



# **ENVIRONMENTAL AUDIT, INC.**

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February 16, 1995

Project No. 1233-

Ms. Medula Logan  
Alameda County  
Environmental Health Department  
Environmental Protection Division  
1131 Harbor Bay Parkway, #250  
Alameda, CA 94502-6577

**RE: RESPONSES TO COMMENTS  
ADDENDUM TO RISK BASED CORRECTIVE ACTIONS ANALYSIS  
Montgomery Ward Auto Service Center and  
Enea Properties Sites  
Dublin, California**

Dear Ms. Logan:

Pursuant to a telephone conversation with you on February 14, 1995, the following are the revised calculations for benzene and TPH emissions into outdoor and indoor (enclosed space) air (see Attachment) for the risk based corrective actions (RBCA) analyses for the Montgomery Ward and Enea Properties sites in Dublin, California. These revised calculations reflect a depth to ground water (DTW) of approximately nine feet below ground surface (bgs). In our letter dated February 6, 1995 titled, "Addendum to Risk Based Corrective Actions Analysis" (Environmental Audit, Inc. [EAI], 1995), we used a DTW of approximately 10 feet (305 centimeters [cm]) in our calculations for emissions into outdoor and indoor air. Review of recent data contained in Table 3 of EAI, 1995 document indicates that the DTW at the Montgomery Ward site is approximately 11 to 12 feet bgs, while the DTW at the Enea Properties site ranges from approximately nine to 10 feet bgs. Therefore, these data support the use of the "10 feet DTW" value used in the calculations contained in the EAI, 1995 document. As stated above, we used a DTW of nine feet (274 cm) in the revised calculations contained herein and the results of these revised calculations are, therefore, conservative.

Table 1 summarizes the outdoor and indoor (enclosed space) air, health risk assessment based on incremental cancer risks of  $1 \times 10^{-6}$  and  $1 \times 10^{-5}$ . These TPH and benzene results were compared to recent data, that is 1994 quarterly ground water monitoring data (see Tables 1 and 2 in EAI, 1995 document), which reflect current conditions. The following provides a summary of these results for the Enea Properties and Montgomery Ward sites.

## **ENEA PROPERTIES**

### Outdoor Air

None of the concentrations in ground water exceed the maximum allowable benzene or TPH concentration in ground water for emissions into outdoor air using either a risk of either  $1 \times 10^{-6}$  and  $1 \times 10^{-5}$  (see Table 1).

### Indoor (Enclosed Space)

Use of a risk of  $1 \times 10^{-5}$  results in calculations that demonstrate that none of the constituents in ground water at the Enea Properties site have exceeded the maximum allowable benzene and TPH concentration in ground water for emissions into indoor air emissions (see Table 1).

Based on a risk of  $1 \times 10^{-6}$ , the calculations show that none of the benzene concentrations in ground water at the Enea Properties site exceeded the calculated maximum benzene concentration of 65.3 micrograms/liter (ug/l) during 1994. The benzene concentration in ground water at the Enea Properties site exceed the calculated maximum allowable benzene concentration in well MW-1 for only one sampling event (October 14, 1993 in which 76 ug/l of benzene was detected) (see Table 1 and Table 1 of EAI, 1995).

Quarterly monitoring shows that dissolved TPH detected in water samples from wells MW-1 and MW-3 have exceeded maximum allowable TPH concentration in ground water of 1,113 ug/l during all sampling events in 1994 (see Table 1 of EAI, 1995). No problematic concentrations of TPH, however, were detected in wells MW-2 and MW-4. As stated in EAI, 1995, the use of a toxicity factor of  $0.0017 \text{ (mg/kg-day)}^{-1}$  for gasoline is probably not appropriate for the Enea Properties site, since this toxicity factor is derived from a gasoline sample which is probably dissimilar in original composition and is not weathered as compared to the dissolved material in ground water at the site. Consequently, the calculated maximum value for TPH emissions from ground water based on the toxicity factor of  $0.0017 \text{ (mg/kg-day)}^{-1}$  is too conservative and is probably not appropriate (see EAI, 1995).

## **Montgomery Ward Site (including off-site wells MW-100, 101, and 102)**

### Outdoor Air

None of the concentrations in ground water exceed the maximum allowable benzene or TPH concentration in ground water for emissions into outdoor air using either a cancer risk level of either  $1 \times 10^{-6}$  or  $1 \times 10^{-5}$  (see Table 1).

### Indoor Air

Use of a cancer risk level of  $1 \times 10^{-5}$  results in no problematic concentrations of TPH or benzene in ground water for emissions into indoor air (see Table 1).

The maximum benzene concentration in ground water is 65.3 ug/l based on use of a  $1 \times 10^{-6}$  risk. Water samples obtained from wells B-5, B-10, and B-12 contain benzene which exceed this maximum allowable concentration.

Analytical testing of water samples from wells B-5, B-10, B-12, and MW-100 show that TPH detected in samples from these wells exceed the maximum allowable TPH limit of

1,113 ug/l which is based on a risk of  $1 \times 10^{-6}$ . As stated above, use of this toxicity factor of  $0.0017 \text{ (mg-kg/day)}^{-1}$  may not be appropriate since the toxicity factor used is based on a gasoline sample of likely dissimilar composition to the TPH in ground water at the site.

### LIMITATION

Our professional services have been performed using that degree of care and skill ordinarily exercised, under similar circumstances, by reputable environmental consultants in this or similar localities. No other warranty, expressed or implied, is made as to the professional advice contained in this report.

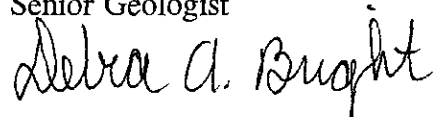
Please call if you have any questions or need additional information.

Sincerely,

ENVIRONMENTAL AUDIT, INC.



Frank S. Muramoto, R.G.  
Senior Geologist



Debra A. Bright, M.P.H.  
Senior Vice President

FSM:DAB:sh

attachments

cc: E. Chu, Alameda County  
C. West, Montgomery Ward  
G. Jonas, Montgomery Ward  
M. Gilmartin, Straw & Gilmartin  
R. Enea, Enea Properties  
R. Arulanantham, BARWQCB

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TABLE 1

SUMMARY OF OUTDOOR  
AND INDOOR (ENCLOSED SPACE) AIR  
HEALTH RISK ASSESSMENT

RISK	$1 \times 10^{-6}$		$1 \times 10^{-5}$ - 10 <sup>-4</sup>	
	TPH	BENZENE	TPH	BENZENE
	$\mu\text{g/l}$	$\mu\text{g/l}$	$\mu\text{g/l}$	$\mu\text{g/l}$
OUTDOOR AIR	35,216	2,064	352,164	20,644
INDOOR AIR	1,113	65.3	11,132	653.3

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MONTGOMERY WARDS - DUBLIN  
 HEALTH RISK ASSESSMENT  
 Benzene Impacts - Indoor air

$$RBSL(air) = (TR)(BW)(ATc)(365)(1000)/(SFi*IR*EF*ED)$$

RBSL(air) 4.933793 (ug/m3)

TR 0.00001  
 BW 70 kg  
 ATc 70 years  
 SFi 0.029 (mg/kg-day)<sup>-1</sup>  
 IRair 20 m3/day  
 EF 250 days/year  
 ED 25 years

$$Ds = Dair (Oas \wedge 3.33/Ot \wedge 3.33) + Dwat(1/H)(Ows \wedge 3.33/Ot \wedge 3.33)$$

Ds 0.026283 (cm2/sec)  
 Dair 0.093 cm2/s  
 Oas 0.26  
 Ot 0.38  
 Dwat 0.000011 cm2/s  
 H 0.22 l water/l air  
 Ows 0.12

$$Dcrack = Dair (Oacrack \wedge 3.33/Ot \wedge 3.33) + Dwat(1/H)(Owcrack \wedge 3.33/Ot \wedge 3.33)$$

Dcrack 0.026283 cm2/sec  
 Dair 0.093 cm2/sec  
 Oacrack 0.26  
 Ot 0.38  
 Dwat 0.000011 cm2/s  
 H 0.22 l water/l air  
 Owcrack 0.12

$$Dcap = Dair (Oacap \wedge 3.33/Ot \wedge 3.33) + Dwat(1/H)(Owcap \wedge 3.33/Ot \wedge 3.33)$$

Dcap 0.093035 cm2/sec  
 Dair 0.093 cm2/sec  
 Ocap 0.38  
 Ot 0.38  
 Dwat 0.000011 cm2/s  
 H 0.22 l water/l air  
 Owcap 0.342

$$Dws = (Hcap + Hv)(Hcap/Dcap + Hv/Ds) \wedge -1$$

Dws 0.026632 cm2/s  
 Hcap 5 cm  
 Hv 269 cm  
 Dcap 0.093035 cm2/s  
 Ds 0.026283

1st Term 274  
 2nd Term 0.000097

$$VFwesp = H(Dws/Lgw/(ER*Lb)/1 + (Dws/Lgw/(ER*Lb) + Dws/Lgw/(Dcrack/Lcrack) \wedge n) \times 1000$$

VFwesp 0.007552 kg/m3  
 H 0.22 l water/l air  
 Dws 0.026602  
 Lgw 274  
 ER 0.0028  
 Lb 1010  
 Dcrack 0.026283 g/cm3  
 Lcrack 15  
 n 0.01

1st Term 0.007553  
 2nd Term 0.000034  
 3rd Term 0.000103

$$RBSLw = RBSLair \times 0.001/VFwesp$$

RBSLw 0.653332 mg/l  
 or 653.3318 ug/l

MONTGOMERY WARDS – DUBLIN  
 HEALTH RISK ASSESSMENT  
 Benzene Impacts – Indoor air

$$RBSL(air) = (TR)(BW)(ATc)(365)(1000)/(SFi*IR*EF*ED)$$

RBSL(air) 0.493379 (ug/m3)

TR 1.0E-06  
 BW 70 kg  
 ATc 70 years  
 SFi 0.029 (mg/kg-day)<sup>-1</sup>  
 IRair 20 m3/day  
 EF 250 days/year  
 ED 25 years

$$Ds = Dair (Oas \wedge 3.33/Ot \wedge 3.33) + Dwat(1/H)(Ows \wedge 3.33/Ot \wedge 3.33)$$

Ds 0.026283 (cm2/sec)  
 Dair 0.093 cm2/s  
 Oas 0.26  
 Ot 0.38  
 Dwat 0.000011 cm2/s  
 H 0.22 l water/l air  
 Ows 0.12

$$Dcrack = Dair (Oacrack \wedge 3.33/Ot \wedge 3.33) + Dwat(1/H)(Owcrack \wedge 3.33/Ot \wedge 3.33)$$

Dcrack 0.026283 cm2/sec  
 Dair 0.093 cm2/sec  
 Oacrack 0.26  
 Ot 0.38  
 Dwat 0.000011 cm2/s  
 H 0.22 l water/l air  
 Owcrack 0.12

$$Dcap = Dair (Oacap \wedge 3.33/Ot \wedge 3.33) + Dwat(1/H)(Owcap \wedge 3.33/Ot \wedge 3.33)$$

Dcap 0.093035 cm2/sec  
 Dair 0.093 cm2/sec  
 Ocap 0.38  
 Ot 0.38  
 Dwat 0.000011 cm2/s  
 H 0.22 l water/l air  
 Owcap 0.342

$$Dws = (Hcap + Hv)(Hcap/Dcap + Hv/Ds) \wedge -1$$

Dws 0.026632 cm2/s  
 Hcap 5 cm  
 Hv 269 cm  
 Dcap 0.093035 cm2/s  
 Ds 0.026283

1st Term 274  
 2nd Term 0.000097

$$VFwesp = H(Dws/Lgw/(ER*Lb)/1 + (Dws/Lgw/(ER*Lb) + Dws/Lgw/(Dcrack/Lcrack) \wedge n) \times 1000$$

VFwesp 0.007552 kg/m3  
 H 0.22 l water/l air  
 Dws 0.026602  
 Lgw 274  
 ER 0.0028  
 Lb 1010  
 Dcrack 0.026283 g/cm3  
 Lcrack 15  
 n 0.01

1st Term 0.007553  
 2nd Term 0.000034  
 3rd Term 0.000103

$$RBSLw = RBSLair \times 0.001/VFwesp$$

RBSLw 0.065333 mg/l  
 or 65.33318 ug/l

MONTGOMERY WARDS – DUBLIN  
 HEALTH RISK ASSESSMENT  
 Gasoline Vapor Impacts/Revised assumptions – Indoor Air

$$RBSL(air) = (TR)(BW)(ATc)(365)(1000)/(SFi*IR*EF*ED)$$

RBSL(air) 84.16471 (ug/m3)

TR 0.00001  
 BW 70 kg  
 ATc 70 years  
 SFi 0.0017 (mg/kg-day)<sup>-1</sup>  
 IRair 20 m3/day  
 EF 250 days/year  
 ED 25 years

$$Ds = Dair (Oas \wedge 3.33/Ot \wedge 3.33) + Dwat(1/H)(Ows \wedge 3.33/Ot \wedge 3.33)$$

Ds 0.026283 (cm2/sec)  
 Dair 0.093 cm2/s  
 Oas 0.26  
 Ot 0.38  
 Dwat 0.000011 cm2/s  
 H 0.22 l water/l air  
 Ows 0.12

$$Dcrack = Dair (Oacrack \wedge 3.33/Ot \wedge 3.33) + Dwat(1/H)(Owcrack \wedge 3.33/Ot \wedge 3.33)$$

Dcrack 0.026283 cm2/sec  
 Dair 0.093 cm2/sec  
 Oacrack 0.26  
 Ot 0.38  
 Dwat 0.000011 cm2/s  
 H 0.22 l water/l air  
 Owcrack 0.12

$$Dcap = Dair (Oacap \wedge 3.33/Ot \wedge 3.33) + Dwat(1/H)(Owcap \wedge 3.33/Ot \wedge 3.33)$$

Dcap 0.093035 cm2/sec  
 Dair 0.093 cm2/sec  
 Ocap 0.38  
 Ot 0.38  
 Dwat 0.000011 cm2/s  
 H 0.22 l water/l air  
 Owcap 0.342

$$Dws = (Hcap + Hv)(Hcap/Dcap + Hv/Ds) \wedge -1$$

Dws 0.026632 cm2/s  
 Hcap 5 cm  
 Hv 269 cm  
 Dcap 0.093035 cm2/s  
 Ds 0.026283 cm2/sec

1st Term 274  
 2nd Term 0.000097

$$VFwesp = H(Dws/Lgw/(ER*Lb)/1 + (Dws/Lgw/(ER*Lb) + Dws/Lgw/(Dcrack/Lcrack) \wedge n) \times 1000$$

VFwesp 0.00756 kg/m3  
 H 0.22 l water/l air  
 Dws 0.026632 cm2/sec  
 Lgw 274 cm  
 ER 0.0028 1/sec  
 Lb 1010 cm  
 Dcrack 0.026283 g/cm3  
 Lcrack 15 cm  
 n 0.01

1st Term 0.007561  
 2nd Term 0.000034  
 3rd Term 0.000104

$$RBSLw = RBSLair \times 0.001/VFwesp$$

RBSLw 11.13245 mg/l  
 or 11132.45 ug/l

MONTGOMERY WARDS – DUBLIN  
 HEALTH RISK ASSESSMENT  
 Gasoline Vapor Impacts/Revised assumptions – Indoor Air

$$RBSL(air) = (TR)(BW)(ATc)(365)(1000)/(SF_i \cdot IR \cdot EF \cdot ED)$$

RBSL(air) 8.416471 (ug/m3)

TR 1.0E-06  
 BW 70 kg  
 ATc 70 years  
 SF<sub>i</sub> 0.0017 (mg/kg-day)<sup>-1</sup>  
 IR<sub>air</sub> 20 m3/day  
 EF 250 days/year  
 ED 25 years

$$D_s = D_{air} (O_{as} \wedge 3.33 / O_t \wedge 3.33) + D_{wat}(1/H)(O_{ws} \wedge 3.33 / O_t \wedge 3.33)$$

D<sub>s</sub> 0.026283 (cm2/sec)  
 D<sub>air</sub> 0.093 cm2/s  
 O<sub>as</sub> 0.26  
 O<sub>t</sub> 0.38  
 D<sub>wat</sub> 0.000011 cm2/s  
 H 0.22 l water/l air  
 O<sub>ws</sub> 0.12

$$D_{crack} = D_{air} (O_{acrack} \wedge 3.33 / O_t \wedge 3.33) + D_{wat}(1/H)(O_{wcrack} \wedge 3.33 / O_t \wedge 3.33)$$

D<sub>crack</sub> 0.026283 cm2/sec  
 D<sub>air</sub> 0.093 cm2/sec  
 O<sub>acrack</sub> 0.26  
 O<sub>t</sub> 0.38  
 D<sub>wat</sub> 0.000011 cm2/s  
 H 0.22 l water/l air  
 O<sub>wcrack</sub> 0.12

$$D_{cap} = D_{air} (O_{acap} \wedge 3.33 / O_t \wedge 3.33) + D_{wat}(1/H)(O_{wcap} \wedge 3.33 / O_t \wedge 3.33)$$

D<sub>cap</sub> 0.093035 cm2/sec  
 D<sub>air</sub> 0.093 cm2/sec  
 O<sub>acap</sub> 0.38  
 O<sub>t</sub> 0.38  
 D<sub>wat</sub> 0.000011 cm2/s  
 H 0.22 l water/l air  
 O<sub>wcap</sub> 0.342

$$D_{ws} = (H_{cap} + H_v)(H_{cap}/D_{cap} + H_v/D_s)^{-1}$$

D<sub>ws</sub> 0.026632 cm2/s  
 H<sub>cap</sub> 5 cm  
 H<sub>v</sub> 269 cm  
 D<sub>cap</sub> 0.093035 cm2/s  
 D<sub>s</sub> 0.026283 cm2/sec

1st Term 274  
 2nd Term 0.000097

$$VF_{wesp} = H(D_{ws}/L_{gw}/(ER \cdot L_b)/1 + (D_{ws}/L_{gw}/(ER \cdot L_b)) + D_{ws}/L_{gw}/(D_{crack}/L_{crack})^n \times 1000$$

VF<sub>wesp</sub> 0.00756 kg/m3  
 H 0.22 l water/l air  
 D<sub>ws</sub> 0.026632 cm2/sec  
 L<sub>gw</sub> 274 cm  
 ER 0.0028 1/sec  
 L<sub>b</sub> 1010 cm  
 D<sub>crack</sub> 0.026283 g/cm3  
 L<sub>crack</sub> 15 cm  
 n 0.01

1st Term 0.007561  
 2nd Term 0.000034  
 3rd Term 0.000104

$$RBSL_w = RBSL_{air} \times 0.001 / VF_{wesp}$$

RBSL<sub>w</sub> 1.13245 mg/l  
 or 113.245 ug/l



MONTGOMERY WARDS – DUBLIN  
 HEALTH RISK ASSESSMENT  
 Benzene Impacts – Outdoor Air Concentrations

$$RBSL(air) = (TR)(BW)(ATc)(365)(1000)/(SFI*IR*EF*ED)$$

RBSL(air) 4.933793 (ug/m3)

TR 0.00001  
 BW 70 kg  
 ATc 70 years  
 SFI 0.029 (mg/kg-day) -1  
 IRair 20 m3/day  
 EF 250 days/year  
 ED 25 years

$$RBSL(water) = RBSL(air) * 0.001 / VFwamb$$

RBSL 20.64413 mg/l - H2O  
 20644.13 ug/l - H2O

RBSL(a) 4.933793 (ug/m3)  
 VFwamb 0.000239 (mg/m3)(mg/l)

$$VFwamb = H \times 1000 \text{ l/m}^3 / [1 + (Uair * oair * Lgw / (W * Dws))]$$

VFwamb 0.000239 (mg/m3)(mg/l)

H 0.22 l water/l air  
 Uair 894 cm/s  
 oair 244 cm  
 Lgw 274 cm  
 W 2438 cm  
 Dws 0.026632 cm2/sec

$$Ds = Dair (Oas \wedge 3.33 / Ot \wedge 3.33) + Dwat(1/H) (Ows \wedge 3.33 / Ot \wedge 3.33)$$

Ds 0.026283 (cm2/sec)  
 Dair 0.093 cm2/s  
 Oas 0.26  
 Ot 0.38  
 Dwat 0.000011 cm2/s  
 H 0.22 l water/l air  
 Ows 0.12

$$Dcap = Dair (Oacap \wedge 3.33 / Ot \wedge 3.33) + Dwat(1/H) (Owcap \wedge 3.33 / Ot \wedge 3.33)$$

Dcap 0.093035 cm2/sec  
 Dair 0.093 cm2/sec  
 Oacap 0.38  
 Ot 0.38  
 Dwat 0.000011 cm2/s  
 H 0.22 l water/l air  
 Owcap 0.342

$$Dws = (Hcap + Hv) (Hcap / Dcap + Hv / Ds) \wedge -1$$

Dws 0.026632 cm2/s  
 Hcap 5 cm  
 Hv 269 cm  
 Dcap 0.093035 cm2/s  
 Ds 0.026283

1st Term 274  
 2nd Term 0.000097

1233TB9

MONTGOMERY WARDS – DUBLIN  
 HEALTH RISK ASSESSMENT  
 Benzene Impacts – Outdoor Air Concentrations

$$RBSL(air) = (TR)(BW)(ATc)(365)(1000)/(SFi*IR*EF*ED)$$

RBSL(air) 0.493379 (ug/m3)

TR 1.0E-06  
 BW 70 kg  
 ATc 70 years  
 SFi 0.029 (mg/kg-day)-1  
 IRair 20 m3/day  
 EF 250 days/year  
 ED 25 years

$$RBSL(water) = RBSL(air)*0.001/VFwamb$$

RBSL 2.064413 mg/l-H2O  
 2064.413 ug/l-H2O

RBSL(a) 0.493379 (ug/m3)  
 VFwamb 0.000239 (mg/m3)(mg/l)

$$VFwamb = H \times 1000 \text{ l/m}^3 / [1 + (Uair \times oair \times Lgw / (W \times Dws))]$$

H 0.22 l water/l air  
 Uair 894 cm/s  
 oair 244 cm  
 Lgw 274 cm  
 W 2438 cm  
 Dws 0.026632 cm2/sec

$$Ds = Dair (Oas \wedge 3.33 / Ot \wedge 3.33) + Dwat(1/H)(Ows \wedge 3.33 / Ot \wedge 3.33)$$

Ds 0.026283 (cm2/sec)  
 Dair 0.093 cm2/s  
 Oas 0.26  
 Ot 0.38  
 Dwat 0.000011 cm2/s  
 H 0.22 l water/l air  
 Ows 0.12

$$Dcap = Dair (Oacap \wedge 3.33 / Ot \wedge 3.33) + Dwat(1/H)(Owcap \wedge 3.33 / Ot \wedge 3.33)$$

Dcap 0.093035 cm2/sec  
 Dair 0.093 cm2/sec  
 Ocap 0.38  
 Ot 0.38  
 Dwat 0.000011 cm2/s  
 H 0.22 l water/l air  
 Owcap 0.342

$$Dws = (Hcap + Hv)(Hcap/Dcap + Hv/Ds) \wedge -1$$

Dws 0.026632 cm2/s  
 Hcap 5 cm  
 Hv 269 cm  
 Dcap 0.093035 cm2/s  
 Ds 0.026283

1st Term 274  
 2nd Term 0.000097

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HEALTH RISK ASSESSMENT  
 TPH Impacts—Outdoor Air Concentrations

$$RBSL(air) = (TR)(BW)(ATc)(365)(1000)/(SFi*IR*EF*ED)$$

RBSL(air) 84.16471 (ug/m3)

TR 0.00001  
 BW 70 kg  
 ATc 70 years  
 SFi 0.0017 (mg/kg-day)<sup>-1</sup>  
 IRair 20 m3/day  
 EF 250 days/year  
 ED 25 years

$$RBSL(water) = RBSL(air)*0.001/VFwamb$$

RBSL 352.1646 mg/l-H2O  
 352164.6 ug/l-H2O

RBSL(a) 84.16471 (ug/m3)  
 VFwamb 0.000239 (mg/m3)(mg/l)

$$VFwamb = H \times 1000 \text{ l/m}^3 / [1 + (Uair*oair*Lgw/(W*Dws))]$$

VFwamb 0.000239 (mg/m3)(mg/l)

H 0.22 l water/l air  
 Uair 894 cm/s  
 oair 244 cm  
 Lgw 274 cm  
 W 2438 cm  
 Dws 0.026632 cm2/sec

$$Ds = Dair (Oas \wedge 3.33/Ot \wedge 3.33) + Dwat(1/H)(Ows \wedge 3.33/Ot \wedge 3.33)$$

Ds 0.026283 (cm2/sec)  
 Dair 0.093 cm2/s  
 Oas 0.26  
 Ot 0.38  
 Dwat 0.000011 cm2/s  
 H 0.22 l water/l air  
 Ows 0.12

$$Dcap = Dair (Oacap \wedge 3.33/Ot \wedge 3.33) + Dwat(1/H)(Owcap \wedge 3.33/Ot \wedge 3.33)$$

Dcap 0.093035 cm2/sec  
 Dair 0.093 cm2/sec  
 Ocap 0.38  
 Ot 0.38  
 Dwat 0.000011 cm2/s  
 H 0.22 l water/l air  
 Owcap 0.342

$$Dws = (Hcap + Hv)(Hcap/Dcap + Hv/Ds) \wedge -1$$

Dws 0.026632 cm2/s  
 Hcap 5 cm  
 Hv 269 cm  
 Dcap 0.093035 cm2/s  
 Ds 0.026283

1st Term 274  
 2nd Term 0.000097

1233tcb

HEALTH RISK ASSESSMENT  
 TPH Impacts—Outdoor Air Concentrations

$$RBSL(air) = (TR)(BW)(ATc)(365)(1000)/(SFi*IR*EF*ED)$$

RBSL(air) 8.416471 (ug/m3)

TR 1.0E-06  
 BW 70 kg  
 ATc 70 years  
 SFi 0.0017 (mg/kg-day) - 1  
 IRair 20 m3/day  
 EF 250 days/year  
 ED 25 years

$$RBSL(water) = RBSL(air)*0.001/VFwamb$$

RBSL 35.21646 mg/l-H2O  
 35216.46 ug/l-H2O

RBSL(a) 8.416471 (ug/m3)  
 VFwamb 0.000239 (mg/m3)(mg/l)

$$VFwamb = H \times 1000 \text{ l/m}^3 / [1 + (Uair \times oair \times Lgw / (W \times Dws))]$$

VFwamb 0.000239 (mg/m3)(mg/l)

H 0.22 l water/l air  
 Uair 894 cm/s  
 oair 244 cm  
 Lgw 274 cm  
 W 2438 cm  
 Dws 0.026632 cm2/sec

$$Ds = Dair (Oas \wedge 3.33 / Ot \wedge 3.33) + Dwat(1/H) (Ows \wedge 3.33 / Ot \wedge 3.33)$$

Ds 0.026283 (cm2/sec)  
 Dair 0.093 cm2/s  
 Oas 0.26  
 Ot 0.38  
 Dwat 0.000011 cm2/s  
 H 0.22 l water/l air  
 Ows 0.12

$$Dcap = Dair (Oacap \wedge 3.33 / Ot \wedge 3.33) + Dwat(1/H) (Owcap \wedge 3.33 / Ot \wedge 3.33)$$

Dcap 0.093035 cm2/sec  
 Dair 0.093 cm2/sec  
 Oacap 0.38  
 Ot 0.38  
 Dwat 0.000011 cm2/s  
 H 0.22 l water/l air  
 Owcap 0.342

$$Dws = (Hcap + Hv)(Hcap/Dcap + Hv/Ds) \wedge -1$$

Dws 0.026632 cm2/s  
 Hcap 5 cm  
 Hv 269 cm  
 Dcap 0.093035 cm2/s  
 Ds 0.026283

1st Term 274  
 2nd Term 0.000097

1233tbc