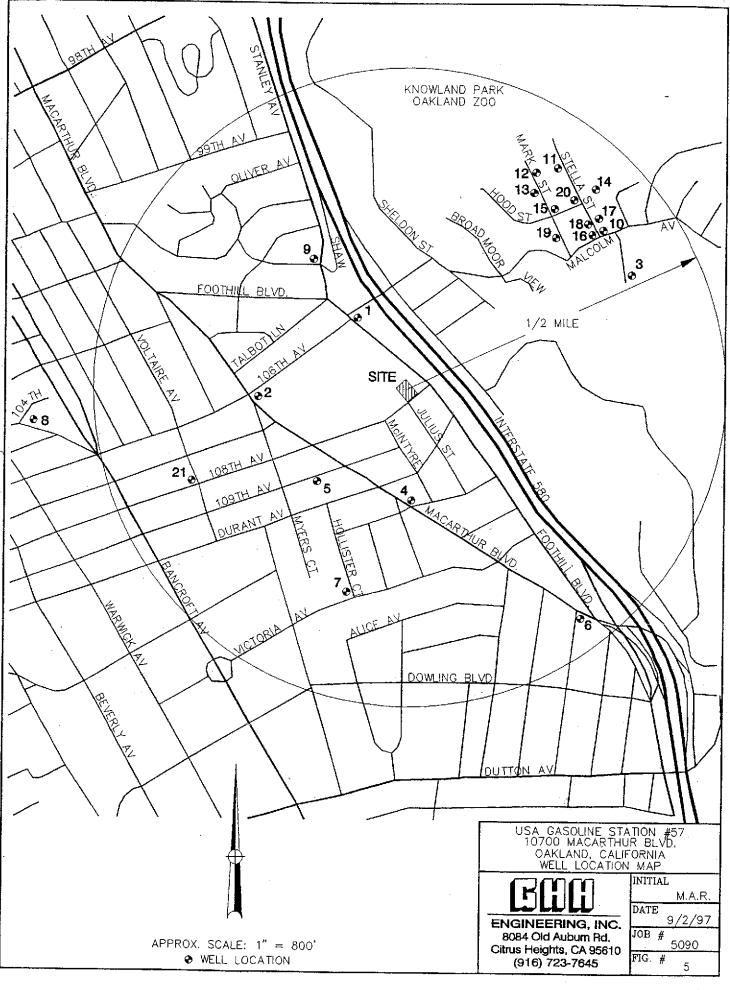


FIGURE B

APPENDIX L DOMINICO GROUNDWATER MODEL OUTPUT

DOMINICO MODEL FOR CALCULATING CONCENTRATIONS OF IMPACTED GROUNDWATER AT STEADY STATE

Directions: input all data requested in unshaded areas

Benzene Concentration	Distance to Nearest Recentor	Decay Rate	Groundwater Velocity	Width of impacted soil	Depth of impacted soil	in the Y	in the Z	of dispersion in	
(ug/l) 5,700	(feet) 1,800	(/days) 0.0009	(feet/year)	(feet)	(feet) 40	erf()	erf()	the Y Direction 0.0172	0.0626

aipha?	C (feet)	180
alpha '	(feet)	60.00
alpha 2	C (feet)	18
Groun		
	ocity	0.0274
(feet	'day')	

- *At steady state the concentration of benzene at the nearest receptor will be approximately 1.50E-08 ug/l
- *If the decay is assumed to be first order reaction then the approx. time to reach steady state will be 81 years

ASSUMPTIONS - one-dimensional flow and 3-dimensional dispersion

- first-order decay rate based on dissolved and adsorbed phases decaying at the same rate
- medium is isotropic and homogeneous
- source concentration is constant
- aerial source perpendicular to the direction of flow

Source: Gitt Engineering, Inc., Closure Information Proposal (dated April, 2002)

APPENDIX M RWQCB ESL TABLES

TABLE A. ENVIRONMENTAL SCREENING LEVELS (ESLs) Shallow Soils (≤3m bgs) Groundwater IS Current or Potential Source of Drinking Water

	¹ Shall	ow Soil	³Groundwater (ug/L)	
CHEMICAL PARAMETER	² Residential Land Use (mg/kg)	Commercial/ Industrial Land Use Only (mg/kg)		
ACENAPHTHENE	1.6E+01	1.6E+01	2.0E+01	
ACENAPHTHYLENE	1.3E+01	1.3E+01	3.0E+01	
ACETONE	5.0E-01	5.0E-01	1.5E+03	
ALDRIN	3.2E-02	1.3E-01	2.0E-03	
ANTHRACENE	2.8E+00	2.8E+00	7.3E-01	
ANTIMONY	6.1E+00	4.0E+01	6.0E+00	
ARSENIC	5.5E+00	5.5E+00	3.6E+01	
BARIUM	7.5E+02	1.5E+03	1.0E+03	
BENZENE	4.4E-02	4.4E-02	1.0E+00	
BENZO(a)ANTHRACENE	3.8E-01	1.3E+00	2.7E-02	
BENZO(b)FLUORANTHENE	3.8E-01	1.3E+00	2.9E-02	
BENZO(k)FLUORANTHENE	3.8E-01	1.3E+00	2.9E-02	
BENZO(g,h,i)PERYLENE	2.7E+01	2.7E+01	1.0E-01	
BENZO(a)PYRENE	3.8E-02	1.3E-01	1.4E-02	
BERYLLIUM	4.0E+00	8.0E+00	2.7E+00	
BIPHENYL, 1,1-	6.5E-01	6.5E-01	5.0E-01	
BIS(2-CHLOROETHYL)ETHER	1.8E-04	1.8E-04	1.4E-02	
BIS(2-CHLOROISOPROPYL)ETHER	5.4E-03	5.4E-03	5.0E-01	
BIS(2-ETHYLHEXYL)PHTHALATE	6.6E+01	6.6E+01	4.0E+00	
BORON	1.6E+00	2.0E+00	1.6E+00	
BROMODICHLOROMETHANE	1.4E-02	3.9E-02	1.0E+02	
BROMOFORM	2.2E+00	2.2E+00	1.0E+02	
BROMOMETHANE	2.2E-01	3.9E-01	9.8E+00	
CADMIUM	1.7E+00	7.4E+00	1.1E+00	
CARBON TETRACHLORIDE	1.2E-02	3.4E-02	5.0E-01	
CHLORDANE	4.4E-01	1.7E+00	4.0E-03	
CHLOROANILINE, p-	5.3E-02	5.3E-02	5.0E+00	
CHLOROBENZENE	1.5E+00	1.5E+00	2.5E+01	
CHLOROETHANE	6.3E-01	8.5E-01	1.2E+01	
CHLOROFORM	8.8E-01	1.9E+00	7.0E+01	
CHLOROMETHANE	7.0E-02	2.0E-01	1.3E+00	
CHLOROPHENOL, 2-	1.2E-02	1.2E-02	1.8E-01	
CHROMIUM (Total)	5.8E+01	5.8E+01	5.0E+01	
CHROMIUM III	7.5E+02	7.5E+02	1.8E+02	
CHROMIUM VI	1.8E+00	1.8E+00	1.1E+01	
CHRYSENE	3.8E+00	1.3E+01	2.9E-01	
COBALT	1.0E+01	1.0E+01	3.0E+00	
COPPER	2.3E+02	2.3E+02	3.1E+00	
CYANIDE (Free)	3.6E-03	3.6E-03	1.0E+00	
DIBENZO(a,h)ANTHTRACENE	1.1E-01	3.8E-01	8.5E-03	
DIBROMOCHLOROMETHANE	1.9E-02	5.4E-02	1.0E+02	
1.2-DIBROMO-3-CHLOROPROPANE	4,5E-03	4.5E-03	2.0E-01	
DIBROMOETHANE 1,2-	3.3E-04	3.3E-04	5.0E-02	
DICHLOROBENZENE, 1,2-	1.1E+00	1.1E+00	1.0E+01	

TABLE A. ENVIRONMENTAL SCREENING LEVELS (ESLs) Shallow Soils (≤3m bgs) Groundwater IS Current or Potential Source of Drinking Water

	¹ Shallow Soil			
CHEMICAL PARAMETER	² Residential Land Use (rng/kg)	Commercial/ Industrial Land Use Only (mg/kg)	³ Groundwater (ug/L)	
DICHLOROBENZENE, 1,3-	7.4E+00	7.4E+00	6.5E+01	
DICHLOROBENZENE, 1,4-	4.6E-02	1.3E-01	5.0E+00	
DICHLOROBENZIDINE, 3,3-	7.7E-03	7.7E-03	2.9E-02	
DICHLORODIPHENYLDICHLOROETHANE (DDD)	2.3E+00	9.0E+00	1.0E-03	
DICHLORODIPHENYLDICHLOROETHYLENE (DDE)	1.6E+00	4.0E+00	1.0E-03	
DICHLORODIPHENYLTRICHLOROETHANE (DDT)	1.6E+00	4.0E+00	1.0E-03	
DICHLOROETHANE, 1,1-	2.0E-01	2.0E-01	5.0E+00	
DICHLOROETHANE, 1,2-	4.5E-03	4.5E-03	5.0E-01	
DICHLOROETHYLENE, 1,1-	1.0E+00	1.0E+00	6.0E+00	
DICHLOROETHYLENE, Cis 1,2-	1.9E-01	1.9E-01	6.0E+00	
DICHLOROETHYLENE, Trans 1,2-	6.7E-01	6.7E-01	1.0E+01	
DICHLOROPHENOL, 2,4-	3.0E-01	3.0E-01	3,0E-01	
DICHLOROPROPANE, 1,2-	5.1E-02	1.2E-01	5.0E+00	
DICHLOROPROPENE, 1,3-	3.3E-02	5.9E-02	5.0E-01	
DIELDRIN	2.3E-03	2.3E-03	1.9E-03	
DIETHYLPHTHALATE	3.5E-02	3.5E-02	1.5E+00	
DIMETHYLPHTHALATE	3.5E-02	3.5E-02	1.5E+00	
DIMETHYLPHENOL, 2,4-	6.7E-01	6.7E-01	1.0E+02	
DINITROPHENOL, 2,4-	4.0E-02	4.0E-02	1.4E+01	
DINITROTOLUENE, 2,4-	8.5E-04	8.5E-04	1.1E-01	
1,4 DIOXANE	1.8E-03	1.8E-03	3.0E+00	
DIOXIN (2,3,7,8-TCDD)	4.6E-06	1.9E-05	5.0E-06	
ENDOSULFAN	4.6E-03	4.6E-03	8.7E-03	
ENDRIN	6.5E-04	6.5E-04	2.3E-03	
ETHANOL	4.5E+01	4.5E+01	5,0E+04	
ETHYLBENZENE	3.3E+00	3.3E+00	3.0E+01	
FLUORANTHENE	4.0E+01	4.0E+01	8.0E+00	
FLUORENE	8.9E+00	8.9E+00	3.9E+00	
HEPTACHLOR	1.4E-02	1.4E-02	3.8E-03	
HEPTACHLOR EPOXIDE	1.5E-02	1.5E-02	3.8E-03	
HEXACHLOROBENZENE	2.7E-01	9.6E-01	1.0E+00	
HEXACHLOROBUTADIENE	1.0E+00	1.0E+00	2.1E-01	
HEXACHLOROCYCLOHEXANE (gamma) LINDANE	4.9E-02	4.9E-02	8.0E-02	
HEXACHLOROETHANE	2.4E+00	2.4E+00	7.0E-01	
INDENO(1,2,3-cd)PYRENE	3.8E-01	1.3E+00	2.9E-02	
LEAD	1.5E+02	7.5E+02	2.5E+00	
MERCURY	3.7E+00	1.0E+01	1.2E-02	
METHOXYCHLOR	1.9E+01	1.9E+01	1.9E-02	
METHYLENE CHLORIDE	7.7E-02	7.7E-02	1.9E-02 5.0E+00	
METHYL ETHYL KETONE	3.9E+00	3.9E+00	4.2E+03	
METHYL ISOBUTYL KETONE	2.8E+00			
METHYL MERCURY	1.2E+00	2.8E+00	1.2E+02	
METHYLNAPHTHALENE (total 1- & 2-)		1.0E+01	3.0E-03	
METHYL TERT BUTYL ETHER	2.5E-01	2.5E-01	2.1E+00	
WEITHEREN	2.3E-02	2.3E-02	5.0E+00	

TABLE A. ENVIRONMENTAL SCREENING LEVELS (ESLs) Shallow Soils (≤3m bgs) Groundwater IS Current or Potential Source of Drinking Water

	¹ Shall	low Soil			
CHEMICAL PARAMETER	² Residential Land Use (mg/kg)	Commercial/ Industrial Land Use Only (mg/kg)	³ Groundwater (ug/L)		
MOLYBDENUM	4.0E+01	4.0E+01	3.5E+01		
NAPHTHALENE	4.6E-01	1.5E+00	1.7E+01		
NICKEL	1.5E+02	1.5E+02	8.2E+00		
PENTACHLOROPHENOL	4.4E+00	5.0E+00	1.0E+00		
PERCHLORATE	1.0E-02	1.0E-02	6.0E+00		
PHENANTHRENE	1.1E+01	1.1E+01	4.6E+00		
PHENOL	7.6 E-0 2	7.6E-02	5.0E+00		
POLYCHLORINATED BIPHENYLS (PCBs)	2.2E-01	7.4E-01	1.4E-02		
PYRENE	8.5E+01	8.5E+01	2.0E+00		
SELENIUM	1.0E+01	1.0E+01	5.0E+00		
SILVER	2.0E+01	4.0E+01	1.9E-01		
STYRENE	1.5E+00	1.5E+00	1.0E+01		
tert-BUTYL ALCOHOL	7.3E-02	7.3E-02	1.2E+01		
TETRACHLOROETHANE, 1,1,1,2-	2.4E-02	2.4E-02	1.3E+00		
TETRACHLOROETHANE, 1,1,2,2-	9.1E-03	1.8E-02	1.0E+00		
TETRACHLOROETHYLENE	8.7E-02	2.4E-01	5.0E+00		
THALLIUM	1.0E+00	1.3E+01	2.0E+00		
TOLUENE	2.9E+00	2.9E+00	4.0E+01		
TOXAPHENE	4.2E-04	4.2E-04	2.0E-04		
TPH (gasolines)	1.0E+02	1.0E+02	1.0E+02		
TPH (middle distillates)	1.0E+02	1.0E+02	1.0E+02		
TPH (residual fuels)	5.0E+02	1.0E+03	1.0E+02		
TRICHLOROBENZENE, 1,2,4-	3.8E-01	1.0E+00	2.5E+01		
TRICHLOROETHANE, 1,1,1-	7.8E+00	7,8E+00	6.2E+01		
TRICHLOROETHANE, 1,1,2-	3.2E-02	7.0E-02	5.0E+00		
TRICHLOROETHYLENE	2.6E-01	4.6E-01	5.0E+00		
TRICHLOROPHENOL, 2,4,5-	1.8E-01	1.8E-01	1.1E+01		
TRICHLOROPHENOL, 2,4,6-	1.7E-01	1.7E-01	5.0E-01		
VANADIUM	1.1E+02	2.0E+02	1.5E+01		
VINYL CHLORIDE	6.7E-03	1.9E-02	5.0E-01		
XYLENES	2.3E+00	2.3E+00	2.0E+01		
ZINC	6.0E+02	6.0E+02	8.1E+01		

TABLE A. ENVIRONMENTAL SCREENING LEVELS (ESLs) Shallow Soils (≤3m bgs)

Groundwater IS Current or Potential Source of Drinking Water

	¹ Shallow Soil			
CHEMICAL PARAMETER	² Residential Land Use (mg/kg)	Commercial/ Industrial Land Use Only (mg/kg)	³Groundwater (ug/L)	
Electrical Conductivity (mS/cm, USEPA Method 120.1 MOD)	2.0	4.0	not applicable	
Sodium Adsorption Ratio	5.0	12	not applicable	

Red: Updated with respect to ESLs presented in July 2003 document.

Notes:

- 1. Shallow soils defined as soils less than or equal to 3 meters (approximately 10 feet) below ground surface.
- 2. Category "Residential Land Use" generally considered adequate for other sensitive uses (e.g., day-care centers, hospitals, etc.)
- Assumes potential discharge of groundwater into a freshwater, marine or estuary surface water system.

Source of soil ESLs: Refer to Appendix 1, Tables A-1 and A-2.

Source of groundwater ESLs: Refer to Appendix 1, Table F-1a.

Soil data should be reported on dry-weight basis (see Appendix 1, Section 6.2).

Soil ESLs intended to address direct-exposure, groundwater protection, ecologic (urban areas) and nuisance concerns under noted land-use scenarios. Soil gas data should be collected for additional evaluation of potential indoor-air impacts at sites with significant areas of VOC-impacted soil. See Section 2.6 and Table E.

Groundwater ESLs intended to be address drinking water, surface water, indoor-air and nuisance concerns. Use in conjunction with soil gas screening levels to more closely evaluate potential impacts to indoor-air if groundwater screening levels for this concern approached or exceeded (refer to Section 2.6 and Appendix 1, Table F-1a).

Aquatic habitat goals for bioaccumulation concerns not considered in selection of groundwater goals (refer to Section 2.7).

Refer to appendices for summary of ESL components.

Soil and water ESLs for ethanol based on gross contamination concerns (see Appendix 1, Chapter 5 and related tables).

TPH -Total Petroleum Hydrocarbons. TPH ESLs must be used in conjunction with ESLs for related chemicals (e.g., BTEX, PAHs, oxidizers, etc.). See Volume 1, Section 2.2 and Appendix 1, Chapter 5.