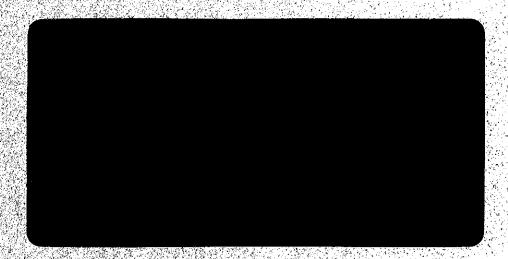
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5500 Shellmound Street, Emeryville, CA 94608-2411

Fax: 510-547-5043 Phone: 510-450-6000

RISK-BASED CORRECTIVE ACTION EVALUATION

for

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Former New Century Beverage Company Facility
1150 Park Avenue
Emeryville, California

Submitted to

Alameda County Health Care Services Agency
Department of Environmental Health
1131 Harbor Bay Parkway
Alameda, California 94102

prepared for

New Century Beverage Company 29000 Hesperian Boulevard Hayward, California 94545

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November 27, 1996

PROJECT#:

14-1239-01

To:

Ms. Susan Hugo.

PHONE:

510-567-6700

Senior Hazardous Materials Specialist

Alameda County Health Care Services Agency

Department of Environmental Health Division of Hazardous Materials 1131 Harbor Bay Parkway Alameda, California 94502

FROM:

Carolyn Atwood

ENCLOSED PLEASE FIND: DRAFT RBCA REPORT FOR 1150 PARK AVE. EMERYVILLE

VIA:	FAX:	As:	For:
☐ Fax	# of pages:	Per our phone call	☐ Your information
☐ 1 st Class Mail	(including this cover)	You requested	Return to you
Overnight Delivery	☐ Hard Copy to follow	☐ Is required	Your action
UPS (Surface)		We believe you may	Your review &
Courier		be interested	comments

Please call (510) 450-6000 if there are any problems with transmission.

SUSAN:

Enclosed please find the draft Risk Based Corrective Action Plan for 1150 Park Ave in Emeryville, as promised. At your request during our earlier meeting, we have incorporated a construction scenario. Copies of the draft have also been transmitted directly to counsel for Del Monte and Pixar on Nov 19, 1996. As I mentioned during our recent conversation, we are awaiting comments from Kaiser Foundation before finalizing this draft, as we are contractually required to do. I expect to receive their comments the first week of December, but do not anticipate any significant changes to the document. Therefore, I wanted to get this draft in to you so you could begin your review. Please anticipate that with the final document we will also submit a formal request to modify the RAP based on the results of this analysis. Please feel free to call me directly with any questions you may have, at 510-450-6000.

M.

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Fax: 510-547-5043 Phone: 510-450-6000

RISK-BASED CORRECTIVE ACTION **EVALUATION**

for

Former New Century Beverage Company Facility 1150 Park Avenue Emeryville, California

prepared by

Weiss Associates 5500 Shellmound Street Emeryville, CA 94608

WA Job # 14-1239-01

Thomas Fojut * Project Hydrogeologist

Weiss Associates' work for the former New Century Beverage Company facility was conducted under my supervision. To the best of my knowledge, the data contained herein are true and accurate and satisfy the scope of work prescribed by the client for this project. The data, findings, recommendations, specifications or professional opinions were prepared solely for the use of the New Century Beverage Company in accordance with generally accepted professional engineering and geological practice. We make no other warranty, either expressed or implied, and are not responsible for the interpretation by others of the contents herein.

Carolyn J. Atwood

Date

Senior Project Engineer, R.E.A. #01704



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SUMMARY

Weiss Associates (WA) completed this Risk-Based Correction Action (RBGA) Evaluation for the former New Century Beverage Company Facility in Emeryville, California. The evaluation was performed in accordance with the American Society for Testing and Materials Standard E 1739-95, Risk-Based Corrective Action Applied at Petroleum Release Sites (ASTM, 1995). This evaluation also serves as a formal amendment to the Remedial Action Plan submitted in Jan 1995 and approved in August 1995. The objective of this evaluation is to determine the most appropriate future action for the site based on site-specific characteristics of the site and the extent and nature of the known subsurface hydrocarbon-related impacts.

The evaluation assesses potential impacts of chemicals of concern (COC) on future potential site occupants and on ground water quality. The chemicals of concern have been previously identified and include benzene, ethylbenzene, toluene, xylenes, naphthalene, fluorene, fluoranthene and pyrene. WA evaluated three different exposure scenarios in this assessment: construction, commercial/industrial, and residential. The construction scenario was added at the request of the Alameda County Health Care Services Agency (ACHCSA). For each exposure scenario, potentially complete exposure pathways were identified and evaluated.

WA established Tier 1 risk-based screening levels (RBSLs) for each COC/potentially complete exposure pathway pair in each scenario. These conservative Tier 1 RBSLs were established using the models and recommended parameter values in the ASTM Standard. Tier 1 RBSLs represent extremely conservative concentrations, below which no significant adverse effects on human health are expected to occur. For those contaminant/pathway pairs for which the conservative Tier 1 RBSLs were exceeded in a particular medium (surface soil, subsurface soil, or ground water), WA completed a Tier 2 analysis. Tier 2 site-specific target levels (SSTLs), which represent the same level of health protection as the Tier 1 RBSLs, were developed using generally accepted modeling methods with site-specific characterization data. The Tier 2 SSTL is a site-specific, rather than generic, level below which contaminants are not expected to pose a significant threat to human health, including by ground water ingestion.

The Tier 2 SSTLs developed in this analysis are WA's recommended final cleanup levels for the site, and thereby represent a proposed modification to the target levels previously recommended by the ACHCSA in its August 1995 approval of the Remedial Action Plan.

The 1995 source area excavations removed much of the vadose zone source area, reducing future leaching of hydrocarbons into ground water and removing most soil with more than 100 parts per million (ppm) total petroleum hydrocarbons (TPH). This analysis shows that worst-case (maximum) site-specific levels of contaminants of concern remaining in the subsurface do not exceed Tier 1 RBSLs or Tier 2 SSTLs for any of the three exposure scenarios. Therefore, residual contaminants do not appear to pose any significant risk to future potential receptors at the site, nor to



offsite residential use of shallow ground water. Petroleum hydrocarbons in ground water are limited to a stable, onsite plume. Furthermore, natural attenuation is likely to eventually reduce hydrocarbon concentrations to below maximum contaminant levels for drinking water.

Therefore, WA recommends no further action as the most appropriate action for the site, based on the excavation of the source areas associated with the former underground tanks, the comparison of site data to RBSLs and SSTLs, and the stability of the dissolved hydrocarbon plume. WA further recommends that ACHCSA consider this site for closure.

1. INTRODUCTION

At the request of New Century Beverage Company (New Century) and the Alameda County Health Care Services Agency (ACHCSA), Weiss Associates (WA) has prepared this Risk-Based Corrective Action (RBCA) Evaluation for the former New Century facility located at 1150 Park Avenue in Emeryville, California. This evaluation serves as a formal amendment to the Remedial Action Plan (RAP) submitted in January 1995 (WA, 1995) and approved in August 1995 (ACHCSA, 1995). The objective of this evaluation is to determine the most appropriate future action for the site based on site-specific characteristics and the extent and nature of known subsurface petroleum hydrocarbons. This RBCA evaluation follows the process outlined by the American Society for Testing and Materials (ASTM) Standard E 1739-95, Risk Based Corrective Action Applied at Petroleum Release Sites.

The RAP and this subsequent RBCA analysis address petroleum hydrocarbons in soil and ground water at the site from two underground fuel storage tanks (USTs). Prior to submittal of the RAP, the two USTs had been removed from the site. In approving the RAP, the ACHCSA agreed that soil excavation in the known source areas with four subsequent quarters of ground water monitoring was the most feasible remedial option for the site. Furthermore, the RAP approval letter established target soil cleanup levels of 100 parts per million for (ppm) total petroleum hydrocarbons (TPH) and concentrations equal to the EPA Region IX Preliminary Remediation Goals for Residential Soil for benzene, ethylbenzene, toluene and xylenes (BETX).

The source areas were excavated in October and November 1995. Most soil containing hydrocarbons above these cleanup levels was removed. However, some soil containing hydrocarbons above the cleanup levels west and east of the southern former UST (UST #2) was not excavated due to nearby buildings. Excavation north of the UST ceased because WA determined that it would be more cost-effective to pre-characterize the surrounding soil to determine the need for further excavation, if any. The building on the east side of former UST #1 similarly precluded complete removal of soil with hydrocarbon concentrations above the cleanup levels. Additionally, further excavation would be impractical with the upcoming site demolition and rainy season. Thus, excavation was discontinued with the verbal approval of the ACHCSA (Personal communication, 1995), and WA drilled borings B-50 through B-63 in November 30, 1995 to further characterize soil north of UST #2.

The post-excavation ground water monitoring was initiated in the fourth quarter of 1995 as required by the RAP approval. New Century has now completed the required four quarters of ground water monitoring following the soil excavations. The third quarter 1996 monitoring report was submitted to the ACHCSA on November 15, 1996.

In May and June 1996, following facility shutdown and the winter storm season, and prior to the facility demolition, WA drilled borings B-64 through B-95. These borings were drilled to

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characterize soil during site demolition in accordance with certain provisions of a contractual agreement with Kaiser Foundation, owner of the property on which the buildings were located. Samples from the borings were not intended to assess the extent of petroleum hydrocarbons in the subsurface in relation to the tanks, and are thus unassociated with the Remedial Action Plan. Therefore, the results were not used for this evaluation.

WA and New Century met with representatives of the ACHCSA on June 20, 1996, and presented the characterization results conducted subsequently to the October 1995 soil excavations. At that time, ACHCSA representatives requested that WA sample ground water monitoring wells MW-5, MW-6, and MW-13 for polynuclear-aromatic hydrocarbons (PAHs) to assess if PAHs had impacted ground water. That sampling was completed during the second quarter ground water monitoring event, and reported in the Third Quarter 1996 Status Report (WA, 1996). The ACHCSA also requested that soil samples near the former diesel UST #2 be analyzed for PAHs. In July 1996, borings B-96 and B-97 were subsequently drilled and soil from each was analyzed for PAHs.

Furthermore, it was agreed during the June 20, 1996 meeting that a RBCA analysis be completed along with an amendment to the RAP to develop constituent- and site-specific rather than general TPH target cleanup levels. With this submittal, WA is satisfying that commitment.

A summary of the site background, the RBCA evaluation, and conclusions are presented in the following sections. The conclusions and recommendations also serve as the formal amendment to the January 1995 RAP for this site.

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2. SITE BACKGROUND

2.1 Topography

The site is located about 40 ft above mean sea level on an alluvial plain that gently slopes toward San Francisco Bay, located about one-half mile to the west (Figure 1). The north-northwest trending Berkeley Hills are about two miles to the east. Ground surface at the site slopes gently southwest, and north of the site, the topography slopes northwest toward Temescal Creek, about 1,500 ft north of the site. The site is currently an unpaved, vacant lot.

2.2 Hydrogeology

The uppermost sediments beneath the site vicinity have been characterized as Quaternary alluvial and fluvial deposits consisting primarily of fine sand, silt and silty clay (Helley, 1972). Interfluvial basin deposits consisting of plastic silty clay and clay underlie the fluvial deposits. Descriptions of soil samples from the New Century site indicate that the site is underlain by interfingering sediments ranging from silty clay to silty sand, sediments with low to moderate estimated permeabilities.

Since monitoring commenced in 1994, ground water beneath the site has fluctuated seasonally between 4 and 11 ft below grade. Ground water consistently flows southwestward with an average gradient of 0.017 ft/ft. This flow direction is consistent with the flow direction beneath the adjacent Del Monte property, located west of the site (CH₂M HILL, 1992).

2.3 Adjacent Hydrocarbon Sources

Previous investigations have identified numerous potential offsite sources of hydrocarbons in the surrounding commercial/industrial neighborhood. Adjacent properties with former or existing underground fuel tanks include Standard Brands Paint, a former gasoline service station northeast of the site; the former Emeryville Fire Department Station east of the site; the "Corner Site", a former gasoline service station southeast of the site; and the United States Post Office, located east of the site. All four properties are located upgradient of the New Century property. Based on the distribution of hydrocarbons in ground water beneath the New Century site, it appears that petroleum hydrocarbons have migrated onto the New Century property from the Standard Brands property or the former Emeryville Fire Department and the Corner Site.

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2.4 Site Use

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Except for a residential structure, the 2.9-acre property remained undeveloped until 1913, when a baseball park was built. After the park was removed, the bottling plant was constructed in 1958. The plant housed administrative offices; a quality control laboratory; a production area including beverage canning, packaging and storage; a vehicle maintenance shop and two USTs (Figure 2).

In November 1992, New Century began leasing the adjacent, unpaved parcel west of the site from Del Monte Foods (Figure 2). New Century used the adjacent parcel for delivery truck and employee parking, as did Del Monte prior to the lease. Based on aerial photographs, this parcel was always unpaved and unimproved.

In August 1996, New Century demolished the plant. Currently, the site is unpaved and has no structures.

2.5 Site Environmental History

New Century has fully characterized the site. A summary of completed investigation and remedial activities is presented in Table 1.

3. RBCA EVALUATION

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3.1 Introduction

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The objective of this RBCA assessment is to evaluate the most appropriate corrective action for the site based upon the known distribution of hydrocarbon-related contaminants in the subsurface and their potential (if any) to adversely affect future potential human receptors at the site. To meet this objective, WA has employed the RBCA process as outlined in ASTM Standard E 1739-95, Standard Guide for Risk-Based Corrective Action Applied at Petroleum Release Sites.

The ASTM RBCA framework is a tiered decision-making process whereby site contaminant levels, as determined during an initial site assessment, are compared to conservatively-derived risk-based screening levels (RBSL) for contaminants of concern in each environmental medium. In the RBCA process, Tier 1 - Site Classification and Non-Site-Specific-Screening Level Corrective Action Goals - sites are classified by the urgency of need for initial corrective action, and then site-specific contaminant concentrations are compared to target Tier 1 RBSLs. The ASTM guidance provides example RBSL look-up tables intended as a guide for state and local enforcement agencies; the RBSLs in the look-up tables are not intended to be stand-alone cleanup standards. Site-specific contaminant concentrations below the RBSLs by definition represent human health risks less than the target level, and human health risk may reasonably be assumed to be insignificant if site-specific concentrations are below these target risk levels.

If the Tier 1 RBSLs are exceeded, the RBCA process provides several alternatives for subsequent action. These options include a Tier 2 application of Tier 1 RBSLs at an alternative point(s) of exposure, a Tier 2 analysis including development of Tier 2 site-specific target levels (SSTLs), the provision of institutional or engineering mechanisms to limit or reduce exposures, or remediation to Tier 1 RBSLs. In the Tier 2 analysis included in this document, site-specific risk-based target levels (SSTLs) have been calculated. Similarly to the Tier 1 RBSLs, the Tier 2 SSTLs represent contaminant concentrations below which associated human health risks may reasonably be assumed to be insignificant.

Following this framework, this evaluation includes a brief discussion of the previous site investigation results, identification of the contaminants of concern, a description of potential exposure scenarios, and identification of potentially complete exposure pathways for each scenario. To complete the Tier 1 analysis, the reasonable worst-case contaminant concentration is then identified, and these site-specific concentrations are compared to the appropriate Tier 1 RBSL for each potentially complete exposure pathway.

For exposure pathways where site-specific concentrations exceed the very conservative Tier 1 RBSLs, WA has opted to proceed to a Tier 2 analysis as the most appropriate option. In Tier 2,

SSTLs are calculated following the RBCA framework, and site-specific concentrations are compared to the appropriate Tier 2 SSTL(s) to complete the risk analysis for the site. WA then makes recommendations for future action based on the Tier 2 results.

3.2 Site Assessment

Initial site assessment as suggested by the ASTM framework is the collection and assembly of data required to complete a RBCA Tier 1 analysis. Extensive site characterization has been completed at this site. Site assessment data, specifically analytic results for soil, analytic results for ground water and ground water elevation data, are presented in Appendices A, B and C, respectively. A summary of environmental activities is presented in Table 1.

3.2.1 Identification of Chemicals of Concern

Site investigations have identified specific chemicals of concern (COCs) that are associated with gasoline and diesel in soil and ground water. The COCs that are considered in this evaluation include: benzene, toluene, ethylbenzene and xylenes (BTEX) and four polynuclear aromatic hydrocarbons (PAHs): naphthalene, fluoranthene, fluorene and pyrene.

Although halogenated volatile organic compounds have been detected in soil and ground water, WA has not considered them in this evaluation. However, WA has compared the maximum concentration of each HVOC in soil and ground water with USEPA Preliminary Remediation Goals. All maximum HVOC concentrations are below their respective USEPA PRGs. Therefore, HVOCs in the subsurface do not pose an unacceptable risk to human health.

The distribution of the COCs considered for this evaluation is discussed below.

Surface Soil

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No PAHs have been identified in surface soil, soil between ground surface and 3-ft depth, based on sampling conducted in 1996. Other COCs above laboratory method detection limits have been identified in three areas:

- 1) BETX near the former gasoline underground fuel tank (UST #1) and associated product piping and dispensers. WA excavated surface soil in November 1995 from the area south of the tank, but due to the presence of a site building at the time, overexcavation to completely remove all hydrocarbon contaminated soil could not be completed. Benzene at 0.008 ppm and 5.2 ppm xylenes remain in surface soil in this area.
- 2) Ethylbenzene and xylenes beneath the former vehicle maintenance area. A maximum of 0.98 ppm ethylbenzene and 1.1 ppm xylenes have been detected. Hydrocarbons beneath this area are not associated with the underground fuel tanks and are not considered in this evaluation.

3) Xylenes beneath the chemical storage area in the southeastern portion of the property. Xylenes at 6.1 ppm were detected in one sample. Again, hydrocarbons are not associated with the underground tanks and are not considered in this evaluation.

Since the date that surface soil samples giving these results were collected, the buildings and other structures on site have been completely demolished or removed from the site. During demolition activities this year, it is likely that surface soils in each of these areas were significantly disturbed, likely resulting in significant aeration of these soil and a resulting decrease in contaminant concentration. However, to be conservative, the worst-case concentrations of COCs detected at any time during previous UST investigations were used in this RBCA analysis.

Subsurface Soil

No PAHs have been identified in subsurface soil (soil below 3 ft depth per ASTM definition) based on sampling conducted in 1996. BTEX, however, have been identified in unsaturated subsurface soil in two areas:

- 1) In the vicinity of the former northern underground fuel tank (UST #1) and associated product piping and dispensers and in the smear zone above the water table downgradient of UST #1. WA overexcavated impacted subsurface soil from south of the tank in November 1995. Up to 1.7 ppm benzene remains in subsurface soil.
- 2) In the vicinity of the former southern underground fuel tank (UST #2) and in the smear zone above the water table downgradient of UST #2. WA overexcavated impacted subsurface soil from west of the tank in November 1995. Based on soil sample results, no benzene remains in soil around UST #2.

Xylenes at 0.008 ppm were detected in unsaturated, subsurface soil in two other areas of the site. However, because no other hydrocarbons were detected in soil from these areas, WA has concluded that these positive detections are not significant. Furthermore, these levels are below the maximum used in this evaluation.

Ground Water

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COCs have been detected in ground water samples from monitoring wells and in grab ground water samples from borings onsite. Limited hydrocarbon impacts have been identified in ground water in these areas:

1) Near and downgradient of the former USTs. New Century has been monitoring ground water near and downgradient of these two source areas since 1994. During the most recent four quarters of monitoring, the maximum detected benzene concentration was 1,700 ppb in MW-13. Toluene, xylenes, & ethylbenzene are also present. Low concentrations of four PAHs likely associated with diesel also have been detected: pyrene, fluorene, flouranthene, and naphthalene.

- 2) Beneath the northeast corner of the site. Petroleum hydrocarbons in ground water in this area are likely from an upgradient, offsite source. Grab ground water samples from boring B-10 contained 340 ppb benzene. Only up to 21 ppb benzene was detected in samples from well MW-2.
- 3) Beneath the southeast corner of the site. Petroleum hydrocarbons in ground water in this area are also likely from an upgradient, offsite source. Only 1 ppb benzene was detected in a grab sample from boring B-3 and no BETX were detected in samples from wells MW-3 and MW-4.

Because petroleum hydrocarbons in the latter two areas are the result of offsite sources, WA has not considered data from these areas in the RBCA evaluation. However, the maximum hydrocarbon concentrations in the latter two areas are lower than hydrocarbon concentrations associated with the site source areas.

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3.2.2 Identification of Potential Receptors

Previous investigations have identified potential receptors to COCs beneath the site. A summary of identified potential receptors is presented below.

Human Receptors

Because all site buildings have been demolished and the site is vacant, no current residential or commercial human receptors exist at the site. No offsite receptors are impacted by the known hydrocarbon plume. However, future occupancy is likely, considering that the property will probably be developed. According to the Emeryville Planning Department, the property is zoned for commercial development. Residential development is not planned for the site. Therefore, WA has performed this evaluation assuming that future workers will occupy the property.

Ground Water Wells in the Site Vicinity

There is no current or anticipated future use of ground water at the site. During site demolition, an apparent water supply well was discovered. The discovery was reported to the ACHCSA and the Alameda County Flood Control and Water Conservation Department (ACFCWCD), the local well permitting agency. The well will be properly destroyed by the end of 1996. The well appears to be about 300 to 350 ft deep and does not appear to be screened in the first water-bearing zone. No installation records exist for the well, nor does it appear in any agency files or databases. Anecdoted information indicates that the well was probably installed around when the building was constructed in 1958. The well was not used because the well did not produce water of adequate quality or quantity.

According to the ACFDWCD, no documented domestic or municipal supply wells are within one-half mile of the site. ACFCWCD records show that one industrial supply well is located at 3516 Adeline Street, near the intersection of Adeline and Hollis Streets, about a half-mile south (crossgradient) of the site. The building on the site is signed "City of Paris Cleaners and Dryers" and

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does not appear to be in active industrial use. The well was installed to 97 ft below ground surface in 1936. It is not known whether the well still exists and actively used. To be conservative, WA assumed this well to be a potential receptor for the purpose of this evaluation.

ACFCWCD will allow supply wells near or on the site in the future. However, the ACFCWCD requires a 50-ft deep sanitary seal for municipal and industrial supply wells, and therefore, it is not probable that petroleum hydrocarbons in shallow ground water beneath the site would impact water captured by a future supply well.

Environmental Receptors

WA reviewed topographic maps and surveyed the site vicinity and did not identify any potential environmental receptors. San Francisco Bay is about one-half mile to the west and Temescal Creek, which flows into the Bay, is about 1,500 ft north of the site. Based on their distance from their site, WA does not consider either surface water body to be a potential receptor of COCs from the site.

3.2.3 Exposure Scenarios and Potentially Complete Exposure Pathways

WA selected two exposure scenarios for evaluation. These are a future construction scenario and a future commercial/industrial scenario. The potentially complete exposure pathways for each scenario are presented below.

Construction Scenario

Since the demolition of all site structures in August 1996, the property has remained vacant and unpaved. Sale and development of the property in the near future is likely, and therefore, WA has evaluated possible potential exposure pathways to future construction workers. The following pathways are potentially complete during site construction:

- Inhalation of outdoor air containing volatilized COCs from soil
- Ingestion of, inhalation of or dermal contact with surficial soil containing COCs
- Inhalation of outdoor air containing volatilized COCs from ground water

Commercial/Industrial Scenario

The site will likely be developed into a commercial or industrial facility. Therefore, this scenario considers future exposure to workers that occupy the property for up to 8 hours per day. WA identified the following potentially complete exposure pathways:

- Inhalation of outdoor air containing volatilized COCs from soil
- Inhalation of indoor air containing volatilized COCs from soil
- Ingestion of, inhalation of or dermal contact with surficial soil containing COCs
- Inhalation of outdoor air containing volatilized COCs from ground water

Inhalation of indoor air containing volatilized COCs from ground water

Ingestion of ground water is not considered potentially complete for onsite commercial or industrial receptors. Water will likely be supplied by the local water utility, the East Bay Municipal Utility District. Also, the local permitting agency requires a 50-ft deep sanitary seal for municipal and industrial supply wells. A seal this deep will probably prevent the migration of impacted ground water into any future supply well installed on the property.

Residential Scenario - Ground Water Considerations

WA has identified ingestion of ground water by residential receptors as highly unlikely but possible. Subsurface hydrocarbons are not near or below residential property, and therefore, no residential receptors are currently exposed to petroleum hydrocarbons. However, WA has assumed for the purpose of this evaluation that the industrial supply well might be used for municipal well and that it is downgradient of the site. These are very conservative assumptions considering that WA's well survey identified the well as an industrial supply well, and that it is crossgradient, not downgradient, of the site. Nevertheless, to demonstrate that the well will not be impacted by COCs from the site, WA has considered the well as a potential receptor. Therefore, WA has evaluated the following potentially complete exposure pathway for a residential scenario:

- Impact of ground water for ingestion by COCs in soil leachate
- Ingestion of ground water containing COCs

3.3 Site Classification and Initial Response Action

ASTM Standard E 1739-95 recommends classifying the site as investigation data is assembled to determine the most appropriate initial response action to protect potential receptors. The classification criteria, presented in Table 1 of the Standard, are qualitative. Based upon current site conditions, the site best satisfies the criteria for Classification 3, possible "Long-term (>2 years) threat to human health, safety, or sensitive environmental receptors." This description is the most appropriate because surface soils containing COCs are possibly accessible to the public; the shallowest, potable ground water is likely more than 50 ft below impacted soil; shallow ground water is non-potable and not likely be used; and no buildings are above subsurface COCs.

The initial response action is to "Notify appropriate authorities, property owners, and potentially affected parties, and only evaluate the need to monitor ground water and evaluate effect of natural attenuation on dissolved plume migration,...leachate migration,...[and] dissolved plume migration and restrict access to surface soils." New Century informed all involved parties, has installed 14 ground water monitoring wells monitored ground water beneath the site since March 1994. Up until the site demolition, surface soils were covered by concrete slab or asphalt. Therefore, New Century has satisfied the initial response action.

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3.4 Tier 1 Evaluation

3.4.1 Tier 1 Risk-Based Screening Levels

WA established risk-based screening levels (RBSLs) for each COC and each potentially complete exposure pathway for each of the exposure scenarios evaluated. The RBSLs conservatively assume that future receptors of each pathway will be adjacent to the location of the highest COC concentrations.

The RBSLs in this evaluation are based on a target risk level of 1 x 10⁻⁵ for carcinogens and a chronic hazard quotient of 1.0 for non-carcinogens. The levels have been accepted previously by the ACHCSA. For ethylbenzene, toluene, xylenes and naphthalene in the commercial/industrial scenario, WA used the RBSLs recommended in the ASTM Standard's Table X2.1, "Example Tier 1 Risk-Based Screening Level (RBSL) Look-up Table." For benzene, WA adjusted the ASTM RBSLs to reflect a cancer slope factor of 0.1 mg/kg-day, as established by the California Department of Health Services. Thus, benzene RBSLs used in this evaluation are 29% of those suggested in the Standard's look-up table.

To calculate RBSLs for the other PAHs, fluorene, pyrene and fluoranthene and for all COCs in the construction scenario, WA used the chemical and toxicological properties listed for each hydrocarbon in Table X1.2 of the Standard for the pathway specific equations in Table X2.3. For the construction scenario, RBSLs were calculated using the Standard ASTM equations and toxicological values, and Standard ASTM default values for everything except exposure duration and exposure frequency. Exposure frequency was set to 250 days per year (comparable to commercial/industrial exposure), and exposure duration was set to two years, representing a reasonable worst-case duration for future construction. RBSLs for each COC in each exposure scenario are presented in Tables 2 through 7.

3.4.2 Comparison of Site Concentrations with Risk-Based Screening Levels

WA compiled the maximum concentration for each COC in surface soil (soil between ground surface and 3 ft depth) and subsurface soil (soil deeper than 3 ft below ground surface), and the maximum concentrations detected in ground water during the past four quarters, September 1995 through June 1996. For the construction scenario, WA did not distinguish between surface and subsurface soil because site workers will likely have dermal contact with subsurface soil. The site-specific maximum contaminant concentrations in each medium are presented with their corresponding RBSLs in Tables 2 through 7.

As shown in Tables 2 and 3, all maximum COC concentrations are below the RBSLs for the construction scenario.

For the commercial/industrial scenario (Tables 4 and 5), the maximum concentrations are below the respective RBSLs except for the following exposure pathways for benzene:

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- Inhalation of outdoor air containing volatilized benzene from soil
- Inhalation of indoor air containing volatilized benzene from soil
- Inhalation of indoor air containing volatilized benzene from ground water

All maximum COC concentrations are below the residential RBSLs except the following potentially complete exposure pathways for benzene (Tables 6 and 7):

- Leachate from soil to ground water designated for potential ingestion
- Ingestion of benzene in ground water designated for potential municipal supply

The residential RBSLs were used for ground water because the exposure scenario assumes an off-site residential supply.

3.4.3 Tier 1 Recommendations

The comparison of site-specific maximum contaminant concentrations to conservative Tier 1 RBSLs indicates that no significant adverse risk is posed to future construction workers by the known subsurface contaminants at the site. Therefore, no further action is warranted based on the evaluation of the construction scenario.

For future potential on-site commercial/industrial receptors, the comparison of site-specific maximum contaminant levels to conservative, Tier 1 RBSLs indicates that no significant adverse risk is associated with petroleum-related impacts at the site, with the possible exception of benzene impacts.

Maximum benzene concentrations in soil and ground water exceed the conservative RBSLs for three potentially complete exposure pathways. Because the assumptions in the Tier 1 evaluation very conservatively estimate the risk posed by residual petroleum hydrocarbons beneath the site, and because ample site-specific investigation data are available, WA believes the most appropriate option is to assess each of these pathways specifically in a Tier 2 evaluation.

To evaluate the potential for known petroleum hydrocarbons in soil and ground water to impact potential residential receptors through ground water ingestion, the Tier 1 analysis has very conservatively compared worst-case on-site COC concentrations to residential Tier 1 RBSLs. Even using the very conservative approach, no significant adverse health affects are predicted as a result of the xylene, ethylbenzene, toluene, pyrene, flourene, naphthalene, or flouranthene in ground water. Benzene concentrations in onsite ground water do, however, exceed the conservative Tier 1 RBSL for residential ingestion. The known ground water plume is stable and limited to the site, and future use of shallow onsite ground water is not a reasonable assumption. Furthermore, because monitoring data to date show that the plume is stable, it is extremely unlikely that offsite migration would to occur. Nonetheless, WA has opted to evaluate the benzene impacts on shallow ground water further at Tier 2. In Tier 2, as discussed below, the nearest known ground water supply well will be used as the most reasonable assumed point of exposure.



3.5 Tier 2 Evaluation

The objective of this Tier 2 evaluation is to use site-specific data to determine site-specific target levels (SSTLs) for comparison to site-specific levels of COCs, followed by a determination of the need for further action. Tier 2 SSTLs are typically less than Tier 1 conservative RBSLs, not because they represent a lesser protection to human or ecological receptors, but because the site-specific evaluation eliminates some of the very conservative assumptions used to formulate the RBSLs. In fact, like Tier 1 RBSLs, Tier 2 SSTLs are conservative estimates of the maximum concentrations that do not pose a significant risk to identified receptors. Once the SSTLs are established, WA compares them to maximum site concentrations and makes a recommendation based on this comparison.

3.5.1 Tier 2 Site-Specific Target Levels

The Tier 1 evaluation identified four pathways for which the maximum benzene concentrations in soil and ground water exceeded RBSLs. Only these pathways are evaluated at Tier 2. Three of these are associated with benzene vapor pathway exposures for future commercial receptors, and two are concerning ingestion of ground water for postulated residential exposure. WA derived a SSTL for benzene for each of these pathways as described below. The SSTLs are provided in Table 8 and calculations for each SSTL are included in Appendix E.

Volatilization from Soil to Outdoor Air - Commercial/Industrial Scenario

To establish an appropriate SSTL for benzene in soil, WA used an adaptation of the Jury contaminant transport model as described in Sanders and Stern (1994). Jury originally published this model, describing the transport of organic compounds from a contaminant source through soil in a series of papers in 1983 and 1984, followed by a paper in 1990 (Jury, et al., 1983; Jury, et al., 1984a,b,c; Jury, et al., 1990.) Jury's model, which has been widely used in environmental risk assessments, addresses transport from soil through a thickness of overlying soil to ground surface. It further assumes first-order degradation of the contaminant over time in the media of concern and can be solved for assuming either a finite or infinite contaminant source with a specified initial contaminant concentration.

Using site-specific data, WA calculated the dose and target risk level presented by the maximum benzene concentration in site soil. Then, WA determined the dose that would result in a risk level of 10⁻⁵ and, with this adjusted dose, back-calculated to a soil concentration using the same site-specific data. This back-calculated concentration is the SSTL for this pathway. WA's calculations are shown in Appendix E.

WA input conservative parameters into the model. The maximum benzene concentration in soil, 1.7 ppm at 10 ft depth, was used as the representative concentration in soil. The model assumes all soil between 0.5 and 10 ft has this representative concentration. It also assumes a vadose zone half life for benzene of 365 days, generally accepted as a very conservative value for the vadose zone. The other soil and chemical parameters used to calculate the SSTL are the same values used by the Standard to calculate the Tier 1 RBSL.

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Volatilization from Soil to Indoor Air - Commercial/Industrial Scenario

The Sanders and Stern adaptation of Jury's model allows the calculation of a time-dependent concentration for indoor air, assuming a contaminant source in soil or ground water. WA substituted the surface zone of influence (area of a potential future building) for the soil surface area used by Jury, under the assumption that volatile chemical transport into buildings will be controlled only by the rate of diffusion to the zone of influence. The model then calculates the contaminant flux into a hypothetical building through a foundation slab. The calculation of total dose (i.e., the amount of benzene inhaled over the exposure period) is then made by integrating the rate expression over the entire period.

The representative concentration for soil, contaminant thickness and benzene half-life are the same as used to calculate the SSTL in the volatilization from soil to outdoor air pathway. In addition, WA assumed a worst case scenario of the construction of a future building directly over the source area. This 120 by 330 ft hypothetical building is located directly over an assumed 9.5-ft thickness of soil with a benzene concentration of 1.7 ppm. A slab attenuation factor is used to calculate the flux through the building foundation. The slab attenuation factor corresponds to that in the Johnson and Ettinger model used in the Standard to calculate Tier 1 RBSLs. The resulting Tier 2 SSTL is still an extremely conservative (i.e., health protective) number, because of the conservative nature of the assumptions used as input to the model.

Volatilization from Ground Water to Indoor Air - Commercial/Industrial Scenario

Jury's model also allows the assumption that the contaminant is present at a specified initial concentration in a layer of infinite thickness at some distance below the ground surface, equivalent to an infinite contaminant source. The mathematical solution for the model under this set of assumptions is appropriate for use in establishing the SSTL for benzene in ground water for this transport pathway. The solution assumes an infinite source at an initial source strength in soil. The initial concentration in soil is defined by Jury as the sum of the contaminant present at a specific depth that is i) adsorbed onto soil, ii) as vapor in the air-filled pore spaces, and iii) as a dissolved phase in the liquid-filled pore spaces. With ground water as the contaminant source, it is appropriate to assume that initially no contaminant is adsorbed onto soil or present as a dissolved phase in soil pores, and the initial concentration is completely represented by that in the soil vapor. Thus, WA has calculated the initial source strength assuming contaminants in ground water volatilize into soil and are present as soil vapor at the ground water/soil interface. To convert the worst-case concentration of benzene in ground water to a concentration in the air-filled pore spaces, Henry's Law is assumed to be applicable, and the worst-case concentration in soil vapor is calculated from the worst-case concentration in ground water. This assumption is appropriate for dilute solutions of benzene in ground water and is valid for this site.

As with the volatilization of benzene from soil into indoor air, a hypothetical building is assumed to be located directly above the source. All other parameters are the same except for WA's estimated value for the benzene half-life. WA chose a more conservative value of 730 days because biodegradation is slower beneath the water table due to the limited supply of oxygen.

Leachate from Soil to Ground Water for Ingestion

To calculate a SSTL, WA modeled leaching of benzene from soil into ground water using the Tier 1 default values for soil and chemical parameters that are proposed by the ASTM Standard. After establishing a concentration in ground water based on the soil leachate, the model proceeds as described below for the ground water ingestion SSTL.

Ground Water Ingestion - Residential Scenario

Although shallow ground water beneath the site vicinity has no current or likely future use, WA conservatively assumed that a reported industrial supply well, located a half-mile crossgradient of the site, is hypothetically downgradient of the site and used for municipal supply. WA modeled benzene transport toward this hypothetical receptor by calculating a site-specific dilution-attenuation factor (DAF). The DAF is calculated empirically from concentrations in ground water detected along the longitudinal axis of the dissolved plume. Once the DAF is established, a curve is selected for the site and projected downgradient to predict a concentration at the hypothetical receptor location. The DAF is normalized to the maximum acceptable concentration at the receptor location and the model back-calculates the maximum acceptable concentration at the source that could hypothetically result in the acceptable concentration at the down-gradient location.

For this evaluation, WA selected data from boring B-40, the location of the maximum benzene concentration detected onsite, well MW-13 and MW-8. The acceptable or target concentration at the downgradient point of exposure was set at the MCL for benzene, 1 ppb. The model estimates a SSTL at the source above the solubility limit for benzene. The calculations are presented in Appendix D.

3.5.2 Comparison of Site Concentrations with Site-Specific Target Levels

Table 8 presents a SSTL summary, and compares the SSTLs with maximum on-site contaminant concentrations. As shown, the site-specific maximum contaminant concentrations are below Tier 2 SSTLs for each pathway evaluated at Tier 2.

3.5.3 Tier 2 Recommendations

Considering that the Tier 2 evaluation models rigorously applied conservative input values to formulate each SSTL and that the resulting SSTLs were compared to maximum site concentrations, this Tier 2 evaluation clearly demonstrates that benzene in the subsurface does not pose a risk to human health under a commercial/industrial or residential scenario. Therefore, WA recommends no further risk evaluation concerning petroleum hydrocarbons in soil and ground water beneath the site, and recommends that no further action at the site is necessary.

The Tier 2 evaluation assesses not only potential risk to human health but also to the potential degradation of ground water quality. Even though benzene concentrations in the stable on-site plume exceed the California Department of Health Services maximum contaminant level for

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drinking water, the modeling performed to establish the SSTL for ground water ingestion showed that the dissolved hydrocarbon plume does not pose an unacceptable risk for hypothetical future use of ground water at the point of exposure examined. Strong evidence supports that the plume is stable:

- Benzene concentrations in ground water decreases rapidly to concentrations below laboratory method detection limits between well MW-13 and wells MW-8, MW-11 and MW-14. This suggests that although concentrations remain elevated above MCLs, the plume concentrations attenuate significantly at the downgradient plume edge.
- Even under a steep hydraulic gradient of 0.172 and with a calculated hydraulic conductivity of 9.1 ft/day, dissolved hydrocarbons have not migrated from the original source. Because UST #1 was not used for gasoline storage after 1987, the benzene likely is the result of a pre-1987 release. Thus, petroleum hydrocarbons have migrated less than 240 ft, the distance between the source and the clean downgradient wells, in more than nine years since the time of the release.

4. CONCLUSIONS AND RECOMMENDATIONS

4.1 RBCA Conclusions

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The objective of this RBCA evaluation was to assess the most appropriate future action for the site based on the risk to human health and ground water quality posed by petroleum hydrocarbons in soil and ground water beneath the site. The evaluation can be summarized as follows:

- BETX and four PAHs--naphthalene, fluorene, flouranthene and pyrene--have been identified as contaminants of concern associated with hydrocarbon impacts from the former USTs.
- Three potential exposure scenarios were examined in this analysis. Future
 workers in a construction or commercial/industrial scenario are the most likely
 receptors. Exposure to residential receptors through ground water ingestion is a
 possible but improbable scenario. No sensitive environmental receptors were
 identified near the site; therefore, risks to environmental receptors were not
 considered.
- Potentially complete exposure pathways were identified for all scenarios, and site-specific contaminant concentrations were compared to conservativelyderived Tier 1 RBSLs.
- No Tier 1 RBSLs were exceeded for the construction scenario. All site-specific maximum concentrations of all COCs except benzene were below the Tier 1 RBSLs for the commercial/industrial scenario. Maximum benzene concentrations in soil exceed RBSLs for volatilization from soil into outdoor air, volatilization from soil into indoor air, and volatilization from ground water into indoor air. Benzene in ground water exceeded the Tier 1 RBSL for residential soil leachate to ground water and ground water ingestion
- Tier 2 SSTLs were developed for those pathway/contaminant pairs for which maximum site-specific COC concentrations exceeded the Tier 1 RBSLs using generally accepted modeling methodologies and site-specific characterization data.
- Maximum benzene concentrations in soil and ground water are below Tier 2 SSTLs for all pathways examined.
- Based on WA's ground water modeling to establish a SSTL for the ground water ingestion pathway, the dissolved plume appears stable. It is unlikely that the plume will degrade ground water quality in the site vicinity.

4.2 Proposed RAP Amendment

The RBSLs and SSTLs not only determine maximum acceptable concentrations of COCs, but also may be used to establish target cleanup concentrations based on each COC's risk to human health. Typically, the lowest RBSL for all potentially complete exposure pathways for a COC in a particular medium is selected as the cleanup goal. If a pathway-COC pair is evaluated at Tier 2 to establish a SSTL, then the SSTL is considered in lieu of the RBSL.

Using this methodology, WA has proposed new cleanup goals to replace the cleanup levels proposed in the RAP (Table 9). Because the RBCA process does not evaluate TPH as a viable measure of risk, no TPH cleanup levels are proposed. WA believes that specific COC cleanup goals is more defensible because the reporting standards for TPH differ among analytical laboratories, TPH values may represent concentrations of non-petroleum hydrocarbons, and TPH values measure the aggregate concentrations of possibly hundreds of compounds, many of which may pose little or no health risk.

4.3 Recommendation for Closure

The results of this evaluation conclude that subsurface petroleum hydrocarbons do not pose a significant risk to human health or ground water quality. Therefore, WA recommends that the ACHCSA grant case closure for this site because:

- The underground fuel tanks have been removed.
- New Century has remediated the source. The majority of the hydrocarbonbearing soil from around the former underground fuel tanks was excavated, minimizing future leaching of hydrocarbons into ground water.
- Petroleum hydrocarbons in ground water can be expected to attenuate more rapidly now that the source areas have been remediated. Over two years of monitoring data shows that the plume is stable.
- Future use of shallow ground water is unlikely. Well permits require a minimum 50-ft seal for municipal and supply wells.

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FIGURES



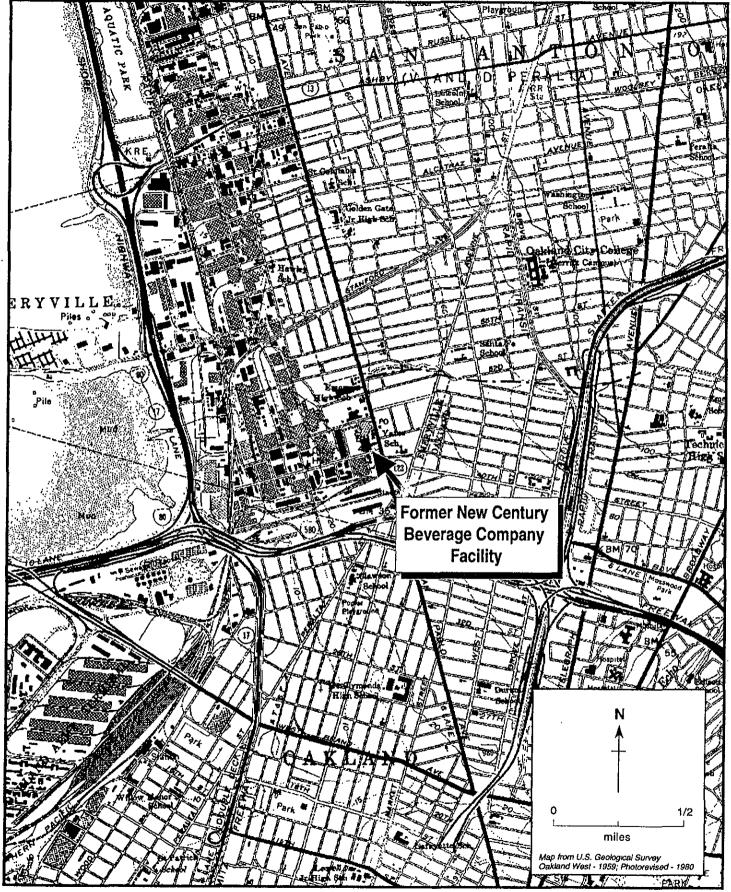


Figure 1. Site Vicinity Map - Former New Century Beverage Company Facility, 1150 Park Avenue, Emeryville, California

Figure 2. Ground Water Monitoring Well and Soil Boring I



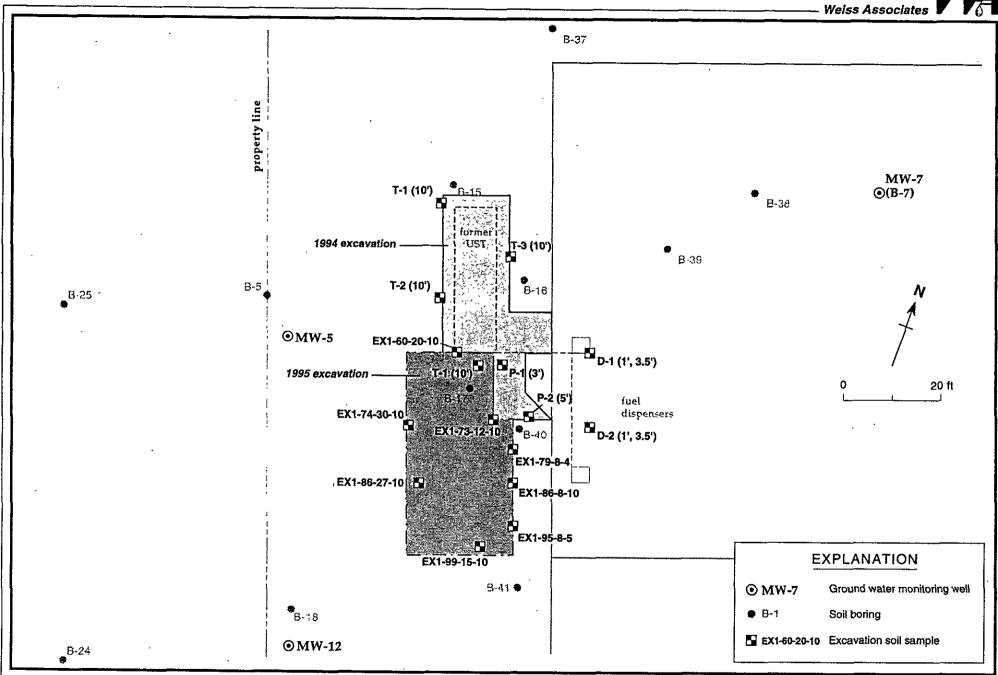
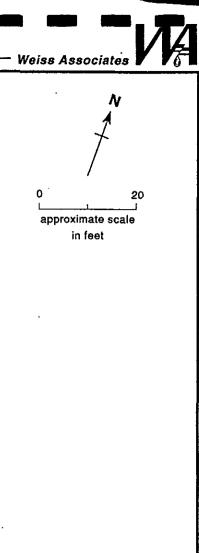
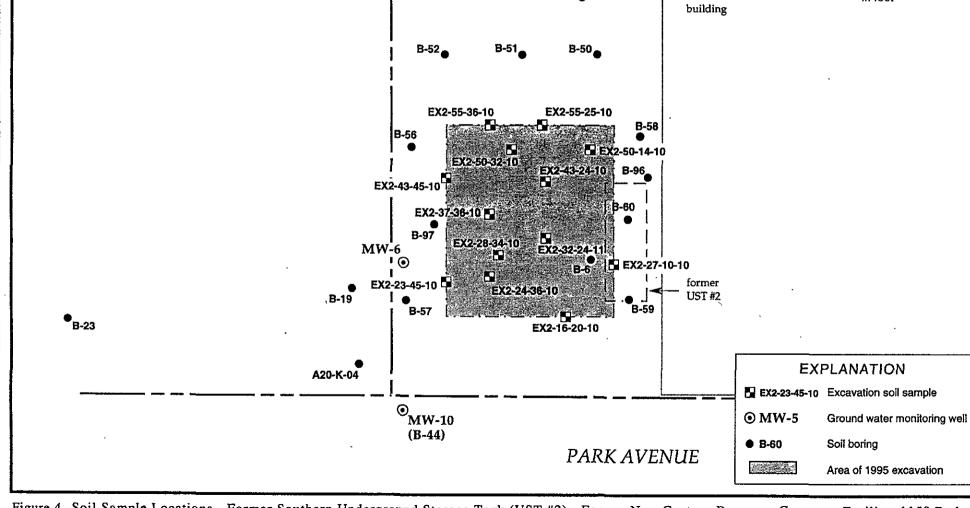


Figure 3. Soil Sample Locations - Former Northern Underground Fuel Tank (UST #1) - Former New Century Beverage Company Facility, 1150 Park Avenue, Emeryville, California



former



B-61

B-55

B-54

property line

Figure 4. Soil Sample Locations - Former Southern Underground Storage Tank (UST #2) - Former New Century Beverage Company Facility, 1150 Park Avenue, Emeryville, California

TABLES

Table 1.	Summary of Environmental Activities - Former New Century Beverage Company
	Facility, 1150 Park Avenue, Emeryville, California

Activity	
Date Completed	

Result

UST #1 and #2 Installations 1958

UST #2 Removal March 1987

UST #1 Decommissioning 1993

Subsurface Investigation October 1993

Subsurface Investigation June-October 1994

The property's USTs may have been installed as early as when the beverage production facility was constructed.

One 10,000-gallon diesel UST (UST #2) was removed from the southwest portion of the property. No TPH-D was detected in soil samples from beneath the tank. No notes are available about the condition of the UST upon its removal. The other UST (UST #1), which had previously stored gasoline, was converted for diesel storage.

The remaining UST (UST #1) was decommissioned but not removed.

As part of a subsurface investigation for Del Monte Plant 35, CH₂M HILL drilled borings A20-K-04 and A20-K-05 on the Del Monte property across the property line from the New Century facility. Soil from boring A20-K-05, located about 100 ft southwest of remaining New Century UST #1, contained 110 parts per million (ppm) total petroleum hydrocarbons as gasoline (TPH-G) and ground water from the boring collected on the adjacent Del Monte property about 50 ft west of former UST #2 contained 220 ppm TPH-D. A grab ground water sample from the same boring contained 1,900 parts per billion (ppb) TPH-G.

WA drilled soil borings B-1 through B-48 and installed ground water monitoring wells MW-1 through MW-12 to:

- Characterize soil and ground water around four onsite potential source areas--UST #1, former UST #2, a vehicle maintenance shop, and an above ground chemical storage area;
- Assess if COCs from offsite sources were in ground water beneath the site; and
- Determine the extent of subsurface COCs that were associated with potential source areas.

Four areas of petroleum hydrocarbon-impacted ground water were identified:

- Gasoline constituents were detected at and downgradient (southwest) of the gasoline UST #1;
- Diesel constituents were detected at and downgradient of the former diesel UST #2;
- Gasoline and diesel constituents were detected beneath the northeastern
 portion of the property, which is downgradient of an UST on the adjacent
 Emeryville Fire Department property; a former UST at the former Oliver
 Rubber Company and a reported subsurface fuel release at the United
 States Post Office; and

Table 1.	Summary of Environmental Activities - Former New Century Beverage Company
	Facility, 1150 Park Avenue, Emeryville, California (Continued)

- Taomer, 1150 Family one, Camerina (Community)		
Activity Date Completed	Result	
Subsurface Investigation June-October 1994 (continued)	 Low concentrations of gasoline constituents were detected beneath the southeastern corner of the property, which is adjacent to a former gasoline service station at the Corner Site restaurant. Except for only 0.007 ppm in one sample, no benzene was detected in unsaturated soil, but a maximum of 1,800 ppb benzene was detected in ground water. 	
UST #1 Removal July 1994	WA coordinated the removal of remaining UST #1 and the associated product piping and dispenser. No holes were noted in the tank and up to 170 ppm TPH-G was detected in soil beneath the tank. Soil from beneath the dispensers contained up to 1,300 ppm TPH-G, 22,000 total petroleum hydrocarbons as diesel (TPH-D) and 0.51 ppm benzene.	
Hydraulic Tests October 1994	WA conducted slug tests on wells MW-5, MW-6, MW-10, MW-11 and MW-12 to estimate the hydraulic conductivity of sediments beneath the site. Based on the test results, hydraulic conductivities ranged between 0.01 and 0.00002 ft per minute.	
Remedial Action Plan Submittal January 1995	WA completed a remedial action plan (RAP). The RAP evaluated possible remedial alternatives and selected soil excavation and continued ground water monitoring as the most appropriate option for the site.	
Soil Excavation October 1995	As proposed in the RAP, WA excavated hydrocarbon-bearing soil from the areas surrounding each former underground fuel tank to remove the hydrocarbon source in the vadose zone. Vadose zone soil was removed from near the northern and southern underground fuel tank (USTs #1 and #2), respectively, and the soil was disposed offsite (Figures 3 and 4). Confirmation soil samples from the former northern tank (UST #1) excavation indicated that most of the soil containing hydrocarbons was removed, except for residual hydrocarbons in soil that was inaccessible due to the presence of the adjacent, former building (Appendix A). After conducting some excavation near the former UST #2, WA determined that it would be cost-effective to cease the excavation and further characterize the soil around this source area.	
Soil Characterization November 1995	WA drilled soil borings B-50 through B-63 to further characterize soil around the former southern fuel tank UST #2. The analytic results for the borings indicate that over 100 ppm TPH-D remains in soil north and west of the final excavation limit. Almost no BETX were detected in soil samples from the 14 borings.	
Ground Water Sampling March 1996	First quarter 1996 ground water monitoring was calculated in March. The ground water sample from well MW-14 was reanalyzed to correct for laboratory analysis errors in May 1996. MW-5, MW-6, MW-12, and MW-13 were also resampled.	
Facility Closing April 1996	New Century closed the facility for the upcoming demolition of the site structures.	

Weiss Associates

Table 2. Future Construction Receptors - Comparison of BETX Concentrations to Tier 1 Risk-Based Screening Levels - Former New Century Beverage Company Facility, 1150 Park Avenue, Emeryville, California.

			Benzer	ne	Ethylben	гепе	Toluen	e	Xylene	s
Source Medium	Exposure Pathway	Potentially Complete Pathway?	Maximum Detected Concentration ^a	RBSL ^b	Maximum Detected Concentration ^a	RBSL°	Maximum Detected Concentration ^a	RBSL ^c	Maximum Detected Concentration ^a	RBSI
Soil (mg/kg)	Volatilization to Outdoor Air	Yes	1.7 B-40, 10 ft 10/10/94	16.6	21 D-2, 3.5 ft 8/05/94	RES	21 D-2, 3.5 ft 8/05/94	RES	100 - D-2, 3.5 ft 8/05/94	RE:
	Vapor Intrusion to Buildings	No	1.7 8-40, 10 ft 10/10/94	0.4	21 D-2, 3.5 ft 8/05/94	13,750	21 D-2, 3.5 ft 8/05/94	681	100 D-2, 3.5 ft 8/05/94	RE
	Ingestion/Dermal/Inhalation	Yes	1.7 B-40, 10 ft 10/10/94	354	21 D-2, 3.5 ft 8/05/94	137,200	21 D-2, 3.5 ft 8/05/94	230,700	100 D-2, 3.5 ft 8/05/94	RE
	Leachate to Ground Water for Ingestion	No	1.7 B-40, 10 ft 10/10/94	2.1	21 D-2, 3.5 ft 8/05/94	20,125	21 D-2, 3.5 ft 8/05/94	4,513	100 D-2, 3.5 ft 8/05/94	RE
Ground Water (mg/l)	Volatilization to Outdoor Air	Yes	1.7 MW-13 12/20/95	667.5	0.67 MW-13 6/25/96	>\$	0.018 MW-12 12/20/95	>S	0.50 MW-12 12/20/95	>5
	Vapor Intrusion to Buildings	No	1.7 MW-13 12/20/95	2.6	0.67 MW-13 6/25/96	>\$	0.018 MW-12 12/20/95	>S	0.50 MW-12 12/20/95	>5
	Ingestion	No	1.7 MW-13 12/20/95	0.36	0.67 MW-13 6/25/96	128	0.018 MW-12 12/20/95	255	0.50 MW-12 12/20/95	>:

RBSL = ASTM RBCA Tier 1 Risk-Based Screening Level

RES = Selected risk level is not exceeded for pure compound present at any concentration in soil.

>S = At pure compound solubility (mg/l), selected risk level is not exceeded.

a = Location and date of sample indicated. Concentrations for ground water are the highest detected onsite during the most recent four quarters of ground water sampling (December 1995 - September 1996).

The RBSLs used for benzene are based on a carcinogenic risk of 1 in 100,000 (10-5) and California Department of Health Services' standard cancer slope factor of 0.1 mg/kg-day.

Table 3. Future Construction Receptors - Comparison of PAH Concentrations to Tier 1 Risk-Based Screening Levels - Former New Century Beverage Company Facility, 1150 Park Avenue, Emeryville, California.

		1	Naphtha	lene	Fluoranth	ene	Fluoren	е	Pyrene	;
Source Medium	Exposure Pathway	Potentially Complete Pathway?	Maximum Detected Concentration	RBSL ^b	Maximum Detected Concentration ²	RBSL ^b	Maximum Detected Concentration ²	RBSL ^b	Maximum Detected Concentration ^a	RBSLb
Soil (mg/kg)	Volatilization to Outdoor Air	Yes	<20	RES	<1.0	NC	<2.0	NC	<1.0	NC
\ <i>\\\\\\\\\\\\</i>	Vapor Intrusion to Buildings	No	<20	1,338	<1.0	NC	<2.0	NC	<1.0	NC
	Ingestion/Dermal/Inhalation	Yes	<20	17,100	<1.0	NC	<2.0	NC	<1.0	NC
	Leachate to Ground Water for Ingestion	No	<20	803	<1.0	NC	<2.0	NC	<1.0	NC
Ground Water (mg/l)	Volatilization to Outdoor Air	Yes	0.0041 MW-13 6/25/96	>\$	0.0005 MW-5 6/25/96	>\$	0.0034 MW-5 6/25/96	>S	0.0005 MW-5 6/25/96	>S
	Vapor Intrusion to Buildings	No	0.0041 MW-13 6/25/96	>S	0.0005 MW-5 6/25/96	> s	0.0034 MW-5 6/25/96	>S	0.0005 MW-5 6/25/96	>S
	Ingestion	No	0.0041 MW-13 6/25/96	5.1	· 0.0005 MW-5 6/25/96	50	0.0034 MW-5 6/25/96	50	0.0005 MW-5 6/25/96	>S

PAH = Polynuclear Aromatic Hydrocarbon

RBSL = ASTM RBCA Tier 1 Risk-Based Screening Level

RES = Selected risk level is not exceeded for pure compound present at any concentration in soil.

< n = Not detected above laboratory mehtod detection omit of n mg/kg

NC = Not calculated

>S = At pure compound solubility (mg/l), selected risk level is not exceeded.

a = Location and date of sample indicated. Concentrations for ground water are the highest detected onsite.

	•		Benzen	le	Ethylben	zene	Toluer	ie	Xylene	es .
Source Medium	Exposure Pathway	Potentially Complete Pathway?	Maximum Detected Concentration ^a	RBSLb	Maximum Detected Concentration ^a	RBSL°	Maximum Detected Concentration ^a	RBSL°	Maximum Detected Concentration	RBSL
Soil (mg/kg)	Volatilization to Outdoor Air	Yes	1.7 B-40, 10 ft 10/10/94	1.33	21 D-2, 3.5 ft 8/05/94	RES	21 D-2, 3.5 ft 8/05/94	RES	100 D-2, 3.5 ft 8/05/94	RES
	Vapor Intrusion to Buildings	Yes	1.7 B-40, 10 ft 10/10/94	0.032	21 D-2, 3.5 ft 8/05/94	1,100	21 D-2, 3.5 ft 8/05/94	54.5	100 D-2, 3.5 ft 8/05/94	RES
	Surficial Soil (0-3 ft depth): Ingestion/Dermal/Inhalation	Yes	0.08 D-2, 1.0 ft 7/19/94	29	0.94 D-2, 1.0 ft 7/19/94	11,500	1.1 D-2, 1.0 ft 7/19/94	18,700	5,2 D-2, 1.0 ft 7/19/94	208,000
	Leachate to Ground Water for Ingestion	No	1.7 B-40, 10 ft 10/10/94	0.17	21 D-2, 3.5 ft 8/05/94	1,610	21 D-2, 3.5 ft 8/05/94	361	100 D-2, 3.5 ft 8/05/94	RES
Ground Water (mg/l)	Volatilization to Outdoor Air	Yes	1.7 MW-13 12/20/95	53.4	0.67 MW-13 6/25/96	> s	0.018 MW-12 12/20/95	>\$	0.50 MW-12 12/20/95	>\$
	Vapor Intrusion to Buildings	Yes	1.7 MW-13 12/20/95	0.21	0.67 MW-13 6/25/96	>S	0.018 MW-12 12/20/95	85	0.50 MW-12 12/20/95	>S
	Ingestion	No	1.7 MW-13 12/20/95	0.029	0.67 MW-13 6/25/96	10.2	0.018 mw-12 12/20/95	20.4	0.50 MW-12 12/20/95	>S

Table 4.

RBSL = ASTM RBCA Tier 1 Risk-Based Screening Level

RES = Selected risk level is not exceeded for pure compound present at any concentration in soil.

>S = At pure compound solubility (mg/l), selected risk level is not exceeded.

= Location and date of sample indicated. Concentrations for ground water are the highest detected onsite during the most recent four quarters of ground water sampling (December 1995 - September 1996).

= The RBSLs used for benzene are based on a carcinogenic risk of 1 in 100,000 (10-5) and California Department of Health Services' standard cancer slope factor of 0.1 mg/kg-day.

Table 6. Future Residential Receptors - Comparison of BETX Concentrations to Tier 1 Risk-Based Screening Levels - Former New Century Beverage Company Facility, 1150 Park Avenue, Emeryville, California

			Benzer	ie	Ethylben	zene	Tolue	1e	Xyle	nes
Source Medium	Exposure Pathway	Potentially Complete Pathway?	Maximum Detected Concentration*	RBSL ^b	Maximum Detected Concentration ^a	RBSL°	Maximum Detected Concentration ^a	RBSL°	Maximum Detected Concentration*	RBSL*
Soil (mg/kg)	Volatilization to Outdoor Air	No	I.7 B-40, 10 ft 10/10/94	0.79	21 D-2, 3.5 ft 8/05/94	RES	21 D-2, 3.5 ft 8/05/94	RES	100 D-2, 3.5 ft 8/05/94	RES
	Vapor Intrusion to Buildings	No	1.7 B-10, 10 ft 10/10/94	0.016	21 D-2, 3 5 ft 8/05/94	427	21 D-2, 3.5 ft 8/05/94	20.6	100 D-2, 3.5 ft 8/05/94	RES
	Surficial Soil (0-3 ft depth): Ingestion/Dermal/Inhalation	No	0.08 B-40, 10 ft 10/10/94	17	0.94 D-2, 1.0 ft 7/19/94	7,830	I.I D-2, 1.0 ft 7/19/94	13,300	5.2 D-2, 1.0 ft 7/19/94	1,450,000
	Leachate to Ground Water for Ingestion	Yes	1.7 B-40, 10 ft 10/10/94	0.050	21 D-2, 3.5 ft 8/05/94	575	21 D-2, 3.5 ft 8/05/94	129	100 D-2, 3.5 ft 8/05/94	RES
Ground Water (mg/l)	Volatilization to Outdoor Air	No	1.7 MW-13 12/20/95	31.9	0.67 MW-13 6/25/96	>S	0.018 MW-12 12/20/95	>S	0.50 MW-12 12/20/95	>S
	Vapor Intrusion to Buildings	No	1.7 MW-13 12/20/95	0.069	0.67 MW-13 6/25/96	77.5	0.018 мw-12 12/20/95	32.8	0.50 MW-12 12/20/95	>\$
	Ingestion	Yes	1.7 MW-13 12/20/95	0.0085	0.67 MW-13 6/25/96	3.65	0.018 MV-12 12/20/95	7.30	0.50 MW-12 - 12/20/95	73

RBSL = ASTM RBCA Tier 1 Risk-Based Screening Level

RES = Selected risk level is not exceeded for pure compound present at any concentration in soil.

>S = At pure compound solubility (mg/l), selected risk level is not exceeded.

The RBSLs used for benzene are based on a carcinogenic risk of 1 in 100,000 (10-5) and California Department of Health Services' standard cancer slope factor of 0.1 mg/kg-day.

a = Location and date of sample indicated. Concentrations for ground water are the highest detected onsite during the most recent four quarters of ground water sampling (December 1995 - September 1996).

Table 8. Comparison of Maximum Benzene Concentrations to Tier 2 Site-Specific Target Levels - Former New Century Beverage Company Facility, 1150 Park Avenue, Emeryville, California.

ļ			Benze	ne
Source Medium	Receptor Scenario	Exposure Pathway	Maximum Detected Concentration*	Site-Specific Target Level ^b
Soil (mg/kg)	Commercial/ Industrial	Volatilization to Outdoor Air	1.7 B-40, 10 ft 10/10/94	119
	Commercial/ Industrial	Volatilization to Indoor Air	1.7 B-40, 10 ft 10/10/94	2.82
	Residential	Leachate to Ground Water for Ingestion	1.7 B-40, 10 ft 10/10/94	RES
Ground Water (mg/l)	Commercial/ Industrial	Volatilization to Indoor Air	1.7 MW-13 12/20/95	2.09
	Residential	Ingestion	1.7 MW-13 12/20/95	>\$

RES = Selected risk level is not exceeded for pure compound present at any concentration in soil.

>S = At pure compound solubility (mg/l), selected risk level is not exceeded.

a = Location and date of sample indicated. Concentrations for ground water are the highest detected onsite during the most recent four quarters of ground water sampling (December 1995 - September 1996).

b = Site-specific target levels are based on a carcinogenic risk of 1 in 100,000 (10.5) and California Department of Health Services' cancer slope factor of 0.1 mg/kg-day.

APPENDIX A

ANALYTIC RESULTS FOR SOIL

Soil

Soil samples from A20-K-04 and A20-K-05 were collected from drill cuttings as a result of organic vapor field equipment readings. Depths to samples were approximated based on auger position. TEPH analysis for those soil samples was run after hold time had expired. During resampling due to laboratory method holding time expirations, soil samples were collected from continuous cores based on highest organic vapor meter readings. Analytical results of soil samples are shown on Table 8.

Table 8

Res	ults of Soil . Del Monte	Analysis, I Plant 35,				
			Anal	yte		
Sample Identification	Gasoline (mg/kg)	Ethyl Benzene (mg/kg)	Xylenes (mg/kg)	Diesel (mg/kg)	TRPH (mg/kg)	1,1,1- TCA (mg/kg)
A20-K-04-7.0	1.6	< 0.005	< 0.005	35	116	0.0071
A20-K-04R- 9.0,9.0(d)	2.5 (3.1)	0.0063	0.0093	220 (220)	NA	NA
A20-K-05 A20-K-05R	110 NA	0.037 NA	· 0.340	<1.0	<10	0.008

SAMPLE DATE 10/28/93

Notes:

²<0.005 indicates that the laboratory detection limit was not exceeded.

Shading indicated that the laboratory holding time was exceeded.

^cAll samples were analyzed for Gas/BTEX, TEPH and Chlorinated hydrocarbons.

^dNA = Not Analyzed

Analytic Results of Soil Samples Collected During Underground Tank Removal, New Century Beverage Company, 1150 Park Avenue, Emeryville,

Sample 10	Depth (ft)	Date Sampled	Sat/ Unsat	Analyte: EPA Method:	TVH-G 8015	TEH . 8015	B 8020	E 8020 parts per mill	7 8020	X 8020	Lead 7420
Tank Exca	avation Sam	ples	•			-			1011 (1119 (11497		
T-1 T-2 T-3 T-4	10.0 10.0 10.0 10.0	07/19/94 07/19/94 07/19/94 07/19/94	Sat Sat Sat Sat		<1 2.0 5.0 170	15 ⁸ 4.0 9.0 74.0	0.059 <0.005 0.14 0.14 ^b	0.009 0.007 0.015 1.9	<0.005 <0.005 0.19 0.46	0.019 0.038 0.87 5.9	
D-1 D-1 D-2 D-2	1.0 4.0 1.0 3.5	07/19/94 08/05/94 07/19/94 08/05/94	Unsat Unsat Unsat Unsat	-	180 1.0 210 1,300	22,000 <1.0 11,000 150	<0.04 <0.005 0.08 0.51	0.28 <0.005 0.94 21.0	0.18 0.008 1.1 21.0	4.1 0.007 5.2 100	
P-1 P-2 Stockpile	3.0 5.0 ed Soil Comp	07/21/94 08/05/94 Posites	Unsat Unsat		120 170	110 6.0	<0.07 0.23 ^b	0.39 2.8	0.35 0.29	1.6 10.0	13
SP-1 SP-2 SP-3		07/20/94 07/20/94 07/20/94			25 2.0 17	950 100 350	<0.005 <0.005 <0.005	0.026 ^b <0.005 0.017	<0.005 <0.005 <0.005	0.12 0.010 0.069	<5.0 <5.0 <5.0

Sat/Unsat = Saturated or unsaturated in-place soil sample TVH-G = Total Volatile Hydrocarbons as Gasoline

TEH = Total Extractable Hydrocarbons - reported as diesel unless noted

B = Benzene

E = Ethylbenzene T = Toluene

X = Xylenes

<n = Not detected at a detection limit of n ppm</pre>

--- = Not analyzed

Notes:

All laboratory analyses completed by Curtis & Tompkins, Ltd., of Berkeley, CA, DHS Certification #1459

- a = Reported as Kerosene Diesel range not reported due to overlap of hydrocarbon ranges
- b = Presence of this compound confirmed by second column; however, the confirmation concentration differed from the reported result by more than a factor of two.



Weiss Associates

Sample Depth TVH-G Date Analyte: TEH B E X T 8020 8020 (ft) Sampled 8015 ID EPA Method: 8015 8020 8020 -parts per million (mg\kg)-----> **Excavation 1 Samples** 11° EX1-60-20-10 10 10/24/95 3 0.017 0.032 0.006 0.077 6^d EX1-74-30-10 10 10/24/95 1 < 0.005 0.008 < 0.005 < 0.005 10 10/24/95 13 <1 EX1-86-8-10 0.065 0.110 0.051 0.240 19^c EX1-86-27-10 10 10/24/95 11 0.040 0.230 0.038 0.200 18^c EX1-99-15-10 10 10/24/95 16 < 0.005 0.210 0.058 0.222 EX1-73-12-10 10 10/24/95 3 20 0.031 0.037 0.008 0.036 23^d EX1-95-8-5 5 10/24/95 <1 < 0.005 < 0.005 < 0.005 < 0.005 EX1-79-8-4 10/24/95 49^d `4 < 0.005 1 0.006 < 0.005 0.010 **Excavation 2 Samples** 10/25/95 22 EX2-43-24-10 10 2,500 < 0.005 0.052 0.060 0.32 580a EX2-27-10-10 10 10/25/95 11 < 0.005 0.029 0.019 0.14 10 EX2-28-34-10 10 10/25/95 1,200 < 0.005 0.028 0.016 0.13 <1 EX2-16-20-10 10/25/95 10 2 < 0.005 < 0.005 < 0.005 < 0.005 10 EX2-50-32-10 10/26/95 <1 28 < 0.005 < 0.005 < 0.005 < 0.005 EX2-24-36-10 10/26/95 2 10 190 < 0.005 < 0.005 < 0.005 0.009 < 0.005 EX2-50-14-10 10 10/26/95 8 970 0.017 0.007 0.10 EX2-37-36-10 10 10/26/95 2 210 < 0.005 0.006 0.005 0.027 EX2-32-24-11 11 10/26/95 1 91 < 0.005 < 0.005 0.009 < 0.005 11/15/95 1,200 EX2-23-45-10 10 17 < 0.005 < 0.005 < 0.005 < 0.005 EX2-43-45-10 10 11/15/95 < 0.005 18 1,500 < 0.005 < 0.005 < 0.005 EX2-55-36-10 10 11/15/95 3,000 < 0.005 17 < 0.005 < 0.005 < 0.005 EX2-55-25-10 11/15/95 1,300 10 43 < 0.013 < 0.013 < 0.013 0.044

Table 1. Analytic Results of Soil Samples Collected During Remedial Soil Excavation, New Century Beverage Company, 1150 Park Avenue, Emeryville, California

Table 1.

Analytic Results of Soil Samples Collected During Remedial Soil Excavation, New Century Beverage Company, 1150 Park Avenue, Emeryville, California, continued

Abbreviations:

Sat/Unsat = Saturated or unsaturated in-place soil sample

TVH-G = Total Volatile Hydrocarbons as Gasoline

TEH = Total Extractable Hydrocarbons - reported as diesel from C-10 to C-42 unless noted

B = Benzene

E = Ethylbenzene

T = Toluene

X = Xylenes

< n = Not detected at a detection limit of n ppm

--- = Not analyzed

Notes:

- a = Laboratory Reported 160 ppm TPH-O, extractable petroleum hydrocarbons from C-20 to C-42 quantified as motor oil.
- b = Sample exhibits pattern which does not resemble standard.
- c = Sample does not match the typical diesel pattern. Sample appears to be jet fuel.
- d = Unidentified hydrocarbons present in diesel and oil range; quantitations based on diesel.

Table 1. Analytic Results for Soil and Open-borchole Water Samples - New Century Beverage Co., 1150 Park Avenue, Emeryville, California

Oth		1,2-DCA	Xylenes	Ethyl- benzene	Toluene	Benzene	ТЕН	TVH-G	Sat/ Unsat	Date Sampled	Depth	Boring ID
>	PCE	1,2-DCA	•	arts per million			<	<				
N	ND	ND	ND	ND	ND	ND	ND	ND	Sat	3/15/94	6.4	B-1
	ND	ND	ND	ND	ND	ND	ND	ND	Sat	3/15/94	8.9	
<u>N</u>	 ND	ND	ND		ND	ND	ND	0.2		3/15/94	Water	
		ND	ND	ND	ND	ND	ND	ND	Unsat	3/16/94	6.0	B-2
N	ND	עא DN .	ND	ND ND	ND	ND	ND	ND	Sat	3/16/94	8.5	
NI NI	ND ND	ND	ND	0.0005	0.0005	<i>ND</i>	ND	ND		3/16/94	Water	
		ND(0.03)	ND	ND	ND	ND	ND	ND	Unsat	3/15/94	2.5	B-3
ND(0.03-0.1	0.28 ND	ND ND	ND	ND	ND	ND	ND	ND	Unsat	3/15/94	7.5	
NI NI	ND ND	ND ND	ND	ND	ND	ND	ND	ND	Unsat	3/15/94	10.0	
	ND	 ND	0.046	0.0084	0.019	0.001	ND	0.52		3/15/94	Water	
	ND	ND	ND	ND	ND	ND	ND	ND	Unsat	3/15/94	5.0	B-4
ND ND	ND ND	ND	ND	ND	ND	ND	49 (K)	ND	Sat	3/15/94	10.0	
ND	ND	ND	ND	ND ND	ND	ND	ND	ND ND		3/15/94	Water	
ND	ND	ND	ND	ND	ND	ND	50 (D) 2,200 (MO)	ND	Unsat	3/14/94	5.0	B-5
ND	ND	ND	ND	ND	ND	ND	ND	ND	Unsat	3/14/94	7.5	
ND	ND	ND	0.012	ND	ND	0.015	ND	ND	Sat	3/14/94	12.5	
ND	MD	ND	0.088	ND(1)	ND(I)	0.18	15 (K)	0.95		3/14/94	Water	
ND	ND	ND	ND	ND	ND	ND	4 (D) 37 (MO)	ND	Unsat	3/14/94	5.0	B-6
ND(0.03-0.1)	ND(0.03)	ND(0.03)	ND(0.03)	0.017	ND(0.03)	ND(0.03)	230 (D) 1,200 (MO)	. 10	Unsat	3/14/94	7.5	
0.001 c1,2-DCE	ND	ND	<5	7	<5	<5	79 (D) 730 (MO)	4.0		3/14/94	Water	
ND	ND	ND	ND	ND	ND	ND	ND	ND	Sat	3/16/94	8.5	B-7
ND ND	ND	ND	ND	ND	ND	ND	ND	ND	Sat	3/16/94	13.5	
 סא	ND	ND	ND	ND	0.002	ND	ND	0.06		3/16/94	Water	

⁻⁻ Table 1 continues next page --

Table 1. Analytic Results for Soil and Open-borchole Water Samples - New Century Beverage Co., 1150 Park Avenue, Emeryville, California (continued)

Oth HVO	PCE	1,2-DCA	Xylenes	Ethyl- benzene	Toluene	Benzene	ТЕН	TVH-G	Sat/ Unsat	Date Sampled	Depth	Boring ID
>				arts per million-			ND	ND	Unsat	3/16/94	5.0	B-8
N:	ND	ND	ND	ND	ND	ND	ND		~	3/16/94	Water	
N	ND	ND	ND	ND	ND	ND	ND	ND ————		·	5.0	B-9
NI	ND	ND	ND	ND	ND	ND	ND	ND	Unsat	3/17/94	Water	-
<u></u>	 ND	 ND	ND	ND	ND	ND	ND	ND		3/17/94		
	ND	ND	ND	ND	ND	. ND	ND	ND	Unsat	3/14/94	5.9	B-10
NI		ND(0.01)	1.9	0.64	0.031	0.34	3 (K)	15		3/14/94	Water	
ND(0.01-0.2)	ND(0.01)			ND	ND	ND	ND	ND	Unsat	3/16/94	2.5	B-11
NE	ND	ND	ND	ND ND	ND	ND	ND	ИD	Unsat?	3/16/94	7.5	
ND	ND	D 	ND .		0.0008	ND	 ND	0.06		3/16/94	Water	
ND	ND	ND	ND	ND			ND	ND	Unsat	3/17/94	7.5	B-12
ND	ND	ND ·	ND	ND 	D	ND	 ND			3/17/94	Water	•
ND	ND	ND	ND	ND,	ND	ND			**		2.5	3-13
0.05 MC 0.009 1,1-DCA	0.005	ND	0.008	ND	ND	ND	2 (D)	ND	Unsat	3/16/94		
0.05 TCE	3.00	ND	ND	ND	ND	ND	ND	ND	Unsat	3/16/94	7.5	-
ND	ND		<u></u>				ND	ND		3/16/94	Water -	
ND	MD				ND	ND	ND	ND	Unsat	3/16/94	2.5	-14
ND	ND	ND	ND	ND	ND	ND	ND	ND	Unsat	3/16/94	7.5	_
ND	ND	ND	0.007	ND	 ND					3/16/94	Water	
ND	ND	ND	ND .	ND		<u> </u>		ND	Unsat	3/17/94	2.5	-15
ND	ND	ND	ND	ND	ND	ND	ND	ND	Unsat	3/17/94	7.5	
ND	ND	ND	ND	ND	ND	ND	ND	0.07		3/17/94	Water	
ND	ND ND	ND	0.0076	0.0011	ND	0.0097	1 (K)				5.0	16
ND	ND	ND	ND	ND	ND	ND	ND	ND	Unsat	3/18/94 3/18/94	7.5	
ND	ND	ND	ND	ND	ND	ND	ND	ND				_
<u>ND</u>	ND	 ND	5.4	1.5	0.28	0.57	15 (K)	<i>38</i>		3/18/94	muler	·

⁻⁻ Table 1 continues next page --



Other HVOCs	PCE	1,2-DCA	Xylenes	Ethyl- benzene	Toluene	Benzene	ТЕН	TVH-G	Sat/ Unsat	Date Sampled	Depth	Boring ID
>		1,2-00/1	•	arts per million-		DC12.016		<	0.000	Jan prot		
ND	ND	ND	0.055	0.005	ND	ND	2 (D) 50 (MO)	1	Unsat	3/17/94	2.5	B-17
ND(0.03-0.1)	ND(0.03)	ND(0.03)	1.4	1.2	0.19	ND(0.08)	190 (K)	130	Unsat	3/17/94	7.5	
0.001 CB	ND	ND	2.4	I.I	0.78	1.8	6 (K)	32		3/17/94	Water	
ND	ND	ND	ND	ND	ND	ND	ND	1	Unsat	3/14/94	8.4	B-18
ND	ND	ND	ND	ND	ND	ND	ND	1	Sat	3/14/94	13.4	
ND	MD	0.003	0.0038	0.0048	0.0006	0.032	ND	0.65		3/14/94	Water	
ND(0.1-0.5)	ND(0.1)	ND(0.1)	0.019	0.061	ND(0.01)	ND(0.01)	150 (D)	23ª	Unsat	3/14/94	7.5	B-19
ND	ND	ND	ND	ND	ND	ND	ND	ND	Sat	3/14/94	12.5	
ND.	ND	ND ND	ND ND	ND	ND	ND	110 (D)	ND		3/14/94	Water	
ND	ND	ND	ND	ND	ND .	ND	ND		Unsat	3/14/94	7.5	B-20
ND	ND	ND	ND	ND	ND	ND	ND	ND	Şat	3/14/94	12.5	
ND	ND	ND	D	DD D	 ND	ND	ND	ND		3/14/94	Water	
ND	ND	ND	ND	ND	ND	ND	ND	ND	Unsat	3/15/94	5.0	B-21
ND	ND	ND	ND(0.1)	ND(0.1)	ND(0.1)	ND(0.1)	ND	11	Sat	3/15/94	10.0	
0.018 CB 0.004 1,2-DCB	ND	ND .	0.0006	ND	ND	ND	ND	0.14		3/15/94	Water	
ND	ND	ND	ND	ND .	ND	ND	ND	ND	Unsat	3/18/94	5.0	B-22
ND(0.03-0.1)	ND(0.03)	ND(0.03)	0.25	0.07	0.98	0.07	340 (D)	130	Sat	3/18/94	7.5	
סא	ND	ND	0.06	0.03	0.02	0.06	220 (D)	6.0		3/18/94	Water	
ND	ND	ND	ND	ND	ND	ND	ND	ND	Unsat	3/30/94	10.0	B-23
ND	ND	ND	ND	ND	ND	ND	ND	ND	Sat?	3/30/94	12.5	
TCE 0.004 c-1,2-DCE 0.006 VC 0.004	ND	ND .	ND	ND	ND.	ND	ND	ND		3/30/94	Water	
ND(0.03-0.1)	ND(0.03)	ND(0.03)	0.19	0.045	ND	0.13	20 (K)	4	Sat?	3/18/94	9.0	B-24
ND	ND	0.004	1.9	0.52	0.03	1.8	2 (K)	22		3/18/94	Water	

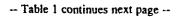




Table I. Analytic Results for Soil and Open-borehole Water Samples - New Century Beverage Co., 1150 Park Avenue, Emeryville, California (continued)

Boring ID	Depth	Date Sampled	Sat/ Unsat	TVH-G	тен	Benzene	Toluene	Ethyl- benzene	Xylenes	1,2-DCA	PCE	. Other HVOCs
				<]	Parts per million-				>
B-25	10.0	3/18/94	Sat?	ND	ND	ND	ND	ND	ND	ND	ND	ND
	12.5	3/18/94	Sat	ND	ND	ND	ND	ND	ND	ND	ND	ND
	Water	3/18/94		ND	ND	MD	ND	ND ND	ND	ND	ND	 סא
B-26	6.0	3/27/94	Unsat	ND	ND	ND	ND	ND	ND	ND	ND	ND
	Water	3/27/94		0.18	ND	0.0012	ND	ND	ND		ND	ND
B-27	Water	3/26/94		ND	ND	ND	ND	ND	ND	ND	ND	ND
B-28	8.5	3/26/94	Sat?	ND	ND	ND	ND	ND	ND	ND	ND	ND
	Water	3/26/94		0.06	ND	ND	ND	ND	ND	ND	ND	 סא
B-29	6.0	3/27/94	Unsat	ND	ND	ND	ND	ND	ND	ND	ND	ND
	Water	3/27/94		20	2 (K)	0.13	0.041	0.77	0.36	ND	DD	D
B-30	6.0	3/27/94	Unsat	ND	ND	ND	ND	ND,	ND	ND	ND	ND
	8.5	3/27/94	Sat?	ND	ND	ND	ND	ND	ND	ND	ND	ND
	Water	3/27/94		· ND	ND	ND	ND	ND	ND	ND	ND	ND
B-31	6.0	3/27/94	Unsat	ND	ND	DM	ND	ND	ND	ND	ND	ND
	8.5	3/27/94	Sat?	ND	ND	ND	ND	ND	ND	ND	ND	ND
	Water	3/27/94		ND	ND	MD	ND	ND ND	ND	 ND	ND	ND.
B-32	8.5	3/26/94	Unsat?	ND	ND	ND	ND	ND	ND	ND	ND	ND
	Water	3/26/94		ND	ND	ND ND	ND	ND ND	ND	ND	ND	0.001 c1,2-DCE
B-33	8.5	3/26/94	Unsat?	ND	ND	ND	ND	ND	ND	ND	ND	ND
	11.5	3/26/94	Sat	ND	ND	ND	ND	ND	ND	ND	ND	ND
	Water	3/26/94		ND	ND	ND ,	ND	ND	ND	ЛD	0.003	0.005 TCE 0.004 c1,2-DCE
B-34	10.0	3/30/94	Sat?	ND	ND	ND	ND	ND	ND	ND	ND	ND
	12.5	3/30/94	Sat	ND	ND	ND	ND	ND	ND	ND	ND	ND
	Water	3/30/94		0.15	ND	0.001	. 0.01	0.003	0.019	ND	ND	ND



Boring ID	Depth	Date Sampled	Sat/ Unsat	TVH-G	тен	Benzene	Toluene	Ethyl-	·····			Other
					<	DCIMEIR		benzene Parts per million-	Xylenes	1,2-DCA	PCE	HVOCs
B-35	10.0	3/30/94	Sat?	ND	ND	ND	ND					>
	Water	3/30/94		ND		 ND		ND	ND	ND	ND ND	ND ND
B-36	7.5	3/30/94	Unsat	ND	ND		ND	MD	<i>N</i> D	ND	ND	TCE 0.002
	10.0	3/30/94	Sat	ND	ND	ND	ND	ND	0.007	ND	ND	ND
	Water	3/30/94				ND	ND	ND	ND	ND	ND	ND
B-37	8.5	3/27/94	Unsat?	<i>ND</i>	ND	ND	ND	ND	0.0005	ND	ND	ND ND
	Water	3/27/94		ND	ND	ДИ	ND	ND	ND	ND	ND	ND
B-38	5.0			ND	<i>N</i> D	ND	ND	ND	ND ND	 ND	ND	0.002 I,I-DCE
2 30	7.5	3/31/94	Unsat	ND	ND	ND	ND	ND	ND	ND	ND	ND
		3/31/94	Unsat	ND	ND	ND	ND	ND	ND	ND	ND	ND
	Water	3/31/94		ΝD	ND	ND	D	ND	ND	 ND	 ND	<u>ND</u> .
-	Water	3/31/94		ND(0.01)	ND (0.01)	ND (0.0003)	ND(0.0003)	ND (0.0003)	ND *	ND	ND	ND ND
B-39	7.5	3/31/94	Unsat	ND	ND	ND	ND	ND	ND			
	10.0	3/31/94	Sat?	ND	ND	ND	ND	ND		ND	ND	ND
	Water	3/31/94		 ND	ND	 ND	 ND		0.01	ND	ND	ND
	Water	3/31/94		ND(0.01)	ND(0.01)	ND (0.0003)	ND (0.0003)	ND	ND	ND	ND	ND
B-40	5.0	10/10/94	Unsat	64	35(K)	0.098	·	ND (0.0003)	ND	ND	ND	ND
	10.0	10/10/94	Sat?	390	100(K)		0.28	0.74	1.2	***		
B-41	5.0	10/10/94	Unsat	ND	·	1.7		. 13	49			_
	10.0	10/10/94	Sat?		ND	ND	ND	ND	ND			
3-42	5.0	10/10/94	Unsat	5	4(K)	110.0	0.012	0.013	ND		_	
3-43	5.0	10/10/94		ND	ND	ND	ND	ND	ND			
3-44	5.0		Unsat	ND	ND	ND	ND	ND	ND			
		10/10/94	Unsat	ND	ND	ND	ND	ND	· ND			
	9.0	10/10/94	Unsat?	ND	ND	ND ND	ND	ND	ND			_
 	Water	10/10/94		ND	ND(0.05) ^d	ND ND	ND	ND	 ND	~		
-45	Water	10/10/94		ND	0.1(K) d	ND	ND	ND	ND			
 _	Water	10/10/94			ND (0.05) *				<i>ND</i>	_		
-4 6	Water	10/10/94		ND	ND (0.05) d	ND	ND	ND	ND			

⁻⁻ Table 1 continues next page --



Table 1. Analytic Results for Soil and Open-borehole Water Samples - New Century Beverage Co., 1150 Park Avenue, Emeryville, California (continued)

Other HVOCs	PCE	1,2-DCA	Xylenes	Ethyl- benzene	Toluene	Benzene	тен	TVH-G	Sat/ Unsat	Date Sampled	Depth	Boring ID
~>				rts per million	Pa		·n	<				
			0.16	ND	ND	0.007	1.8(K)	3	Unsat	10/10/94	5.0	B-48
			42	8	0.77	1.5	52(K)	470	Sat	10/10/94	10.0	
		-	0.019	0.004	ND	0.003	0.13(K) ^d	0.17		10/10/94	Water	
 -							ND (0.05)			10/10/94	Water ^b	
			ND	ND	ND	ND	ND	ND	Unsat	10/10/94	5.0	B-49
			ND	ND	ND	ND	ND	ND	Sat	10/10/94	10.0	
			0.0016	ND	DD OTHER	0.0007	. 0.069 ^d	ND		10/10/94	Water	
ND	ŃD	ND	ND	ND	ND	ND		ND		3/27/94	Water	Travel
ND	ND	ND	ND	ND	ND	ND				3/31/94	Water	Blank
0.002 MC	מא	ND	ND	ND	ND	ND	***			3/31/94	Water	
			ND	ND	ND	ND		ND		10/10/94	Water	
0.005-0.02	0.005	0.005	0.005	0.005	0.005	0.005	1 (K,D)	1	,		Soil	Standard
							30 (MO)					detection
0.001-0.02	0.001	0.001	0.0005	0.0005	0.0005	0.0005	1 (K,D)	0.05			Water	limit
· · · · · · · · · · · · · · · · · · ·							20 (MO)					
			980	3,400	870	1.9	<u>., </u>					PRG
0.03 CE 0.005 1,1-DCA	0.005	0.0005	1.75	0.68	0.1 ^f	0.001	· · · · · · · · · · · · · · · · · · ·		***			MCL
0.13 1,2-DCB 0.006 1,1-DCI 0.006 c1,2-DCI 0.005 MC 0.005 TCI 0.0005 VC					·							

Sat/Unsat = indicates whether soil sample was saturated with ground water

TVH-G = Total volatile hydrocarbons as gasoline detected by EPA Method 8015, modified per California Department of Health Services (DHS) note: mineral spirits were also screened with this method, however, all detected TVH were characterized as gasoline

TEH = Total extractable hydrocarbons [kerosene (K), diesel (D), and motor oil (MO) range] detected by EPA Method 8015, modified by DHS notes: hydraulic oil was also screened with this method, however, no hydraulic oil was reported in any samples

Kerosene-range compounds, where reported, are characterized by the laboratory as a fraction of gasoline hydrocarbons HVOCs = Halogenated volatile organic compounds detected by EPA Method 8010

ND = Not detected at standard detection limit (indicated on the last row of the table)

ND(n) = Not detected at detection limit of n ppm, due to dilution of sample prior to analysis

--- = Not analyzed

PRG = Region IX, US EPA Preliminary Remediation Goal for residential soil

MCL = Maximum Contaminant Level for Drinking Water established by the California Department of Toxic Substances Control

Notes:

Analyses performed by Curtis & Tompkins, Ltd. of Berkeley, CA except as noted (CA DHS certification # 1459)

⁸Reported concentration falls in volatile range but does not match gasoline or mineral spirits fingerprint

^bSplit duplicate analysis:

March 1994 splits performed by GTEL Environmental Laboratories, Inc. of Concord, CA (CA DHS certification # E1075)

October 1994 splits performed by Superior Precision Analytical Laboratories, Inc. of Martinez, CA (CA DHS certification #1542)

^cMethylene chloride was also reported in the method blank at 0.0007 ppm - no methylene chloride was detected in the site ground water samples (methylene chloride is used during some laboratory procedures and is a common laboratory contaminant)

Benzoic acid was reported as a single peak on the chromatogram. Since this is not a fuel compound, the laboratory calculated the TEH concentrations excluding the benzoic acid contribution, and issued a revised report showing these corrected concentrations. Both the revised and uncorrected analytic reports are included in Appendix C.

A single peak on the chromatogram in the range of benzoic acid reportedly attributed to the detection of TEH above the detection limit. Since SPAL could not positively identify the compound at the peak, the report was not revised. However, the reported concentration may not be representative of field conditions since TEH is not detectable if the benzoic acid peak is discounted.

DTSC Recommended Action Level - no MCL established

Table 4. Analytic Results for Soil Samples, Former New Century Beverage Facility, 1150 Park Avenue, Emeryville, California - November 1995.

Boring ID	Boring Interval	Date Sampled	Unsaturated/	TVPH-G	TEPH	Benzene	Toluene	Ethylbenzene	Xylenes
	mervai	Sampled	Saturated	<		Parts	per million-	**	>
B50-5	4.25-5.0	11/30/95	Unsat.	<1	<1	< 0.005	< 0.005	<0.005	<0.005
B50-8	7.3-8.0	11/30/95	Unsat.	3	540(D)	< 0.005	< 0.005	< 0.005	0.039
B50-10	9.25-10.0	11/30/95	Sat.	7	490(D)	< 0.005	< 0.005	< 0.005	0.11
B51-5	4.3-5.0	11/30/95	Unsat.	<1	<1	< 0.005	0.009	< 0.005	0.006
B51-8	7.3-8.0	11/30/95	Unsat.	5	560(D)	< 0.005	< 0.005	< 0.005	0.068
B51-10	9.0-10.0	11/30/95	Sat.	6	480(D)	< 0.005	< 0.005	< 0.005	0.079
B52-5	4.65-5.0	11/30/95	Unsat.	<1	27(D)	< 0.005	< 0.005	< 0.005	< 0.005
B52-8	7.2-8.0	11/30/95	Unsat.	3	440(D)	< 0.005	< 0.005	< 0.005	0.046
B52-10	9.1-10.0	11/30/95	Sat.	12	110(D)	< 0.005	< 0.005	< 0.005	0.16
B53-5	4.25-5.0	11/30/95	Unsat.	<1	1.4(D)	< 0.005	< 0.005	<0.005	<0.005
B53-7	6.6-7.0	11/30/95	Unsat.	<1	1(D)	< 0.005	< 0.005	< 0.005	< 0.005
B53-10	9.15-10.0	11/30/95	Sat.	5	9,800(D)	< 0.005	< 0.005	< 0.005	0.056
B54-5	4.35-5.0	11/30/95	Unsat.	<1	<1	< 0.005	< 0.005	< 0.005	< 0.005
B54-8	7.35-8.0	11/30/95	Unsat.	<1	16(D)	< 0.005	< 0.005	< 0.005	< 0.005
B54-10	9.35-10.0	11/30/95	Sat.	6	13,000(D)	< 0.005	< 0.005	< 0.005	0.089
B55-5	4.4-5.0	11/30/95	Unsat.	<1	2.1(D)	< 0.005	< 0.005	< 0.005	<0.005
B55-8	7.4-83.0	11/30/95	Unsat.	<1	120(D)	< 0.005	0.009	< 0.005	0.010
B55-10	9.35-10.0	11/30/95	Sat.	8	1,500(D)	< 0.005	< 0.005	< 0.005	0.12
B56-5	NR	11/30/95	Unsat.						
B56-8	7.35-8.0	11/30/95	Unsat.	2	510(D)	< 0.005	< 0.005	< 0.005	< 0.005
B56-10	9.4-10.0	11/30/95	Sat.	3	880(D)	< 0.005	< 0.005	< 0.005	0.044
B57-5	4.45-5.0	11/30/95	Unsat.	<1	1.2(D)	< 0.005	< 0.005	< 0.005	<0.005
B57-8	7.3-8.0	11/30/95	Unsat.	<1	140(D)	< 0.005	< 0.005	< 0.005	< 0.005
B57-10	9.4-10.0	11/30/95	Sat.	5	1,100(D)	< 0.005	< 0.005	< 0.005	0.064
B58-5	4.2-5.0	11/30/95	Unsat.	3	830(D)	< 0.005	< 0.005	< 0.005	0.041
B58-8	7.35-8.0	11/30/95	Unsat.	4	1,300(D)	< 0.005	< 0.005	< 0.005	0.048
B58-10	9.3-10.0	11/30/95	Sat.	7	980(D)	< 0.005	0.007	0.031	0.09
B59-5	4.4-5.0	11/30/95	Unsat.	<1	1.4(D)	< 0.005	< 0.005	< 0.005	< 0.005
B59-8	7.3-8.0	11/30/95	Unsat.	<1	<1	< 0.005	< 0.005	< 0.005	< 0.005
B59-10	9.3-10.0	11/30/95	Sat.	<1	<1	< 0.005	< 0.005	< 0.005	< 0.005
B60-5	NR	11/30/95	Unsat.		****				
B60-8	7.6-8.0	11/30/95	Unsat.	<1	95(D)	< 0.005	< 0.005	< 0.005	<0.005
B60-10	9.5-10.0	11/30/95	Sat.	2	1,400(D)	< 0.005	< 0.005	< 0.005	<0.005
B61-5	4.25-5.0	11/30/95	Unsat.	<1	1.8(D)	<0.005	<0.005	<0.005	<0.005
B61-8	7.35-8.0	11/30/95	Unsat.	<1	3.2(D)	<0.005	<0.005	< 0.005	< 0.005
B61-10	9.3-10.0	11/30/95	Sat.	21	300(D)	0.12	0.031	<0.005	0.14

Table 4. Analytic Results for Soil Samples, Former New Century Beverage Facility, 1150 Park Avenue, Emeryville, California - November 1995.

Boring ID	Boring Interval	Date Sampled	Unsaturated/ Saturated	TVPH-G <	ТЕРН	Benzene Parts	Toluene per million-	Ethylbenzene	Xylenes
							·		
B62-5	4.45-5.0	11/30/95	Unsat.	<1	1.2(D)	< 0.005	< 0.005	< 0.005	< 0.005
B62-7	6.55-8.0	11/30/95	Unsat.	<1	1.6(D)	< 0.005	< 0.005	< 0.005	< 0.005
B62-10	9.2-10.0	11/30/95	Sat.	5	560(D)	< 0.005	<0 005	< 0.005	0.061
B63-3	3.2-3.8 ⁻	11/30/95	Unsat.	<1	1.9(D)	< 0.005	< 0.005	< 0.005	< 0.005
B63-8	7.2-8.0	11/30/95	Unsat.	<1	<1	0.009	0.04	0.007	0.033
B63-10	9.3-10.0	11/30/95	Sat.	<1	1.1(D)	< 0.005	<0.005	< 0.005	<0.005
PRG	 _		· · · · · · · · · · · · · · · · · · ·		 -		1.9	870	3,400
MCL							0.001	0.1*	0.68

Sat/Usat = Indicates whether or not sample was saturated with ground water.

TVPH-G = Total volatile petroleum hydrocarbons as gasoline detected by EPA Method 8015, modified per California Department of Health Services (DHS) Note. Mineral spirits were also screened with this method, however, all detected TVPH were characterized as gasoline.

TEPH = Total extractable petroleum hydrocarbons [kerosene (K), diesel (D), and motor oil (MO) range] detected by EPA

Method 8015, modified by DHS. Note Hydraulic oil was also screened with this method, however, no hydraulic oil
was reported in any samples.

NR = No recovery at time of sampling

--- = Not analyzed

PRG = US EPA Region IX Preliminary Remediation Goal for residential soil

MCL = California Maximum Contaminant Level for Drinking Water established by the California Department of Toxic Substances Control (DTSC)

Notes.

Analyses performed by Superior Analytical Laboratory of Martinez, California

*DTSC Recommended Action Level - no MCL established

Table 5. Hydrocarbons in Soil, Former New Century Beverage Facility, 1150 Park Avenue, Emeryville, California - July 1996.

Borehole- Sample	Date Samped	Analytical Lab	TEPH-D	TEPH-U	TVPH-G	TVPH-U	PNA
Depth (ft)		,	<	pa	arts per million		>
B96-1 _. 5	07/29/96	SAL	340	ND			ND
96-7.5	07/29/96	SAL	880				ND
97-1.5	07/29/96	SAL	<1	ND			ND
97-7.5	07/29/96	SAL	460		سنب	****	ND

TEPH-D = Total Extractable Petroleum Hydrocarbons - Diesel

TEPH-U = Total Extractable Petroleum Hydrocarbons - Unknown hydrocarbons

TVPH-G = Total Volatile Petroleum Hydrocarbons - Gasoline range

TVPH-U = Total Volatile Petroleum Hydrocarbons - Unknown hydrocarbons

PNA = Polynuclear Aromatic Hydrocarbons by EPA Method 8310

SAL = Superior Analytical Laboratory, Martinez, California

--- = Not analyzed

ND = None detected

APPENDIX B

ANALYTIC RESULTS FOR GROUND WATER

Table 7 Results of Groundwater Analysis, Area 20 Del Monte Plant 35, Emeryville, California

							Analyt	ė			
Sample Identification	Gasoline (ug/l)	(ug/I)	Ethyl Benzene (ug/l)	(ug/l)	(ug/l)	Trans-1,2- Dichloroethene (ug/l)	Cis-1,2- Dichloroethene (ug/l)	1,1- Dichloroethane (ug/l)	Trichloroethylene (ug/l)	Tetrachloroethene (ug/l)	Dibromochloromethane (ug/l)
A20-K-02	₹50	<0.5	<0.5	< 0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5
A20-K-02R	<50	< 0.5	<0.5	<0.5	NA	NA	NA	NA	NA	NA	NA
A20-K-03	<50	< 0.5	<0.5	<0.5	<0.5	<0.5	1.4	<0.5	1.5	4.9	<0.5
A20-K-04	<50	< 0.5	<0.5	<0.5	<0.5	· <0.5	. <0.5	< 0.5	< 0.5	<0.5	<0.5
A20-K-05	1900	51	12	48	<0.5	<0.5	<0.5	1.9	<0.5	<0.5	<0.5
A20-DM-02	<50	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5
A20-DM-03	<50	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5
A20-DM-04	<50	<0.5	<0.5	<0.5	2.1	<0.5	<0.5	<0.5	<0.5	<0.5	6.6
A20-DM-05	<50	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5
A20-DM-06	<50	<0.5	<0.5	<0.5	5.3	3.8	38	<0.5	21	41	<0.5

10/28/93

Note:

^{&#}x27;<50 indicates that the laboratory detection limit was not exceeded.</p>
'All samples were analyzed for Gas/BTEX, TEPH, and Chlorinated hydrocarbons.

[&]quot;NA = Not Analyzed.

Shading indicates laboratory analysis was performed after hold time had expired.

Boring ID	D. 1	Date	Sat/					Edua	·			
iu	Depth	Sampled	Unsat	TVII-G	TEH	Benzene	Toluene	Ethyl- benzene	Xylenes	1,2-DCA	PCE	Other HVOCs
B-35	10.0	3/30/94	Sat?					-Parts per million-		·····		>
					ND	D	ND.	ND	ND	ND	ND	ND
B-36	7.5	3/30/94		MD	<i>ND</i>	· · MD	ND	ND.	ND	ND	ND	TCE 0.002
	10.0		Unsat	ND	ND	ND	ND	ND	0.007	ND	ND	ND
		3/30/94		ND.	ND	DM	ND	ND	ND	ND	ND	ND
B-37	Water	3/30/94		ND	ND	ND	ND	ND	0.0005	 ND	<u></u> ND	
B-37	8.5	3/27/94	Unsat?	ND	ND	ND	ND	ND	ND	ND		ND
	Water	3/27/94		ND	ND	D		ND	ND		ND	ND
B-38	5.0	3/31/94	Unsat	ND	ND	ND	ND	ND	ND	ND	MD	0.002 I,I-DCE
	7.5	3/31/94 ·	Unsat	ND	ND	ND	ND	םא מא		. ND	ND	ND
	Water	3/31/94		ND	ND	ND ND	 ND		ND	ND	ND 	ND ND
	Water ^b	3/31/94		ND(0.01)	ND(0.01)	ND (0.0003)	ND (0.0003)	ND ATD 40 cooks	ND	ND	ND	ND
B-39	7.5	3/31/94	Unsat	ND				ND (0.0003)	ND *	ND	ND	ND
	10.0	3/31/94	Sat?		ND	ND	ND	ND	ND	ND	ND	ND
	Water	3/31/94		ND	ND	ND	ND	ND	0.01	ND	ND	ND
	Water	3/31/94		ND	ND	ND	ND	ND ND	ND -	ND	ND	ND
B-40	5.0			ND(0.01)	ND(0.01)	ND (0.0003)	ND (0.0003)	ND (0.0003)	MD	מא	ND	ND ND
2 ,0		10/10/94	Unsat	64	35(K)	0.098	0.28	0.74	1.2			112
D 41	10.0	10/10/94	Sat?	390	100(K)	1.7	2.8	13	49	_		· ·
3-41	5.0	10/10/94	Unsat	ND	ND	ND	ND	ND	ND			****
	10.0	10/10/94	Sat?	5	4(K)	0.011	0.012	0.013	ND			
3-42	5.0	10/10/94	Unsat	ND	ND	ND	ND	ND	ND			
3-43	5.0	10/10/94	Unsat	ND	ND	ND	ND	ND		-	-	
3-44	5.0	10/10/94	Unsat	ND	ND	ND	ND		ND		***	
	9.0	10/10/94	Unsat?	ND	ND	ND		ND	·ND			
	Water	10/10/94		ND ND	ND(0.05) ^d	ND	ND	ND	ND			<u></u>
45	Water	10/10/94					ND	ND	ND.	-		
				ND	0.1(K) ^d	ND	ND	ND	ND			
	Water ^b	10/10/94			ND(0.05) *		•	***				
-1 6	Water	10/10/94		ND	ND(0.05) d	ND	ND	ND	ND			

⁻ Table 1 continues next page --



Veiss Associates

Table 1. Analytic Results for Soil and Open-borehole Water Samples - New Century Beverage Co., 1150 Park Avenue, Emeryville, California (continued)

Other HVOCs	PCE	1,2-DCA	Xylenes	Ethyl- benzene	Toluene	Benzene	тен	TVH-G	Sa <i>U</i> Unsat	Date Sampled	Depth	Boring ID
->				rts per million-	Pa	···		<				
-			0.16	ND	ND	0.007	1.8(K)	3	Unsat	10/10/94	5.0	B-48
			42	8	0.77	1.5	52(K)	470	Sat	10/10/94	10.0	
		,	0.019	0.004	ND	0.003	0.13(K) ^d	0.17		10/10/94		
	<u>-</u>	***					ND (0.05)	-		10/10/94	Water ^b	
_		***	ND	ND	ND	ND	ND	ND	Unsat	10/10/94	5.0	B-49
			ND	ND	ND	ND	ND	ND	Sat	10/10/94	10.0	
			0.0016	MD	ND	0.0007	0.069 d	 אD		10/10/94	Water	
ND	ND	ND	ND	ND	ND	ND		ND		3/27/94	Water	Travel
ND	ND	ND -	ND.	ND	ND	ND				3/31/94	Water	Blank
0.002 MC ^c	ND	ND	ND	ND	ND	ND		***		3/31/94	Water	21112
			ND	ND	. ND	ND		ND		10/10/94	Water	
0.005-0.02	0.005	0.005	0.005	0.005	0.005	0.005	t (K,D)	1			Soil	Standard
							30 (MO)					detection
0.001-0.02	0.001	0.001	0.0005	0.0005	0.0005	0.0005	1 (K,D)	0.05			Water	limit
				·			20 (MO)					
			980	3,400	870	1.9		<u> </u>				PRG
0.03 CB 0.005 1,1-DCA	0.005	0.0005	1.75	0.68	0.1	0.001						MCL
0.13 1,2-DCB 0.006 1,1-DCE 0.006 e1,2-DCE 0.005 MC 0.005 TCE 0.0005 VC								· ·				

Sat/Unsat = indicates whether soil sample was saturated with ground water

TVH-G = Total volatile hydrocarbons as gasoline detected by EPA Method 8015, modified per California Department of Health Services (DHS) note: mineral spirits were also screened with this method, however, all detected TVH were characterized as gasoline

TEH = Total extractable hydrocarbons [kerosene (K), diesel (D), and motor oil (MO) range] detected by EPA Method 8015, modified by DHS notes: hydraulic oil was also screened with this method, however, no hydraulic oil was reported in any samples

Kerosene-range compounds, where reported, are characterized by the laboratory as a fraction of gasoline hydrocarbons

HVOCs = Halogenated volatile organic compounds detected by EPA Method 8010

ND = Not detected at standard detection limit (indicated on the last row of the table)

ND(n) = Not detected at detection limit of n ppm, due to dilution of sample prior to analysis

--- = Not analyzed

PRG = Region IX, US EPA Preliminary Remediation Goal for residential soil

MCL = Maximum Contaminant Level for Drinking Water established by the California Department of Toxic Substances Control

Notes:

Analyses performed by Curtis & Tompkins, Ltd. of Berkeley, CA except as noted (CA DHS certification # 1459)

^aReported concentration falls in volatile range but does not match gasoline or mineral spirits fingerprint

^bSplit duplicate analysis:

March 1994 splits performed by GTEL Environmental Laboratories, Inc. of Concord, CA (CA DHS certification # E1075)

October 1994 splits performed by Superior Precision Analytical Laboratories, Inc. of Martinez, CA (CA DHS certification #1542)

Methylene chloride was also reported in the method blank at 0.0007 ppm - no methylene chloride was detected in the site ground water samples (methylene chloride is used during some laboratory procedures and is a common laboratory contaminant)

denzoic acid was reported as a single peak on the chromatogram. Since this is not a fuel compound, the laboratory calculated the TEH concentrations excluding the benzoic acid contribution, and issued a revised report showing these corrected concentrations. Both the revised and uncorrected analytic reports are included in Appendix C.

A single peak on the chromatogram in the range of benzoic acid reportedly attributed to the detection of TEH above the detection limit. Since SPAL could not positively identify the compound at the peak, the report was not revised. However, the reported concentration may not be representative of field conditions since TEH is not detectable if the benzoic acid peak is discounted.

DTSC Recommended Action Level - no MCL established

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Well/ Boring ID	Date Sampled	TVH-G	ТЕН	Benzene	Тошепе	Ethyl- benzene ——— parts per n	Xylenes nillion (mg/L) —	1,2-DCA	PCE	Other HVOCs	МТВЕ
MW-I	03/29/94 05/20/94	ND ND	ND (1) ND	ND ND	ND ND	NĐ ND	ND ND	ND ND	ND ND	ND ND	
MW-2	03/29/94 05/20/94	2.4 1.9	37 (D) 6.7	0.017 0.021	ND (0.001) 0.0086	0.005 0.0061	0.015 0.0059	ND ND	ND ND	ND ND	
MW-3	03/29/94 05/20/94	ND ND	ND (1) ND	ND ND	ND ND	ND ND	ND · ND	ND ND	ND ND	ND ND	
MW-4	03/29/94	0.13	ND (1)	ND	ND	ND	ND	ND	ND	0.017 CB 0.004 I,2-DCB	
	05/20/94 06/01/94	0.22	ь ND	0.0006	0.0015	0.0011	0.0035	ND	ND	0.017 CB 0.005 1,2-DCB	
											•••
/W-5	03/29/94	2.1	30 (K)	0.39	ND (0.003)	ND (0.003)	0.18	ND	ND	ND	
	05/20/94	2.3	2.7 (D)	0.49	0.005	0.033	0.23	ND	ND	ND	
44.4	10/20/94	0.77	9(K)	0.23	ND(0.001)	0.019	0.077			***	
split ^d	10/20/94		ND					air tir-un			
	02/28/95	1.2	3.6 (D)	0.33	0.0016	0.041	0.013				
	06/27/95	0.72	2.1 (D)	0.28	ND	ND	ND				ND
	09/21/95	0.71	3.5 ⁸	0.24	0.0021	0.045 ^j	ND			***	_
	12/20/95	0.86	6.10 ⁸	0.28	0.003	0.039	0.0059				
	03/27/96 05/22/96 ⁿ	1.6 ^g	7.5 ⁸	0.38	0.0008	0.0017	0.031				
	05/22/96	0.75		0.27	0.0045	0.0026	0.01			***	
	09/26/96	0.75	30 ^p	0.18	0.0018	ND	0.0058				
	09/20/90	0.29	4.6	0.120	0.0033	0.0026	0.0091	-			
/IW-6	03/29/94	ND	5 (D)	ND	ND	ND	ND	ND	ND	ND	
	05/20/94	ND	2.4 (D)	ND	ND	ND	ND	ND	ND	ND	
	10/20/94	0.055	NĐ	ND	ND	0.0021	0.0024		ND	ND	
split ^e	10/20/94		0.27 (D)	***			•			720	
	02/28/95		0.78 (D)	ND	ND	ND	ND				
	06/27/95	ND	0.51 (D)	ND	ND	ND	ND				ND
	09/21/95 12/20/95 ^k		0.96 ^{g,h}	ND	ND	ND	ND			•==	

Table 2. Ground Water Analytical Results, Former New Century Beverage Facility, 1150 Park Avenue, Emeryville, California.

Table 2. Ground Water Analytical Results, Former New Century Beverage Facility, 1150 Park Avenue, Emeryville, California. (continued)

Well/	Date	TVH-G	TEH	Benzene	Toluene	Ethyl- benzene	Xylenes	1,2-DCA	PCE	Other HVOCs	МТВІ
Boring ID	Sampled	<				parts per n	nillion (mg/L) —				
MW-6	03/27/96		1.5 ^{g,h}	0.0009	ND	ND	ND				
(cont.)	05/22/96"	•••		ND	ND	ND	ND		***	4	
` ,	06/25/96	ND	1.3 ^q	ND	ND	ND	ND				
	09/26/96		140	ND	ND	ND	ND ND	_			
MW-7	03/29/94	0.16	ND (1)	ND	ND	ND	ND	ND	ND	ND	
dup	03/29/94	ND	ND (I)	ND	ND	ND	ND	ND	ND		***
•	05/20/94	ND	ND	ND	ND	ND	ND	ND	ND ND	ND	
split*	05/20/94	ND	· ND	ND	ND	ND	ND	ND (0.0005)		ND	
dup	05/20/94	ND	ь	ND	ND	ND	ND	(כנייטטט) עא ND	ND (0.0005)	ND	
•	06/01/94		ND			NO	 ND	עא	ND 	ND	
	10/20/94	· ND	ND	ND	ND	ND	ND			•	***
	02/28/95	ND	ND	ND	ND	ND	ND				
	06/27/95	ND	ND	ND	ND	ND	ND				
	09/21/95	ND	0.110 ⁸	ND	ND	ND	ND ND			***	ND
	12/20/95	ND	ND	ND	ND	ND ND	ND ND				ND
	03/27/96	ND	ND	ND	ND	ND	ND		***		
	06/25/96	ND	0.1 ^r	ND	0.0032	ND	0.0006	•••		***	ND
•	09/26/96	ND	ND	ND	ND	ND ND	N D				ND ND
MW-8	04/05/94	ND	ND (1)	ND	ND ·	ND	ND	NID)./D	3.755	
split*	04/05/94	ND(0.01)	ND (1)	ND(0.0003)	0.0004	ND(0.0003)		ND	ND	ND	
	05/20/94	ND ND	ND°	ND	0.0004 ND	ND(0.0003)	ND(0.0003)	ND	ND	ND	****
	10/20/94	ND	ND	ND ND	ND		ND	ND	ND	ND	***
split ^e	10/20/94		ND ND			ND	ND	***	700		***
op	02/28/95	ND	ND	ND	ND			*			
	06/27/95	ND	ND	ND ND	ND ND	ND	ND				***
	09/21/95	ND	ND	ND ND	ND ND	ND ND	ND				ND
	12/20/95	ND	ND	ND ND	ND		ND				***
	03/27/96	ND	ND	ND	ND ND	ND	ND				***
	06/25/96	ND	0.06 ^r	ND ND	ND	ND	ND		***		
	09/26/96	ND	ND	ND ND	ND ND	ND	ND				
				ND	ND	ND	ND	_	***	_	
MW-9	04/05/94	ND	ND (1)	ND	ND	ND	ND	NĐ	ND	ND	
	05/20/94	ND	ND	ND	ND	ND	ND	ND	ND	ND	
MW-I0	10/20/94	ND	ND	ND	ND	ND	ND		4		

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Table 2. Ground Water Analytical Results, Former New Century Beverage Facility, 1150 Park Avenue, Emeryville, California. (continued)

						Ethyl-			•	Other	
Well/	Date	TVH-G	TEH	Benzene	Toluene	benzene	Xylenes	1,2-DCA	PCE	HVOCs	MTBI
Boring ID	Sampled	<		·····		parts per m	illion (mg/L) —			************	
									,		
split ^e	10/20/94		ND	•••	***						
	02/28/95		ND	ND	ND	ND	ND				
MW-10	06/27/95	ND	ND	ND	ND	ND	ND				ND
(cont.)	09/21/95		ND	ND	ND	ND	ND				
	12/20/95	NĐ	ND	ND	ND	ND	ND				
	03/27/96		ND.	ND	ND	ND	ND				
	06/25/96		0.07 ^r	ND	ND	ND	ND				
	09/26/96		ND	ND	ND	ND	ND		_		_
MW-11	10/20/94	ND	ND	ND	ND	ND	ND				
split ^d	10/20/94	ND	ND	ND(0.0003)	ND(0.0003)	ND(0.0003)	ND ND				
op	02/28/95	ND	ND	ND	ND ND	ND(0.0003)	ND ND				
	06/27/95	ND	ND ND	ND	ND	ND					
	09/21/95	ND	0.10 ^{g,i}	ND	ND		ND			***	ND
	12/20/95	ND	ND			ND	ND				***
	03/27/96	ND	ND ND	ND	ND	ND	ND			•••	
	06/25/96	ND		ND	ND	ND	ND				
	09/26/96	ND ND	0.05 ^r ND	ND	ND	ND	ND	***			
	03/20/30	עא	ND	ND	ND	ND	ND	***	-	*****	_
MW-12	10/20/94	0.087	0.13(K)	0.0063	ND	0.0014	0.0027		***		
split ^d	10/20/94	0.057	ND	0.0073	ND(0.0003)	0.0016	0.0029				
• -	02/28/95	0.16	0.077 (K)	0.018	ND	0.0028	0.0027	****			
	06/27/95	ND	0.16 (K)	0.011	ND	ND	0.0009		***		ND
	09/21/95	ND	0.14 ^{g,i}	0.0015	ND	ND	ND				110
	12/20/95	2.8	$0.61^{g,t}$	0.420	0.018	0.170	0.500		***		,
	03/27/96	0.5 ^g	0.38 ^g	0.05	0.0009	0.018	0.0051				
	05/22/96°			0.034	ND	0.013	0.0051				
	06/25/96	0.12	0.35 ^{q,s}	0.0093	ND	0.0027	0.0031				
	09/26/96	ND	0.140 ^{g,i}	0,0024	ND	ND	ND		***		
MW-13	03/30/05	<i>5</i> 0	1.0.475	0.71							
	02/28/95	5.8	1.0 (K)	0.76	0.021	0.049	0.58			450	
dup	02/28/95	6.3	0.74 (K)	0.77	0.013	0.058	0.58			<i>'</i>	
•	06/27/95	4.7	0.35 (K)	1.6	0.01	0.26	0.40				ND (0.03
dup	06/27/95	3.8	0.32 (K)	2.0	ND (0.018)	0.27	0.39				ND (0.07
	09/21/95	4.1	0.34 ^{g,1}	1.1	0.0034	0.15	0.123				
	09/21/95	3.7	0.40 ^{g,i}	1.1	0.008	0.13	0.158				
	12/20/95	4.5	0.15 ⁸	1.7	0.012	0.16	0.273		***		

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Boring ID	Depth	Date Sampled	Sat/ Unsat	тун-с	ТЕН	Benzene	Toluene	Ethyl- benzene	Xylenes	1,2-DCA	PCE	Other HVOCs
					<- 		·	-Parts per million		·	1	` >
B-1	6.4	3/15/94	Sat	ND	'ND	NQ .	ND	· IND	(ND (,ND:	· ND	, ND
	8.9	3/15/94	Sat	ND	ND	ND	` ND	ND	ND	ND	ND	ND
	Water	3/15/94		0.2	אס	סא	סא	ָ אַס	, כמא	, ND,	; ND	
B-2	6.0	3/16/94	Unsat	ND	ND	ND	ND	ND	, ND	, ND	i i	·
	8.5	3/16/94	Sat	ND	ND	ND	ND	ND	ND	ND ND	ND	· ND
	Water	3/16/94		ND	ND	ND	0.0005	: 0.0005	 ND	, ND	į MD	ND
B-3	2.5	3/15/94	Unsat	ND	ND	ND	ND	, ND (ND	ND(0.03)	0.28	·
	7.5	3/15/94	Unsat	ND	ND	ND	, ND	. ND	· ND	ND(0.03)	0.28	ND(0.03-0.1)
	10.0	3/15/94	Unsat	ND	ND	ND	ND	, ND	ND	ND	ND	· ND
	Water	3/15/94		0.52	ND	0.001	0.019	0.0084	0.046	E ND	E ND	ND
B-4	5.0	3/15/94	Unsat	ND	ND	ND	ND	ND	ND	ND	ND:	<u>:</u>
	10.0	3/15/94	Sat	ND	49 (K)	ND	ND	ND	ND	ND	ND	ND ND
	Water	3/15/94	— — — — — .	D	ND	<i>ND</i>	ND	ND:	 DD :	MD;	E ND	<i>אט</i> מא
B-5	5.0	3/14/94	Unsat	ND	50 (D) 2,200 (MO)	ND	. ND ,	ND	ND	ND	ND	ND
,	7.5	3/14/94	Unsat	ND	ND	ND	ND	ND	ND	ND	ND	ND
	12.5	. 3/14/94	Sat	ND	ND	. 0.015	ND	ND	0.012	ND	ND	ND
	Water	3/14/94		0.95	15 (K)	0.18	ND(1)	ND(1)	0.088	ND	 ND	 ND
3-6	5.0	3/14/94	Unsat	ND	4 (D) 37 (MO)	. ND .	ND	ND	ND	ND	ND	ND
	7.5	3/14/94	Unsat	10	230 (D) 1,200 (MO)	ND(0,03)	ND(0.03)	0.017	ND(0.03)	ND(0.03)	ND(0.03)	ND(0.03-0.1)
	Water	3/14/94		4.0	79 (D) 730 (MO)	. <5	<5	7	<5	ND ·	ND .	0.001 c1,2-DCE
L-7	8.5	3/16/94	Sat	ND	ND	ND	ND	ND	ND	ND	ND	ND
· ,	13.5	3/16/94	Sat	ND	ND	ND	ND	ND	· ND	ND	ND	ND
	Water	3/16/94		0.06	ND	ND	0.002	 ND	ND	ND ND	ND	 ND

⁻ Table 1 continues next page --

Table 1. Analytic Results for Soil and Open-borchole Water Samples - New Century Beverage Co., 1150 Park Avenue, Emeryville, California (continued)

Othe HVOC	PCE	1,2-DCA	Xylenes	Ethyl- benzene	Toluene	Benzene	ТЕН	TVH-G	Sav Unsat	Date Sampled	Depth ,	Boring ID
<u>-> </u>				rts per million-	······································	110	ND	ND	Unsat	3/16/94	5.0	B-8
NI	. ND	ND	ND	ND.	- ND-	- ND				3/16/94	Water	
, NI	ND .	· <i>ND</i>	- ND -	D	<i>MD</i> .	. ND	<i>N</i> D			· · · · · · · · · · · · · · · · · · ·	5.0	B-9
ND	ND	ND	ND	ND	ND	ND	D	ND	Unsat	3/17/94	Water	D ,
תאר (ר		· ND	·ND	· ND	· ND	, NID	MD	ND	<u> </u>	3/17/94		
`	" ND	. ND.	ND .	· ND ·	· ND ·	- ND -	ND	ND	Unsat	3/14/94 .	5.9	B-10
) Z OND		ND(0.01)	1.9	0.64	0.031	0.34	3 (K)	15		3/14/94	Water	
ND (0.01-0.2)	ND(0.01)	· · ·	<u> </u>	<u>· </u>	ND	ND	ND	ND	Unsat	3/16/94	2,5	B-11
ND	ND	ND	ND	ND		ND	ND	ND	Unsat?	3/16/94	7.5	
NĎ	, ND	DND		ND .	ND		<u></u> -	0.06		3/16/94	Water	
ND	D	, ND	ND	OND	0.00d8	ND			12	3/17/94	7.5	B-12
ND	· ND	ND	ND	ND	ND	ND	ND	ND	Unsat		Water	
<i>ND</i>	 ND	ND .	ND D	D,	ND .	ND	ND	D		3/17/94		
0.05 MC 0.009 1,1-DCA 0.05 TCE	0.005	ND	0.008	ND	ND .	ND	2 (D)	ND	Unsat	3/16/94	2.5	B-13
ND	ND	ND	ND	ND	ND	ND	ND	ND	Unsat	3/16/94	7.5	-
	ND	 DND	~ ND	ND .	ND .	ND	ND	ND		3/16/94	Water	
ND				···	ND ,	ND	ND	. ND	Unsat	3/16/94	2.5	B-14
ND	ND.	, ND	ND	ND	- ND	ND .	ND	ND ND	Unsat	3/16/94	7.5 ·	•
. ND	ND	ND '	0.007	ND 		ND	<u></u>	ND	·	3/16/94	Water	, . .
ND	- ND	` אס	ND.	ND	ND .				Unsat	3/17/94	2.5	B-15
ND	ND	ND	ND	ND ·	ND ,	ND	ND	ND '	Unsat	3/17/94	7.5	
ND	'ND	ND	ND .	ND	» ND 🧸	. ND	. ND			3/17/94	Water	, -
ND .	ND	ND .	0.0076	0.0011	ND	0.0097	1 (K)	.0.07				D. 16
	· ND	ND	ND	ND	ND	ND	ND	ND	Unsat	3/18/94	5.0	B-16
ND ND	ND	ND	ND	ND	ND	ND .	ND	ND	Unsat	3/18/94	· 7.5	_
ND ND	ND	ND	5.4	1.5	0.28	0.57	15 (X)	. 38		3/18/94	Water	

⁻⁻ Table 1 continues next page --

Boring	b a	Date	Sat/			_		Ethyl-			:	Other
ID	Depth	Sampled	Unsat	TVH-G	TEH	Benzene	Toluene	benzene	Xylenes	1,2-DCA	PCE	HVOCs
		····		<-				Parts per million				> ì
B-17	2.5	3/17/94	Unsat	1	2 (D) 50 (MO)	ND	ND	0.005	0.055	ND	· ND	ָּ אַס
	7.5	3/17/94	Unsat	130	190 (K)	ND(0.08)	0.19	1.2	1.4	ND(0.03)	ND(0.03)	ND(0.03-0.1)
	Water	3/17/94		32	6 (K)	1.8	0.78	1.1	2.4	. ND	ND	0.001 CB
B-18	8.4	3/14/94	Unsat	i	ND	ND .	ND	. ND	,ND	ND	ND	ND
	13.4	3/14/94	Sat .	. 1	ND	ND	ND	ND	ND	· ND	- ND	. ND
	Water	3/14/94		0.65	ND	0.032	0.0006	0.0048	0.0038	0.003	, ND	לא
B-19	7.5	3/14/94	Unsat	· 23ª	150 (D)	ND(0.01)	ND(0.01)	0.061	0,019	ND(0,1)	ND(0.1)	ND(0.1-0.5)
	12.5	3/14/94	Sat	ND	ND	ND	ND	ND	ND ·	ND	· ND	· ND
	Water	3/14/94		· · · ND	110 (D)	ND	ON	ND		ND	ND	ND
B-20	7.5	3/14/94	Unsat	ND	ND	ND	ND	. ND	ND	ND	ND	, ND
	12.5	3/14/94	Sat	ND	· ND	ND	ND	NĎ	ND	ND	ND .	ND
	Water	3/14/94		ND	ND	DΩ	ND	ND	D	D	ND	ND
B-21	5.0	3/15/94	Unsat	ND	ND	ND	ND	ND	ND	ND	ND	ND
٠	10.0	3/15/94	Sat	11	ND	ND(0.1)	ND(0.1)	ND(0.1)	ND(0.1)	ND	ND	ND
	Water	. 3/15/94		0.14	ND	D	ND	ND	0.0006	סא	D	0.018 CB 0.004 1,2-DCB
B-22	5.0	3/18/94	Unsat	ND	ND	ND	ND	ND .	ND	ND	ND	ND
	7.5	3/18/94	Sat	130	340 (D)	0.07	0.98	0.07	0.25	ND(0.03)	ND(0.03)	ND(0.03-0.1)
- :-	Water	3/18/94	,	" <i>:</i> " 6.0	, 220 (D)	0.06	0.02	0.03	0.06	ND	ND	.∵, ND
B-23	10.0	3/30/94	Unsat	.> ND	ND	ND	, ND .	ND	· ND	ND	ND	ND
	12.5	3/30/94	Sat?	ND	ND	ND	ND	ND	ND	ND	ND	ND
•	Water	3/30/94		, ND	D	ַלא אַ	, ND	· MD.	ND	, ND	ND	TCE 0.004
-,	<u>.</u>	*						<u>.</u>			· ·	c-1,2-DCE 0.006 VC 0.004
B-24	9.0	3/18/94	Sat?	4	20 (K)	0.13	ND	0.045	0.19	ND(0.03)	ND(0.03)	ND(0.03-0.1)
-	Water	3/18/94		22 .	2 (K)	1.8	0.03	0.52	1.9	0.004	ND	סא



⁻⁻ Table 1 continues next page --

Table 1. Analytic Results for Soil and Open-borehole Water Samples - New Century Beverage Co., 1150 Park Avenue, Emeryville, California (continued)

Date Sampled	oring D De	Sat/	TVH-G	TEH	Danzana	Tolores	Ethyl-	Yulaman	1.2 DCA	PCE	. Other
Затриси	<i>D</i>	Unsat	1 V M-G	1 EN	Benzene	Toluene	benzene Parts per million-	Xylenes	1,2-DCA	, re	>
0 3/18/94	25	Sat?	ND	ND	ND ·	· ND	ND	ND	· ND	, ND	· ND
5 3/18/94		Sat	· ND	ND	ND	ND	ND	ND	ND	ND	ND
r 3/18/94	!	_ 	, סא	ND	ND	ND	ND	ND	סא	D	אס
0 3/27/94	26	Unsat	ND	ND	ND	ND	ND	ND	· ND	ND	ND
r 3/27/94			0.18	D	0.0012	ND .	ND	ND	D D	ND	אס
r 3/26/94	27		ND	ND	ND	ND	ND	ND	ND	· ND	ND
5 3/26/94	28 ·	Sat?	ND	ND	ND	ND	ND	ND	ND	ı, ND.	ND
r 3/26/94	1		0.06	ND	ND	DM	ND	ND	סא	ND	ND
0 3/27/94	29	Unsat	ND	ND	ND	ND	ND	ND	ND	ND	ND
r 3/27/94			20	2 (K)	0.13	0.041	0.77	0.36	ND	ND	. סא
0 3/27/94	30	Unsat	ND	ND	ND	ND	ND,	ND	ND	ND	ND
5 3/27/94		Sat?	ND	ND	ND	ND	ND	ND	ND	ND	ND
r 3/27/94	. 1		· ND	ΝD	ND	ND	ND	D	ND	ND	סא
0 3/27/94	31	Unsat	ND	ND	ND	ND	ND	ND	ND	ND	ND
5 3/27/94		Sat?	ND	ND	ND	ND	ND	ND	ND	ND	ND
r 3/27/94	1	,	, <i>N</i> D	ND	ND .	ND	D	ND	ND	> ND	ND
5 3/26/94	32	Unsat?	ND	ND	ND .		ND	ND	· ND	ND	ND
7 3/26/94	1		ND	ND	ND .	, ND	ND	ND	ND , ;	ND	0.001 c1,2-DCE
5 3/26/94	33	Unsat?	, ND	ND	ND	- ND	ND	ND	"ND ;	- ND	ND
5 3/26/94	<u>-</u>	Sat	ND	ND	ND	ND	ND	ND	מא .	: ND	ND
3/26/94	, 1		ND	ND	ND ;	ND	ND	ND	ND	0.003	0.005 TCE 0.004 c1,2-DCE
0 3/30/94	34	Sat?	, ND	ND	ND	ND	ND .	ND	- ND	ND	ND
5 . 3/30/94	·	Sat	ND	ND	ND	ND	ND .	ND	ND	ND	ND
r 3/30/94	1		0.15	ND	0.001	· 0.01	0.003	0.019	ND	סא	ND



Table 2. Ground Water Analytical Results, Former New Century Beverage Facility, 1150 Park Avenue, Emeryville, California. (continued)

*** ***				_		Ethyl-			_	Other	
Well/	Date	TVH-G	TEH	Benzene	Toluene	benzene	Xylenes	1,2-DCA	PCE	HVOCs	MTBE
Boring ID	Sampled	<u> </u>				parts per n	nillion (mg/L) —				
dup	12/20/95	3.5	0.59 ^{g,l}	1.2	0.013	0.086	0.258				
dup	03/27/96	4.88	0.23 ⁸	0.98	0.013	0.12	0.238				
dup	03/27/96	4,3 ⁸	0.39 ⁸	1.1	0.0041	0.12	0.16	***			
MW-13	05/22/96		U.	0.310	0.0031	0.039	0.13			***	
(cont.)	06/25/96	1.6	0.48 ^{q,s}	0.510	0.0011	0.039	0.018				
dup	06/25/96	1.5	0.40 ^{q.5}	0.5	0.0011	0.64	0.23			***	
шир	09/26/96	4.9	0.140 ^{g.l}	1.4	ND	0.04	0.23 0.786		***	•••	
dup	09/26/96	1.3	0.072 ^{دن}	0.54	ND ND			-		- .	_
dup	07/20/70	1.0	0.072	0.54	ΝD	0.081	0.188		-	_	
MW-14	06/27/95	ND	ND	ND	ND	ND	ND				ND
	09/21/95	ND	ND	ND	ND	ND	ND			***	
	12/20/95	ND	0.120^{8}	ND	ND	ND	ND			275	
	03/27/96	ND	ND	0.0029	ND	ND	ND			***	
	05/03/96°			ND	ND ·	ND	ND				
	05/07/96°			ND	ND	ND	ND				
	06/25/96	ND	0.07 ^r	ND	ND	ND	ND				
	09/26/96	ND	ND	ND .	ND	ND	ND	***		_	
Travel Blank	03/29/94	ND	***	ND	ND	ND	ND	ND	ND	ND	
	04/05/94	ND		ND	ND	ND	ND	ND	ND	ND ND	
	05/20/94	ND		ND ND	ND	ND					
	10/20/94	ND		ND	ND ND	ND	ND ND	ND	ND	ND	
split ^d	10/20/94	ND		ND(0.0003)	ND(0.0003)		ND ND			***	
split ^e	10/20/94	ND		ND(0.0003)	ND(0.0003)	ND(0.0003) ND					
3piit	03/27/96 ^m			ND ND	ND ND	ND ND	ND				
	03/2/1/90			, ND	ND	ND	ND		***		
Bailer Blank	03/29/94	ND	ND (1)	ND	ND	ND	ND	ND	ND	ND	
	04/05/94	ND	ND (1)	ND	ND	ND	ND	ND	ND	ND	
	05/20/94	ND	0.42b	ND	ND	ND	ND	ND	ND	ND	
	02/28/95	ND	ND	ND	ND	ND	ND	***			
	06/27/95	ND	ND	ND	ND	ND	ND	***			ND
		0.05	0.05 (K,D)	0.0005	0.0005	0.0005	0.0005	0.001	0.001	0.001-0.02	0.002
MCL		NE	NE	0.001	0.1 ^f	0.68	1.75	0.0005	0.005	0.13 1,2-DCB ^f 0.03 CB	NE

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Table 2. Ground Water Analytical Results, Former New Century Beverage Facility, 1150 Park Avenue, Emeryville, California (continued)

Abbreviations:

- TVH-G = Total volatile hydrocarbons as gasoline detected by EPA Method 8015, modified by DHS note: Mineral spirits were also screened with this method for analyses prior to 10/20/94, however, all detectable TVH was characterized as gasoline.
- TEH = Total extractable hydrocarbons [kerosene (K) and diesel (D)] detected by EPA Method 8015, modified per DHS notes: Hydraulic oil and motor oil were also screened with this method for analyses prior to 10/20/94, however, all detected TEH was characterized as kerosene or diesel. All reported kerosene-range TEH was characterized as a fraction of gasoline compounds by the analytical laboratory.

BTEX = Benzene, toluene, ethylbenzene, and xylenes.

HVOCs = Halogenated volatile organic compounds detected by EPA Method 8010

MTBE = Methyl-tert-butyl ether by EPA Method 8020

ND = Not detected at standard detection limit specified on the last row of the table ND(n) = Not detected at detection limit of n ppm, due to dilution of sample prior to analysis

--- = Not analyzed

MCL = Maximum Contaminant Level for Drinking Water established by the California Department of Toxic Substances Control

NE = Not established

Notes:

Benzene, toluene, ethylbenzene, xylenes and MTBE were analyzed by EPA Method 8020

Analyses performed by Curtis & Tompkins, Ltd. of Berkeley, CA except as noted (CA DHS certification # 1459)

- Split duplicate analysis performed by GTEL Environmental Laboratories, Inc. of Concord, CA (CA DHS certification # E1075)
- b. TEH as diesel was detected at 0.42 ppm in the bailer blank collected on 5/20/94, and similar concentrations were reported in well MW-4 (0.31 ppm) and MW-7 (0.45 ppm) samples. Since no TEH was detected in earlier MW-4 and MW-7 samples, this indicated the samples were contaminated with the sampling equipment. Samples were collected in wells MW-4 and MW-7 again on 6/01/94, and no TEH was detected in either sample, consistent with the 3/94 results.

Notes (cont.):

- c. Although no TEH as diesel, kerosene or motor oil was reported, the laboratory reported a single peak on the gas chromatogram that was identified as pentatriacontane (a nonhazardous alkaline or paraffin organic compound C36H74) using EPA Method 8270 (Gas chromatography with Mass spectrometry)
- Split duplicate analysis performed by WEST Laboratory of Sacramento, CA (CA DHS certification #1346)
- e. Split duplicate analysis performed by Superior Precision Analytical Laboratories, Inc. of Martinez, CA (CA DHS certification #1542)
- f. DTSC Recommended Action Level no MCL established
- g. Sample exhibits fuel pattern that does not resemble standard
- h. Heavier hydrocarbons than indicated standard
- Lighter hydrocarbons than indicated standard
- Presence of this compound confirmed by second column; however, the confirmation concentration differed from the reported result by more than a factor of two
- k. Well MW-6 damaged by excavation. Not sampled 12/20/95. Repaired 1/5/96.
- I. Sample exhibits single unknown peak or peaks
- m. Sample analyzed after expiration of holding time.
- n. Analyses performed by Superior Analytical Laboratory, Martinez, California
- o. Analyses performed by Sequoia Analytical, Walnut Creek, California
- p. Lighter hydrocarbons were found in the range of diesel, but do not resemble a diesel fingerprint.
- q. The pattern of the chromatogram resembles a weathered, aged or degraded diesel petroleum hydrocarbon
- Heavier hydrocarbons were found in the range of diesel, but do not resemble a diesel fingerprint. Possible motor oil.
- s. Sample also contains gasoline

Table 3. Polynuclear Aromatic Hydrocarbons in Ground Water-New Century Beverage Co., 1150 Park Avenue Emeryville, California

Weil ID	Date Sampled	Naphthalene	Fluorantheneparts per	Fluorene million	Pyrene
MW-5	06/25/96	ND	0.0005	0.0034	0.0005
MW-6	06/25/96	ND	ND	ND	ND
MW-13	06/25/96	0.0041	ND	0.0003	ND

ND = Not detected above laboratory detection limit.



APPENDIX C

HISTORICAL GROUND WATER ELEVATION DATA

Table 1. Historical Ground Water Elevations - New Century Beverage Co., 1150 Park Avenue, Emeryville, California Top-of-Casing Ground Water Elevation Depth to Water -Elevation Well ID (ft above msl) Date (ft) (ft above msl) MW-1 03/27/94 38.74 5.90 32.84 03/29/94 5.89 32.85 04/15/94 6.24 32.50 05/20/94 5.79 32.95 02/28/95 5.13 33.61 06/27/95 7.69 31.05 09/21/95 8.25 30.19 12/20/95 5.94 32.80 03/27/96 4.96 33.78 06/25/96 6.81 31.93 MW-2 03/27/94 38.87 6.57 32.30 03/29/94 6.58 32.29 04/15/94 6.86 32.01 05/20/94 6.45 32.42 02/28/95 5.64 33.23 06/27/95 7.34 31.53 09/21/95 8.80 30.07 12/20/95 6.81 32.06 03/27/96 5.78 33.09 06/25/96 -⁷7.34 31.53 MW-3 03/29/94 40,79 10.69 30.10 04/15/94 10.90 29.89 05/20/94 10.81 29,98 02/28/95 10.35 30.44 06/27/95 10.43 30.36 09/21/95 10.65 30.14 12/20/95 10.65 30.14 03/27/96 10.50 30.29 06/25/96 10.73 30.06 MW-4 03/27/94 40.15 8.23 31.92 03/29/94 8.21 31.94 04/15/94 8.78 31.37 05/20/94 8.54 31.61 02/28/95 7.71 32,44 06/27/95 7.90 32.25 09/21/95 8.50

31.65

Historical Ground Water Elevations - New Century Beverage Co., 1150 Park Avenue, Table 1, Emeryville, California Top-of-Casing Ground Water Elevation Depth to Water Elevation Well ID (ft above msl) Date (ft) (ft above msl) MW-4 12/20/95 8.05 32.10 (cont.) 03/27/96 7.74 32.41 06/25/96 8.29 31.86 MW-5 03/27/94 36.49 8.02 28.47 03/29/94 7.93 28.56 04/15/94 8.10 28.39 05/20/94 7.88 28.61 10/20/94 9.45 27.04 02/28/95 7.57 28.92 06/27/95 8.99 27.50 09/21/95 9.56 26.91 12/20/95 9.02 27.47 03/27/96 7.60 28.89 06/25/96 27.79 MW-6 03/27/94 35.52 9.60 25.92 03/29/94 9.59 25.93 04/15/94 9.64 25.88 05/20/94 9.47 26.05 10/20/94 10.51 25.01 02/28/95 35.531 8.54 26.99 06/27/95 10.02 25.51 09/21/95 10.47 25.05 12/20/95 2 03/27/96 b 9.01 06/25/96 35.48² 9.96 25.52 MW-7 03/27/94 37.53 7.25 30.28 03/29/94 7.27 30.26 04/15/94 7.47 30.06 05/20/94 7.25 30.28 10/20/94 8.87 28.66 02/28/95 6.89 30.64 06/27/95 7.90 29.63 09/21/95 8.81 28.72 12/20/95 7.10 30.43 03/27/96 6.67 30.86 06/25/96 8.01 29.52

Table 1. Historical Ground Water Elevations - New Century Beverage Co., 1150 Park Avenue, Emeryville, California Top-of-Casing Ground Water Elevation Depth to Water Elevation Well ID (ft above msl) Date (ft) (ft above msl) MW-8 04/05/94 33.11 9.03 24.08 04/15/94 8.94 24.17 05/20/94 8.70 24.41 10/20/94 10.00 23.11 02/28/95 8.48 24.63- -06/27/95 9.64 23.47 09/21/95 9.83 23.28 ... 12/20/95 8.80 24.31 03/27/96 8.83 24.28 06/25/96 10.11 23.00 MW-9 04/05/94 36.06 7.60 28.46 04/15/94 7.60 28.46 05/20/94 7.39 28.67 02/28/95 6.85 29.21 06/27/95 8.31 27.75 09/21/95 8.75 27.31 12/20/95 7.73 28.33 03/27/96 7.48 28.58 06/25/96 8.18 27.88 MW-10 10/20/94 35.03 10.14 24.89 02/28/95 -8.98 26.05 06/27/95 9.59 25.44 09/21/95 10.00 25.03 12/20/95. 8.88 26.15 03/27/96 8.98 26.05 06/25/96 9.74 25.29 MW-11 10/20/94 32.74 9.71 23.03 02/28/95 7.66 25.08 06/27/95 8.86 23.88 09/21/95 9.44 23.30 12/20/95 8.81 23.93 03/27/96 8.07 24.67 06/25/96 9.72 23.02 MW-12 10/20/94 36.18 12.66 23.52

7.60

28.58

02/28/95

Table 1. Historical Ground Water Elevations - New Century Beverage Co., 1150 Park Avenue, Emeryville, California

Top-of-Casing Ground Water

Well ID	Date	Top-of-Casing Elevation (ft above msl)	Depth to Water (ft)	Ground Water Elevation (ft above msl)
MW-12	06/27/95		9.56	26.60
(cont.)	09/21/95		10.17	26.62 26.01
	12/20/95		8.19	27.99
	03/27/96		8.66	27.52
	06/25/96		9.63	26.55
MW-13	02/28/95	34.65	8.72	25.93
	06/27/95		8.99	25.66
	09/21/95		10.37	23.66 24.28
·	12/20/95		10.20	24.45
	03/27/96		9.22	25.43
	06/25/96	200	11.16	23.49
MW-14	06/27/95	33.68	9.88	23.80
	09/21/95		10.07	
	12/20/95		9.02	23.61
	03/27/96		9.15	∴ 24.66 24.53
	06/25/96	•	10.08	23.60

Notes:

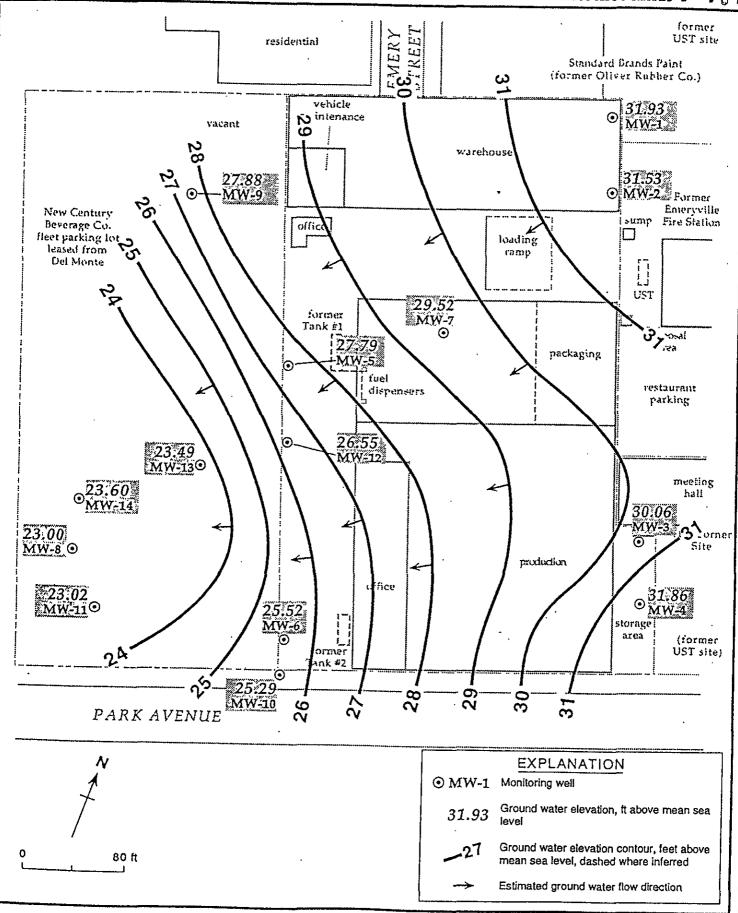
Resurveyed 3/13/95.

² Resurveyed 5/3/96 by PLS Surveys, Inc., Alameda, CA.

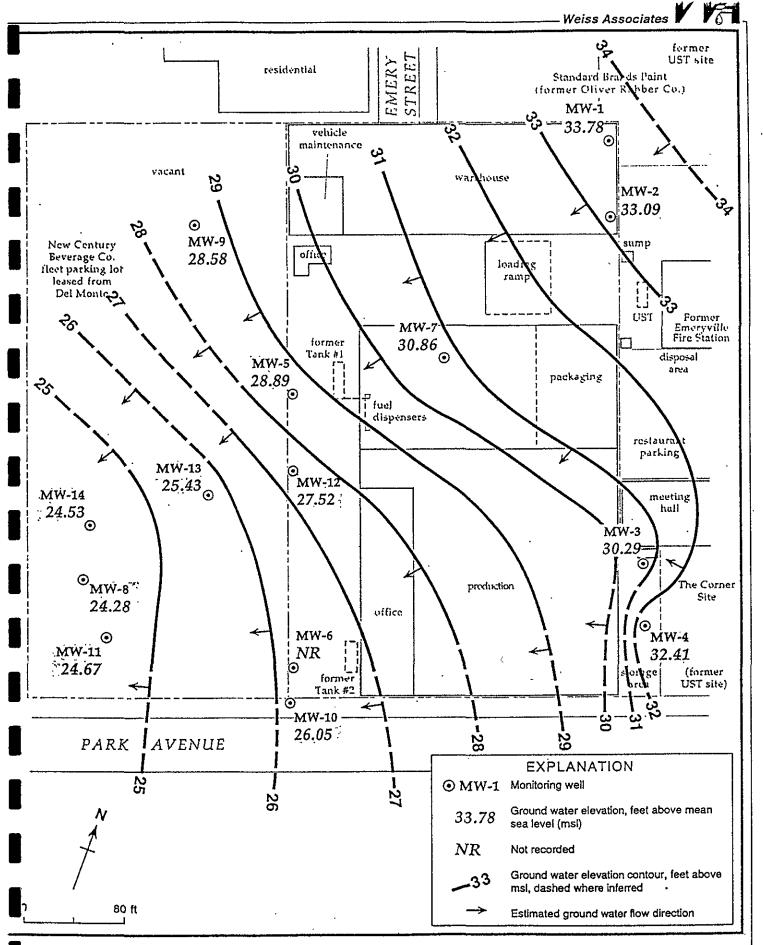
^{*} Well MW-6 damaged by excavation, therefore no water level was taken at MW-6 on 12/20/95.

^b Well MW-6 was repaired 1/5/96. Well MW-6 top-of-casing elevation will be resurveyed during 5/96. No ground water elevation calculated at well on 3/27/96.

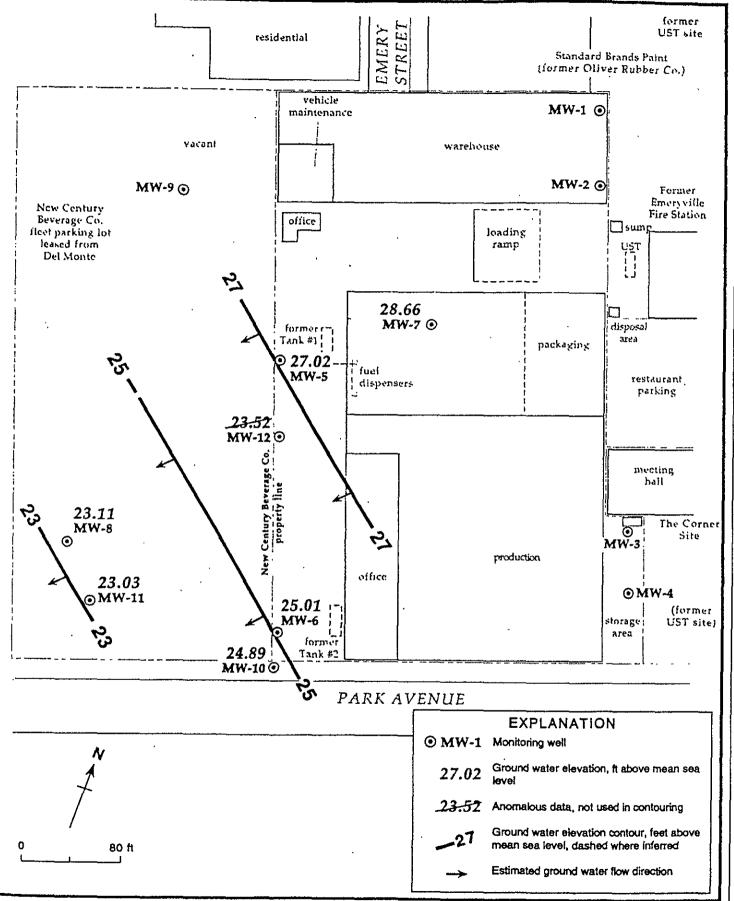




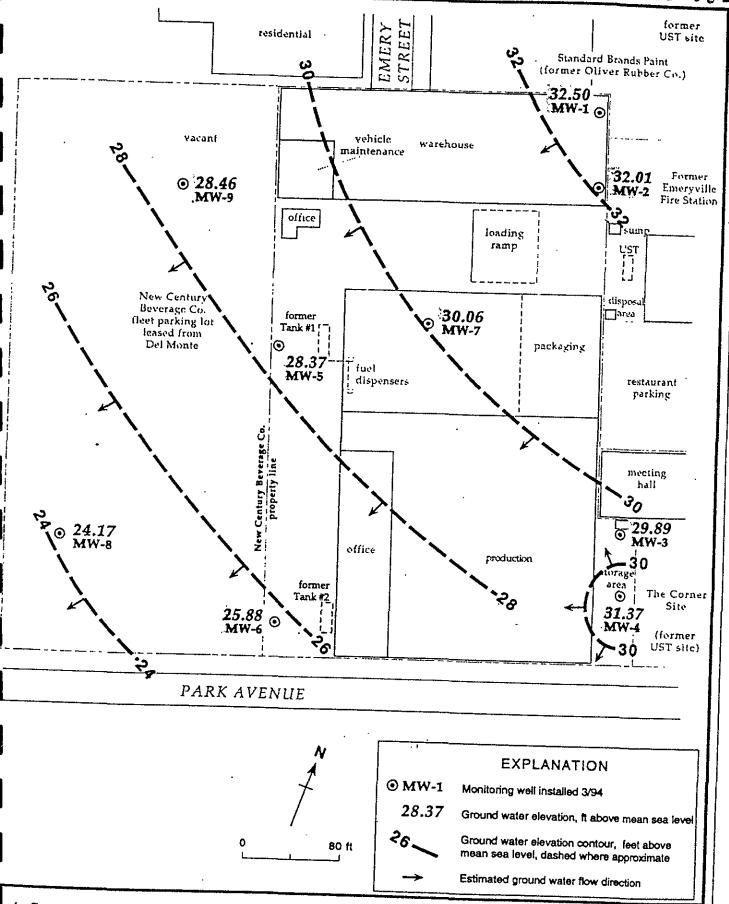
igure 2. Ground Water Elevation Contours and Estimated Flow Direction - June 25, 1996 - New Century Beverage Company, 1150 Park Avenue, Emeryville, California



ure 2. Ground Water Elevation Contours and Estimated Flow Direction - March 27, 1996 - New Century Beverage Company, 1150 Park Avenue, Emeryville, California



gure 8. Ground Water Elevation Contours and Estimated Flow Direction - October 20, 1994 - New Century Beverage Company, 1150 Park Avenue, Emeryville, California



4. Ground Water Elevation Contours and Estimated Flow Direction - April 15, 1994 - New Century Beverage Company, 1150 Park Avenue, Emeryville, California

APPENDIX D

TIER 1 RBSL CALCULATIONS

Pepsi Emeryville RBCA Comm/Ind Scenario

					Commercial/I	ndustrial RBS	SLs		
Chemical Specific Parameters		Benzene	Toluene	EB	Xvlenes		F1		
Carcinogenic/noncarcinogenic					,	Naphth.	Fluorene	Fluoranth.	Pyrene
		С	nc	nc	nc	nc	nc	nc	nc
Henry's Constant	Н	0.22	0.26	0.32	0.29	0.049	4.87E-03	2.79	2.91E-07
Air Diffusion Coefficient (cm^2/s)	D ^{air}		0.085	0.076	0.072	0.072	3.63E-02	3.02E-02	2.72E-02
Water Diffusion Coefficient (cm^2/s)	D ^{wat}	1.10E-05	9.40E-06	8.50E-06	8.50E-06	9.40E-06	7.88E-06	6.35E-06	7.24E-06
Effective Diffusion Coefficient soil (cm^2/s) calc	D ^{eff} s	7.26E-03	6.63E-03	5.93E-03	5.62E-03	5.62E-03	2.84E-03	2.36E-03	1.50E-01
Carbon - Water Sorption Coefficient (L/kg)	k _{oc}	38	134.90	95.5	239.9	1288.2	7244.35	38018.94	38018.9
Log carbon-water sorption (calculated) (L/kg)	Log Koc	1.58	2.13	1.98	2.38	3.11	3.86	4.580000004	4.58
Soil-water sorbtion coeff (calculated)	ks	0.38	1.35	0.96	2.40	12.88	72.44		
Solubility (mg/l)	S	1750	535	152	198	31	1.69	0.206	0.132
Reference dose oral	RfDo		0.2	0.1	2		0.04	1	0.132
Reference dose - inhal	RfDi		0.11	0.29			0.04	1	0.03
Cancer slope factor-inhal (kg-day/mg)	SFi	0.1							
Cancer slope factor- oral (kg-day/mg)	SFo	0.1					-		
Calculated parameters									
Volatilization factors, subsoil -> outdoor (mg/m3	VFsamb	1.10E-03	3.94E-04	1.27E-03	1.10E-03	2.00E-04	1.02E-05	2.50E-03	3.23E-08
Vol factor surficial soil-ambient air (1)	VFss-1	,				5.37E-09	5.09E-10		
Vol factor surficial soil - ambient air (2)	VFss-2		7.1912E-06	7.1912E-06		7.19E-06	7.19E-06		7.19E-06
Max vol factor (correction to ASTM)	VFss	7.19E-06	7.1912E-06	7.1912E-06		7.19E-06	7.19E-06		7.19E-06
Surficial soil part - ambient air	VFp	2.3E-12	2.3E-12	2.3E-12	2.3E-12	2.30E-12	2.30E-12		2.30E-12
Soil conc for sat vapor and pore-water (mg/kg)	Csat	847.74	780.73	163.33	497.76	401.76	122.55	78.42	50.19
Commercial/Industrial RBSLs									
RBSL - outdoor ambient air (ug/m³ - air)		1.43	562	1482	10220	20	204	204	153
RBSL - subsurface soil to outdoor air (mg/kg	1)	1.30	1427	1171	9317	102	20002	1	4749129
RBSL - surficial soil (mg/kg)	· · · · · · · · · · · · · · · · · · ·	28.34	18453	10974	202430	1	13684		10263
RBSL - gw to outdoor air (mg/l)	***	52.82	2.09E+04	5.33E+04	4.08E+05	1	1.50E+05	1	3.11E+07
RBSL - gw to indoor air (mg/l)		0.214			1587.54	12.28	1874.31	9.67	435497.12
Note RBSL = >RES if calculated RBSL > calculated				olubility					
Calculated using Tier 1 methodology. Adjusted	for CA ben:	zene cance	r slope factor						7
Target HI = 1, target cancer risk = 1E-5						_			
Groundwater pathway calculated parameters	;							1	
Vol factor gw->ambient air	VFwamb	2.71E-05	2.69E-05	2.78E-05	2.51E-05	1.02E-05	1.36E-06	7.29E-05	4.93E-09
Effective Diffusion Coefficient gw(cm^2/s) calc	D ^{eff} ws	1.11E-03	9.31E-04	7.82E-04	7.77E-04	1.88E-03	2.51E-03		1.52E-01
Effective Diffusion Coefficient cap(cm^2/s) calc	D ^{eff} cap	2.17E-05	1.80E-05	1.50E-05	1.50E-05	4.66E-05	3.19E-04	4.34E-06	4.84E+00
Effective Diffusion Coefficient crack(cm^2/s) ca	D ^{eff} crack	7.26E-03	6.63E-03	5.93E-03	5.62E-03	5.62E-03	2.84E-03	2.36E-03	1.50E-01
Vol factor gw->enclosed space air	VFwesp	6.68E-03	6.87E-03	7.29E-03	6.44E-03	1.66E-03	1.09E-04		3.52E-07

Weiss Associates 11/1/96

Pepsi Emeryville RBCA Construction Scenario

					Constructi	on RBSLs			
Chemical specific parameters		Benzene	Toluene	EB	Xylenes	Naphth.	Fluorene	Fluoranth.	Pyrene
Carcinogenic/noncarcinogenic		С	nc	пс	пс	пс	nc	nc	nc
Henry's Constant	н	0.22	0.26	0.32	0.29	0.049	4.87E-03	2.79	2.91E-07
Air Diffusion Coefficient (cm^2/s)	Dau	9.30E-02	0.085	0.076	0.072	0.072	3.63E-02	3.02E-02	2.72E-02
Water Diffusion Coefficient (cm^2/s)	Dwat	1.10E-05	9.40E-06	8.50E-06	8.50E-06	9.40E-06	7.88E-06	6.35E-06	7.24E-06
Effective Diffusion Coefficient soil (cm^2/s) calc	D ^{eff} s	7.26E-03	6.63E-03	5.93E-03	5.62E-03	5.62E-03	2.84E-03	2.36E-03	1.50E-01
Carbon - Water Sorption Coefficient (L/kg)	k _{oc}	38	134.90	95.5	239.9	1288.2	7244.35	38018.94	38018.9
Log carbon-water sorption (calculated) (L/kg)	Log Koc	1.58	2.13	1.98	2.38	3.11	3.86		
Soil-water sorbtion coeff (calculated)	k _s	0.38	1.35	0.96	2.40	12.88	72.44		
Solubility (mg/l)	S	1750	535	152	198	31	1.69	0,206	0.132
Reference dose oral	RfDo		0.2		2	0.004	0.04		0.03
Reference dose - inhal	RfDi		0.11	0.29	2	0.004	0.04	0.04	
Cancer slope factor-inhal (kg-day/mg)	SFi	0.1							
Cancer slope factor- oral (kg-day/mg)	SFo	0.1							
Calculated parameters									
Volatilization factors, subsoil -> outdoor (mg/m3	VFsamb	1.10E-03	3.94E-04	1.27E-03	1.10E-03	2.00E-04	1.02E-05	2.50E-03	3.23E-08
Vol factor surficial soil-ambient air (1)	VFss-1	6.69E-08	1.		2.97E-08		5.09E-10		
Vol factor surficial soil - ambient air (2)	VFss-2	7.19E-06				7.19E-06	7.19E-06		
Max vol factor (correction to ASTM)	VFss	7.19E-06			7.19E-06	7.19E-06	7.19E-06		
Surficial soil part - ambient air	VFp	2.3E-12			2.3E-12	2.30E-12	2.30E-12	4	
Soil conc for sat vapor and pore-water (mg/kg)	Csat	847.74	780.73	1	497.76	401.76	122.55		
Construction RBSLs				}		-			
RBSL - outdoor ambient air (ug/m³ - air)		17.89	7026	18524	127750	256	2555	2555	1916
RBSL - subsurface soil to outdoor air (mg/kg	1)	16.28	17836	14632	116457	1276	250029	1023	59364108
RBSL - surficial soil (mg/kg)		3.5E+02	2.3E+05	1.4E+05	2.5E+06	1.7E+04	1.7E+05	1.7E+05	1.3E+05
RBSL - gw to outdoor air (mg/l)	· · ·	660.24	2.61E+05	6.66E+05	5.10E+06	2.50E+04	1.88E+06	3.51E+04	
RBSL - gw to indoor air (mg/l)		2.678			1.98E+04	1.54E+02	2.34E+04	1.21E+02	
Calculated using Tier 1 methodology, assuming	2 year con	struction duration	on. Adjusted fo	or CA benzene	cancer slope fa	ctor	2511		
Target HI = 1, target cancer risk = 1E-5				-		-			
Groundwater pathway calculated parameters	<u> </u>	.,,							
Vol factor gw->ambient air	VFwamb	2.71E-05	2.69E-05	2.78E-05	2.51E-05	1.02E-05	1.36E-06	7.29E-05	4.93E-09
Effective Diffusion Coefficient gw(cm^2/s) calc	D ^{eff} ws	1.11E-03	9.31E-04	7.82E-04	7.77E-04	1.88E-03	2.51E-03	2.35E-04	1.52E-01
Effective Diffusion Coefficient cap(cm^2/s) calc	D ^{eff} cap	2.17324E-05	1.80072E-05	1.49801E-05	1.49977E-05	4.6596E-05	0.000319273		4.837106311
Effective Diffusion Coefficient crack(cm^2/s) ca	D ^{eff} crack	7.26E-03	6.63E-03	5.93E-03	5.62E-03	5.62E-03	2.84E-03	2.36E-03	1.50E-01
Vol factor gw->enclosed space air	VFwesp	6.68E-03	6.87E-03	7.29E-03	6.44E-03	1.66E-03	1.09E-04	2.11E-02	
			1						

Weiss Associates 11/1/96

heet No of	84	_		WEISS ASSOCI	. 3 ===
roject No	1/2/96	JECT: <u>/6</u>		RBSL.	•
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Project No. 14 ps 10		JECT:	Poss	trion	WKG-1	LSGA.		
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NAOHTHOLENE	0.409			· 3/ ` ≥ '	7 3	1	3	25
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24		<u> </u>			\$		·	12
PYRONE	3.07		A 2	32 2	20 3.	76		2
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28 /			800	SOT PG			507 1	
PESIDENTIAL	RBSL-GW 1	NG 1	1	LGWO	WTDOOR	RBSL	GW-1	NDOGR
NAPHTHALENE	0.146	, ,	· :>	\$1 = : 7	» \$ · · ·/·	4.	74	
FLUORENE	1,46		> 3	310 = 3	5 V	47	,4.	
PYRENE	1.10		> 2	232 = >	> \$	35	6	
FLUORANTHENE	1.46		<u> </u>	310 =	>:5	47	.4	

APPENDIX E

TIER 2 SSTL CALCULATIONS

WA implementation of Jury model, from Sanders and Stem 1994

Appendix E - CALCULATIONS - Commercial Receptor - Soil to Indoor Air SSTL

Diffusivity Parameters (symbol notation from ASTM for consistency)

Source		Chemical	Specific Parameters
		benzene	Chemical Name
ASTM 95	Н		Henry's Constant
Calculated	Thaif	91	Contaminant Half Life (d)
Calculated	•	2.772589	First order rate constant (years ⁻¹)
ASTM 95	D ^{air}	9.30E-06	Air Diffusion Coefficient (m^2/s)
ASTM 95	D ^{wat}	1.10E-09	Water Diffusion Coefficient (m^2/s)
ASTM 95	foc	0.01	Organic Carbon Fraction
ASTM 95	K _{oc}	0.038	Organic Carbon Partition Coefficient (m^3/Kg)
			(Log Koc = 1.58)
		Soil Sp	ecific Parameters
ASTM 95	$\rho_{\boldsymbol{s}}$	1700	Bulk Density(kg/m^3)
ASTM 95	θ_{as}	0.26	Air Content (v/v)
ASTM 95	θ_{M2}	0.12	Water Content (v/v)
ASTM 95	$\boldsymbol{\theta_t}$	0.38	Porosity (v/v)
calc, Jury	D ^{eff} soil	6.140793	Effective Diffusion Coefficient - Soil (m^2/year)
		Building	Floor Parameters
Lindeburg	Ps,concrete	2,378	Bulk Density (kg/m³) 150 lb/ft³ concrete with 1% air by volume
ASTM 95	R		Areal Fraction of Cracks in Floor
ASTM 95	1_concrete	0.15	Concrete Slab Thickness (m)
Calculated	$\theta_{as,concrete}$	0.01	Concrete Air Content (v/v)
Calculated	$\theta_{\text{ws,concrete}}$	0	Concrete Water Content (v/v)
Calculated	$\theta_{t,concrete}$	0.01	Concrete Porosity (v/v)
calc, Jury	D ^{eff} concrete	0.154821	Effective Diffusion Coefficient - Concrete (m^2/year)

Integration Parameters Integration Constants ICs 969.5384 ICs=(Co*A*I)/Qb (mg/m) Integration Time Limits to 0.01 Lower time Limit (years) to 25 Upper time Limit (years) Intervals 2000 Number of intervals of Integration

0.01 Finite time differential (years)

Integration Error Estimate Integration Error (%) = 0.1731 OK - Integration Error is < 1% Chemical Dose Calculation

Results

Calculated Dose (mg) = 107.6649 = 6.0E-06 risk Acceptable Dose (mg) 179 = 1.0E-05 risk

dt

Calculated SSTL

SSTL (mg/kg). 2.82 Soil Vapor Intrusion to Indoor Air.

Formulas Presented on Following Page

Site Specific Parameters (symbol notation consistent with Sanders and Stem)

C_{soil}	1.70 Representative Soil Concentration (mg/kg)	Boring B-40, 10 ft depth, 10/10/94
Co	2.89 Soil Concentration by Volume (g/m^3)	using 1.7 density
L	0.30 Depth to Contamination (m)	first detected benzene at 1 ft
Α	3679 Zone of Influence, Building Area (m^2)	assumes 120 x 330 ft building over plume
Qb		ht= 300 cm(ASTM 95), vent rate = .00023/sec (ASTM 95)
1		20 m^3/day(ASTM 95)
	Co L A	Co 2.89 Soil Concentration by Volume (g/m^3) L 0.30 Depth to Contamination (m) A 3679 Zone of Influence, Building Area (m^2) Qb 9139 Building Ventilation Rate (m^3/Hr)

WA implementation of Jury model, from Sanders and Stern 1994

Appendix E - CALCULATIONS - Commercial Receptor - Soil to Indoor Air SSTL

Formulas

Diffusivity

$$D^{\text{eff}} = \frac{\left(\theta_{\text{cc}}^{10/3} D^{\text{vir}} H + \theta_{\text{vc}}^{10/3} D_{\text{vcr}}\right) / \theta_{t}^{2}}{\left(\rho_{\text{s}} f_{\text{cc}} K_{\text{cc}} + \theta_{\text{vc}} + \theta_{\text{cc}} H\right)}$$

Dase

$$Dose = \frac{C_0 AI}{Q_b} \int_0^1 e^{\left(-\mu t - \frac{2}{4D^{eff}t}\right)} \left(\frac{D^{eff}}{\pi t}\right)^{1/2} dt$$

For transport media with more than one Diffusivity ie. Soil Diffusivity and Building Foundation Diffusivity

$$Dose = \frac{C_0^{AI}}{Q_b} \int_0^1 \frac{1}{\frac{1}{X_1} + \frac{1}{X_2}} dt$$

Where

$$X_{\mathrm{l}} = e^{\left(-\mu t - \frac{1}{4D^{\mathrm{eff}}} \frac{2}{\mathrm{soil}}\right)} \left(\frac{D^{\mathrm{eff}} \, \mathrm{soil}}{\pi t}\right)^{1/2}$$

$$\dot{X}_2 = e^{\left(-\mu - \frac{corone}{4D^{eff} concrete}\right)} \left(\frac{D^{eff} concrete}{\pi t}\right)^{1/2}$$

WA implementation of Jury model, from Sanders and Stern 1994

Appendix E - CALCULATIONS - Commercial Receptor - Soil to Outdoor Air SSTL

Diffusivity Parameters (symbol notation from ASTM for consistency)

Source		Chemical Speci	fic Parameters
		benzene Chem	ical Name
ASTM 95	Н	0.222 Henry	's Constant
Calculated	Thalf	91 Conta	minant Half Life (d)
Calculated	μ	2.772589 First (order rate constant (years ⁻¹)
ASTM 95	D^{air}	9.30E-06 Air Di	ffusion Coefficient (m^2/s)
ASTM 95	D ^{wat}	1.10E-09 Water	Diffusion Coefficient (m^2/s)
ASTM 95	foc		nic Carbon Fraction
ASTM 95	K _{oc}	0.038 Organ	nic Carbon Partition Coefficient (m^3/Kg)
		(Log I	(oc = 1.58)
		Soil Specific	Parameters
ASTM 95	ρ_{s}	1700 Bulk (Density(kg/m^3)
ASTM 95	θ_{ss}	0.26 Air Co	ontent (v/v)
ASTM 95	θ _{ws}	0.12 Water	Content (v/v)
ASTM 95	θ_t	0.38 Poros	ity (v/v)
calc, Jury	D ^{eff} soit	6.140793 Effect	ive Diffusion Coefficient - Soil (m^2/year)

Dose Integration Parameters

lCs	Integration Constants 2.23 ICs=(Co*A*I)/Qb (mg/m) Integration Time Limits
t _o	0.01 Lower time Limit (years)
t _r	25 Upper time Limit (years)
intervals dt	2000 Number of intervals of Integration 0.01 Finite time differential (years)

Results

Integration Error Estimate

Integration Error (%) = 1.39E-01 OK - Integration Error is < 1%

Chemical Dose Calculation

Calculated Dose (mg) = 2.55 = 1.4E-07 risk Acceptable Dose (mg) 179 = 1.0E-05 risk

Calculated SSTL

SSTL (mg/kg) 119 Soll Vapor to Outdoor Air.

Site Specific Parameters (symbol notation consistent with Sanders and Stern)

Site Spec	C _{soil}	1.70 Representative Soil Concentration (mg/kg)
Calculated	Co	2.89 Soil Concentration by Volume (g/m^3)
Site Spec	L	0.30 Depth to Contamination (m)
ASTM 95	δ	2 Ambient Air Mixing height (m)
ASTM 95	Γ	15 Width of Source Area Parallel to Wind (m)
ASTM 95	Uair	2.25 Ambient Wind Speed (m/sec)
ASTM 95	11	20 Inhalation volume (m^3/day)

Boring B-40, 10 ft depth, 10/10/94 using 1.7 density

first detected benzene at 1 ft

$D^{\text{eff}} = \frac{\left(\theta_{cs}^{10/3} D^{\text{eff}} H + \theta_{ws}^{10/3} D_{wct}\right) / \theta_{t}^{2}}{\left(\rho_{s} f_{cc} K_{cc} + \theta_{ws} + \theta_{cs} H\right)}$

Formulas Diffusivity

Dose

$$Dose = \frac{e^{0} \Gamma I}{U_{air} \delta} \int_{0}^{t} e^{\left(-\mu - \frac{1}{4D^{eff}}\right)} \left(\frac{D^{eff}}{\pi t}\right)^{1/2} dt$$

WA implementation of Jury model, from Sanders and Stern 1994

Appendix E - CALCULATIONS - Commercial Receptor - Ground Water to Indoor Air SSTL

Diffusivity Parameters (symbol notation from ASTM for consistency)

Source		Chemical	Specific Parameters
			Chemical Name
ASTM 95	Н		Henry's Constant
Calculated		365	Contaminant Half Life (d)
Calculated	μ	0.693147	First order rate constant (years ⁻¹)
ASTM 95	D ^{air}	9.30E-06	Air Diffusion Coefficient (m^2/s)
ASTM 95	D ^{wat}	1.10E-09	Water Diffusion Coefficient (m^2/s)
ASTM 95	foc		Organic Carbon Fraction
ASTM 95	K _{oc}	0.038	Organic Carbon Partition Coefficient (m^3/Kg)
			(Log Koc = 1.58)
		Soil Spe	ecific Parameters
ASTM 95	$\rho_{\mathbf{z}}$	1700	Bulk Density(kg/m^3)
ASTM 95	θ_{as}	0.26	Air Content (v/v)
ASTM 95	θ_{ws}	0.12	Water Content (v/v)
ASTM 95	θ_{t}	0.38	Porosity (v/v)
caic, Jury	D ^{eff} soil	6.140793	Effective Diffusion Coefficient - Soil (m^2/year)
		Building	Floor Parameters
Lindeburg	Ps,concrete	2,378	Bulk Density (kg/m³) 150 lb/ft³ concrete with 1% air by volume
ASTM 95	n		Areal Fraction of Cracks in Floor
ASTM 95	L _{concrete}	0.15	Concrete Slab Thickness (m)
Calculated	$\theta_{as,concrete}$	0.01	Concrete Air Content (v/v)
Calculated		0 (Concrete Water Content (v/v)
Calculated	$\theta_{t,concrete}$		Concrete Porosity (v/v)
calc, Jury	D ^{eff} concrete	0.154821	Effective Diffusion Coefficient - Concrete (m^2/year)

Dose Integration Parameters

Integration Constants
ICs 570.3167 ICs=(Co*A*I)/Qb (mg/m)

Integration Time Limits

t_o 0.01 Lower time Limit (years)

t_f 25 Upper time Limit (years)
Intervals 300 Number of intervals of Integration

dt 0.08 Finite time differential (years)

Results

Integration Error Estimate

Integration Error (%) = 2.81E-01 OK - Integration Error is < 1%

Chemical Dose Calculation

Calculated Dose (mg) = 145.2091 = 8.1E-06 risk Acceptable Dose (mg) 179 = 1.0E-05 risk

Calculated SSTL

SSTL (mg/L) 2.09 Ground Water Volatilization to Indoor Air

Formulas Presented on Following Page

Site Specific Parameters (symbol notation consistent with Sanders and Stem)

Site Spec	Co	1.7 Representative Ground Water Concentration (mg/L) = (g/m³)
Site Spec	Ĺ	2.31 Depth to Contamination (m)
Site Spec	Α	3679 Zone of Influence, Building Area (m^2)
ASTM 95	Qb	9139 Building Ventilation Rate (m^3/Hr)
ASTM 95	1	20 Inhalation volume (m^3/day)

MW-13, 12/20/1995, max in past year shallowest MW-5 water depth recorded assumes 120 x 330 ft building over plume ht= 300 cm(ASTM 96), vent rate = .00023/sec (ASTM96) 20 m^3/day(ASTM 96)

WA implementation of Jury model, from Sanders and Stem 1994

Appendix E - CALCULATIONS - Commercial Receptor - Ground Water to Indoor Air SSTL

Formulas

Diffusivity

$$D^{\text{eff}} = \frac{\left(\theta_{cs}^{10/3} D^{cir} H + \theta_{ws}^{10/3} D_{wct}\right) / \theta_{t}}{\left(\rho_{s} f_{cc} K_{cc} + \theta_{ws} + \theta_{cs} H\right)}$$

Dose

$$Dose = \frac{C_0 AI}{Q_b} \int_{0}^{1} e^{\left(-\mu u - \frac{2}{4D^{\text{eff}}}\right)} \left(\frac{D^{\text{eff}}}{\pi t}\right)^{1/2} dt$$

For transport media with more than one Diffusivity ie. Soil Diffusivity and Building Foundation Diffusivity

$$Dose = \frac{C_0^{a}AI}{Q_b} \int_0^T \frac{1}{\frac{1}{X_1} + \frac{1}{X_2}} dt$$

Where

$$X_1 = e^{\left(-\mu t - \frac{t}{4D^{\text{off}}} \frac{2}{\text{soit}}\right)} \left(\frac{D^{\text{off}} \cdot \text{soit}}{\pi t}\right)^{1/2}$$

$$X_2 = e^{\left(-\mu t - \frac{t^{\text{concret}}^2}{4D^{\text{off}}_{\text{concret}}t}\right)} \left(\frac{D^{\text{off}}_{\text{concrete}}}{\pi t}\right)^{1/2}$$

		RBC	A SITE ASS	ESSMENT						Tier 2 Wo	rksheet 9.3	
Site Name: P Site Location	- ·		•	Completed By: Tim Utterback Date Completed: 10/30/1996								
(GROUNDWATER S	Target	k (Class A & B) Risk (Class C) lazard Quotient	1.0E-5	■ MCL exp			Calculation Option: 2				
		•		SST	L Results For Con	plete Exposur	e Pathways ("x" If C	omplete)				
CONSTITUE	Representative Concentration CONSTITUENTS OF CONCERN			Groundwater	Ingestion		vater Volatilization Indoor Air		er Volatilization utdoor Air	Applicable SSTL	SSTL Exceeded ?	Required CRF
CAS No.	Name	(mg/L)	Residential: 2640 feet	Commercial: 2640 feet	Regulatory(MCL): 2640 feet	Residential: (on-site)	Commercial: (on-site)	Residential (on-site)	Commercial: (on-site)	(mg/L	"■" if yes	Only if "yes" left
71-43-2	Benzene	1.7E+0	>Sol	NA	>Sol	. NA	NA	NA	NA	>Sol		<1

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Software: GSI RBCA Spreadsheet Version: v 1.0

Serial: G-201-BPX-156

		RBCA SIT	E ASSESSI	VIENT						ler 2 Worksh	eet 9.2	
Site Name: I	Pepsi		Completed B	y: Tim Utterbad	ck					······································		
Site Location	ı: Emeryville	<u> </u>	Date Comple	ted: 10/30/199	6							1 OF 1
			Target Risk (Class A & B) 1.0E-5			MCL exposure limit?			Calculation Option: 2			
SI	SUBSURFACE SOIL SSTL VALUES			Target Risk (Class C) 1.0E-5			☐ PEL exposure limit?					*
	(> 3 FT BGS)			Target Hazard Quotient 1.0E+0								
				SSTL	Results For Comp	ete Exposure Pa	athways ("x" If C	omplete)				
CONSTITUE	Representative Concentration CONSTITUENTS OF CONCERN			il Leaching to (Groundwater	1 1	latilization to		olatilization to	Applicable SSTL	SSTL Exceeded ?	Required CRF
CAS No.	Name	(mg/kg)	Residential: 2640 feet	Commercial: 2640 feet	Regulatory(MCL): 2640 feet	Residential: (on-site)	Commercial: (on-site)	Residential: (on-site)	Commercial: (on-site)	(mg/kg)	"■" If yes	Only if "yes" left
71-43-2	Benzene	1.7E+0	>Res	NA	>Res	NA NA	NA	NA	NA	>Res		<1

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Software: GSI RBCA Spreadsheet Version: v 1.0

Serial: G-201-BPX-156

RBCA TIER 1/TIER 2 EVALUATION

Output Table 1

	Site Name: Site Location:	•		ob Identification: Date Completed: Completed By:	10/30/96		Version:				
]	DEFA	ULT PARA	METERS				NOTE: values	s which differ from Tier 1 default values are shown i	n bold italies and	l underlined.	
Exposure			Residential		Commerci	el/Industrial	Surface			Commerci	el/industrial
Parameter	Definition (Units)	Adult	(1-6yrs)	(1-16 yrs)	Chronic	Constrctn	Parameters 2 4 1	Definition (Units)	Residential	Chronic	Construction
ATC	Averaging time for carcinogens (yr)	70					1	Exposure duration (yr)	30	25	1
ATn	Averaging time for non-carcinogens (yr)	30	6	16	25	1	Α	Contaminated soil area (cm^2)	2.2E+06		1.0E+06
BW	Body Weight (kg)	70	15	35	70		W	Length of affected soil parallel to wind (cm)	1.5E+03		1.0E+03
ÉD	Exposure Duration (yr)	30	6	16	25	1	W gw	Length of affected soil parallel to groundwater (c	1.5E+03		
EF	Exposure Frequency (days/yr)	350			250	180	Uair	Ambient air velocity in mixing zone (cm/s)	2.3E+02		
EF Denn	Exposure Frequency for dermal exposure	350			250		deita	Air mixing zone height (cm)	2.0E+02		
iRgw	Ingestion Rate of Water (I/day)	2			1		Lss	Definition of surficial soils (cm)	1.0E+02		
IRs	Ingestion Rate of Soil (mg/day)	100	200		50	100	Pe	Particulate areal emission rate (g/cm^2/s)	2.2E-10		
(Radi	Adjusted soiling, rate (mg-yr/kg-d)	1.1E+02			9.4E+01						
lRain lRaout	Inhalation rate Indoor (m^3/day)	15			20			r Definition (Units)	Value	_	
SA	Inhalation rate outdoor (m^3/day)	20		0.05.00	20	10	delta.gw	Groundwater mixing zone depth (cm)	2.0E+02		
SAadi	Skin surface area (dermal) (cm^2)	5.8E+03		2.0E+03	5.8E+03	5.8E+03	<u> </u>	Groundwater infiltration rate (cm/yr)	3.0E+01		
Overal .	Adjusted dermal area (cm^2-yr/kg) Soil to Skin adherence factor	2.1E+03			1.7E+03		Ugw	Groundwater Darcy velocity (cm/yr)	2.5E+03		
AAF3	Age adjustment on soil ingestion	1			F-11-0-		Ugw.tr	Groundwater Transport velocity (cm/yr)	6.6E+03		
AAFd	Age adjustment on skin surface area	FALSE			FALSE		Ks	Saturated Hydraulic Conductivity(cm/s)			
tox	Use EPA tox data for air (or PEL based)	FALSE TRUE			FALSE		grad	Groundwater Gradient (cm/cm)			
gwMCL?	Use MCL as exposure limit in groundwater?	TRUE					'Sw	Width of groundwater source zone (cm)	,		
Aumor:	Ose sion as exposure will al Brong Mares a	INUE					Sd BC	Depth of groundwater source zone (cm)			
}								Biodegradation Capacity (mg/L)	Thur		
							BIO?	Is Bioattenuation Considered	TRUE		
ì							phi.eff	Effective Porosity in Water-Bearing Unit	4.05.00		
Matrix of Expe	osed Persons to	Residential			Commerci	al/Industrial	foc.sat	Fraction organic carbon in water-bearing unit	1 0E-03		
	osure Pathways	- ttosigentual			Chronic	Constrctn	Soil	Definition (Units)	Value		
Groundwater					0.000.0		hc hc	Capillary zone thickness (cm)	5.0E+00	-	
GW,i	Groundwater Ingestion	TRUE			FALSE		hv	Vadose zone thickness (cm)	3.0E+02		
GW v	Volatifization to Outdoor Air	FALSE			FALSE		rho	Soil density (g/cm^3)	1.7		
GW b	Vapor Intrusion to Buildings	FALSE			FALSE		foc	Fraction of organic carbon in vadose zone	0.01		
Soil Pathways	•						phi	Soil porosity in vadose zone	0.38		
Sv	Volatiles from Subsurface Soils	FALSE			FALSE		Lgw	Depth to groundwater (cm)	3.0E+02		
SS v	Volatiles and Particulate Inhalation	FALSE			FALSE	FALSE	Ls	Depth to top of affected soil (cm)	1.0E+02		
SS.d	Direct Ingestion and Dermal Contact	FALSE			FALSE	TRUE	Lsubs	Thickness of affected subsurface soils (cm)	2.0E+02		
sı	Leaching to Groundwater from all Soils	TRUE			FALSE		Ha	Soil/groundwater pH	6.5		
Sb	Intrusion to Buildings - Subsurface Soils	FALSE			FALSE		•	•	capillary	vadose	foundation
							phi.w	Volumetric water content	0.342	0.12	0.12
							phia	Volumetric air content	0.038	. 0 26	0.26
ľ			,				•				
							Building	Definition (Units)	Residential	Commercial	
							Lb	Building volume/area ratio (cm)	2.0E+02	3.0E+02	
Matrix of Rece			ientiai		Commerci	al/Industrial	ER	Building air exchange rate (s^-1)	1.4E-04	2 3E-04	
and Location	on- or off-site	Distance	On-Site		Distance	On-Site	Lork	Foundation crack thickness (cm)	1.5E+01		
l							eta	Foundation crack fraction	0.01		
GW	Groundwater receptor (cm)	8 0E+04	FALSE		8,0E+04	FALSE					
is	Inhalation receptor (cm)		FALSE			FALSE					
							Dispersive Tr				
Matrix of		F. 40.73	0 11					Definition (Units)	Residential	Commercial	
Target Risks		Individual	Cumulative	_			Groundwater				
TRab	Toront Durk (alone ASD	405.55					ax	Longitudinal dispersion coefficient (cm)			
TRo	Target Risk (class A&B carcinogens)	1.0E-05					ay	Transverse dispersion coefficient (cm)			
THQ	Target Risk (class C carcinogens)	1.0E-05					az	Vertical dispersion coefficient (cm)			
	Target Hazard Quotient	1.0E+00					Vapor				
Opt Tier	Calculation Option (1, 2, or 3)	2					ocy	Transverse dispersion coefficient (cm)			
tæf	RBCA Tier	22					dcz	Vertical dispersion coefficient (cm)			

			R	BC	A CHEMI	CAL DA	AT.	ABASE			•			Physical	Prop	6	Da	
						<u></u>				<u> </u>		Vapor		·	-			_
CAS			Molecu Weigi	ht		ision icients in wate (cm2/s		log (Kod log(Kd (@ 20 - 2 (l/kg)	d) (5 C)	•	aw Constant 0 - 25 C) (unitless)	Pressur (@ 20 - 25 (mm Hg Pure	C)	Solubilit (@ 20 - 25 (mg/l) Pu	C)	acid	bas	se
Number	Constituent	type	MW	ref	Dair re	Dwat	г е	Koc	ref	mol	re	Component	t ref	Component	t ref	pKa	рK	b
71-43-2	Benzene	Α	78.1	5	9.30E-02 A	1.10E-05	A	1.58	Α	5.29E-03	2.20E-01 A	9.52E+01	4	1.75E+03	Α	•	•	
	Site Name: Pepsi		Site Lo	catio	on: Emeryvi	lle		Complete	ed By	r: Tim Utter		Date Compl	eted	: 10/30/1996				

Software version: v 1.0

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			RBCA CHEMICAL DATABASE								y Data	
			eferen Dose			F	Slope actors	•		EPA Weight	ſs	
CAS		Oral	· 3· · · · 3 · ·	Inhalation				Inhalation		of	Constituen	
Number	Constituent	RfD_oral	ref	RfD inhal	re	SF_oral	ref	SF inhal	ref	Evidence	Carcinogenio	
71-43-2	Benzene	-	R	1.70E-03	R	2.90E-02	A	2.90E-02	Α	Α	TRUE	
	Site Name: Pepsi	Site Location:	Emer	vville		completed By	: Tim !	Utterback		Date Completed	I: 10/30/1996	

Software version: v 1.0

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DDCA	\sim A I	DATABA	S 12
$\mathbf{x} = \mathbf{x} \cdot \mathbf{x}$		# * * * * * * * * * * * * * * * * * * *	_

Miscellaneous Chemical Data

CAS	. Maximum Contaminant Level		Maximum Exposure Ab Contaminant Level Limit PEL/TLV		Abs	elative orption octors	Detection I Groundwater (mg/L)		Limits Soil (mg/k		Half Life (First-Order Decay) (days)		
Number Constituent	MCL (mg/L)	reference	(mg/m3)	ref	Oral	Dermal		ref		re	Saturated	Unsaturated	ref
71-43-2 Benzene	1.00E-03	CAL DOHS	3.20E+00	OSHA	1	0.5	0.002	С	0.005	S	720	720	H
Site Name: Pepsi	Site Location: E	meryville				Comple	ted By: Ti	m Uti	erback	ς <u>Γ</u>	Date Comp	leted: 10/30/	—— 1996

Software version: v 1.0

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REPRESENTATIVE COC CONCENTRATIONS IN SOURCE MEDIA

(Complete the following table)

	Representative COC Concentration										
CONSTITUENT	in Groundw	in Surface	Soil	in Subsurface Soil							
	value (mg/L)	note	value (mg/kg	note	alue (mg/kg	note					
Benzene	1.7E+0				1.7E+0						
Site Name: Pepsi				Comple	eted By: Tim Utte	erback					
Site Location: Emeryville				Date Co	ompleted: 10/30	/1996					

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GROUNDWATER DAF VALUES

(Enter DAF values in the following table)

Dilution Attenuation Factor

	(DAF) in Groundwater							
CONSTITUENT	Residential	Comm./Ind.						
	Receptor	Receptor						
Benzene	3.3E+29	#VALUE!						

Site Name: Pepsi Completed By: Tim Utterback Site Location: Emeryville Date Completed: 10/30/1996

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Empirical DAF

Anal	vtical	Data	(Un	to	10	Data	Points)
/ 11 / MII.	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	~~~	100		,,,	Mulu	1 0111101

	1	2	3	4	5	6	7	8
	(mg/L)	(mg/L)_	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L) ·
Well Name	MW-5	MW-13	MW-8	,				
Distance from Source	40'	140'	260'					
Date Sampled	10/1/94	10/1/94	10/1/94	***		· · · · · · · · · · · · · · · · · · ·		
	0.23	0.88	0.0005					