

3315 Almaden Expressway, Suite 34 San Jose, CA 95118 Phone: (408) 264-7723 FAX: (408) 264-2435

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August 18, 1993 0811BCHA.4494

Mr. Barney Chan Alameda County Health Care Services Agency 80 Swan Way, Room 200 Oakland, California 94624

Subject:

Response to Your Letter Dated May 24, 1993 Concerning the Report of Findings Underground Gasoline Tank Removal and Replacement at ARCO Station 4494, 566 Hegenberger Road, Oakland, California.

Mr. Chan:

On behalf of Arco Products Company (ARCO) this letter is written in response to your letter dated May 24, 1993 (Attachment A) concerning the Report of Findings Underground Gasoline Tank Removal and Replacement (Tank Report) at ARCO Station 4494, 566 Hegenberger Road, Oakland, California. The following paragraphs specifically address ARCO's response to Items 1 through 4 of your letter.

ARCO Responses

1. The "hydrocarbon fingerprinting analyses data" you requested in Item 1 of your letter (Attachment A) was submitted to your office in May 1993 as "Appendix H - Fingerprint Analytical Reports" of the Report of Findings Underground Gasoline Tank Removal and Replacement. These analyses were performed by Core Laboratories in Long Beach, California and ARCO Petroleum Products Company Laboratory in Carson, California. Copies of the analytical reports are included in Attachment B of this letter.

The second comment in Item 1 of your letter requested that your office be informed how any release from the former tanks will be distinguished from that of the black hydrocarbon product. RESNA does not anticipate it will be necessary to distinguish the released gasoline from the black hydrocarbon product because 1) source removal



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of gasoline impacted soil occurred on December 17 and 18, 1992 and 2) a slurry wall has been constructed to mitigate the flow of black hydrocarbon product into the former tank pit.

- 1) ARCO conducted a remedial excavation of gasoline impacted soils, subsequent to discovery of a release of gasoline hydrocarbons from the former underground storage tanks. Laboratory results of soil samples collected from the former gasoline tank pit to verify removal of impacted soil indicated TPHg concentrations ranging from 2 parts per million (ppm) to 33 ppm (RESNA, May 17, 1993).
- 2) ARCO has constructed a slurry wall as a barrier between the storm drain backfill and the former tank pit backfill. The slurry wall is located along the northeastern portion of the former tank pit parallel to the storm drain to mitigate the flow of black hydrocarbon product into the backfilled former tank pit.

However, if the black hydrocarbon product needs to be distinguished from the gasoline, both compounds have separate characteristics and can be identified by field observations and laboratory analyses. The black hydrocarbon product is characterized as a hydrocarbon compound that is significantly heavier than the gasoline generated from the former tanks and physically appears black. The following three paragraphs explain the results of laboratory analyses of the black hydrocarbon product collected from a "grab" water sample.

As stated in RESNA's Tank Report, the black hydrocarbon product observed seeping into the northeastern corner of the former tank pit during remedial excavation activities appears to have migrated from an offsite source through the sand and gravel trench backfill material of a 6-feet-diameter storm drain. The black hydrocarbon product was visibly different then the gasoline impacted soils observed in the field. It appeared that the black hydrocarbon product was ponding on groundwater in the bottom of the tank pit. As requested by your office, a "grab" water sample was collected from the bottom of the tank pit and submitted for analyses. ARCO submitted a split "grab" water samples TP-2s and TP-2b to Core Laboratories and ARCO's Laboratory for fingerprinting analyses.

As presented in Core Laboratories analytical report, the simulated distillation test method used on split sample TP-2s, collected from the former tank pit, identified the black hydrocarbon compound as being heavier than gasoline. According to Greg Cook of Core Laboratories (personal communication, August 1993), the initial



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boiling point for the black hydrocarbon compound was 200 degrees Fahrenheit, which is significantly higher than the typical gasoline initial boiling point of 90 to 100 degrees Fahrenheit (Attachment C). Core Laboratories Sample 930006-1 Distillation Profile included in the Tank Report and attached as Attachment B, includes a graph showing the Percent Evaporated versus Temperature for the subject compound. As seen in the graph, the black hydrocarbon compound (sample 930006-1) initially evaporates at temperatures equivalent to Jet-A fuel and #2 diesel fuel. After reaching a temperature of approximately 500 degrees Fahrenheit, the compound begins to simulate a profile more equivalent to motor oil.

Based on the results generated at ARCO's laboratory, the black hydrocarbon product (split sample TP-2S) did not resemble any of ARCO's finished products.

Additionally, laboratory results of soil samples collected from boring B-1, drilled in the immediate vicinity of the former waste oil tank (removed in December 1989), indicated Oil and Grease concentrations attenuating with depth to levels below laboratory detection limits.

Based on the above fingerprinting analytical results and field activities, gasoline hydrocarbons released from the former tanks appears to have been remediated during tank removal operations and does not appear to be present in the "grab" water sample collected from the bottom of the former tank pit.

- 2. As discussed in our telephone conversation on June 30, 1993 and RESNA's Follow-up letter dated July 13, 1993 (Attachment D), ARCO will not replace MW-2 but instead will use monitoring wells MW-5 and MW-6 to evaluate groundwater downgradient of the former tank pit.
- 3. Recovery well RW-1 will be monitored on a monthly basis for the presence of free product. If during the monitoring period free product is detected, ARCO will implement procedures to remove the free product at that time.
- 4. RESNA recommended this site for alternative points of compliance based on the following:
 - Based on site specific subsurface data from previous environmental investigations at the site and published geologic literature the site is underlain by water bearing soils that typically produce low yielding wells. The subject



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site is located along the eastern margin of San Francisco Bay within the East Bay Plain. The site and vicinity were formerly occupied by shallow tidal marshes, and a channelized tidal slough is still located directly west of the site, across Hegenberger Road. Helley and others (1979) mapped the earth materials underlying the site area as being Holocene bay mud estuarine deposits composed of unconsolidated, water-saturated, dark plastic clay and silty clay rich in organic materials, with local lenses and stringers of well-sorted silt, fine sand, and peat. These estuarine materials, known locally as Bay Mud, were deposited primarily in brackish- to salt-water marshes along the margins and beneath the waters of San Francisco Bay during interglacial periods before and after the Wisconsin Glaciation in late Pleistocene time (Goldman, 1969).

The Bay Mud acts as a barrier to the vertical movement of salt water from San Francisco Bay into the older alluvium. The Bay Mud is generally water-saturated because most of it lies below the water table. However, it is not considered as a useable source of groundwater to wells because of its low permeability and because it is believed to contain mostly salt water (Hickenbottom and Muir, June 1988).

- Source removal was conducted during tank removal and replacement operations. The former tanks and product lines were removed in December 1992. Gasoline impacted soil was excavated and removed from the site during remedial activities.
- Analytical results of groundwater samples from groundwater monitoring wells located upgradient, crossgradient and downgradient of the former tank pit and product lines indicated TPHg and BTEX concentrations were less than laboratory detection limits.
- Because typical Bay Muds possess low permeability and when saturated produce low yielding wells remedial technologies such as pump-and-treat, vapor extraction and air sparging do not appear to be feasible at this site.
- RESNA recommends that quarterly groundwater monitoring continue to evaluate TPHg and BTEX concentrations across the site.



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If you have any questions or comments concerning this matter, please contact us at (408) 264-7723.

Sincerely,

RESNA Industries Inc.

John C. Young

Project Manager

cc:

Mr. Michael Whelan, ARCO Products Company

Mr. Britt Johnson, ACHCSA

encl: References

Attachment A - Letter from the ACHCSA to ARCO dated May 24, 1993

Attachment B - Fingerprint Analyses Reports Attachment C - Core Laboratory Facsimile

Attachment D - RESNA Follow-up Letter to ACHCSA dated July 13, 1993



REFERENCES

- Goldman, Harold B. 1969. Geology of San Francisco Bay, Alameda County, California. California Division of Mines and Geology Special Report 97, pgs. 9 27.
- Helley, E. S., K. R. Lajoie, W. E. Spangle, and M. L. Blair. 1979. <u>Flatland Deposits of the San Francisco Bay Region, California</u>, U.S. Geological Survey Professional Paper 943.
- Hickenbottom, Kelvin, and Muir, Kenneth. June 1988. Geohydrology and Groundwater Quality Overview of the East Bay Plain Area, Alameda County, California. Alameda County Flood Control and Water Conservation District Report 205 (J).
- RESNA. May 17, 1993. Report of Findings Underground Gasoline-Storage Tank Removal and Replacement at ARCO Station 4494, 566 Hegenberger Road in Oakland, California. RESNA Report 69038.13.

ATTACHMENT A LETTER FROM THE ACHCSA TO ARCO (DATED MAY 24, 1993)

ALAMEDA COUNTY HEALTH CARE SERVICES AGENCY

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DAVID J. KEARS, Agency Director

May 24, 1993 StID # 3854

Mr. Michael Whelan ARCO Products Company P.O. Box 5811 San Mateo, CA 94402

A RAPATIA, SHAHID, ASST AGENCY DIRECTOR.

DEPARTMENT OF EILL BURNMENTAL HEALTH. State Matt.: Basources Control Board.

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Carland, CA 94691

(510) 271-4530

Re: Comment on May 17, 1993 Report of Findings Underground Gasoline Tank Removal and Replacement at 566 Hegenberger Rd., Oakland CA 94621

Dear Mr. Whelan:

Our office has received and reviewed the above referenced report as prepared by Resna for ARCO. We would like to comment on the conclusions and recommendations which follow the text of the report.

- The last point of the Conclusion section states that the black hydrocarbon product does not resemble any of ARCO's finished products. Please provide the "hydrocarbon fingerprinting analyses data" which documents this conclusion. Please also inform our office how any release from the former tanks (TPHg and BTEX) will be distinguished from that of the black hydrocarbon product.
- The first point of the Recommendations states that MW-2, the decommissioned well, will be replaced with a 4-inch well in the area of this former well. Please insure that this well is installed into native soils as oppose to backfilled materials.
- The second point of the Recommendations referrs to RW-1, the recovery well installed between the slurry wall and the storm drain. Please verify that in addition to monitoring for the presence of the black hydrocarbon on a monthly basis, you will also take steps to remove all free product at the same time.
- The third point of the Recommendations states that this site may qualify for alternate points of compliance. Please verify that the conditions necessary for this remedial approach exist at this site ie low yielding soils exist, alternate or best available technologies are inappropriate or not cost-effective and that an acceptable plan for containing and managing the remaining contamination exists. (It is acknowledged that adequate source removal has already been done). Given the previous groundwater gradient determined for this site, additional well(s) may be appropriate at compliance points on-site to monitor any groundwater impact from the former dispenser islands.

Mr. Michael Whelan StID #3854 566 Hegenberger Rd. May 24, 1993 Page 2.

Please provide written comment to the above items to our office. This may be included in separate letter or included as a signed letter attached to your next quarterly monitoring report for this site.

You may contact me at (510) 271-4530 if you have any questions.

Sincerely,

Barney M. Chan

Hazardous Materials Specialist

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cc: G. Jensen, Alameda County District Attorney Office

R. Hiett, RWQCB

J. Young, RESNA, 3315 Almaden Expressway, Suite 34, San Jose, CA 95118

E. Howell, files

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ATTACHMENT B FINGERPRINT ANALYSES REPORTS

APPENDIX H FINGERPRINT ANALYTICAL REPORTS

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Sample I.D.	Lab no.	Container no.	Soil	Water			Acid	Sampling date	Sampling time	BTEX 602/EPA 8020	BTEX/TPH EPA M602/8020	TPH Modified 80 Gas T Diesel	Oil and Greese 413.1 🗀 413.2	TPH EPA 418.1/SMS	EPA 601/8010	EPA 624/8240	EPA 625/8270	TCLP Semi	CAM Metals EPA TTLC STL(Lead Org./DHS Lead EPA 7420/7421	がまりは、おいまり	Special detection
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CORE LABORATORIES
ANALYTICAL REPORT

Job Number: 930006 Prepared For:

RESNA Company Robert D. Campbell 3315 Almaden Expressway, Suite 34 San Jose, CA 95118

Date: 01/05/93

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Signature

Name: Ryan S. Nakatani

Core Laboratories - Long Beach

3700 Cherry Avenue

Long Beach, CA 90807

Title: Laboratory Supervisor



RESULTS LABORATORY TESTS

01/05/93

JOB NUMBER: 930006 CUSTOMER: RESNA Company ATTN: Robert D. Campbell

CLIENT 1.D..... TP-25 DATE \$AMPLED....: 12/28/92 LABORATORY I.D...: 930006-0001 DATE RECEIVED: 12/31/92

TIME SAMPLED.....: 07:00 WORK DESCRIPTION...: TP-25

TIME RECEIVED...: :
REMARKS....... 3 - 40 mt vials

EST DESCRIPTION	FINAL RESULT	LIMITS/*DILUTION	UNITS OF MEASURE	TEST METHOD	DATE	TECH
imulated Distillation, Distillate		*1		ASTM D-2887	01/05/93	FA
IBP	215	1	Deg F	ASTM D-2887	-	
1 % Off	238	1 1	Deg F	ASTM D-2887		
2 % Off	279	1	Deg F	ASTM D-2887		
3 % Off	299	1	Deg F	ASTM D-2887	i	
4 % Off	320	1	Deg F	ASTM D-2887	ţ	
5 % Off	327	l i	Deg F	ASTM D-2887	1	
6 % Off	333	i	Deg F	ASTM D-2887		
7 % Off	341	;	Deg F	ASTM D-2887		
	352		Deg F	ASTM D-2887		
8 % Off	359		Deg F	ASTM D-2887		
9 % Off	363		Deg F	ASTM D-2887		
10 % Off		4 .	Deg F	ASTM D-2887		
11 % Off	368	!		ASTM D-2887	1	
12 % Off	372	1	Deg f	ASTM D-2887	1	
13 % Off	378	1	Deg F	ASTM D-2887		
14 % Off	384	1 1	Deg f			
15 % Off	387	1 1	Deg F	ASTM D-2887		
16 % Off	391	1 1	Deg F	ASTM D-2887		
17 % Off	393	1	Deg F	ASTM D-2887		
18 % Off	396	1	Deg F	ASTM D-2887		
19 % Off	399	1	Deg F	ASTM D-2887		
20 % Off	401	1	Deg F	ASTM D-2887		
21 % Off	404	1	Deg F	ASTM D-2887		
22 % Off	406	1	Deg F	ASTM D-2887		
23 % Off	409	1	Deg F	ASTM D-2887		
24 % Off	412	1	Deg f	ASTM D-2887		
25 % Off	416	i	Deg F	ASTM D-2887		
	420	i	Deg F	ASTM D-2887		
26 % Off	424	1	Deg F	ASTM D-2887		
27 % Off	428		Deg F	ASTM D-2887	1	
28 % Off	432		Deg F	ASTM D-2887		
29 % Off	435	1 1	Deg F	ASTM D-2887		
30 % Off			Deg F	ASTM D-2887		
31 % Off	437		*	ASTM D-2887		
32 % Off	440		Deg F	ASTM D-2887		
33 % Off	442	1 !	Deg F	ASTM D-2887		
34 % Off	445	1 1	Deg F	ASIM D-2007		
35 % Off	449	1 1	Deg f	ASTM D-2887		
36 % Off	456	1	Deg F	ASTM D-2887	ļ	
37 % Off	465	1	Deg F	ASTM D-2887	1	
38 % Off	474	1	Deg F	ASTM D-2887	Į.	
39 % Off	480	1	Deg F	ASTM D-2887		
40 % Off	485	1	Deg F	ASTM D-2887		
41 % Off	495	1	Deg F	ASTM D-2887		
42 % Off	509	1 1	Deg F	ASTM D-2887	1	



RESULTS LABORATORY TESTS

01/05/93

JOS NUMBER: 930006

CLIENT I.D..... TP-25

WORK DESCRIPTION ...: TP-25

DATE SAMPLED.....: 12/28/92 TIME SAMPLED.....: 07:00

CUSTOMER: RESNA Company

ATTN: Robert D. Campbell

LABORATORY I.D...: 930006-0001 DATE RECEIVED: 12/31/92

TIME RECEIVED: :

REMARKS..... 3 - 40 mt vials

TEST DESCRIPTION	FINAL RESULT	LIMITS/*DILUTION	UNITS OF MEASURE	TEST METHOD	DATE	TECH
43 % Off	520	1	Deg F	ASTM D-2887		
44 % Off	532	1	Deg F	ASTM D-2887		
45 % Off	544	1	Deg F	ASTM D-2887	1	
46 % Off	560	1	Deg F	ASTM D-2887	Ì	
47 % Off	573	1	Deg. F	ASTM 0-2887		
48 % Off	589	1 1	Deg F	ASTM D-2887		
49 % Off	605	1	Deg F	ASTM D-2887		
50 % Off	622	1	Deg F	ASTM D-2887	Ì	
Simulated Distillation, Continued		*1		ASTM 0-2887	01/05/93	FA
51 % Off	640	1	Deg F	ASTM D-2887		
52 % Off	657	1	Deg F	ASTM D-2887		
53 % Off	678	1 1	Deg F	ASTM D-2887		
54 % Off	700	1 1	Deg F	ASTM D-2887		
55 % Off	723	1	Deg F	ASTM D-2887		
56 % Off	743	1	Deg F	ASTM D-2887		
57 % Off	762	1	Deg F	ASTM D-2887		
58 % Off	778	1 1	Deg F	ASTM D-2887		
59 % Off	792	l i	Deg F	ASTM D-2887	l	
	804	1 1	Deg F	ASTM D-2887		
60 % Off	815	1 1	Deg F	ASTM D-2887		
61 % Off	825	1 1	Deg F	ASTM D-2887		
62 % Off	835	1 1	Deg F	ASTM D-2887		
63 % Off	845	1 1	Deg F	ASTM D-2887		
64 % Off	854	1 :	Deg F	ASTM D-2887		
65 % Off		;	Deg F	ASTM D-2887	Ì	
66 % Off	864 873	;	Deg F	ASTM D-2887	ì	
67 % Off		;	Deg F	ASTM D-2887		
68 % Off	881		1 ~	ASTM D-2887		
69 % Off	890	1 1	Deg F	ASTM D-2887	İ	
70 % Off	898	1 1	Deg F	ASTM D-2887	ļ	
71 % Off	905		Deg F	ASTM 0-2887		
72 % Off	913	1 !	Deg F	ASTM D-2887		
73 % Off	920	1 1	Deg F	ASTM D-2887	ļ	
74 % Off	927	1	Deg F	ASIM 0-2007		
75 % Off	930	1	Deg F	ASTM D-2887 ASTM D-2887	İ	
76 % Off	932	1	Deg F	ASTR 0-2007		
77 % Off	934	1	Deg F	ASTM D-2887		
78 % Off	936	1	Deg f	ASTM 0-2887		
79 % Off	938	1	Deg f	ASTM D-2887		
80 % Off	939	1	Deg f	ASTM D-2887		
81 % Off	941	1	Deg F	ASTM D-2887		
82 % Off	943	1	Deg F	ASTM D-2887		
83 % Off	945	1	Deg F	ASTM D-2887		
84 % Off	947	l t	Deg F	ASTM D-2887	1	



LABORATORY TESTS RESULTS

01/05/93

JOB NUMBER: 930006

CUSTOMER: RESNA Company

ATTN: Robert D. Campbell

CLIENT I.D..... TP-25 DATE SAMPLED.....: 12/28/92

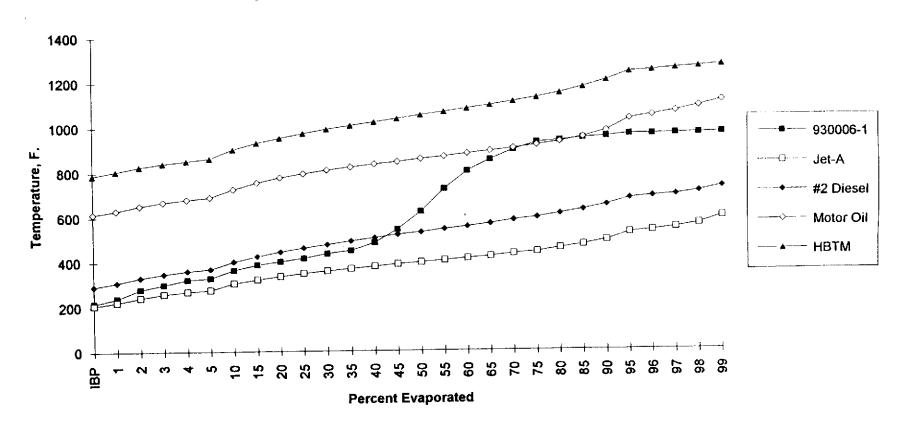
LABORATORY I.D...: 930006-0001 DATE RECEIVED...: 12/31/92
TIME RECEIVED...: :
REMARKS....: 3 - 40 ml vials

TIME SAMPLED.....: 07:00 WORK DESCRIPTION ...: TP-25

TEST DESCRIPTION	FINAL RESULT	LIMITS/*DILUTION	UNITS OF MEASURE	TEST METHOD	DATE	TECHN
85 % Off	949	1	Deg F	ASTM D-2887		
86 % Off	950	1	Deg F	ASTM D-2887	1	
87 % Off	952	1	Deg F	ASTM D-2887	1	
88 % Off	954	1	Deg F	ASTM D-2887	Į.	
89 % Off	956	1	Deg F	ASTM D-2887	1	
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91 % Off	959	1	Deg F	ASTM D-2887		
92 % Off	960	1	Deg F	ASTM D-2887	ļ	
93 % Off	962	ļ 1	Deg f	ASTM D-2887	1	
94 % Off	964	1	Deg F	ASTM D-2887		
95 % Off	966	1	Deg F	ASTM D-2887		
96 % Off	967	1	Deg F	ASTM D-2887		
97 % Off	969	1	Deg F	ASTM D-2887		
98 % Off	971	1	Deg F	ASTM D-2887		
99 % Off	973	1	Deg F	ASTM D-2887		
FBP	974	1	Deg f	ASTM D-2887	1	



Sample 930006-1 Distillation Profile





	QUAL	ITY ASSU 01/0		PORT	•	
JOB NUMBER: 930006 CUSTO	MER: RESNA Compa	any		ATTN: Robert	D. Campbell	
Simulated Distillation, Distillate	DATE ANALYZED	: 01/05/93 TIME	ANALYZED: 11:46	METHOD: ASTM D	-2887 QC	NUMBER:936850
		BLAN	K \$			
TEST DESCRIPTION	ANALY SUB-TYPE	ANALYSIS I.D.	DILUTION FACTOR	ANALYZED VALUE	DETECTION LIMIT	UNITS OF MEASURE
Simulated Distillation ASTM D-2887	Reagent	cs2	1	<1	1	Vol.%
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QUALITY ASSURANCE REPORT

STANDARDS

01/05/93

JOB NUMBER: 93006 CUSTOMER

CUSTOMER: RESNA Company

ATTN: Robert D. Campbell

Simulated Distillation, Distillate DATE ANALYZED: 01/05/93 TIME ANALYZED: 11:46 METHOD: ASTM D-2887

REFERENCE

QC NUMBER:936850

	ANALYSIS SUB-TYPE	ANALYSIS I. D.	DILUTION FACTOR	ANALYZED VALUE	TRUE VALUE	PERCENT RECOVERY	DETECTION LIMITS	UNITS OF MEASURE
Simulated Distillation ASTM D-2887	Reference	RGO #1	1	241	238	101	1	Vol.%
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QUALITY ASSURANCE FOOTER 01/05/93

Analyses performed in accordance with ASTM Testing Procedures.

Samples retained for thirty days after report submission. After thirty days, samples are disposed in accordance with Core Laboratories' Disposal Policy. Samples will be retained longer with prior arrangement. Storage fees may apply.

The acceptance criteria for duplicate analyses are the applicable ASTM Repeatability Statements.

The "Time Analyzed" in the QA Report refers to the start time of the analytical batch. It may not reflect the actual analysis time. The "Date Analyzed" reflects the actual analysis date.

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				Matrix		Preser	vation			1	8015	\$E		33E				Semi DVOA	60107000		72 T	0	Method of shipment
Sample t.D.	Lab no.	Container no	Soil	Water	Other	ice	Acid	Sampling date	Sampling time	BTEX 602/EPA 8020	BTEX/TPH EPA M602/8026/8015	TPH Modified 8015 Gas Diesel	Oil and Grease 413.1 C 413.2	TPH EPA 418.1/SM503E	EPA 601/8010	EPA 624/8240	EPA 625/8270	TCLP Metals □ VOA	CAN Metals EPA TTLC [] STL	Lead Org./DHS ☐ Lead EPA 7420/7421 ☐	Findents		Special detection
TP-2B		3		V				12/28/92					1		-						X		Limit/reporting
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<u> </u>	 	 		 		 	-	-			1	1 -	 				 	1					Turnaround time
	 	 	╁		 	<u> </u>					 	1-	\vdash	1				 					Priority Rush 1 Business Day
0	d same!	<u></u>	<u> </u>	1	1/	<u> </u>	1		L	Tem	peratur	a receiv	ed:	<u></u>	<u> </u>	1	1	<u> </u>					Rush
Condition of Boliganish	 -		_	/	IV		Date	<u></u>	Time	1	ived by	$\overline{\Delta}$		d	C.	-		~~	D				2 Business Days
1/00	44 by	DU.	4	/w	4		12/28/	72	17-00 Time		oived by							- (}				Expedited 5 Business Days
Aelinquish Relinquish				<u>.</u>			Date		Time	a Rece	eived by	y labora	tory	<u></u>			Date			Time			Standard 10 Business Days

. Alberta

REECON LAANNONS



Date:

January 6, 1993

hpany

Subject:

Analysis of Monitoring Well Samples

SS#4494, Oakland, CA

Lynn M. Lane

LAR, AS

310/816-8673

To/Location:

From/Location:

M. Whelan

SM

ARCO Net 571-2449

cc:

J.M. DeJovine J.A. Jaecker

A.V. Nowak D.C. Tong

R.Campbell, Resna Industries

3 samples from 1 Well were received on January 4, 1993. They were placed in a cold room and maintained at 38 F until removed for analysis. The samples were identified as follows:

- TP-2B, 1
- 2. TP-2B, 2
- 3. TP-2B, 3

A Simulated Distillation by Gas Chromatography was performed on the samples. All are predominantly weathered gasolines. TP-2B 1 had 34% percent of the product boiling outside of the normal gasoline range. TP-2B 2 and TP-2B 3 had 17% and 15% respectively outside of the normal range. The contaminants do not resemble any of our finished hydrocarbon products.

If you have any questions concerning these analyses, please call. The original copies of the Simulated Distillation Reports are attached to this report. Due to limited sample storage capabilities, all of these samples will be discarded 60 days from issue of this report unless otherwise requested.

*** SIMULATED DISTILLATION REPORT ***

Operator Initials:

* Sample Name: well 1, station 4494 * Date: 01-01-1993 10:45:24 Method:1:0CSIMD DATA FILE: H:WELL111.PTS Cycle#: 1 Channel#: O Vial#: N.A. * Interface: 7

* Starting Peak Widtn: 10 Threshold: 10

Ending Retention Time: 32.00 Starting Delay: 0.00

Calibration file: i:ocsimd.SCL Date printed:01-01-1993 Time printed 12:34:52

ASTM D 2887 Method Percent Off Table

31.81 Baseline from: 0.47 to Process from: 0.47 to 31.81

Total Area: 12374959 ~3.25678 Slope :

% OFF	Ret. Time	Temp
IBP	0.59	218.4
1.00	0.64	223.7
2.00	0.94	254.7
3.00	0.99	260.2
4.00	1.07	268.2
5.00	1.13	274.3
6.00	1.15	. 276.7
7.00	1.28	290.8
3.00	1.35	298.2
9.00	1.53	311.8
10.00	1.56	314.2
11.00	1.60	316.5
12.00	1.64	319.2
13.00	1.73	325.2
14.00	1.76	327.3
15.00	1.79	329.5
16.00	1.82	331.5
17.00	1.88	335.8
18.00	1.97	342.3
19.00	2.05	347.3
20.00	2.08	349.2
21.00	2.12	352.2
22.00	2.18	356.2
23.00	2.22	359.3
24.00	2.26	361.9
25.00	2.29	363.8
26.00	2.33	366.3
27.00	2.36	368.5
28.00	2.41	371,.8
29.00	2.45	374.7
30.0 0	2.47	376.2
31.00	2.49	377.4
32.00	2.51	378.9
33.00	2.54	381.2
34.00	2.60	385.0
35.00	2.64	387.8
77.00	n 47	ସ୍ଥାତ ହ

389.9

390.0

2.67

2.71

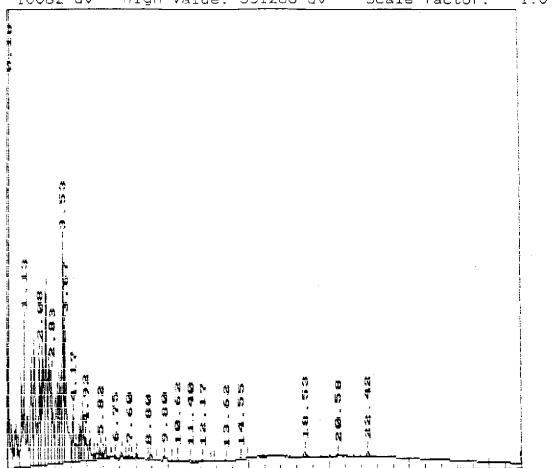
35.00

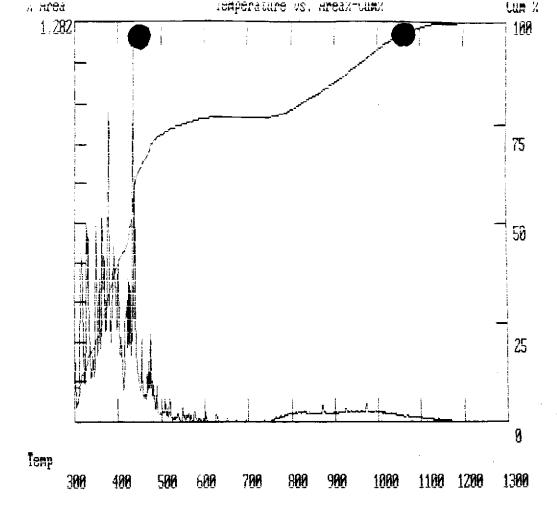
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70 , 00	2.33 _	400.7	_
41.00	2.38	404.2	
42.00	2.95	409.0	
43.00 .	3.06	416.2	
44.00	3.11	419.5	
45.00	3.15	421.8	
45.00			•
46.00	3.21	423.8	
47.00	3.25	425.1	
	3.31	427.0	
48.00			
49.00	3.35	428.4	
50.00	3.40	430.1	
51.00	3.47	432.4	
	3.51		
52.00		433.6	
53.00	3.52	434.1	
54.00	3.54	434.5	
55.00	3.55	435.0	
56. 0 0	3.57	435.6	
57.00	3.61	437.0	
58.00	3.64	438.1	
	3.66	438.8	
59.00			
50.00	3.69	439.7	
61.00	3.74	441.3	
62.00	3.81	443.7	
63.00	3.92	447.2	
64.00	4.06	451.8	
65.00	4.16	455.2	
	4.30	459.9	
66.00		•	
67.00	4.50	466.5	
68.00	4.62	470.5	
69.00	4.73	474.1	
		476.4	
70.00	4.80		
71.00	4.96	481.7	
72.00	5.19	489.2	
	5 70	504 9	
. 73.00	5.70	504.9	
	6.15	518.8	
. 73.00 74.00			
. 73.00 74.00 75.00	6.15 7.12	518.8 548.5	
. 73.00 74.00 75.00 76.00	6.15 7.12 8.11	518.8 548.5 576.9	
. 73.00 74.00 75.00 76.00 77.00	6.15 7.12 8.11 14.19	518.8 548.5 576.9 752.3	
. 73.00 74.00 75.00 76.00	6.15 7.12 8.11	518.8 548.5 576.9 752.3 786.2	
. 73.00 74.00 75.00 76.00 77.00 78.00	6.15 7.12 8.11 14.19 15.43	518.8 548.5 576.9 752.3	
. 73.00 74.00 75.00 76.00 77.00 78.00 79.00	6.15 7.12 8.11 14.19 15.43 16.09	518.8 548.5 576.9 752.3 786.2 804.1	
. 73.00 74.00 75.00 76.00 77.00 78.00 79.00 80.00	6.15 7.12 8.11 14.19 15.43 16.09 16.66	518.8 548.5 576.9 752.3 786.2 804.1 819.6	
73.00 74.00 75.00 76.00 77.00 78.00 79.00 80.00	6.15 7.12 8.11 14.19 15.43 16.09 16.66 17.20	518.8 548.5 576.9 752.3 786.2 804.1 819.6 834.5	
. 73.00 74.00 75.00 76.00 77.00 78.00 79.00 80.00	6.15 7.12 8.11 14.19 15.43 16.09 16.66 17.20 17.80	518.8 548.5 576.9 752.3 786.2 804.1 819.6 834.5 851.2	
.73.00 74.00 75.00 76.00 77.00 78.00 79.00 80.00 81.00	6.15 7.12 8.11 14.19 15.43 16.09 16.66 17.20	518.8 548.5 576.9 752.3 786.2 804.1 819.6 834.5	
. 73.00 74.00 75.00 76.00 77.00 78.00 79.00 80.00 81.00 82.00	6.15 7.12 8.11 14.19 15.43 16.09 16.66 17.20 17.80 18.44	518.8 548.5 576.9 752.3 786.2 804.1 819.6 834.5 851.2	
. 73.00 74.00 75.00 76.00 77.00 78.00 79.00 80.00 81.00 82.00 83.00 84.00	6.15 7.12 8.11 14.19 15.43 16.09 16.66 17.20 17.80 18.44 18.91	518.8 548.5 576.9 752.3 786.2 804.1 819.6 834.5 851.2 868.8 881.4	
. 73.00 74.00 75.00 76.00 77.00 78.00 79.00 80.00 81.00 82.00 83.00 84.00 85.00	6.15 7.12 8.11 14.19 15.43 16.09 16.66 17.20 17.80 18.44 18.91	518.8 548.5 576.9 752.3 786.2 804.1 819.6 834.5 851.2 868.8 881.4 897.6	
. 73.00 74.00 75.00 76.00 77.00 78.00 79.00 80.00 81.00 82.00 83.00 84.00	6.15 7.12 8.11 14.19 15.43 16.09 16.66 17.20 17.80 18.44 18.91	518.8 548.5 576.9 752.3 786.2 804.1 819.6 834.5 851.2 868.8 881.4 897.6 912.5	
.73.00 74.00 75.00 76.00 77.00 78.00 79.00 80.00 81.00 82.00 83.00 84.00 85.00	6.15 7.12 8.11 14.19 15.43 16.09 16.66 17.20 17.80 18.44 18.91 19.53 20.10	518.8 548.5 576.9 752.3 786.2 804.1 819.6 834.5 851.2 868.8 881.4 897.6	
. 73.00 74.00 75.00 76.00 77.00 78.00 79.00 80.00 81.00 82.00 83.00 84.00 85.00 86.00 87.00	6.15 7.12 8.11 14.19 15.43 16.09 16.66 17.20 17.80 18.44 18.91 19.53 20.10 20.61	518.8 548.5 576.9 752.3 786.2 804.1 819.6 834.5 851.2 868.8 881.4 897.6 912.5 925.8	
. 73.00 74.00 75.00 76.00 77.00 78.00 79.00 80.00 81.00 82.00 83.00 84.00 85.00 86.00 87.00	6.15 7.12 8.11 14.19 15.43 16.09 16.66 17.20 17.80 18.44 18.91 19.53 20.10 20.61 21.09	518.8 548.5 576.9 752.3 786.2 804.1 819.6 834.5 851.2 868.8 881.4 897.6 912.5 925.8 938.2	
. 73.00 74.00 75.00 76.00 77.00 78.00 79.00 80.00 81.00 82.00 83.00 84.00 85.00 86.00 87.00 88.00 89.00	6.15 7.12 8.11 14.19 15.43 16.09 16.66 17.20 17.80 18.44 18.91 19.53 20.10 20.61 21.09 21.60	518.8 548.5 576.9 752.3 786.2 804.1 819.6 834.5 851.2 868.8 881.4 897.6 912.5 925.8 938.2 951.0	
. 73.00 74.00 75.00 76.00 77.00 78.00 79.00 80.00 81.00 82.00 83.00 84.00 85.00 86.00 87.00	6.15 7.12 8.11 14.19 15.43 16.09 16.66 17.20 17.80 18.44 18.91 19.53 20.10 20.61 21.09	518.8 548.5 576.9 752.3 786.2 804.1 819.6 834.5 851.2 868.8 881.4 897.6 912.5 925.8 938.2 951.0 963.6	
73.00 74.00 75.00 76.00 77.00 78.00 79.00 80.00 81.00 82.00 83.00 84.00 85.00 86.00 87.00 88.00 89.00	6.15 7.12 8.11 14.19 15.43 16.09 16.66 17.20 17.80 18.44 18.91 19.53 20.10 20.61 21.09 21.60 22.09	518.8 548.5 576.9 752.3 786.2 804.1 819.6 834.5 851.2 868.8 881.4 897.6 912.5 925.8 938.2 951.0	
73.00 74.00 75.00 76.00 77.00 78.00 79.00 80.00 81.00 82.00 83.00 84.00 85.00 86.00 87.00 88.00 89.00	6.15 7.12 8.11 14.19 15.43 16.09 16.66 17.20 17.80 18.44 18.91 19.53 20.10 20.61 21.09 21.60 22.09 22.51	518.8 548.5 576.9 752.3 786.2 804.1 819.6 834.5 851.2 868.8 881.4 897.6 912.5 925.8 938.0 943.6 974.1	
73.00 74.00 75.00 76.00 77.00 78.00 79.00 80.00 81.00 82.00 83.00 84.00 85.00 86.00 87.00 88.00 89.00 90.00	6.15 7.12 8.11 14.19 15.43 16.09 16.66 17.20 17.80 18.44 18.91 19.53 20.10 20.61 21.09 21.60 22.09 22.51 23.02	518.8 548.5 576.9 752.3 786.2 804.1 819.6 834.5 851.2 868.8 881.4 897.6 912.5 925.8 938.2 951.0 963.6 974.1 986.4	
73.00 74.00 75.00 76.00 77.00 78.00 79.00 80.00 81.00 82.00 83.00 84.00 85.00 86.00 87.00 88.00 89.00	6.15 7.12 8.11 14.19 15.43 16.09 16.66 17.20 17.80 18.44 18.91 19.53 20.10 20.61 21.09 21.60 22.09 22.51 23.02 23.52	518.8 548.5 576.9 752.3 786.2 804.1 819.6 834.5 851.2 868.8 881.4 897.6 912.5 925.8 938.2 951.0 963.6 974.1 986.4 998.6	
73.00 74.00 75.00 76.00 77.00 78.00 79.00 80.00 81.00 82.00 83.00 84.00 85.00 86.00 87.00 88.00 89.00 90.00	6.15 7.12 8.11 14.19 15.43 16.09 16.66 17.20 17.80 18.44 18.91 19.53 20.10 20.61 21.09 21.60 22.09 22.51 23.02	518.8 548.5 576.9 752.3 786.2 804.1 819.6 834.5 851.2 868.8 881.4 897.6 912.5 925.8 938.2 951.0 963.6 974.1 986.4	
73.00 74.00 75.00 76.00 77.00 78.00 79.00 80.00 81.00 82.00 83.00 84.00 85.00 86.00 87.00 88.00 89.00 90.00 91.00 92.00 93.00	6.15 7.12 8.11 14.19 15.43 16.09 16.66 17.20 17.80 18.44 18.91 19.53 20.10 20.61 21.09 21.60 22.09 22.51 23.02 24.08	518.8 548.5 576.9 752.3 786.2 804.1 819.6 834.5 851.2 868.8 881.4 897.6 912.5 925.8 938.2 951.0 963.6 974.1 986.4 998.6 1011.9	
73.00 74.00 75.00 76.00 77.00 78.00 79.00 80.00 81.00 82.00 83.00 84.00 85.00 86.00 87.00 88.00 89.00 90.00 91.00 92.00 93.00 94.00 95.00	6.15 7.12 8.11 14.19 15.43 16.09 16.66 17.20 17.80 18.44 18.91 19.53 20.10 20.61 21.09 21.60 22.09 22.51 23.02 24.08 24.71	518.8 548.5 576.9 752.3 786.2 804.1 819.6 834.5 851.2 868.8 881.4 897.6 912.5 925.8 938.2 951.0 963.6 974.1 986.4 998.6 1011.9 1026.8	
73.00 74.00 75.00 76.00 77.00 78.00 79.00 80.00 81.00 83.00 83.00 83.00 84.00 85.00 86.00 87.00 88.00 89.00 90.00 91.00 92.00 93.00 94.00 95.00	6.15 7.12 8.11 14.19 15.43 16.09 16.66 17.20 17.80 18.44 18.91 19.53 20.10 20.61 21.09 21.60 22.09 22.51 23.02 24.08 24.71 25.40	518.8 548.5 576.9 752.3 786.2 804.1 819.6 834.5 851.2 868.3 881.4 897.5 912.5 925.8 938.0 943.1 986.4 998.6 1011.9 1026.8 1043.1	
73.00 74.00 75.00 76.00 77.00 78.00 79.00 80.00 81.00 82.00 83.00 84.00 85.00 86.00 87.00 88.00 89.00 90.00 91.00 92.00 93.00 94.00 95.00	6.15 7.12 8.11 14.19 15.43 16.09 16.66 17.20 17.80 18.44 18.91 19.53 20.10 20.61 21.09 21.60 22.09 22.51 23.02 24.08 24.71	518.8 548.5 576.9 752.3 786.2 804.1 819.6 834.2 851.2 868.8 881.4 897.5 912.8 925.8 938.0 963.6 974.1 986.4 998.6 1011.9 1026.3 1043.1 1062.4	
73.00 74.00 75.00 76.00 77.00 78.00 79.00 80.00 81.00 83.00 84.00 85.00 86.00 87.00 88.00 89.00 90.00 91.00 92.00 93.00 94.00 95.00 96.00 97.00	6.15 7.12 8.11 14.19 15.43 16.09 16.66 17.20 17.80 18.44 18.91 19.53 20.10 20.61 21.09 21.60 22.09 22.51 23.02 24.71 25.40 26.23	518.8 548.5 576.9 752.3 786.2 804.1 819.6 834.5 851.2 868.3 881.4 897.5 912.5 925.8 938.0 943.1 986.4 998.6 1011.9 1026.8 1043.1	
73.00 74.00 75.00 76.00 77.00 78.00 79.00 80.00 81.00 82.00 83.00 84.00 85.00 86.00 87.00 88.00 99.00 91.00 92.00 93.00 94.00 95.00 96.00 97.00 98.00	6.15 7.12 8.11 14.19 15.43 16.09 16.66 17.20 17.80 18.44 18.91 19.53 20.10 20.61 21.09 21.60 22.09 22.51 23.02 24.08 24.71 25.40 26.23 27.21	518.8 548.5 576.9 752.3 786.2 804.1 819.6 834.5 851.2 868.8 881.4 897.6 912.5 925.8 938.2 951.0 963.6 974.1 986.4 998.6 1011.9 1026.8 1043.1 1062.4 1084.4	
73.00 74.00 75.00 76.00 77.00 78.00 79.00 80.00 81.00 82.00 83.00 84.00 85.00 86.00 87.00 88.00 89.00 91.00 92.00 93.00 94.00 95.00 96.00 97.00 98.00 97.00	6.15 7.12 8.11 14.19 15.43 16.09 16.66 17.20 17.80 18.44 18.91 19.53 20.10 20.61 21.09 21.60 22.09 22.51 23.02 24.08 24.71 25.40 26.23 27.21 28.44	518.8 548.5 576.9 752.3 786.2 804.1 819.6 834.5 851.2 868.8 881.4 897.6 912.5 925.8 938.2 951.0 963.6 974.1 986.4 998.6 1011.9 1026.8 1043.1 1062.4 1084.4 1111.5	
73.00 74.00 75.00 76.00 77.00 78.00 79.00 80.00 81.00 82.00 83.00 84.00 85.00 85.00 86.00 87.00 88.00 91.00 92.00 91.00 92.00 93.00 94.00 95.00 96.00 97.00 98.00	6.15 7.12 8.11 14.19 15.43 16.09 16.66 17.20 17.80 18.44 18.91 19.53 20.10 20.61 21.09 21.60 22.09 22.51 23.02 24.08 24.71 25.40 26.23 27.21 28.44 29.30	518.8 548.5 576.9 752.3 786.2 804.1 819.6 834.5 851.2 868.8 881.4 897.6 912.5 925.8 938.2 951.0 963.6 974.1 986.4 998.6 1011.9 1026.8 1043.1 1062.4 1084.4 1111.5 1130.5	
73.00 74.00 75.00 76.00 77.00 78.00 79.00 80.00 81.00 82.00 83.00 84.00 85.00 85.00 86.00 87.00 88.00 91.00 92.00 91.00 92.00 93.00 94.00 95.00 96.00 97.00 98.00	6.15 7.12 8.11 14.19 15.43 16.09 16.66 17.20 17.80 18.44 18.91 19.53 20.10 20.61 21.09 21.60 22.09 22.51 23.02 24.08 24.71 25.40 26.23 27.21 28.44 29.30	518.8 548.5 576.9 752.3 786.2 804.1 819.6 834.5 851.2 868.8 881.4 897.6 912.5 925.8 938.2 951.0 963.6 974.1 986.4 998.6 1011.9 1026.8 1043.1 1062.4 1084.4 1111.5	

Data File = H:WELL111.PTS Printed on 01-01-1993 at 12:34:11 Start time: 0.00 min. Stop time: 32.00 min. Offset: 0 mv. Low Value: 10082 uv High Value: 351286 uv Scale factor: 1.0

Offset: 0 mv.





*** SIMULATED DISTILLATION REPORT ***

Operator Initials:

* Sample Name: well 2, station 4494 * Date: 01-01-1993 11:34:06 Method:I:0CSIMD DATA FILE: H:WELL22.PTS Channel#: 0 Vial#: N.A. Cycle#: 2 * Interface: 7

* Starting Peak Widtn: 10 Threshold: 10

] 38

37 00

Ending Retention Time: Starting Delay: 0.00

Calibration file: i:ocsimd.SCL Date printed:01-01-1993 Time printed 12:31:21

ASTM D 2887 Method Percent Off Table

31.81 Baseline from: 0.47 to 0.47 to Process from: 31.81

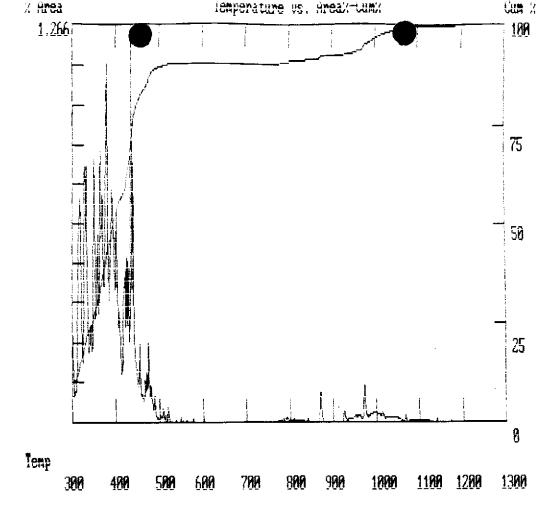
Total Area: 3104260 -1.27858 Slope :

Increment: 1

% OFF	Ret. Time	Temp
	Q.60	219.4
IBP	0.64	224.1
1.00	0.92	253.3
2.00		258.9
3.00	0.98	265.3
4.00	1.04	
5.00	1.09	271.0
6.00	1 - 13	274.8
7.00	1.15	276.7
8.00	1.22	284.2
9.00	1.31	293.6
10.00	1.36	299.1
11.00	1.51	310.3
12.00	1.55	313.3
13.00	1.58	315.0
14.00	1.60	316.7
15.00	1.63	318.4
16.00	1.67	321.8
17.00	1.73	325.8
18.00	1.75	327.2
19.00	1.78	328.8
20.00	1.80	330.4
21.00	1.82	331.9
22.00	1.86	334.3
23.00	1.92	338.6
24.00	1.98	342.7
25.00	2.04	346.7
	2.07	348.4
26.00		349.9
27.00	2.09	
28.00	2.12	352.1
2 9. 00	2.17	355.3
30.00	2.20	357.4
31.00	2.24	360.1
32.00	2.26	361.9
33.0 0	2.28	363.2
34.00	2.31	365.Q
35.00	2.33	3 6 6.7
- 36.00	2.36	368.3
	2 70	7.7/^ ~~

370.D

	J7.00		
٠,	40,00	2.47	3 76.3
•	41.00	2.49	377.4
	42.00	2.50	378.4
	43.00	2.52	379.7
	44.00	2.55	381.5
	45.00	2.59	384.1
	46.00	2.62	386.4
	47.00	2.65	388.4
	48.00	2.67	389.9
	49.00	2.70	391.6
	50.00	2.72	393. 5
	51.00	2.75	395.5
	52.00	2.79	398.1
	53.00	2.82	400.1
	54.00	2.85	402.0
	55.00	2.90 2.95	405.3 408.8
	56.00 57.00	3.03	414.7
	58.00	3.08	417.9
	59.00	3.12	420.5
	40.00	3.16	422.0
	61.00	3.21	423.7
	62.00	3.24	424.8
	63.00	3.28	426.2
	64.00	3.33	427.7
	65.00	3.36	428.8
	66.00	3.41	430.4
	67.00	3.47	432.4
	68.00	3.51	433.6
	69.00	3.52	434.2
	70.00	3.54	434.6
	71.00	3.55	435.1
	72.00	3.57	435.6
	73.00	3.60	436.6
	74.00	3.63	437.8
	75.00	3.66	438.6
	76.00	3.68	439.3
	77.00	3.70	440.2
	78.00	3.75	441.6
	79.00	3.81	443.6
	80.00	3.90	446.5
	81.00	4.00	450.1
	82.00	4.13	454.4
	83.00	4.23	457.5
	84.00	4.43	464.2
	85.00	4.60	469.8
	86.00	4.72	473.9
	87.00	4.80	476.4
	38.00	4.96	481.8
	89.00	5.23	490.7
	90.00	6.17	519.6
	91.00	16.31	810.1
	92.00	18.59	872.7
	93.00	21.55	949.8 970.8
	94.00	22.37	976.4
	95.00	22.60	976.4
	96.00	23.29	
	97.00	23.88	1007.2 1029. 3
	98.00	24.82	1029.3
	99.00	26.29	1063.9
	FBP	27.67	
	MAKNINGFND	POTIAL DELOND	THE SCOPE OF D2887



*** SIMULATED DISTILLATION REPORT *** 7628

* Date: 01-01-1993 12:22:27 Method:DCSIMD DATA FILE: H:WELL33.PTS

* Interface: 7 Cycle#: 3 Channel#: 0 Vial#: N.A.

* Starting Peak Width: 10 Threshold: 10

Starting Delay: 0.00 Ending Retention Time: 32.00

Calibration file: i:ocsimd.SCL Date printed:01-01-1993 Time printed 12:55:23

ASTM D 2887 Method Percent Off Table

Baseline from: 0.47 to 31.81 Process from: 0.47 to 31.81

Total Area: 13913458 Slope : -6.67783

Increment: 1

	_	
% OFF	Ret. Time	Temp
IBP	0.56	215.4
1.00	0.60	219.6
2.00	0.72	232.0
3.00	0.92	253.3
4.00	0.96	257.2
5.00	1.00	261.7
6.00	1.06	267.6
7.00	1.11	272.9
8.00	1.13	274.5
9.00	1.14	276.3
10.00	1.23	285 .5
11.00	1.31	293.5
12.00	1.36	298.8
13.00	1.52	311.1
14.00	1.55	313.0
15.00	1.57	314.4
16.00	1.59	316.0
	1.61	317.6
17.00		320.8
18.00	1.66	325.2
19.00	1.72	326.6
20.00	1.74	
21.00	1.77	328.0
22.00	1.79	329.6
23.00	1.81	331.0
24.00	1.84	333.2
25.00	1.91	338.0
26.00	1.98	342.4
27.00	2.04	346.5
28.00	2.06	348.0
29.00	2.08	349.4
30.00	2.11	351.8
31.00	2.16	355.1
32.00	2.19	357.1
33.00	2.23	360.0
34.00	2.26	361.5
35.00	2.28	362.8
36.00	2.30	364.6

366.4

2,33

37.00

40,00	2.42	372.3
41.00	2.45	374.7
		375.7
42.00	2.46	
43.00	2.48	376.6
44.00	2.49	377.5
45.00	2.51	378.8
46.00	2.53	380.5
47.00	2.58	383. 4
48.00	2.61	386.0
49.00	2.64	388.0
50.00	2.57	389.5
51.00	2.69	391.2
52.00	2.72	393.2
53.00	2.75	395.3
54.00	2.79	398.1
55.00	2.82	400.0
56.00	2.85	402.0
57.00	2.91	405.8
58.00	2.97	410.2
59.00	3.06	416.2
60.00	3.10	418.9
61.00	3.13	421.2
62.00	3.18	422.8
63.00	3.22	424.1
64.00	3.25	425.2
65.00	3.31	427.0
66.00	3.34	428.1
67.00	3.38	429.4
68.0 0	3.44	431.4
69.00	3.49	433.0
70.0 0	3.51	433.6
71.00	3.52	434.0
72.00	3.53	434.3
73.00	3.54	434.7
74.00	3.55	435.1
75.00	3.5 7	435.8
76.00	3.62	437.2
77.0 0	3.64	438.0
78.00	3.66	438.6
79.00	3.68	439.3
		440.5
80.00	3.72	
81.00	3.78	442.5
82.00	3.87	445.8
83.00	4.00	450.0
84.00	4.14	454.6
85.00	4.27	459.0
44 × 45 5	4.51	467.0
36.00		
87.00	4.63	471.0
88.00	4.74	474.5
89.00	4,85	478.2
90.00	5.14	487.8
91.00	16.04	802.8
	17.90	853.9
92.00		
93.00	19.61	899.6
94.00	20.75	929.5
95.00	21.71	953.8
96.00	22.50	973.9
97.00	23.42	996.0
		1021.8
98.00	24.50	
99.00	26.11	1059.6
FBP	27.38	1088.2
WARNINGEND	POINT BEYOND	THE SCOPE OF D2887

well 3. st Processed: 01-01-1993 12:54:28, segment 3, cycle 3

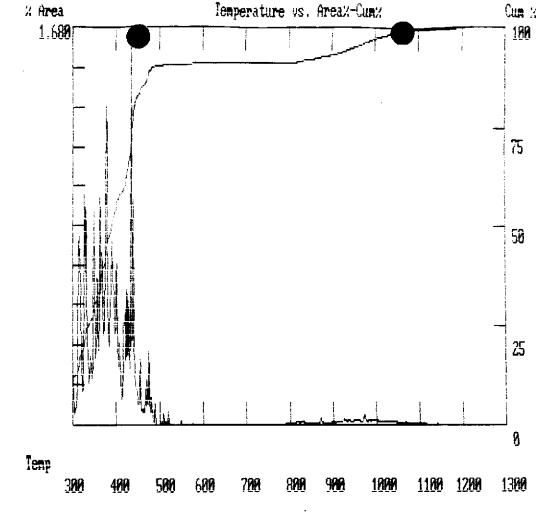
RAW DATA SAVED IN FILE H: WELL33.PTS

Areas, times, and heights stored in: H:WELL33.ATB

Low Value:

Start time: 0.00 min. Stop time: 32.00 min. Offset: O mv. 10111 uv High Value: 375035 uv Scale factor:

1.0



ATTACHMENT C CORE LABORATORY FACSIMILE



TELECOMMUNICATIONS FORM

Number of pages (including cover page):	
DATE: 8/13 193	
10: John Young	
FAX#: (408) 264 - 2435	
FROM: Grey Cook	
All analytical reports, interpretations or information faxed by CORE LABORATORIES to its Customers are preliminary data only! . Due to the probems that can occur with the transmission of data via Fax, CORE LABORATORIES will not guarantee or assume any responsability for the following transmitted data.	
MESSAGE/COMMENTS:	
John	
The initial boiling point is not listed	02
this spec sheet because it is not consid	
a specipoint by law. However it typica	elly
intiels between 90-100°F.	<u></u>
- Grea "	

If you have any question or you did not receive all pages noted, please call us at: (310) 595-8401, (310) 595-8402, (310) 595-8403, (310) 595-8404. FAX #: (310) 427-5174 CORE LABORATORIES, 3700 Cherry Avenue, Long Beach, CA 90807-4392



GASOLINE SPECIFICATION'S

•							
Lead Content, g/gal, max			0.050				
Copper strip corrosion, 3 hrs 2 122 deg F, max		#1					
Existent gum, mg/100ml, max		5 1000(a)					
Total Sulfur, ppm-wt, max							
Oxidation Stability, minutes, min	240						
VOLATILITY CLASS (b)	A	8	Ċ	D	E		
D-86 Distillation, deg F 10% evaporated, max 50% evaporated, min 50% evaporated, max 90% evaporated, max Final boiling point, max Residue, vol%, max	158 170 250 374 437 2	149 170 245 374 437 2	140 170 240 365 437	131 170 235 365 437	122 170 230 365 437 2		
Temperature at which the Vapor/Liquid Ratio is 20, deg F	140	133	124	116	105		
Reid Vapor Pressure, psi	9.0(c)	10.0	11.5	13.5	15.0		

Octane Ratings:

The EPA has set a minimum octane requirement of B7 for unleaded fuels currently marketed. However, waivers granted by the EPA allow for an octane rating as low as 84 in some mountain areas. There are no specifications for octanes above the EPA minimum; marketers set the grades and octane rating based on their perception of the technical and competitive needs of the market. Typically, in California, you would find three grades of unleaded with the following octanes:

GRADE Regular unleaded Nid-grade unleaded Promium unleaded

OCTANE 87 89 91 or 92

- (a) In California the maximum sulfur content allowed in unleaded gasoline is 300 ppm-wt
- (b) The letter designations represent volutility classes which are based on geographic locations (see chart attached)
- (c) A Reid Vapor Pressure maximum limit of 8.0 psi is currently in effect for most areas of California. This is supposed to drop to 7.0 psi in 1993. In both California and Navada there is a 1.0 psi waiver allowed for fuels containing ethanol.

Effective date July 2, 1992



SCHEDULE OF SEASONAL AND GEOGRAPHICAL VOLATILITY CLASSES

STATE

California

North Coast

South Coast

Southeast

Interior

J	F	М	A	М	J	J	A	S	0	И	D
E/D	D	D	D/C	С	C/B	B	В	В	В/С	C/D	D/E
D	D	C/B	λ	Α	A	λ	λ	A	A	B/C	D
D	D/C	C/B	В	B/A	A	λ	λ	A	A/B	B/C	C/D
E/D	ם	D	D/C	C/B	В	В	В	В	B/C	C/D	D/E

Nevada

N 38 deg. Latitude

S 38 deg. Latitude

Е	E/D	D	D/C	C/B	В	В	В	В	B/C	C/D	D/E
D	D/C	C/B	В	B/A	A	A	λ	λ	A/B	B/C	C/D

Effective date July 2, 1992

ATTACHMENT D RESNA FOLLOW-UP LETTER TO ACHSCA

(DATED JULY 13, 1993)



3315 Almaden Expressway, Suite 34 San Jose, CA 95118

Phone: (408) 264-7723 FAX: (408) 264-2435

> July 13, 1993 0709BCHA.4494

Mr. Barney Chan Alameda County Health Care Services Agency 80 Swan Way, Room 200 Oakland, California 94624

Subject:

Follow-Up to Telephone Conversation Concerning Replacement of Monitoring Well MW-2 at ARCO Station 4494, 566 Hegenberger Road,

Oakland, California.

Mr. Chan:

This letter is written as follow-up to our telephone conversation of June 30, 1993, concerning replacement of monitoring well MW-2 at the above-referenced site. A brief chronology which led to our June 30, 1993 telephone conversation is described below.

As stated in RESNA's Report of Findings Underground Gasoline Tank Removal and Replacement, dated May 17, 1993, RESNA recommended that decommissioned monitoring well MW-2 be replaced with a four-inch diameter monitoring well in the approximate vicinity of well MW-2. In a letter dated May 24, 1993 from the Alameda County Health Care Services Agency (ACHCSA), you requested that the new well be installed in native soils as opposed to backfill materials.

RESNA contacted Mr. Walt Or of Golden West Contractors Builders & Consultants (Golden West), who is the foreman for construction activities at the subject site, and discussed the installation of the replacement well. Mr Or indicated that in order to install a monitoring well in native soils, the well would have to be located offsite. RESNA then contacted ACHCSA to inform you of our intentions of replacing the well.

Per our telephone conversation on June 30, 1993, you stated that it does not seem necessary to replace well MW-2 with a new well. You stated that if a new well would be placed in backfill materials as opposed to native soils, no apparent beneficial use would be gained from the new well. RESNA informed you that, in order to replace the well into native soils



Follow-Up to Telephone Conversation ARCO Station 4494, Oakland, California

the well would have to be placed offsite. Additionally, two monitoring wells (MW-5, MW-6) are already located in native soils offsite and down-gradient of the former tank pit.

In summary, as a result of our telephone conversation, RESNA will not replace decommissioned well MW-2 with a four-inch monitoring well. Monitoring wells MW-5 and MW-6 will currently serve as down-gradient monitoring wells.

If you have any questions or comments concerning this matter, please contact us at (408) 264-7723.

Sincerely,

RESNA Industries Inc.

John C. Young Project Manager

cc: Mr. Michael Whelan, ARCO Products Company

Mr. Britt Johnson, ACHCSA