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11:51 am, Aug 19, 2011 Alameda County Environmental Health

August 18, 2011

Mr. Jerry Wickham Alameda County Environmental Health 1131 Harbor Bay Parkway, Suite 250 Alameda, California 94502-6577

Re: Former Signal Oil Marine Storage and Distribution Facility (Former Chevron Bulk Plant 20-6127) 2301-2311 Blanding Avenue Alameda, California LOP Case RO0002466

Dear Mr. Wickham:

The purpose of this letter is to verify that as a representative for Chevron Environmental Management Company (Chevron), I reviewed, and concur with, the comments in the *Draft Corrective Action Plan* for the referenced facility, prepared on behalf of Chevron by Conestoga-Rovers & Associates. I declare under penalty of perjury that the foregoing is true and correct.

Please feel free to contact me at (714) 671-3207 if you have any questions.

Sincerely,

MS Bauer

Mike Bauer Project Manager

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DRAFT CORRECTIVE ACTION PLAN

FORMER SIGNAL OIL MARINE STORAGE AND DISTRIBUTION FACILITY CHEVRON FACILITY 20-6127 2301-2311 BLANDING AVENUE ALAMEDA, CALIFORNIA AGENCY CASE NO. RO0002466

Prepared for: Mr. Jerry Wickham Alameda County Health Care Services Agency Environmental Health Services

> Prepared by: Conestoga-Rovers & Associates

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Brian Silva

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1.0 INTRODUCTION

Conestoga-Rovers & Associates (CRA), on behalf of Chevron Environmental Management Company (Chevron), has prepared this *Draft Corrective Action Plan* (draft CAP) for the former Signal Oil Marine Storage and Distribution facility (former Chevron facility 20-6127) located at 2301-2311 Blanding Avenue in Alameda, California. This draft CAP was requested by the Alameda County Health Care Services Agency, Environmental Health Services (ACEH) in a letter to Chevron dated May 26, 2011 (Appendix A) to evaluate potential remedial alternatives for mitigating petroleum impacts at the site.

This document complies with California Code of Regulations, Title 23, Division 3, Chapter 16, Underground Storage Tank (UST) Regulations. A site background, previous site investigations, groundwater monitoring activities, hydrocarbon distribution, remediation goals, evaluation of remedial alternatives, and final remediation recommendations are presented below.

2.0 <u>SITE BACKGROUND</u>

The following sections provide a description of the site and a summary of the geologic and hydrogeologic setting at the site.

2.1 <u>SITE DESCRIPTION</u>

The approximately 3.5-acre site is located on the northeast side of Blanding Avenue between Oak and Park Streets in Alameda, California (Figures 1 and 2). Land use in the site vicinity is primarily commercial and industrial. The Alameda Canal and a marina are located adjacent to the northeast side of the site. The site is currently occupied by three large commercial buildings, which are used for office, retail, and storage space, and identified as Park Street Landing at 2307-2337 Blanding Avenue. A summary of the site history dating back to 1897 is included in Appendix B.

2.2 SITE GEOLOGY AND HYDROGEOLOGY

Based on past investigation, the soils encountered beneath the site generally consist of silty sand and clayey sand from just beneath grade to approximately 5 to 9 feet below grade (fbg). Fill consisting of black sand and debris, including concrete fragments, has

been reported in several borings at shallow depths. A 4 to 5 foot-thick layer of clay with some sand underlies the silty sand and clayey sand. Below the clay is silty sand and sandy silt to the maximum depth explored of approximately 20.5 fbg. Groundwater is typically encountered in site borings at approximately 14.5 to 15 fbg within the silty sand and sandy silt, and subsequently rises in the borings/wells to approximately 7 to 10 fbg suggesting the groundwater beneath the site is semi-confined. Geologic cross-sections are provided in Figures 3 and 4. Boring logs are presented in Appendix C.

2.3 <u>PREVIOUS ENVIRONMENTAL WORK</u>

To date, seven groundwater monitoring wells, one replacement groundwater monitoring well, six vapor wells, and seven sub-slab vapor probes have been installed at the site. Additionally, twenty-eight soil borings have been advanced and three surface soil samples have been collected at the site. Quarterly monitoring and sampling of wells MW-1 through MW-5 was initiated in 2001 is ongoing. Recently installed wells MW-1RA, MW-1RB (which was installed to replace well MW-1), and MW-6 were added to the quarterly monitoring and sampling program, beginning in the fourth quarter 2010. Well construction specifications are summarized in Table 1. A summary of previous environmental work performed at the site is presented in Appendix B.

2.4 PRODUCT RELEASES AND SOURCE AREA

No records of historical releases have been located for the site. Based on soil and groundwater data, the source area appears to be from the former AST and loading rack area. All facilities were removed between 1957 and 1965. Cumulative historical soil data is presented in Tables 2 and 3. Grab-groundwater analytical data is presented in Table 4 and historical monitoring and sampling data is included as Appendix D.

2.5 <u>SENSITIVE RECEPTOR SURVEY</u>

The following sections provide a summary of wells, surface water bodies and other sensitive receptors located near the site. The sensitive receptor and well survey map is shown graphically on Figure 5, and sensitive receptor and well survey data is summarized in Table 5.

2.5.1 <u>AREA WELL SURVEY</u>

In June 2011, CRA reviewed Department of Water Resources (DWR) well completion reports to identify wells within a 2,000-foot radius of the site, using aerial photography to measure approximate distances from the site to each well. Review of DWR files identified two industrial wells within the 2,000-foot radius. The two wells are located on the same property at 2307 Clement Avenue, approximately 310 to 340 feet southwest of the site (Figure 5). No domestic, irrigation, or municipal water supply wells were identified.

The wells identified in the survey are not considered at risk from petroleum hydrocarbons originating from the site, as these wells are located upgradient of the site and petroleum hydrocarbon concentrations detected in well MW-2 onsite, nearest to these wells, have been below environmental screening levels (ESLs) since sampling began. Given the relative lack of petroleum hydrocarbon detections in MW-2 and the direction of groundwater flow, it is unlikely that the shallow dissolved petroleum hydrocarbon plume onsite is migrating to the identified well receptors; therefore they are not considered at risk.

2.5.2 SURFACE WATER SURVEY

The nearest surface water to the site is Alameda Canal which is located along the northern property boundary. Historical grab surface water samples collected from canal sample location CS-2 indicate only minor, sporadic hydrocarbon detections (mainly total petroleum hydrocarbons as diesel [TPHd]) since July 2001. However, the origin of hydrocarbon detections in canal water cannot be accurately determined, as the source could possibly be from offsite, including the marina adjacent to the site.

2.5.3 <u>ADDITIONAL RECEPTORS</u>

CRA reviewed internet search engines to identify schools, daycares, and hospitals within a 2,000-foot radius of the site and used aerial photography to measure approximate distances from the site to each receptor. The search identified one school at 2226 Pacific Avenue, located approximately 1,775 feet southwest (crossgradient) of the site (Figure 5). No daycare or hospital facilities were identified within the search radius. Based on its relative direction to and distance from the site, the school identified is not considered at risk from hydrocarbons originating from the site.

2.5.4 ADJACENT LAND USE

Current land use adjacent to the site is primarily commercial and industrial. To the west and north (across Alameda Canal) are mainly industrial properties. The adjacent western property is occupied by four warehouses, a building, and two docks on Alameda Canal. The three properties to the north, across Alameda Canal are occupied by a boat electronics service shop, a boat motor shop, and a concrete/cement mixing facility. The properties immediately to the south and east are commercial properties. A commercial office building is located immediately to the east. A marina associated with the boat rigging shop located on the subject property is located immediately to the north on Alameda Canal.

3.0 <u>HYDROCARBON DISTRIBUTION</u>

The primary constituents of concern (COCs) are:

- TPHd soil and groundwater.
- Total petroleum hydrocarbons as gasoline (TPHg) soil, soil vapor, and groundwater.
- Benzene soil vapor and groundwater.
- Ethylbenzene soil vapor.

Toluene, xylenes, methyl tertiary butyl ether (MTBE), and other volatile organic compounds (VOCs) are not considered COCs due to the relative low concentrations detected.

3.1 <u>SOIL</u>

The highest hydrocarbon concentrations of 6,900 milligrams per kilogram (mg/kg) TPHd and 11,000 mg/kg TPHg were detected in vapor well VP-4 at 5 fbg. As shown on Figures 6 and 7, the horizontal extent of the soil impacts is defined in all directions within the vicinity of the former fueling facilities. Concentrations that exceed applicable ESLs¹ are primarily detected between 2 to 14 fbg. Concentrations decrease with depth and are vertically delineated outside the source area and to low levels at depth within the source area by confirmation samples collected from MW-1 (0.53 mg/kg benzene,

¹ Environmental Screening Level (ESL) from the San Francisco Regional Water Quality Control Board's (RWQCB's) *Screening for Environmental Concerns at Sites with Contaminated Soil and Groundwater,* Interim Final November 2007, Revised May 2008

0.021 mg/kg toluene, 0.028 mg/kg ethylbenzene, 0.065 mg/kg xylenes), MW-4 (non-detect for TPHd, TPHg, BTEX, and MTBE), MW-6 (1.2 mg/kg TPHg, 0.12 mg/kg benzene, 0.002 mg/kg toluene, 0.003 mg/kg ethylbenzene, and 0.003 mg/kg xylenes), and SB-9 (1.2 mg/kg TPHd and 0.22 mg/kg benzene) at 15 fbg (Figures 3, 4, 6, and 7). Cumulative soil analytical data are summarized in Tables 2 and 3.

3.2 <u>GROUNDWATER</u>

Groundwater has been monitored for approximately 10 years. The highest hydrocarbon detections in grab-groundwater samples collected were from boring SB-18 at concentrations of 19,000 microgram per liter (μ g/L) TPHd, 3,800 μ g/L TPHg, and 590 μ g/L benzene.

The highest hydrocarbon concentrations detected in site monitoring wells were in former well MW-1 and newly installed well MW-1RA (in the vicinity of SB-18) with maximum concentrations of $4,000 \,\mu\text{g/L}$ TPHd, $6,400 \,\mu\text{g/L}$ TPHg, and $920 \,\mu\text{g/L}$ benzene. The most recent data for each well (third quarter 2011) are summarized in Table A below. The third quarter 2011 monitoring and sampling event will be reported under separate cover. Hydrocarbons in groundwater are highest near well MW-1RA, which is screened within a shallow "pearched" zone adjacent to Alameda Canal to the north. The extent of hydrocarbons in groundwater is generally limited to onsite and defined laterally to the south by MW-2 and GWS-14, east by GWS-11, GWS-12, and MW-4, and west by GWS-7, GWS-13, and GWS-15 (Figures 8 through 10 and Table 4).

TABLE A CURRENT HYDROCARBON CONCENTRATIONS IN GROUNDWATER							
Well	Most Recent	TPHd	TPHg	Benzene	Toluene	Ethyl-be	Xylenes
	Sampling Date					nzene	
		Concentrations in µg/L					
ESL		100	100	1	40	30	20
MW-1RA	6/30/2011	3,700	6,800	780	13	36	13
MW-1RB	6/30/2011	1,900	310	9	< 0.5	<0.5	<0.5
MW-2	6/30/2011	120	<50	< 0.5	< 0.5	<0.5	<0.5
MW-3	6/30/2011	740	<50	< 0.5	< 0.5	<0.5	<0.5
MW-4	6/30/2011	<50	<50	< 0.5	< 0.5	<0.5	<0.5
MW-5	6/30/2011	3,200	2,900	99	6	1	7
MW-6	6/30/2011	640	200	3	<0.5	<0.5	<0.5
ESL Environmental Screening Level (ESL) from Table A. ESLs Shallow Soils, Groundwater is Current or Potential Source of Drinking Water from the San Francisco Bay Region RWQCB <i>Screening for</i> <i>Environmental Concern at Sites with Contaminated Soil and Groundwater</i> . Interim Final November 2007							

Revised May 2008

Data in **bold** represent concentrations that exceed applicable ESLs.

The dissolved hydrocarbon plume is generally stable based on trends observed in site wells. Limited sampling of newly installed wells MW-1RA, MW-1RB, and MW-6 indicate generally stable concentrations; however further sampling is needed to establish a trend. Concentration trend graphs for MW-1 (replaced by MW-1RB), MW-3, and MW-5 are presented in Appendix E. Historical and current groundwater data are presented in Appendix D and grab-groundwater sample data is summarized in Table 4.

3.3 LIGHT NONAQEOUS PHASE LIQUIDS (LNAPL)

LNAPL has never been detected in any site monitoring well or in any grab-groundwater samples collected from soil borings.

3.4 SOIL VAPOR, SUB-SLAB VAPOR, INDOOR AND OUDOOR AIR

Soil vapor sampling was initiated at the site in August 2008. The highest soil vapor concentrations detected were from vapor wells VP-4 and VP-5 in August and October 2008 at concentrations of 110,000 micrograms per cubic meter (μ g/m³) TPHd in VP-5, 220,000,000 μ g/m³ TPHg in VP-4, 1,100,000 μ g/m³ benzene in VP-4, and 650,000 μ g/m³

ethylbenzene. Subsequent soil vapor sampling indicates concentrations are relatively stable or decreasing.

Sub-slab vapor sampling was initiated in July 2009. The highest sub-slab vapor concentrations were mainly detected during the first two sampling events in August and October 2009, with subsequent sampling events indicating minor or non-detect concentrations. The highest sub-slab vapor concentrations detected were from sub-slab vapor probes VP-8, VP-9, and VP-10 in July 2009 and June 2010 at concentrations of 8,800 μ g/m³ TPHg in VP-9, 24 μ g/m³ benzene and 71 μ g/m³ toluene in VP-8, and 52 μ g/m³ ethylbenzene in VP-10. During the last two sub-slab sampling events, all COCs were below ESLs except for a slight exceedance of benzene in VP-8 during the June 2010 sampling event. However benzene was below the ESL in VP-8 during the most recent (November 2010) event.

Indoor and outdoor air sampling was initiated in June 2010. Indoor and outdoor air samples collected in site buildings are at relatively low concentrations with the highest concentrations detected in sampling location IA-3 at $530 \,\mu\text{g/m}^3$ TPHg, $4.20 \,\mu\text{g/m}^3$ benzene, and $6.00 \,\mu\text{g/m}^3$ ethylbenzene. The disparity between the sub-slab and indoor air results suggest that other sources within the buildings are contributing to the indoor air results. Each of the suites where the indoor air samples were collected had numerous sources of VOCs present/stored inside and the outdoor air sample also contained TPHg and benzene levels above the indoor air ESLs. Due to this disparity, further indoor air sampling is not recommended.

Current sub-slab results are all below ESLs for indoor air under commercial/industrial land use adjusted by a factor of 100 to account for attenuation between sub-slab and indoor air (Table E, SFRWQCB, 2008). This further supports that there are other indoor sources contributing to the indoor air results. While there are highly elevated concentrations observed in the vapor well samples collected at 5 fbg, sub-slab results show low level vapor impact in near surface soil suggesting vapor intrusion from deeper soil (5 fbg) into the site buildings is not a risk. The soil vapor, sub-slab vapor, and indoor and outdoor air analytical results are presented in Tables 6 and 7.

5.0 <u>CLEANUP GOALS</u>

The following sections summarize soil, soil vapor and groundwater cleanup goals.

5.1 SOIL AND SOIL VAPOR CLEANUP GOALS

As evidenced by the dissolved concentration degradation trend graphs for source area wells MW-1 (replaced by MW-1RB), MW-3, and MW-5 (Appendix E), the rate at which the soil mass is leaching to groundwater is less than or equal to the rate of natural degradation. Additionally as described above in Section 3.4, current soil impacts do not result in a vapor intrusion risk. Therefore, active soil remediation is not warranted. If the site is redeveloped, a soil management plan (Section 8.0) has been prepared to address potential risks from residual soil impacts.

5.2 <u>GROUNDWATER CLEANUP GOALS</u>

Since soil and soil vapor concentrations have been ruled out as drivers for cleanup, dissolved concentration reduction will be the measure of remedial success. The RWQCB's Water Quality Control Plan (Basin Plan) for the San Francisco Bay Basin Region states that existing and potential beneficial uses applicable to groundwater in the region include domestic and municipal water supply. Table B presents the COCs, ESLs to protect designated beneficial uses, highest historical concentrations, and current maximum concentrations (using third quarter 2011 monitoring and sampling data) for this site.

TABLE B				
ESLs AND CONCENTRATIONS IN GROUNDWATER				
		Historical Maximum	Current Maximum	
Constituent of	ESL	Detected	Concentration	
Concern	(µg/L)	Concentration (µg/L)	(µg/L)	
		MW-1		
TPHd	100	3,300	Replaced	
TPHg	100	5,210	Replaced	
Benzene	1	920	Replaced	
MW-1RA				
TPHd	100	4,000	3,700	
TPHg	100	6,800	6,800	
Benzene	1	830	780	
MW-1RB (Replaced MW-1)				
TPHd	100	1,900	1,900	
TPHg	100	650	310	
Benzene	1	9	9	

TABLE B				
Constituent of	ESL	Historical Maximum Detected	Current Maximum Concentration	
Concern	(µg/L)	Concentration (µg/L)	(µg/L)	
		MW-2	-	
TPHd	100	120	120	
TPHg	100	<50	<50	
Benzene	1	<0.5	<0.5	
		MW-3		
TPHd	100	1,800	740	
TPHg	100	310	<50	
Benzene	1	2	<0.5	
		MW-4		
TPHd	100	370	<50	
TPHg	100	<50	<50	
Benzene	1	<0.5	<0.5	
		MW-5		
TPHd	100	3,200	3,200	
TPHg	100	2,900	2,900	
Benzene	1	99	99	
MW-6				
TPHd	100	640	640	
TPHg	100	620	200	
Benzene	1	7	3	

Current maximum TPHd, TPHg, and benzene concentrations exceed ESLs. TPHd, TPHg, and benzene concentration trends in source area wells MW-1 (replaced by MW-1RB), MW-3, and MW-5 are generally stable to decreasing over time. Concentrations in newly installed wells MW-1RA, MW-1RB, and MW-6 are generally stable; however further sampling is required to establish a trend. Concentrations in the remaining wells (MW-2 and MW-4) are below ESLs (except for a slight exceedance of the TPHd ESL in MW-2 in the most recent sampling event). Based on current concentrations onsite, the groundwater cleanup goal will be to establish declining trends that predict ESLs will be achieved within a reasonable timeframe and that the residual dissolved mass is not impacting Alameda Canal. Prior canal sampling (Appendix D) indicates that Alameda Canal is not being impacted by residual mass remaining on site. Section 7.0 proposes a tidal influence study and mass flux calculation to confirm that Alameda Canal is not being impacted.

6.0 <u>REMEDIAL ALTERNATIVES DISCUSSION AND APPROACH</u>

Remedial alternatives are evaluated in this draft CAP based on implementing the most cost-effective remedial approach that will meet the cleanup goals stated above. This evaluation assumes the proposed mass flux calculation verifies that Alameda Canal is not being impacted by residual mass remaining on site.

6.1 <u>REMEDIAL ALTERNATIVES</u>

The following remedial technologies have been evaluated in the sections below on the basis of their ability to achieve the cleanup goal:

- Groundwater extraction (GWE)
- Multi-phase extraction (MPE)
- Air sparging-enhanced soil vapor extraction (AS/SVE)
- In-situ chemical oxidation (ISCO)
- In-situ enhanced biodegradation (ISEB)
- Monitored natural attenuation (MNA)

Each of these alternatives is evaluated below based on technical feasibility. The alternatives that are retained for consideration based on technical feasibility are then compared on the basis of cost effectiveness. The most cost-effective of the viable alternatives has been recommended for implementation at this site.

6.1.1 <u>GROUNDWATER EXTRACTION (GWE)</u>

GWE has historically been the most common remedial technology applied for groundwater restoration at petroleum hydrocarbon release sites. Groundwater is extracted using submersible pumps and routed to a fixed treatment system, utilizing treatment equipment such as granular-activated carbon (GAC) vessels or an air stripper. The treatment system removes COCs from the extracted groundwater and the treated groundwater is then typically discharged under permit to the sanitary or storm sewer after treatment.

Source removal can only be achieved indirectly using GWE, as contaminants gradually desorb from soil and enter the dissolved phase. The rate of desorption from soil is often the limiting factor for contaminant removal using GWE, thus requiring sustained operation of the system over a relatively long timeframe. Sustained pumping of groundwater will induce drawdown of the water table, creating a gradient toward the extraction well. Sufficient dewatering of the local formation can prevent contaminants from migrating with the natural groundwater flow and remove contaminants from areas away from the extraction well. However, dewatering can also potentially induce the migration of contaminants from outside the area of groundwater impacts at the site. Use of GWE and placement of extraction wells must be performed carefully to ensure that impacts from offsite sources are not artificially commingled with the onsite source.

6.1.1.1 <u>GWE FEASIBILITY EVALUATION</u>

Based on the remaining impacts, a fixed GWE system would include pumping from the vicinity of MW-5 and use of GAC to treat hydrocarbons in the extracted groundwater. GWE would be implementable at this site; however, a high extraction rate would be expected, given the close proximity to Alameda Canal, producing a large volume of extracted water to treat and dispose of.

6.1.1.2 <u>GWE RECOMMENDATION</u>

GWE is considered a viable remedial alternative for this site. Therefore, GWE has been retained for consideration and the overall cost to implement this technology is summarized in Table C shown in Section 6.2 below.

6.1.2 <u>MULTI-PHASE EXTRACTION (MPE)</u>

MPE consists of the vacuum-enhanced extraction of groundwater performed simultaneously with SVE. The vacuum increases the groundwater yield compared to standard GWE in low permeability formations. The extended dewatering of the saturated zone attained through GWE allows volatile constituents adsorbed to previously saturated soil to be removed in the vapor phase. In addition, the groundwater extraction component of MPE may provide hydraulic control of the chemical plume and reduce chemical migration as well as remove dissolved chemical mass. At this site, MPE would be performed by using a submersible groundwater pump to extract groundwater while the vacuum blower is used solely to extract soil vapors. The details of a MPE design would be based on site-specific pilot testing of the technology. The vapor extraction system would need a soil vapor treatment system (e.g., thermal destruction, GAC adsorption). Extracted groundwater would be treated and discharged to the sewer system.

6.1.2.1 <u>MPE FEASIBILITY EVALUATION</u>

MPE is typically used for the remediation of residual LNAPL and volatile petroleum hydrocarbons adsorbed to soil beneath the water table. Based on the close proximity to Alameda Canal and semi-confined water-bearing zone, dewatering of the remedial well may not be feasible. Additionally, MPE is not typically used to treat TPHd due to its low volatility. Therefore, MPE is not considered viable for this site.

6.1.2.2 <u>MPE RECOMMENDATION</u>

CRA does not recommend MPE for further consideration at this site and a cost estimate to implement this technology has not been presented below for comparison.

6.1.3 AIR SPARGING-ENHANCED SOIL VAPOR EXTRACTION (AS/SVE)

SVE is a process used to remove VOCs from soil in vapor phase by applying a vacuum in the vadose zone. SVE is a common remediation technology applied for addressing gasoline in the subsurface, such as at this site. AS is a remedial technology whereby air is injected into the saturated zone to remove VOCs from below the groundwater table. AS is typically implemented to remove VOCs adsorbed to saturated soil, although it can also be implemented to remove LNAPL or dissolved-phase VOCs. AS is typically designed to operate at relatively high air injection rates (greater than ten cubic feet per minute [cfm] per injection point) in order to volatilize the VOCs. AS usually operates in tandem with an SVE system that captures the VOCs stripped from the saturated zone. AS/SVE improves groundwater quality by removing source area VOC mass and by delivering oxygen to the subsurface to accelerate hydrocarbon biodegradation.

SVE system components would include appropriately constructed SVE wells, vapor conveyance piping, a vapor/liquid separator, a vapor extraction device, and a vapor treatment device. The vapor extraction device (blower) would be sized based on the

radius of influence and applied vacuum of the vapor extraction wells observed during pilot testing. Extracted hydrocarbons are typically treated by GAC, a catalytic or thermal oxidizer, or an internal combustion engine. The treatment device is determined by the influent flow rate, hydrocarbon concentrations, air quality requirements, and operating duration. Equipment required to implement AS would include a compressed air source (air compressor/blower), compressed air conveyance piping, and specifically designed AS wells. The air compressor or blower would be sized based on the number of injection points, pressure requirements, and minimum pressure and flow delivery at the injection depth.

6.1.3.1 <u>AS/SVE FEASIBILITY EVALUATION</u>

AS/SVE, like MPE, is typically used for the remediation of residual LNAPL and volatile petroleum hydrocarbons adsorbed to soil beneath the water table. Based on the fine grained soils and the very low oxygen levels (<1%) observed where the highest vapor concentrations have been collected (approximately 5 fbg), the radius of influence is expected to be very limited. Furthermore vapors generated from sparging into the silty sand water-bearing zone would likely be trapped below the overlying fine grained layer and not be captured by SVE. Therefore, AS/SVE is not considered viable for this site.

6.1.3.2 <u>AS/SVE RECOMMENDATION</u>

CRA does not recommend AS/SVE for further consideration at this site and a cost estimate to implement this technology has not been presented below for comparison.

6.1.4 IN-SITU CHEMICAL OXIDATION (ISCO)

ISCO uses a strong oxidizing agent to promote a chemical reaction with hydrocarbons. During the reaction, the oxidizing agent breaks the carbon bonds in unsaturated compounds and converts them into carbon dioxide (CO₂) and water (H₂O). Another benefit of ISCO includes an increase in dissolved oxygen, which in turn accelerates naturally-occurring hydrocarbon biodegradation.

Common oxidizing agents include permanganate (MnO_4), Fenton's reagent (hydrogen peroxide [H_2O_2] and ferrous iron [Fe⁺²]), ozone (O_3), and persulfate ($S_2O_8^{2-}$). Persulfate, a strong oxidizer, is commonly applied in the form of sodium persulfate to effectively buffer the pH (Interstate Technology & Regulatory Council Guidance Documents, 2005).

Because persulfate is also more persistent than H_2O_2 or ozone, the radius of influence will be greater. However, Fenton's reagent has been most commonly used and is effective when treating hydrocarbon contamination (Environmental Protection Agency Guidance Documents, 2005).

6.1.4.1 <u>ISCO FEASIBILITY EVALUATION</u>

While ISCO could be effective for remediating residual COC impacts in the subsurface, safety considerations outweigh the potential benefits of implementing this technology at the site. The exothermic reaction typical of most ISCO applications occurring in shallow groundwater near the existing building and underground utilities discourage the use of this technology. Therefore, CRA does not consider this technology viable for this site.

6.1.4.2 <u>ISCO RECOMMENDATION</u>

CRA does not recommend ISCO for further consideration at this site and a cost estimate to implement this technology has not been presented below for comparison.

6.1.5 IN-SITU ENHANCED BIODEGRADATION (ISEB)

Biodegradation is the process whereby chemicals are metabolized into less toxic or non-toxic compounds by naturally occurring microorganisms. The microorganisms utilize the chemicals as a source of carbon and energy. In order to enhance natural processes, nutrients and/or oxygen can be introduced into the subsurface, or microbial cultures appropriate for the degradation of target compounds can be introduced. ISEB manipulates site conditions to speed up degradation rates of COCs.

6.1.5.1 ISEB FEASIBILITY EVALUATION

One method for adding oxygen to the subsurface is ozone sparging. CRA would propose the use of ozone emitters in 2 to 3 wells in the remaining source area. Each emitter consists of a down-well ozone generator and delivery device, connected to an external air pump and power supply, mounted to the top of the well, and suspended below the water table. Air would be pumped from the surface down into the ozone generating device where ozone is generated and then injected from the device into the surrounding groundwater. This creates micro bubbles 0.5 to 2 millimeters in diameter that rise through the surrounding saturated soil. The micro bubbles increase molecular oxygen, which enhances bioremediation in the source area. Monitoring of aqueous geochemical parameters and dissolved chemical concentrations would be conducted to assess the effectiveness of the ISEB.

6.1.5.2 ISEB RECOMMENDATION

ISEB is considered a viable remedial alternative for this site. Therefore, ISEB has been retained for consideration and the overall cost to implement this technology is summarized in Table C shown in Section 6.2 below.

6.1.6 MONITORED NATURAL ATTENUATION (MNA)

Biodegradation, adsorption, chemical reactions, and volatilization can all naturally degrade hydrocarbons. Natural attenuation is defined as a process whereby the mass or concentration of a chemical compound is reduced over time or distance from the source area due to naturally occurring physical, chemical, and biological processes. The processes involved in natural attenuation of petroleum hydrocarbons include aerobic and anaerobic biodegradation, dispersion, volatilization, and adsorption (Wiedemeier, et al., 1999). The primary line of evidence to demonstrate the occurrence of natural attenuation in groundwater is the plume structure; a stable or shrinking plume is direct evidence that natural attenuation is occurring at a site. To evaluate the applicability of using remediation by natural attenuation, the site must be adequately assessed.

6.1.6.1 <u>MNA FEASIBILITY EVALUATION</u>

MNA is implementable at the site. Concentrations in site monitoring wells are either stable or decreasing. Based on current data, CRA cannot predict a timeframe for meeting ESLs. However, applying the concentration reduction trend for MW-1 before it was replaced with MW-1RB, the predicted timeframe for meeting ESLs was 16 years (Appendix E). To be conservative, CRA has chosen 30 years to calculate the cost of MNA. With MNA, the only cost associated with the alternative is for performing periodic groundwater monitoring and reporting.

6.1.6.2 <u>MNA RECOMMENDATION</u>

MNA is considered a viable remedial alternative for this site; however a mass flux evaluation, including an updated tidal study is needed before MNA can be fully recommended. Therefore, MNA has been retained for consideration and the overall cost to implement this technology is summarized in Table C shown in Section 6.2 below.

6.2 <u>SUMMARY OF REMEDIAL ALTERNATIVES</u>

TABLE C				
SUMMARY OF REMEDIAL ALTERNATIVES				
Alternative	GWE	ISEB	MNA	
Pilot Testing	\$25,000	NA	NA	
Design and Permitting	\$25,000	\$5,000	NA	
Equipment and Installation	\$150,000	\$20,000	NA	
Operational Duration	5	10	NA	
Average Annual Operational Cost	\$75,000	\$25,000	NA	
Total Operational Cost	\$375,000	\$250,000	NA	
Annual Groundwater Monitoring Cost	\$20,000	\$20,000	\$15,000	
Total Groundwater Monitoring Duration	7	12	30 years	
Total Groundwater Monitoring Cost	\$140,000	\$240,000	\$450,000	
System Demo	\$20,000	\$5,000	NA	
Closure Request/Well Destructions	\$50,000	\$50,000	\$50,000	
Total Cost	\$785,000	\$570,000	\$500,000	

Table C below presents the cost to perform GWE, ISEB, and MNA.

We recommend completing a tidal influence study so that the mass flux into Alameda Canal can be evaluated. If the results are favorable, MNA will be recommended as the preferred remedial strategy. The proposed tidal influence study and mass flux calculation is summarized in the following section.

7.0 PROPOSED MASS FLUX CALCULATION AND TIDAL INFLUENCE STUDY

The primary concern with this environmental case is TPHd, TPHg, and benzene migration into Alameda Canal. However, to accurately estimate the mass flux of

contaminants at the site, tidal influence on site groundwater from Alameda Canal must be taken into account. CRA proposes to install transducers temporarily in site wells as well as a stilling well off the marina dock to evaluate changes in groundwater elevation at the site. Groundwater elevation data will be collected for a period of 3 days and once all data has been collected, CRA will evaluate the data and perform the mass flux calculation as shown below.

Mass flux calculation is a method of estimating contaminant mass flowing past a cross section, perpendicular to groundwater flow direction (Alameda Canal in relation to groundwater flow direction), in the groundwater system per unit time (grams per day or g/d). These estimations are based on the following equation:

$$M_d = \sum_i^n Q_i C_i C_f$$

Where:

 M_d = Contaminant Mass Flux

 Q_i = Extraction rate from well

 C_i = Contaminant concentration measured in extracted groundwater (µg/L or ppb)

 C_f = Conversion factor = 5.45 x 10 -5 (min-L-g)/(d-gal-µg)

8.0 SOIL MANAGEMENT PLAN

The Soil Management Plan (SMP) has been prepared to provide information regarding residual petroleum constituents that may be present beneath the site to ensure that subsequent land owners, utility workers, and construction workers involved in future subsurface activities are made aware of the residual impact. It is recommended that site construction workers review this SMP prior to subsurface activities so that they are aware of site conditions and understand how to properly respond if residual petroleum-impacted materials are encountered during construction activities. Residual soil analytical data are presented in Tables 2 and 3. The approximate extent of TPHd and TPHg in soil is presented on Figures 6 and 7.

The extent of soil with elevated concentrations of one or more of the COCs generally appears limited to north and east of the westernmost building at the property in the vicinity of the former AST and fuel pumps. Based on the current and anticipated future land use, the only potential exposure pathway to residual impacted soil beneath the site is direct contact by construction workers. It is anticipated that the residual petroleum hydrocarbons in soil will continue to naturally degrade. Thus, the residual impacts at the site pose no significant risk to human health or the environment currently or in the foreseeable future.

8.1 <u>MANAGEMENT PLAN</u>

Prior to future subsurface activities at the site, a Health and Safety Plan (HASP) should be prepared by a qualified person describing the health and safety training requirements, personal protective equipment (PPE) requirements, specific personal hygiene, and monitoring and equipment that will be used during activities to protect and verify the health and safety of the construction workers and the general public from exposure to the COCs in soil. If impacted soil is encountered, it is recommended that subsurface construction activities cease and that the ACEH, current property owner/lessee, and Chevron be contacted to assess conditions and provide oversight for continued construction activities. The contact information for these parties is provided in Section 8.3.

It is recommended that all excavated soil suspected of containing petroleum hydrocarbons be stockpiled on, and covered with, plastic sheeting onsite or contained in an appropriately covered bin. Some of the field indicators for potential petroleum hydrocarbon impact in soil include the following:

- Gasoline or petroleum odor.
- Soil discoloration or staining (i.e. green, grey, and black) that is inconsistent with surrounding native material.

Samples should be collected (using EPA-approved protocols) of any soil intended to be transported offsite for disposal or other reasons and analyzed (at a minimum) for petroleum hydrocarbons by a state-certified analytical laboratory to determine the proper management/disposal procedures. The site property owner/lessee/developer should contact Chevron to arrange for proper characterization of any excavated material intended for disposal or offsite re-use and suspected of containing petroleum hydrocarbons.

As previously mentioned, groundwater at the site is relatively shallow and, subsurface activities should cease and Chevron should be contacted to determine proper management procedures. At no time should groundwater should be discharged to sanitary sewer lines, storm drains, the ground surface, or surface drainage systems (creeks, drainage ditches, etc.).

8.2 WORKER SAFETY AND EXPOSURE PROTECTION

It is recommended that workers who performs subsurface activities at the site have the appropriate Occupational Safety and Health Administration (OSHA) Hazardous Waste Operation and Emergency Response (HAZWOPER) training in accordance with 29 Code of Federal Regulations (CFR) 1910.120, so they are aware of proper operating procedures related to impacted materials. At a minimum, it is recommended that the construction foreman be OSHA HAZWOPER trained according to 29 CFR 1910.120 so they can provide appropriate oversight to site workers unfamiliar with proper operating procedures related to impacted materials and determine safe working areas for non-trained workers. Site workers working in areas where residual impacted soil may be encountered should wear appropriate Level D personal protective equipment consisting of gloves, steel-toed boots, safety glasses, and hard hats. Based on field conditions, the PPE may be upgraded to include respiratory protection.

8.3 <u>CONTACT INFORMATION</u>

As mentioned above, it is recommended that Chevron, ACEH, and the property lessee be contacted prior to initiating subsurface construction activities at the site so that they are aware of the construction schedule. If impacted material is encountered, subsurface construction activities at the site should cease and the following parties should be contacted immediately.

Chevron:	Mike Bauer	(714) 671-3207 Site Reference 20-6127
ACEH	Jerry Wickham	(510) 567-6791
Property Lessee	Monroe Wingate	(480) 551-6588
Property Manager	Tom Foley	(925) 671-7000

8.4 <u>LIMITATIONS</u>

This SMP is intended to provide the necessary background information and instructions to inform the reader of the potential for encountering petroleum hydrocarbon-impacted soil during construction work at this site. This document is not intended for use as a work plan or health and safety plan for future activities. CRA is not responsible for any activities at this site, unless performed by CRA employees.

9.0 <u>RECOMMENDED ALTERNATIVE</u>

Based on our evaluation of remedial alternatives, CRA selects MNA as the preferred remedial strategy contingent on the results of the mass flux calculation. Upon approval of this draft CAP, CRA will implementation activities associated with tidal influence study and mass flux calculation.

FIGURES





631916-2011(021)GN-WA003 AUG 04/2011



631916-2011(021)GN-WA001 AUG 04/2011



631916-2011(021)GN-WA001 AUG 04/2011

COMMERCIAL/INDUSTRIAL SOILS WHERE GROUNDWATER IS NOT A POTENTIAL DRINKING WATER SOURCE (DASHED WHERE INFERRED) TPHd ESL ISOCONTOUR FOR SHALLOW

COMMERCIAL/INDUSTRIAL SOILS WHERE GROUNDWATER IS NOT A POTENTIAL DRINKING WATER SOURCE (DASHED WHERE INFERRED)

figure 4

GEOLOGIC CROSS-SECTION B-B' 2301-2311 BLANDING AVENUÉ Alameda, California





631916-2011(021)GN-WA005 AUG 04/2011



631916-2011(021)GN-WA006 AUG 04/2011



631916-2011(021)GN-WA007 AUG 04/2011


631916-2011(021)GN-WA008 AUG 04/2011



631916-2011(021)GN-WA009 AUG 04/2011

WELL CONSTRUCTION SPECIFICATIONS FORMER SIGNAL OIL MARINE STORAGE AND DISTRIBUTION FACILITY (CHEVRON BULK PLANT 20-6127) 2301-2311 BLANDING AVENUE ALAMEDA, CALIFORNIA

				Casing				
Well ID	Date Installed	тос	Total Depth (fbg)	Diameter ¹ (inches)	Slot Size (inches)	Screen Interval (fbg)	Filter Pack (fbg)	Status
Monitoring	Wells							
MW-1	8/15/1990	13.49	19.5	2	0.020	4-19	3-19.5	Replaced w/MW-1RB
MW-1RA	8/4/2010	13.02	13	2	0.020	8-13	7-13	Active
MW-1RB	8/4/2010	13.21	20	2	0.020	16.5-20	15.5-20	Active
MW-2	6/19/2009	10.63	18	2	0.020	10.5-15.5	10-16	Active
MW-3	6/19/2009	10.72	18.5	2	0.020	13.5-18.5	12.5-18.5	Active
MW-4	6/19/2009	11.40	20.5	2	0.020	15.5-20.5	14.5-20.5	Active
MW-5	6/23/2009	10.50	18	2	0.020	13-18	12-18	Active
MW-6	8/4/2010	12.98	20	2	0.020	16.5-20	15.5-20	Active
Vapor Well	<u>s</u>							
VP-1	7/9/2008	NS	4.25	1	0.020	3.75-4.25	3.5-4.5	Vapor only
VP-2	7/9/2008	NS	4.75	1	0.020	4.25-4.75	4-5	Vapor only
VP-3	7/14/2008	NS	5.75	1	0.020	5.25-5.75	5-6	Vapor only
VP-4	7/14/2008	NS	5.75	1	0.020	5.25-5.75	5-6	Vapor only
VP-5	7/14/2008	NS	5.75	1	0.020	5.25-5.75	5-6	Vapor only
VP-6	7/9/2008	NS	5.75	1	0.020	5.25-5.75	5-6	Vapor only
Sub-Slab V	apor Probes							
VP-7	7/17/2009	NS	0.5	0.25	NA	NA	NA	Vapor only
VP-8	7/17/2009	NS	0.5	0.25	NA	NA	NA	Vapor only
VP-9	7/22/2009	NS	0.5	0.25	NA	NA	NA	Vapor only
VP-10	7/22/2009	NS	0.5	0.25	NA	NA	NA	Vapor only
VP-11	7/17/2009	NS	0.5	0.25	NA	NA	NA	Vapor only
VP-12	7/22/2009	NS	0.5	0.25	NA	NA	NA	Vapor only
VP-13	7/22/2009	NS	0.5	0.25	NA	NA	NA	Vapor only

Abbreviations / Notes

TOC = Top of casing elevation (feet above mean sea level)

¹ = Schedule 40 PVC casing material

fbg = Feet below grade

NA = Not applicable

NS = Not surveyed

Boring ID	Depth (fbg)	Sample Date	TPHd	TPHg	Benzene	Toluene	Ethylbenzene	m+p-Xylene	o-Xylene	Total Xylenes	MTBE	Acetone	Carbon Disulfide	2-Butanone	Isopropyl- benzene	n-Propyl- benzene	1,3,5 - Trimethyl- benzene	tert-Butyl- benzene	1,2,4- Trimethyl- benzene	sec-Butyl- benzene	p-Isopropyl- toluene	n-Butyl- benzene	Naphthalene
											Concer	ntrations repor	ted in milligra	m per kilogran	n - mg/kg								
SB-1	3.5	2/17/1995	110	ND	ND^1	ND^1	ND^1			ND^1													
SB-1	5.5	2/17/1995	10	390	0.08^{1}	0.20^{1}	0.58^{1}			0.86^{1}													
SB-1	9.5	2/17/1995	ND	ND	ND^1	ND^1	ND^1			ND^1													
CR 2	2.5	2 / 20 / 1005	40	NID	ND^1	NID^1	ND^1			ND^1													
5D-2	5.5	2/20/1995	40	2,000	1 ND 2.7^{1}	ND 24 ¹	14 ¹																
5D-2	/	2/20/1995	35	2,000	5.7	34	14			40													
SB-3	1.5	2/17/1995	ND	ND	ND^1	ND^1	ND^1			ND^1													
SB-3	7	2/17/1995	230	150	ND^1	0.46^{1}	0.58^{1}			0.51^{1}													
SB-3	10	2/17/1995	ND	ND	ND^1	ND^1	ND^1			ND^1													
SB-4	15	2/17/1995	20	ND	ND^1	ND^1	ND^1			ND^1													
SB-4	6.5	2/17/1995	240	860	2.0^{1}	0.81 ¹	36^{1}			13 ¹													
SB-4	7	2/17/1995	240		2.0^{2}	8.7 ²	3.5^2			35 ²													
SB-4	10	2/17/1995	ND	4	0.34^{1}	ND^1	ND^1			ND^1													
		_, _, , _, ., .		-																			
SB-5	1.5	2/17/1995	10	ND	ND^1	ND^1	ND^1			ND^1													
SB-5	5.5	2/17/1995	15	ND	ND^1	ND^1	ND^1			ND^1													
SB-5	6	2/17/1995			ND^2	ND^2	ND^2			ND^2													
SB-6	15	2/17/1995	40	ND	ND^1	ND^1	ND^1			ND^1													
SB-6	7	2/17/1995	170	400	ND^1	0.12^{1}	0.56^{1}			ND^1													
000	,	2/11/1990	170	100	112	0.12	0.00			112													
SB-7	1	2/17/1995	110	ND	ND^1	ND^1	ND^1			ND^1													
SB-7	4	2/17/1995	250	ND	ND^1	ND^1	ND^1			ND^1													
CD 0	1	0 / 00 / 1005	75	NID	NID^1	NID^1	ND^1			ND^1													
5D-8	1	2/20/1995	75	ND		ND ND ¹	ND ND ¹																
SB-8	6.5	2/20/1995	ND	ND	ND	ND ND ²	ND ND ²			ND^{2}													
56-8	7	2/20/1995			ND	ND	ND			ND													
SB-9	5	10/28/1998	$3,300^3$	130	0.36^{1}	< 0.12 ¹	< 0.12 ¹			0.28^{1}	< 0.62 ¹												
SB-9	13	10/28/1998	$1,300^{3}$	900	3.3^{1}	<1.2 ¹	2.1^{1}			2.0^{1}	<12 ⁴												
SB-9	15	10/28/1998	1.2 ³	<1.0	0.22^{1}	$< 0.0050^{1}$	< 0.0050 ¹			$< 0.0050^{1}$	< 0.025 ¹												
CD 10		10/00/1000	1203	-1.0		<0.00F0 ¹	<0.00 5 0 ¹			<0.00F0 ¹	<0.0 2 5 ¹												
SD-10	5.5	10/28/1998	150	<1.0	<0.0050	<0.0050	<0.0050			<0.0050	N0.025												
SB-11	6	10/28/1998	60^{3}	140	< 0.10 ¹	0.12^{1}	0.24^{1}			0.49^{1}	< 0.50 ¹												
CR 12	F	10/29/1009	<10	<10	<0.0050 ¹	<0.0050 ¹	$< 0.0050^{1}$			<0.0050 ¹	<0.025 ¹												
SD-12 CD 10	5	10/28/1998	<1.0	<1.0	< 0.0050	<0.0050	<0.0050 ¹			<0.0050 ¹	<0.025												
SD-12 CD 12	14	10/28/1998	<1.0 <1.0	<1.0	< 0.0050	<0.0050	<0.0050 ¹			<0.0050 ¹	<0.025												
5D-12	14	10/28/1998	<1.0	<1.0	<0.0050	<0.0050	<0.0050			<0.0050	<0.025												
MW-1	5	12/29/2000	30	<1.0	< 0.0050	< 0.0050	< 0.0050			0.017	< 0.050												
MW-1	10	12/29/2000	160	320	0.40	1.6	0.90			1.1	<1.2												
MW-1	15	12/29/2000	<1.0	<2.5	0.53	0.021	0.028			0.065	< 0.12												
S 1	0.5	1/13/2004	14	<10	<0.0005	<0.001	<0.001			<0.001	<0.0005												_
52	0.5	1/13/2004	220	<20		<0.001	<0.001			<0.001													
52	0.5	1/13/2004	220	~20		<0.001	<0.001			<0.001													
50	0.5	1/15/2004	220	N10	NU.0005	\0.001	NU.UU1			\0.001	NU.0005												

SOIL ANALYTICAL RESULTS FORMER SIGNAL OIL MARINE STORAGE AND DISTRIBUTION FACILITY (CHEVRON FACILITY 20-6127) 2301-2311 BLANDING AVENUE ALAMEDA, CALIFORNIA

Boring ID	Depth (fbg)	Sample Date	TPHd	TPHg	Benzene	Toluene	Ethylbenzene	m+p-Xylene	o-Xylene	Total Xylenes	MTBE	Acetone	Carbon Disulfide	2-Butanone	Isopropyl- benzene	n-Propyl- benzene	1,3,5 - Trimethyl- benzene
											Concer	itrations repoi	rted in milligra	am per kilogran	n - mg/kg		
VP-1	3	7/9/2008	12	<1.0	0.001	0.003	0.002	0.004	0.002		< 0.0005	<0.007	<0.001	< 0.004	0.001	0.003	<0.001
VP-2*	3	7/9/2008	240	330	0.079	0.080	0.080	0.18	0.066		<0.026	<0.36	< 0.051	<0.21	0.23	0.51	0.088
VP-2	5	7/9/2008	2,100	670	0.52	0.16	0.36	0.46	0.085		<0.025	0.44	<0.50	<0.20	4.6	9.9	0.065
VP-3	2.5	7/14/2008	5.4	<1.0	< 0.0005	<0.0009	< 0.0009	< 0.0009	< 0.0009		< 0.0005	< 0.007	< 0.0009	< 0.004	< 0.0009	< 0.0009	< 0.0009
VP-3	5	7/14/2008	<4.0	<1.0	0.001	< 0.0009	< 0.0009	< 0.0009	<0.0009		< 0.0005	0.039	<0.0009	0.007	< 0.0009	<0.0009	< 0.0009
VP-4	2.5	7/14/2008	1,700	1,300	5.0	0.54	13	8.1	0.60		< 0.024	0.65	< 0.048	<0.19	3.7	5.9	4.1
VP-4	5	7/14/2008	6,900	11,000	16	2.4	120	15	2.8		<0.093	<1.3	<0.19	<0.74	27	48	11
VP-5	2.5	7/14/2008	20	1.7	0.0008	< 0.001	< 0.001	< 0.001	< 0.001		< 0.0005	< 0.007	< 0.001	< 0.004	< 0.001	0.001	< 0.001
VP-5	5	7/14/2008	6,000	540	0.11	0.051	0.11	0.23	0.072		<0.023	< 0.33	< 0.047	<0.19	1.1	1.6	0.13
VP-6	3	7/9/2008	340	<10	< 0.0005	< 0.001	< 0.001	< 0.001	< 0.001		< 0.0005	< 0.007	< 0.001	< 0.004	< 0.001	< 0.001	< 0.001
VP-6	5	7/9/2008	350	910	<0.026	<0.053	0.31	0.37	<0.053		<0.026	<0.37	<0.053	0.33	2.1	3.3	0.10
SB-13	1	7/7/2008	47	1.0	<0.0005	< 0.001	< 0.001	0.002	< 0.001		< 0.0005	< 0.007	< 0.001	< 0.004	< 0.001	< 0.001	< 0.001
SB-13	5	7/7/2008	630	350	< 0.027	< 0.054	< 0.054	< 0.054	< 0.054		< 0.027	< 0.38	< 0.054	< 0.22	0.12	0.14	< 0.054
SB-13	10	7/8/2008	<4.0	<1.0	< 0.0005	< 0.001	< 0.001	< 0.001	< 0.001		< 0.0005	<0.007	< 0.001	< 0.004	< 0.001	< 0.001	< 0.001
SB-14	1	7/7/2008	89	<1.0	0.002	0.004	0.002	0.005	0.003		< 0.0005	0.018	< 0.001	< 0.004	< 0.001	< 0.001	< 0.001
SB-14	5	7/7/2008	29	<1.0	0.002	0.003	0.002	0.003	0.002		< 0.0005	0.026	< 0.001	0.005	< 0.001	< 0.001	< 0.001
SB-14	10	7/8/2008	<4.0	<1.0	0.0006	0.001	<0.001	0.002	0.001		< 0.0005	<0.007	< 0.001	< 0.004	< 0.001	<0.001	< 0.001
SB-15	1	7/7/2008	45	<1.0	0.0007	0.001	< 0.001	0.001	< 0.001		< 0.0005	< 0.007	< 0.001	< 0.004	< 0.001	< 0.001	< 0.001
SB-15	5	7/7/2008	42	<1.0	< 0.0005	< 0.001	< 0.001	< 0.001	< 0.001		< 0.0005	< 0.007	< 0.001	< 0.004	< 0.001	< 0.001	< 0.001
SB-15	9.5	7/8/2008	71	1.0	0.002	0.006	0.005	0.012	0.006		<0.0005	<0.007	<0.001	< 0.004	0.001	0.001	0.001
SB-16A	1	7/7/2008	140	<10	0.004	0.012	0.008	0.024	0.013		< 0.0005	< 0.007	< 0.001	< 0.004	0.001	0.001	0.001
SB-16B	1	7/7/2008	83	<1.0	0.004	0.013	0.012	0.035	0.019		< 0.0005	< 0.007	< 0.0009	< 0.004	0.002	0.002	0.002
SB-16C	2	7/8/2008	250	<10	0.003	0.009	0.006	0.018	0.011		< 0.0005	< 0.007	< 0.001	< 0.004	0.001	0.001	0.002
SB-16C	3	7/8/2008	960	<40	0.005	0.008	0.006	0.018	0.011		< 0.0005	0.063	0.002	0.012	0.001	0.002	0.003
SB-17	1	7/7/2008	120	<10	0.0007	0.001	< 0.001	0.002	0.001		< 0.0005	0.015	0.001	< 0.004	< 0.001	< 0.001	< 0.001
SB-17	5	7/7/2008	97	40	0.22	0.053	0.63	1.3	0.19		< 0.025	< 0.35	< 0.050	< 0.20	0.14	0.35	0.73
SB-17	9.5	7/8/2008	<4.0	4.9	0.021	0.003	0.025	0.013	0.003		< 0.0005	0.015	< 0.001	< 0.004	0.016	0.015	0.003
SB-18	1	7/7/2008	61	150	0.0008	0.002	0.003	0.005	0.003		< 0.0005	< 0.007	0.002	< 0.004	0.003	0.003	< 0.001
SB-18	5	7/7/2008	1,500	630	0.21	< 0.052	0.053	0.098	< 0.052		< 0.026	< 0.37	< 0.052	< 0.21	0.36	0.61	0.089
SB-18	10	7/8/2008	310	160	0.056	< 0.049	< 0.049	<0.049	< 0.049		<0.024	< 0.34	< 0.049	<0.19	0.10	0.11	< 0.049
SB-19	1	7/7/2008	190	<10	0.001	0.002	< 0.001	0.002	0.001		< 0.0005	< 0.008	< 0.001	< 0.004	< 0.001	< 0.001	< 0.001
SB-19	5	7/7/2008	680	960	0.29	0.92	3.9	7.6	3.3		< 0.023	0.43	< 0.047	<0.19	4.5	4.7	3.2
SB-19	10	7/8/2008	<4.0	<1.0	< 0.0005	<0.001	<0.001	<0.001	< 0.001		< 0.0005	< 0.007	< 0.001	< 0.004	< 0.001	< 0.001	< 0.001
MW-2	4.5	6/18/2009	480	1,100	< 0.027	<0.055	0.19			0.19	<0.027						
MW-2	8.5	6/19/2009	17	4.8	< 0.0005	< 0.001	< 0.001			< 0.001	< 0.0005						

SOIL ANALYTICAL RESULTS FORMER SIGNAL OIL MARINE STORAGE AND DISTRIBUTION FACILITY (CHEVRON FACILITY 20-6127) 2301-2311 BLANDING AVENUE ALAMEDA, CALIFORNIA

-	tert-Butyl- benzene	1,2,4- Trimethyl- benzene	sec-Butyl- benzene	p-Isopropyl- toluene	n-Butyl- benzene	Naphthalene
	<0.001	<0.001	< 0.001	0.002	<0.001	<0.001
	0.098	0.29	0.18	< 0.051	0.22	0.28
	0.84	0.11	1.8	0.051	4.4	0.48
	< 0.0009	< 0.0009	<0.0009	<0.0009	<0.0009	<0.0009
	<0.0009	<0.0009	<0.0009	< 0.0009	<0.0009	< 0.0009
	0.32	41	1.4	2.5	2.0	3.4
	3.0	5.0	11	13	23	42
	< 0.001	0.001	< 0.001	0.001	0.001	0.010
	< 0.047	0.33	0.37	0.42	0.37	0.83
	< 0.001	< 0.001	< 0.001	< 0.001	< 0.001	< 0.001
	0.060	< 0.053	1.1	0.26	1.7	2.9
	< 0.001	< 0.001	< 0.001	0.003	< 0.001	< 0.001
	< 0.054	< 0.054	0.23	< 0.054	0.12	0.16
	< 0.001	< 0.001	< 0.001	< 0.001	< 0.001	< 0.001
	< 0.001	0.001	< 0.001	0.001	< 0.001	< 0.001
	< 0.001	< 0.001	< 0.001	< 0.001	< 0.001	< 0.001
	< 0.001	< 0.001	< 0.001	0.001	< 0.001	<0.001
	< 0.001	< 0.001	< 0.001	< 0.001	<0.001	< 0.001
	< 0.001	< 0.001	< 0.001	< 0.001	< 0.001	< 0.001
	< 0.001	0.002	< 0.001	0.008	< 0.001	0.001
	< 0.001	0.003	< 0.001	0.007	< 0.001	< 0.001
	< 0.0009	0.006	< 0.0009	0.015	< 0.0009	< 0.0009
	< 0.001	0.004	< 0.001	0.007	< 0.001	< 0.001
	< 0.001	0.006	< 0.001	0.01	< 0.001	0.001
	< 0.001	< 0.001	< 0.001	0.002	< 0.001	<0.001
	< 0.050	2.7	0.063	0.18	0.13	0.96
	0.001	0.002	0.005	0.003	0.004	0.007
	0.005	0.002	0.013	0.003	0.005	0.013
	< 0.052	0.57	0.44	0.45	0.72	4.9
	< 0.049	< 0.049	0.053	0.079	0.095	<0.049
	< 0.001	0.002	< 0.001	0.002	< 0.001	< 0.001
	0.28	5.3	1.4	42	2.0	3.8
	< 0.001	< 0.001	< 0.001	< 0.001	<0.001	<0.001

Boring ID	Depth (fbg)	Sample Date	TPHd	TPHg	Benzene	Toluene	Ethylbenzene	m+p-Xylene	o-Xylene	Total Xylenes	MTBE	Acetone	Carbon Disulfide	2-Butanone	Isopropyl- benzene	n-Propyl- benzene	1,3,5 - Trimethyl- benzene	tert-Butyl- benzene	1,2,4- Trimethyl- benzene	sec-Butyl- benzene	p-Isopropyl- toluene	n-Butyl- benzene	Naphthalene
											Concen	trations repor	ted in milligra	am per kilogran	n - mg/kg								
MW-3	4	6/18/2009	610	700	0.64	0.099	6.1			0.85	<0.026												
MW-3	6	6/18/2009	170	960	0.39	0.069	2.5			0.67	< 0.025												
MW-3	8.5	6/19/2009	16	66	0.062	0.003	0.058			0.012	< 0.0005												
MW-4	15	6/19/2009	<4.0	<1.0	<0.0005	<0.0009	<0.0009			<0.0009	<0.0005												
MW-5	7	6/19/2009	500	520	0.076	< 0.049	0.061			< 0.080	< 0.024												
MW-5	10.5	6/23/2009	36	170	0.043	< 0.048	< 0.048			0.048	< 0.024												
MW-5	14	6/23/2009	270	170	0.075	< 0.047	< 0.047			< 0.047	<0.023												
MW-1RA ⁵	10	8/4/2010	260^{3}	380	0.54	< 0.050	0.43			0.12	< 0.025												
MW-1RA ⁵	13.5	8/4/2010	120^{3}	490	0.24	< 0.050	0.068			0.057	< 0.025												
MW-6	15	8/4/2010	<4.0 ³	1.2	0.12	0.002	0.003			0.003	<0.0005												
	ESLs		180	180	0.27	9.3	4.7	11	11	11	8.4	0.5	NE	NE	NE	NE	NE	NE	NE	NE	NE	NE	2.8

Abbreviations and Notes:

fbg = Feet below grade

TPHd = Total petroleum hydrocarbons as diesel by EPA Method 8015

TPHg = Total petroleum hydrocarbons as gasoline by EPA Method 8015

<x = not detected at or above stated laboratory reporting limit</pre>

 1 = EPA Method 8020 2 = EPA Method 8240

³ = Additional analyses were performed with silica gel cleanup

⁴ = RRM reported as a false positive associated with EPA Method 8020

⁵ = The GC/MS volatile analysis was performed according to the high level soil method due to the level of non-target compounds. Therefore, the reporting limits were raised.

-- = Not Analyzed

* 1,2,3-Trichlorobenzene also detected at 0.067 mg/kg

ND = Not detected

VOCs = Volatile organic compounds by EPA method 8260B

Note: Other VOCs not included in the table were not detected in any of the samples.

ESL = Environmental screening level for shallow soil (<3m fbg) at commercial/industrial sites where groundwater is not a current or potential source of drinking water (Table B)-RWQCB May 2008 NE = Not established

Benzene, toluene, ethylbenzene, and xylenes EPA Method 8260B

MTBE = Methyl tertiary butyl ether EPA Method 8260B

TABLE 2

SOIL ANALYTICAL RESULTS FORMER SIGNAL OIL MARINE STORAGE AND DISTRIBUTION FACILITY (CHEVRON FACILITY 20-6127) 2301-2311 BLANDING AVENUE ALAMEDA, CALIFORNIA

SOIL ANALYTICAL DATA - METALS FORMER SIGNAL OIL MARINE STORAGE AND DISTRIBUTION FACILITY (CHEVRON BULK PLANT 20-6127) 2301-2311 BLANDING AVENUE, ALAMEDA, CALIFORNIA

Boring ID	Depth (ft)	Sample Date	Mercury	Thallium	Arsenic	Selenium	Antimony	Barium	Beryllium	Cadmium	Chromium	Cobalt	Copper	Lead	Molybdenum	Nickel	Silver	Vanadium	Zinc
									Concentratio	ons reporte	d in milligran	n per kilogi	am (mg/kg)					
SB-1	3	2/17/1995	0.43	7	6.1	ND	2	110	0.2	0.7	39	9.6	51	110	ND	30	0.1	37	210
SB-2	2	2/20/1995	0.7	ND	9.7	ND	2	120	0.1	ND	89	11	170	77	0.7	49	0.1	35	280
SB-3	1	2/17/1995	0.71	6	68	ND	2	56	0.2	ND	12	7.4	19	22	0.3	16	0.2	32	90
SB-4	1	2/17/1995	0.63	4	46	ND	2	59	0.2	ND	17	9.3	36	30	0.7	22	0.3	34	110
SB-5	1	2/17/1995	0.37	3	12	ND	1	46	0.2	ND	19	7.7	21	12	ND	22	0.2	32	74
SB-6	1	2/17/1995	0.94	8	130	ND	4	67	0.2	ND	16	8.7	31	32	1.1	23	0.7	34	100
SB-7	1.5	2/17/1995	0.16	ND	ND	ND	2	150	0.1	0.3	36	7.1	44	89	ND	24	0.1	47	200
SB-8	0.5	2/20/1995	0.09	ND	4.5	ND	2	88	0.2	ND	23	7.8	30	30	ND	15	ND	29	110
VP-1	3	7/9/2008	0.0756	<1.25	2.32	<0.961	<0.980	92.6	0.225	<0.137	5.68	2.95	23	42.1	0.565	6.08	0.184	27.6	117
VP-2 VP-2	3 5	7/9/2008 7/9/2008	0.247 0.025	<1.26 <1.21	6.78 1.78	<0.970 <0.933	<0.990 <0.952	137 78.8	0.392 0.166	<0.139 <0.133	17.9 24.9	7.01 4.13	47.4 7.19	185 9.67	1.04 0.463	15.8 9.17	0.302 <0.162	38.3 22.2	167 10.7
VP-3 VP-3	2.5 5	7/14/2008 7/14/2008	0.285 0.155	2.26 <1.22	9.45 3.46	<0.980 <0.942	2.64 <0.962	164 94.5	0.235 0.149	<0.700 <0.135	101 34.5	7 3.47	175 13.7	189 19.5	3.26 <0.423	45.7 33.7	0.393 <0.163	51.3 23.6	690 45.5
VP-4 VP-4	2.5 5	7/14/2008 7/14/2008	0.883 0.0134	<1.25 <1.25	8.37 3.19	<0.961 <0.961	4.15 <0.980	1,090 70.4	0.221 0.149	2.44 <0.137	41.4 34.4	3.41 2.46	139 5.91	903 16.3	0.743 <0.431	21.4 13.7	0.351 <0.167	27.9 32.6	1,670 15.5
VP-5 VP-5	2.5 5	7/14/2008 7/14/2008	0.256 0.0849	2.24 <1.26	5.74 3.2	<0.970 <0.970	1.23 <0.990	198 94.2	0.3 0.136	<0.139 <0.139	29.4 27.6	7.44 3.17	40.8 11.2	63.9 21.9	0.582 <0.436	26.1 10.8	0.421 <0.168	61.7 25.5	190 138
VP-6 VP-6	3 5	7/9/2008 7/9/2008	0.154 0.0342	<1.27 <1.25	5.86 3.72	<0.980 <0.961	<1.00 <0.980	80.6 188	0.562 0.325	<0.140 <0.137	18.6 46.4	7.43 2.12	27.7 11.1	50.6 5.24	1.08 <0.431	29.3 42.2	0.203 <0.167	27.9 39.1	88.5 29.3
SB-13 SB-13 SB-13	1 5 10	7/7/2008 7/7/2008 7/8/2008	0.118 0.0529 0.0223	<1.25 <1.26 <1.26	21.6 3.27 3.14	<0.961 <0.970 <0.970	<0.980 <0.990 <0.990	105 98.2 127	0.265 0.364 0.3	0.329 <0.137 <0.139	34.7 55.2 52.1	6.84 5.13 5.77	28.4 8.47 12.5	141 4.08 3.8	0.559 <0.436 <0.436	20.2 48.7 45	<0.167 <0.168 <0.168	30.5 32.1 36.6	144 23 30.2
SB-14 SB-14 SB-14	1 5 10	7/7/2008 7/7/2008 7/8/2008	0.114 0.0353 0.028	<1.25 <1.21 <1.27	8.17 5.39 3.04	<0.961 <0.933 <0.980	<0.980 <0.952 <1.00	111 53.4 397	0.242 0.272 0.306	<0.139 <0.139 <0.140	29.9 12 51.4	8.27 5.29 9.57	59.4 15.3 11.8	115 14 3.29	1.02 <0.419 <0.440	28.9 4.9 51.1	<0.167 <0.162 0.547	42.4 25.2 37.2	369 84.6 28.8
SB-15 SB-15 SB-15	1 5 9.5	7/7/2008 7/7/2008 7/8/2008	0.117 0.157 <0.0109	<1.27 <1.22 <1.25	7.1 34.7 3.23	<0.980 <0.942 <0.961	1.75 <0.962 <0.980	126 112 132	0.303 0.249 0.362	0.267 0.169 <0.137	71.5 41.5 43.9	11.3 7.66 3.25	116 58.7 11.7	107 74.1 5.77	0.809 0.888 0.673	167 27.5 42.1	0.191 <0.163 <0.167	42.7 30.4 27.6	283 153 30.1
SB-16A SB-16B SB-16C SB-16C	1 1 2 3	7/7/2008 7/7/2008 7/8/2008 7/8/2008	0.14 0.112 0.219 0.233	<1.27 <1.22 <1.27 <1.27	22.2 9.6 9.74 12.5	<0.980 <0.942 <0.980 <0.980	<1.00 5.8 2.4 <1.0	230 181 184 183	0.459 0.228 0.229 0.263	0.263 <0.135 0.272 2.61	45.9 275 66.3 49.5	9.07 12.7 6.54 4.8	184 180 254 90.7	115 125 204 264	0.958 10.6 1.63 1.25	34.3 129 39.1 39.4	0.387 0.469 0.363 0.247	37.4 42.7 36.1 31.4	1,340 876 408 268

SOIL ANALYTICAL DATA - METALS FORMER SIGNAL OIL MARINE STORAGE AND DISTRIBUTION FACILITY (CHEVRON BULK PLANT 20-6127) 2301-2311 BLANDING AVENUE, ALAMEDA, CALIFORNIA

Boring ID	Depth (ft)	Sample Date	Mercury	Thallium	Arsenic	Selenium	Antimony	Barium	Beryllium	Cadmium	Chromium	Cobalt	Copper	Lead	Molybdenum	Nickel	Silver	Vanadium	Zinc
									Concentrati	ons reported	d in milligran	n per kilog	ram (mg/kg)					
SB-17	1	7/7/2008	0.144	<1.25	4.49	< 0.961	< 0.980	121	0.322	0.316	63.1	9.16	65.2	81.5	0.678	49.5	0.177	38.3	162
SB-17	5	7/7/2008	0.0337	<1.22	2.47	< 0.942	< 0.962	87.8	0.209	< 0.137	26.2	5.37	12.2	22.4	< 0.423	10.7	< 0.163	24.1	38.5
SB-17	9.5	7/8/2008	< 0.0113	1.52	14.9	< 0.961	< 0.980	118	0.154	<0.137	48.5	6.3	12.2	3.69	< 0.431	47.6	0.34	38.5	29
SB-18	1	7/7/2008	0.0528	<1.27	3.1	< 0.980	<1.00	106	0.293	< 0.136	53.7	7.41	43.5	30.5	< 0.440	42.1	< 0.170	31.8	58.1
SB-18	5	7/7/2008	0.361	<1.25	3.14	< 0.961	< 0.980	117	0.206	0.605	30.4	7.15	32.9	164	0.544	12.9	0.338	24	478
SB-18	10	7/8/2008	0.0163	4.78	6.05	< 0.942	< 0.962	82.3	0.123	<0.135	48	5.14	13.6	3.56	<0.423	44.8	0.244	35.9	27.2
SB-19	1	7/7/2008	0.184	<1.21	8.31	0.965	3.11	313	0.455	60.6	29.7	6.81	26.7	353	0.438	24.4	0.296	25.3	318
SB-19	5	7/7/2008	0.033	<1.22	3.63	< 0.942	< 0.962	114	0.397	< 0.133	52.9	6.51	10.2	10.4	< 0.423	66.6	< 0.163	39.7	30.9
SB-19	10	7/8/2008	0.0568	<1.25	1.78	< 0.961	< 0.980	91.8	0.145	< 0.137	54.1	5.19	11.1	2.9	< 0.431	44.3	0.201	35.7	29.8
	ESLs		10	16	1.6	10	40	1,500	8.0	7.4	750*	80	230	750	40	150	40	200	600

Abbreviations / Notes

CAM 17 Metals by EPA Method 6010B/7471A

<x = not detected at or above the stated laboratory reporting limit</pre>

Concentrations in **bold** indicate that the constituent exceed their respective ESL

ND = Not detected at or above the stated laboratory reporting limit

ESL = Environmental screening level for shallow soil (<3m fbg) at commercial/industrial sites where groundwater is not a current or potential source of drinking water (Table B)-RWQCB May 2008 * ESL is for Chromium III

HISTORICAL GRAB GROUNDWATER ANALYTICAL DATA FORMER SIGNAL OIL MARINE STORAGE AND DISTRIBUTION FACILITY (CHEVRON BULK PLANT 20-6127) 2301-2311 BLANDING AVENUE, ALAMEDA, CALIFORNIA

Boring/ Well ID	Sample Date	TPHd	TPHg	Benzene	Toluene	Ethyl- benzene	m+p Xylene	o-Xylene	MTBE	Vinyl Chloride	cis-1,2- DCE	TCE	Isopropyl- benzene	n-Propyl- benzene	1,3,5- Trimethyl- benzene	tert-Butyl- benzene	1,2,4- Trimethyl- benzene	sec-Butyl- benzene	p- Isopropyl- toluene	n-Butyl- benzene	Naphthale ne	TBA	Aceton e	Metals
											Con	ıcentrati	ons in micro	ograms per	liter (µg/L)									
GWS-7	4/24/1995	ND	ND	ND	ND	ND	ND	ND																
GWS-8	4/24/1995	0.06	3.7	0.036	0.0069	0.027	0.011 ²																	
GWS-9	4/24/1995	1.2	22	6.2	0.14	1.1	1.2 ²																	
GWS-10	4/24/1995	0.24	11	0.88	0.04	0.1	0.05 ²																	
GWS-11	4/24/1995	0.07	1.4	ND	0.001	0.0014	0.0084^{2}																	
GWS-12	4/24/1995	ND	ND	ND	0.0006	ND	ND	ND																
GWS-13	4/24/1995	ND	ND	ND	ND	ND	ND	ND																
GWS-14	4/24/1995	ND	ND	ND	ND	ND	ND	ND																
GWS-15	4/24/1995	ND	ND	ND	ND	ND	ND	ND																
GWS-16	4/24/1995	ND	0.07	ND	ND	0.002	0.0011 ²																	
SB-13	7/8/2008	600	<50	<0.5	<0.5	<0.5	<0.5	<0.5	3.0	<1.0	<0.8	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<5.0	<6.0	
SB-14	7/8/2008	750	<50	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<1.0	<0.8	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<5.0	<6.0	
SB-15	7/8/2008	430	<50	<0.5	<0.5	<0.5	<0.5	<0.5	0.8	1.0	69	5.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<5.0	<6.0	
SB-18	7/8/2008	19,000	3,800	590	18	7.0	15	3.0	<0.5	<1.0	<0.8	<1.0	45	67	1.0	2.0	3.0	5.0	2.0	5.0	2.0	15	35	
SB-19	7/8/2008	1,600	650	3.0	8.0	9.0	26	16	<0.5	<1.0	<0.8	<1.0	4.0	4.0	5.0	<1.0	13	<1.0	58	<1.0	2.0	<5.0	6.0	
MW-1	7/8/2008	2,800	120	0.8	<0.5	< 0.5	<0.5	<0.5	< 0.5	<1.0	<0.8	<1.0	<1.0	<1.0	<1.0	1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<5.0	8.0	ND^2
I	ESLs	210	210	46	130	43	10)0*	1,800	3.8	590	360	NE	NE	NE	NE	NE	NE	NE	NE	24	18,000	1,500	1,000**

Abbreviations/notes:

TPHg/JPHd = Total petroleum hydrocarbons as gasoline/diesel by EPA Method 8015 VOCs = Volatile Organic Compounds by EPA Method 8260B MTBE = Methyl tertiary butyl ether cis-1,2-DCE = cis-1,2-Dichloroethene TCE = Trichloroethene TBA = Tertiary butyl alcohol <x = not detected at or above stated laboratory detection limit</pre> - - = Not analyzed ND = Not detected; detection limits vary ¹ Total xylenes ² Metals not detected except barium at 451 ug/L

* ESL is for total xylenes NE = Not established

** ESL for barium

SENSITIVE RECEPTOR AND WELL SURVEY FORMER SIGNAL OIL BULK PLANT (FORMER CHEVRON FACILITY 20-6127) 2301-2311 BLANDING AVENUE ALAMEDA, CALIFORNIA

ID on Map	Sensitive Receptor Type	DWR Well Drillers Report Number	Address	Owner	Well Type	Date Installed	Depth (fbg)	Screened (fbg)	Approximate Distance From Site
	Surface Water	NA	Alameda Canal		NA	NA	NA	NA	20 feet north
1	Well	32164	2307 Clement Avenue	Bob Tennant	Industrial	4/9/1977	80	20-80; 40-80	310 feet sounthwest
2	Well	32163	2307 Clement Avenue	Bob Tennant	Industrial	4/9/1977	71	20-71; 30-71	340 feet southwest
3	School	NA	2226 Pacific Avenue	Alameda Christian School	NA	NA	NA	NA	1775 feet southwest

Notes and Abbreviations

fbg = feet below grade

NA = not applicable

Well locations provided by the California Department of Water Resources (June 2011)

Virit The state Table of the state																	1,3,5-				,		
Here Thema Tature System System <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>Ethyl-</th> <th>m,p-</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>Propyl-</th> <th>Trimethy</th> <th>4-Ethyl-</th> <th></th> <th></th> <th></th> <th></th> <th></th>							Ethyl-	m,p-								Propyl-	Trimethy	4-Ethyl-					
Varpur Well Sample Date (ug/m ¹) (ug/m ¹)			TPHd	TPHg	Benzene	Toluene	benzene	Xylene	Naphthalene	Chloromethane	Bromomethane	Hexane	Cyclohexane	e Heptane	Cumene	benzene	l-benzene	toluene	<i>O</i> ₂	N_2	CO_2	CH_4	He
Support Support <t< th=""><th>Vapor Well</th><th>Sample Date</th><th>$(\mu g/m^{3})$</th><th>(µg/m³)</th><th>(µg/m³)</th><th>(µg/m³)</th><th>(µg/m³)</th><th>(µg/m³)</th><th>$(\mu g/m^3)$</th><th>(µg/m³)</th><th>$(\mu g/m^{3})$</th><th>$(\mu g/m^3)$</th><th>(µg/m³)</th><th>(µg/m³)</th><th>$(\mu g/m^3)$</th><th>$(\mu g/m^3)$</th><th>$(\mu g/m^3)$</th><th>(µg/m³)</th><th>(%)</th><th>(%)</th><th>(%)</th><th>(%)</th><th>(%)</th></t<>	Vapor Well	Sample Date	$(\mu g/m^{3})$	(µg/m ³)	$(\mu g/m^3)$	(µg/m ³)	$(\mu g/m^{3})$	$(\mu g/m^3)$	(µg/m ³)	(µg/m ³)	$(\mu g/m^3)$	$(\mu g/m^3)$	$(\mu g/m^3)$	(µg/m ³)	(%)	(%)	(%)	(%)	(%)				
VP-1 (6) (6) (7)	<u>Soil Vapor Wells</u>																						
10/22/10	VP-1	08/19/08	13,000	1,300,000	<u>300</u>	140	240	540		<160	<75	9,400	12,000	27,000	1,600	2,800	<95	660	17		4.00		< 0.12
ub/29/10 NS <		10/22/09		<88	<3.4	<4.1	<4.7	<4.7		<8.9	<4.2	<3.8	<3.7	<4.4	<5.3	<5.3	<5.3	<5.3	9.4		5.70		< 0.11
11/16/10 NS NS NS NS NS NS NS N		06/29/10	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS
VP2 98/19/8 24.000 1500.000 140 <td></td> <td>11/16/10</td> <td>NS</td>		11/16/10	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS
10/22/09 695 63.7 63.7 63.7 63.7 65.7 <t< td=""><td>VP-2</td><td>08/19/08</td><td>24,000</td><td>1,500,000</td><td><u>140</u></td><td><86</td><td>130</td><td>300</td><td></td><td><190</td><td><89</td><td>5,500</td><td>19,000</td><td>12,000</td><td>900</td><td>1,700</td><td><110</td><td>370</td><td>8.9</td><td></td><td>11.00</td><td></td><td>< 0.11</td></t<>	VP-2	08/19/08	24,000	1,500,000	<u>140</u>	<86	130	300		<190	<89	5,500	19,000	12,000	900	1,700	<110	370	8.9		11.00		< 0.11
06/29/10 - - - - <td></td> <td>10/22/09</td> <td></td> <td><95</td> <td><3.7</td> <td><4.4</td> <td><5.0</td> <td><5.0</td> <td></td> <td><9.6</td> <td><4.5</td> <td><4.1</td> <td><4.0</td> <td><4.8</td> <td><5.7</td> <td><5.7</td> <td><5.7</td> <td><5.7</td> <td>13</td> <td></td> <td>8.00</td> <td></td> <td>< 0.12</td>		10/22/09		<95	<3.7	<4.4	<5.0	<5.0		<9.6	<4.5	<4.1	<4.0	<4.8	<5.7	<5.7	<5.7	<5.7	13		8.00		< 0.12
06/29/10 ¹ - 820 <4.3		06/29/10		<280	<4.3	<5	<5.9	<5.9	<28										16	79	5.10	0.0005	< 0.14
11/16/10 ² - - // 101 10		$06/29/10^{1}$		820	<4.3	<5.0	<5.8	<5.8	<28										16	79	5.10	< 0.00027	< 0.13
VP-3 08/19/08 53,000 4100,000 <700 <480 <700 <7100 4,000 <700 <100 1.7 - 1.100 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <1.01 - <th< td=""><td></td><td>$11/16/10^2$</td><td></td><td><160</td><td><3.8</td><td><4.4</td><td><5.1</td><td><5.1</td><td><25</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>18</td><td>79</td><td>3.10</td><td>< 0.00024</td><td>< 0.12</td></th<>		$11/16/10^2$		<160	<3.8	<4.4	<5.1	<5.1	<25										18	79	3.10	< 0.00024	< 0.12
10/22/99 1,800,000 <130 <150 <180 <180 <- < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < < <	VP-3	08/19/08	53,000E	4,100,000	<700	<830	<960	1,200		<1,800	<850	38,000	47,000	77,000	4,000	5,700	1,200	<1100	1.7		11.00		<0.11
06/29/10 NS <		10/22/09		1,800,000	<130	<150	<180	<180		<330	<160	6,200	6,200	1,800	<200	<200	<200	<200	1.4		8.10		< 0.12
11/16/10 - 340,000 <38 <45 <52 <250 - - - -		06/29/10	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS
VP4 08/19/08 91.0005 20.000.00 110.000 49.00 57.000 70.000 54.000 5.0000 51.0000 51.0000 51.0000 51.0000 51.0000 51.0000 51.0000 51.0000 51.0000 51.0000 50.000 50.000 51.0000 51.0000 51.0000 50.000 51.0000 50.000 51.0000 50.000 50.000 51.0000 50.000 50.000 50.000 50.000 51.0000 50.000		11/16/10		340,000	<38	<45	<52	<52	<250										4.1	87	8.10	0.66	< 0.12
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	VP-4	08/19/08	<u>91,0005</u>	220,000,000	1,100,000	49,000	<u>570,000</u>	70,000		<u>3,900,000</u>	<u>70,000</u>	8,400,000	3,600,000	5,100,000	57,000	84,000	<19,000	37,000	0.55		16.00		<0.13
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		10/22/09		140,000,000	1,100,000	<48,000	650,000	71,000		<100,000	<49,000	7,700,000	3,400,000	4,900,000	64,000	110,000	<62,000	<62,000	0.64		15.00		< 0.13
VP-5 08/19/08 110,0005 29,000,000 28,000 <4,400 <5,000		$10/22/09^{1}$		130.000.000	1.000.000	<46.000	540.000	57.000		<100.000	<47.000	7.300.000	3.200.000	4.600.000	<59.000	92,000	<59.000	<59.000	0.62		14.00		< 0.12
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		06/29/10	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS
VP-5 08/19/08 110,0005 29,000,000 28,000 <44,00 <5,000 < <9,600 <4,500 630,000 430,000 660,000 7,000 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 <5,700 </td <td></td> <td>11/16/10</td> <td></td> <td><u>130,000,000</u></td> <td>830,000</td> <td>30,000</td> <td><u>470,000</u></td> <td>44,000</td> <td><25,000</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>1.1</td> <td>43</td> <td>12.00</td> <td>41</td> <td>0.28</td>		11/16/10		<u>130,000,000</u>	830,000	30,000	<u>470,000</u>	44,000	<25,000										1.1	43	12.00	41	0.28
10/22/09 20,000,000 16,000 <4,800 <5,500 < <10,000 <4,900 370,000 310,000 490,000 12,000 <6,200 <6,200 <1.3 17.00 <0.13 06/29/10 NS	VP-5	08/19/08	110,000S	29,000,000	28,000	<4,400	<5,000	<5,000		<9,600	<4,500	630,000	430,000	660,000	7,000	<5,700	<5,700	<5,700	2.0		15.00		<0.12
06/29/10 NS		10/22/09		20,000,000	16,000	<4,800	<5,500	<5,500		<10,000	<4,900	370,000	310,000	490,000	12,000	15,000	<6,200	<6,200	1.3		17.00		< 0.13
11/16/10 18,000,000 11,000 1600 <600 1,600 <8000		06/29/10	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS
11/16/10 ¹ 18,000,000 12,000 1,500 <1600 1,700 <8000 1.4 82 16.00 0.030 <0.11 VP-6 08/19/08 96,0005 150,000,000 20,000 <10,000		11/16/10		<u>18,000,000</u>	11,000	1,600	<1600	1,600	<8000										1.5	82	16.00	0.030	< 0.11
VP-6 08/19/08 96,000S 150,000,000 20,000 <10,000 <12,000 <12,000 <12,000 <12,000 <12,000 <12,000 <12,000 <12,000 <12,000 <12,000 <12,000 <12,000 <12,000 <12,000 <12,000 <12,000 <12,000 <12,000 <12,000 <12,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <14,000 <10,000 <10,000 <10,000 <10,000		$11/16/10^{1}$		18,000,000	12,000	1,500	<1600	1,700	<8000										1.4	82	16.00	0.030	<0.11
08/19/08 ¹ 22,000 840,000 100 <86	VP-6	08/19/08	<u>96,</u> 000S	<u>150,0</u> 00,000	<u>20</u> ,000	<10,000	<12,000	<12,000		<u>1,20</u> 0,000	<u>25</u> ,000	3,300,000	3,200,000	2,800,000	17,000	<14,000	<14,000	<14,000	3.9		9.80		<0.11
06/29/10 NS <		$08/19/08^{1}$	22.000	840.000	100	<86	130	290		<190	<89	4,400	9,800	12,000	890	1.700	<110	390	9.2		10.00		<0.11
11/16/10 NS		06/29/10	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS
		11/16/10	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS

SOIL VAPOR ANALYTICAL RESULTS FORMER SIGNAL OIL MARINE STORAGE AND DISTRIBUTION FACILITY (CHEVRON FACILITY 20-6127) 2301-2311 BLANDING AVENUE ALAMEDA, CALIFORNIA

																1,3,5-				12211,		
						Ethyl-	<i>m,p</i> -								Propyl-	Trimethy	4-Ethyl-					
		TPHd	TPHg	Benzene	Toluene	benzene	Xylene	Naphthalene	Chloromethane	e Bromomethane	Hexane	Cyclohexan	e Heptane	Cumene	benzene	l-benzene	toluene	<i>O</i> ₂	N_2	CO_2	CH_4	He
Vapor Well	Sample Date	$(\mu g/m^3)$	$(\mu g/m^{3})$	$(\mu g/m^3)$	$(\mu g/m^3)$	$(\mu g/m^{3})$	$(\mu g/m^{3})$	$(\mu g/m^{3})$	$(\mu g/m^{3})$	$(\mu g/m^3)$	(µg/m ³)	$(\mu g/m^{3})$	$(\mu g/m^{3})$	(µg/m ³)	(µg/m ³)	$(\mu g/m^{3})$	(µg/m ³)	(%)	(%)	(%)	(%)	(%)
<u>Sub-Slab Soil Vapo</u>	<u>r Probes</u>																					
VP-7	07/24/09		<95	<3.7	<4.4	<5.0	<5.0		<9.6	<4.5	<4.1	<4.0	<4.8	<5.7	<5.7	<5.7	<5.7	19		0.60		< 0.12
	06/29/10		<240	<3.7	<4.3	<5.0	<5.0	<24										21	78	0.30	< 0.00023	, 0.21
	11/16/10		<260 ³	<4.1	<4.9	<5.6	<5.6	<27										20	79	0.50	< 0.00026	0.54
VP-8	07/24/09		490	<3.5	<4.1	<4.8	<4.8		<9.1	<4.3	<3.9	<3.8	<4.5	<5.4	<5.4	<5.4	<5.4	21		0.56		<0.11
	$07/24/09^{1}$		8,200	7	48	24	100		<9.1	<4.3	<3.9	<3.8	<4.5	<5.4	14	33	79	21		0.56		< 0.11
	06/29/10		310	24	71	5.9	47	<25										20	79	0.61	< 0.00024	0.57
	$06/29/10^{1}$		340	24	70	53	44	<25														
	11/16/10		$<250^{3}$	< <u></u> <3.9	<4.6	<5.2	<5.2	<25										19	79	0.98	< 0.00024	1.10
VP_9	07/24/09		8 800	<38	38	<53	19		<98	<16	<12	<11	<19	< 5.8	< 5.8	< 5.8	<5.8	15		0.14		29.00
VI-9	10/22/09		<90	<3.5	<41	<4.8	<4.8		<9.0	<4 3	<3.9	<3.8	<4.5	<5.0	<5.0	<5.0	<5.0	20		0.14		<0.11
	$\frac{10}{22}$		<230	<3.6	<4.3	<4.9	<5.0	<24										19	80	1.10	<0.00023	<0.11 < <0.11
	11/16/10		$<250^{3}$	<3.9	<4.6	<5.3	<5.3	<26										19	80	1.20	< 0.00024	< < 0.12
VP-10	07/24/09		2 500B	<37	7	52	130		<96	<4 5	<4 1	<4.0	12	<57	12	21	59	17		0.48		16.00
VI-10	10/22/09		<u>2,500D</u> 2 100	16	61	12	<5.2		<10	<4.7	100	45	91	<5.9	<5.9	<59	<59	20		0.40		2 40
	$\frac{10}{22}$		<250	<3.8	<4 5	<5.2	<5.2	<25										19	73	0.43	<0.00024	2.40
	11/16/10		260^3	<4.0	6.3	<5.4	<5.4	<26										18	72	0.42	< 0.00025	5 10.00
VD 11	07/24/00		4 F OD	<2.0	10	<f 0<="" td=""><td>0</td><td></td><td>~10</td><td>< 1 🔽</td><td>-10</td><td><1.2</td><td></td><td></td><td><F 0</td><td></td><td></td><td>16</td><td></td><td>0.20</td><td></td><td>22.00</td></f>	0		~10	< 1 🔽	-10	<1.2			< F 0			16		0.20		22.00
VP-11	07/24/09		450B	<3.9	13	<5.2	8 <5 0		<10	<4.7	<4.3	<4.2	<5.0	<5.9	<5.9	<5.9	<5.9	16 14		0.26		22.00
	10/22/09		<99	< 3.9	<4.6	< 5.2	<0.2		<10	<4.7	<4.3	<4.2	<5.0	<5.9	< 5.9	< 5.9	< 5.9	14 19		4.00		<0.12
	06/29/10		<240 <260	<5.0 <1.0	<4.5 <4.7	<5.1	<5.1	<25										10 18	80	1.90	<0.00024	< 0.12
	11/10/10 $11/16/10^{1}$		$<260^{3}$	<4.0	<4.7 <4.7	<5.4	<5.4 <5.4	<26										18	80	1.70	< 0.00025	<0.12 5 <0.12
VD 12	07/24/00		100B	1 36	-12	<10	<10		<0.2	<13	<20	-2 P	<16	~ 5 5	~ 5 5	~ 5 5	~ 5 5	10		0.73		0.43
V1-12	07/24/09		190D	<0.0	N4.2	~4.9	~4.9		< 9.2	\4. 3	<0.9	< 3.8	\4.0	<5.5 <5.5	<0.0 <5.5	<5.5 <5.5	<0.5 <5.5	19		0.73		0.43
	07/24/09		<u>1,600B</u>	< 3.6	<4.2	<4.9	<4.9		< 9.2	<4.3	<3.9	< 3.8	<4.6	<5.5	<5.5	<5.5	<5.5	19		0.73		0.44
	10/22/09		<95	<3.7	<4.4	< 5.0	< 5.0		<9.6	<4.5	<4.1	<4.0	<4.8	<5.7	<5.7	<5.7	<5.7	18		1.40		<0.12
	06/29/10		<220	<5.5 10.0	\4.1	~ 4.8	\4.0	< <u>2</u> 5										20	80	0.45	<0.00022	×0.11
	11/16/10		<240	<3.8	<4.5	<5.2	<5.2	<25										20	80	0.50	<0.00024	<0.12
VP-13	07/24/09		<u>8,600B</u>	<3.6	200	<5.0	9		<9.4	<4.4	<4.0	<3.9	<4.7	<5.6	<5.6	<5.6	<5.6	15		0.16		26.00
	10/22/09		<95	<3.7	<4.4	<5.0	<5.0		<9.6	<4.5	<4.1	<4.0	<4.8	<5.7	<5.7	<5.7	<5.7	20		1.30		< 0.12
	06/29/10		<240	<3.8	<4.4	<5.1	<5.1	<25										16	82	2.00	< 0.00024	< < 0.12
	11/16/10		450^{3}	<3.9	<4.6	<5.3	<5.3	<26										15	78	2.60	< 0.00024	4.70
SFRWQCB ESLs ^a		29,000	29,000	280	180,000	3,300	58000 ⁴	240	53,000	2,900	NE	NE	NE	NE	NE	NE	NE	NE	NE	NE	NE	NE
SFRWQCB ESLs ^b		1,400	1,400	14	8,800	160	2,900 ⁴	12	2,600	150	NE	NE	NE	NE	NE	NE	NE	NE	NE	NE	NE	NE

SOIL VAPOR ANALYTICAL RESULTS FORMER SIGNAL OIL MARINE STORAGE AND DISTRIBUTION FACILITY (CHEVRON FACILITY 20-6127) 2301-2311 BLANDING AVENUE ALAMEDA, CALIFORNIA

SOIL VAPOR ANALYTICAL RESULTS FORMER SIGNAL OIL MARINE STORAGE AND DISTRIBUTION FACILITY (CHEVRON FACILITY 20-6127) 2301-2311 BLANDING AVENUE ALAMEDA, CALIFORNIA 1,3,5-

					Ethyl-	<i>m,p-</i>								Propyl-	Trimethy	4-Ethyl-					
	TPHd	TPHg	Benzene	Toluene	benzene	Xylene	Naphthalene	Chloromethane	Bromomethane	Hexane	Cyclohexane	Heptane	Cumene	benzene	l-benzene	toluene	O ₂	N_2	CO_2	CH_4	He
Vapor Well	Sample Date (µg/m³)	$(\mu g/m^3)$	$(\mu g/m^{3})$	$(\mu g/m^3)$	(µg/m ³)	$(\mu g/m^3)$	$(\mu g/m^{3})$	$(\mu g/m^{3})$	$(\mu g/m^{3})$	$(\mu g/m^3)$	(µg/m ³)	$(\mu g/m^{3})$	$(\mu g/m^3)$	$(\mu g/m^{3})$	(µg/m ³)	$(\mu g/m^3)$	(%)	(%)	(%)	(%)	(%)

Abbreviations and Notes:

Bold = indicates that measured concentration exceeds the ESL for shallow soil gas under commercial/industrial land use.

<u>Underline</u> = indicates that measured concentration exceeds the ESL for indoor air under commercial/industrial land use adjusted by a factor of 100 to account for attenuation between sub-slab and indoor air. TPHd = Total petroleum hydrocarbons as diesel by EPA Method TO-17

TPHg = Total petroleum hydrocarbons as gasoline by EPA Method TO-3 (8/19/08) or TO-15 GC/MS

Volatile Organic Compounds by EPA Method TO-15

Oxygen (O₂₎, nitrogen (N₂), carbon dioxide (CO₂₎, methane (CH₄) and helium (He) by ASTM Method D-1946

NE = Not established

NS = Not sampled due to the presence of water in vapor well

B = Compound present in laboratory blank greater than reporting limit, background subtraction not per

^a = Environmental Screening Levels for shallow soil gas associated with potential vapor intrusion concerns at commercial/industrial sites (Table E, SFRWQCB, 2008).

^b = Environmental Screening Levels for indoor air under commercial/industrial land use adjusted by a factor of 100 to account for attenuation between sub-slab and indoor air (Table E, SFRWQCB, 2008).

- ¹ = Field duplicate sample
- 2 = TPHg analysis by TO-15 APH
- ³ = Estimated value due to laboratory error
- 4 = ESL is for total xylenes
- < = Not detected at or above stated laboratory reporting limit
- -- = Not analyzed

TABLE 6

INDOOR AND OUTDOOR AIR ANALYTICAL RESULTS FORMER SIGNAL OIL MARINE STORAGE AND DISTRIBUTION FACILITY (CHEVRON FACILITY 20-6127) 2301-2311 BLANDING AVENUE ALAMEDA, CALIFORNIA

		TPHg	Benzene	Toluene	Ethylbenzene	m,p-Xylene	Naphthalene	<i>O</i> ₂	N_2	CO_2	CH_4	He
Vapor Well	Sample Date					(µg/n	n ³)					
IA-1	06/29/10	290	0.52	4.50	0.27	0.97	<4.0					
$11/16/10^2$	220	1.70	7.70	0.61	2.20	<4.1	22	78	0.042	0.00021	< 0.078	
IA-2 06/2 11/1	06/29/10	490	0.57	5.20	2.30	8.3	<4.1					
	$11/16/10^2$	390	0.97	15.00	1.80	5.7	<4.4	22	78	0.048	0.00021	< 0.084
IA-3	07/09/10	110	0.39	1.80	0.27	0.92	<4.3	22	78	0.040	0.00019	< 0.082
	$07/09/10^3$	100	0.41	2.00	0.26	0.91	<4.3					
	$11/16/10^2$	530	4.20	35.00	6.00	23.00	<4.2	22	78	0.046	0.00021	< 0.081
IA-4	06/29/10	490	1.80	16.00	2.10	7.9	<4.0					
	$11/16/10^2$	200	0.77	4.40	0.74	2.5	<4.4	22	78	0.041	0.00020	< 0.084
OA-1	06/29/10	<160	0.24	0.78	0.15	0.48	<4.0					
	$11/16/10^2$	110	0.61	2.10	0.38	1.20	<4.1	22	78	0.043	0.00021	<0.078
SFRWQCB ESLs		14	0.14	88.00	1.60	29 ¹	0.12	NE	NE	NE	NE	NE

Abbreviations and Notes:

Bold = indicates that measured concentration exceeds the ESL for indoor air under commercial/industrial land use.

TPHg = Total petroleum hydrocarbons as gasoline by EPA Method TO-15 GC/MS SIM.

Volatile organic compounds by EPA Method TO-15 GC/MS SIM.

Oxygen (O_2) , nitrogen (N_2) , carbon dioxide (CO_2) , methane (CH_4) and helium (He) by ASTM Method D-1946.

ESLs = Environmental Screening Levels associated with ambient and indoor air at commercial/industrial sites (Table E, SFRWQCB, 2008).

 1 = ESL is for total xylenes.

² = Samples analyzed by Modified TO-15 APH

³ = Field duplicate sample

NE = Not established.

< = Not detected at or above stated laboratory reporting limit.

-- = Not analyzed/not applicable.

APPENDIX A

REGULATORY CORRESPONDENCE

ALAMEDA COUNTY HEALTH CARE SERVICES AGENCY

ALEX BRISCOE, Director



ENVIRONMENTAL HEALTH SERVICES ENVIRONMENTAL PROTECTION 1131 Harbor Bay Parkway, Suite 250 Alameda, CA 94502-6577 (510) 567-6700 FAX (510) 337-9335

May 26, 2011

Mr. Mike Bauer Chevron Environmental Management Company 145 S. State College Blvd. Brea, CA 92821

Ms. Julie Beck Ball Mr. Peter Reinhold Beck 2720 Broderick Street San Francisco, CA 94123

Subject: Case File Review for SLIC Case No. RO0002466 and GeoTracker Global ID T06019744728, Park Street Landing 2301-2337 Blanding Avenue, Alameda, CA 94501

Dear Mr. Bauer and Ms. Ball:

Alameda County Environmental Health (ACEH) staff has reviewed the Spills, Leaks, Investigations, and Cleanups (SLIC) case file for the above referenced site including the recently submitted documents entitled, "Second Soil Vapor, Sub-Slab, and Indoor Air Sampling Report," dated March 30, 2011 and "First Quarter 2011 Groundwater Monitoring and Sampling Report," dated March 18, 2011. Both documents were prepared on Chevron's behalf by Conestoga-Rovers & Associates. The "Second Soil Vapor, Sub-Slab, and Indoor Air Sampling Report," dated March 30, 2011, presents soil vapor, sub-Slab, and indoor air sampling results from November 16, 2010. Total petroleum hydrocarbons as gasoline (TPHg) and benzene were detected in soil vapor samples at concentrations up to 130,000,000 and 830,000 micrograms per cubic meter (μ g/m³), respectively. TPHg was detected in sub-slab vapor samples at concentrations up to 530 and 4.2 μ g/m³, respectively.

The "*Groundwater Monitoring and Sampling Report*," dated March 18, 2011, presents results from groundwater sampling conducted on January 14, 2011. TPHg and benzene were detected in groundwater from downgradient well MW-1RA at concentrations of 790 and 160 micrograms per liter. The concentrations of TPHg and benzene in groundwater exceed the surface water screening levels for estuary habitats (San Francisco Bay Regional Water Quality Control Board Environmental Screening Levels May 2008).

Based on the results of investigations conducted to date, a significant mass of petroleum hydrocarbons remains in the subsurface at this site. Based on sub-slab and soil vapor sampling results to date, the residual petroleum hydrocarbons may not pose a significant risk for vapor intrusion to indoor air for current use of the site; however, there is some uncertainty in the soil vapor, indoor air, and sub-slab results due to significant temporal and spatial variability in the results. Based on the highly elevated concentrations of volatile petroleum hydrocarbons in soil vapor beneath portions of the site, the residual contamination poses a potential risk for future development of the site.

Elevated concentrations of petroleum hydrocarbons are present in groundwater beneath the site including the downgradient wells located nearest to the Alameda Canal. The site represents a chronic source for petroleum hydrocarbons discharging to the adjacent surface water. Based on these considerations, remediation is required for this site. Therefore, we request that you address the following technical comments and submit a Draft Corrective Action Plan.

Responsible Parties RO0002466 May 26, 2011 Page 2

TECHNICAL COMMENTS

- 1. Corrective Action Plan. Based on the highly elevated concentrations of volatile petroleum hydrocarbons in soil vapor beneath portions of the site, the significant mass of petroleum hydrocarbons remaining in the subsurface, and the discharge of groundwater containing elevated concentrations of petroleum hydrocarbons to the Alameda Canal, site cleanup is required. We request that you prepare a Draft Corrective Action Plan (Draft CAP) that meets the provisions of section 2725 of the UST regulations (CCR, Title 23, Chapter 16, section 2600, et seq.) and includes the following minimum information:
 - Proposed cleanup goals and the basis for cleanup goals.
 - Summary of site characterization data.
 - Receptor information including likely future land use scenarios, adjacent land use and sensitive receptors, and potential groundwater receptors.
 - Evaluation of a minimum of three active remedial alternatives including discussion of feasibility, cost effectiveness, estimated time to reach cleanup goals, and limitations for each remedial alternative.
 - Detailed description of proposed remediation including confirmation sampling and monitoring during implementation.
 - Post-remediation monitoring.
 - Schedule for implementation of cleanup.

Public participation is a requirement for the Corrective Action Plan process. Therefore, we request that you submit a Draft CAP for ACEH review. Upon ACEH approval of a Draft CAP, ACEH will notify potentially affected members of the public who live or own property in the surrounding area of the proposed remediation described in the Draft CAP. Public comments on the proposed remediation will be accepted for a 30-day period.

2. Vapor Sample Quality. Helium was detected in several of the sub-slab vapor samples at concentrations up to 10 percent, indicating that there was a leak of ambient air into the samples. The "Second Soil Vapor, Sub-Slab, and Indoor Air Sampling Report," concludes that the vapor sampling results are valid based on low concentrations of hydrocarbon vapor detected and "minor detection of helium." However, the concentration of helium in the sampling shroud during sampling was not reported. Unless the concentration of helium in the shroud is known, it is not possible to know the degree of leakage of ambient air and the validity of the results. Therefore, we do not concur that the samples can be assumed to be valid based on the factors cited. Vapor samples may generally be considered valid if the concentration of helium in the sample is less than 10 percent of the helium concentration in the shroud. A soil vapor sample with 10 percent helium would generally not be considered a valid result. The results for VP-10 and VP-13 are questionable based on the information presented. Please use a more rigorous approach in assessing the validity of future vapor sampling results.

Responsible Parties RO0002466 May 26, 2011 Page 3

- 3. Sub-slab Attenuation Factor. The "Second Soil Vapor, Sub-Slab, and Indoor Air Sampling Report," (Report) includes several statements indicating that the application of a factor of 0.01 for attenuation between the sub-slab and indoor air is overly conservative. We believe this statement cannot be supported by the data presented. The repeated statements that a sub-slab attenuation factor of 0.01 is overly conservative for the site appears to be based on a comparison of indoor air sampling results to sub-slab sampling results. Table 3 of the Report uses indoor air results to predict sub-slab soil vapor results and then compares the predicted value to actual sub-slab results. Since the actual sub-slab results are less than the predicted values in Table 3, the Report concludes that a sub-slab attenuation factor of 0.01 is overly conservative. However, most of the indoor air concentrations exceed both the outdoor air concentrations and sub-slab concentrations. We concur with the conclusion stated elsewhere in the Report that the indoor air concentrations may be affected by sources within the building. Given that the indoor air concentrations to estimate a sub-slab to indoor air attenuation factor.
- 4. **Groundwater Monitoring.** We concur with the proposal in the "First Quarter 2011 Groundwater Monitoring Report," to continue quarterly groundwater monitoring. Please present the results from quarterly groundwater monitoring in the reports requested below.

TECHNICAL REPORT REQUEST

Please submit technical reports to Alameda County Environmental Health (Attention: Jerry Wickham), according to the following schedule:

- June 30, 2011 Second Quarter 2011 Groundwater Monitoring Report
- July 21, 2011 Draft Corrective Action Plan
- September 30, 2011 Third Quarter 2011 Groundwater Monitoring Report

If you have any questions, please call me at (510) 567-6791 or send me an electronic mail message at jerry.wickham@acgov.org.

Sincerely,

Jerry Wickham, California PG 3766, CEG 1177, and CHG 297 Senior Hazardous Materials Specialist

Attachment: Responsible Party(ies) Legal Requirements/Obligations

Enclosure: ACEH Electronic Report Upload (ftp) Instructions

Responsible Parties RO0002466 May 26, 2011 Page 4

cc: Mr. Brian Silva, Conestoga-Rovers & Associates, 10969 Trade Center Drive, Suite 107, Rancho Cordova, CA 95670 (Sent via E-mail to: <u>bsilva@craworld.com</u>)

Mr. Monroe Wingate, C/o Alan Wingate, 18360 Carriger Road, Sonoma, CA 95476

Donna Drogos, ACEH (Sent via E-mail to: <u>donna.drogos@acgov.org</u>) Jerry Wickham, ACEH (Sent via E-mail to: <u>jerry.wickham@acgov.org</u>)

GeoTracker, e-File

Attachment 1

Responsible Party(ies) Legal Requirements / Obligations

REPORT REQUESTS

These reports are being requested pursuant to California Health and Safety Code Section 25296.10. 23 CCR Sections 2652 through 2654, and 2721 through 2728 outline the responsibilities of a responsible party in response to an unauthorized release from a petroleum UST system, and require your compliance with this request.

ELECTRONIC SUBMITTAL OF REPORTS

ACEH's Environmental Cleanup Oversight Programs (LOP and SLIC) require submission of reports in electronic form. The electronic copy replaces paper copies and is expected to be used for all public information requests, regulatory review, and compliance/enforcement activities. Instructions for submission of electronic documents to the Alameda County Environmental Cleanup Oversight Program FTP site are provided on the attached "Electronic Report Upload Instructions." Submission of reports to the Alameda County FTP site is an addition to existing requirements for electronic submittal of information to the State Water Resources Control Board (SWRCB) GeoTracker website. In September 2004, the SWRCB adopted regulations that require electronic submittal of information for all groundwater cleanup programs. For several years, responsible parties for cleanup of leaks from underground storage tanks (USTs) have been required to submit groundwater analytical data, surveyed locations of monitoring wells, and other data to the GeoTracker database over the Internet. Beginning July 1, 2005, these same reporting requirements were added to Spills, Leaks, Investigations, and Cleanup (SLIC) sites. Beginning July 1, 2005, electronic submittal of a complete copy of all reports for all sites is required in GeoTracker (in PDF format). Please visit SWRCB website information on these requirements the for more (http://www.waterboards.ca.gov/water_issues/programs/ust/electronic_submittal/).

PERJURY STATEMENT

All work plans, technical reports, or technical documents submitted to ACEH must be accompanied by a cover letter from the responsible party that states, at a minimum, the following: "I declare, under penalty of perjury, that the information and/or recommendations contained in the attached document or report is true and correct to the best of my knowledge." This letter must be signed by an officer or legally authorized representative of your company. Please include a cover letter satisfying these requirements with all future reports and technical documents submitted for this fuel leak case.

PROFESSIONAL CERTIFICATION & CONCLUSIONS/RECOMMENDATIONS

The California Business and Professions Code (Sections 6735, 6835, and 7835.1) requires that work plans and technical or implementation reports containing geologic or engineering evaluations and/or judgments be performed under the direction of an appropriately registered or certified professional. For your submittal to be considered a valid technical report, you are to present site specific data, data interpretations, and recommendations prepared by an appropriately licensed professional and include the professional registration stamp, signature, and statement of professional certification. Please ensure all that all technical reports submitted for this fuel leak case meet this requirement.

UNDERGROUND STORAGE TANK CLEANUP FUND

Please note that delays in investigation, later reports, or enforcement actions may result in your becoming ineligible to receive grant money from the state's Underground Storage Tank Cleanup Fund (Senate Bill 2004) to reimburse you for the cost of cleanup.

AGENCY OVERSIGHT

If it appears as though significant delays are occurring or reports are not submitted as requested, we will consider referring your case to the Regional Board or other appropriate agency, including the County District Attorney, for possible enforcement actions. California Health and Safety Code, Section 25299.76 authorizes enforcement including administrative action or monetary penalties of up to \$10,000 per day for each day of violation.

Alamada County Environmental Cleanus	REVISION DATE: July 20, 2010		
Alameda County Environmental Cleanup Oversight Programs	ISSUE DATE: July 5, 2005		
(LOP and SLIC)	PREVIOUS REVISIONS: October 31, 2005; December 16, 2005; March 27, 2009; July 8, 2010		
SECTION: Miscellaneous Administrative Topics & Procedures	SUBJECT: Electronic Report Upload (ftp) Instructions		

The Alameda County Environmental Cleanup Oversight Programs (LOP and SLIC) require submission of all reports in electronic form to the county's ftp site. Paper copies of reports will no longer be accepted. The electronic copy replaces the paper copy and will be used for all public information requests, regulatory review, and compliance/enforcement activities.

REQUIREMENTS

- Please <u>do not</u> submit reports as attachments to electronic mail.
- Entire report including cover letter must be submitted to the ftp site as a single portable document format (PDF) with no password protection.
- It is preferable that reports be converted to PDF format from their original format, (e.g., Microsoft Word) rather than scanned.
- Signature pages and perjury statements must be included and have either original or electronic signature.
- <u>Do not</u> password protect the document. Once indexed and inserted into the correct electronic case file, the document will be secured in compliance with the County's current security standards and a password. Documents with password protection <u>will not</u> be accepted.
- Each page in the PDF document should be rotated in the direction that will make it easiest to read on a computer monitor.
- Reports must be named and saved using the following naming convention:

RO#_Report Name_Year-Month-Date (e.g., RO#5555_WorkPlan_2005-06-14)

Submission Instructions

- 1) Obtain User Name and Password
 - a) Contact the Alameda County Environmental Health Department to obtain a User Name and Password to upload files to the ftp site.
 - i) Send an e-mail to <u>deh.loptoxic@acgov.org</u>
 - b) In the subject line of your request, be sure to include "ftp PASSWORD REQUEST" and in the body of your request, include the Contact Information, Site Addresses, and the Case Numbers (RO# available in Geotracker) you will be posting for.
- 2) Upload Files to the ftp Site
 - a) Using Internet Explorer (IE4+), go to <u>ftp://alcoftp1.acgov.org</u>
 - (i) Note: Netscape, Safari, and Firefox browsers will not open the FTP site as they are NOT being supported at this time.
 - b) Click on Page located on the Command bar on upper right side of window, and then scroll down to Open FTP Site in Windows Explorer.
 - c) Enter your User Name and Password. (Note: Both are Case Sensitive.)
 - d) Open "My Computer" on your computer and navigate to the file(s) you wish to upload to the ftp site.
 - e) With both "My Computer" and the ftp site open in separate windows, drag and drop the file(s) from "My Computer" to the ftp window.
- 3) Send E-mail Notifications to the Environmental Cleanup Oversight Programs
 - a) Send email to <u>deh.loptoxic@acgov.org</u> notify us that you have placed a report on our ftp site.
 - b) Copy your Caseworker on the e-mail. Your Caseworker's e-mail address is the entire first name then a period and entire last name @acgov.org. (e.g., firstname.lastname@acgov.org)
 - c) The subject line of the e-mail must start with the RO# followed by **Report Upload**. (e.g., Subject: RO1234 Report Upload) If site is a new case without an RO#, use the street address instead.
 - d) If your document meets the above requirements and you follow the submission instructions, you will receive a notification by email indicating that your document was successfully uploaded to the ftp site.

APPENDIX B

PREVIOUS ENVIRONMENTAL INVESTIGATION

PREVIOUS ENVIRONMENTAL INVESTIGATION FORMER SIGNAL OIL MARINE STORAGE AND DISTRIBUTION FACILITY 20-6127 (CHEVRON 20-6127)

Site History

A Sanborn map dated 1897 showed the site as occupied by several residential structures and outbuildings; the southeast portion of the site was shown as occupied by a laundry facility and a blacksmith. From at least 1930 until approximately 1961, the northwestern portion of the site was occupied by a petroleum bulk plant operated by Signal Oil & Gas Company. Former bulk plant facilities consisted of one large and seven smaller gasoline aboveground storage tanks (ASTs) within concrete secondary containment, underground piping, an office building, a loading rack, and a small structure containing gasoline pumps (Figure 2). The northeast portion of the facility was shown as occupied by a structure identified as an auto garage and also used for paint storage on Sanborn maps dated between 1932 and 1950. A rail spur was shown to service the facilities on Blanding Avenue. The central portion of the site was shown as occupied by two structures identified as wholesale tires and a can warehouse. An additional larger structure was shown in the central portion of the site that was identified as vacant on the 1948 Sanborn map and as a ladder factory on the 1950 Sanborn map. Several structures appeared to be present in the southeast portion of the site in the 1939 aerial photograph. However, only one or two small sheds were shown in this area on the 1948 and 1950 Sanborn maps. In the 1958 aerial photograph, the ladder factory structure no longer appeared present and the southeast portion of the site appeared vacant and used for parking. Between 1957 and 1963, the buildings at the site were reportedly removed; it is assumed that the ASTs and piping were also removed at this time. In the 1965 aerial photograph, all the bulk plant facilities appear to have been removed and the majority of the site appears occupied by a construction materials yard with several small structures. Several additional structures also appear present in the southeast portion of the site. From 1973 to 1983, the northwestern portion of the site reportedly was used as a construction yard and for boat repair activities; and the southeastern portion was occupied by a restaurant, paved parking area, and a possible automobile sales lot. In 1987, the site was redeveloped with the current configuration.

1995 Soil and Groundwater Investigation

In February 1995, Geomatrix Consultants, Inc. (Geomatrix) advanced eight soil borings (SB-1 through SB-8) to approximately 10 feet below grade (fbg) in the northwestern portion of the site to evaluate if previous site uses had impacted soil and groundwater quality. Groundwater was not encountered in the borings. Two to three soil samples were collected at various depths from each boring for laboratory analysis. Nineteen samples were analyzed for total petroleum hydrocarbons as gasoline (TPHg) and diesel (TPHd); and benzene, toluene, ethylbenzene, and xylenes (BTEX). TPHg was detected in six of the samples at concentrations ranging from 4.0 to 2,000 milligrams per kilogram (mg/kg). TPHd was detected in the majority of the samples at concentrations ranging from 10 to 250 mg/kg. BTEX were also detected in several of the samples (benzene up to 3.7 mg/kg). The highest concentrations of petroleum hydrocarbons generally were detected in borings SB-2 and SB-4 located in the vicinity of the former ASTs and

gasoline pump, respectively, between 4 and 7 fbg. One sample from each boring (depths ranging from 0.5 to 3 fbg) was also analyzed for CAM 17 metals. The detected metals concentrations generally appeared to be within the range of natural background levels with the exception of slightly elevated arsenic in a few samples. Arsenic was detected in the samples collected at 1 fbg from borings SB-3, SB-4, and SB-6 at 68 mg/kg, 46 mg/kg, and 130 mg/kg, respectively. As a result, deeper samples collected from borings SB-3 (6.5 fbg) and SB-6 (8 fbg) were also analyzed for arsenic; arsenic was not detected in the sample collected from SB-3, but was detected at 2.5 mg/kg in the sample collected from SB-6. Based on these results, the soil impacted with arsenic appeared to be of limited vertical extent. Three soil samples (SB-4-7', SB-5-6', and SB-8-7') were also analyzed for VOCs, which were not detected. Based on the soil analytical results, a shallow groundwater survey was recommended to evaluate if groundwater had been impacted by petroleum hydrocarbons.

In April 1995, Geomatrix collected grab-groundwater samples from 10 shallow borings (GWS-7 through GWS-16) drilled to depths of 15 to 21.5 fbg at the site. Borings GWS-7 through GWS-12 were located in the northeastern portion of the site adjacent to Alameda Canal to evaluate if impacted groundwater was flowing toward the canal; based on an assumed groundwater flow direction toward the canal. Borings GWS-13 through GWS-15 were located on the southwest and northwest property boundaries in the assumed upgradient and perimeter crossgradient directions to evaluate the quality of groundwater coming onto the site. Boring GWS-16 was located to the northeast of the former ASTs and was drilled approximately 6 feet deeper than the remaining borings to evaluate deeper groundwater quality. The groundwater samples were analyzed for TPHg, BTEX, and TPHd; the samples were filtered by the laboratory to remove turbidity and a silica-gel cleanup was performed to remove non-petroleum organic matter prior to the TPHd analysis. TPHg was detected in the samples collected from borings GWS-8 through GWS-11 and GWS-16 at concentrations ranging from 70 (GWS-16) to 22,000 micrograms per liter (μ g/L) (GWS-9). TPHd was detected in the samples collected from borings GWS-8 through GWS-11 at concentrations ranging from 60 (GWS-8) to 1,200 µg/L (GWS-9). Benzene was detected in the samples collected from borings GWS-8 through GWS-10 and GWS-16 at concentrations of 36 µg/L, 6,200 µg/L, and 880 µg/L, respectively. Toluene, ethylbenzene, and xylenes (up to 1,200 μ g/L) were also detected in several of the samples. The maximum concentrations were detected in boring GWS-9 located downgradient of the gasoline pump and loading rack. Petroleum hydrocarbons were not detected in the upgradient borings GWS-13 through GWS-15. The deeper sample (GWS-16) contained only low to trace hydrocarbon concentrations.

A black granular material was encountered in boring GWS-7 in the northern corner of the site from approximately 2.5 to 6 fbg. This material appeared similar to a small pile of black granular material observed on the northwestern property boundary that appeared to have originated from the adjacent property (a metal fabrication company). A sample of this material was collected and analyzed for TPHd, VOCs, semi-VOCs, and CAM 17 metals. An elevated concentration of copper (1,700 mg/kg) was detected in the sample. The detected concentration did not exceed the Total Threshold Limit Concentration (TTLC) of 2,500 mg/kg, which is the concentration above which a waste may be considered hazardous in California. The sample was also analyzed for soluble copper using the Waste Extraction Test (WET) method; which

was detected at 0.04 milligrams per liter (mg/L). The detected soluble lead concentration did not exceed the Soluble Threshold Limit Concentration (STLC) of 25 mg/L, which is also the concentration above which a waste may be considered hazardous in California. Details of this investigation were presented in the report titled *Soil Investigation and Shallow Groundwater Survey, Northwestern Portion of the Park Street Landing Site,* prepared by Geomatrix and dated September 1995.

1998 RBCA Tier 1 Evaluation

In July 1998, RRM, Inc. (RRM) performed a Tier 1 Risk-Based Corrective Action (RBCA) assessment to evaluate the potential health risks posed by residual petroleum hydrocarbons in soil and groundwater at the site. Based on the results, RRM recommended the collection of site-specific data to complete a Tier 2 RBCA evaluation; the identification of the beneficial uses of groundwater beneath the site; an evaluation of background water quality in Alameda Canal; and to provide evidence that biodegradation was reducing hydrocarbon concentrations. Details of this investigation were presented in the report entitled *Risk-Based Corrective Action (RBCA) Tier 1 Evaluation, Park Street Landing Site*, prepared by RRM and dated July 24, 1998.

1998 Soil and Groundwater Investigation

In October 1998, RRM performed an additional soil and groundwater investigation at the site. The purpose of the investigation was to

1) collect site-specific data to complete a Tier 2 RBCA evaluation; 2) identify the beneficial uses of groundwater beneath the site; 3) evaluate the background water quality in Alameda Canal; and 4) evaluate whether biodegradation of petroleum hydrocarbons was occurring beneath the site. Four additional borings (SB-9 through SB-12) were advanced to depths of 15 to 18 fbg during the investigation. A total of eight soil samples were collected at various depths from the borings and analyzed for TPHg, TPHd, BTEX, and methyl tertiary butyl ether (MTBE). TPHg was detected in the soil samples collected at 5 and 13 fbg from boring SB-9 (130 and 900 mg/kg, respectively); and in the sample collected at 6 fbg from boring SB-11 (140 mg/kg). TPHd was detected in the soil samples collected at 5, 13, and 15 fbg from boring SB-9 (3,300 mg/kg, 1,300 mg/kg, and 1.2 mg/kg, respectively); in the sample collected at 5.5 fbg from boring SB-10 (130 mg/kg); and in the sample collected at 6 fbg from boring SB-11 (60 mg/kg). BTEX (up to 3.3 mg/kg) were detected in the soil samples collected from borings SB-9 and SB-11; MTBE (using EPA Method 8020) was only detected in the sample collected at 13 fbg from boring SB-9 (12 mg/kg). Following the initial TPHd analysis, two rounds of silica gel cleanup followed by TPHd analysis were performed on the soil samples from boring SB-9. The detected TPHd concentrations were reduced after each round, indicating that biodegradation was occurring, and natural organic matter was present in the subsurface.

Grab-groundwater samples were collected from each boring and analyzed for TPHg, TPHd, BTEX, and MTBE. TPHg was only detected in the samples collected from borings SB-9 (14,000 μ g/L) and SB-11 (310 μ g/L). TPHd was detected in the samples collected from borings SB-9 (83,000 μ g/L), SB-10 (97 μ g/L), and SB-11 (270 μ g/L). Benzene and MTBE (using

EPA Method 8020) were only detected in the sample collected from boring SB-9 (1,400 and 260 μ g/L, respectively); the sample was re-analyzed for MTBE using EPA Method 8260, and MTBE was not detected. Toluene, ethylbenzene, and xylenes (up to 630 μ g/L) were detected in the samples collected from borings SB-9 and SB-11. As with the soil samples, a silica-gel cleanup reduced the detected TPHd concentrations. Based on the depth to water in the borings, and the elevation of the borings, the groundwater flow direction was calculated to be northerly. Based on natural biodegradation indicator parameters in groundwater (dissolved oxygen, oxidation-reduction potential, nitrate, and sulfate), it appeared that petroleum hydrocarbons were being degraded both aerobically and anaerobically; although it appeared that anaerobic processes dominated.

Three grab-water samples (CS-1 through CS-3) were collected from Alameda Canal (Figure 2) and analyzed for TPHg, TPHd, BTEX, and MTBE; which were not detected. Water level measurements were collected from the Alameda Canal and the four temporary wells placed in borings SB-9 through SB-12 to evaluate potential tidal influence on groundwater beneath the site. The fluctuations in borings SB-10 through SB-12 were minimal indicating that groundwater was tidally influenced to a limited degree in these areas. A more significant fluctuation was observed in SB-9; suggesting that groundwater in this area was tidally influenced, and tidal fluctuations would tend to stabilize the petroleum hydrocarbon plume in this area. Two concrete sea walls separated shallow groundwater beneath the site from canal water; likely causing the limited tidal influence. Based on the site data, relevant beneficial uses, and associated water quality parameters, the most applicable beneficial use of groundwater beneath the site was determined to be freshwater replenishment to surface water.

A well survey was performed for a ¹/₂-mile radius around the site. Nine wells were identified within the search radius (one recovery well, one irrigation well, five extraction wells, and two industrial wells). All the wells were either located up-gradient of the site or across the Alameda Canal. Based on the results of the Tier 2 RBCA evaluation, soil and groundwater petroleum hydrocarbon concentrations at the site did not exceed the site-specific target levels (SSTLs). Details of this investigation were presented in the report entitled *Soil and Groundwater Investigation Results, Former Signal Oil Marine Terminal*, prepared by RRM and dated May 7, 1999.

2000 Monitoring Well Installation

In December 2000 Gettler-Ryan Inc., under the supervision of Delta Environmental Consultants, Inc. (Delta), installed one groundwater monitoring well (MW-1) along the northeastern portion of the site adjacent to the Alameda Canal. Soil samples were collected at depths of 5, 10, and 15 fbg from the well boring and analyzed for TPHg, TPHd, BTEX, and MTBE. TPHg was only detected in the sample collected at 10 fbg (320 mg/kg). TPHd was only detected in the samples collected at 5 and 10 fbg (30 and 160 mg/kg, respectively). Low concentrations of BTEX were detected in all the samples; MTBE was not detected in any of the samples. The initial groundwater sample collected from the well contained TPHg, TPHd, and benzene at $5,210 \mu g/L$, $1,100 \mu g/L$, and $868 \mu g/L$, respectively. Details of this investigation were presented

in the report entitled *Monitoring Well Installation Report*, prepared by Delta and dated April 10, 2001.

2004 Soil Investigation

In January 2004, Cambria Environmental Technology, Inc. (Cambria) collected three surface soil samples (S1, S2, and S3) from the bank above the western shore of the Alameda Canal. Sample S2 was collected directly down-slope of well MW-1 near a water seep observed on the slope above the canal. Samples S1 and S3 were collected approximately 70 feet east and 90 feet north of well MW-1, respectively, to evaluate background concentrations. The three samples were analyzed for TPHg, TPHd, BTEX, and MTBE. TPHg, BTEX, and MTBE were not detected in any of the samples. TPHd was detected in samples S1, S2, and S3 at 14 mg/kg, 220 mg/kg, and 220 mg/kg, respectively. The laboratory chromatographs indicated that the hydrocarbon pattern observed in these soil samples was not typical of diesel fuel. Therefore, it was concluded the TPHd detections may have represented either highly-degraded diesel fuel from various historical onsite and nearby operations, or residual organic material of unknown origin present in local fill material. Details of this investigation were presented in the report entitled *Soil Sampling Report*, prepared by Cambria and dated February 18, 2004.

Based on generally decreasing petroleum hydrocarbon concentrations in well MW-1 observed during quarterly monitoring, Cambria submitted a case closure request to ACEH dated January 10, 2006. In response to this request, and in a letter dated October 17, 2007, the ACEH requested the collection of additional data to substantiate the conclusion that petroleum hydrocarbons were not migrating and discharging into Alameda Canal. In addition, the potential for vapor intrusion was to be evaluated. Therefore, CRA prepared and submitted *Soil Boring and Vapor Point Installation Work Plan*, dated January 10, 2008. In a letter dated January 30, 2008, the ACEH approved the work plan, with several provisions.

2008 Site Investigation

In July 2008, CRA advanced six soil borings (SB-13 through SB-15 and SB-17 through SB-19) to a maximum depth of 16 fbg, and installed and sampled six permanent soil vapor wells (VP-1 through VP-6) to depths of 4.5 to 6 fbg. Soil boring SB-16 was cleared to 3 fbg but could not be completed due to refusal encountered at three locations (16A, B, and C). Soil boring SB-16 was cleared to 3 fbg but could not be completed due to refusal encountered at three locations (16A, B, and C).

Soil boring SB-16 was cleared to 3 fbg but could not be completed due to refusal encountered at three locations (16A, B, and C).

Soil analytical data indicated that the majority of TPHd and TPHg concentrations in soil are generally located in the area of and downgradient of the former ASTs. The highest concentrations were detected in boring VP-4 at 5 fbg. Relatively low concentrations of TPHd and TPHg were detected in the perimeter borings. Low concentrations of petroleum-related VOCs were also detected in the majority of the soil samples. The BTEX and VOC concentrations generally did not exceed the ESLs, with the exception of a few samples. Concentrations generally appeared to attenuate or were significantly reduced at 10 fbg. Generally, concentrations of metals were consistent with background levels and only exceeded

the ESLs in a few of the samples. Metals in shallow soil across the northwest portion of the site do not appear to be a result of former bulk plant operations. The metals do not appear to have impacted groundwater as only barium was detected in well MW-1.

The highest concentrations of hydrocarbons in groundwater were generally located downgradient of the former ASTs. TPHd, TPHg, and benzene were detected in downgradient boring SB-18 at 19,000 μ g/L, 3,800 μ g/L, and 590 μ g/L, respectively; but only at 1,600 μ g/L, 650 μ g/L, and 3 μ g/L, respectively, in boring SB-19 adjacent to the former large AST. Only relatively low concentrations of TPHd (up to 750 μ g/L) were detected in perimeter borings SB-13, SB-14, and SB-15; and as evidenced by the work performed by RRM, some or most of the detected TPHd may be due to natural organic matter. The extent of the impacted groundwater is well-defined by borings GWS-7, GWS-12 through GWS-15, SB-10 (following silica gel cleanup), and SB-12. Chlorinated solvents were not detected in any of the soil samples collected, and generally were not detected in the groundwater samples with the exception of low concentrations of TCE, cis-1,2-DCE, and vinyl chloride in the sample collected from boring SB-15 in the northeast corner of the site.

The highest hydrocarbon concentrations in soil gas were detected in vapor wells VP-4, VP-5, and VP-6 located in the area of the former ASTs. Significantly lower concentrations were detected in vapor wells VP-1 and VP-2 located downgradient of VP-4. Chlorinated solvents were not detected in the soil vapor samples. Additional details of this investigation are presented in CRA's report entitled *Site Investigation Report*, dated October 2008.

2009 Monitoring Well Installation and Sub-Slab Vapor Sampling

In June 2009, CRA installed monitoring wells MW-2 through MW-5 to total depths of 16 to 20.5 fbg in order to further evaluate groundwater quality beneath the site. The new monitoring wells were installed within the former ASTs (MW-3), and north (MW-5), south (MW-2), and east (MW-4) of the former ASTs. Soil analytical data indicated that the majority of TPHd and TPHg concentrations in soil are located north to south through the former ASTs and generally decreases with depth. The highest TPHd concentration detected was from well boring MW-3 at 4 fbg at a concentration of 610 mg/kg. The highest TPHg concentration detected was from well boring MW-2 at 4.5 fbg at 1,100 mg/kg. No petroleum hydrocarbons were detected in perimeter well boring MW-4. No grab-groundwater samples were collected.

CRA also installed sub-slab vapor points beneath the two western buildings at the site in order to further evaluate potential vapor intrusion beneath the buildings. Two sub-slab vapor points (VP-7 and VP-8) were installed inside 2317 Blanding Avenue and five sub-slab vapor points (VP-9 through VP-13) were installed inside 2307 Blanding Avenue. The highest hydrocarbon concentrations in soil gas were detected in vapor points VP-9 and VP-13, located west-southwest of the former ASTs. Lower concentrations were detected in vapor points VP-8, and VP-10 through VP-12. All detected concentrations were below the shallow soil gas ESL of 29,000 micrograms per cubic meter (μ g/m³). Target chlorinated solvents were not detected in the soil vapor samples. Additional details of this investigation are presented in CRA's *Well Installation and Sub-Slab Vapor Sampling Report*, dated September 8, 2009.

2009 Vapor Sampling

In October 2009, CRA re-install and re-sample sub-slab vapor points VP-9 through VP-13 due to ambient air leaks detected during the initial sampling and to further evaluate the elevated soil vapor concentrations detected in vapor wells VP-1 through VP-6. The results of the re-sampling of the vapor wells VP-1 through VP-5 located outside of the buildings were consistent with previous results for vapor wells VP-3 through VP-5. However, results of the re-sampling of vapor wells VP-1 and VP-2 indicated no TPHg or benzene vapor concentrations at each of these locations, which is not consistent with the initial sample results from August 2008. Additional details of this investigation are presented in CRA's *Vapor Sampling Report*, dated December 2, 2009.

2010 Well Installation

In August 2010, CRA replaced well MW-1 with a more discretely screened well, MW-1RB, and installed wells MW-1RA and MW-6 to depths between 13 to 20 fbg to further evaluate shallow groundwater near Alameda Canal. Well MW-1RA and MW-1RB are located in the vicinity of former well MW-1 and MW-6 is located downgradient of well MW-5. Soil analytical data indicated that minor hydrocarbon impact to soil remains in the vicinity of MW-1 and generally decreases with depth. The highest TPHd and TPHg concentrations detected were from well boring MW-1RA at 10 fbg at a concentration of 260 mg/kg and at 13.5 fbg at 490 mg/kg, respectively. Only trace concentrations of hydrocarbons were detected in well boring MW-6. No grab-groundwater were collected from the well boring as the wells will be incorporated into the site's monitoring and sampling program. Additional details of this investigation are presented in CRA's *Well Installation Report*, dated September 29, 2010.

APPENDIX C

BORING LOGS





PROJECT: PARK STRE	ET LANDING	Log of Bo	ring No. SB3
Alameda, Ca		ELEVATION AND DATUM	
BORING CONTRACTOR	Precision Sampling	DATE STARTED: 2/17/95	DATE FINISHED: 2/17/95
DRILLING CONTRACTOR.		TOTAL DEPTH: 10 feet bgs	MEASURING POINT: Ground surface
DRILLING METHOD: Direc		DEPTH TO FIRST	COMPL. 24 HRS.
DRILLING EQUIPMENT: X		LOGGED BY:	
SAMPLING METHOD: ENV		RESPONSIBLE PROFES	SIONAL: REG. NO. BG 5713
HAMMER WEIGHT:		A. L. Spencer	
PTH Beading (1) PTH PTH PTH PTH PTH PTH PTH PTH PTH PTH	DESCRIFT NAME (USCS Symbol): color, moist, % by wt., plast., density	VIN , structure, cementation, react. w/HCI, geo. inter.	REMARKS
PIDI PIDI PIDI	Surface Elevation	on:	
	Asphalt	~	-
SB3- 1.0 7	CLAYEY SAND with GRAVEL (SC Verv dark gray (10YR 3/1); dry; 40	% fine to medium sand;	-
' S83- 1.5 36	40% fine to coarse angular gravel;	20% medium plasticity	د. •
	tines; loose		+
			-
3 - //			-
			· · ···
	SANDY I FAN CLAY (CL)		
	Dark greenish gray (5BG 4/1); mo	ist; 60 -65% fines; 35-40%]
5-	fine sand; medium plasticity; lifti		
6 - _{SB3-}			-
SB3- 338			
7 - 7.0			
			-
8-			
	Manual with dark gray (5X 4/1)		-
9 - _{SB3-}			
SB3- 100 19			4 -
10 - 10.0	Bottom of boring at 10 feet bgs		
			-
			-
			B-1 (11/92
298.00 1	Geomatrix Consultants	Project No. 2	2436.02 Figure

BORING LOCATION:	, ounorme		Log of Boring No. SB4			
		ELEVATION AND DATUM: Ground surface				
	OB: Precision Sampling	DATE STARTED: 2/17/95	DATE FINISHED: 2/17/95			
		TOTAL DEPTH: 10 feet bos	MEASURING POINT: Ground surface			
DRILLING METHOD:		DEPTH TO FIRST	COMPL. 24 HRS.			
DRILLING EQUIPMEN	T: XD 1	LOGGED BY:				
SAMPLING METHOD:	Enviro Core System	RESPONSIBLE PROFESS	IONAL: REG. NO.			
HAMMER WEIGHT: _	DROP:	A. L. Spencer	; HG 5713			
SAMPLES E B B B	문 DESC 행 윤 NAME (USCS Symbol): color, moist, % by wt., plast.,	RIPTION density, structure, cementation, react, w/HCI, geo, inter.	REMARKS			
(fet Samp Samp Fool Fool	Surface E	levation:	<u> </u>			
	Asphalt					
$1 - \frac{584}{1.5}$ $2 - \frac{1.5}{2}$ $2 - \frac{1.5}{1.5}$ $2 - \frac{1.5}{1.5}$ $3 - \frac{1.5}{1.5}$ $4 - \frac{1.5}{1.5}$ $5 - \frac{1.5}{5}$ $584 - \frac{1.5}{5}$ $584 - \frac{1.5}{5}$ $8 - \frac{1.5}{5}$ $8 - \frac{1.5}{5}$ $8 - \frac{1.5}{5}$ $10 - \frac{11.5}{10.0}$ $- \frac{11}{10.0}$	 Very dark gray (104H 3/1) to dry; 40% fine to coarse sand; gravel; 20% medium plasticity SANDY LEAN CLAY (CL) Dark greenish gray (5BG 4/1) fine sand; medium plasticity f 726 1247 Black mottling 270 111 Bottom of boring at 10 feet b 	40% fine to coarse angular fines; loose y; moist; 60-65% fines; 35-40% ines; firm				
12 - - 13 -			- - - -			
		Project No. 24	136.02 Figure			


PROJ	ECT: PA	ARK S amed	TREE a. Cal	ET LANDIN ifornia	G			Log	of Bor	ring No	o. SB6
BORIN		TION:						ELEVATION A Ground surfa	ND DATUM: Ice		
DRILL			TOR: F	Precision Sa	ampling			DATE STARTE 2/17/95	:D:	DATE FIN 2/17/95	ISHED:
DRILL	ING MET	HOD:	Direc	t push				TOTAL DEPTH 10 feet bgs	l:	Ground	NG POINT: surface
DBILL		JIPMEN		D 1				DEPTH TO WATER	FIRST		24 HRS.
SAME		THOD	: Env	iro Core Sy	stem			LOGGED BY: T. F. Wood			
HAM	AER WEI	GHT:			DROP:			RESPONSIBL A. L. Spence	E PROFESS er	IONAL:	REG. NO. RG 5713
PTH iet)	SAMP 용 용	LES	leading pm)	NAME (USCS	; Symbol): color, moist, %	DESCRIPTION 6 by wt., plast., density, st	VI tructure, cen	nentation, react. w/HC	X, geo. inter.	F	REMARKS
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				Aspha	t					4	
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PROJEC		ARK S	STREE	ET LANDING ifornia	Log of B	ori	ng No	. SB7
					ELEVATION AND DATU	M:		
BORING		TION:			DATE STARTED:		DATE FINIS	HED:
DRILLIN	IG CON	NTRAC	TOR: F	Precision Sampling	2/17/95		2/17/95 MEASURIN	G POINT:
DRILLIN	IG ME	THOD:	Direc	t push	10 feet bgs		Ground su	T24 HBS
DBILLIN		JIPME	NT: XÍ	01	WATER			124 HN3.
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SAMPLI					RESPONSIBLE PROFE	SSIC	DNAL:	REG. NO.
HAMME	ER WEI	GHT:		DROP:	A. L. Spencer	-		N
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┢					D		l	3-4'	2 -			\otimes	r 11	3"-3':fill is a siltiy to clayey sand; olive brown		
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F	E	-	-						.	-	1.	<i>\//;</i>				
F	M	-	-					SB-10	. 6 -	-		V//	sc	3-7': Clayey Sand: dark brown; 20% clayey fines; 80% fine		
L	E	-	-	-			1.0	J.J-0.3	-	-		K/		Sanu, organic matter, dark brown to black		
	N	-	-	1	1			SB-10	8 .	-	1:	V	1			
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\mathbf{F}	G	_	_					1		Ţ	1	V//		7-14':Sandy Clay:dark brown; low plasticity clayey fines; 25%		
F	R	-	_	1					12	+-	_	<i>V//</i>	1	nne sano; roots common		
E	0	-	-		M					-		V//	1			
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\vdash	T	· ·			w	'		SB-10	16	Ţ	1		1	14-16': No Recovery		
\vdash		-	_					17-18						16-18':Sand: greenish gray; trace fines; fine sand		
	•		_				1.0	{	18	_	4		<u>4 5P</u>	- 18': Bottom of Boring		
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	- F11/5		GI	00	ATIC		ρT	REMEDIATION RISK MANAGEMENT, INC. WELL/BORING:SB-11							:SB-11			
Ň	ㄴㄴ나/[. 		11	19F1	ŀ	DATE:10/28/98 DRILLING METHOD:GEOPROBE						BE				
Î ↑		,	\sim				ŀ	PRO.IF	ECT:AA	46				SA	MPLING ME	THOD:CONTIN	UOS CORE	
[\mathbf{b}	•		ł	CLIEN	T:CHE	VRO	ЛС			BC	RING DIAME	TER:2"	·	
I .		/	•	/			ŀ	LOCA	TION:B		NDI	NG AV	Έ	BC	RING DEPTI	-1:~15'		
$>$		[/	/●	٤	SB-11	ŀ	CITY	LAME					WI	ELL CASING	Temporary 1"	sch 40 PVC	
8/	ind:		/				ŀ	<u> </u>	TATE		ME	DA		WELL SCREEN:				
1	-" ⁿ g,	Ave		<			ŀ	DRILL	ER:EC	Ā				SAND PACK:				
										ž			ا ير	WATER LEVEL:	8.19'	7.57	6.50'	
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	M								4-	Ļ	1	\otimes	١		, . ,			
L					D		ł	en	-				CL	5.5-14': Sandy Clay	r: greenish arav	r: 85% moderate	plasticity	
F			-		,,	ł	0.2	୍	6 -			(//	1	clayey fines; 15% s	and; some iror	1-oxide staining a	is veinlets	
⊢			1		1.01			SB-11				V//	1			· •>		
		_	1				ł	7-8'	8-			V//	1			*æ		
F	P]		w		1.0	SB-11	10 -			V//	1	@11':Increase in s	and content to	20-25%; fine san	ıd	
L			-					10-11			ľ	V//	1	@121.250/ 5	d' occasional a	and stringers an	d root holes	
F		_	-		W	1	0.3	SR-11	12 -			V//	1 00	@13.23% IINE Sal	ish grav: trace	clayey to silty fin	es; fine sand	
┢	T		-				0.3	14-15						15': Bottom of Bon	ing			
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	WELL/BORING LOCATION M/							P		REMI	EDI	ATI	ON R	SKN	IANAGEMENT, INC. WE	LL/BORING:SE	3-12
		N							DATE:	10/28/9	8				DRILLING METHO	D:GEOPROBE	
		T		٦					PROJ	ECT:AA	46				SAMPLING METH	OD:CONTINUC	S CORE
									CLIEN	T:CHE	VR	ON			BORING DIAMETE	ER:2"	
	``	$\overline{\ }$]					LOCA	TION'R		NDI	NG A	/E.	BORING DEPTH:~	-15'	
			$\overline{\ }$	_	<u> </u>	_ q			CITY		DA				WELL CASING:Te	mporary 1" sch	40 PVC
1	1				SB-	12			CO /S	TATE		MF	DA		WELL SCREEN:		
		A	VE.						DRII I	ERICA	• • • • • • • • •				SAND PACK:		
							<u> </u>	<u> </u>			~				WATER I EVEL: 4.63'		
								ESI	щК	ΞC	ER	<u></u> ,	₽	ABOL	TIME: 11:35		
W	/ELL/	BOR		RS	ABILL	JT L	NS NS	FN	MPI	EE	8	IMPL	API	SYN	DATE: 40/29/09		
	OMP	LET	ION	Ē	ST/	ő	LO D	H	NUS	ШĒ	Ц Ш	N IN	GR	nscs		1	I
L				∇	Y	Σ	ā	۲.			2	-	0000		DESCRIPTION/LOGGED BT.DR		
		Γ					p			-			\otimes		Planter Fill Top Soil; silty to clayey sa	nd; olive brown	
L			-						58_12	2-			\otimes				
	-					ס			2-3'	-			\otimes	F111			
\mathbf{F}			_		-				1	4-			\sim				
\vdash	-	M				м		1.0	SB-12	-			\langle / \rangle	C	4-12 5' Sandy Clay: dark gravish brow	n; low plasticity 8	0% fines:
F	1	E							6-7	6-			V//		20% fine sand		- •
	-	N		1			ĺ		SB-12	8-			V//		· · · · ·		
Ē	_	T						1.0	7-8'	Ŭ.			V//		@9':Sandy Clay: olive yellow;; low .p la	asticity 80% fines	; 25%
L		G							I	10-		-	V//	1	fine sand	plasticity 80% fr	165.
	-	R		-		M	Į	10	1	·			V//	1	20% fine sand	pidaticity 00 % III	
┢		0	_	1		VM				12 -			×	sc	12.5-14.5': Clayey Sand; greenish gra	ay; 25% fines; 75	% sand
\vdash	-	U		1			}	1	SB-12	44-				1	14.5-15': Sand; greenish gray; trace f	ines	
F		T		1		1	ļ	1.0	14-15	14 -		ļ		SP	15': Bottom of Boring		
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REMARKS

WELL LOG (PID) \\RAC-S1\SHARED\CHEVRON\6319-\631916-1\632941~1\BORING~1\20-6127 BORING LOGS.GPJ DEFAULT.GDT 7/9/09

Conestoga Rovers & Associates 10969 Trade Center Drive, Suite 107 Rancho Cordova, CA Telephone: 916-889-8900 Fax: 916-889-8999

Hand-Augered/Airknifed to 8 fbg.

BORING/ WELL LOG

CLIENT NAME	Chevron Environmental Management Co.	BORING/WELL NAME	SB-13		
JOB/SITE NAME	Former Signal Oil Bulk Plant	DRILLING STARTED	07-Jul-08		
LOCATION	2301-2311 Blanding Avenue, Alameda, CA	DRILLING COMPLETED	08-Jul-08		
PROJECT NUMBER	631916 (20-6127)	WELL DEVELOPMENT D	ATE (YIELD)	NA	
DRILLER	Woodward Drilling Co. Inc.	GROUND SURFACE ELE	VATION _	NA	
DRILLING METHOD	Hydraulic push	TOP OF CASING ELEVA		NA	
BORING DIAMETER	2 inches	SCREENED INTERVALS	_	NA	
LOGGED BY	C. Benedict	DEPTH TO WATER (First	Encountered	d) 15.0 fbg (08-Jul-08)	$\overline{\Sigma}$
REVIEWED BY	J. Kiernan, PE# C68498	DEPTH TO WATER (Stati	c)	NA	Ţ

CONTACT DEPTH (fbg) SAMPLE ID GRAPHIC LOG BLOW COUNTS PID (ppm) EXTENT DEPTH (fbg) U.S.C.S. LITHOLOGIC DESCRIPTION WELL DIAGRAM Asphalt ه ز Concrete 0.5 <u>Silty SAND</u>:Dark brown; dry; 60% sand, 25% silt, 10% gravel, 5% clay; low plasticity. SB-13 -1 43.2 SM 5 249 SB-13 -5 Silty SAND :Greenish grey; moist; 50% sand, 30% silt, 10% sand, 10% gravel; medium plasticity. Portland Type I/II 9.0 CLAY : Greenish grey; moist; 55% clay, 30% silt, 15% sand; medium plasticity. 10 SB-13 -10 CL 13.0 Silty SAND :Greenish grey; wet; 65% sand, 20% silt, 15% sand; medium plasticity; poorly graded medium to fine grained sand. SM Ā 5 16.0 Bottom of Boring @ 16 fbg



REMARKS

WELL LOG (PID) \RAC-S1\SHARED\CHEVRON(6319-\631916-1\632941-1\BORING-1\20-6127 BORING LOGS.GPJ DEFAULT.GDT 7/9/09

Conestoga Rovers & Associates 10969 Trade Center Drive, Suite 107 Rancho Cordova, CA Telephone: 916-889-8900 Fax: 916-889-8999

Hand-Augered/Airknifed to 8 fbg.

BORING/ WELL LOG

CLIENT NAME	Chevron Environmental Management Co	BORING/WELL NAME	SB-14		
JOB/SITE NAME	Former Signal Oil Bulk Plant	DRILLING STARTED	07-Jul-08		
LOCATION	2301-2311 Blanding Avenue, Alameda, CA	DRILLING COMPLETED	08-Jul-08		
PROJECT NUMBER	631916 (20-6127)	WELL DEVELOPMENT D	ATE (YIELD)	NA	
DRILLER	Woodward Drilling Co. Inc.	_ GROUND SURFACE ELE		NA	
DRILLING METHOD	Hydraulic push	TOP OF CASING ELEVAT		NA	
BORING DIAMETER	2 inches	SCREENED INTERVALS	_	NA	
LOGGED BY	C. Benedict	DEPTH TO WATER (First	Encountered	d) 14.5 fbg (08-Jul-08)	$\overline{\nabla}$
REVIEWED BY	J. Kiernan, PE# C68498	DEPTH TO WATER (Stati	c)	NA	Ţ

CONTACT DEPTH (fbg) SAMPLE ID GRAPHIC LOG PID (ppm) BLOW COUNTS EXTENT DEPTH (fbg) U.S.C.S. LITHOLOGIC DESCRIPTION WELL DIAGRAM Asphalt 50 Concrete 0.5 Clayey SAND Dark brown; dry; 65% sand, 15% clay, 10% silt, 10% gravel; low plasticity. SB-14 -1 2.0 SC 4.0 Silty SAND: Black; moist; 45% sand, 30% silt, 25% clay; low plasticity. SM 5 1.6 SB-14 -5 5.5 CLAY: Grey; moist; 55% clay, 30% silt, 15% sand (well-sorted fined grained); medium plasticity; CL Portland Type I/II SB-14 -10 10 10.5 CLAY with sand: Grey; moist; 55% clay, 30% silt, 15% sand; medium plasticity. CL 11.5 Sandy CLAY:Brown; moist; 50% clay, 35% sand, 15% silt; medium plasticity. CL 13.0 <u>Silty SAND</u>:Brown with grey mottling; moist 55% sand, 30% silt, 10% clay; low plasticity. SM ☑ 14.5 Silty SAND:Brown; wet; 75% sand, 15% silt, 10% clay; low plasticity. SM 16.0 Bottom of Boring @ 16 fbg



REMARKS

WELL LOG (PID) \\RAC-S1\SHARED\CHEVRON\6319-\631916-1\632941~1\BORING~1\20-6127 BORING LOGS.GPJ DEFAULT.GDT 7/9/09

Conestoga Rovers & Associates 10969 Trade Center Drive, Suite 107 Rancho Cordova, CA Telephone: 916-889-8900 Fax: 916-889-8999

BORING/ WELL LOG

CLIENT NAME	Chevron Environmental Management Co.	BORING/WELL NAME	SB-15		
JOB/SITE NAME	Former Signal Oil Bulk Plant	_ DRILLING STARTED	07-Jul-08		
LOCATION	2301-2311 Blanding Avenue, Alameda, CA	DRILLING COMPLETED	08-Jul-08		
PROJECT NUMBER	631916 (20-6127)	WELL DEVELOPMENT D	ATE (YIELD)	NA	
DRILLER	Woodward Drilling Co. Inc.	_ GROUND SURFACE ELE		NA	
DRILLING METHOD	Hydraulic push	_ TOP OF CASING ELEVA		NA	
BORING DIAMETER	2 inches	SCREENED INTERVALS	_	NA	
LOGGED BY	C. Benedict	DEPTH TO WATER (First	Encountere	d) 15.0 fbg (08-Jul-08)	$\overline{\Sigma}$
REVIEWED BY	J. Kiernan, PE# C68498	_ DEPTH TO WATER (Stati	ic)	NA	Ţ

Hand-Augered/Airknifed to 8 fbg. CONTACT DEPTH (fbg) SAMPLE ID PID (ppm) GRAPHIC LOG BLOW COUNTS EXTENT DEPTH (fbg) U.S.C.S. LITHOLOGIC DESCRIPTION WELL DIAGRAM Asphalt 50 Concrete 0.5 Silty SAND :Dark brown; moist; 65% sand, 20% silt, 15% clay, 5% gravel; low plasticity. SB-15 -1 0 SM 4.0 <u>Clayey SAND</u>:Black; moist; 60% sand, 20% clay, 10% silt, 10% gravel; low plasticity. 5 0.4 SB-15 -5 <u>Clayey SAND</u>:Dark brown; moist; 60% sand, 20% clay, 10% silt, 10% gravel; low plasticity. SC Portland Type I/II 52.1 SB-15 -9.5 9.5 CLAY with sand: Green; moist; 45% clay, 30% sand, 20% silt, 5% gravel; medium plasticity. n CL 14.5 <u>Silty SAND</u>:Greenish grey; wet; 55% sand (medium to fine grained), 30% silt, 10% clay; low plasticity. Ā SM 16.0 Bottom of Boring @ 16 fbg

PAGE 1 OF 1



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BORING/ WELL LOG

CLIENT NAME	Chevron Environmental Management Co.	BORING/WELL NAME SB-16	
JOB/SITE NAME	Former Signal Oil Bulk Plant	DRILLING STARTED 07-Jul-08	·
LOCATION	2301-2311 Blanding Avenue, Alameda, CA	DRILLING COMPLETED 08-Jul-08	
PROJECT NUMBER	631916 (20-6127)	WELL DEVELOPMENT DATE (YIEL	D) NA
DRILLER	Woodward Drilling Co. Inc.	GROUND SURFACE ELEVATION	NA
DRILLING METHOD	Hydraulic push	TOP OF CASING ELEVATION	NA
BORING DIAMETER	2 inches	SCREENED INTERVALS	NA
LOGGED BY	C. Benedict	DEPTH TO WATER (First Encounte	red) NA 💆
REVIEWED BY	J. Kiernan, PE# C68498	DEPTH TO WATER (Static)	NA T

REMARKS

WELL LOG (PID) NRAC-S1\SHARED\CHEVRON6319-\631916~1\632941~1\BORING~1\20-6127 BORING LOGS.GPJ DEFAULT.GDT 7/9/09

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WEL	L DIAGRAM
					SM		<u>Silty SAND</u> :Brown; dry; 50% sand, 20 gravel, 20% silt, 10% clay; low plasticity.	3.0		
							Refusal at 3 feet.			Bottom of Boring @ 3 fbg



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BORING/ WELL LOG

CLIENT NAME	Chevron Environmental Management Co.	BORING/WELL NAME SB	-17	
JOB/SITE NAME	Former Signal Oil Bulk Plant	_ DRILLING STARTED07-	Jul-08	
LOCATION	2301-2311 Blanding Avenue, Alameda, CA	DRILLING COMPLETED08-	Jul-08	
PROJECT NUMBER	631916 (20-6127)	WELL DEVELOPMENT DATE	(YIELD) NA	
DRILLER	Woodward Drilling Co. Inc.	GROUND SURFACE ELEVAT	ION NA	
DRILLING METHOD	Hydraulic push	TOP OF CASING ELEVATION	NA	
BORING DIAMETER	₹ 2 inches	SCREENED INTERVALS	NA	
LOGGED BY	C. Benedict	DEPTH TO WATER (First Enc	ountered) NA	$\overline{\Delta}$
REVIEWED BY	J. Kiernan, PE# C68498	DEPTH TO WATER (Static)	NA	Ţ
LOGGED BY _ REVIEWED BY _	C. Benedict J. Kiernan, PE# C68498	_ DEPTH TO WATER (First Enc _ DEPTH TO WATER (Static)	ountered) NA NA	

REMARKS Hand-Augered/Airknifed to 8 fbg. CONTACT DEPTH (fbg) SAMPLE ID GRAPHIC LOG PID (ppm) BLOW COUNTS EXTENT DEPTH (fbg) U.S.C.S. LITHOLOGIC DESCRIPTION WELL DIAGRAM Asphalt ه ز Concrete 0.5 <u>Silty SAND</u>:Grey; moist; 60% sand, 20% silt, 10% clay, 10% gravel; low plasticity. SB-17 -1 1.7 SM 4.0 <u>Clayey SAND</u>:Black; moist; 55% sand, 20% clay, 15% silt, 10% gravel (coarse angular); low plasticity. SC 5 122 SB-17 -5 6.0 CLAY with sand: Greenish grey; moist; 45% 5 clay, 25% silt, 20% sand; medium plasticity. CL Portland Type I/II SB-17 -9.5 10 10.5 Silty SAND: Greenish grey; moist 55% sand (medium to fine grained), 30% silt, 10% clay; low plasticity. SM 16.0 Bottom of Boring @ 16 fbg



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BORING/ WELL LOG

WELL DIAGRAM

Concrete

Portland Type

Bottom of Boring @ 16 fbg

I/II

10

CLIENT NAME	Chevron Environmental Management Co.	BORING/WELL NAME	SB-18		
JOB/SITE NAME	Former Signal Oil Bulk Plant	DRILLING STARTED	07-Jul-08		
LOCATION	2301-2311 Blanding Avenue, Alameda, CA	DRILLING COMPLETED	08-Jul-08		
PROJECT NUMBER	631916 (20-6127)	WELL DEVELOPMENT D	ATE (YIELD)	NA	
DRILLER	Woodward Drilling Co. Inc.	GROUND SURFACE ELE	VATION _	NA	
DRILLING METHOD	Hydraulic push	TOP OF CASING ELEVAT	ION _	NA	
BORING DIAMETER	2 inches	SCREENED INTERVALS	_	NA	
LOGGED BY	C. Benedict	DEPTH TO WATER (First	Encountered	l) 14.5 fbg (08-Jul-08)	$\underline{\nabla}$
REVIEWED BY	J. Kiernan, PE# C68498	DEPTH TO WATER (Stati	c)	NA	Ţ

Brown with grey mottling; moist 55% sand, 30% silt, 10%

Brown; wet; 75% sand, 15% silt, 10% clay; low plasticity.

REMARKS Hand-Augered/Airknifed to 8 fbg. CONTACT DEPTH (fbg) SAMPLE ID GRAPHIC LOG PID (ppm) BLOW COUNTS EXTENT DEPTH (fbg) U.S.C.S. LITHOLOGIC DESCRIPTION Asphalt 0.5 <u>Silty SAND</u>:Grey; moist; 60% sand, 20% silt, 10% clay, 10% gravel; low plasticity. SB-18 -1 56.3 SM 4.0 Clavey SAND: Black; moist; 55% sand, 20% clay, 15% WELL LOG (PID) \RAC-S1\SHARED\CHEVRON(6319-\631916-1\632941-1\BORING-1\20-6127 BORING LOGS.GPJ DEFAULT.GDT 7/9/09 silt, 10% gravel (coarse angular); low plasticity. SC 5 114 SB-18 -5 6.0 CLAY with sand: Grey with green mottling; moist; 45% clay, 30% sand, 20% silt, 5% gravel; medium plasticity. CL SB-18 -9.5 10 10.5 Silty SAND: Greenish grey; moist 55% sand (medium to fine grained), 30% silt, 10% clay; low plasticity.

clay; low plasticity.

SM

 ∇

16.0



WELL LOG (PID) NRAC-S1\SHARED\CHEVRON\6319-\631916-1\632941-1\BORING~1\2015 BORING LOGS.GPJ DEFAULT.GDT 7/9/09

Conestoga Rovers & Associates 10969 Trade Center Drive, Suite 107 Rancho Cordova, CA Telephone: 916-889-8900 Fax: 916-889-8999

BORING/ WELL LOG

CLIENT NAME	Chevron Environmental Management Co.	BORING/WELL NAME SB-19
JOB/SITE NAME	Former Signal Oil Bulk Plant	DRILLING STARTED 07-Jul-08
LOCATION	2301-2311 Blanding Avenue, Alameda, CA	DRILLING COMPLETED 08-Jul-08
PROJECT NUMBER	631916 (20-6127)	WELL DEVELOPMENT DATE (YIELD) NA
DRILLER	Woodward Drilling Co. Inc.	_ GROUND SURFACE ELEVATIONNA
DRILLING METHOD	Hydraulic push	TOP OF CASING ELEVATION NA
BORING DIAMETER	2 inches	SCREENED INTERVALS NA
LOGGED BY	C. Benedict	_ DEPTH TO WATER (First Encountered) 14.5 fbg (08-Jul-08)
REVIEWED BY	J. Kiernan, PE# C68498	_ DEPTH TO WATER (Static) NA
REMARKS	Hand-Augered/Airknifed to 8 fbg.	

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WEI	LL DIAGRAM
							Asphalt	0.5	0,00,0,0	 Concrete
362		SB-19 -1					<u>Silty SAND</u> :Dark brown; moist; 60% sand, 20% silt, 10% clay, 10% gravel; low plasticity; conrete fragements.			
1 070		SP 10 5		 - 5	SM		Brown; wet; 75% sand, 15% silt, 10% clay; low plasticity. Black; moist; 60% sand, 20% silt, 10% clay, 10% gravel; low plasticity.			
1,373		28-19-2					low plasticity.			
							Greenish grey; moist; 70% sand, 20% silt, 10% clay; low plasticity.	7.0		
							CLAY with sand: Greenish grey with balck mottling; moist; 45% clay, 30% sand, 25% silt; medium plasticity.			
		SB-19 -10								 Portland Type I/II
					CL					
								14.0		
					SM		Silty SAND:Greenish grey; wet; 65% sand (poorly graded), 20% silt, 15% clay; low plasticity. □	16.0		
										Bottom of Boring @ 16 fbg

Plantedu denome Plantedu	PROJECT: PARK STRE	ET LANDING	Log of Bori	n <mark>g No. GWS-7A</mark>
United Evolution: Note Services Date Services Date Services PRILLING CONTRACTOR: Precision Sampling TOTAL DEPTH: MetaBulko PONT: PRILLING CONTRACTOR: Direct push 0 feet Gravel services PRILLING CONTRACTOR: Precision Sampling TOTAL DEPTH: MetaBulko PONT: PRILLING CONTRACTOR: Enviro CONTRACTOR: Precision Sampling PRILLING CONTRACTOR: Enviro PRES COMPL 24 HR3. Advected Enviro DROP: A L Spencer Red. Not. Advected Sampling MetaBulko PONT: REG. NO. Red. Not. Sampling Gravel sidewalk Red. Not. CLAYEY SAND (SC) 2- 3- 3- 3-		thwest corner by canal	ELEVATION AND DATUM	1:
RILLING METHOD: Direct push 472490 Instruction Prediction Sampling RILLING EQUIPMENT: XD-3 0 FIRST GOWH 24 HIS. Ground auface AMPLING EQUIPMENT: XD-3 0 FIRST COMPL 24 HIS. Market WEIGHT: AMPLING EGUIPMENT: XD-3 0 FIRST COMPL 24 HIS. Market WEIGHT: MAMER WEIGHT: DROP: A.L. Spenner RESPONSIBLE PROFESSIONAL: PRE. NO SAMPLES B B B B B B Singe S SAMPLES B B B B Singe S SAMPLES B B B B Singe S Singe Elevation: CLAYEY SAND (SC) Very dark gray/sh brown (10Y 3/2), dry, 60% medium sand, 30% low plasticity fines, 10% small gravel, loose - Gravel sidewalk Gravel sidewalk - - - GRANULAR MATERIAL Black (7.5YR 2.5/1), moist, 60% fine to medium grains, 35% low plasticity fines, 5% small gravel, loose - Fefusal at 6 feet bgs - - - - - - - - - - - - - - - - - - - - - - - <tr< td=""><td>BORING LOCATION: NOR</td><td></td><td>DATE STARTED:</td><td>DATE FINISHED:</td></tr<>	BORING LOCATION: NOR		DATE STARTED:	DATE FINISHED:
IRILLING ECUIPMENT: XD-3 6 feet FIRST COMPL 24 HBS. IRILLING ECUIPMENT: XD-3 WATER FIRST COMPL 24 HBS. AMPUING METHOD: Enviro Core System S. L. Anich FIRST COMPL 24 HBS. IAMMER WEIGHT: Image: Core System DESCRIPTION A. L. Spencer RG S71 Image: SAMPLes Image: Samples Image: Samples Image: Samples RG S71 Image: Samples Image: Samples Image: Samples Image: Samples RG S71 Image: Samples Image: Samples Image: Samples Image: Samples RG S71 Image: Samples Image: Samples Image: Samples Image: Samples RG S71 Image: Samples Image: Samples Image: Samples Image: Samples RG S71 Image: Samples Image: Samples Image: Samples Image: Samples RG S71 Image: Samples Image: Samples Image: Samples Image: Samples RG S71 Image: Samples Image: Samples Image: Samples Image: Samples Image: Samples Image: Samples Image: Samples Image: Samples I	DRILLING CONTRACTOR:	Precision Sampling	4/24/95 TOTAL DEPTH:	MEASURING POINT:
MATER		ct push	DEPTH TO FIRST	COMPL. 24 HRS.
AMPLIAB METHOD: Enviro Core System S.L. Anich S.M. Anic		(D-3	LOGGED BY:	
MAMMER WEIGHT: DDOP: A.L.Spencer R6 57: SAMPLES Samples Samples Samples Rescuence	SAMPLING METHOD: EN	viro Core System	S. L. Anich RESPONSIBLE PROFES	SSIONAL: REG. NO.
SAMPLES Market UUGCE Symbol: code; midd, Styme, Law, Annow, Structure, carentation, mact. wh7C; get. Inter. REMARKS - - - - - - - - - <td< td=""><td>HAMMER WEIGHT:</td><td>DROP:</td><td>A. L. Spencer</td><td>RG 5713</td></td<>	HAMMER WEIGHT:	DROP:	A. L. Spencer	RG 5713
3 3 3 4 2 Surface Elevator: 1 4 Gravel sidewalk - 2 - - - - 3 - - - - 3 - - - - 4 - - - - 4 - - - - 5 - - - - 6 - - - - 7 - - - - 9 - - - - 11 - - - - 12 - - - - 13 - - - - 14 - - - -	(feet) mple ows/Sading (ppm)	DESCRI NAME (USCS Symbol): color, moist, % by wt, plast, de	PTION nsity, structure, comentation, react. w/HCI, geo. inter.	REMARKS
CLAYEY SAND (SC) Very dark gravish brown (10Y 3/2), dry, 60% medium sand, 30% low plasticity fines, 10% small gravel, loose Gray concrete and brick fragments GRANULAR MATERIAL Black (7.5/R 2.5/1), moist, 60% fine to medium grains, 35% low plasticity fines, 5% small gravel, loose Refusal at 6 feet bgs		Surface Elev	vation:	
2 CLAYEY SAND (SC) Very dark grayish brown (10Y 3/2), dry, 60% medium sand, 30% low plasticity fines, 10% small gravel, loose 3 4 Black (7.5YR 2.5/1), moist, 60% fine to medium grains, 35% low plasticity fines, 5% small gravel, loose 5 6 7 8 9 10 11 12 13 14		Glaver sidewaik		-
3 sand, 30% low plasticity fines, 10% small gravel, loose 3 Gray concrete and brick fragments 4 Black (7.5YR 2.5/1), moist, 60% fine to medium grains, 35% low plasticity fines, 5% small gravel, loose 5 Black (7.5YR 2.5/1), moist, 60% fine to medium grains, 35% low plasticity fines, 5% small gravel, loose 6 Refusal at 6 feet bgs 7 - 8 - 9 - 10 - 11 - 12 - 13 - 14 -		CLAYEY SAND (SC) Very dark grayish brown (10Y 3	/2), dry, 60% medium	
GRANULAR MATERIAL Black (7.5YR 2.5/1), moist, 60% fine to medium grains, 35% low plasticity fines, 5% small gravel, loose	3-	sand, 30% low plasticity fines, 1 Gray concrete and brick fragme	10% small gravel, loose	
6 Refusal at 6 feet bgs - 7 - 8 - 9 - 10 - 11 - 12 - 13 - 14 -	4 - 5 -	GRANULAR MATERIAL Black (7.5YR 2.5/1), moist, 60% low plasticity fines, 5% small gr	6 fine to medium grains, 35% avel, loose	-
		Refusal at 6 feet bgs		
	7-			
9- 10- 11- 11- 12- 13- 14- 14- 14- 15- 15- 15- 15- 15- 15- 15- 15	8-			
10- - 11- - 12- - 13- - 14- - - - - - - - - - - - - -	9-			
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	11 -			
	12 -			
14 B-1	13 -			

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PROJECT: PARK STRE Alameda, Ca	ET LANDING Ilifornia	Log of Bo	ring No.	GWS-7B
DODING LOCATION: Nort	bwest corner by canal	ELEVATION AND DAT Gravel sidewalk	TUM:	
	Precision Sampling	DATE STARTED:	DATE FIN	NISHED:
DRILLING CONTRACTOR:	Precision Sampling	TOTAL DEPTH:	MEASUR	ING POINT:
DRILLING METHOD: Direc	ct push	6 feet	T COMPL.	24 HRS.
DRILLING EQUIPMENT: X	D-3	WATER		
SAMPLING METHOD: EN	viro Core System	S. L. Anich		DEG NO
HAMMER WEIGHT:	DROP:	RESPONSIBLE PROP A. L. Spencer	FESSIONAL:	RG 5713
	DESCRIP NAME (USCS Symbol); color, moist, % by wt. plast, dens	TION ity, structure, cementation, react. w/HCl, geo. int	er.	REMARKS
(fec fec Samples Blows PID Re PID Re	Surface Eleva	tion:		
	Gravel sidewalk CLAYEY SAND (SC)	2), dry, 60% medium		
	sand, 30% low plasticity fines, 10 Gray concrete / brick	% small gravel, loose		
- - - - - - - -	GRANULAR MATERIAL Black (7.5YR 2.5/1), moist, 60% low plasticity fines, 5% small gra	fine to medium grains, 35% vel, loose		
	Refusal at 6 feet bgs			
-				
9-				
10-				
12-				
13 -				
				B-1 (1
14		Project N	0. 2436.02	Figure

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PROJECT: PAF Alar	RK STRE	EET LANDING alifornia	Log	of Borin	g No. GWS-7
BORING LOCATI	ON: Nor	thwest corner of property	ELEVATION Gravel sid	I AND DATUM: ewalk	
DRILLING CONT	RACTOR:	Precision Sampling	DATE STAR 4/24/95	TED:	DATE FINISHED: 4/24/95 1000 hrs.
DRILLING METH	OD: Dire	ect push	TOTAL DEP	TH:	MEASURING POINT: Ground surface
	MENT: X	(D-3	DEPTH TO	FIRST as 9 feet	COMPL. 24 HRS.
		viro Core System	LOGGED B	Y: 1	
		DROP:	RESPONSI A L Sper	BLE PROFESSIO	DNAL: REG. NO.
H SAMPLE	ot C Reading Ppm)	DESCF NAME (USCS Symbol): color, moist, % by wt., plast, «	IPTION density, structure, comentation, react. w	/HCl, geo. inter.	REMARKS
DE Sam Sam Sam Sam		Surface El	evation:		
		CLAYEY SAND (SC) Very dark grayish brown (10YF sand, 30% low plasticity fines,	3/2), dry, 60% medium 10% small gravel, loos	n – e –	2
		GRANULAR MATERIAL			
		CLAYEY SAND (SC) Light olive brown (2.5Y 5/3), di sand, 35% low plasticity fines,	y, 60% fine to medium 5% small gravel, loose	_ _ _ _	
6		CLAYEY SAND (SC) Light olive brown (2.5Y 5/3) wi 60% fine sand, 35% low plastic loose	th brick fragments, mois city fines, 5% small grav	st, –	
		LEAN CLAY with SAND (CL) Black (10YR 2/1), moist, 80% plasticity, soft	fines, 20% sand, low	- - - 포 -	
		1-inch lense of coarse grave			
12 -		LEAN CLAY (CL) Black (10YR 4/1), wet, 95% fir hard	nes, 5% sand, high plas	ticity, -	
13-		LEAN CLAY (CL) Greenish gray gley (5G 5/1), n medium plasticity	noist, 95% fines, 5% sa	nd, \	0.1/0-201
		Geometrix Consultante		Project No. 2436	.02 Figure
2436.02.016		Geomatrix Consultants			

PROJECT: PARK STREET LANDING Alameda, California	Log of Boring No.	GWS-7 (cont.)
H L d B C C C C C C C C C C C C C C C C C C	RIPTION density, structure, cementation, react. w/HCI, geo. inter.	· REMARKS
LEAN CLAY (CL) (continued)		-
Orange mottling		-
Bottom of boring at 15 feet bgs	s	-
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27-		-
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31		B-2 (11
2438.02.017 Geomatrix Consultants	Project No. 24	36.02 Figure

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PROJECT: PARK STRE Alameda, Ca	ET LANDING alifornia	Log of Bori	ng No. GWS-8
BORING LOCATION: Side	ewalk, northwest corner	ELEVATION AND DATUM: Grassy area	
DRILLING CONTRACTOR:	Precision Sampling	DATE STARTED: 4/24/95	DATE FINISHED: 4/24/95 - 1130 hrs
	ect push	TOTAL DEPTH: 16 feet	MEASURING POINT: Ground surface
	(D-3	DEPTH TO FIRST	COMPL. 24 HRS.
	vite Core System	LOGGED BY:	
		RESPONSIBLE PROFESS	IONAL: REG. NO.
		A. L. Spencer	
PTH ws/ ppm)	DESCRIPTION NAME (USCS Symbol): color, moist, % by wt., plast., density, str	ucture, cementation, react. w/HCl, geo. inter.	REMARKS
DE Sarr Sarr Blo PID PID	Surface Elevation:		
$ \begin{array}{c} - \\ 1 - \\ - \\ 2 - \\ - \\ 3 - \\ - \\ 3 - \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\$	CLAYEY SAND (SC) Very dark gray (10YR 3/1) with abun grass), moist, 65% medium sand, 25 10% fine to coarse gravel, loose	dant organics (roots, % low plasticity fines, 9% low plasticity fines ∑ 25% fine sand, low % fines, 5% fine sand, low	No recovery in upper 2 feet
			B-1 (11/92)
2436.02.018	Geomatrix Consultants	Project No. 243	6.02 Figure

PROJECT: PARK STREET LANDING Alameda, California	Log of Boring No.	GWS-8	(cont.)
SAMPLES D L ed od L ed od U ed U	RIPTION density, structure, cementation, react. w/HCI, geo. inter.	RE	MARKS
LEAN CLAY (CL) (continued) Increase sand content to 20	%		
15 - CLAYEY SAND (SC) Light olive brown (2.5Y 5/4) wi moist, 60% fine sand, 40% lov	ith green and brown mottling, v plasticity fines	-	
16 - Bottom of boring at 16 feet bg	S	-	
		4	
		-	
21-			
22-		-	
23-			
24-			
25-			
26-			
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31		0.426.02	B-2 (11/
Geomatrix Consultants	Project No.	2436.02	

PROJECT: PARK STRE		Log of Borin	ng No. GWS-9
Alameda, Ca	anorna	ELEVATION AND DATUM:	
BORING LOCATION: Alor	ng canal - middle	Sidewalk (gravel)	DATE FINISHED:
DRILLING CONTRACTOR:	Precision Sampling	4/24/95	4/24/95 - 1330 hrs
	ct push	16 feet	Ground surface
		DEPTH TO FIRST	COMPL. 24 HRS.
		LOGGED BY:	
SAMPLING METHOD: En	viro Core System	S. L. Anich RESPONSIBLE PROFESS	IONAL: REG. NO.
HAMMER WEIGHT:	DROP:	A. L. Spencer	RG 5713
	DESCRIPT	ION ty, structure, cementation, react. w/HCI, geo. inter.	REMARKS
(fee ample foot foot foot	Surface Elevat	ion:	
$ \begin{array}{c} - \\ 1 \\ - \\ 2 \\ - \\ 3 \\ - \\ - \\ 3 \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ -$	SANDY LEAN CLAY with GRAVE Very dark gray (10YR 3/1), dry, 6 medium sand, 15% medium grave CLAYEY SAND with GRAVEL (S Very dark gray (10YR 3/1), calciu medium sand, 25% low plasticity loose Increase sand content to 80% LEAN CLAY with SAND (CL) Black (10YR 2/1), moist, 85% fine plasticity Increase sand content to 30% LEAN CLAY (CL) Greenish gray (10GY 5/1), moist low plasticity Orange mottling	EL (CL) 0% fines, 25% fine to el, low plasticity C) Im deposits, dry, 60% fine to fines, 15% fine gravel, es, 15% fine sand, low 5, 95% fines, 5% fine sand,	No recovery in upper 3 feet
			8-1 (11)
	Geometrix Consultants	Project No. 24	36.02 Figure
2428 02 020	Geomatrix Consultante	and the second secon	

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BAMPLES B </th <th>PROJECT: PARK STREET LANDING Alameda, California</th> <th>Log of Boring N</th> <th>No. GWS-9 (cont.)</th>	PROJECT: PARK STREET LANDING Alameda, California	Log of Boring N	No. GWS-9 (cont.)
a a	H (199) SAMPLES Sample Soot L Sample NAME (USCS Symbol): cok	DESCRIPTION or, moist, % by wt., plast., density, structure, cementation, react. w/HCl, geo. ir	inter. REMARKS
15 CLAYEY SAND (SC) Greenish gray (10Y S/1) with orange mottling, moist, 60% fine sand, 40% low plasticity fines 16 Bottom of boring at 16 feet bgs 17 - 18 - 19 - 20 - 21 - 22 - 23 - 24 - 25 - 26 - 27 - 28 - 29 - 30 - 31 -		CL) (continued)	
16- Bottom of boring at 16 feet bgs 17- - 18- - 19- - 20- - 21- - 22- - 23- - 24- - 25- - 26- - 27- - 28- - 29- - 30- - 31- -	15 - CLAYEY SAN Greenish gray sand, 40% low	D (SC) (10Y 5/1) with orange mottling, moist, 60% find plasticity fines	
	16 Bottom of bori	ng at 16 feet bgs	
21 1 22 1 23 1 24 1 25 1 26 1 27 1 28 1 29 1 30 1			
	21-		
	22-		
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25- - 26- - 27- - 28- - 29- - 30- - 31- -	24-		
26- - 27- - 28- - 29- - 30- - 31- -	25-		
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	31		B-2 (1

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ROJECT: PARK STRE	ET LANDING	Log of Borir	ng No. GWS-10
Alameda, Ca		ELEVATION AND DATUM:	
ORING LOCATION:' Alor	ng canal - middle	Gravel sidewalk	DATE FINISHED:
BULING CONTRACTOR:	Precision Sampling	4/24/95	4/24/95 - 1430 hrs
	-t	TOTAL DEPTH:	Ground surface
		DEPTH TO FIRST	COMPL. 24 HRS.
RILLING EQUIPMENT:)	(D-3	UNTER LOGGED BY:	
AMPLING METHOD: En	viro Core System	S. L. Anich	SIONAL: REG. NO.
AMMER WEIGHT:	DROP:	A. L. Spencer	RG 5713
SAMPLES P	DESCRIF NAME (USCS Symbol): color, moist, % by wt., plast, der	PTION hsity, structure, cementation, react. w/HCI, geo. inter.	REMARKS
(fe Foo Blow Foo PiD R Foo	Surface Elev	ation:	
-	CLAYEY SAND (SC) Very dark gray (10YR 3/1), mois plasticity fines, 5% fine to coarse Increase gravel content to 15 SANDY LEAN CLAY (CL) Black (5Y 2.5/1), moist, 60-70% sand, low plasticity, soft Increase moisture LEAN CLAY (CL) Dark greenish gray (5G 4/1), m brown organics, moist, 80-90% sand, trace fine gravel, low pla Organics and orange mottlin	st, 70% fine sand, 25% low e subangular gravel % % 6 fines, 30-40% fine to coarse noderate amount yellow to 6 fines, 10-20% fine to coarse asticity, firm	2 feet
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			-

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PROJECT: PARK STREET LANDING Alameda, California

Log of Boring No. GWS-10 (cont.)

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20							-	
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19-								
4			1					
18-]	
4							1	
17-							1	
-					Bottom of boring at 16 feet bgs		-	
16-		Ц		ł	fines, loose		-	
15					POORLY GRADED SAND WITH CLAY (SP - SC) Grav (N54) moist 90% fine to medium sand, 10% low p	plasticity	-	
							4	
				>1200	LEAN CLAY (CL) (continued)			
DEPT (feet sample	No.	Bious/	Foot	OVN Readi	NAME (USCS Symbol): color, moist, % by wt., plast., density, structure, cementation, react. w/H	ICI, geo. inter.		REMARKS
Eal	SAM	PLE	S	P gui	DESCRIPTION			
				_			1	

BORING LOCATION: Along canal - southeast side EI DRILLING CONTRACTOR: Precision Sampling D, DRILLING METHOD: Direct push Tr DRILLING EQUIPMENT: XD-3 DI SAMPLING METHOD: Enviro Core System S HAMMER WEIGHT: DROP: The second	LEVATION AND DATUM: Gravel sidewalk ATE STARTED: /24/95 OTAL DEPTH: 6 feet EPTH TO FIRST VATER OGGED BY: 5, L. Anich IESPONSIBLE PROFESS A. L. Spencer ation, react. w/HCl, geo. inter.	DATE FINIS 4/24/95 - 1 MEASURIN Ground su COMPL.	SHED: 1530 hrs G POINT: Irface 24 HRS. 24 HRS. REG. NO. RG 5713
DRILLING CONTRACTOR: Precision Sampling Dr. DRILLING METHOD: Direct push Tr DRILLING EQUIPMENT: XD-3 DI SAMPLING METHOD: Enviro Core System S HAMMER WEIGHT: DROP: HAME (USCS Symbol): color, moist, % by wt. plast. density, structure, cemental Surface Elevation: GRAVEL SIDEWALK	ATE STARTED: /24/95 OTAL DEPTH: 6 feet EPTH TO FIRST VATER OGGED BY: 5, L. Anich IESPONSIBLE PROFESS A. L. Spencer ation, react. w/HCl, geo. inter.	DATE FINIS 4/24/95 - 1 MEASURIN Ground su COMPL.	HED: 1530 hrs G POINT: Irface 24 HRS.
DRILLING METHOD: Direct push Tr DRILLING EQUIPMENT: XD-3 Di SAMPLING METHOD: Enviro Core System LC HAMMER WEIGHT: DROP: T OROP: T OROP: <	OTAL DEPTH: 6 feet EPTH TO FIRST VATER OGGED BY: 5, L. Anich IESPONSIBLE PROFESS A. L. Spencer ation, react. w/HCl, geo. inter.	IONAL:	G POINT: Irface 24 HRS. REG. NO. REG. NO. RG 5713
DRILLING EQUIPMENT: XD-3 D SAMPLING METHOD: Enviro Core System LC HAMMER WEIGHT: - DROP: R HAMMER WEIGHT: - DROP: A DROP: - B DROP: </td <td>EPTH TO FIRST VATER OGGED BY: 3. L. Anich IESPONSIBLE PROFESS A. L. Spencer ation, react. w/HCl, geo. inter.</td> <td>IONAL:</td> <td>24 HRS.</td>	EPTH TO FIRST VATER OGGED BY: 3. L. Anich IESPONSIBLE PROFESS A. L. Spencer ation, react. w/HCl, geo. inter.	IONAL:	24 HRS.
BAMPLING METHOD: Enviro Core System LC SAMPLING METHOD: Enviro Core System S HAMMER WEIGHT: DROP: R HAMMER WEIGHT: DROP: A DROP: DESCRIPTION A DESCRIPTION NAME (USCS Symbol): color, moist, % by wt. plast, density, structure, cementa Surface Elevation: GRAVEL SIDEWALK	VATER OGGED BY:), L. Anich IESPONSIBLE PROFESS A. L. Spencer ation, react. w/HCl, geo. inter.	IONAL:	REG. NO.
SAMPLING METHOD: Enviro Core System S HAMMER WEIGHT: - DROP: R L SAMPLES B DESCRIPTION MAME B B B Max B B B B B	ation, react. w/HCl, geo. inter.	IONAL:	REG. NO. RG 5713
HAMMER WEIGHT: DHOP: A Image: Structure of the structu	A, L. Spencer	RE	; RG 5/13
Image: Samples Image	ation, react. w/HCl, geo. inter.	RE	
			MARKS
	(
1- A SANDY LEAN CLAY (CL)		1 1/2 feet	ery in upper
2 - Very dark grayish brown (10YR 3/2), moist, 60 fine to coarse sand, 10% subangular gravel, lo soft	ow plasticity, -		
4 - Increase organic content, wood fragments	-		
0	6 fines, 15% el, low plasticity,		
8 - LEAN CLAY (CL) Bluish gray (10B 6/1), moist, 90% fines, 10% coarse sand, low plasticity, firm	medium to	-	
10 - Color change to pale olive with green and o	ange mottling	-	
12 - 		-	
		_	
	Project No. 243	6.02	B-1 (11/92 Figure

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PROJECT: PARK STREET LANDING Alameda, California

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Log of Boring No. GWS-11 (cont.)

I	SA	MP	LES	_ p		
DEPTI (feet)	Sample No.	Sample	Blows/ Foot	OVM Readir	DESCRIPTION NAME (USCS Symbol): color, moist, % by wt., plast., density, structure, cementation, react. w/HCl, geo. inter.	REMARKS
- 15-				100	SANDY LEAN CLAY (CL) Greenish gray (10Y 5/1), moist, 60% fines, 40% fine to coarse sand, low plasticity, firm	-
- 16 ⁻					CLAYEY SAND (SC) Dark bluish gray (10B 4/1), moist, 70% fine to coarse sand, 30% low plasticity fines, dense	-
- 17-					Bottom of boring at 16 feet bgs	-
- 18 ⁻					· · · · · · · · · · · · · · · · · · ·	-
- 19 -						
20-						-
21-						
22-		-				
23						-
25-						
26-		- 				-
27-		- 				
28-						-
29-						4
30-						4
31-	L			I		B-2 (11/92)
2436.02.0	025				Geomatrix Consultants Project No. 2436	5.02 Figure

PLANTICIAN CAND CATUAL: CREATION AND DATUME: CONTRACTOR: Precision Sampling 42495 42495 42495 Carter Finisher 42495 42495 42495 Constraints 9 16 feet 9 Cited push 10 DEFTH TO 11 Enviro 9 Cited push 12 DESCRIPTION 13 Market WEIGHT: 14 DESCRIPTION 15 SAMPLIES 16 Sampling 17 DESCRIPTION 18 Sampling 19 Market (usc6 symbol): dev. melt. % 19 vr. pail. davie, supervision, next. whol.gen.next. 11 CitAYEY SAND (SC) 12 Data gray (7.5/YR 4/1), molst, 70% fine to coarse sand, 25% iow plasticity fines, 5% rounded and subangular gravel, meduum dansity, glass fragments 11 CitAYEY SAND (SC) 11 Color change to very dark gray (2.5Y 3/1), increase low 11 Color change to very dark gray (2.5Y 3/1), increase low 12 File 13 Color change to very dark gray (2.5Y 3/1), increase low 14 File 14 Color change to very dark gray (2.5Y 3/1), increase low 14	PROJECT: PARK STR	EET LANDING California	Log of Borin	g No. GWS-12
SAMPLES DATE STATED: PALLING CONTRACTOR: Precision Sampling DATE STATED: 424/95 DATE STATED: 424/95 DATE STATED: 424/95 PILLING ECURTRACTOR: Precision Sampling UZ4295 A24/95 HEMSING POINT: 424/95 PILLING ECURTRACTOR: Precision Sampling UZ4295 A24/95 HEMSING POINT: 424/95 PILLING ECURTRACTOR: Precision Sampling UZ4295 A24/95 HEMSING POINT: 424/95 PILLING ECURTRACTOR: Precision Sampling DEFINITION MARE MEDIA PATER 24/95 SAMPLES Barget DESCRIPTION A. L. Spencer PAG. NO ROSTI SAMPLES Barget DESCRIPTION A. L. Spencer No recovery in uppe 2 1/2 feet SAMPLES Barget Surface Elevation: No recovery in uppe 2 1/2 feet CLAYEY SAND (SC) Dark gray (7.5YR 4/1), moist, 70% fine to coarse sand, 25% low plasticity fines, 5% rounded and subangular gravel, medium density, glass fragments No recovery in uppe 2 1/2 feet White "chalky" mottling or inclusions Increase in low plasticity fines to 30% Increase low ULEAN CLAY with SAND (CL) Olive (SY 5/4) with green mottling, moist, 85% fine to coarse sand, 5% low plasticity fines to 20% Increase low Increase sand content to 30% with orange mottling, CLAYEY SAND (SC) Olive (SY 5/4) with green and orange mottling, very moist, 65% fine to coarse sand, 35% low plasticity fines Increase Brater		ong canal - southeast side	ELEVATION AND DATUM: Gravel sidewalk	
SAMPLES 422000 BPTH: DRILLING METHOD: Direct push 122000 BPTH: Environmethod Direct push 122000 BPTH: Direct push COMPL 24 HRS. DRILLING ECUIPMENT: XD-3 DEFTN TO PIRET DEFTN TO DIRECT PIRET COMPL 24 HRS. SAMPLING HERTHOD: Environ Core System S. L. Anich S. L. Anich RESPONSILE PROFESSIONAL: REG. NO AMMEEN WEIHOF: DROP: A. L. Spencer RESPONSILE PROFESSIONAL: REG. NO Sampling Bar and Bar an			DATE STARTED:	DATE FINISHED:
DIRLLING EQUIPMENT: XD-3 DEFTM TO FIREST COMPL. 24 HRS. SAMPLING METHOD: Enviro Core System S.L. Anich S.L. Anich RESONSIBLE PROFESSIONAL: REG. NO AMMER WEIGHT: Image: Some in the second standards DESCRIPTION A.L. Spencer RESONSIBLE PROFESSIONAL: REG. NO SAMPLING METHOD: Environment in the second standards DESCRIPTION REMARKS REMARKS Same in the second standards Surface Elevation: A.L. Spencer REMARKS Same in the second standards Surface Elevation: No recovery in uppe 2 1/2 feet Image: in the second standards Signard standards Signard No recovery in uppe Image: in the second standards Signard Signard No recovery in uppe Image: in the second standards Signard Multie "chalky" motiling or inclusions Image: in the second standards Image: in the second standards Vell_GRADED SAND (SW) Light olive brown (2:SY 5/3), moist, 95% fine to coarse sand, 5% low plasticity fines, loose Image: instructure second standards Image: interm second standards Signard standards Image: instructure second standards Image: inte the second standards Signard standardsta	DRILLING CONTRACTOR	Precision Sampling	TOTAL DEPTH:	MEASURING POINT:
SAMPLING EQUIPMENT: XD-3 WATER WATER	DRILLING METHOD: Dir	ect push	16 feet	COMPL. 24 HRS.
SAMPLING METHOD: Enviro Care System S.L. Ankci. TAMMER WEIGHT: DROP: A.L. Spencer RESPONSIBLE PROFESSIONAL: REG. NO. SAMPLES Market USC3 Symbol: core relative, starty, direct, adapt, distribute, consentation, react, which, pee, hiter. REMARKS Starting Start Market USC3 Symbol: core, relat, "by ut, and,", distructure, consentation, react, which, pee, hiter. REMARKS CLAYEY SAND (SC) Dark gray (7.5YR 4/1), moist, 70%, fine to coarse sand, 25%, tow plasticity fines, 5% founded and subangular gravel, medium density, glass fragments No recovery in uppe 2 1/2 feet Increase in low plasticity fines, 5% rounded and subangular gravel, medium density, glass fragments Increase in low plasticity fines to 30%, White "chalky" mottling or inclusions Note (SY S/4), moist, 95% fine to coarse sand, 25%, low plasticity fines, loose VelLL-GRADED SAND (SW) Light olive brown (2.5Y S/3), moist, 95% fine to coarse sand, 5% low plasticity fines, loose So LEAN CLAY with SAND (CL) Olive (SY S/4) with green mottling, moist, 85% fines, 15%, fine to medium sand, low plasticity, soft Increase sand content to 30% with orange mottling, very moist, 65% fine to coarse sand, 35% low plasticity fines	ORILLING EQUIPMENT:	XD-3	WATER	· · · · · · · · · · · · · · · · · · ·
MAMER WEIGHT: DROP: RESCRIPTION 3	SAMPLING METHOD: E	nviro Core System	S. L. Anich	IONAL PEG NO
SAMPLES By any answer Description 1 MARE (USCS Symee); coor, max, % by at, part, density, struture, ceneration, react, which, gen, inter. REMARKS 1 Surface Elevation; No recovery in uppe 2 CLAYEY SAND (SC) Dark gray (7.5YR 4/1), moist, 70% fine to coarse sand, 25% low plasticity fines, 5% founded and subangular gravel, medium density, glass fragments No recovery in uppe 4 CLAYEY SAND (SC) Dark gray (7.5YR 4/1), moist, 70% fine to coarse sand, 25% low plasticity fines, 5% founded and subangular gravel, medium density, glass fragments Increase in low plasticity fines to 30% 5 WELL-GRADED SAND (SW) Light olive brown (2.5Y 5/3), moist, 95% fine to coarse sand, 5% low plasticity fines, loose 7 7 7 8 Color change to very dark gray (2.5Y 3/1), increase low plasticity fines to 20% 11 50 LEAN CLAY with SAND (CL) 01 Olive (5Y 5/4) with green mottling, moist, 85% fines, 15% fine to medium sand, low plasticity, soft 12 Increase sand content to 30% with orange mottling 13 CLAYEY SAND (SC) 14 CLAYEY SAND (SC) 15 Increase sand content to 30% with orange mottling, very moist, 65% fine to coarse sand, 35% low plasticity fines	HAMMER WEIGHT:	DROP:	A. L. Spencer	RG 5713
3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 1 No recovery in uppe 2 -		DESCRIPT	ION	REMARKS
a a a b a No recovery in uppe 1 CLAYEY SAND (SC) Dark gray (7.5YR 4/1), moist, 70% fine to coarse sand, 25% low plasticity fines, 5% rounded and subangular gravel, medium density, glass fragments - - - 4 - - - - - - - 5 - - - - - - - 6 - - - - - - - - 7 -	(fee ample ample foot foot foot foot foot foot foot foo	NAME (USCS Symbol): color, moist, 76 by wt. plast, certain	ion:	
13 CLAYEY SAND (SC) Olive (5Y 5/4) with green and orange mottling, very moist, 65% fine to coarse sand, 35% low plasticity fines 14	$ \begin{array}{c} - \\ 1 - \\ - \\ 2 - \\ - \\ 3 - \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\$	CLAYEY SAND (SC) Dark gray (7.5YR 4/1), moist, 70% low plasticity fines, 5% rounded a medium density, glass fragments Increase in low plasticity fines to White "chalky" mottling or inclus WELL-GRADED SAND (SW) Light olive brown (2.5Y 5/3), mois 5% low plasticity fines, loose Color change to very dark gray plasticity fines to 20% LEAN CLAY with SAND (CL) Olive (5Y 5/4) with green mottling fine to medium sand, low plasticity Increase sand content to 30% of	6 fine to coarse sand, 25% nd subangular gravel, 0 30% sions st, 95% fine to coarse sand, (2.5Y 3/1), increase low g, moist, 85% fines, 15% ty , soft with orange mottling	2 1/2 feet
14 Broject No. 2436.02 Figure		Olive (5Y 5/4) with green and ora 65% fine to coarse sand, 35% lo	ange mottling, very moist, w plasticity fines	-
			Broject No. 24	B-1 (1 36.02 Figure

PROJECT: PARK Alame	STRE da, C	EET LANDING alifornia	Log of Boring No. GWS-12 (cont.)		
CET IA (feet) Sample Sample Blows/ Foot	OVM Reading	DESCRIF NAME (USCS Symbol): color, moist, % by wt., plast., der	PTION sity, structure, cementation, react. w/HCl, geo. inter.	REMARKS	
		CLAYEY SAND (SC) (continued	(1		
15-		Increase sand content to 80% gray (10GY 5/1)	and color change to greenish	-	
		Bottom of boring at 16 feet bgs		-	
17-					
18-				-	
19-				-	
20-					
21 -					
22-				-	
23-					
24-		1		-	
25 -				-	
26 -				-	
				-	
27 -				-	
28-				-	
29-					
30-				-	
31				B-2 (11)	
		Geomatrix Consultants	Project No. 24	36.02 Figure —	

PROJE	ECT:	P/ Ala	AR am	K S ieda	TRE a, Ca	ET LANDING lifornia	Log of Borin	g No.	GWS-13
BORIN	IG LO		TIC	DN:	Alon	g Blanding Ave., N side of driveway, next to bldg	ELEVATION AND DATUM: Vegetated area		
DBILL	ING		ITF	AC	TOR:	Precision Sampling	DATE STARTED: 4/25/95	DATE FINI 4/25/95 -	SHED: 1045 hrs
OBILL	ING	MET	нс	DD:	Dire	et push	TOTAL DEPTH: 16 feet	MEASURIN Ground s	NG POINT: urface
		FOI				D-3	DEPTH TO FIRST	COMPL.	24 HRS.
CAMP					- Eo	viro Core System	LOGGED BY:		
		WE	GH	 T: .	·	DROP:	RESPONSIBLE PROFESSI	IONAL:	REG. NO.
-	SA	MP	LES	5	2	DESCRIPTION	<u></u>		
EPTF (feet)	nple Vo.	mple	/SMO	ğ	(ppm)	NAME (USCS Symbol): color, moist, % by wt, plast, density, structure, cem	entation, react. w/HCl, geo. inter.	RI	EMARKS
<u> </u>	S. L	l ⁸	Ē	_	<u>a</u>	Surface Elevation:		<u> </u>	
						CLAYEY SAND (SC) Black (2.5Y 2.5/1), orange organic nodules,	very moist,	Did not e petroleur however readings measure recovery 2 1/2 fee	encounter m-like odors; , PID were ed. No r in upper et.
3-						loose	-		
-	1							-	
-						LEAN CLAY (CL) Dark grayish brown (2.5Y 4/2), organic nod nodules), moist, 80-90% fines, 10-20% fine	ules (roots, black - to medium sand, _	-	
-					162	Gravel content to 5% (medium, angular)		4	
- 7						CLAYEY SAND (SC) Dark greenish gray (10GY 4/1), moist, 70% sand, 30% low plasticity fines, dense	fine to coarse -		
-	$\left\{ \right.$				100		ATD	-	
8-]				120	CLAYEY SILT (ML) '	es, 5-10% fine to	-	
9-					120	medium sand, low plasticity, firm	-	-	
10 -					170	Orange mottling and organic nodules, inc	reasing clay content		
11 -					190			-	
- 12 ·					380	CLAYEY SAND (SC) Dark greenish gray (10Y 4/1), moist, 60 % sand, 40% low plasticity fines, including 10 dense	fine to coarse % silt, medium		
13					650	LEAN CLAY (CL) Olive gray (5Y 4/2), moist, 80% fines, 20% sand, low plasticity	fine to coarse	-	
14						Coometrix Congultante	Project No. 2430	6.02	Figure

PROJ	ECT:	P/ Al	ARK ame	STR da, C	EET LANDING alifornia	Log of Boring No.	GWS-13	3 (cont.)
DEPTH (feet)	sample No.	sample M	Blows/ Foot	OVM Reading	DESCRIP NAME (USCS Symbol): color, moist, % by wt., plast., den:	TION sity, structure, cementation, react. w/HCl, geo. inter.	RE	EMARKS
15 ⁻					WELL-GRADED SAND with CLA Dark greenish gray (10GY 4/1), r sand, 40% low plasticity fines, lo Color change to olive brown (2	AY (SW-SC) noist, 90% fine to coarse ose 2.5Y 4/4)	-	
16 [.]		μ			Bottom of boring at 16 feet bgs			
17							-	
18							-	
-19	4							
20								
21								
22								
23								
-24								
25	5-							
26	- 3- 1-							
2	7-							`
2	- в-							
2	- - -9							
3	- -0							
	-]]	B-2 (11/92
3	1					Project No.	2436.02	Figure
2430	3.02.029	 }			Geomatrix Consultants			<u></u>

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PROJECT: PARK STRE	ET LANDING alifornia	Log of Borin	g No. GWS-14	
ROBING LOCATION: Alor	on Blanding Ave., south side of driveway	ELEVATION AND DATUM:		
	Provision Sampling	DATE STARTED:	DATE FINISHED:	
DRILLING CONTRACTOR:	Precision Sampling	4/25/95 TOTAL DEPTH:	MEASURING POINT:	
DRILLING METHOD: Dire	ct push	DEPTH TO FIRST	COMPL. 24 HRS.	
	(D-3	WATER		
SAMPLING METHOD: En	viro Core System	S. L. Anich	ONAL: REG. NO.	
HAMMER WEIGHT:	DROP:	A. L. Spencer	RG 5713	
SAMPLES No. 00 Soot Sample (ppm)	DESCRIPTION NAME (USCS Symbol): color, moist, % by wt., plast, density, struct	ure, cementation, react. w/HCl, geo. inter.	REMARKS	
	Surface Elevation:			
			Did not encounter petroleum-like odors; however, PID readings were measured. No recovery in upper 2 1/2 feet.	
3-	CLAYEY SAND (SC) Reddish black (10R 2.5/1), moist, 60-7 sand, 30-40% low plasticity fines, loose	0% fine to coarse -		
	(10YR 5/3)			
6 -	Light yellowish brown (2.5Y 6/4), moist to coarse sand, 10% fine gravel, low p	t, 60% fines, 30% fine		
7-				
8-	CLAYEY SAND (SC) Greenish gray (5G 5/1) with orange mo organic pockets, moist, 60-70% fine to low plasticity fines, medium dense to c	ottling and black - coarse sand, 30-40% - lense		
	LEAN CLAY with SAND (CL) Olive (5Y 5/3) with orange mottling and pockets (some roots), moist, 80% fine	d black organic s (including silt), 20%	-	
10 271	fine to medium sand, low plasticity, firr	n .		
		모.	-	
	CLAYEY SAND (SC) Olive (5Y 5/6) with orange and black n 60-70% fine to coarse sand, 30-40% h medium dense	nottling, very moist, ow plasticity fines,		
14	<u> </u>		B-1 (11/	
• •	Geomatrix Consultants	Project No. 243	6.02 Figure -	

BAMPLES B </th <th>PROJEC</th> <th>T: P/ Al</th> <th>ARK ame</th> <th>STRE da, Ca</th> <th>EET LANDING alifornia</th> <th colspan="3">Log of Boring No. GWS-14 (cont.)</th> <th>nt.)</th>	PROJEC	T: P/ Al	ARK ame	STRE da, Ca	EET LANDING alifornia	Log of Boring No. GWS-14 (cont.)			nt.)	
3 3 3 4 4 SAMDY LEAN CLAY (CL) Dark greenish gray (5G 3/1), moist, 70% fines, 30% fine to - - 15 - - - - 16 - WELL-GRADED SAND with CLAY (SW-SC) - - 18 - - - - - 18 - - - - - 19 - - - - - 20 - - - - - 19 - - - - - 21 - - - - - 22 - - - - - 23 - - - - - 24 - - - - - - 25 - - - - - - - 25 - - - - - - - - 26 - - -	EPTH feet) nple 00		oot SH	OVM leading	DESCRI NAME (USCS Symbol): color, moist, % by wt., plast., de	PTION nsity, structure, cementation, react. w	//HCI, geo. inter.		REMARKS	
15- Coarse sand, low plasticity. dense WELL-GRADED SAND with CLAY (SW-SC) Olive (6Y 4/3), moist, 300% fine to coarse sand, 10% low plasticity fines, loose Bottom of boring at 16 feet bgs 20- 21- 22- 23- 24- 25- 26- 27- 28- 29- 31- Bound for the coarse sand, 10% low	DE San	Sar N	98 F	æ	SANDY LEAN CLAY (CL) Dark greenish gray (5G 3/1), mo	bist, 70% fines, 30% fi	ne to	-		
16	15- -				coarse sand, low plasticity, der WELL-GRADED SAND with CL Olive (5Y 4/3), moist, 90% fine	ise AY (SW-SC) to coarse sand, 10% lo	w	-		
17- - 18- - 19- - 20- - 21- - 22- - 23- - 24- - 25- - 26- - 27- - 28- - 29- - 30- - 31- - Beomatrix Consultants	16- -				plasticity fines, loose Bottom of boring at 16 feet bgs					
18- - 19- - 20- - 21- - 22- - 23- - 24- - 25- - 26- - 27- - 28- - 29- - 30- - 31- - Beomatrix Consultants Project No. 2438.02 Figure -	17-									
19- - 20- - 21- - 22- - 23- - 24- - 25- - 26- - 27- - 28- - 29- - 30- - 31- - Geomatrix Consultants Project No. 2436.02 Figures -	18-									
20 21 22 23 24 24 25 26 27 28 29 30 30 4 4 5 5 6 6 7 7 8 8 9 9 1 1 1 1 1 1 1 1 1 1 1 1 1	19-									
21-	20-									
22- - 23- - 24- - 25- - 26- - 27- - 28- - 29- - 30- - 31- - B2(IIV B2(IIV B2(IIV	21-							-		
23	22-									
24 - - 25 - - 26 - - 27 - - 28 - - 29 - - 30 - - 31 - - B2(IV B2(IV								-		
20 - 26 - 27 - 28 - 29 - 30 - 31 - B2(117 B2(117	24							-		
27- - 28- - 29- - 30- - 31- - B-2(11/2) Geomatrix Consultants Project No. 2436.02 Figure	26							-		
28 - - 29 - - 30 - - 31 - - Geomatrix Consultants	27 -							-		·
29 -	28-									
30 - - - - 31 - - - - 31 - - - - 31 - - - - 31 - - - -	29-									
31 B-2 (11/ B-2 (11/ B-2 (11/ Geomatrix Consultants Project No. 2436.02 Figure	30 -									
Geomatrix Consultants Project No. 2436.02 Figure										8-2 (11/9
					Geomatrix Consultants		Project No. 24	436.02	Figure –	

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PROJECT: PARK Alame	STRE da, Ca	ET LANDING Ilifornia	Log	of Borin	g No. (GWS-15
BORING LOCATION	: North	n side of propertydriveway	ELEVATIO Asphalt o	N AND DATUM: driveway	<u></u>	
DRILLING CONTRA	CTOR:	Precision Sampling	DATE STA 4/25/95	DATE STARTED: DATE FINISHED: 4/25/95 4/25/95 - 1200 hrs		
DRILLING METHOD	: Direc	ct push	TOTAL DE 16 feet	EPTH:	MEASURIN Ground su	IG POINT: urface
	INT: X	D-3	DEPTH TO WATER	FIRST	COMPL.	24 HRS.
SAMPLING METHO	D: Env	iro Core System	LOGGED S. L. Anio	BY: ch		
HAMMER WEIGHT:	~	DROP:	RESPONS A. L. Spe	SIBLE PROFESSI	ONAL:	REG. NO. RG 5713
H SAMPLES	eading pm)	DESCRIPT NAME (USCS Symbol): color, moist, % by wt., plast., densi	TION ity, structure, cementation, react.	w/HCl, geo. inter.	RE	MARKS
DE Samp No Sam Blow Foc	R OI P OI	Surface Eleval	tion:			
$ \begin{array}{c} - \\ 1 - \\ - \\ 2 - \\ - \\ 3 - \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\$	300 8700 250 122 200	GRAVEL CLAYEY SAND (SC) Very dark grayish brown (10YR 3, coarse sand, 20-30% low plasticit LEAN CLAY with SAND (CL) Black (10YR 2/1), some orange o 60-70% fines (5-10% silt), 30-409 plasticity, soft CLAYEY SAND (SC) Dark yellowish brown (10YR 4/4), 75-85% fine to coarse sand, 15-2 loose to medium dense SANDY LEAN CLAY (CL) Olive (5Y 5/3), moist, 70% fines, 3 low plasticity, firm Decreasing sand content to 209 Black organic nodules, greenist orange mottling	/2), moist, 70-80% f cy fines, loose rganic nodules, moi % fine to coarse sar moist to very moist 5% low plasticity fin 30% fine to coarse s % n gray (5G 5/1) pock	ine to	No recor 2 1/2 fee	very in upper et
-				-		
12 -	+9000					
	1200	Increasing sand content to 30-4 yellowish brown (10YR 5/6)	0%, color change to	-		B.1 /(102
· · ·		Geomatrix Consultants		Project No. 2436.	02 F	Figure

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PROJECT: PARK STREET LANDING Alameda, California

Log of Boring No. GWS-15 (cont.)

_ S	AMP	LES	5				
DEPTH (feet) Sample	No. Sample	Blows/ Foot	OVM Readin	DESCRIPTION NAME (USCS Symbol): color, moist, % by wt., plast., density, structure, cementation, react. w/HCl, geo. ii	nter.		REMARKS
	$\dagger \uparrow$			SANDY LEAN CLAY (CL) (Continued)			
- 15- -		470		CLAYEY SAND (SC) Light olive brown (2.5Y 5/4) black organic nodules, green mottling, moist, 60% fine to coarse sand, 40% low plasticity		-	
16-				Increase sand content to 70-80%	\square		
17-				Bottom of boring at 16 feet bgs		4	
		·				4	
18-						-	
-						- .,	
197							
20-						-	
4							
21							
22-							
23-							
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26 -			•				
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28-							
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30-							
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JI	<u> </u>			Project	No 2	2436.02	B-2
436.02.033				Geomatrix Consultants			

PROJECT: PARK	STRE	ET LANDING lifornia	Log of B	oring	g No. (GWS-16
		drivowov	ELEVATION AND	ATUM:		
BORING LOCATION	: Main	driveway	DATE STARTED:		DATE FINIS	SHED:
DRILLING CONTRA	CTOR:	Precision Sampling	4/25/95 TOTAL DEPTH:		4/25/95 - MEASURIN	1415 hrs IG POINT:
DRILLING METHOD	Direc	t push	21.5 feet	BST	Ground su	urface
DRILLING EQUIPM	ENT: X	D-3	WATER		1	
SAMPLING METHO	D: Env	iro Core System	S. L. Anich			_
HAMMER WEIGHT:		DROP:	RESPONSIBLE PF A. L. Spencer	OFESSIO	DNAL:	REG. NO. RG 5713
H () SAMPLES	(eading pm)	DESCRIPT NAME (USCS Symbol): color, moist, % by wt., plast., density	ION y, structure, cementation, react. w/HCl, geo	inter.	RE	MARKS
Blow No Sam (fc	99	Surface Elevati	on:			· · · · · · · · · · · · · · · · · · ·
$ \begin{array}{c} - \\ 1 - \\ - \\ 2 - \\ - \\ 3 - \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\$	200	GRAVEL CLAYEY SAND (SC) Black (7.5YR 2.5/1), moist, 70% fi low plasticity fines, loose to mediu Increased sand content to 80% SANDY LEAN CLAY (CL) Dark greenish gray (5GY 4/1), mo fine to coarse sand, low plasticity, Orange organic nodules	ne to coarse sand, 30% im dense		No recov 2 1/2 fee	very in upper at
10 - - 11 - -	14	LEAN CLAY with SAND (CL) Olive (5Y 5/4), with green and ora 70-80% fines, 20-30% fine to coat hard	inge mottling, moist, rse sand, low plasticity,			
13	8	WELL-GRADED SAND with CLA Greenish gray (5G 5/1), moist, 85 10-15% low plasticity fines, loose	r (SW-SC) -90% fine to coarse sand, to medium dense	-		
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CLIENT NAME	Chevron Environmental Management Co.	BORING/WELL NAME MW-2
JOB/SITE NAME	Former Signal Oil Bulk Plant 20-6127	DRILLING STARTED 18-Jun-09
LOCATION	2301-2311 Blanding Avenue, Alameda, CA	DRILLING COMPLETED 19-Jun-09
PROJECT NUMBER	631916	WELL DEVELOPMENT DATE (YIELD) 30-Jun-09
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION 10.87 ft above msl
DRILLING METHOD	Direct Push / Hollow-Stem Auger	TOP OF CASING ELEVATION 10.63 ft above msl
BORING DIAMETER	8"	SCREENED INTERVAL 10.5 to 15.5 fbg
LOGGED BY	E. Namba	DEPTH TO WATER (First Encountered) 11.5 fbg (18-Jun-09)
REVIEWED BY	G. Barclay	DEPTH TO WATER (Static) 4.0 fbg (19-Jun-09)
REMARKS	Cleared to 8 fbg with air-knife	

	PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION		CONTACT DEPTH (fbg)	WEL	L DIAGRAM
	0.0					SM		Asphalt Silty SAND with gravel: Brown; dry		.0.5		
	189		MW-2- 4.5		 - 5 	ML SM		Sandy SILT: Grey; dry Silty SAND: Greyish green; dry	_	4.0 5.0 7.0		 Portland Type I/II 2" diam., Schedule 40
	0.0 0.0		MW-2- 7.5 MW-2- 8.5			ML		Sandy SILT with clay: Greyish green with brown; dry; moderate plasticity Grey staining observed				PVC ◄ Bentonite Seal
//26/09	0.0				—10— 			Less grey staining observed Silty SAND with clay: Grey: wet: fine grain: grey staining	<u> </u>	11.5		 Monterey Sand #2/12
DEFAULT.GDT 8	0.0 0.0		MW-2- 13			SM		observed; decreasing clay content with depth				 2"-diam., 0.020" Slotted Schedule 40 PVC
31916-GINT.GPJ	0.0		MW-2- 15.5		_ 15					16.0		Bottom of Boring @ 16 fbg
LEN/DESKTOP/6												
SETTINGS/NAL												
CUMENTS AND												
DG (PID) C:\DO												
MELL LC												PAGE 1 OF 1



CLIENT NAME	Chevron Environmental Management Co.	BORING/WELL NAME MW-3
JOB/SITE NAME	Former Signal Oil Bulk Plant 20-6127	DRILLING STARTED 18-Jun-09
LOCATION	2301-2311 Blanding Avenue, Alameda, CA	DRILLING COMPLETED 19-Jun-09
PROJECT NUMBER_	631916	WELL DEVELOPMENT DATE (YIELD) 30-Jun-09
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION 11.08 ft above msl
DRILLING METHOD	Direct Push / Hollow-Stem Auger	TOP OF CASING ELEVATION 10.72 ft above msl
BORING DIAMETER	8"	SCREENED INTERVAL 13.5 to 18.5 fbg
LOGGED BY	E. Namba	DEPTH TO WATER (First Encountered) 8.5 fbg (18-Jun-09)
REVIEWED BY	G. Barclay	DEPTH TO WATER (Static) 4.8 fbg (19-Jun-09)





CLIENT NAME	Chevron Environmental Management Co.	BORING/WELL NAME MW-4
JOB/SITE NAME	Former Signal Oil Bulk Plant 20-6127	DRILLING STARTED 18-Jun-09
LOCATION	2301-2311 Blanding Avenue, Alameda, CA	DRILLING COMPLETED 19-Jun-09
PROJECT NUMBER	631916	WELL DEVELOPMENT DATE (YIELD) 30-Jun-09
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION 11.65 ft above msl
DRILLING METHOD	Direct Push / Hollow-Stem Auger	TOP OF CASING ELEVATION 11.40 ft above msl
BORING DIAMETER	8"	SCREENED INTERVAL 15.5 to 20.5 fbg
LOGGED BY	E. Namba	DEPTH TO WATER (First Encountered) 17.0 fbg (18-Jun-09)
REVIEWED BY	G. Barclay	DEPTH TO WATER (Static) 6.8 fbg (19-Jun-09)









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BORING/ WELL LOG

CLIENT	NAME	_(Chev	ron En	vironm	ental N	lanagement Co.	BORING/WELL NAME MW-1RA					
JOB/SI	TE NAME	E _	Form	ner Sigr	al Oil I	Bulk Pla	ant (Chevron 20-6127)	DRILLING STARTED	04-Aug-10				
LOCAT	ION		2301	-2311 E	Blandir	ig Aver	uue, Alameda, CA	DRILLING COMPLETED	04-Aug-10				
PROJE	СТ NUM	BER _	6319	916				WELL DEVELOPMENT DATE (YIELD) NA					
DRILLE	R		Pene	ecore				GROUND SURFACE ELEVATION			13.68 ft above msl		
DRILLI			Hollo	w-stem	auger	•		TOP OF CASING ELEVA		13.02	ft above me	sl	
BORING	G DIAME	TER a	8"					SCREENED INTERVALS	_	8 to 13 fbg d) 8.0 fbg (04-Aug-10) ⊻			
LOGGE	DBY		B. Yi	fru				DEPTH TO WATER (First	Encountered				
REVIEV	VED BY		G. B	arclay				DEPTH TO WATER (Stati	c)	NA	4		
REMAR	REMARKS			red to 8	fbg wi	ith Air k	Knife						
PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	LITHO	DLOGIC DESCRIPTION		CONTACT DEPTH (fbg)	WELL	. DIAGRAM	
1,149				 			<u>FILL:</u> concrete trag <u>Sandy SILT with cla</u> fine sand @ 8 fbg: wet	ay: dark grey; moist; low pla	sticity; ⊻	7.5		 Portland Type I/II 2" diam., Schedule 40 PVC Bentonite Seal Monterey Sand #2/12 	
816 305		MW-1R A -S-10		 	ML		@ 10 fbg: greenish (grey				 2"-diam., 0.020" Slotted Schedule 40 	

@ 13 fbg: mottled

SAND with silt: wet

Silty SAND with clay: greenish grey; fine sand

WELL LOG (PID) 1:\CHEVRON\6319--\631916~1\634E63~1\631916-GINT-082010.GPJ DEFAULT.GDT 9/15/10

249

360

49.0

370

4.9

1.1 1.5 0.8 MW-1R A -S-13.5

5

-20

SP

Portland Type I/II

Bottom of Boring @ 20 fbg

14.0

20.0



WELL LOG (PID) I:/CHEVRON/6319--\631916~1\634E63~1\631916-GINT-082010.GPJ DEFAULT.GDT 9/15/10

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CLIENT NAME	Chevron Environmental Management Co.	BORING/WELL NAME	MW-1RB		
JOB/SITE NAME	Former Signal Oil Bulk Plant (Chevron 20-6127)	DRILLING STARTED	04-Aug-10		
LOCATION	2301-2311 Blanding Avenue, Alameda, CA	DRILLING COMPLETED	04-Aug-10		
PROJECT NUMBER	631916	WELL DEVELOPMENT D	ATE (YIELD)	NA	
DRILLER	Penecore	GROUND SURFACE ELE	VATION	13.65 ft above msl	
DRILLING METHOD	Hollow-stem auger	TOP OF CASING ELEVAT		13.21 ft above msl	
BORING DIAMETER	8"	SCREENED INTERVALS	_	16.5 to 20 fbg	
LOGGED BY	B. Yifru	DEPTH TO WATER (First	Encountered) 8.0 fbg (04-Aug-10)	$\overline{\Delta}$
REVIEWED BY	G. Barclay	DEPTH TO WATER (Stati	c)	NA	Ţ
REMARKS	Cleared to 8 fbg with Air Knife; re-installed well, pr	eviously MW-1			

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WEL	LL DIAGRAM
					- - - - - -		Please refer to boring log MW-1RA for lithology.			 2" diam., Schedule 40 PVC Portland Type I/II
				 	-					✓ Bentonite Seal
				 						 Monterey Sand #2/12 2"-diam., 0.020" Slotted Schedule 40
				—20—				20.0		PVC Bottom of Boring @ 20 fbg



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CLIENT NAME	Chevron Environmental Management Co.	BORING/WELL NAME	MW-6		
JOB/SITE NAME	Former Signal Oil Bulk Plant (Chevron 20-6127)	DRILLING STARTED	04-Aug-10		
LOCATION	2301-2311 Blanding Avenue, Alameda, CA	DRILLING COMPLETED	04-Aug-10		
PROJECT NUMBER	631916	WELL DEVELOPMENT D	ATE (YIELD)	NA	
DRILLER	Penecore	GROUND SURFACE ELE	VATION _	13.21 ft above msl	
DRILLING METHOD	Hollow-stem auger	TOP OF CASING ELEVAT	ION _	12.98 ft above msl	
BORING DIAMETER	8"	SCREENED INTERVALS		16.5 to 20 fbg	
LOGGED BY	B. Yifru	DEPTH TO WATER (First	Encountered) 8.0 fbg (04-Aug-10)	$\overline{\Delta}$
REVIEWED BY	G. Barclay	DEPTH TO WATER (Station	c)	NA	Ţ
REMARKS	Cleared to 8 fbg with Air Knife				





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BORING/ WELL LOG

CLIENT NAME	Chevron Environmental Management Co.	BORING/WELL NAME	VP-1		
JOB/SITE NAME	Former Signal Oil Bulk Plant	DRILLING STARTED	09-Jul-08		
LOCATION	2301-2311 Blanding Avenue, Alameda, CA	DRILLING COMPLETED _	09-Jul-08		
PROJECT NUMBER	631916 (20-6127)	WELL DEVELOPMENT DA	TE (YIELD)	NA	
DRILLER	Woodward Drilling Co. Inc.	GROUND SURFACE ELEV	ATION _	NA	
DRILLING METHOD	Hand-Auger/Airknife	TOP OF CASING ELEVAT	ION _	NA	
BORING DIAMETER	3.25 inches	SCREENED INTERVALS	_	3.75 to 4.25 fbg	
LOGGED BY	C. Benedict	DEPTH TO WATER (First	Encountered) NA	$\underline{\nabla}$
REVIEWED BY	J. Kiernan, PE# C68498	DEPTH TO WATER (Statio)	NA	Ţ

REMARKS

WELL LOG (PID) NRAC-S1\SHARED\CHEVRON6319-\631916~1\632941~1\BORING~1\20-6127 BORING LOGS.GPJ DEFAULT.GDT 7/9/09

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WEL	LL DIAGRAM
		VP-1- 3			SM		Asphalt Silty SAND with gravelBrown; dry; 45% sand, 25% silt, 15% clay, 15% coarse gravel; low plasticity; 1/2-3/4 inch subangular pebbles. Silty GRAVEL with sandBrown; dry; 45% gravel, 30% sand, 15% silt, 10% clay; low plasticity. Clayey GRAVEL with sandBrown; dry; 60% gravel, 20% clay, 10% silt, 10% sand; low plasticity.	0.5 0.5 4.0 4.5		 Concrete Portland Type I/II 1/4"-inner diam. Nylaflow® tubing Bentonite Seal Monterey Sand #3 1"-diam., 0.020" Slotted Schedule 40 PVC Bottom of Boring @ 4.5 fbg



REMARKS

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BORING/ WELL LOG

CLIENT NAME	Chevron Environmental Management Co.	BORING/WELL NAME	VP-2		
JOB/SITE NAME	Former Signal Oil Bulk Plant	DRILLING STARTED	09-Jul-08		
LOCATION	2301-2311 Blanding Avenue, Alameda, CA	DRILLING COMPLETED	09-Jul-08		
PROJECT NUMBER	631916 (20-6127)	WELL DEVELOPMENT DAT	TE (YIELD)_	NA	
DRILLER	Woodward Drilling Co. Inc.	GROUND SURFACE ELEV	ATION _	NA	
DRILLING METHOD	Hand-Auger/Airknife	TOP OF CASING ELEVATION	ON	NA	
BORING DIAMETER	3.25 inches	SCREENED INTERVALS		4.25 to 4.75 fbg	
LOGGED BY	C. Benedict	DEPTH TO WATER (First E	ncountered) NA	Ā
REVIEWED BY	J. Kiernan, PE# C68498	DEPTH TO WATER (Static)		NA	Ţ

CONTACT DEPTH (fbg) SAMPLE ID GRAPHIC LOG PID (ppm) BLOW COUNTS EXTENT U.S.C.S. DEPTH (fbg) LITHOLOGIC DESCRIPTION WELL DIAGRAM Asphalt Concrete 0.5 Silty SAND Brown; dry; 45% sand, 35% silt, 20% clay; low plasticity. Portland Type I/IISM 1/4"-inner diam. Nylaflow® 2.0 tubing CLAY with sand :Brown; dry; 45% clay, 30% silt, 25% sand; medium plasticity. Bentonite Seal CL VP-2-3 4.0 Silty SAND :Brown; moist; 55% sand, 30% silt, 15% Monterey Sand #3 clay; low plasticity. 1"-diam., 0.020" Slotted Schedule 40 SM 649 VP-2-5 5.0 PVC 5 Bottom of Boring @ 5 fbg



REMARKS

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BORING/ WELL LOG

CLIENT NAME	Chevron Environmental Management Co.		/P-3		
JOB/SITE NAME	Former Signal Oil Bulk Plant	DRILLING STARTED 1	4-Jul-08		
LOCATION	2301-2311 Blanding Avenue, Alameda, CA	DRILLING COMPLETED 1	4-Jul-08		
PROJECT NUMBER	631916 (20-6127)	WELL DEVELOPMENT DAT	E (YIELD)	NA	
DRILLER	Woodward Drilling Co. Inc.	GROUND SURFACE ELEVA	TION _	NA	
DRILLING METHOD	Hand-Auger/Airknife	TOP OF CASING ELEVATIO	N _	NA	
BORING DIAMETER	3.25 inches	SCREENED INTERVALS	_	5.25 to 5.75 fbg	
LOGGED BY	B. Campbell	DEPTH TO WATER (First Er	ncountered) NA	$\underline{\nabla}$
REVIEWED BY	J. Kiernan, PE# C68498	DEPTH TO WATER (Static)		NA	Ţ

CONTACT DEPTH (fbg) SAMPLE ID PID (ppm) GRAPHIC LOG BLOW COUNTS EXTENT U.S.C.S. DEPTH (fbg) LITHOLOGIC DESCRIPTION WELL DIAGRAM Asphalt Concrete 0.5 **<u>GRAVEL with sand</u>**Brown; dry; 60% gravel, 30% sand, 5% clay, 5% silt; low plasticity. Portland Type I/IIGW 1/4"-inner diam. Nylaflow® 2.0 tubing Silty SAND with gravel Dark brown; moist; 30% sand, 30% silt, 30% gravel,10% clay; low-medium plasticity. VP-3- 2.5 1.5 Bentonite Seal SP 5.0 5 Silty SAND with clay Dark brown; moist; 40% sand, 35% silt, 25% clay; medium plasticity. VP-3- 5 4.5 Monterey SM Sand #3 5.5 CLAY: Grey; moist; 55% clay, 35% silt, 25% clay; medium plasticity. 1"-diam., 0.020" Slotted Schedule 40 CL 6.0 PVC Bottom of Boring @ 6 fbg



REMARKS

WELL LOG (PID) NRAC-S1/SHARED/CHEVRON/6319-/631916-1/632941-1/BORING-1/20-6127 BORING LOGS.GPJ DEFAULT.GDT 7/9/09

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BORING/ WELL LOG

CLIENT NAME	Chevron Environmental Management Co.	BORING/WELL NAME	VP-4		
JOB/SITE NAME	Former Signal Oil Bulk Plant	DRILLING STARTED	14-Jul-08		
LOCATION	2301-2311 Blanding Avenue, Alameda, CA	DRILLING COMPLETED	14-Jul-08		
PROJECT NUMBER	631916 (20-6127)	WELL DEVELOPMENT DA	TE (YIELD)	NA	
DRILLER	Woodward Drilling Co. Inc.	GROUND SURFACE ELEV	ATION _	NA	
DRILLING METHOD	Hand-Auger/Airknife	TOP OF CASING ELEVATI	ON _	NA	
BORING DIAMETER	3.25 inches	SCREENED INTERVALS	_	5.25 to 5.75 fbg	
LOGGED BY	B. Campbell	DEPTH TO WATER (First B	Encountered) NA	$\underline{\nabla}$
REVIEWED BY	J. Kiernan, PE# C68498	DEPTH TO WATER (Static)	NA	Ţ

CONTACT DEPTH (fbg) SAMPLE ID GRAPHIC LOG PID (ppm) BLOW COUNTS EXTENT U.S.C.S. DEPTH (fbg) LITHOLOGIC DESCRIPTION WELL DIAGRAM Asphalt Concrete 0.5 Silty GRAVEL with sand Brown; dry; 45% gravel, 40% sand, 10% silt, 5% clay; low plasticity. Portland Type I/IIGM 1/4"-inner diam. Nylaflow® 2.0 tubing <u>Silty SAND with clay:</u>Brown; moist; 40% sand, 35% silt, 25% clay; medium plasticiy. VP-4- 2.5 121 SM Bentonite Seal 4.5 <u>CLAY:</u> Brown; moist; 50 % clay, 30% sand, 20% silt; medium plasticity. 5 408 VP-4- 5 Monterey CL Sand #3 1"-diam., 0.020" Slotted Schedule 40 6.0 PVC Bottom of Boring @ 6 fbg

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BORING/ WELL LOG

CLIENT NAME	Chevron Environmental Management Co.	BORING/WELL NAME	VP-5		
JOB/SITE NAME	Former Signal Oil Bulk Plant	DRILLING STARTED	14-Jul-08		
LOCATION	2301-2311 Blanding Avenue, Alameda, CA	DRILLING COMPLETED	14-Jul-08		
PROJECT NUMBER	631916 (20-6127)	WELL DEVELOPMENT DAT	re (YIELD)_	NA	
DRILLER	Woodward Drilling Co. Inc.	GROUND SURFACE ELEVA	ATION _	NA	
DRILLING METHOD	Hand-Auger/Airknife	TOP OF CASING ELEVATION	ON _	NA	
BORING DIAMETER	3.25 inches	SCREENED INTERVALS	_	5.25 to 5.75 fbg	
LOGGED BY	B. Campbell	DEPTH TO WATER (First E	ncountered) NA	$\underline{\nabla}$
REVIEWED BY	J. Kiernan, PE# C68498	DEPTH TO WATER (Static)		NA	Ţ

REMARKS

WELL LOG (PID) I/RaC-S1/SHARED/CHEVRON/6319-/631916~1/632941-1/BORING~1/20-6127 BORING LOGS.GPJ DEFAULT.GDT 7/9/09

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WEL	L DIAGRAM
							Asphalt <u>Silty GRAVEL with sand</u> Brown; dry; 45% gravel, 40% sand, 10% silt, 5% clay; low plasticity.	0.5		Concrete Portland Type
45		VP-5- 2.5			GM	$\begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} $				 Interpretation of the second se
								4.0		 Bentonite Seal
				5	CL		CLAY with sand Brown; moist; 55% clay, 25% silt, 10% sand, 10% gravel; medium plasticity.	5.0		
566		VP-5- 5			CL		CLAY with sand :Brown; moist; 50% clay, 20% silt, 30% sand; medium plasticity.	6.0		 Monterey Sand #3 1"-diam., 0.020" Slotted Schedule 40 PVC
										Bottom of Boring @ 6 fbg



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BORING/ WELL LOG

CLIENT NAME	Chevron Environmental Management Co.	BORING/WELL NAME	VP-6		
JOB/SITE NAME	Former Signal Oil Bulk Plant	DRILLING STARTED	09-Jul-08		
LOCATION	2301-2311 Blanding Avenue, Alameda, CA	DRILLING COMPLETED _	09-Jul-08		
PROJECT NUMBER	631916 (20-6127)	WELL DEVELOPMENT DA	TE (YIELD)	NA	
DRILLER	Woodward Drilling Co. Inc.	GROUND SURFACE ELEV	ATION _	NA	
DRILLING METHOD	Hand-Auger/Airknife	TOP OF CASING ELEVAT	ION _	NA	
BORING DIAMETER	3.25 inches	SCREENED INTERVALS	_	5.25 to 5.75 fbg	
LOGGED BY	C. Benedict	DEPTH TO WATER (First	Encountered) NA	$\underline{\nabla}$
REVIEWED BY	J. Kiernan, PE# C68498	DEPTH TO WATER (Static)	NA	Ţ

REMARKS

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WEL	L DIAGRAM
3.2	BLC	UWES			GM		Asphalt Silty GRAVEL with sand Brown; dry; 45% gravel, 40% sand, 10% silt, 5% clay; low plasticity; 1-10 inch conrete fragments. CLAY with sand:Brown; moist; 55% clay, 25% silt, 10% sand, 10% gravel; medium plasticity. Sandy CLAY:Brown; moist; 50% clay, 20% silt, 30% sand; medium plasticity.	0.5 3.5 5.0 6.0		 Concrete Portland Type I/II 1/4"-inner diam. Nylaflow® tubing Bentonite Seal Monterey Sand #3 1"-diam., 0.020" Slotted Schedule 40 PVC Bottom of Boring @ 6 fbg
									PAGE	1 OF 1

APPENDIX D

CUMULATIVE GROUNDWATER TABLES

					HYDROCARBONS PRIMARY VOCS						CS	
Location	Date	тос	DTW	GWE	TPH-DRO	TPH-DRO w/Si Gel	TPH-GRO	В	Т	Е	X	MTBE by SW8260
	Units	ft	ft	ft-amsl	µg/L	µg∕L	µg∕L	µg/L	µg∕L	µg/L	µg/L	µg/L
MW-1 MW-1	07/21/2010 10/22/2010 ¹	13.49 13.49	9.47 -	4.02	440 -	-	65 J -	<0.5 -	<0.5 -	<0.5 -	<0.5 -	<0.5 -
MW-1RA	10/28/2010	13.02	9.23	3.79	-	4,000	6,400	830	22	65	20	-
MW-1RA	01/14/2011	13.02	7.20	5.82	-	1,500	790	160	2	1	1	-
MW-1RA	4/19/2011	13.02	7.46	5.56	-	3,000	3,800	600	9	18	9	-
MW-1RA	6/30/2011	13.02	7.51	5.51	-	3,700	6,800	780	13	36	13	-
MW-1RB MW-1RB MW-1RB	10/28/2010 01/14/2011 4/19/2011	13.21 13.21 13.21	9.00 10.97 12.11	4.21 2.24 1.10	- -	1,600 960 1,200	650 150 190	3 1 6	<0.5 <0.5 <0.5	0.8 <0.5 <0.5	<0.5 <0.5 <0.5	- -
MW-1RB	6/30/2011	13.21	11.86	1.35	-	1,900	310	9	<0.5	<0.5	<0.5	-
MW-2 MW-2	07/21/2010 10/22/2010	10.63 10.63	4.12 4.31	6.51 6.32	65 J -	- 58	<50 <50	<0.5 <0.5	<0.5 <0.5	<0.5 <0.5	<0.5 <0.5	-
MW-2	10/28/2010 ²	10.63	3.65	6.98	-	-	-	-	-	-	-	-
MW-2	01/14/2011	10.63	3.12	7.51	-	68	<50	< 0.5	<0.5	< 0.5	< 0.5	-
MW-2	4/19/2011	10.63	3.51	7.12	-	<50	<50	< 0.5	<0.5	< 0.5	< 0.5	-
MW-2	6/30/2011	10.63	3.74	6.89	-	120	<50	<0.5	<0.5	<0.5	<0.5	-

					Н	YDROCARBON	IS	PRIMARY VOCS				
Location	Date	тос	DTW	GWE	IPH-DRO	IPH-DRO w∕ Si Gel	IPH-GRO	В	Т	Ε	X	MTBE by SW8260
	Units	ft	ft	ft-amsl	µg∕L	µg∕L	µg∕L	µg∕L	µg∕L	µg∕L	µg∕L	µg/L
MW-3	07/21/2010	10.72	5.09	5.63 5.40	640	-	65 J	0.6 J	<0.5	<0.5	<0.5	-
MW 3	10/22/2010 $10/28/2010^2$	10.72	4.74	5.98	-	570	75	N 0.5	<0.5	<0.5	N 0.5	-
MW-3	01/14/2011	10.72	4.11	6.61	-	1.000	91	< 0.5	< 0.5	< 0.5	< 0.5	-
MW-3	4/19/2011	10.72	5.03	5.69	-	1,200	180	< 0.5	< 0.5	< 0.5	< 0.5	-
MW-3	6/30/2011	10.72	4.97	5.75	-	740	<50	<0.5	<0.5	<0.5	<0.5	-
MW-4	07/21/2010	11.40	6.72	4.68	<50	-	<50	<0.5	<0.5	<0.5	<0.5	-
MW-4	10/22/2010	11.40	6.87	4.53	-	91	<50	< 0.5	<0.5	< 0.5	< 0.5	-
MW-4	10/28/2010 ²	11.40	6.38	5.02	-	-	-	-	-	-	-	-
MW-4	01/14/2011	11.40	5.32	6.08	-	<50	<50	< 0.5	<0.5	< 0.5	< 0.5	-
MW-4	4/19/2011	11.40	7.65	3.75	-	<50	<50	<0.5	<0.5	<0.5	< 0.5	-
MW-4	6/30/2011	11.40	6.93	4.47	-	<50	<50	<0.5	<0.5	<0.5	<0.5	-
MW-5	07/21/2010	10.50	5.76	4.74	2,000	-	1,500	80	2	1	2	-
MW-5	10/22/2010	10.50	5.94	4.56	-	1,500	830	47	<0.5	1	< 0.5	-
MW-5	10/28/2010 ²	10.50	5.17	5.33	-	-	-	-	-	-	-	-
MW-5	01/14/2011	10.50	4.40	6.10	-	1,800	2,100	61	4	1	6	-
MW-5	4/19/2011	10.50	5.69	4.81	-	2,000	2,200	73	4	1	6	-

					Н	HYDROCARBONS				CS		
Location	Date	тос	DTW	GWE	TPH-DRO	TPH-DRO w/ Si Gel	TPH-GRO	В	Т	Е	X	MTBE by SW8260
	Units	ft	ft	ft-amsl	µg∕L	µg/L	µg∕L	µg∕L	µg∕L	µg∕L	µg∕L	µg∕L
MW-5	6/30/2011	10.50	5.82	4.68	-	3,200	2,900	99	6	1	7	-
MW-6	10/28/2010	12.98	8.35	4.63	-	300	620	7	< 0.5	1	2	-
MW-6	01/14/2011	12.98	7.58	5.40	-	560	120	3	< 0.5	<0.5	< 0.5	-
MW-6	4/19/2011	12.98	9.90	3.08	-	590	240	7	< 0.5	<0.5	<0.5	-
MW-6	6/30/2011	12.98	9.97	3.01	-	640	200	3	<0.5	<0.5	<0.5	-
QA	07/21/2010	-	-	-	-	-	<50	<0.5	<0.5	<0.5	<0.5	<0.5
QA	10/22/2010	-	-	-	-	-	<50	< 0.5	< 0.5	< 0.5	<0.5	<0.5
QA	10/28/2010	-	-	-	-	-	<50	< 0.5	< 0.5	< 0.5	<0.5	-
QA	01/14/2011	-	-	-	-	-	<50	< 0.5	< 0.5	< 0.5	<0.5	-
QA	4/19/2011	-	-	-	-	-	<50	< 0.5	< 0.5	< 0.5	< 0.5	-
QA	6/30/2011											

Abbreviations and Notes:

TOC = Top of Casing

DTW = Depth to Water

GWE = Groundwater elevation

(ft-amsl) = Feet Above Mean sea level

					HYDROCARBONS			PRIMARY VOCS				
Location	Date	тос	DTW	GWE	TPH-DRO	TPH-DRO w/ Si Gel	TPH-GRO	В	Т	Ε	X	MTBE by SW8260
	Units	ft	ft	ft-amsl	µg/L	µg∕L	µg/L	µg∕L	µg∕L	µg∕L	µg∕L	µg∕L

ft = Feet

 μ g/L = Micrograms per Liter

TPH-DRO = Total Petroleum Hydrocarbons - Diesel Range Organics

TPH-GRO = Total Petroleum Hydrocarbons - Gasoline Range Organics

B = Benzene

T = Toluene

E = Ethylbenzene

X = Xylene

MTBE = Methyl tert butyl ether

-- = Not available / not applicable

<x = Not detected above laboratory method detection limit

- * TOC elevations for all wells were surveyed on July 30, 2009, by Morrow Surveying. Vertical Datum is NAVD 88 from GPS observations. TOC elevations were surveyed on January 25, 2001, by Virgil Chacez Land Surveying. The benchmark used for the survey was a City of Alameda benchmark being a cut square at the centerline return, south corner of Oak and Blanding, (Benchmark Elevation = 8.236 feet, NGVD 29).
- ¹ Destroyed and re-installed as MW-1RB.
- ² Monitored only for the 10/28/10 Special Event

WELL ID/	TOC*	DTW	GWE	TPH-DRO	TPH-GRO	B	Т	Е	X	MTBE
DATE	(ft.)	(ft.)	(msl)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)
MW-1										
01/23/011		7.16		$1,100^{2,3}$	$5,210^4$	868	<50.0	<50.0	<50.0	<250
04/09/01	10.62	8.12	2.50	$1,200^{6}$	3,000 ⁵	920	<20	<20	<20	<100
07/30/01	10.62	9.15	1.47	550 ^{3,8}	$2,000^7$	730	13	<5.0	<5.0	<25
10/08/01	10.62	7.86	2.76	$2,200^{9}$	1,200	120	2.4	5.9	6.4	<2.5
01/13/02	10.62	7.02	3.60	$3,300^3$	930	320	0.78	0.87	3.8	<2.5
04/08/02	10.62	9.60	1.02	$1,200^3$	960	50	1.4	2.6	9.0	<2.5
07/31/02	10.62	9.27	1.35	$2,800^3$	930	64	1.4	1.9	11	<5.0
10/15/02	10.62	8.00	2.62	$1,000^3$	620	25	0.78	1.4	4.3	<2.5
01/14/03	10.62	7.05	3.57	960 ³	1,600	20	1.3	1.3	<1.5	<2.5
04/15/03	10.62	8.02	2.60	920^{3}	870	56	1	1.4	3.1	<2.5
07/16/03 ¹⁰	10.62	10.08	0.54	$1,400^3$	780	85	1	0.8	0.7	< 0.5
10/18/03 ¹⁰	10.62	8.51	2.11	$1,200^3$	640	42	0.8	<0.5	0.5	< 0.5
01/22/04 ¹⁰	10.62	8.95	1.67	$1,500^{3}$	440	18	< 0.5	<0.5	< 0.5	< 0.5
04/23/04 ¹⁰	10.62	8.95	1.67	$2,200^3$	410	10	< 0.5	<0.5	< 0.5	< 0.5
07/23/04 ¹⁰	10.62	9.21	1.41	$1,800^{3}$	400	6	< 0.5	<0.5	< 0.5	< 0.5
10/22/04 ¹⁰	10.62	8.36	2.26	$2,200^3$	150	2	< 0.5	<0.5	< 0.5	< 0.5
01/28/05 ¹⁰	10.62	7.09	3.53	$1,200^3$	55	8	< 0.5	<0.5	< 0.5	< 0.5
04/26/05 ¹⁰	10.62	7.84	2.78	480^{3}	<50	5	< 0.5	<0.5	< 0.5	< 0.5
07/15/05 ¹⁰	10.62	8.12	2.50	$610^{3,11}$	<50	< 0.5	< 0.5	<0.5	< 0.5	< 0.5
10/14/05 ¹⁰	10.62	8.07	2.55	920 ^{3,12}	<50	10	< 0.5	<0.5	< 0.5	< 0.5
01/12/06 ¹⁰	10.62	6.98	3.64	960 ^{3,12}	<50	6	< 0.5	<0.5	< 0.5	< 0.5
04/13/06 ¹⁰	10.62	7.04	3.58	$1,200^3$	<50	< 0.5	< 0.5	<0.5	< 0.5	< 0.5
07/13/06 ¹⁰	10.62	7.13	3.49	$1,200^{3}$	92	14	< 0.5	<0.5	< 0.5	< 0.5
10/17/06 ¹⁰	10.62	7.64	2.98	990 ³	<50	3	< 0.5	<0.5	< 0.5	< 0.5
01/16/07 ¹⁰	10.62	7.09	3.53	840^{3}	83	4	< 0.5	<0.5	< 0.5	< 0.5
04/17/07 ¹⁰	10.62	7.11	3.51	$1,200^3$	57	< 0.5	< 0.5	<0.5	< 0.5	< 0.5
07/17/07 ¹⁰	10.62	7.41	3.21	$1,100^{3}$	120	8	< 0.5	<0.5	< 0.5	< 0.5
10/16/07 ¹⁰	10.62	7.55	3.07	750^{3}	<50	< 0.5	< 0.5	<0.5	< 0.5	< 0.5
01/16/08 ¹⁰	10.62	6.98	3.64	$1,700^{3}$	<50	< 0.5	< 0.5	<0.5	< 0.5	< 0.5
04/16/08 ¹⁰	10.62	7.36	3.26	$1,100^{3}$	62	<0.5	<0.5	<0.5	<0.5	<0.5
07/16/08 ¹⁰	10.62	7.89	2.73	580^{3}	93	3	<0.5	<0.5	<0.5	<0.5
10/15/08 ¹⁰	10.62	7.46	3.16	740^{3}	56	0.7	< 0.5	< 0.5	0.8	<0.5

WELL ID/	TOC*	DTW	GWE	TPH-DRO	TPH-GRO	В	Т	E	x	MTBE
DATE	(ft.)	(ft.)	(msl)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)
MW-1 (cont)										
$01/21/09^{10}$	10.62	7.19	3.43	390^{3}	<50	<0.5	< 0.5	<0.5	< 0.5	< 0.5
04/15/09 ¹⁰	10.62	6.93	3.69	1.400^{3}	80	0.7	< 0.5	<0.5	< 0.5	< 0.5
07/03/09 ¹⁰	13.49	8.08	5.41	$1,300^{3}$	51	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5
10/01/09 ¹⁰	13.49	9.52	3.97	$1,500^{3}$	86	<0.5	< 0.5	< 0.5	< 0.5	< 0.5
01/19/10 ¹⁰	13.49	7.64	5.85	340 ^{3,15}	<50	<0.5	< 0.5	< 0.5	< 0.5	< 0.5
04/26/10¹⁰	13.49	9.20	4.29	820 ³	66	<0.5	<0.5	<0.5	<0.5	<0.5
MW-2										
06/30/09 ¹	10.63	3.80	6.83							
07/03/09 ¹⁴	10.63	3.91	6.72	< 50 ³	<50	< 0.5	< 0.5	< 0.5	<0.5	
10/01/09 ¹⁴	10.63	4.11	6.52	< 50 ³	<50	< 0.5	< 0.5	< 0.5	<0.5	
01/19/10 ¹⁴	10.63	3.90	6.73	< 50 ³	<50	<0.5	< 0.5	< 0.5	<0.5	
04/26/10¹⁴	10.63	4.08	6.55	< 50 ³	<50	<0.5	<0.5	<0.5	<0.5	
MXX/ 2										
MW-3	10.72	4.61	6 11							
06/30/09	10.72	4.01	6.15	1703						
07/03/09 10/01/00 ¹⁴	10.72	4.37	5.50	170	52	-0.5	<0.5	<0.5	<0.5	
10/01/09	10.72	J.22 1 81	5.88	1,000	120	<0.5 2	<0.5	<0.5	<0.5	
04/26/10 ¹⁴	10.72 10.72	4.86	5.86	1,800 1,700 ³	120 170	2	< 0.5	< 0.5	< 0.5	
MW-4										
06/30/09 ¹	11.40	6.02	5.38							
07/03/09 ¹⁴	11.40	5.85	5.55	<50 ³	<50	<0.5	< 0.5	< 0.5	<0.5	
10/01/09 ¹⁴	11.40	6.95	4.45	370^{3}	<50	<0.5	< 0.5	< 0.5	<0.5	
01/19/10 ¹⁴	11.40	6.22	5.18	110^{3}	<50	<0.5	< 0.5	< 0.5	<0.5	
04/26/10¹⁴	11.40	6.61	4.79	210^{3,17}	<50	<0.5	<0.5	<0.5	<0.5	

WELL ID/	TOC*	DTW	GWE	TPH-DRO	TPH-GRO	В	Т	E	X	MTBE
DATE	(ft.)	(ft.)	(msl)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)
MW-5										
06/30/09 ¹	10.50	5.20	5.30							
07/03/09 ¹⁴	10.50	5.17	5.33	110^{3}	930	33	2	0.6	3	
10/01/09 ¹⁴	10.50	5.66	4.84	2.500^{3}	1,800	57	3	0.9	5	
$01/19/10^{14}$	10.50	5.48	5.02	2.600^{3}	2,200	74	4	1	5	
04/26/10 ¹⁴	10.50	5.91	4.59	1,700³	2,200	94	4	2	5	
CS-2										
07/30/01				$140^{3,5}$	<50	<0.50	<0.50	<0.50	<0.50	<2.5
10/08/01				53 ⁹	<50	<0.50	<0.50	<0.50	<1.5	<2.5
01/13/02				$< 50^{3}$	<50	<0.50	<0.50	<0.50	<1.5	<2.5
04/08/02				77^{3}	<50	<0.50	< 0.50	<0.50	<1.5	<2.5
07/31/02				$< 50^{3}$	<50	< 0.50	< 0.50	< 0.50	<1.5	<2.5
10/15/02				$< 50^{3}$	<50	<0.50	< 0.50	< 0.50	<1.5	<2.5
01/14/03				$< 50^{3}$	<50	<0.50	< 0.50	< 0.50	<1.5	<2.5
04/15/03				$<50^{3}$	<50	<0.5	<0.5	<0.5	<1.5	<2.5
07/16/03 ¹⁰				$<50^{3}$	<50	< 0.5	0.7	<0.5	0.6	< 0.5
10/18/03 ¹⁰				< 50 ³	<50	<0.5	< 0.5	<0.5	<0.5	<0.5
01/22/04 ¹⁰				< 50 ³	<50	<0.5	< 0.5	<0.5	<0.5	<0.5
04/23/04 ¹⁰				< 50 ³	<50	<0.5	< 0.5	<0.5	<0.5	<0.5
07/23/04 ¹⁰				< 50 ³	<50	<0.5	< 0.5	<0.5	< 0.5	<0.5
10/22/04 ¹⁰				$< 50^{3}$	<50	<0.5	< 0.5	<0.5	<0.5	< 0.5
01/28/05 ¹⁰				$<50^{3}$	<50	<0.5	< 0.5	<0.5	<0.5	<0.5
04/26/05 ¹⁰				< 50 ³	<50	<0.5	< 0.5	<0.5	<0.5	<0.5
07/15/05 ¹⁰				$< 50^{3}$	<50	<0.5	< 0.5	<0.5	<0.5	< 0.5
10/14/05 ¹⁰				< 50 ³	<50	< 0.5	< 0.5	< 0.5	<0.5	< 0.5
01/12/06 ¹⁰				< 50 ³	<50	<0.5	< 0.5	<0.5	< 0.5	< 0.5
04/13/06 ¹⁰				< 50 ³	<50	< 0.5	<0.5	<0.5	< 0.5	< 0.5
07/13/06 ¹⁰				140^{3}	<50	< 0.5	<0.5	< 0.5	<0.5	< 0.5
10/17/06 ¹⁰				< 50 ³	<50	<0.5	<0.5	<0.5	< 0.5	<0.5
01/16/07 ¹⁰				< 50 ³	<50	<0.5	<0.5	<0.5	< 0.5	< 0.5
04/17/07 ¹⁰				< 50 ³	<50	< 0.5	< 0.5	<0.5	<0.5	< 0.5

WELL ID/ DATE	TOC*	DTW	GWE (msl)	TPH-DRO	TPH-GRO	B (ug/I)	T (ug/I.)	E (µg/I)	X (µg/I)	MTBE
	0)	0	(11131)	(#8/12)	(#8/12)	(#5/2)	(#5/12)	(#5/=/	(#5/=)	(#8/12)
CS-2 (cont)				2						
07/17/07 ¹⁰				<503	<50	<0.5	<0.5	<0.5	<0.5	<0.5
10/16/07 ¹⁰				<503	<50	<0.5	<0.5	<0.5	<0.5	<0.5
01/16/0810				853	<50	<0.5	<0.5	<0.5	<0.5	<0.5
04/16/0810				<50°	<50	<0.5	<0.5	<0.5	<0.5	<0.5
07/16/08 ¹⁰				<503	<50	<0.5	<0.5	<0.5	<0.5	<0.5
10/15/08 ¹⁰				<503	<50	<0.5	<0.5	<0.5	<0.5	<0.5
$01/21/09^{10}$				$<50^{3}$	<50	<0.5	< 0.5	<0.5	<0.5	<0.5
04/15/09 ¹⁰				86 ³	<50	< 0.5	<0.5	< 0.5	< 0.5	< 0.5
07/03/09 ¹⁰				<50 ³	<50	< 0.5	< 0.5	<0.5	<0.5	<0.5
10/01/09 ¹⁰				< 50 ³	<50	< 0.5	< 0.5	<0.5	<0.5	<0.5
01/19/10 ¹⁰				210 ^{3,16}	<50	<0.5	<0.5	<0.5	<0.5	<0.5
TRIP BLANK										
TB-LB										
01/23/01					<50.0	< 0.500	< 0.500	< 0.500	< 0.500	<2.50
04/09/01					<50	< 0.50	< 0.50	< 0.50	< 0.50	<2.5
07/30/01					<50	< 0.50	< 0.50	< 0.50	< 0.50	<2.5
OA										
10/08/01					<50	< 0.50	< 0.50	< 0.50	<1.5	<2.5
01/13/02					<50	< 0.50	< 0.50	< 0.50	<1.5	<2.5
04/08/02					<50	< 0.50	< 0.50	< 0.50	<1.5	<2.5
07/31/02					<50	< 0.50	< 0.50	< 0.50	<1.5	<2.5
10/15/02					<50	< 0.50	< 0.50	< 0.50	<1.5	<2.5
01/14/03					<50	< 0.50	< 0.50	< 0.50	<1.5	<2.5
04/15/03					<50	< 0.5	<0.5	<0.5	<1.5	<2.5
$07/16/03^{10}$					<50	< 0.5	<0.5	< 0.5	< 0.5	< 0.5
10/18/03 ¹⁰					<50	<0.5	<0.5	<0.5	<0.5	<0.5
$01/22/04^{10}$					<50	<0.5	<0.5	<0.5	<0.5	<0.5
$04/23/04^{10}$					<50	<0.5	<0.5	<0.5	<0.5	<0.5
$07/23/04^{10}$					<50	<0.5	<0.5	<0.5	<0.5	<0.5
$10/22/04^{10}$					<50	<0.5	< 0.5	<0.5	<0.5	<0.5

WELL ID/	TOC*	DTW	GWE	TPH-DRO	TPH-GRO	В	Т	Е	x	MTBE
DATE	(ft.)	(ft.)	(msl)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)
OA (cont)										
01/28/05 ¹⁰					<50	< 0.5	< 0.5	< 0.5	<0.5	< 0.5
04/26/05 ¹⁰					<50	< 0.5	< 0.5	< 0.5	<0.5	< 0.5
07/15/05 ¹⁰					<50	< 0.5	< 0.5	< 0.5	<0.5	< 0.5
10/14/05 ¹⁰					<50	< 0.5	< 0.5	< 0.5	<0.5	< 0.5
01/12/06 ¹⁰					<50	< 0.5	< 0.5	< 0.5	<0.5	< 0.5
04/13/06 ¹⁰					<50	< 0.5	< 0.5	< 0.5	<0.5	< 0.5
07/13/06 ¹⁰					<50	< 0.5	< 0.5	< 0.5	<0.5	< 0.5
10/17/06 ¹⁰					<50	< 0.5	< 0.5	< 0.5	<0.5	< 0.5
01/16/07 ¹⁰					<50	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5
04/17/07 ¹⁰					<50	<0.5	< 0.5	< 0.5	< 0.5	< 0.5
07/17/07 ¹⁰					<50	< 0.5	< 0.5	< 0.5	<0.5	< 0.5
10/16/07 ¹⁰					<50	< 0.5	< 0.5	< 0.5	<0.5	< 0.5
01/16/08 ¹⁰					<50	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5
04/16/08 ¹⁰					<50	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5
07/16/08 ¹⁰					<50	< 0.5	< 0.5	< 0.5	<0.5	< 0.5
10/15/08 ¹⁰					<50	< 0.5	< 0.5	< 0.5	<0.5	< 0.5
01/21/09 ¹⁰					<50 ¹³	< 0.5	< 0.5	< 0.5	<0.5	< 0.5
04/15/09 ¹⁰					<50	< 0.5	< 0.5	< 0.5	<0.5	< 0.5
07/03/09 ¹⁰					<50	< 0.5	< 0.5	< 0.5	<0.5	< 0.5
10/01/09 ¹⁰					<50	< 0.5	< 0.5	< 0.5	<0.5	< 0.5
01/19/10 ¹⁰					<50	< 0.5	< 0.5	< 0.5	<0.5	< 0.5
04/26/10¹⁰					<50	<0.5	<0.5	<0.5	<0.5	<0.5

EXPLANATIONS:

TOC = Top of Casing (ft.) = Feet DTW = Depth to Water GWE = Groundwater Elevation (msl) = Mean sea level TPH = Total Petroleum Hydrocarbons DRO = Diesel Range Organics GRO = Gasoline Range Organics B = Benzene T = Toluene E = Ethylbenzene X = Xylenes MTBE = Methyl Tertiary Butyl Ether (µg/L) = Micrograms per liter -- = Not Measured/Not Analyzed CS-2 = Creek Sample QA = Quality Assurance/Trip Blank

* TOC elevations for all wells were surveyed on July 30, 2009, by Morrow Surveying. Vertical Datum is NAVD 88 from GPS observations. TOC elevations were surveyed on January 25, 2001, by Virgil Chavez Land Surveying. The benchmark used for the survey was a City of Alameda benchmark being a cut square at the centerline return, south corner of Oak and Blanding, (Benchmark Elevation = 8.236 feet, NGVD 29).

- ¹ Well development performed.
- ² Laboratory report indicates unidentified hydrocarbons <C16.
- ³ Analyzed with silica gel cleanup.
- ⁴ Laboratory report indicates weathered gasoline C6-C12.
- ⁵ Laboratory report indicates discrete peaks.
- ⁶ Laboratory report indicates diesel C9-C24 + unidentified hydrocarbons <C16.
- ⁷ Laboratory report indicates gasoline C6-C12.
- ⁸ Laboratory report indicates unidentified hydrocarbons C9-C24.
- ⁹ Analysis performed without silica gel cleanup although was requested on the Chain of Custody.
- ¹⁰ BTEX and MTBE by EPA Method 8260.
- ¹¹ Laboratory report indicates the observed sample pattern is not typical of #2 fuel/diesel. It elutes in the DRO range later than #2 fuel.
- ¹² Laboratory report indicates the observed sample pattern includes #2 fuel/diesel and an additional pattern which elutes later in the DRO range.
- ¹³ Laboratory report indicates the original analysis was performed on an instrument where the ending calibration standard failed the method criteria. The sample was originally analyzed approximately 60 minutes after the LCS/LCSD. The LCS/LCSD showed good GRO recovery and the surrogate recovery for this sample was 85%. The sample was reanalyzed from a vial with headspace since only 1 vial was submitted. The results for the original and the reanalysis were similar. The reanalysis was reported.
- ¹⁴ BTEX by EPA Method 8260.
- ¹⁵ Laboratory report indicates DRO was detected in the method blank at a concentration of $38 \mu g/L$. Results from the reextraction are within limits. The hold time had expired prior to the reextraction therefore, all results are reported from the original extract. Similar results were obtained in both extracts.
- ¹⁶ Laboratory report indicates DRO was detected in the method blank at a concentration of $38 \mu g/L$. Results from the reextraction are within limits. The hold time had expired prior to the reextraction therefore, all results are reported from the original extract. The DRO result for the reextract is $96 \mu g/L$.
- ¹⁷ Laboratory report indicates DRO was detected in the method blank at a concentration of $47 \mu g/L$. Results from the reextraction are within limits. The hold time had expired prior to the reextraction therefore, all results are reported from the original extract. Similar results were obtained in both extracts.

 Table 2

 Groundwater Analytical Results - Metals

Chevron #206127 (Former Signal Oil Marine Terminal)

2301-2337 Blanding Avenue

Alameda, California

WELL ID/ DATE	Antimony (μg/L)	Arsenic (<i>h</i> g/ <i>T</i>)	Barium (μg/L)	Beryllium (μg/L)	(T/ ⁸ m)	(hall) (homiun	Cobalt (T/SĦ	Copper (<i>µg/L</i>)	pead Γcad (μg/L)	unnabydydenun (µg/L)	Nickel	Selenium	Silver Slver	(µg/L)	۲ مسطنس (<i>µg/L</i>)	cupy (μg/L)	hman Mercmy (μg/L)
MW-2 07/03/09	<9.7	<7.2	28.1	<1.4	<2.0	14.6	<2.1	<2.7	<6.9	<4.9	10.6	<8.9	<2.3	<14.0	12.6	11.6	<0.056
MW-3 07/03/09	<9.7	<7.2	143	<1.4	<2.0	8.5	<2.1	3.3	<6.9	<4.9	7.8	<8.9	<2.3	<14.0	13.8	18.8	<0.056
MW-4 07/03/09	<9.7	<7.2	83.5	<1.4	<2.0	10.0	<2.1	<2.7	<6.9	<4.9	4.5	<8.9	<2.3	<14.0	6.3	15.8	<0.056
MW-5 07/03/09	<9.7	32.7	148	<1.4	<2.0	<3.4	<2.1	3.1	<6.9	<4.9	3.6	<8.9	<2.3	<14.0	<2.5	19.2	<0.056

EXPLANATIONS

 $(\mu g/L) =$ Micrograms per liter

ANALYTICAL METHODS:

Metals analyzed by EPA Method SW-846 6010B Mercury analyzed by Method SW-7470A APPENDIX E

DEGRADATION RATE CALCULATIONS

Well	Analyte	Maximum Concentration (ug/L)	Current Concentration (ug/L)	Half-Life (years)	Date to Reach WQG
MW-1	TPHd	3,300	440	6.12	May 2027
	TPHg	5,210	65	NA	Met
	Benzene	920	<0.5	NA	Met
MW-1RA	TPHd	4,000	3,700	NA	NA
	TPHg	6,800	6,800	NA	NA
	Benzene	830	780	NA	NA
MW-1RB	TPHd	1,900	1,900	NA	NA
	TPHg	650	310	NA	NA
	Benzene	9	9	NA	NA
MW-3	TPHd	1,800	740	1.61	May 2016
	TPHg	310	<50	NA	Met
	Benzene	2	<0.5	NA	Met
MW-5	TPHd	3,200	3,200	NA	Stable
	TPHg	2,900	2,900	NA	Stable
	Benzene	99	99	NA	Stable
MW-6	TPHd	640	640	NA	NA
	TPHg	620	200	NA	NA
	Benzene	7	3	NA	NA

Table A - Summary of Degradation Rate CalculationsFormer Signal Oil Bulk Plant (Chevron Facility 20-6127), 2301-2311 Blanding Avenue, Alameda, CA





