



October 1, 1997  
AA12

Mr. Phil Briggs  
Chevron Products Company  
P. O. Box 5004  
San Ramon, California 94583-0804

Re: Former Signal Bulk Plant  
2001 Versailles Avenue  
Alameda, California

Dear Mr. Briggs:

This letter serves as an addendum to the risk-based corrective action evaluation prepared for the referenced site. The original evaluation was completed by Touchstone Developments and presented in a document titled, "*Corrective Action Evaluation RBCA Tier I*" dated June 13, 1997. The purpose of this addendum is to address concerns/requests described by the Alameda County Environmental Health Services (ACEHS) in their letter dated September 15, 1997.

The ACEHS noted that for each area of the site characterized, a comparison of risk-based screening levels (RBSLs) with average benzene concentrations may show that spot soil excavation is not necessary. For this addendum, RRM, Inc. (RRM) calculated average benzene concentrations for each area and compared them with RBSLs. Also, to take the process a step further, RRM used site parameters (e.g., depth to soil impact) to develop site-specific target levels (SSTLs) and compared those to average benzene concentrations. Methods and results are described below, followed by conclusions and recommendations. For reference, site maps prepared by Touchstone Developments and presented in their corrective action evaluation are provided in Attachment A.

not true

## METHODS

Data used in calculating average benzene concentrations were summarized by Touchstone Developments in their document titled *Corrective Action Evaluation RBCA Tier I*. The summarized data were generated by Harding Lawson Associates, Kleinfelder, and Touchstone Developments. Only soil data examined, and only benzene concentrations were considered. Averages were calculated using established methods, and all benzene data were used. To make use of data reported as "not detected", one-half the detection limit (0.005 parts per million

[ppm]) was used. Average benzene concentrations, and data used to calculate them, are given in Table 1.

As mentioned previously, SSTLs were also calculated to compare with average benzene concentrations. SSTLs were developed using the relationships provided in American Society for Testing and Materials (ASTM) Standard E1739 for Risk-Based Corrective Action at Petroleum Release Sites. Additionally, Tier 1 input parameters provided in the ASTM Standard were used where site-specific data were not available. Because of the low average benzene concentrations, only inhalation risk scenarios were examined; no other risk scenarios were applicable. Leaching to groundwater followed by ingestion of groundwater was not considered because: (1) shallow groundwater is not a drinking water source; (2) there are no nearby exposure points; and (3) the dissolved hydrocarbon plume has been noted to be stable.

Site-specific parameters used to calculate SSTLs are described below.

- **Depth to Subsurface Soil Impact:** the Tier 1 input parameter is 3.28 feet (100 centimeters) below grade surface (bgs). The average depth to soil impact that exceeded RBSLs is 5.6 feet (170.7 centimeters). The value of 170.7 centimeters was used in calculating SSTLs.
- **Volumetric Air Content:** on average, the soil impact is either below the groundwater table or at the capillary fringe. The ASTM Standard Tier 1 parameter for volumetric air content at the capillary fringe is 0.038 cubic centimeters air per cubic centimeters soil; this value was used in calculating SSTLs.

SSTL calculation worksheets that show input parameters and calculation results are provided in Attachment B.

## RESULTS

Area-specific average benzene concentrations are compared with RBSLs in Table 2. The comparison suggests there would be risks associated with atmospheric and enclosed space inhalation. Considering one in one million (1E-06) additional probability that an individual may develop cancer over a 70-year lifetime as a result of the exposure conditions evaluated, it can be seen:

- The residential and commercial atmospheric inhalation RBSLs are exceeded by the average benzene values for Areas 2 and 5;
- The residential and commercial enclosed space inhalation RBSLs are exceeded by the average benzene values for Areas 2, 4, 5, and 6.

Considering one in ten thousand (1E-04) additional probability, it was found:

- The residential enclosed space inhalation RBSL is exceeded by the average benzene values for Areas 2 and 5.

SSTLs are compared with area-specific average benzene concentrations in Table 3. The table shows that the enclosed-space inhalation SSTL for residential exposure, considering 1E-06 additional probability, is exceeded by average benzene values for Areas 2, 5, and 6. It can also be seen that the enclosed space inhalation SSTL for commercial exposure, considering 1E-06 additional probability, is exceeded by the average benzene value for Area 2. SSTLs associated with 1E-04 and 1E-05 additional probabilities are not exceeded by any average benzene values.

### CONCLUSIONS AND RECOMMENDATIONS

Based on the comparison with SSTLs, there may be a 1E-06 additional probability that an individual may develop cancer over a 70-year lifetime as a result of enclosed space inhalation at the conditions evaluated. This risk does not exist at probability levels of 1E-04 and 1E-05; the recommended range of acceptable risk probabilities, according to the Environmental Protection Agency (EPA), is 1E-04 to 1E-06.

*not true!*

With proper precautions, such as implementation of a risk management plan and participation in a County operated property development notification program, the risk identified here can be controlled and/or mitigated. RRM understands some excavation is proposed, but given that risk probabilities for the site lie between 1E-05 and 1E-06 for enclosed space inhalation, it does not appear that excavation is necessary. Instead, RRM recommends development of a risk management plan (RMP) that is acceptable to the ACEHS, implementation of the approved RMP, and participation in a property development notification program.

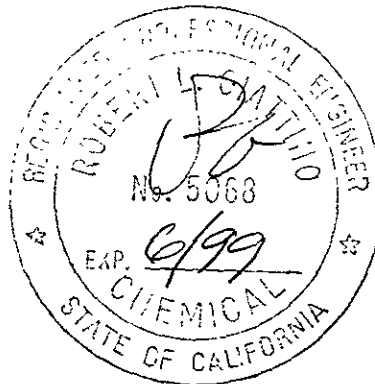
Please call me at (408) 475-8141 with questions or comments regarding this letter.

Sincerely,

RRM, Inc.



R. L. Giattino  
Chemical Engineer



- Attachments:
- Table 1 - Area Specific Average Benzene Concentrations in Soil
  - Table 2 - Area Specific Average Benzene Concentration in Soil Compared to RBSLs
  - Table 3 - Area Specific Average Benzene Concentration in Soil Compared to SSTLs and RBSLs
  - Attachment A - Site Maps
  - Attachment B - SSTL Calculation Worksheets

**Table 1**  
**Area Specific Average Benzene Concentration in Soil**

Former Signal Bulk Plant  
 2001 Versailles Avenue  
 Alameda, California

Area	Depth (feet)	Benzene (ppm)	Area	Depth (feet)	Benzene (ppm)
1	3	0.0025	5	2.5	0.0025
	4	0.002		2.5	0.0025
	5	0.0025		3.5	0.35
	5.25	0.0025		5.5	1.1
	mean	0.002375		6	0.0025
	SD	0.00025		7	0.0025
2	2.5	0.0025		10	0.0025
	3.5	0.0025		mean	0.208929
	4	0.0025		SD	0.413718
	5.5	0.0025		6	0.75
	5.5	0.0025	2		0.0025
	5.5	0.0025	3.75		0.0025
	6	0.003	4		0.0025
	7.5	2.9	5.25		0.0025
	9	0.0025	5.25		0.0025
mean	0.3245	5.5	0.0025		
SD	0.965813	5.5	0.0025		
3	4.75	0.0025	7.5	0.49	
	7	0.0025	8	0.0025	
	mean	0.0025	10	0.0025	
4	5	0.0025	mean	0.046818	
	5	0.0025	SD	0.146987	
	5	0.0025	4	0.1	0.0025
	5	0.0025		1.5	0.0025
	5	0.0025		2.5	0.0025
	5	0.0025		3	0.0025
	5	0.0025		4.5	0.0025
	5	0.63		5	0.0025
	5	0.0025		5	0.0025
5	0.0025	mean		0.080938	
5	0.0025	SD	0.221855		

Table 2  
**Area Specific Average Benzene Concentration in Soil Compared to RBSLs**

Former Signal Bulk Plant  
 2001 Versailles Avenue  
 Alameda, California

*Tier adjusted to PA -*

Area	Average Benzene Concentration (ppm)	Atmospheric Inhalation (ppm)				Enclosed Inhalation (ppm)				Ingestion/Dermal/Soil Inhalation (ppm)			
		Residential		Commercial		Residential		Commercial		Residential		Commercial	
		1.00E-04	1.00E-06	1.00E-04	1.00E-06	1.00E-04	1.00E-06	1.00E-04	1.00E-06	1.00E-04	1.00E-06	1.00E-04	1.00E-06
1	0.002	7.89	0.08	13.25	0.13	0.16	0.002	0.49	0.005	168.8	1.69	290	2.9
2	0.32	7.89	0.08	13.25	0.13	0.16	0.002	0.49	0.005	168.8	1.69	290	2.9
3	0.0025	7.89	0.08	13.25	0.13	0.16	0.002	0.49	0.005	168.8	1.69	290	2.9
4	0.08	7.89	0.08	13.25	0.13	0.16	0.002	0.49	0.005	168.8	1.69	290	2.9
5	0.21	7.89	0.08	13.25	0.13	0.16	0.002	0.49	0.005	168.8	1.69	290	2.9
6	0.047	7.89	0.08	13.25	0.13	0.16	0.002	0.49	0.005	168.8	1.69	290	2.9

ppm = parts per million, milligrams per kilogram  
 RBSL = risk-based screening level

Table 3  
**Area Specific Average Benzene Concentration in Soil Compared to SSTLs and RBSLs**

Former Signal Bulk Plant  
 2001 Versailles Avenue  
 Alameda, California

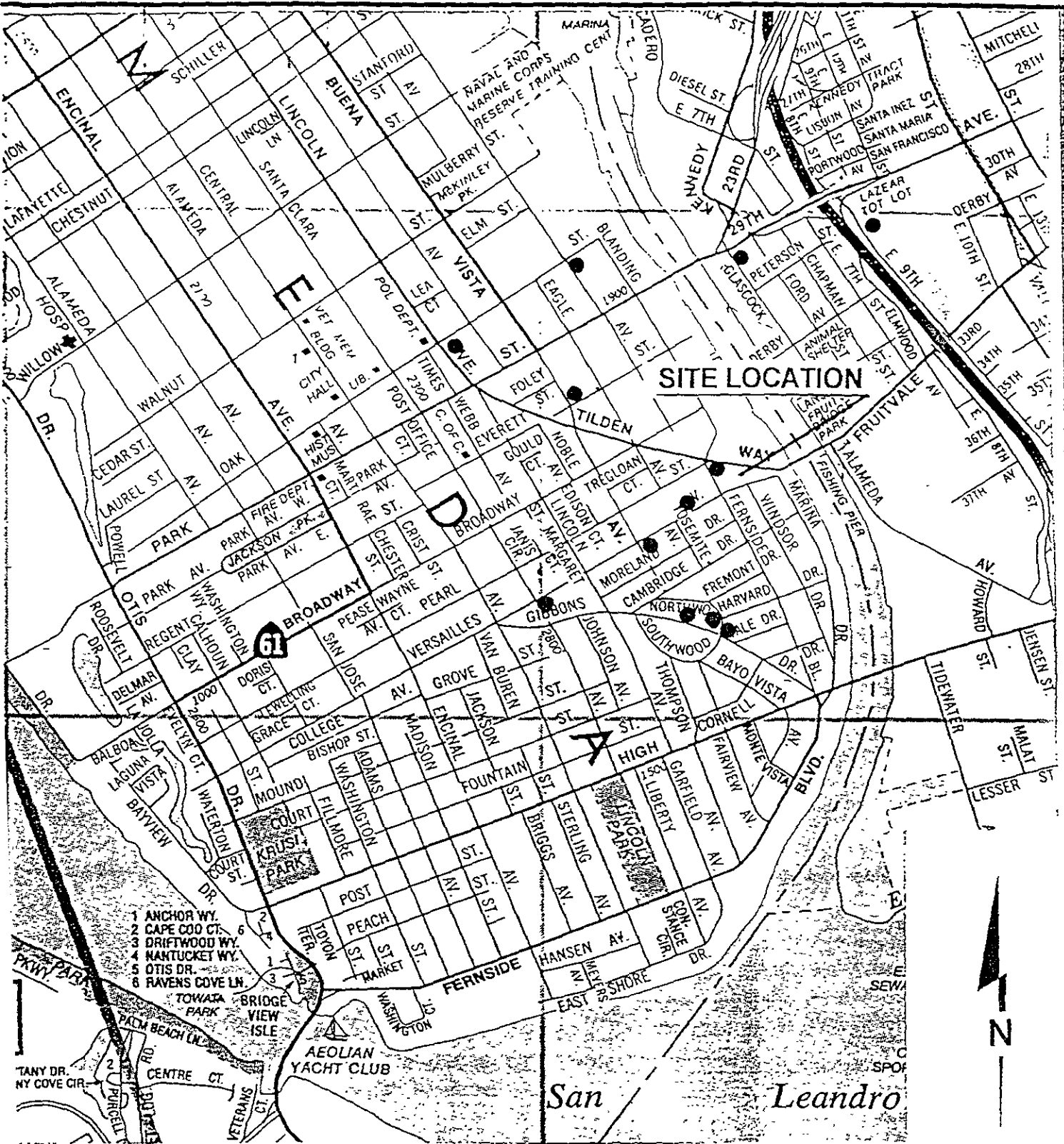
Area	Average Benzene Concentration (ppm)	SSTL Atmospheric Inhalation (ppm)				SSTL Enclosed Inhalation (ppm)				RBSL Ingestion/Dermal/Soil Inhalation (ppm)			
		Residential		Commercial		Residential		Commercial		Residential		Commercial	
		1.00E-04	1.00E-06	1.00E-04	1.00E-06	1.00E-04	1.00E-06	1.00E-04	1.00E-06	1.00E-04	1.00E-06	1.00E-04	1.00E-06
1	0.002	N	54	N	N	7	0.07	21	0.21	168.8	1.69	290	2.9
2	0.32	N	54	N	N	7	0.07	21	0.21	168.8	1.69	290	2.9
3	0.0025	N	54	N	N	7	0.07	21	0.21	168.8	1.69	290	2.9
4	0.08	N	54	N	N	7	0.07	21	0.21	168.8	1.69	290	2.9
5	0.21	N	54	N	N	7	0.07	21	0.21	168.8	1.69	290	2.9
6	0.047	N	54	N	N	7	0.07	21	0.21	168.8	1.69	290	2.9

ppm = parts per million, milligrams per kilogram  
 SSTL = site specific target level  
 RBSL = risk-based screening level  
 N = not necessary, most stringent SSTL not exceeded

*SSTL's based on soil specific parameters*

**ATTACHMENT A**  
**SITE MAPS**

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● WELL LOCATION

0 1/8 1/4  
scale in miles



**SITE VICINITY MAP and  
WELL SURVEY LOCATIONS**  
Former Chevron Bulk Plant  
2001 Versailles Avenue  
Alameda, California

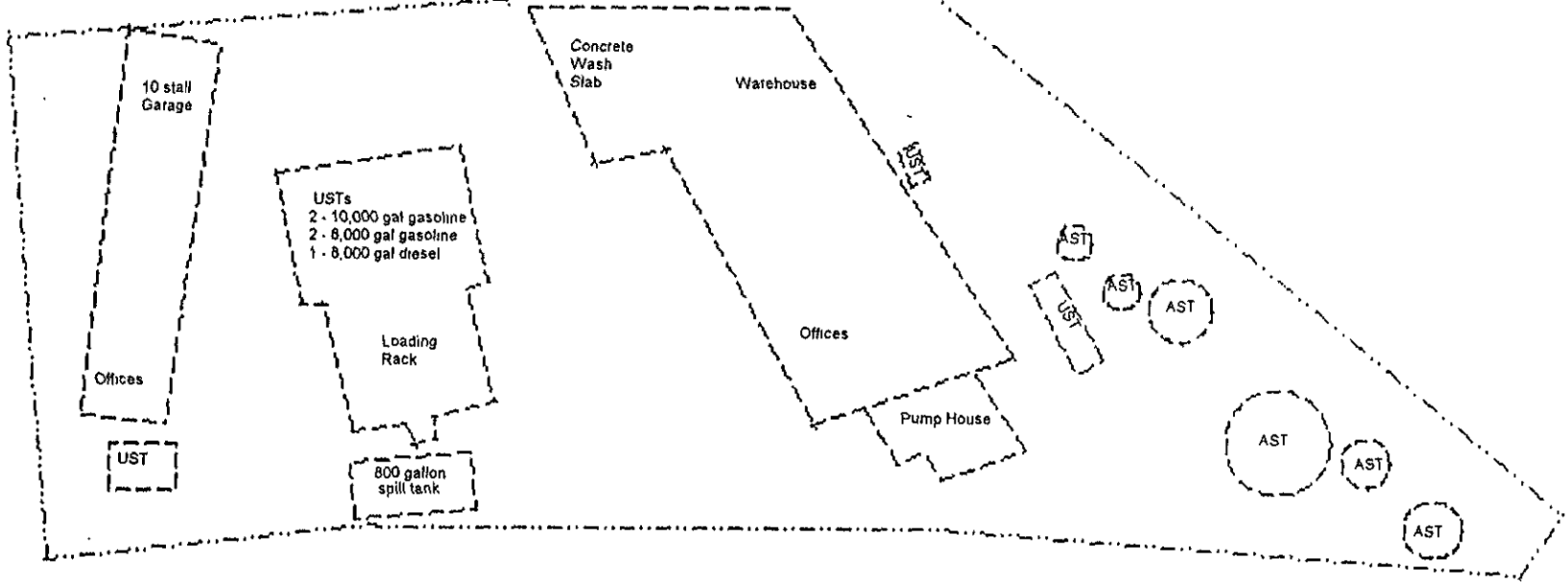
FIGURE

1





- UST    Underground Storage Tank
- AST    Former Above Ground Storage Tank
- Property Line
- - - - - Former Structures/Suspected Sources



0    25    50  
 Scale in feet



**SITE PLAN**  
 FORMER ALAMEDA BULK PLANT  
 2001 VERSAILLES AVENUE  
 ALAMEDA, CALIFORNIA

FIGURE  
**2**

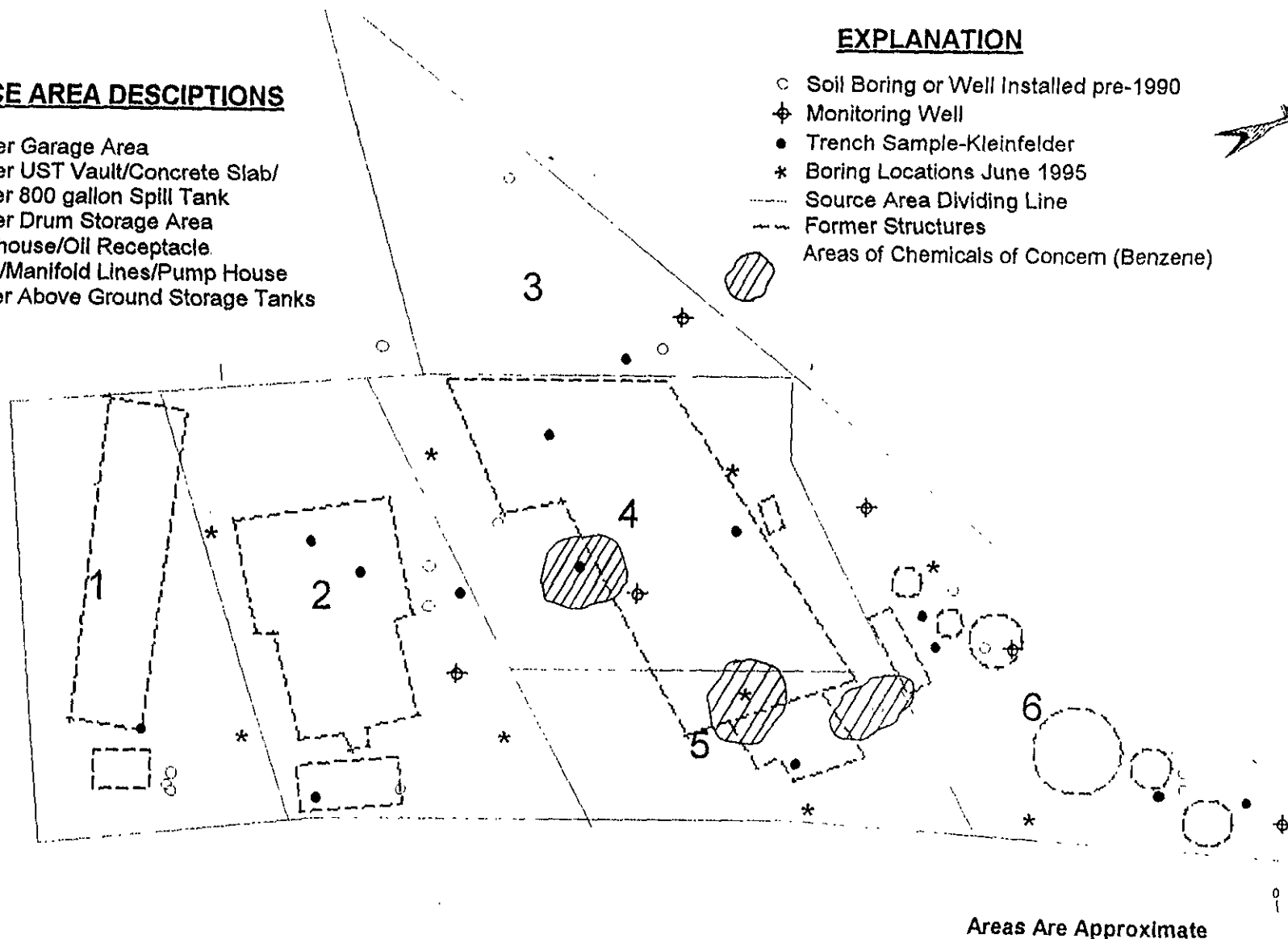
PROJECT NO. chev-1	DRAWN BY: AMD	DATE 1/95	BASE MAP: KLEINFELDER
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### SOURCE AREA DESCRIPTIONS

- 1) Former Garage Area
- 2) Former UST Vault/Concrete Slab/  
Former 800 gallon Spill Tank
- 3) Former Drum Storage Area
- 4) Warehouse/Oil Receptacle
- 5) Sump/Manifold Lines/Pump House
- 6) Former Above Ground Storage Tanks

### EXPLANATION

- Soil Boring or Well Installed pre-1990
- ⊕ Monitoring Well
- Trench Sample-Kleinfelder
- \* Boring Locations June 1995
- - - Source Area Dividing Line
- - - Former Structures
- ▨ Areas of Chemicals of Concern (Benzene)



Areas Are Approximate

0 25 50  
Scale in feet



**POTENTIAL SOURCE AREAS and  
AREAS OF CONCERN**  
FORMER ALAMEDA BULK PLANT  
2001 VERSAILLES AVENUE  
ALAMEDA, CALIFORNIA

FIGURE  
**3**

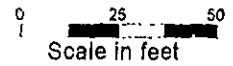
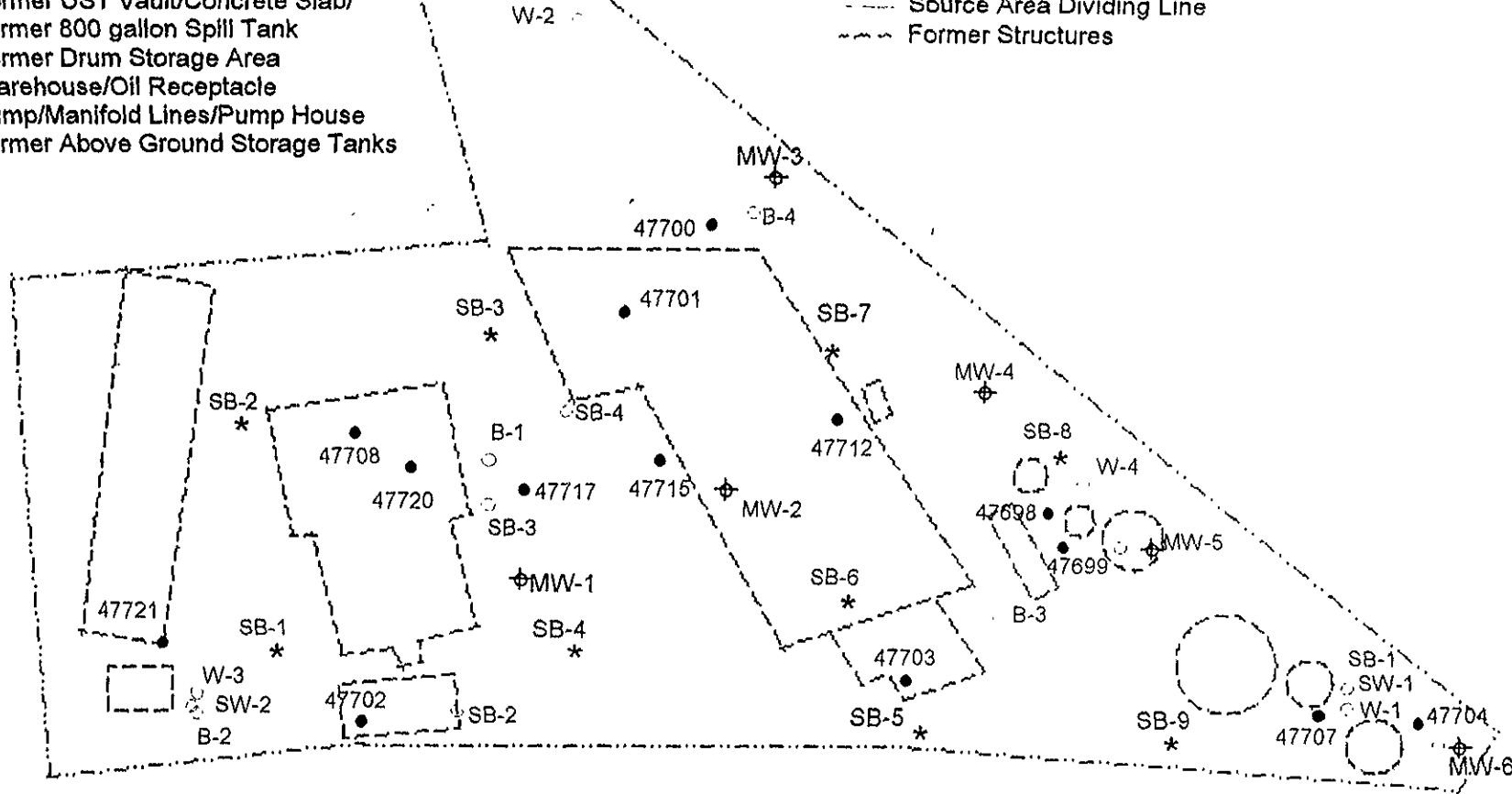
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**BORINGS AND SAMPLE LOCATIONS**  
 FORMER ALAMEDA BULK PLANT  
 2001 VERSAILLES AVENUE  
 ALAMEDA, CALIFORNIA

FIGURE  
**4**

PROJECT NO. chev-1	DRAWN BY: AMD	DATE 7/95	BASE MAP: KLEINFELDER
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**ATTACHMENT B**  
**SSTL CALCULATION WORKSHEETS**

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**Risk Based Corrective Action Soil Cleanup Goal Worksheet**

**Scenario:** residual contaminant dissolved in soil moisture (residual soil impact) volatilizes and is transported through the vadose zone via diffusion. Contaminant vapors leave the soil surface and enter the atmosphere where they are inhaled by a 70 kilogram adult.

*what about children*

**Working Equations:**

$$VF_{amb} = (H \cdot \rho_s) \cdot (1 / (\theta_{ws} + k_s \cdot \rho_s + H \cdot \theta_{as})) \cdot (1 / (1 + (U_{air} \cdot \delta_{air} \cdot L_s) / (D^{eff} \cdot W))) \cdot 10^3$$

where,

- H = Henry's Law Constant (cm<sup>3</sup>-water/cm<sup>3</sup>-air)
- $\rho_s$  = soil bulk density (g-soil/cm<sup>3</sup>-soil)
- $\theta_{ws}$  = volumetric water content in soil (cm<sup>3</sup>-water/cm<sup>3</sup>-soil)
- $\theta_{as}$  = volumetric air content in soil (cm<sup>3</sup>-air/cm<sup>3</sup>-soil)
- $\theta_T$  = total soil porosity (cm<sup>3</sup>-void/cm<sup>3</sup>-soil)
- $k_s$  = soil-water sorption coefficient (cm<sup>3</sup>-water/g-soil) =  $foc \cdot koc$
- foc = fraction of organic carbon in soil (g-carbon/g-soil)
- koc = carbon-water sorption coefficient (cm<sup>3</sup>-water/g-carbon)
- $U_{air}$  = wind speed above ground surface in ambient mixing zone (cm/s)
- $\delta_{air}$  = ambient air mixing zone height (cm)
- $L_s$  = depth to subsurface soil impact (cm)
- $D^{eff}$  = effective diffusion coefficient in soil, vapor (cm<sup>2</sup>/s)  
 $= [D_{air} \cdot (\theta_{as}^{3.33}) / (\theta_T^{2})] + [D_{water} \cdot (1/H) \cdot (\theta_{ws}^{3.33}) / (\theta_T^{2})]$
- $D_{air}$  = diffusion coefficient in air (cm<sup>2</sup>/s)
- $D_{water}$  = diffusion coefficient in water (cm<sup>2</sup>/s)
- W = width of impact area parallel to wind direction (cm)
- $VF_{amb}$  = relationship between outdoor air and soil concentrations (mg/m<sup>3</sup>-air)/(mg/kg-soil)
- RBSL<sub>air</sub> = risk-based screening level (ug-contaminant/m<sup>3</sup>-air) - residential 10<sup>-6</sup> risk
- SSTL = site specific target level (mg-contaminant/kg-soil)  
 $= (RBSL_{air} / VF_{amb}) \cdot 1E-3$
- SSTL = CalEPA risk for benzene multiply by 0.29

Benzene Impact	Benzene Impact	Site Specific
Conservative	Site Specific	Site Specific
Generic Values	Values	
0.22	0.22	
1.7	1.7	
0.12	0.342	
0.26	0.038	
0.38	0.38	
0.380	0.380189	
0.01	0.01	
38.0189	38.0189	
225	225	
200	200	
100	170.7	
0.0072576	2.1732E-05	
0.093	0.093	
1.10E-05	1.10E-05	
1500	1500	
0.001098675	1.5925E-06	
2.94E-01	2.94E-01	
2.68E-01	1.85E+02	
7.76E-02	5.35E+01	

Indoor

**Risk Based Corrective Action Soil Cleanup Goal Worksheet**

**Scenario:** residual contaminant dissolved in soil moisture (residual soil impact) volatilizes and is transported through the vadose zone via diffusion. Contaminant vapors leave the concrete surface through cracks and enter the atmosphere where they are inhaled by a 70 kilogram adult.

**Working Equations:**  $VF_{sesp} = (H \cdot \rho_s) \cdot (1 / (\theta_{ws} + k_s \cdot \rho_s + H \cdot \theta_{as})) \cdot A \cdot B \cdot 10^3$

- H = Henry's Law Constant (cm<sup>3</sup>-water/cm<sup>3</sup>-air)
- ρ<sub>s</sub> = soil bulk density (g-soil/cm<sup>3</sup>-soil)
- θ<sub>ws</sub> = volumetric water content in soil (cm<sup>3</sup>-water/cm<sup>3</sup>-soil)
- θ<sub>as</sub> = volumetric air content in soil (cm<sup>3</sup>-air/cm<sup>3</sup>-soil)
- θ<sub>T</sub> = total soil porosity (cm<sup>3</sup>-void/cm<sup>3</sup>-soil)
- k<sub>s</sub> = soil-water sorption coefficient (cm<sup>3</sup>-water/g-soil) = f<sub>oc</sub>·k<sub>oc</sub>
- f<sub>oc</sub> = fraction of organic carbon in soil (g-carbon/g-soil)
- k<sub>oc</sub> = carbon-water sorption coefficient (cm<sup>3</sup>-water/g-carbon)
- A = (D<sup>eff</sup>/L<sub>s</sub>)·(1/(ER·L<sub>B</sub>))
- B = 1/(1+A+((D<sup>eff</sup>/L<sub>s</sub>)/((D<sub>crack</sub>/L<sub>crack</sub>)·η)))
- L<sub>s</sub> = depth to subsurface soil impact (cm)
- D<sup>eff</sup> = effective diffusion coefficient in soil, vapor (cm<sup>2</sup>/s)  
 $= [D_{air} \cdot (\theta_{as}^{3.33}) / (\theta_T^{3.33})] + [D_{water} \cdot (1/H) \cdot (\theta_{ws}^{3.33}) / (\theta_T^{3.33})]$
- D<sub>air</sub> = diffusion coefficient in air (cm<sup>2</sup>/s)
- D<sub>water</sub> = diffusion coefficient in water (cm<sup>2</sup>/s)
- D<sub>crack</sub> = effective vapor diffusion coefficient through concrete (cm<sup>2</sup>/s)  
 $= [D_{air} \cdot (\theta_{acrack}^{3.33}) / (\theta_T^{3.33})] + [D_{water} \cdot (1/H) \cdot (\theta_{wcrack}^{3.33}) / (\theta_T^{3.33})]$
- θ<sub>acrack</sub> = volumetric air content in crack (cm<sup>3</sup>/cm<sup>3</sup>)
- θ<sub>wcrack</sub> = volumetric water content in crack (cm<sup>3</sup>/cm<sup>3</sup>)
- L<sub>crack</sub> = foundation or wall thickness (cm)
- L<sub>B</sub> = enclosed space volume/infiltration area (cm)
- ER = enclosed space air exchange rate (L/s)
- η = areal fraction of cracks in foundation/walls (cm<sup>2</sup>-cracks/cm<sup>2</sup>-total area)
- VF<sub>sesp</sub> = relationship between indoor air and soil concentrations (mg/m<sup>3</sup>-air)/(mg/kg-soil)
- RBSL<sub>air</sub> = risk-based screening level (ug-contaminant/m<sup>3</sup>-air) - residential 10<sup>-6</sup> risk
- SSTL = site specific target level (mg-contaminant/kg-soil)
- CalEPA = (RBSL<sub>air</sub>/VF<sub>sesp</sub>)·1E-3 (CalEPA risk for benzene multiply by 0.29)

	Benzene Impact Conservative	Benzene Impact Site Specific	Site Specific
	0.22	0.22	
	1.7	1.7	
	0.12	0.342	
	0.26	0.036	
	0.38	0.38	
	0.380189396	0.380189396	
	0.01	0.01	
	38.01893963	38.01893963	
	0.002592011	4.54691E-06	
	0.062489877	0.974357273	
	100	170.7	
	0.007257629	2.17324E-05	
	0.093	0.093	
	1.10E-05	1.10E-05	
	0.007257629	0.007257629	
	0.26	0.26	
	0.12	0.12	
	15	15	
	200	200	
	0.00014	0.00014	
	0.01	0.01	
	0.073560189	0.001662454	
	3.92E-01	3.92E-01	
	5.33E-03	2.36E-01	
	1.55E-03	6.84E-02	

**Risk Based Corrective Action Soil Cleanup Goal Worksheet**

**Scenario:** residual contaminant dissolved in soil moisture (residual soil impact) volatilizes and is transported through the vadose zone via diffusion. Contaminant vapors leave the concrete surface through cracks and enter the atmosphere where they are inhaled by a 70 kilogram adult.

**Working Equations:**  $VF_{sep} = (H \cdot \rho_s) \cdot (1 / (\theta_{ws} + k_s \cdot \rho_s + H \cdot \theta_{as})) \cdot A \cdot B \cdot 10^3$

- H = Henry's Law Constant (cm<sup>3</sup>-water/cm<sup>3</sup>-air)
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- f<sub>oc</sub> = fraction of organic carbon in soil (g-carbon/g-soil)
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- A = (D<sup>eff</sup>/L<sub>s</sub>)·(1/(ER·L<sub>B</sub>))
- B = 1/(1+A+(D<sup>eff</sup>/L<sub>s</sub>)/((D<sub>crack</sub>/L<sub>crack</sub>)·η))
- L<sub>s</sub> = depth to subsurface soil impact (cm)
- D<sup>eff</sup> = effective diffusion coefficient in soil, vapor (cm<sup>2</sup>/s)  
 $= [D_{air} \cdot (\theta_{as}^{3.33}) / (\theta_T^{3.33})] + [D_{water} \cdot (1/H) \cdot (\theta_{ws}^{3.33}) / (\theta_T^{3.33})]$
- D<sub>air</sub> = diffusion coefficient in air (cm<sup>2</sup>/s)
- D<sub>water</sub> = diffusion coefficient in water (cm<sup>2</sup>/s)
- D<sub>crack</sub> = effective vapor diffusion coefficient through concrete (cm<sup>2</sup>/s)  
 $= [D_{air} \cdot (\theta_{crack}^{3.33}) / (\theta_T^{3.33})] + [D_{water} \cdot (1/H) \cdot (\theta_{wcrack}^{3.33}) / (\theta_T^{3.33})]$
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- θ<sub>wcrack</sub> = volumetric water content in crack (cm<sup>3</sup>/cm<sup>3</sup>)
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- RBSL<sub>air</sub> = risk-based screening level (ug-contaminant/m<sup>3</sup>-air) - residential 10<sup>-4</sup> risk
- SSTL = site specific target level (mg-contaminant/kg-soil)
- CalEPA = (RBSL<sub>air</sub>/VF<sub>sep</sub>)·1E-3 (CalEPA risk for benzene multiply by 0.29)

	Benzene Impact Conservative	Benzene Impact Site Specific	Site Specific
	0.22	0.22	
	1.7	1.7	
	0.12	0.342	
	0.26	0.036	
	0.38	0.38	
	0.380189396	0.380189396	
	0.01	0.01	
	38.01893963	38.01893963	
	0.002592011	4.54691E-06	
	0.062489877	0.974357273	
	100	170.7	
	0.007257629	2.17324E-05	
	0.093	0.093	
	1.10E-05	1.10E-05	
	0.007257629	0.007257629	
	0.26	0.26	
	0.12	0.12	
	15	15	
	200	200	
	0.00014	0.00014	
	0.01	0.01	
	0.073560189	0.001662454	
	3.92E+01	3.92E+01	
	5.33E-01	2.36E+01	
	1.55E-01	6.84E+00	

*dup*

**Risk Based Corrective Action Soil Cleanup Goal Worksheet**

**Scenario:** residual contaminant dissolved in soil moisture (residual soil impact) volatilizes and is transported through the vadose zone via diffusion. Contaminant vapors leave the concrete surface through cracks and enter the atmosphere where they are inhaled by a 70 kilogram adult.

**Working Equations:**  $VF_{seps} = (H \cdot \rho_s) \cdot (1 / (\theta_{ws} + k_s \cdot \rho_s + H \cdot \theta_{as})) \cdot A \cdot B \cdot 10^3$

- H = Henry's Law Constant (cm<sup>3</sup>-water/cm<sup>3</sup>-air)
- $\rho_s$  = soil bulk density (g-soil/cm<sup>3</sup>-soil)
- $\theta_{ws}$  = volumetric water content in soil (cm<sup>3</sup>-water/cm<sup>3</sup>-soil)
- $\theta_{as}$  = volumetric air content in soil (cm<sup>3</sup>-air/cm<sup>3</sup>-soil)
- $\theta_T$  = total soil porosity (cm<sup>3</sup>-void/cm<sup>3</sup>-soil)
- $k_s$  = soil-water sorption coefficient (cm<sup>3</sup>-water/g-soil) =  $foc \cdot k_{oc}$
- foc = fraction of organic carbon in soil (g-carbon/g-soil)
- $k_{oc}$  = carbon-water sorption coefficient (cm<sup>3</sup>-water/g-carbon)
- A =  $(D^{eff} / L_s) \cdot (1 / (ER \cdot L_B))$
- B =  $1 / (1 + A + ((D^{eff} / L_s) / ((D_{crack} / L_{crack}) \cdot \eta)))$
- L<sub>s</sub> = depth to subsurface soil impact (cm)
- D<sup>eff</sup> = effective diffusion coefficient in soil, vapor (cm<sup>2</sup>/s)  
 $= [D_{air} \cdot (\theta_{as}^{3.33}) / (\theta_T^{2})] + [D_{water} \cdot (1/H) \cdot (\theta_{ws}^{3.33}) / (\theta_T^{2})]$
- D<sub>air</sub> = diffusion coefficient in air (cm<sup>2</sup>/s)
- D<sub>water</sub> = diffusion coefficient in water (cm<sup>2</sup>/s)
- D<sub>crack</sub> = effective vapor diffusion coefficient through concrete (cm<sup>2</sup>/s)  
 $= [D_{air} \cdot (\theta_{acrack}^{3.33}) / (\theta_T^{2})] + [D_{water} \cdot (1/H) \cdot (\theta_{wcrack}^{3.33}) / (\theta_T^{2})]$
- $\theta_{acrack}$  = volumetric air content in crack (cm<sup>3</sup>/cm<sup>3</sup>)
- $\theta_{wcrack}$  = volumetric water content in crack (cm<sup>3</sup>/cm<sup>3</sup>)
- L<sub>crack</sub> = foundation or wall thickness (cm)
- L<sub>B</sub> = enclosed space volume/infiltration area (cm)
- ER = enclosed space air exchange rate (L/s)
- $\eta$  = areal fraction of cracks in foundation/walls (cm<sup>2</sup>-cracks/cm<sup>2</sup>-total area)
- VF<sub>seps</sub> = relationship between indoor air and soil concentrations (mg/m<sup>3</sup>-air)/(mg/kg-soil)
- RBSL<sub>air</sub> = risk-based screening level (ug-contaminant/m<sup>3</sup>-air) - commercial 10<sup>-6</sup> risk
- SSTL = site specific target level (mg-contaminant/kg-soil)
- CalEPA = (RBSL<sub>air</sub>/VF<sub>seps</sub>)\*1E-3 (CalEPA risk for benzene multiply by 0.29)

	Benzene Impact Conservative	Benzene Impact Site Specific	Site Specific
	0.22	0.22	
	1.7	1.7	
	0.12	0.342	
	0.26	0.038	
	0.38	0.38	
	0.380189396	0.380189396	
	0.01	0.01	
	38.01893963	38.01893963	
	0.00105183	1.84512E-06	
	0.062495892	0.974359838	
	100	170.7	
	0.007257629	2.17324E-05	
	0.093	0.093	
	1.10E-05	1.10E-05	
	0.007257629	0.007257629	
	0.26	0.26	
	0.12	0.12	
	15	15	
	300	300	
	0.00023	0.00023	
	0.01	0.01	
	0.029853385	0.000674621	
	4.93E-01	4.93E-01	
	1.65E-02	7.31E-01	
	4.79E-03	2.12E-01	



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- ρ<sub>s</sub> = soil bulk density (g-soil/cm<sup>3</sup>-soil)
- θ<sub>ws</sub> = volumetric water content in soil (cm<sup>3</sup>-water/cm<sup>3</sup>-soil)
- θ<sub>as</sub> = volumetric air content in soil (cm<sup>3</sup>-air/cm<sup>3</sup>-soil)
- θ<sub>T</sub> = total soil porosity (cm<sup>3</sup>-void/cm<sup>3</sup>-soil)
- k<sub>s</sub> = soil-water sorption coefficient (cm<sup>3</sup>-water/g-soil) = f<sub>oc</sub>·k<sub>oc</sub>
- f<sub>oc</sub> = fraction of organic carbon in soil (g-carbon/g-soil)
- k<sub>oc</sub> = carbon-water sorption coefficient (cm<sup>3</sup>-water/g-carbon)
- A = (D<sup>eff</sup>/L<sub>s</sub>)·(1/(ER·L<sub>B</sub>))
- B = 1/(1+A+((D<sup>eff</sup>/L<sub>s</sub>)/((D<sub>crack</sub>/L<sub>crack</sub>)<sup>3</sup>·η)))
- L<sub>s</sub> = depth to subsurface soil impact (cm)
- D<sup>eff</sup> = effective diffusion coefficient in soil, vapor (cm<sup>2</sup>/s)  
 $= [D_{air} \cdot (\theta_{as}^{3.33}) / (\theta_T^2)] + [D_{water} \cdot (1/H) \cdot (\theta_{ws}^{3.33}) / (\theta_T^2)]$
- D<sub>air</sub> = diffusion coefficient in air (cm<sup>2</sup>/s)
- D<sub>water</sub> = diffusion coefficient in water (cm<sup>2</sup>/s)
- D<sub>crack</sub> = effective vapor diffusion coefficient through concrete (cm<sup>2</sup>/s)  
 $= [D_{air} \cdot (\theta_{crack}^{3.33}) / (\theta_T^2)] + [D_{water} \cdot (1/H) \cdot (\theta_{wcrack}^{3.33}) / (\theta_T^2)]$
- θ<sub>crack</sub> = volumetric air content in crack (cm<sup>3</sup>/cm<sup>3</sup>)
- θ<sub>wcrack</sub> = volumetric water content in crack (cm<sup>3</sup>/cm<sup>3</sup>)
- L<sub>crack</sub> = foundation or wall thickness (cm)
- L<sub>B</sub> = enclosed space volume/infiltration area (cm)
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- η = areal fraction of cracks in foundation/walls (cm<sup>2</sup>-cracks/cm<sup>2</sup>-total area)
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	0.093	0.093	
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	0.007257629	0.007257629	
	0.26	0.26	
	0.12	0.12	
	15	15	
	300	300	
	0.00023	0.00023	
	0.01	0.01	
	0.029853385	0.000674621	
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	4.79E-01	2.12E+01	