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April 25, 1997
941114NA

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Division of Environmental Protection
Department of Environmental Health
Alameda County Health Agency
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Alameda, California 94502

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ENVIRONMENTAL PROTECTION

Subject: Transmittal of RBCA Evaluation Report for the 40th Street Right-of-Way
Emeryville, California

Dear Ms. Hugo:

On behalf of the City of Emeryville Redevelopment Agency, transmitted herewith is the subject site RBCA evaluation results for your review and approval. The RBCA evaluation followed the steps detailed in the workplan (February 5, 1997), which was approved by the County in a letter to the City of Emeryville dated March 7, 1997.

Please do not hesitate to call me at (510) 874-3060 or Mr. Ignacio Dayrit at (510) 596-4356 for questions or comments.

Sincerely,

Xinggang Tong, P.E., Ph.D.
Project Manager

Enclosure.

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REPORT

DEVELOPMENT OF SITE-SPECIFIC TARGET LEVELS FOR SOIL AND GROUNDWATER

40TH STREET RIGHT-OF-WAY EMERYVILLE, CALIFORNIA

Prepared for

City of Emeryville Redevelopment Agency
2200 Powell Street, 12th Floor
Emeryville, CA 94608-4356

April 1997

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1.1 PURPOSE OF REPORT

The purpose of this report is to present the results of a risk-based evaluation to develop site-specific target levels (SSTLs) for chemicals detected in soil, and shallow groundwater for the 40th Street Right-of-Way between San Pablo Avenue and Adeline Street in Emeryville, California (the site). This report was prepared by Woodward-Clyde Consultants (WCC) on behalf of the City of Emeryville Redevelopment Agency (the City).

Following the recommendations in the Regional Water Quality Control Board (RWQCB) - San Francisco Bay Region's Directive of January 5, 1996, a Risk-Based Corrective Action (RBCA) evaluation based on the ASTM Standard E-1739-95 was used to develop the SSTLs. The RBCA evaluation approach for the site was outlined in the Closure Workplan for the Former Celis Alliance Fuel Station (WCC 1996), which was approved by the Alameda County Department of Environmental Health (ACDEH) in a letter to the City dated December 11, 1996. Details about site-specific approach and parameters for the risk-based evaluation were presented for review and approval prior to initiating the evaluation in the RBCA approach workplan (WCC 1997) to the ACDEH dated February 5, 1997. ACDEH approved the RBCA approach workplan in a letter to the City dated March 7, 1997. The soil and groundwater SSTLs developed here were utilized to evaluate the need and extent of remediation activities at the site, with the goal of ultimately obtaining a no further action (NFA) decision from the ACDEH.

The risk-based evaluation was performed according to the American Society for Testing and Materials (ASTM) Risk-Based Corrective Action (RBCA) methodology (ASTM 1995). The RBCA methodology is a consistent and comprehensive approach to risk-based remediation of site contamination based on the protection of human health and environmental resources (e.g., groundwater quality). RBCA is also a risk management tool that may be used to support the selection of appropriate remedial measures. The RBCA methodology evaluates sites according to a tiered approach of increased site-specificity and released conservatism. Tier 1 is applied to initially classify the site, and screen for chemicals and areas of concern using non-site-specific risk-based screening levels (RBSLs). Site-specific risk-based target levels (SSTLs) are then developed using Tier 2. The SSTLs represent a conservative starting point for development of cleanup goals, which are the result of risk management decisions based on protection of human health and environment, and other remedial action criteria such as feasibility, cost effectiveness, public acceptability, etc.

Section 2.0 of this report presents the RBCA Tier 1 screening evaluation. Section 3.0 provides the development of SSTLs for the site according to RBCA Tier 2. Conclusions and recommendations are provided in Section 4.0. Uncertainties and limitations of this report are discussed in Section 5.0. References are in Section 6.0.

1.2 THE ASTM RISK-BASED CORRECTIVE ACTION TIER 1 AND 2 PROCESSES

A brief description of the ASTM RBCA Tier 1 and Tier 2 processes is provided below.

RBCA Tier 1

The scope of the RBCA Tier 1 process is to classify the site in terms of urgency of need for initial corrective action, based on (1) historical information, (2) visual inspection, and (3) available site assessment data.

Specifically, Tier 1 consists of the following:

- Identification of site-related contaminant sources, obvious environmental impacts, potential transport pathways, and potentially impacted receptors.
- Comparison of site-related contaminant concentrations with conservative corrective action goals based on a list of non-site-specific risk-based screening levels (RBSLs) and other appropriate standards.

The sequence of tasks and decisions associated with the RBCA Tier 1 process are outlined below:

Step 1: Initial Site Assessment, involving source characterization, potential for exposure and degradation of beneficial uses, extent of migration, and summary of results.

Step 2: Site Classification and Initial Response Action, based on the scenarios and actions recommended in Table 1 of the RBCA guidance (ASTM 1995).

Step 3: Comparison of Site Conditions with Tier 1 RBSLs and Tier 1 Corrective Action Selection, involving exposure pathway characterization, exposure scenario characterization, selection of acceptable risk range, comparison of chemical concentrations with RBSLs, corrective action assessment, and evaluation of Tier 1 results.

Tier 1 RBSLs are based on default exposure factors and generic site characteristics. Since the exposure and site parameters are not site-specific, the RBSLs incorporate a great amount of conservatism, and therefore they are quite stringent. According to the RBCA guidance, if chemical concentrations detected in soil and groundwater at the site exceed the Tier 1 RBSLs, after the initial RBCA Tier 1 assessment, the site should be evaluated and classified according to Tier 2.

RBCA Tier 2

In Tier 2, site-specific risk-based target levels (SSTLs) for the chemicals and exposure scenarios of concern are developed based on site-specific input parameters. Comparison of site chemical concentrations in soil and groundwater with the SSTLs allows risk managers to evaluate whether the site may be closed without need of further action or, if appropriate, identify specific areas where additional consideration in terms of investigation/remediation is required.

1.3 ASSUMPTIONS OF THIS STUDY

This risk-based evaluation of soil and shallow groundwater was performed according to the methods described in the ASTM guidance E 1739-95 "Emergency Standard Guide for Risk-Based Corrective Action Applied at Petroleum Release Sites" (ASTM 1995), provided in Appendix B. The RBCA methodology evaluates sites according to a tiered approach of increased

site-specificity and released conservatism. Tier 1 is applied to initially classify the site, and screen for compounds and areas of concern using non-site-specific risk-based screening levels (RBSLs). Site-specific risk-based target levels (SSTLs) are then developed using Tier 2. The SSTLs represent a conservative starting point for development of cleanup goals, which are the result of risk management decisions based on protection of human health and environment, and other remedial action criteria such as feasibility, cost effectiveness, public acceptability, etc., as explained in detail in Section 3.3.

The RBCA Tier 1 and Tier 2 evaluation was applied using the following overall approach and assumptions (approved by ACDEH) for the site:

Overall Approach

For each of the areas of concern, the maximum detected media concentration was compared with the appropriate Tier 1 RBSL concentration. If the maximum detections do not exceed RBSL in a given area, the area is considered not of concern. If RBSLs are exceeded, a new set of SSTLs is generated according to Tier 2, as appropriate. Soil and groundwater that exceed Tier 2 SSTLs are recommended for further consideration in terms of additional investigation and/or remedial action.

Source Characterization

Chemicals of concern for the risk-based assessment include the following:

- Gasoline and diesel indicator compounds: benzene, toluene, ethylbenzene, xylenes (BTEX), benzo(a)pyrene, and naphthalene.
- MTBE and lead.

In case benzo(a)pyrene and naphthalene data were not available for soil and groundwater in a specific area, concentration for these compounds was based on available total petroleum hydrocarbon (TPH) as diesel data assuming the following: naphthalene concentration is 0.13 percent of TPH diesel concentration (Calabrese et al., 1993), and benzo(a)pyrene concentration is 0.07 milligrams (mg) for every kilogram (kg) of TPH diesel detected (Guerin et al., 1984).

Due to the historical nature of the hydrocarbon source(s), MTBE is not expected to be a significant concern at the site. However, we developed SSTLs for MTBE to provide reference criteria for future monitoring activities.

For lead in soil we used the USEPA Region 9 Industrial PRG of 1,000 mg/kg as screening level. If necessary, a lead SSTL can be developed using the Cal-EPA DTSC Leadspread model. Due to the very low detected concentration with respect to screening level, lead was not considered further in this assessment.

Exposure Scenarios and Assumptions

1) The site conceptual model illustrated in Figures 3 and 4 provides a schematic illustration of plausible chemical migration pathways and potential exposure scenarios relevant for the site.

2) Soil SSTLs were developed for an outdoor residential exposure scenario, since the present and future land use for the site is to continue to be a city street. It was conservatively assumed that residents (adults and children) in the area may be spending up to two hours per day at the site, 350 days per year, for 30 years.

3) Shallow groundwater SSTLs were developed for an indoor commercial exposure scenario, since the shallow groundwater may migrate off-site, and the land use of the properties downgradient of the site is commercial.

4) We evaluated a construction worker scenario, to verify that the above described soil SSTLs are also protective of construction workers.

5) The exposure pathway of concern for residential and commercial receptors is inhalation of vapor emissions from soil and from shallow groundwater. It is assumed that the site will remain covered with the existing asphalt pavement.

6) The exposure pathway of concern for construction receptors is the "surficial soil" pathway, as defined by ASTM RBCA, including inhalation of vapor and particulate emissions from soil and direct contact with soil.

7) Exposure point concentrations for the vapor emission estimations were based on detected concentrations averaged over the respective area of emission and depth of emission. Where appropriate, particular "hot spots" were addressed individually.

8) Shallow groundwater at the site is not considered a viable source of drinking water, since the water supply wells in the area are screened in hydraulically separated units, and are located at considerable distance from the site.

9) Soil and groundwater SSTLs were calculated for a cancer risk level of 1×10^{-5} and a chronic hazard quotient of 1.

2.1 SCOPE OF RBCA TIER 1

The scope of the RBCA Tier 1 process is to classify the site in terms of urgency of need of initial corrective action, based on (1) historical information, (2) visual inspection, and (3) minimal site assessment data.

Specifically, Tier 1 consists of the following:

- Identification of site-related contaminant sources, environmental impacts, potential transport pathways, and potentially impacted receptors.
- Comparison of site-related contaminant concentrations with conservative corrective action goals based on a list of non-site-specific risk-based screening levels (RBSLs) and other appropriate standards.

Information about the environmental setting at the site and a description of the implementation of the above tasks associated with the RBCA Tier 1 process is described below.

2.2 DESCRIPTION OF SITE ENVIRONMENTAL CONDITIONS

The site is now the section of 40th Street Right-of-Way between San Pablo Avenue and Adeline Street in Emeryville, California (Figure 1), and is approximately 0.83 acres. Prior to the road construction, the site was occupied by the former Celis Alliance Fuel Station (Former Celis Area), the former Anderson Linoleum and Carpet Sales warehouse (Former Warehouse Area), and a portion of an asphalt-paved parking lot (Former Parking Lot Area). In June 1993, Levine-Fricke (1993a) conducted a Phase I environmental site assessment (ESA) on the site. Geologically, the Phase I ESA investigation found that the site is underlain by Holocene alluvial deposits, primarily unconsolidated, fine sand, silt, and clayey silt with occasional thin beds of coarse sand. The site is located approximately 1 mile east of the San Francisco Bay and is essentially flat, with an approximate elevation of 40 feet above mean sea level. The area was redeveloped in 1995 into part of the 40th Street Right-of-Way and was paved with asphalt-concrete mixture. Properties next to the site are either streets or parking lots also having asphalt-concrete surface. Subsurface TPH contamination is a regional problem. Several TPH-affected parcels exist in the area. Information about each of the three areas (see Figure 2) are provided below.

Former Celis Area

The former Celis Alliance Fuel Station was located at 4000 San Pablo Avenue, and occupied an area of approximately 100 feet by 100 feet. A commercial fueling and auto service station operated at the site since 1936 (it ceased operation in April 1994). The station contained a service garage with an attached office and canopy, and one fuel dispenser island, as shown on Figure 2. Environmental conditions of this area can be summarized as follows:

- All underground storage tanks and associated piping were removed in 1994.
- The area has been extensively characterized. Soil and groundwater samples collected at various times from both on- and off-site locations were analyzed for TPH as gasoline, diesel, motor oil, oil and grease, BTEX, organic lead, PCBs, Creosote, PNAs, halogenated VOCs,

and metals (Cd, Cr, Pb, Ni, Zn, and WET CAM 17 metals). Results from these investigations indicate that only petroleum hydrocarbons (TPHg, TPHd, and BTEX) appear to be constituents of concern.

- Three on-site groundwater monitoring wells were installed in 1993 and one downgradient off-site groundwater monitoring well was installed in 1994. Free product was found in one of the on-site monitoring wells (LF-1, now destroyed), but not in others.
- On-site soil from surface to groundwater table was removed and disposed of off-site in 1994. The three on-site monitoring wells were destroyed. Soil samples collected from the side walls and the bottom of the excavation pit showed benzene concentrations up to 3.8 mg/kg, TPHg up to 1,000 mg/kg, and TPHd up to 18,000 mg/kg in the area where the free product was measured in the monitoring well. Clean soil was imported to fill the excavation.

Former Warehouse Area

The warehouse building, built in 1957 or before, was located in the center of the site, directly behind the fuel station and was occupied by Anderson Linoleum and Carpet Sales in 1993. The entrance to the warehouse faced Adeline Street, and consisted of loading docks and doors. The area directly in front of the loading docks was concrete-paved with remainder of the area paved with asphalt (Levine-Fricke, 1993a). The interior of the warehouse was observed to contain large rolls of linoleum, carpet, padding, and several containers of floor adhesive, and was used for storage (Levine-Fricke, 1993b). A monitoring well, MW-1, located immediately adjacent to the concrete-paved area along the site boundary, was installed in September 1992 to assess soil and groundwater quality in the vicinity of two former 10,000-gallon USTs (one containing diesel and the other gasoline) removed in 1989 (Levine-Fricke, 1993b). The well was sampled on a quarterly basis since September 1992 and was abandoned on November 1994. The two USTs and the monitoring well belonged to the former San Francisco Bread Company site, which was located adjacent to and north of the site.

In 1993, one soil boring was drilled approximately 15 feet southwest of MW-1 and three soil samples were collected at depths of 4, 5, 7, and 12 feet bgs and analyzed for BTEX, TPH-gas, -diesel,-motor oil, TRPH, VOCs, PCBs, and SVOCs (Levine-Fricke, 1993b). Results indicated concentrations of TPH-g (up to 500 mg/kg) and benzene, toluene, ethylbenzene, and xylene at maximum concentrations of 4, 27, 12, and 69 mg/kg, respectively. TRPH was detected at concentrations of 70 mg/kg or less. No other VOCs, nor PCBs were detected in any of the soil samples. Naphthalene, 2-methylnaphthalene, and 4-methylphenol were detected at concentrations of 1.7, 1.8, and 0.4 mg/kg, respectively (Levine-Fricke, 1993b). Results for groundwater samples collected from MW-1 indicated TPH-gas and benzene at concentrations of 2.9 and 0.470 mg/L, respectively (Levine-Fricke, 1993b). → 5.8 → 1.7 (3/94)

In 1994, Levine-Fricke (1994) drilled 16 soil borings east of the service station, of which 5 were located inside the warehouse, to a depth of approximately 10 feet. The samples near the former San Francisco Bread Company UST location indicated the presence of TPH-gas and benzene, toluene, ethylbenzene, and xylenes (BTEX) at concentrations up to 8,800, 14, 62, 190, and 870 mg/kg, respectively. TPH-gas and BTEX were detected inside the warehouse at maximum concentrations of 690, 12, 50, 18, and 99 mg/kg, respectively.

Soil was excavated in the vicinity of B3 (120 cubic yards) and B4 (175 cubic yards) from surface to 8 to 10 feet bgs (Levine-Fricke, 1994). No confirmation samples were taken but relatively elevated PID measurements indicated that some affected soil remains in place.

Former Parking Lot Area

Railroad tracks previously crossed San Pablo Avenue and the adjacent sidewalk. Portions of the railroad tracks, present since 1947, have been either paved over in place or removed approximately in 1992 and the roadway or sidewalk surface repaved with asphalt.

Seven soil borings were drilled to depths ranging from 3.5 to 7 feet bgs, and 14 soil samples were collected to depths ranging from 1 foot to 6.5 feet and analyzed for TPH-gas, -diesel, -motor oil, TRPH, and PCBs (Levine-Fricke, 1993b). Results indicated significant concentrations of TPH-gas (up to 6,500 mg/kg), TPH-diesel and TPH-motor oil maximum detections were 560 and 740 mg/kg, respectively. TRPH was detected at concentrations up to 4,600 mg/kg, and PCBs (aroclor 1260) was detected in one sample (SB-14) at a concentration of 0.22 mg/kg (Levine-Fricke, 1993b).

In 1994, soil was excavated in the vicinity of SB-12 (55 cubic yards), SB-15 (55 cubic yards), SB-18 (30 cubic yards), and SB19 (30 cubic yards) to a depth of approximately 6 feet bgs (Levine-Fricke, 1994). Confirmation samples were collected from the excavations in the vicinity of SB-12 and SB-15 and indicate that elevated concentrations of TPH-gas and BTEX remain at the southern and western sidewalls at approximately 7 feet bgs, and at the base of the excavation at approximately 8 feet bgs (Levine-Fricke, 1994).

2.3 CONCEPTUAL SITE MODEL

Figure 3 illustrates the potential exposure scenarios for the site. The site conceptual model presented in Figure 4 provides a schematic description of chemical migration pathways and potential exposure scenarios relevant for the site. Based on the site conceptual model, the potential sources of chemicals at the site are represented by past spills or leaks from USTs into soil.

Chemicals may be released from soil into air as a result of emissions of soil vapors and/or particulates (in case the soil is uncovered, for instance, during excavation of trenches for utility work). Chemicals may be released from soil into shallow groundwater due to leaching and vertical infiltration. Further downward and lateral migration may potentially affect deeper groundwater.

Exposure to chemicals in air may occur through the inhalation route. Exposure to chemicals in soil may occur through the incidental ingestion and dermal contact routes. Exposure to chemicals in water may occur through the ingestion and dermal contact routes. Impact of chemicals on water quality may occur through groundwater withdrawal (e.g., if the water is pumped for domestic or municipal water supply).

Exposure receptors of potential concern at the site are (see Figure 3 and 4):

- Residents passing by (e.g., waiting at the bus stop).
- Off-site commercial workers (e.g., employees at the nearby liquor store).

- Construction workers (e.g., during utility trenches excavation).

The importance of each of the exposure routes associated with the above receptors is represented in Figure 4 by a black dot for potentially significant (complete) pathways, and by a white dot for minor or insignificant pathways (which are evaluated in a qualitative way only). Quantitative target levels for cleanup are developed based on exposure scenarios involving potentially significant pathways (black dots).

As long as the existing asphalt/concrete pavement is left undisturbed, the potential for impact on human health through direct contact is evaluated to be insignificant. Groundwater beneath the site may be affected by chemicals leaching from the soil. Exposure to construction workers due to contact with groundwater is evaluated to be insignificant. Exposure to ecological receptors is evaluated to be insignificant due to the residential/commercial land use of the site. In addition, the pavement prevents potential exposure to biota.

In conclusion, based on the above evaluations, we developed soil target levels for the protection of receptors potentially exposed under the following exposure scenarios:

- Residents potentially exposed to chemicals in air via inhalation of volatile emissions from soil.
- Commercial workers potentially exposed to chemicals in air via inhalation of volatile and particulate emissions from shallow groundwater.
- Construction workers potentially exposed to chemicals in air and soil via inhalation of volatile and particulate emissions and direct contact with soil.

Target excess cancer risk for this assessment was selected as $1x10^{-5}$ (1 in 100,000) for both exposure scenarios. This means that soil and groundwater screening and target levels are calculated for a cancer risk level of $1x10^{-5}$ and a chronic hazard quotient of 1 for both current and potential future on-site commercial receptors. This cancer risk level is within the target range of $1x10^{-6}$ to $1x10^{-4}$, described as acceptable by the U.S. EPA in the National Contingency Plan (NCP, 40 CFR Part 300).

2.4 TIER 1 SCREENING

Tables 1 and 2 provide the maximum reported residual soil and shallow groundwater chemical concentrations for each area of concern after the excavation of soil. Tables 3 and 4 present the comparison of maximum detected on-site soil and shallow groundwater concentration with ASTM RBCA non-site-specific RBSLs and other relevant screening level criteria. Lead was not included in the tables as a chemical of concern, since it was detected at concentrations well below the screening criterion.

Tier 1 RBSLs reported in Table 3 are the screening level soil concentrations for volatilization to outdoor air for residential scenario and for the surficial soil pathway (which is indicative of exposure due to intrusive activities such as construction). Tier 1 RBSLs reported in Table 4 are the screening level water concentrations for indoor vapor emissions from groundwater for commercial receptors. Only the BTEX and PNA compounds are considered in the comparisons. The other compounds listed in Tables 1 and 2 (e.g., 2-methylnaphthalene, Aroclor, etc.) are not

- Construction workers(e.g., during utility trenches excavation).

The importance of each of the exposure routes associated with the above receptors is represented in Figure 4 by a black dot for potentially significant (complete) pathways, and by a white dot for minor or insignificant pathways (which are evaluated in a qualitative way only). Quantitative target levels for cleanup are developed based on exposure scenarios involving potentially significant pathways (black dots).

As long as the existing asphalt/concrete pavement is left undisturbed, the potential for impact on human health through direct contact is evaluated to be insignificant. Groundwater beneath the site may be affected by chemicals leaching from the soil. Exposure to ecological receptors is evaluated to be insignificant due to the residential/commercial land use of the site. In addition, the pavement prevents potential exposure to biota.

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carried in the Tier 1 comparisons due to the very low detection frequency and/or concentrations, which makes them unimportant from the risk standpoint. Petroleum mixtures (e.g., TRPH, etc.) are addressed by conservatively estimating their PNA content. Detections of methylene chloride are attributed to laboratory contamination.

The RBSLs for the BTEX and PNA compounds are taken from page 22 of the ASTM RBCA guidance. The selected target risk level is $1x10^{-6}$ for both receptors.

The results of the ASTM RBCA Tier 1 on-site screening assessment are summarized as follows:

- The Tier 1 comparisons indicate exceedance of RBSLs for benzene.
- According to ASTM RBCA guidance, because of the exceedances of screening criteria, the site will be evaluated in Tier 2 (see Section 3.0).

2.5 INITIAL SITE CLASSIFICATION ACCORDING TO RBCA TIER 1

Based on the results of the Tier 1 evaluation and on the site classification scenarios presented in Table 1 of the RBCA guidance (ASTM 1995, Appendix B), we conclude that the site should be initially classified under either Level 3: Long-Term Threat to Human Health, Safety, or Sensitive Environmental Receptors or Level 4: No Demonstrable Long-Term Threat to Human Health, Safety, or Sensitive Environmental Receptors. The final site classification depends on the results of the Tier 2 evaluation, which will indicate if chemicals present in soil and groundwater present a significant risk by developing site-specific target levels (SSTLs). The Tier 2 evaluation is presented in Section 3.0 of this report.

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2.5 INITIAL SITE CLASSIFICATION ACCORDING TO RBCA TIER 1

Based on the results of the Tier 1 evaluation and on the site classification scenarios presented in Table 1 of the RBCA guidance (ASTM 1995, Appendix B), we conclude that the site should be initially classified under either Level 3: Long-Term Threat to Human Health, Safety, or Sensitive Environmental Receptors or Level 4: No Demonstrable Long-Term Threat to Human Health, Safety, or Sensitive Environmental Receptors. The final site classification depends on the results of the Tier 2 evaluation, which will indicate if chemicals present in soil and groundwater present a significant risk by developing site-specific target levels (SSTLs). The Tier 2 evaluation is presented in Section 3.0 of this report.

3.1 DEVELOPMENT OF TIER 2 SITE-SPECIFIC TARGET LEVELS (SSTLS)

According to the RBCA process, in the cases where chemical concentrations detected in soil and groundwater at the site exceed the Tier 1 look-up table RBSL concentrations, after the initial RBCA Tier 1 screening, the site should be evaluated according to RBCA Tier 2. In Tier 2, a new set of risk-based SSTLs for the chemicals and exposure pathways of concern is developed based on site-specific input parameters. Comparison of site chemical concentrations in soil and groundwater with the SSTLs is used to evaluate whether the site may be closed without need of further remediation or, if appropriate, to identify specific areas where remediation is recommended. This section describes the development of SSTLs and presents the site-specific inputs used to calculate the SSTLs. Note that if ASTM default exposure parameters are used in the ASTM RBCA equations, the SSTLs are numerically equivalent to the RBSLs. This is demonstrated in the WCC spreadsheets attached to a letter from WCC to Shell Development Company regarding errata for RBCA ASTM, provided in this report at the end of Appendix B. Recommendations on how to use the SSTLs for remedial decisions and the final site classification according to ASTM RBCA conclude this section.

Inputs for Development of Residential SSTLs for Soil

SSTLs for soil for the residential outdoor exposure scenario were developed based on the ASTM RBCA default input parameters and equations for exposure to soil emissions. The following parameters affecting exposure to site chemicals were modified from the ASTM Tier 1 defaults to reflect relevant site-specific conditions based on field measurements and/or on professional judgment as follows:

- Exposure duration = 6 years as children and 24 years as adults
- Exposure time and frequency = 2 hours per day, 350 days per year
- Body weight = 15 kg for children.
- Emission reduction factor due to asphalt pavement = 20 percent.

The above site-specific inputs were selected to customize the residential exposure scenario to include children (as required by Cal-EPA exposure assessment guidance), and to account for the emission reduction effect of the asphalt pavement, which is not included in the outdoor scenario equations published by ASTM. A 10-fold to 100-fold emission reduction factor is usually adopted when a concrete pavement is present (Landman 1982). In our case (asphalt) the reduction factor we adopted amounts to about a 5-fold decrease. The remainder of the inputs used to calculate soil SSTLs are default values from the ASTM RBCA guidance. A summary of the inputs used in calculating the SSTLs is tabulated in Appendix C. SSTLs were calculated using the equations provided in Tables X2.2 through X2.7 of the ASTM RBCA guidance (Appendix B). The calculations spreadsheets are shown in Appendix C. Appendix D provides example calculations of SSTLs. Appendix E presents the ASTM RBCA equations.

Inputs for Development of Construction SSTLs

SSTLs for soil for the construction worker exposure scenario were developed based on the ASTM RBCA default input parameters and equations for the surficial soil pathway. The following parameters affecting exposure to site chemicals were modified from the ASTM Tier 1 defaults to reflect relevant site-specific conditions based on field measurements and/or on professional judgment as follows:

- Exposure duration = 0.5 years
- Exposure time and frequency = 8 hours per day, 5 days per week
- Particulate emission rate = 1.5E-9 g/cm^2-se

The particulate emission rate of 1.5E-9 g/cm^2-sec was chosen to correspond to a PM10 concentration of 50 µg/m^3, the maximum allowed by the Clean Air Act, representing a worst case scenario of bare soil erosion. The remainder of the inputs used to calculate SSTLs are default values from the ASTM RBCA guidance. A summary of the inputs used in calculating the SSTLs is tabulated in Appendix C. SSTLs were calculated using the equations provided in Tables X2.2 through X2.7 of the ASTM RBCA guidance (Appendix B). The calculations spreadsheets are shown in Appendix C.

Inputs for Development of Commercial SSTLs for Shallow Groundwater

SSTLs for shallow groundwater for the commercial worker exposure scenario were developed based on the ASTM RBCA default input parameters and equations for exposure to groundwater emissions. The following parameters affecting exposure to site chemicals were modified from the ASTM Tier 1 defaults to reflect relevant site-specific conditions based on field measurements and/or on professional judgment as follows:

- Emission reduction factor = 0.02 (50-fold) based on an areal fraction of cracks in concrete pavement = 5 cm^2/m^2

The areal fraction of cracks in the concrete pavement was set at 5 cm^2/m^2 to represent a good condition pavement slab. The model estimating indoor exposure to vapors relies on an estimate of "emission reduction factor", representative of the vapor barrier effect provided by (as an example) a standard ventilated crawl-space or a concrete slab-on-grade. In ASTM RBCA, the reduction factor relates to the thickness of pavement and the areal fraction of cracks. A 10-fold to 100-fold emission reduction factor is usually adopted when a concrete pavement is present (Landman 1982). In our case (6 inches thickness, 0.5% cracks) the reduction factor we adopted amounts to about a 50-fold decrease. The remainder of the inputs used to calculate the SSTLs were ASTM RBCA default values. A summary of the inputs used in calculating the SSTLs is tabulated in Appendix C. SSTLs were calculated using the equations provided in Tables X2.2 through X2.7 of the ASTM RBCA guidance (Appendix B). The calculations spreadsheets are shown in Appendix C.

Summary of ASTM RBCA Tier 2 SSTLs

Based on the above assumptions, SSTLs protective of human health for BTEX, PNAs, and MTBE were calculated for residential exposure to indoor vapors emitted from soil, commercial exposure to vapors emitted from shallow groundwater, and construction workers exposed to surficial soil, according to ASTM RBCA Tier 2. The SSTLs are presented below (see also Table 5):

Chemical	Receptor: Medium:	*Resid. Outdoor Soil SSTLs*	*Comm. Indoor Shallow GW SSTLs*
Benzene		50.0 mg/kg	2.3 mg/L
Ethylbenzene		350* mg/kg	150* mg/L
Toluene		781* mg/kg	540* mg/L
Xylene		498* mg/kg	200* mg/L
Benzo(a)pyrene		4.7* mg/kg	0.0012* mg/L
Naphthalene		400* mg/kg	31* mg/L
MTBE		9,900* mg/kg	51,000* mg/L

** Target risk level is not exceeded above the soil saturation or water solubility concentration shown, hence the SSTL is set at saturation or solubility.*

The benzene SSTL for construction workers scenario is 1,300 mg/kg (see Appendix C). The construction worker SSTL are not shown above since the residential SSTLs are protective of the construction scenario (see detailed results in the last page of Appendix C). For instance, the construction worker SSTL for benzene is 1,300 mg/kg, compared to 50 mg/kg for residential exposure.

RBCA Tier 2 Comparison

The table below provides a RBCA Tier 2 comparison of maximum detected benzene concentration with the soil and shallow groundwater SSTLs. The Tier 2 comparison involves only benzene because it is the only chemical that failed the Tier 1 screening.

Chemical: Benzene

Exp. Medium	*Receptor*	*SSTL*	*Max. Detected*
Onsite Soil	*Resid. Outdoor*	50.0 mg/kg	16 mg/kg
Onsite Shallow GW	*Comm. Indoor*	2.3 mg/L	13 mg/L
Offsite Shallow GW	*Comm. Indoor*	2.3 mg/L	1.1 mg/L

The above comparison indicates that maximum detection of benzene in soil does not exceed the Tier 2 SSTL. Therefore, on-site soil does not warrant further consideration related to protection of human health.

Maximum onsite detection of benzene in shallow groundwater (13 mg/L) exceeds the SSTL of 2.3 mg/L. The groundwater SSTL is based on protection of indoor commercial receptors, which are located offsite, and offsite maximum detected groundwater concentration (1.1 mg/L) does not exceed SSTL. Therefore, further consideration of site conditions is needed to evaluate whether the onsite groundwater exceedance represents a potential significant human health concern. For instance, the average plume concentration is likely to be lower than the above maximum detection, which was detected more than three years ago (well LF-1, sampled on 8/7/93). In addition, some natural dilution/attenuation processes such as the effect of chemical degradation, retardation, and dispersion, which were not accounted for in the SSTLs development, may be responsible for the observed lower offsite groundwater concentration. To account for such processes would increase the SSTLs and decrease the likelihood of SSTL exceedance. We recommend the implementation of a groundwater monitoring program to address the above considerations and provide an update of groundwater conditions since 1993, and gather evidence of plume stability and chemical degradation.

3.2 FINAL SITE CLASSIFICATION

Based on the results of the ASTM RBCA Tier 1 and 2 evaluation, and on the site classification scenarios presented in Table 1 of the RBCA guidance (ASTM 1995), we conclude that, once the recommended groundwater monitoring program shows attainment of the SSTLs, the site should be classified under Level 4: No Demonstrable Long-Term Threat to Human Health, Safety, or Sensitive Environmental Receptors. This final site classification is based on the results of Tier 1 and Tier 2 evaluation, which indicate that petroleum constituents and other chemicals detected in soil at the site do not present a significant potential risk to residents and construction workers. In addition, the Tier 2 indicates the concentration in shallow groundwater which is protective of residents, construction workers, and commercial workers. Uncertainties and limitations of this study are addressed in Section 5.0. Recommendations about the use of SSTLs in remedial decision are provided below.

3.3 USE OF SSTLS IN REMEDIAL DECISIONS

The SSTLs developed in RBCA Tier 2 for the site are site-specific concentrations in soil and shallow groundwater that are estimated to be protective of human health and the environment based on the application of exposure and risk assessment models. The SSTLs are based on conservative exposure assumptions and input parameters (e.g., for the commercial scenario: 25 years, 250 days/year, 8 hours/day continuous exposure to an infinite mass, non-degrading chemical source, etc.). The SSTLs are not necessarily the final cleanup goals selected for the site. In general, if the SSTLs are exceeded, the site conditions may warrant further consideration in terms of additional investigation, monitoring, fate and transport modeling, or remedial action. On the other hand, if the SSTLs are not exceeded, then the site does not require further consideration.

Cleanup goals should consider potential effects on human health and the environment as well as criteria described by the National Contingency Plan (NCP). The SSTLs produced by a risk-based evaluation represent only one of the variables in the remedial action equation leading towards cleanup goals. The SSTLs are a conservative reference point for site cleanup, but the final cleanup goals should be the outcome of risk management decisions, which include risk assessment considerations as well as the other remedial action criteria listed in the NCP (i.e., implementability, cost effectiveness, time frame of remediation, public acceptability, etc.). In conclusion, the ASTM RBCA Tier 2 SSTLs that have been developed for the site represent a conservative starting point for remedial decision making, and may be selected by the risk managers as cleanup goals.

The conclusions of this study are the following:

- Since maximum detection of benzene in soil does not exceed the Tier 2 SSTL, on-site soil does not warrant further consideration related to protection of human health.
- Maximum detection of benzene in onsite shallow groundwater exceeds the indoor commercial SSTL (well LF-1, sampled on 8/7/93), however the offsite groundwater does not exceed the SSTL. The commercial receptor is located downgradient offsite. Therefore, further consideration of groundwater conditions is needed to evaluate whether the exceedance represents a potential significant human health concern.

The recommendations of this study are the following:

- We recommend no further action for soil
- For groundwater, a monitoring program should be implemented to evaluate current groundwater conditions, and gather evidence of plume stability and chemical degradation.
- If evidence of plume stability and chemical degradation is found, and groundwater concentration of benzene is below SSTL, no further action for groundwater should be required.

The quantitative methods and procedures described in this document for evaluating potential exposure and risk are based on a number of simplifying assumptions related to the characterization of the contaminant sources and of the subsurface environment. The exposure models are based on descriptions of relevant physical/chemical phenomena. Any mechanisms that are neglected, such as neglecting attenuation due to natural biodegradation, result in predictions of exposure and risk that are conservative relative to those likely to occur. In other words, the models are biased towards predicting exposure concentrations in excess of those likely to occur (page 12, ASTM 1994). Uncertainty and variability affect the input parameters of all of the exposure and fate and transport models. Conservative values of those input parameters are selected to deal with this uncertainty and variability. Since the exposure models are multiplicative, conservatism is compounded in the calculations. For this reason, the modeling results in this study are expected to overestimate exposure and risk, rather than underestimate the actual risk posed by the site.

The degree of conservatism in this assessment is illustrated by the following: the screening levels for commercial workers proposed in this study are estimated by the models to be protective of a receptor assumed to work at the site for 25 years, 250 days per year, 8 hours per day, and to inhale volatile emissions from soil and groundwater generated by a continuous (i.e., non-degrading, infinite mass) source for the entire exposure duration. The models estimate that if the average source concentrations do not exceed the cleanup goals, such a receptor would be subject to an excess cancer risk of less than 1 in 100,000 as a consequence of exposure to chemicals in soil and groundwater.

Conservatism is an important feature of predictive modeling in the RBCA process. Tier 1 is the most conservative level and provides a "worst-case scenario" for potential exposure and risk. Tier 1 utilizes conservative models and input parameters (that is, USEPA reasonable maximum exposure (RME) values, and conservative inputs for the contaminant fate and transport models) to establish non-site specific risk-based screening criteria (the RBSLs). Tier 2 is still conservative, but provides flexibility for a site-specific RME scenario evaluation, or a "reasonable case scenario" (that is, USEPA most likely exposure (MLE) values), depending on whether the inputs reflect more of a site-specific RME or MLE exposure scenario. Tier 2 uses site-specific information about the release site and the exposure scenario to develop conservative, site-specific corrective action objectives (the SSTLs) that are protective of human health (ASTM 1995). Tier 2 models still represent a conservative approach, by neglecting, for instance, natural attenuation due to benign biodegradation and source decay due to volatilization and flushing. In fact, Tier 2 models assume no chemical degradation and source of chemicals of constant concentration and infinite mass. More detailed discussion of the exposure models assumptions and limitations is provided in ASTM (1995). In the application of ASTM RBCA to the site that is presented here, conservative but reasonable site-specific estimates of the input parameters have been selected. Rationales and references for input parameters estimated values used in the models are reported in the text and tables.

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TABLE 1
MAXIMUM DETECTED RESIDUAL SOIL CONCENTRATIONS AFTER SOIL EXCAVATION IN EACH AREA OF CONCERN

Chemical of Concern in Soil	Former Celis Area			Former Warehouse Area			Former Parking Lot Area			Offsite Downgradient Area		
	Maximum Detected Conc. [mg/kg]	Location	Depth [feet]	Maximum Detected Conc. [mg/kg]	Location	Depth [feet]	Maximum Detected Conc. [mg/kg]	Location	Depth [feet]	Maximum Detected Conc. [mg/kg]	Location	Depth [feet]
Benzene	3.8	B-D-1	9.5	13	B-2	10	16	SB-12/15W	7	1.7	LF-4	10
Ethylbenzene	11	N-1	9	21	B-2	10	360	SB-12/15W	7	4.5	LF-4	10
Toluene	21	N-1	9	52	B-2	10	210	SB-12/15S	7	6.7	LF-4	10
Xylenes	49	B-C-2	9.5	110	B-2	10	1700	SB-12/15W	7	24	LF-4	10
Napthalene*	23.40	est. B-D-1	9	0.17	est. SB-17	12	0.29	est. B13	2	0.02	est. LF-4	10
Benzo(a)pyrene**	0.00126	est. B-D-1	9	0.0000091	est. SB-17	12	0.0000154	est. B13	2	0.00000133	est. LF-4	10
TPH (gas)	1000	B-C-2	9.5	830	B-2	10	12000	SB-12/15W	7	220	LF-4	10
TPH (diesel)	18000	B-D-1	9.5	130	SB-17	12	220	B13	2	19	LF-4	10
TPH (motor oil)	66	SB-7	NA	190	SB-17	12	480	SB-14	2	49	EB-1	10
TRPH	NA	NA	9.5	110	B-4	10	2400	B5	5	NA	NA	NA
Methylene chloride	NA	NA	NA	2.6	SB-17	4.5	NA	NA	NA	NA	NA	NA
4-Methylphenol	NA	NA	NA	0.4	SB-17	4.5	NA	NA	NA	NA	NA	NA
Naphthalene	NA	NA	NA	1.7	SB-17	12	NA	NA	NA	NA	NA	NA
2-Methylnaphthalene	NA	NA	NA	1.8	SB-17	4.5	1.1	B14	10	NA	NA	NA
Aroclor 1260	NA	NA	NA	ND	NA	NA	0.22	SB-14	2	NA	NA	NA

Legend:
*** Assumed as 0.13% of maximum TPH-diesel concentration (Calabrese et al., 1993).**
**** Assumed as 0.07 mg/kg of maximum TPH-diesel concentration (Guerin et al., 1984).**

3/11/97 MCL

TABLE 2
MAXIMUM DETECTED SHALLOW GROUNDWATER CONCENTRATIONS IN EACH AREA OF CONCERN

Chemical of Concern in Groundwater	Former Celis Area		Former Warehouse Area		Offsite Downgradient Area	
	Maximun Detected Conc. [mg/L]	Location/ Date	Maximum Detected Conc. [mg/L]	Location/ Date	Maximum Detected Conc. [mg/L]	Location/ Date
Benzene	13	LF-1 (8/7/93)	1.7	MW-1 (3/8/94)	1.1	LF-4Dup (1/28/94)
Ethylbenzene	3.1	LF-1 (8/7/93)	0.23	MW-1 (3/8/94)	0.88	LF-4 (1/28/94)
Toluene	9.4	LF-1 (8/7/93)	0.43	MW-1 (3/8/94)	2	LF-4Dup (1/28/94)
Xylenes	14	LF-1 (8/7/93)	0.49	MW-1 (3/8/94)	4.7	LF-4 (1/28/94)
Napthalene*	0.0533	est. LF-1 (8/7/93)	0.00754	est. MW-1 (3/8/94)	0.00286	est. LF-4Dup (1/28/94)
Benzo(a)pyrene**	0.00000287	est. LF-1 (8/7/93)	0.000000406	est. MW-1 (3/8/94)	0.000000154	est. LF-4Dup (1/28/94)
TPH (gas)	100	LF-1 (8/7/93)	5.8	MW-1 (3/8/94)	21	LF-4Dup (1/28/94)
TPH (diesel)	41	LF-1 (8/7/93)	NA	NA	2.2	LF-4Dup (1/28/94)
TPH (motor oil)	<2.5	LF-1 (8/7/93)	NA	NA	0.21	LF-4Dup (1/28/94)
TRPH	11	LF-1 (8/7/93)	NA	NA	NA	NA

Legend:

*** Assumed as 0.13% of maximum TPH-diesel concentration (Calabrese et al., 1993).**

**** Assumed as 0.07 mg/kg of maximum TPH-diesel concentration (Guerin et al., 1984).**

TABLE 3
COMPARISON OF MAXIMUM DETECTED RESIDUAL SOIL CONCENTRATIONS WITH RBCA TIER 1 RBSLs

Chemical of Concern in Soil	Overall Maximum Detected Conc. [mg/kg]	Location of Maximum Detection	1.00E-06 Risk: Residential Outdoor Exposure Tier 1 RBSL*** Concentration [mg/kg]	1.00E-06 Risk: Residential Surficial Soil Exp. Tier 1 RBSL*** Concentration [mg/kg]	RBCA Tier 1 RBSL Exceeded ?
Benzene	16	SB-12/15 W	0.272	5.82	***Exceeded***
Ethylbenzene	360	SB-12/15W	>SATUR (1980)	>SATUR (1980)	*None Exceeded*
Toluene	210	SB-12/15S	>SATUR (781)	>SATUR (781)	*None Exceeded*
Xylenes	1,700	SB-12/15W	>SATUR (498)	>SATUR (498)	*None Exceeded*
Napthalene*	23.4	estim. from B-D-1	>SATUR (402)	>SATUR (402)	*None Exceeded*
Benzo(a)pyrene**	0.00126	estim. from B-D-1	>SATUR (4.67)	0.13	*None Exceeded*
TPH (diesel)	18,000	B-D-1	na	na	na

Legend:

*** Assumed as 0.13% of maximum TPH-diesel concentration (Calabrese et al., 1993).**

**** Assumed as 0.07 mg/kg of maximum TPH-diesel concentration (Guerin et al., 1984).**

***** Based on 10e-6 risk for carcinogens or a unit hazard index for non-carcinogens and for residential exposure scenario.**

> SATUR = Selected risk level is not exceeded at saturated soil concentration (shown in parenthesis).

TABLE 4
COMPARISON OF MAXIMUM DETECTED SHALLOW GROUNDWATER CONCENTRATIONS WITH RBCA TIER 1 RBSLs

Chemical of Concern in Groundwater	Overall Maximum Detected Conc. [mg/L]	Location of Maximum Detection	1.00E-06 Risk Commercial Indoor Exposure Tier 1 RBSL*** Concentration [mg/L]	RBCA Tier I Threshold*** Exceeded ?
Benzene	13	LF-1	0.0739	***Exceeded***
Ethylbenzene	3.1	LF-1	>SOLUB(152)	*None Exceeded*
Toluene	9.4	LF-1	85	*None Exceeded*
Xylenes	14	LF-1	>SOLUB (198)	*None Exceeded*
Napthalene*	0.0533	estim. from LF-1	12.3	*None Exceeded*
Benzo(a)pyrene**	0.00000287	estim. from LF-1	>SOLUB (1.2E-3)	*None Exceeded*
TPH (diesel)	41	LF-1	na	na

Legend:

*** Assumed as 0.13% of maximum TPH-diesel concentration (Calabrese et al., 1993).**

**** Assumed as 0.07 mg/kg of maximum TPH-diesel concentration (Guerin et al., 1984).**

***** Based on 10e-6 risk for carcinogens or a unit hazard index for non-carcinogens and for commercial exposure scenario.**

> SOLUB = Selected risk level is not exceeded in water at solubility (shown in parenthesis).

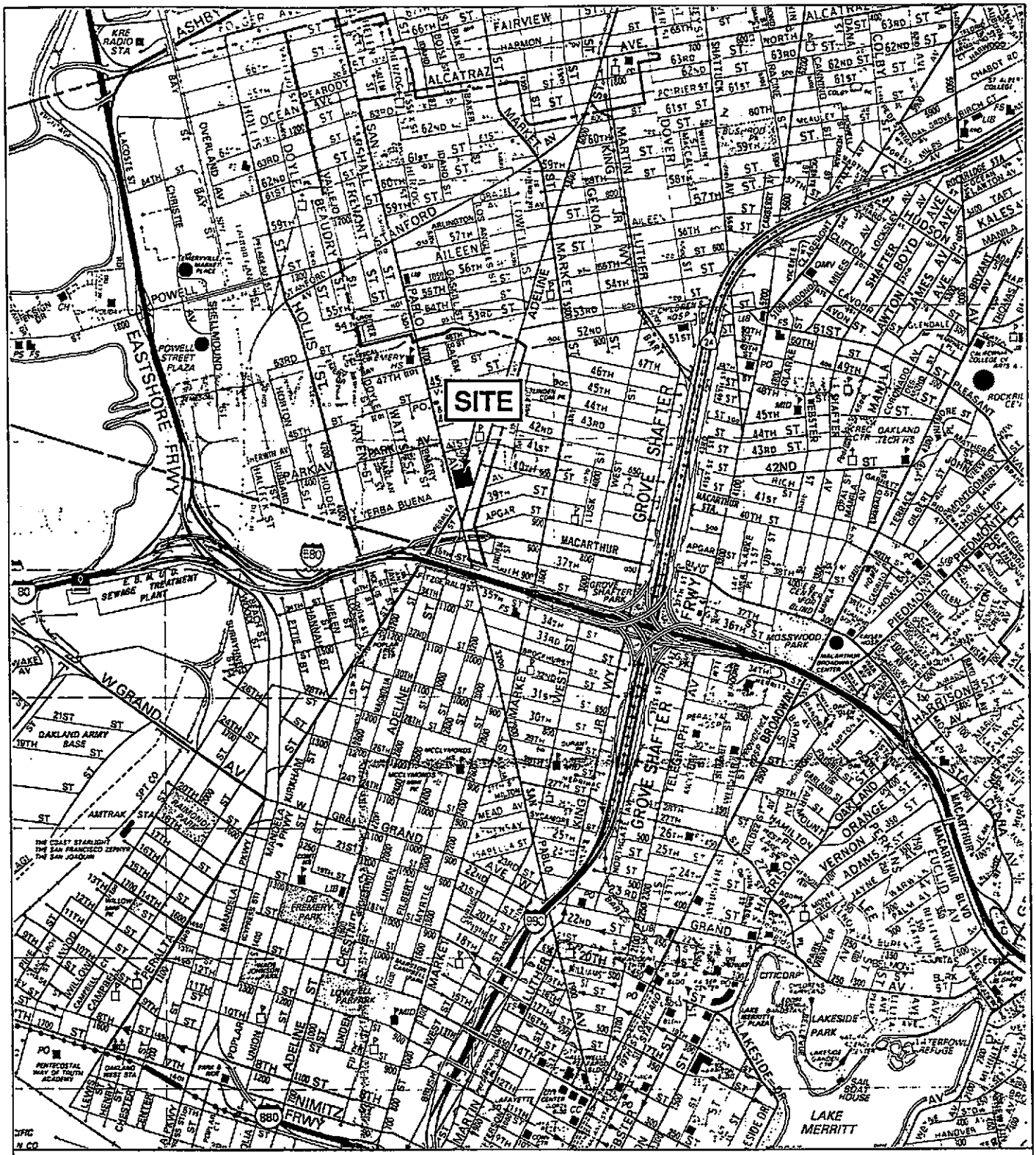
TABLE 5. SUMMARY OF SITE-SPECIFIC TARGET LEVELS

CHEMICAL	SITE-SPECIFIC TARGET LEVELS (1,2)		
	Residential Outdoor Exposure to Soil Emissions [mg/kg]	Commercial Indoor Exposure to GW Emissions [mg/L]	Construction Outdoor Exposure to Surficial Soil [mg/kg]
Benzene	1.0E+1	2.3E+0	1.3E+3
Toluene	7.8E+2 *	5.4E+2 *	7.8E+2 *
Ethylbenzene	3.5E+2 *	1.5E+2 *	3.5E+2 *
Xylene (mixed)	5.0E+2 *	2.0E+2 *	5.0E+2 *
Naphthalene	4.0E+2 *	3.1E+1 *	4.0E+2 *
Benzo(a)pyrene	4.7E+0 *	1.2E-3 *	4.7E+0 *
MTBE	9.9E+3 *	5.1E+4 *	9.9E+3 *

* Indicates SSTL exceeded soil saturation limit or water solubility and hence saturation or solubility are listed as SSTL

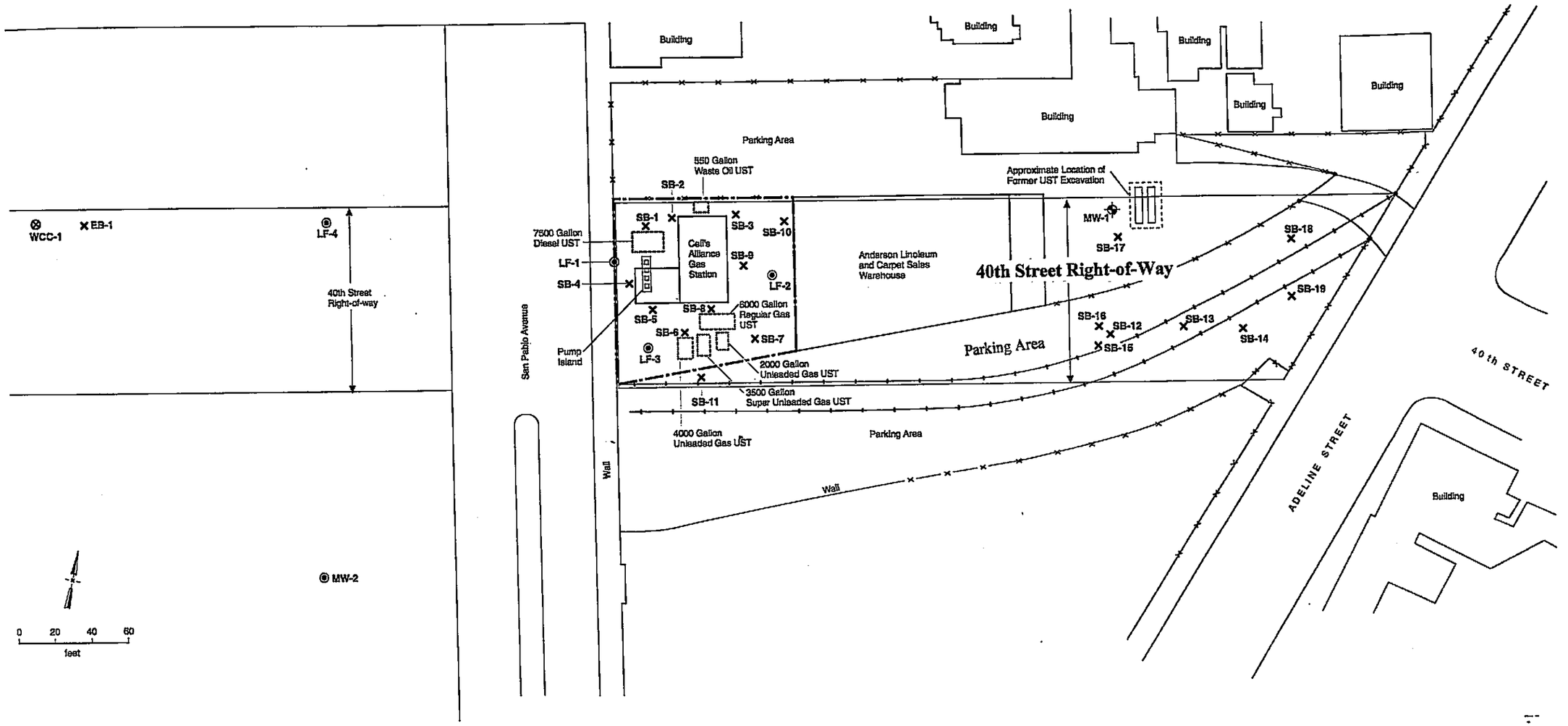
(1) Calculated using the equations in ASTM RBCA guidance. Target risk concentrations are corresponding to a cancer risk of one in 100000 or a non-carcinogenic hazard quotient of unity for the exposure pathway being evaluated.
(2) The SSTL is the lower of the target risk concentrations for carcinogenic and non-carcinogenic effect, unless they exceed soil saturation of water solubility, in which case the SSTL is set at saturation or solubility concentration.

na = Not Applicable/Not Available



Project No. 941114NA	40th Street UST	SITE LOCATION MAP CELI'S ALLIANCE GAS STATION SITE	Figure 1
Woodward-Clyde Consultants			

941114NA-1000/060994



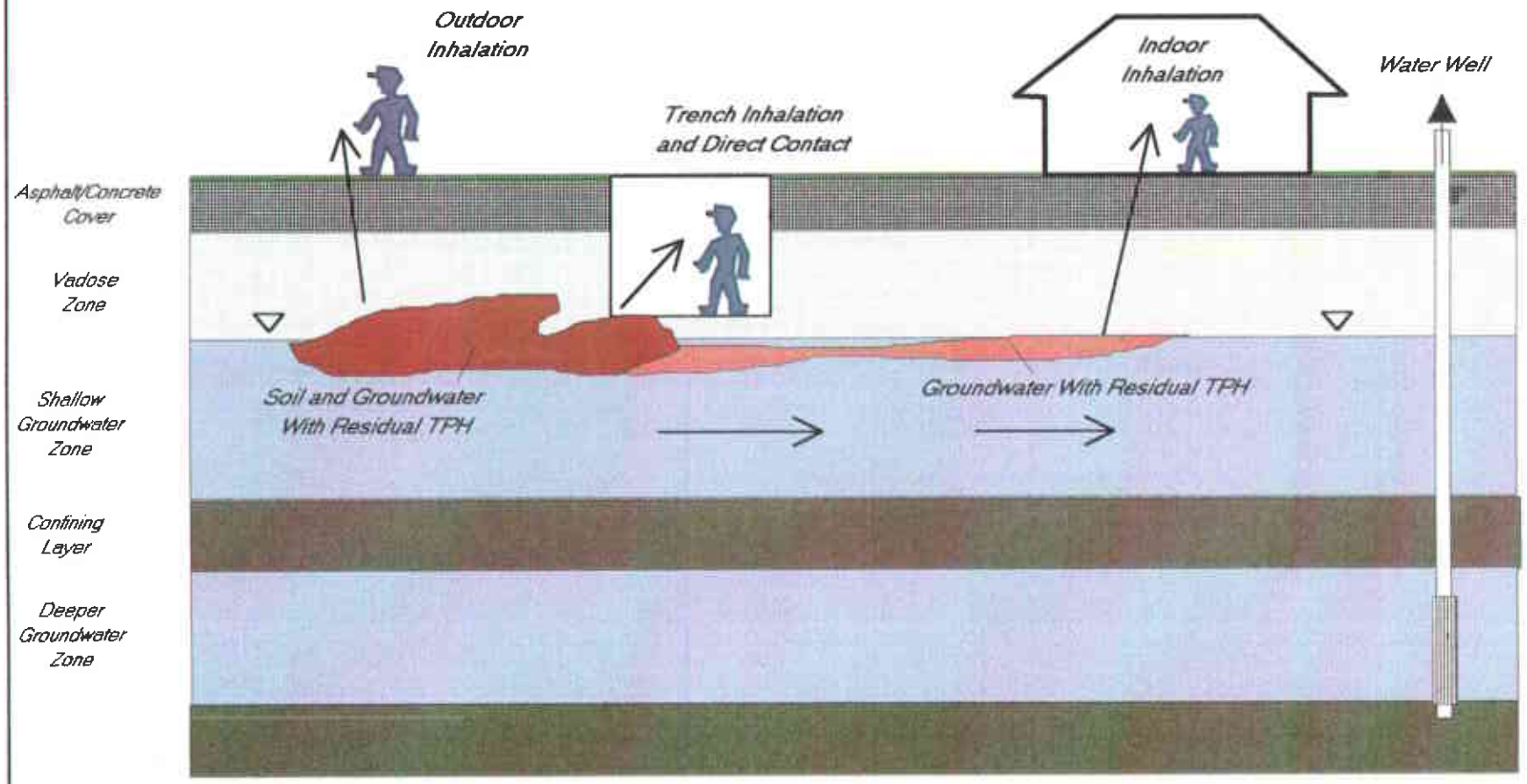
EXPLANATION

- Approximate Location of Former Railroad Tracks
- × Soil Borings by Levine-Fricke
- ◉ Monitoring Well by Levine-Fricke (LF-1, LF-2, & LF-3 destroyed)
- ⌖ Monitoring Well by SECOR (destroyed)
- ⊗ Proposed Monitoring Well by WCC in 1994 (not installed)

Source: Levine-Fricke (1992) and Woodward-Clyde Consultants (1994)

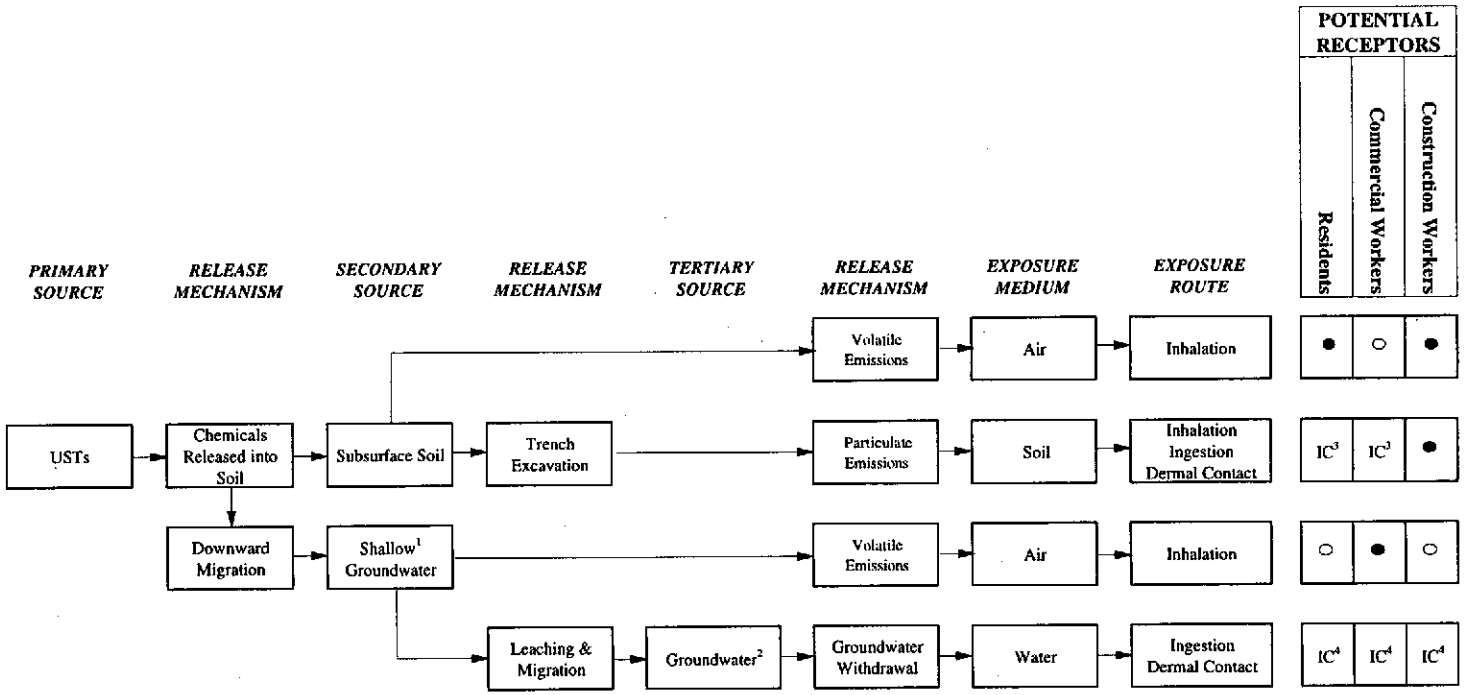
Project No. 941114NA	40th Street UST	SOIL BORING AND MONITORING WELL LOCATIONS 40TH STREET RIGHT-OF-WAY EMERYVILLE, CALIFORNIA	Figure 2
Woodward-Clyde Consultants			

941114NA-9620/05/2/96



NOT TO SCALE

Project No. 941114NA	40th Street Right-of-Way	ILLUSTRATION OF POTENTIAL EXPOSURE SCENARIOS	Figure 3
Woodward-Clyde Consultants			



Legend:

- ● Potentially complete pathway (will be evaluated in a quantitative way)
- ○ Insignificant pathway (will be evaluated in a qualitative way)
- IC Incomplete pathway
- na Not Applicable

Notes:

1 Represented by the first encountered groundwater, typically 10 feet below ground surface.

2 Represented by the groundwater beneath the first encountered aquitard.

3 Asphalt/concrete pavement prevents direct soil contact exposure.

4 Drinking water is supplied by municipal water system, and no water supply wells are located nearby or screened in the shallow zones.

Project No. 941114NA	40th Street Right-of-Way	SITE CONCEPTUAL MODEL	Figure 4
Woodward-Clyde Consultants			

APPENDIX A Summary of Site Investigation and Remediation Results

Phase II Investigation Results
Proposed 40th Street Right-of-Way
Emeryville, California

September 8, 1993
1649.00-15

Prepared for
Catellus Development Corporation
201 Mission Street
San Francisco, California

LEVINE·FRICKE

TABLE 1
ANALYTICAL RESULTS FOR SOIL SAMPLES COLLECTED FROM THE FUEL STATION
40TH STREET RIGHT-OF-WAY, EMERYVILLE, CALIFORNIA
(concentrations in milligrams per kilogram [mg/kg])

Sample Name	Depth (ft)	Sample Date	TPHg	TPHd	TPHmo	Benzene	Toluene	Ethyl-benzene	Total Xylenes	TRPH	PCBs
LF-1-4.5	4.5	07-Aug-93	550	220	16	0.84	1.2	5.6	2.7	77	NA
LF-1-9.5	9.5	07-Aug-93	470	18	<10	0.97	<0.005	6.6	8.9	<30	NA
LF-1-14.5	14.5	07-Aug-93	8.4	16	<10	0.14	0.17	0.081	0.37	60	NA
LF-2-9.5	9.5	07-Aug-93	740	14	<10	4.7	35	13	68	30	NA
LF-2-14.5	14.5	07-Aug-93	<0.5	<10	<10	0.009	0.012	<0.005	0.015	<30	NA
LF-3-9.5	9.5	07-Aug-93	75	<10	<10	0.062	0.28	1.1	1.1	37	NA
LF-3-14.5	14.5	07-Aug-93	<0.5	<10	<10	0.014	<0.005	0.01	0.007	<30	NA
SB-1-7	7	08-Aug-93	850	240	27	5.4	<0.005	25	42	290	NA
SB-1-9.5	9.5	08-Aug-93	180	220	<50	0.89	1.1	4.3	18	130	NA
SB-1-14.5	14.5	08-Aug-93	7.4	<10	<10	0.44	0.44	0.14	0.61	60	NA
SB-2-7	7	08-Aug-93	780	790	57	8	<0.005	31	140	160	ND
SB-2-9.5	9.5	08-Aug-93	720	200	<50	2.4	5.2	14	59	210	NA
SB-2-14.5	14.5	08-Aug-93	1	<10	12	0.2	0.21	0.021	0.12	43	ND
SB-3-9.5	9.5	07-Aug-93	580	11	<10	9.7	50	15	90	37	ND
SB-3-14.5	14.5	07-Aug-93	0.9	<10	<10	0.092	0.16	0.031	0.17	37	ND
SB-4-7	7	08-Aug-93	380	13	<10	3	5.2	8.2	18	70	NA
SB-4-14.5	14.5	08-Aug-93	<0.5	<10	<10	0.026	0.005	0.019	0.023	210	NA
SB-5-7	7	08-Aug-93	410	15	<10	2.4	0.6	16	6.3	37	NA
SB-5-14.5	14.5	08-Aug-93	<0.5	<10	<10	0.011	<0.005	0.008	0.008	93	NA
SB-6-9.5	9.5	08-Aug-93	490	51	<10	2.7	<0.005	15	15	67	NA
SB-6-14.5	14.5	08-Aug-93	<0.5	<10	<10	<0.005	<0.005	<0.005	<0.005	<30	NA
SB-7-9.5	9.5	07-Aug-93	750	52	66	2.5	8.5	22	93	170	NA
SB-7-14.5	14.5	07-Aug-93	2.8	<10	<10	<0.005	<0.005	0.029	0.03	<30	NA
SB-8-9.5	9.5	08-Aug-93	2,800	110	<50	22	9.5	82	290	130	NA
SB-8-14.5	14.5	08-Aug-93	<0.5	<10	11	0.009	<0.005	<0.005	<0.005	37	NA
SB-9-7	7	07-Aug-93	210	14	<10	2.8	13	5.1	29	<30	NA
SB-9-9.5	9.5	07-Aug-93	1,200	NA	NA	14	81	26	140	NA	NA
SB-9-14.5	14.5	07-Aug-93	<0.5	<10	<10	0.079	0.059	0.011	0.041	77	NA
SB-10-7	7	07-Aug-93	73	NA	NA	2.6	4.5	1.6	7.7	NA	NA
SB-10-9.5	9.5	07-Aug-93	1,100	<10	<10	<0.005	7.8	<0.005	22	40	NA
SB-10-14.5	14.5	07-Aug-93	8.6	<10	<10	0.48	0.29	0.1	0.48	<30	NA
SB-11-14.5	14.5	09-Aug-93	<0.5	<10	11	<0.005	<0.005	<0.005	<0.005	40	NA

Data entered by MEK/20-Aug-93. Data proofed by JJB/26-Aug-93. QA/QC by JJB/08-Sep-93.

TPHg = total petroleum hydrocarbons as gasoline
TPHd = total petroleum hydrocarbons as diesel
TPHmo = total petroleum hydrocarbons as motor oil
TRPH = total recoverable petroleum hydrocarbons
PCBs = polychlorinated biphenyls

TABLE 2
ANALYTICAL RESULTS FOR SOIL SAMPLES COLLECTED FROM THE EASTERN PORTION OF THE SITE
40TH STREET RIGHT-OF-WAY, EMERYVILLE, CALIFORNIA
(concentrations in milligrams per kilogram [mg/kg])

Sample Name	Depth (ft)	Sample Date	TPHg	TPHd	TPHmo	Benzene	Toluene	Ethyl-benzene	Total Xylenes	TRPH	PCBs	VOCs	SVOCs
Railroad Tracks													
SB-12-1	1	09-Aug-93	<0.5	<200	400	NA	NA	NA	NA	4,600	ND	NA	NA
SB-12-3	3	09-Aug-93	6,500	560	64	NA	NA	NA	NA	420	ND	NA	NA
SB-13-5	5	09-Aug-93	23	<10	<10	NA	NA	NA	NA	63	ND	NA	NA
SB-13-6.5	6.5	09-Aug-93	13	<10	<10	NA	NA	NA	NA	37	ND	NA	NA
SB-14-2	2	09-Aug-93	42	<200	480	NA	NA	NA	NA	2,200	(7)	NA	NA
SB-14-4.5	4.5	09-Aug-93	<0.5	<10	<10	NA	NA	NA	NA	47	ND	NA	NA
SB-15-4.5	4.5	09-Aug-93	4,700	140	12	NA	NA	NA	NA	480	ND	NA	NA
SB-15-6	6	09-Aug-93	3,700	59	14	NA	NA	NA	NA	120	ND	NA	NA
SB-16-4.5	4.5	09-Aug-93	9	<10	<10	NA	NA	NA	NA	60	ND	NA	NA
SB-16-6	6	09-Aug-93	8	<10	<10	NA	NA	NA	NA	53	ND	NA	NA
SB-18-1	1	09-Aug-93	1	<200	320	NA	NA	NA	NA	2,200	ND	NA	NA
SB-18-3	3	09-Aug-93	<0.5	<200	390	NA	NA	NA	NA	1,100	ND	NA	NA
SB-19-1.5	1.5	09-Aug-93	<0.5	<200	530	NA	NA	NA	NA	2,200	ND	NA	NA
SB-19-3	3	09-Aug-93	1	<200	740	NA	NA	NA	NA	3,600	ND	NA	NA
San Francisco French Bread Company													
SB-17-4.5	4.5	09-Aug-93	260	40	<10	2	22	12	69	70	ND	(1)	(4)
SB-17-7	7	09-Aug-93	440	17	<10	4	27	8	43	50	ND	(2)	(5)
SB-17-12	12	09-Aug-93	500	130	190	2	9	4	23	47	ND	(3)	(6)

Data entered by MEK/20-Aug-93. Data proofed by JJB/26-Aug-93. QA/QC by JJB/08-Sep-93.

TPHg = total petroleum hydrocarbons as gasoline
TPHd = total petroleum hydrocarbons as diesel
TPHmo = total petroleum hydrocarbons as motor oil
TRPH = total recoverable petroleum hydrocarbons
PCBs = polychlorinated biphenyls
VOCs = volatile organic compounds
SVOCS = semivolatile organic compounds
ND = Not detected above laboratory detection limits

(1) 2.6 mg/kg methylene chloride
(2) 2.0 mg/kg methylene chloride
(3) 0.660 mg/kg methylene chloride
(4) 0.4 mg/kg 4-methylphenol, 1.6 mg/kg naphthalene, and 1.8 mg/kg 2-methylnaphthalene
(5) 0.57 mg/kg naphthalene and 0.630 mg/kg 2-methylnaphthalene
(6) 1.7 mg/kg naphthalene and 1.8 mg/kg 2-methylnaphthalene
(7) 0.22 mg/kg Aroclor 1260

TABLE 3
WELL CONSTRUCTION AND GROUND-WATER ELEVATION DATA
40TH STREET RIGHT-OF-WAY, EMERYVILLE, CALIFORNIA

Well Number	Well Elevation (feet msl)	Well Depth (feet)	Screened Interval	Date Measured	Depth to Product	Depth to Water	Ground-Water Elevation (feet msl)	Product Thickness (feet)
LF-1	38.95	20	5-20	08-Aug-93	NA	9.40	29.55	NA
				20-Aug-93	9.48	10.00	29.36*	0.52
LF-2	40.25	20	5-20	08-Aug-93	NA	7.97	32.28	NA
				20-Aug-93	NA	8.29	31.96	NA
LF-3	39.35	20	5-20	08-Aug-93	NA	8.90	30.45	NA
				20-Aug-93	NA	9.18	30.17	NA

msl = mean sea level

* The ground-water elevation for well LF-1 was corrected for the presence of free-phase fuel product using the following equation:

$$G = W + [(PT \times D) - DW]$$

where
G = the ground-water elevation
W = the well elevation
PT = the product thickness
D = product density (mg/l)
DW = the depth to water

A density of 0.796 mg/l was assumed.

TABLE 4
ANALYTICAL RESULTS FOR GROUND-WATER SAMPLES
40TH STREET RIGHT-OF-WAY, EMERYVILLE, CALIFORNIA
(concentrations in milligrams per liter [mg/l])

Sample Name	Sample Date	TPHg	TPHd	TPHmo	Benzene	Toluene	Ethyl-benzene	Total Xylenes	TRPH
LF-1AG	07-Aug-93	100	41	<2.5	13	9.4	3.1	14	11
LF-2AG	07-Aug-93	13	0.095	<0.50	2.4	2.9	0.5	2	<5
LF-3AG	07-Aug-93	11	0.78	<0.250	1.5	0.17	2.9	5.1	<5

Data entered by MEK/20-Aug-93 Data proofed by JJB/26-Aug-93. QA/QC by JJB/08-Sep-93.

TPHg = total petroleum hydrocarbons as gasoline
TPHd = total petroleum hydrocarbons as diesel
TPHmo = total petroleum hydrocarbons as motor oil
TRPH = total recoverable petroleum hydrocarbons

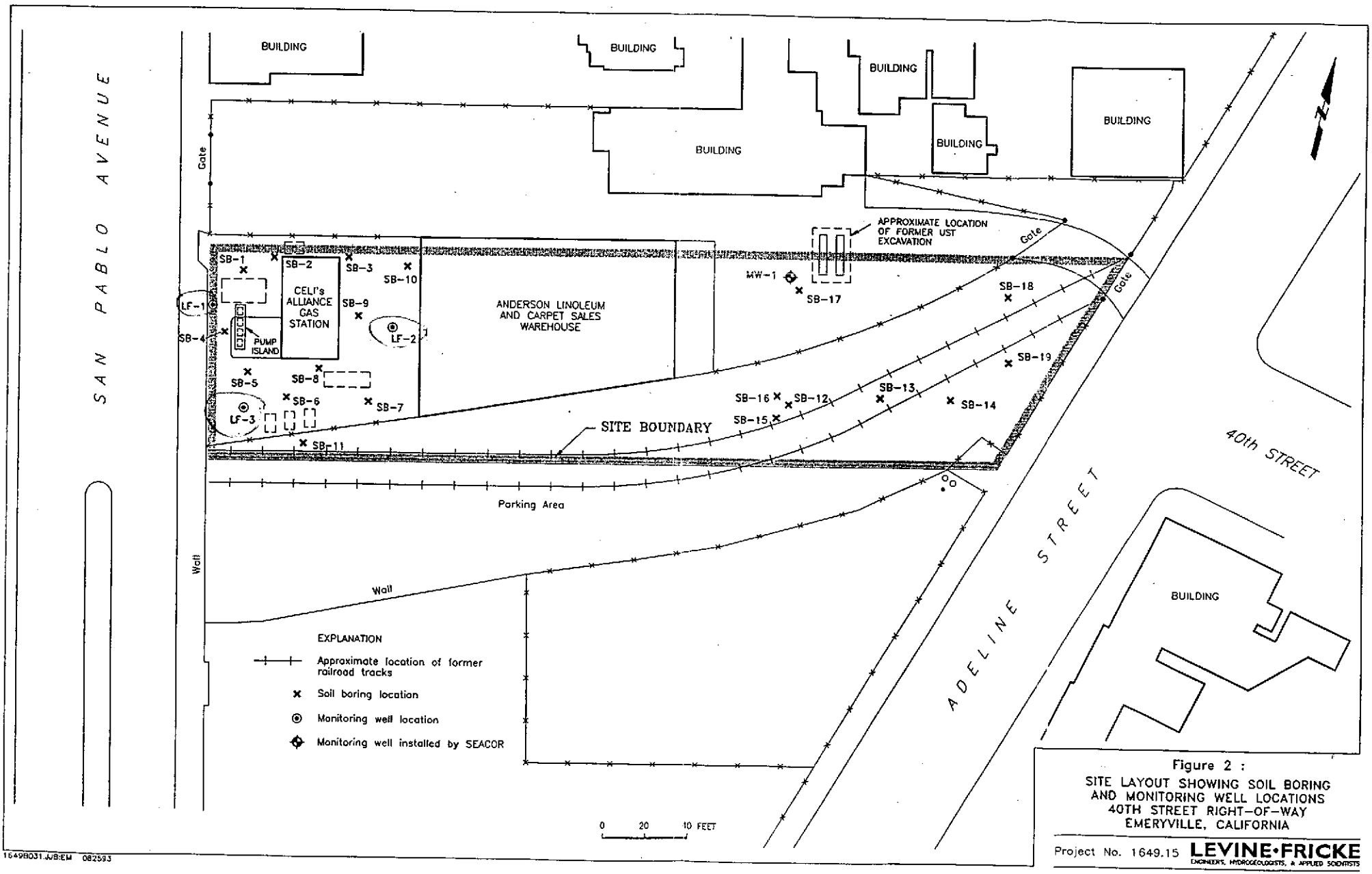


Figure 2 :
SITE LAYOUT SHOWING SOIL BORING AND MONITORING WELL LOCATIONS
40TH STREET RIGHT-OF-WAY
EMERYVILLE, CALIFORNIA

Project No. 1649.15 LEVINE·FRICKE
ENGINEERS, HYDROGEOLOGISTS, & APPLIED SCIENTISTS

16498031.JJB:EM 082593

Further Soil and Ground-Water Investigation
Fuel Station
40th Street Right-of-Way
Emeryville, California

March 30, 1994
1649.15

Prepared for
Catellus Development Corporation
201 Mission Street, Suite 250
San Francisco, California 94105

LEVINE·FRICKE

TABLE 1
ANALYTICAL RESULTS FOR SOIL SAMPLES COLLECTED FROM MONITORING WELL BORINGS AND SOIL BORING
FUEL STATION, 40TH STREET RIGHT-OF-WAY, EMERYVILLE, CALIFORNIA
(concentrations in milligrams per kilogram [mg/kg])

Sample Name	Depth (ft)	Sample Date	TPHg	TPHd	TPHmo	Benzene	Toluene	Ethyl-benzene	Total Xylenes	TRPH
LF-1-4.5	4.5	07-Aug-93	550	220	16	0.84	1.2	5.6	2.7	77
LF-1-9.5	9.5	07-Aug-93	470	18	<10	0.97	<0.005	6.6	8.9	<30
LF-1-14.5	14.5	07-Aug-93	8.4	16	<10	0.14	0.17	0.081	0.37	60
LF-2-9.5	9.5	07-Aug-93	740	14	<10	4.7	35	13	68	30
LF-2-14.5	14.5	07-Aug-93	<0.5	<10	<10	0.009	0.012	<0.005	0.015	<30
LF-3-9.5	9.5	07-Aug-93	75	<10	<10	0.062	0.28	1.1	1.1	37
LF-3-14.5	14.5	07-Aug-93	<0.5	<10	<10	0.014	<0.005	0.01	0.007	<30
LF-4-5.0	5	28-Jan-94	0.8	<10	<10	0.083	<0.005	<0.005	0.034	NA
LF-4-10.0	10	28-Jan-94	220	19	<10	1.7	6.7	4.5	24	NA
EB-1-5.0	5	28-Jan-94	<0.5	<10	17	<0.005	<0.005	<0.005	<0.005	NA
EB1-10.0	10	28-Jan-94	<0.5	<20	49	<0.005	<0.005	<0.005	<0.005	NA

Data entered by MEK/18 Feb 94 Data proofed by [illegible] 3/7 QA/QC by [illegible]

NA = not analyzed
TPHg = total petroleum hydrocarbons as gasoline
TPHd = total petroleum hydrocarbons as diesel
TPHmo = total petroleum hydrocarbons as motor oil
TRPH = total recoverable petroleum hydrocarbons

TABLE 2
ANALYTICAL RESULTS FOR GROUND-WATER SAMPLES
40TH STREET RIGHT-OF-WAY, EMERYVILLE, CALIFORNIA
(concentrations in milligrams per liter [mg/l])

Sample Name	Sample Date	TPHg	TPHd	TPHmo	Benzene	Toluene	Ethyl-benzene	Total Xylenes	TRPH
LF-1AG	07-Aug-93	100	41	<2.5	13	9.4	3.1	14	11
LF-2AG	07-Aug-93	13	0.095	<0.50	2.4	2.9	0.5	2	<5
LF-3AG	07-Aug-93	11	0.78	<0.250	1.5	0.17	2.9	5.1	<5
GWEB1	28-Jan-94	<0.05	0.081	<0.05	<0.0005	0.00057	<0.0005	0.0026	NA
LF-4	28-Jan-94	18	1.4	0.16	1.0	1.9	0.88	4.7	NA
LF-4 (dup)	28-Jan-94	21	2.2	0.21	1.1	2	0.80	4.2	NA

Data entered by MEK/18 Feb 94 Data proofed by JD 3/4/94 QA/QC by Qean 3/4/94

NA = not analyzed
TPHg = total petroleum hydrocarbons as gasoline
TPHd = total petroleum hydrocarbons as diesel
TPHmo = total petroleum hydrocarbons as motor oil
TRPH = total recoverable petroleum hydrocarbons

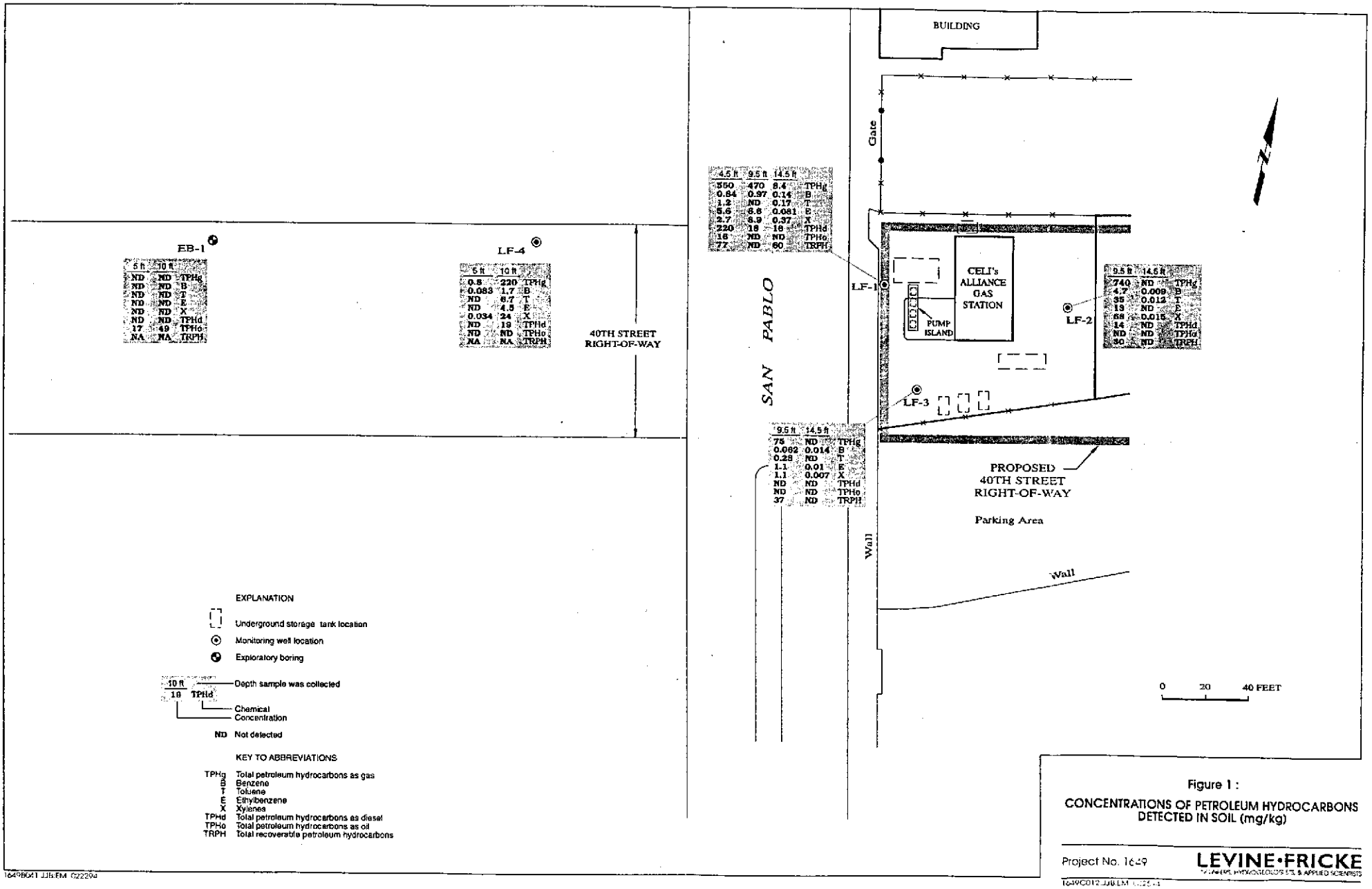


Figure 1 :

CONCENTRATIONS OF PETROLEUM HYDROCARBONS DETECTED IN SOIL (mg/kg)

Project No. 1649

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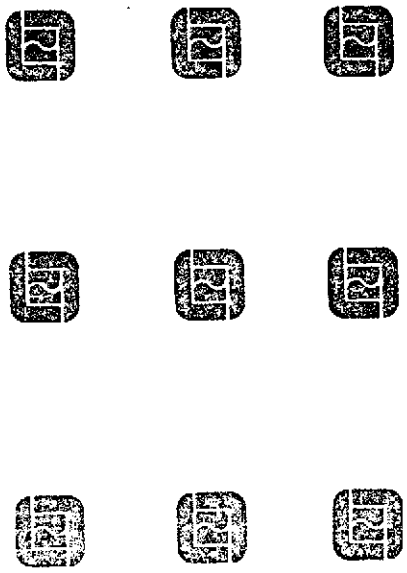
1649B041 JJB:EM 022294

1649C012 JJB:EM



Report on Removal of Six Underground Fuel Storage Tanks and Associated Piping
Celis Alliance Fueling Station
4000 San Pablo Avenue
Emeryville, California

July 6, 1994
LF 3158.00-000

Prepared for
Catellus Development Corporation
201 Mission Street
San Francisco, California 94105

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TABLE 1
ANALYTICAL RESULTS FOR SOIL SAMPLES COLLECTED DURING UST REMOVAL ACTIVITIES
CELIS ALLIANCE SERVICE STATION, EMERYVILLE, CALIFORNIA
(all results in parts per million [ppm])

Sample ID	Date Sampled	TPHg	Benzene	Toluene	Ethyl-benzene	Total Xylenes	TPHd	TPHo	Other Tests
G1-8	18-May-94	640	4.6	4.5	24	21	NA	NA	
G2-10	18-May-94	140	1.9	0.7	4.2	5.2	NA	NA	
G3-9.5	18-May-94	570	5.3	16	18	91	NA	NA	(1)
G4-10.5	18-May-94	3.1	0.006	<0.005	0.018	<0.005	NA	NA	
G5-8.5	20-May-94	<200*	<2*	<0.8*	<4*	<0.8*	NA	NA	
D1-9	20-May-94	<60*	<0.2*	<0.1*	<0.05*	<0.05*	1,300	NA	
D2-9.5	20-May-94	<60*	<0.3*	<0.3*	<0.3*	<0.3*	89	NA	
D1-7	18-May-94	50	0.095	0.15	0.23	<0.05**	29	<5.0	(1, 2, 3, 4, 5, 6)

Data entered by DVN/24-Jun-94. Data proofed by JCC QA/QC by JCC

Sample G2-10 denotes the second soil sample collected from the gasoline UST excavation at ten feet below the ground surface.

Analyses performed by American Environmental Network of Pleasant Hill, California.

TPHg - total petroleum hydrocarbons as gasoline using EPA Method 5030/GCFID
TPHd - total petroleum hydrocarbons as diesel using EPA Method 3550/GCFID
TPHo - total petroleum hydrocarbons as oil using EPA Method 3550/GCFID.
BTEX - benzene, toluene, ethylbenzene and total xylenes using EPA Method 8020.
NA - not analyzed

* Raised reporting limit due to hydrocarbon interferences.
** Raised reporting limit due to high concentrations of non-target compounds.

(1) Sample analyzed for organic lead in soil using Department of Health Services, Leaking Underground Fuel Tank (DOHS-LUFT) Method. Result is non-detect (detection limit 0.5 ppm).
(2) Sample analyzed for cadmium, chromium, lead, nickel, and zinc, using EPA Method 6010 Series. Cadmium was not detected (detection limit 0.1 ppm), chromium was detected at 27 ppm, lead at 2 ppm, nickel at 26 ppm, and zinc at 47 ppm.
(3) Sample analyzed for hydrocarbons and oil and grease by infra-red using Standard Methods 5520F and 5520E, with results of 40 ppm hydrocarbons and 50 ppm oil and grease.
(4) Sample analyzed for PCBs using EPA Method 8080, with results of non-detect (detection limit 0.05 ppm).
(5) Sample analyzed for creosote and PNAs using EPA Method 8270, with results of non-detect (detection limit 5 ppm) for creosote and non-detect (detection limit 0.2 ppm) for PNAs.
(6) Sample analyzed for halogenated volatile organic compounds using EPA Method 8010, with results of non-detect (detection limit 0.005 ppm).

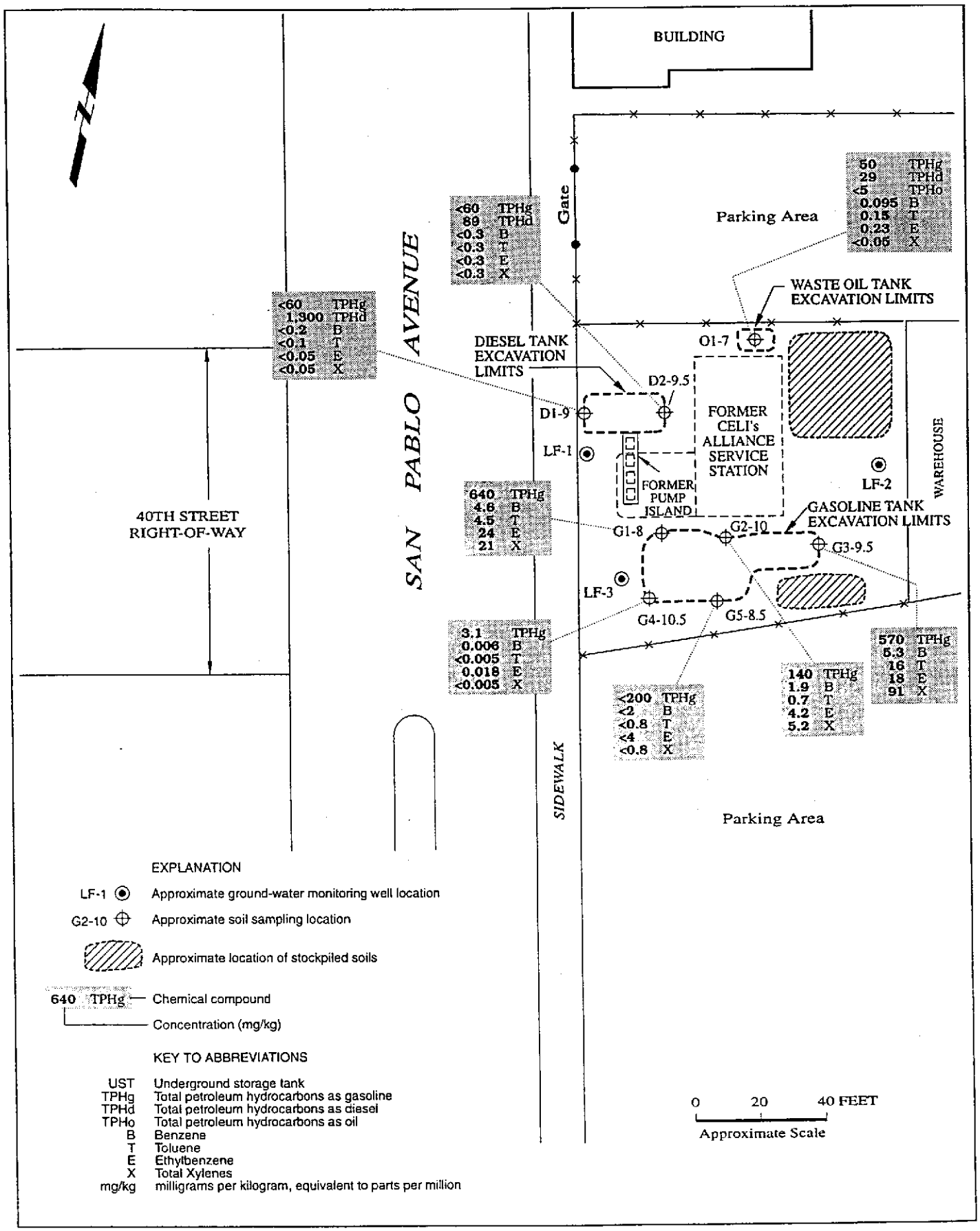


Figure 3 : SITE PLAN SHOWING UST EXCAVATIONS, SOIL SAMPLING LOCATIONS AND TPH AND BTEX CONCENTRATIONS

Summary of Environmental Activities
Proposed 40th Street Extension
Emeryville, California

November 22, 1994
1649.00-034

Prepared for
Catellus Development Corporation
201 Mission Street, 30th Floor
San Francisco, California 94105

LEVINE·FRICKE

TABLE 1
ANALYTICAL RESULTS FOR SOIL SAMPLES COLLECTED FROM PHASE II SOIL BORINGS
PROPOSED 40TH STREET EXTENSION, EMERYVILLE, CALIFORNIA
(concentrations in milligrams per kilogram [mg/kg])

Sample Name	Depth (ft)	Sample Date	TPHg	TPHd	TPHmo	Benzene	Toluene	Ethyl-benzene	Total Xylenes	TRPH	PCBs	VOCs	SVOCs
Former Celis Service Station													
LF-1-4.5	4.5	07-Aug-93	550	220	16	0.84	1.2	5.6	2.7	77	NA	NA	NA
LF-1-9.5	9.5	07-Aug-93	470	18	<10	0.97	<0.005	6.6	8.9	<30	NA	NA	NA
LF-1-14.5	14.5	07-Aug-93	8.4	16	<10	0.14	0.17	0.081	0.37	60	NA	NA	NA
LF-2-9.5	9.5	07-Aug-93	740	14	<10	4.7	35	13	68	30	NA	NA	NA
LF-2-14.5	14.5	07-Aug-93	<0.5	<10	<10	0.009	0.012	<0.005	0.015	<30	NA	NA	NA
LF-3-9.5	9.5	07-Aug-93	75	<10	<10	0.062	0.28	1.1	1.1	37	NA	NA	NA
LF-3-14.5	14.5	07-Aug-93	<0.5	<10	<10	0.014	<0.005	0.01	0.007	<30	NA	NA	NA
SB-1-7	7	08-Aug-93	850	240	27	5.4	<0.005	25	42	290	NA	NA	NA
SB-1-9.5	9.5	08-Aug-93	180	220	<50	0.89	1.1	4.3	18	130	NA	NA	NA
SB-1-14.5	14.5	08-Aug-93	7.4	<10	<10	0.44	0.44	0.14	0.61	60	NA	NA	NA
SB-2-7	7	08-Aug-93	780	790	57	8	<0.005	31	140	160	ND	NA	NA
SB-2-9.5	9.5	08-Aug-93	720	200	<50	2.4	5.2	14	59	210	NA	NA	NA
SB-2-14.5	14.5	08-Aug-93	1	<10	12	0.2	0.21	0.021	0.12	43	ND	NA	NA
SB-3-9.5	9.5	07-Aug-93	580	11	<10	9.7	50	15	90	37	ND	NA	NA
SB-3-14.5	14.5	07-Aug-93	0.9	<10	<10	0.092	0.16	0.031	0.17	37	ND	NA	NA
SB-4-7	7	08-Aug-93	380	13	<10	3	5.2	8.2	18	70	NA	NA	NA
SB-4-14.5	14.5	08-Aug-93	<0.5	<10	<10	0.026	0.005	0.019	0.023	210	NA	NA	NA
SB-5-7	7	08-Aug-93	410	15	<10	2.4	0.6	16	6.3	37	NA	NA	NA
SB-5-14.5	14.5	08-Aug-93	<0.5	<10	<10	0.011	<0.005	0.008	0.008	93	NA	NA	NA
SB-6-9.5	9.5	08-Aug-93	490	51	<10	2.7	<0.005	15	15	67	NA	NA	NA
SB-6-14.5	14.5	08-Aug-93	<0.5	<10	<10	<0.005	<0.005	<0.005	<0.005	<30	NA	NA	NA
SB-7-9.5	9.5	07-Aug-93	750	52	66	2.5	8.5	22	93	170	NA	NA	NA
SB-7-14.5	14.5	07-Aug-93	2.8	<10	<10	<0.005	<0.005	0.029	0.03	<30	NA	NA	NA
SB-8-9.5	9.5	08-Aug-93	2,800	110	<50	22	9.5	82	290	130	NA	NA	NA
SB-8-14.5	14.5	08-Aug-93	<0.5	<10	11	0.009	<0.005	<0.005	<0.005	37	NA	NA	NA
SB-9-7	7	07-Aug-93	210	14	<10	2.8	13	5.1	29	<30	NA	NA	NA
SB-9-9.5	9.5	07-Aug-93	1,200	NA	NA	14	81	26	140	NA	NA	NA	NA
SB-9-14.5	14.5	07-Aug-93	<0.5	<10	<10	0.079	0.059	0.011	0.041	77	NA	NA	NA
SB-10-7	7	07-Aug-93	73	NA	NA	2.6	4.5	1.6	7.7	NA	NA	NA	NA
SB-10-9.5	9.5	07-Aug-93	1,100	<10	<10	<0.005	7.8	<0.005	22	40	NA	NA	NA
SB-10-14.5	14.5	07-Aug-93	8.6	<10	<10	0.48	0.29	0.1	0.48	<30	NA	NA	NA
SB-11-14.5	14.5	09-Aug-93	<0.5	<10	11	<0.005	<0.005	<0.005	<0.005	40	NA	NA	NA
Railroad Tracks													
SB-12-1	1	09-Aug-93	<0.5	<200	400	NA	NA	NA	NA	4,680	ND	NA	NA
SB-12-3	3	09-Aug-93	6,500	560	64	NA	NA	NA	NA	420	ND	NA	NA
SB-13-5	5	09-Aug-93	23	<10	<10	NA	NA	NA	NA	63	ND	NA	NA
SB-13-6.5	6.5	09-Aug-93	13	<10	<10	NA	NA	NA	NA	37	ND	NA	NA
SB-14-2	2	09-Aug-93	42	<200	480	NA	NA	NA	NA	2,200	(7)	NA	NA
SB-14-4.5	4.5	09-Aug-93	<0.5	<10	<10	NA	NA	NA	NA	47	ND	NA	NA
SB-15-4.5	4.5	09-Aug-93	4,700	140	12	NA	NA	NA	NA	480	ND	NA	NA
SB-15-6	6	09-Aug-93	3,700	59	14	NA	NA	NA	NA	120	ND	NA	NA
SB-16-4.5	4.5	09-Aug-93	9	<10	<10	NA	NA	NA	NA	60	ND	NA	NA
SB-16-6	6	09-Aug-93	8	<10	<10	NA	NA	NA	NA	53	ND	NA	NA
SB-18-1	1	09-Aug-93	1	<200	320	NA	NA	NA	NA	2,200	ND	NA	NA
SB-18-3	3	09-Aug-93	<0.5	<200	390	NA	NA	NA	NA	1,100	ND	NA	NA
SB-19-1.5	1.5	09-Aug-93	<0.5	<200	530	NA	NA	NA	NA	2,200	ND	NA	NA
SB-19-3	3	09-Aug-93	1	<200	740	NA	NA	NA	NA	3,600	ND	NA	NA
San Francisco French Bread Company													
SB-17-4.5	4.5	09-Aug-93	260	40	<10	2	22	12	69	70	ND	(1)	(4)
SB-17-7	7	09-Aug-93	440	17	<10	4	27	8	43	50	ND	(2)	(5)
SB-17-12	12	09-Aug-93	500	130	190	2	9	4	23	47	ND	(3)	(6)

Data entered by MEK/20-Aug-93. Data proofed by JJB/26-Aug-93. QA/QC by JJB/08-Sep-93.

TPHg = total petroleum hydrocarbons as gasoline
TPHd = total petroleum hydrocarbons as diesel
TPHmo = total petroleum hydrocarbons as motor oil
TRPH = total recoverable petroleum hydrocarbons
PCBs = polychlorinated biphenyls
NA = parameter not analyzed
ND = parameter not detected

(1) 2.6 mg/kg methylene chloride
(2) 2.0 mg/kg methylene chloride
(3) 0.660 mg/kg methylene chloride
(4) 0.4 mg/kg 4-methylphenol, 1.6 mg/kg naphthalene, and 1.8 mg/kg 2-methylnaphthalene
(5) 0.57 mg/kg naphthalene and 0.630 mg/kg 2-methylnaphthalene
(6) 1.7 mg/kg naphthalene and 1.8 mg/kg 2-methylnaphthalene
(7) 0.22 mg/kg Aroclor 1260

TABLE 2
ANALYTICAL RESULTS FOR SOIL SAMPLES COLLECTED FROM ADDITIONAL SOIL BORINGS
PROPOSED 40TH STREET EXTENSION, EMERYVILLE, CALIFORNIA
(concentrations in milligrams per kilogram (mg/kg))

Sample Name		Depth (ft)	Sample Date	TPHg	TPHd	TRPH	Benzene	Toluene	Ethyl-benzene	Total Xylenes	Total BTEX
B1-2		2	29-Aug-94	0.8	<1	<10	0.008	<0.005	0.016	0.085	0.109
B1-5		5	29-Aug-94	110	<1	30	0.840	0.520	3.200	12.000	16.560
B1-10		10	29-Aug-94	690	<1	30	12.000	50.000	18.000	99.000	179.000
B2-2		2	29-Aug-94	110	<1	10	0.600	2.900	3.300	16.000	22.800
B2-5		5	29-Aug-94	66	1	10	0.370	0.800	0.790	3.500	5.460
B2-10		10	29-Aug-94	830	<1	30	13.000	52.000	21.000	110.000	196.000
B3-2		2	29-Aug-94	440	<1	80	8.500	36.000	12.000	58.000	114.500
B3-5		5	29-Aug-94	810	8	200	14.000	62.000	22.000	100.000	198.000
B3-10		10	29-Aug-94	390	<1	50	7.100	22.000	7.200	38.000	74.300
B4-2		2	29-Aug-94	49	<1	40	0.140	0.120	2.300	11.000	13.560
B4-5		5	29-Aug-94	8,800	28	1,300	6.800	7.300	190.000	870.000	1,074.100
B4-10		10	29-Aug-94	510	3	110	1.100	0.960	3.400	13.000	18.460
B5-2		2	29-Aug-94	0.4	<1	10	<0.005	<0.005	<0.005	<0.005	<0.005
B5-5		5	29-Aug-94	<0.2	<1	2,400	<0.005	<0.005	<0.005	<0.005	<0.005
B5-10		10	29-Aug-94	<0.2	<1	<10	<0.005	<0.005	<0.005	<0.005	<0.005
B6-2 *		2	29-Aug-94	<0.2	<1	20	<0.005	<0.005	<0.005	<0.005	<0.005
B6-5 *		5	29-Aug-94	<0.2	<1	10	<0.005	<0.005	<0.005	<0.005	<0.005
B6-10*		10	29-Aug-94	<0.2	<1	<10	<0.005	<0.005	<0.005	<0.005	<0.005
B7-2		2	30-Aug-94	27	<1	10	0.420	<.010	0.750	0.050	1.220
B7-5		5	30-Aug-94	16	<1	<10	0.670	<0.020	<0.020	0.025	0.695
B7-10		10	30-Aug-94	520	<1	20	7.400	30.000	14.000	78.000	129.400
B8-2		2	29-Aug-94	3.4	<3	50	0.200	<0.005	0.560	0.020	0.780
B8-5		5	29-Aug-94	14	<1	<10	0.300	0.010	0.260	<0.020	0.570
B8-10		10	29-Aug-94	140	<1	20	2.100	5.800	4.000	21.000	32.900
B9-2		2	29-Aug-94	2.8	<1	20	0.330	0.005	0.410	0.070	0.815
B9-5		5	29-Aug-94	40	5	<10	1.200	0.013	2.600	0.150	3.963
B9-10		10	29-Aug-94	190	<1	20	4.300	11.000	5.500	28.000	48.800
B10-2		2	29-Aug-94	29	<1	150	0.038	0.048	0.180	1.200	1.466
B10-5		5	29-Aug-94	13	<1	30	<0.010	0.020	0.050	<0.010	0.070
B-10-10		10	29-Aug-94	<0.2	<1	<10	<0.005	<0.005	<0.005	<0.005	<0.005
B11-2		2	30-Aug-94	<0.2	<1	20	<0.005	<0.005	<0.005	<0.005	<0.005
B11-5		5	30-Aug-94	1	<1	<10	<0.005	<0.005	<0.005	<0.005	<0.005
B11-10		10	30-Aug-94	250	<1	40	1.100	0.350	4.400	21.000	26.850
B12-2		2	30-Aug-94	<0.2	<1	30	<0.005	<0.005	<0.005	<0.005	<0.005
B12-5		5	30-Aug-94	0.9	<1	<10	<0.005	<0.005	<0.005	<0.005	<0.005
B12-10		10	30-Aug-94	160	<1	30	0.970	0.190	4.100	20.000	25.260
B13-2		2	30-Aug-94	<1	220	600	<0.005	<0.005	<0.005	<0.005	<0.005
B13-5		5	30-Aug-94	4.2	10	40	<0.005	<0.005	0.020	<0.005	0.020
B13-10		10	30-Aug-94	6.9	3	20	0.360	<0.005	0.450	0.130	0.940
B14-2 *	(1)	2	30-Aug-94	<1	<100	410	<0.005	<0.005	<0.005	<0.005	<0.005
B14-5 *		5	30-Aug-94	1.6	<1	<10	0.010	<0.005	<0.005	<0.005	0.010
B14-10*	(2)	10	30-Aug-94	2.9	<1	<10	0.006	<0.005	0.010	<0.005	0.016
B15-2		2	30-Aug-94	<0.2	<10	420	<0.005	<0.005	<0.005	<0.005	<0.005
B15-5		5	30-Aug-94	<0.2	<1	<10	<0.005	<0.005	<0.005	<0.005	<0.005
B15-10		10	30-Aug-94	<0.2	<1	20	<0.005	<0.005	<0.005	<0.005	<0.005
B16-2		2	30-Aug-94	<0.2	10	50	<0.005	<0.005	<0.005	<0.005	<0.005
B16-5		5	30-Aug-94	28	<1	<10	0.160	<0.010	0.960	0.037	1.157
B16-10		10	30-Aug-94	130	<1	20	2.500	5.400	2.600	15.000	25.500

Data entered by DLM/19 SEP 94 Data proofed by REG QA/QC by REG

Notes:
* denotes that the sample was analyzed for semivolatile organic compounds using EPA method 8270
(1) 2-Methylnaphthalene detected at 0.670 ppm.
(2) 2-Methylnaphthalene detected at 1.100 ppm.

NA = not analyzed
TPHg = total petroleum hydrocarbons as gasoline
TPHd = total petroleum hydrocarbons as diesel
TRPH = total recoverable petroleum hydrocarbons

TABLE 3

CONFIRMATION SOIL SAMPLES FROM THE EXCAVATION
IN THE VICINITY OF SB-12 AND SB-15
PROPOSED 40TH STREET EXTENSION
EMERYVILLE, CALIFORNIA

(concentrations expressed in parts per million)

Sample ID	Sample Depth (ft bgs)	Date	Lab	TPHg (1)	TPHd (2)	TPHo (3)	Benzene	Toluene	Ethyl-Benzene	Total Xylenes	Total BTEX
North	7	11-Oct-94	AEN(4)	54	16	50	0.027	0.010	0.140	0.090	0.267
South	7	11-Oct-94		7,900	66	64	13.000	[illegible]	220.000	1,200.000	1,643.000
East	7	11-Oct-94		37	6	10	0.010	0.038	0.052	0.670	0.770
West	[illegible]	11-Oct-94		[illegible]	[illegible]	[illegible]	[illegible]	170.000	[illegible]	[illegible]	2,246.000
Bottom	8	11-Oct-94		2,400	140	160	0.520	66.000	73.000	500.000	639.520

NOTES:

AEN = American Environmental Network, Pleasant Hill, California
ft bgs = feet below ground surface
TPHg = total petroleum hydrocarbons as gasoline
TPHd = total petroleum hydrocarbons as diesel
TPHo = total petroleum hydrocarbons as oil

1649\40THCONF.WQ1 22-Nov-94

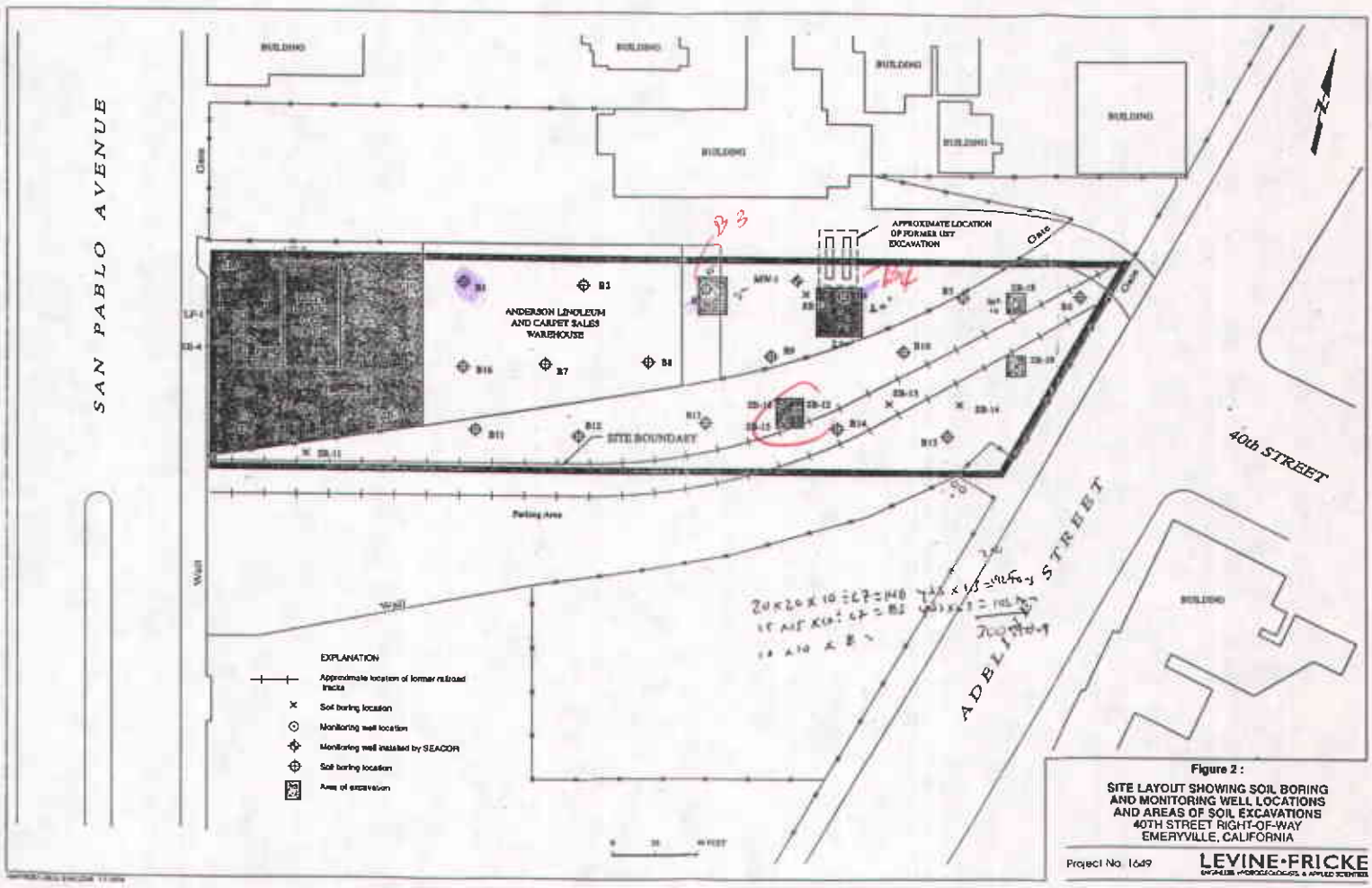


Figure 2 :

SITE LAYOUT SHOWING SOIL BORING AND MONITORING WELL LOCATIONS AND AREAS OF SOIL EXCAVATIONS 40TH STREET RIGHT-OF-WAY EMERYVILLE, CALIFORNIA

Project No. 1649

LEVINE-FRICKE

REPORT ON SOIL REMEDIATION AT THE FORMER CELIS ALLIANCE FUEL STATION 4000 SAN PABLO AVENUE EMERYVILLE, CALIFORNIA

Prepared for

City of Emeryville Redevelopment Agency
2200 Powell Street, 12th Floor, Suite 1200
Emeryville, California 94608-4356

January 6, 1995

Woodward-Clyde

Woodward-Clyde Consultants
500 12th Street, Suite 100
Oakland, California 94607-4014

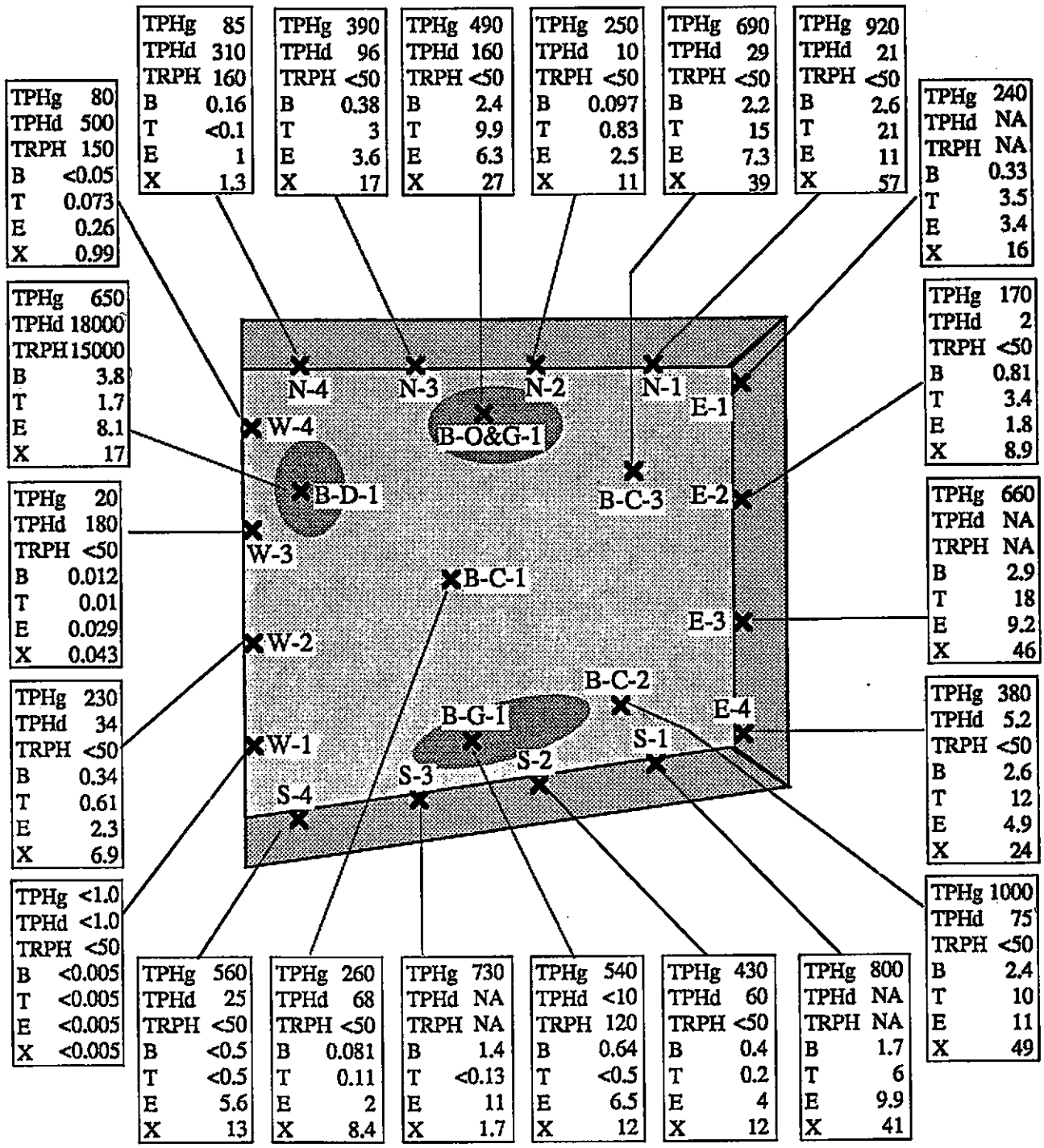
TABLE 6

ANALYTICAL RESULTS FOR SOIL SAMPLES COLLECTED FROM SIDE WALLS AND BOTTOM OF THE EXCAVATION PIT
CELIS ALLIANCE FUEL STATION, EMERYVILLE, CALIFORNIA

Sample ID	Benzene	Toluene	Ethyl benzene	Xylenes	TPHg	TPHd	TRPH (1)	Cadmium	Chromium (total)	Lead	Nickel	Zinc
	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg	mg/kg
E-1	0.33	3.5	3.4	16	240	NA	NA	NA	NA	NA	NA	NA
E-2	0.81	3.4	1.8	8.9	170	2	ND(50)	1.4	18	4.3	34	26
E-3	2.9	18	9.2	46	660	NA	NA	NA	NA	NA	NA	NA
E-4	2.6	12	4.9	24	380	5.2	ND(50)	1.4	16	5.6	17	30
N-1	2.6	21	11	57	920	21	ND(50)	2.1	26	6.1	37	40
N-2	0.097	0.83	2.5	11	250	10	ND(50)	1.4	16	2.8	26	23
N-3	0.38	3	3.6	17	390	96	ND(50)	2.6	20	7.3	25	40
N-4	0.16	ND(0.1)	1	1.3	85	310	160	2.1	28	5	25	29
S-1	1.7	6	9.9	41	800	NA	NA	NA	NA	NA	NA	NA
S-2	0.4	0.2	4	12	430	60	ND(50)	2.3	28	7	39	43
S-3	1.4	ND(0.13)	11	1.7	730	NA	NA	NA	NA	NA	NA	NA
S-4	ND(0.5)	ND(0.5)	5.6	13	560	25	ND(50)	1.9	26	8.3	23	30
W-1	ND(0.005)	ND(0.005)	ND(0.005)	ND(0.005)	ND(1.0)	ND(1.0)	ND(50)	2.2	27	8	34	45
W-2	0.34	0.61	2.3	6.9	230	34	ND(50)	2.3	29	5.5	26	42
W-3	0.012	ND(0.01)	0.029	0.043	20	180	ND(50)	1.4	19	5.6	21	27
W-4	ND(0.05)	0.073	0.26	0.99	80	500	150	2	28	6.2	36	38
B-C-1	0.081	0.11	2	8.4	260	68	ND(50)	2.3	31	6.7	29	37
B-C-2	2.4	10	11	49	1000	75	ND(50)	1.3	18	4	19	25
B-C-3	2.2	15	7.3	39	690	29	ND(50)	1.8	27	5.2	25	33
B-O&G-1	2.4	9.9	6.3	27	490	160	ND(50)	2.7	35	8.3	41	39
B-D-1	3.8	1.7	8.1	17	650	18000	15000	1.9	27	7	25	27
B-G-1	0.64	ND(0.5)	6.5	12	540	ND(10)	120	2.9	25	54	21	200

NOTES (1) TRPH = total recoverable petroleum hydrocarbons as determined by Standard Method 5520 E&F

(2) NA = not available; ND = not detected above the quantification limit given in parenthesis following the ND.



TPHg = total petroleum hydrocarbons as gasoline
TPHd = total petroleum hydrocarbons as diesel
TRPH = total recoverable petroleum hydrocarbons

B = benzene
T = toluene
E = ethyl benzene
X = xylenes

Soil samples on side walls were collected 6-in above the bottom floor

Unit of Concentration: mg/kg

Project No. 941114NA	CITY OF EMERYVILLE REDEVELOPMENT AGENCY	SOIL SAMPLING LOCATIONS & ANALYTE CONCENTRATIONS	Figure 7
Woodward-Clyde Consultants		40th Street UST at 4000 San Pablo Avenue	

APPENDIX B

ASTM RBCA Guidance E 1739-95 and Errata from Woodward-Clyde

Designation: E 1739 – 95

Standard Guide for Risk-Based Corrective Action Applied at Petroleum Release Sites[1]

This standard is issued under the fixed designation E 1739; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ε) indicates an editorial change since the last revision or reapproval.

1. Scope

1.1 This is a guide to risk-based corrective action (RBCA), which is a consistent decision-making process for the assessment and response to a petroleum release, based on the protection of human health and the environment. Sites with petroleum release vary greatly in terms of complexity, physical and chemical characteristics, and in the risk that they may pose to human health and the environment. The RBCA process recognizes this diversity, and uses a tiered approach where corrective action activities are tailored to site-specific conditions and risks. While the RBCA process is not limited to a particular class of compounds, this guide emphasizes the application of RBCA to petroleum product releases through the use of the examples. Ecological risk assessment, as discussed in this guide, is a qualitative evaluation of the actual or potential impacts to environmental (nonhuman) receptors. *There may be circumstances under which a more detailed ecological risk assessment is necessary* (see Ref (1).[2]

1.2 The decision process described in this guide integrates risk and exposure assessment practices, as suggested by the United States Environmental Protection Agency (USEPA), with site assessment activities and remedial measure selection to ensure that the chosen action is protective of human health and the environment. The following general sequence of events is prescribed in RBCA, once the process is triggered by the suspicion or confirmation of petroleum release:

1.2.1 Performance of a site assessment;

1.2.2 Classification of the site by the urgency of initial response;

1.2.3 Implementation of an initial response action appropriate for the selected site classification;

1.2.4 Comparison of concentrations of chemical(s) of concern at the site with Tier 1 Risk Based Screening Levels (RBSLs) given in a look-up table;

1.2.5 Deciding whether further tier evaluation is warranted, if implementation of interim remedial action is warranted or if RBSLs may be applied as remediation target levels;

1.2.6 Collection of additional site-specific information as necessary, if further tier evaluation is warranted;

1.2.7 Development of site-specific target levels (SSTLs) and point(s) of compliance (Tier 2 evaluation);

1.2.8 Comparison of the concentrations of chemical(s) of concern at the site with the Tier 2 evaluation SSTL at the determined point(s) of compliance or source area(s);

1.2.9 Deciding whether further tier evaluation is warranted, if implementation of interim remedial action is warranted, or if Tier 2 SSTLs may be applied as remediation target levels;

1.2.10 Collection of additional site-specific information as necessary, if further tier evaluation is warranted;

1.2.11 Development of SSTL and point(s) of compliance (Tier 3 evaluation);

1.2.12 Comparison of the concentrations of chemical(s) of concern at the site at the determined point(s) of compliance or source area(s) with the Tier 3 evaluation SSTL; and

1.2.13 Development of a remedial action plan to achieve the SSTL, as applicable.

1.3 The guide is organized as follows:

1.3.1 Section 2 lists referenced documents,

1.3.2 Section 3 defines terminology used in this guide,

1.3.3 Section 4 describes the significance and use of this guide,

1.3.4 Section 5 is a summary of the tiered approach,

1.3.5 Section 6 presents the RBCA procedures in a step-by-step process,

1.3.6 Appendix X1 details physical/chemical and toxicological characteristics of petroleum products,

1.3.7 Appendix X2 discusses the derivation of a Tier 1 RBSL Look-Up Table and provides an example,

1.3.8 Appendix X3 describes the uses of predictive modeling relative to the RBCA process,

1.3.9 Appendix X4 discusses considerations for institutional controls, and

1.3.10 Appendix X5 provides examples of RBCA applications.

1.4 This guide describes an approach for RBCA. It is intended to compliment but not supersede federal, state, and local regulations. Federal, state, or local agency approval may be required to implement the processes outlined in this guide.

1.5 The values stated in either inch-pound or SI units are to be regarded as the standard. The values given in parentheses are for information only.

1.6 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.*

2. Referenced Documents

2.1 *ASTM Standard:*

[1] This guide is under the jurisdiction of ASTM Committee E-50 on Environmental Assessment and is the direct responsibility of Subcommittee E50.01 on Storage Tanks.

Current edition approved Sept. 10, 1995. Published November 1995. Originally published as ES 38 – 94. Last previous edition ES 38 – 94.

[2] The boldface numbers in parentheses refer to the list of references at the end of this guide.

E 1599 Guide for Corrective Action for Petroleum Releases[3]

2.2 *NFPA Standard:*

NFPA 329 Handling Underground Releases of Flammable and Combustible Liquids[4]

3. Terminology

3.1 *Descriptions of Terms Specific to This Standard:*

3.1.1 *active remediation*—actions taken to reduce the concentrations of chemical(s) of concern. Active remediation could be implemented when the no-further-action and passive remediation courses of action are not appropriate.

3.1.2 *attenuation*—the reduction in concentrations of chemical(s) of concern in the environment with distance and time due to processes such as diffusion, dispersion, absorption, chemical degradation, biodegradation, and so forth.

3.1.3 *chemical(s) of concern*—specific constituents that are identified for evaluation in the risk assessment process.

3.1.4 *corrective action*—the sequence of actions that include site assessment, interim remedial action, remedial action, operation and maintenance of equipment, monitoring of progress, and termination of the remedial action.

3.1.5 *direct exposure pathways*—an exposure pathway where the point of exposure is at the source, without a release to any other medium.

3.1.6 *ecological assessment*—a qualitative appraisal of the actual or potential effects of chemical(s) of concern on plants and animals other than people and domestic species.

3.1.7 *engineering controls*—modifications to a site or facility (for example, slurry walls, capping, and point of use water treatment) to reduce or eliminate the potential for exposure to a chemical(s) of concern.

3.1.8 *exposure*—contact of an organism with chemical(s) of concern at the exchange boundaries (for example, skin, lungs, and liver) and available for absorption.

3.1.9 *exposure assessment*—the determination or estimation (qualitative or quantitative) of the magnitude, frequency, duration, and route of exposure.

3.1.10 *exposure pathway*—the course a chemical(s) of concern takes from the source area(s) to an exposed organism. An exposure pathway describes a unique mechanism by which an individual or population is exposed to a chemical(s) of concern originating from a site. Each exposure pathway includes a source or release from a source, a point of exposure, and an exposure route. If the exposure point differs from the source, a transport/exposure medium (for example, air) or media also is included.

3.1.11 *exposure route*—the manner in which a chemical(s) of concern comes in contact with an organism (for example, ingestion, inhalation, and dermal contact).

3.1.12 *facility*—the property containing the source of the chemical(s) of concern where a release has occurred.

3.1.13 *hazard index*—the sum of two or more hazard quotients for multiple chemical(s) of concern or multiple exposure pathways, or both.

3.1.14 *hazard quotients*—the ratio of the level of exposure of a chemical(s) of concern over a specified time period to a reference dose for that chemical(s) of concern derived for a similar exposure period.

3.1.15 *incremental carcinogenic risk levels*—the potential for incremental carcinogenic human health effects due to exposure to the chemical(s) of concern.

3.1.16 *indirect exposure pathways*—an exposure pathway with at least one intermediate release to any media between the source and the point(s) of exposure (for example, chemicals of concern from soil through ground water to the point(s) of exposure).

3.1.17 *institutional controls*—the restriction on use or access (for example, fences, deed restrictions, restrictive zoning) to a site or facility to eliminate or minimize potential exposure to a chemical(s) of concern.

3.1.18 *interim remedial action*—the course of action to mitigate fire and safety hazards and to prevent further migration of hydrocarbons in their vapor, dissolved, or liquid phase.

3.1.19 *maximum contaminant level (MCL)*—a standard for drinking water established by USEPA under the Safe Drinking Water Act, which is the maximum permissible level of chemical(s) of concern in water that is delivered to any user of a public water supply.

3.1.20 *Monte Carlo simulation*—a procedure to estimate the value and uncertainty of the result of a calculation when the result depends on a number of factors, each of which is also uncertain.

3.1.21 *natural biodegradation*—the reduction in concentration of chemical(s) of concern through naturally occurring microbial activity.

3.1.22 *petroleum*—including crude oil or any fraction thereof that is liquid at standard conditions of temperature and pressure (60°F and 14.7 lb/in.^{2} absolute: (15.5°C and 10 335.6 kg/m^2)). The term includes petroleum-based substances comprised of a complex blend of hydrocarbons derived from crude oil through processes of separation, conversion, upgrading, and finishing, such as motor fuels, jet oils, lubricants, petroleum solvents, and used oils.

3.1.23 *point(s) of compliance*—a location(s) selected between the source area(s) and the potential point(s) of exposure where concentrations of chemical(s) of concern must be at or below the determined target levels in media (for example, ground water, soil, or air).

3.1.24 *point(s) of exposure*—the point(s) at which an individual or population may come in contact with a chemical(s) of concern originating from a site.

3.1.25 *qualitative risk analysis*—a nonnumeric evaluation of a site to determine potential exposure pathways and receptors based on known or readily available information.

3.1.26 *reasonable maximum exposure (RME)*—the highest exposure that is reasonably expected to occur at a site. RMEs are estimated for individual pathways or a combination of exposure pathways.

3.1.27 *reasonable potential exposure scenario*—a situation with a credible chance of occurence where a receptor may become directly or indirectly exposed to the chemical(s) of concern without considering extreme or essentially impossible circumstances.

3.1.28 *reasonably anticipated future use*—future use of a site or facility that can be predicted with a high degree of

[3] *Annual Book of ASTM Standards*, Vol 11.04.

[4] Available from National Fire Protection Association, 1 Batterymarch Park, P.O. Box 9101, Quincy, MA 02269.

certainty given current use, local government planning, and zoning.

3.1.29 *receptors*—persons, structures, utilities, surface waters, and water supply wells that are or may be adversely affected by a release.

3.1.30 *reference dose*—a preferred toxicity value for evaluating potential noncarcinogenic effects in humans resulting from exposure to a chemical(s) of concern.

3.1.31 *remediation/remedial action*—activities conducted to protect human health, safety, and the environment. These activities include evaluating risk, making no-further-action determinations, monitoring institutional controls, engineering controls, and designing and operating cleanup equipment.

3.1.32 *risk assessment*—an analysis of the potential for adverse health effects caused by a chemical(s) of concern from a site to determine the need for remedial action or the development of target levels where remedial action is required.

3.1.33 *risk reduction*—the lowering or elimination of the level of risk posed to human health or the environment through interim remedial action, remedial action, or institutional or engineering controls.

3.1.34 *risk-based screening level/screening levels (RBSLs)*—risk-based site-specific corrective action target levels for chemical(s) of concern developed under the Tier 1 evaluation.

3.1.35 *site*—the area(s) defined by the extent of migration of the chemical(s) of concern.

3.1.36 *site assessment*—an evaluation of subsurface geology, hydrology, and surface characteristics to determine if a release has occurred, the levels of the chemical(s) of concern, and the extent of the migration of the chemical(s) of concern. The site assessment collects data on ground water quality and potential receptors and generates information to support remedial action decisions.

3.1.37 *site classification*—a qualitative evaluation of a site based on known or readily available information to identify the need for interim remedial actions and further information gathering. Site classification is intended to specifically prioritize sites.

3.1.38 *site-specific target level (SSTL)*—risk-based remedial action target level for chemical(s) of concern developed for a particular site under the Tier 2 and Tier 3 evaluations.

3.1.39 *site-specific*—activities, information, and data unique to a particular site.

3.1.40 *source area(s)*—either the location of liquid hydrocarbons or the location of highest soil and ground water concentrations of the chemical(s) of concern.

3.1.41 *target levels*—numeric values or other performance criteria that are protective of human health, safety, and the environment.

3.1.42 *Tier 1 evaluation*—a risk-based analysis to develop non-site-specific values for direct and indirect exposure pathways utilizing conservative exposure factors and fate and transport for potential pathways and various property use categories (for example, residential, commercial, and industrial uses). Values established under Tier 1 will apply to all sites that fall into a particular category.

3.1.43 *Tier 2 evaluation*—a risk-based analysis applying the direct exposure values established under a Tier 1 evaluation at the point(s) of exposure developed for a specific site and development of values for potential indirect exposure pathways at the point(s) of exposure based on site-specific conditions.

3.1.44 *Tier 3 evaluation*—a risk-based analysis to develop values for potential direct and indirect exposure pathways at the point(s) of exposure based on site-specific conditions.

3.1.45 *user*—an individual or group involved in the RBCA process including owners, operators, regulators, underground storage tank (UST) fund managers, attorneys, consultants, legislators, and so forth.

4. Significance and Use

4.1 The allocation of limited resources (for example, time, money, regulatory oversight, qualified professionals) to any one petroleum release site necessarily influences corrective action decisions at other sites. This has spurred the search for innovative approaches to corrective action decision making, which still ensures that human health and the environment are protected.

4.2 The RBCA process presented in this guide is a consistent, streamlined decision process for selecting corrective actions at petroleum release sites. Advantages of the RBCA approach are as follows:

4.2.1 Decisions are based on reducing the risk of adverse human or environmental impacts.

4.2.2 Site assessment activities are focussed on collecting only that information that is necessary to making risk-based corrective action decisions,

4.2.3 Limited resources are focussed on those sites that pose the greatest risk to human health and the environment at any time,

4.2.4 The remedial action achieves an acceptable degree of exposure and risk reduction,

4.2.5 Compliance can be evaluated relative to site-specific standards applied at site-specific point(s) of compliance,

4.2.6 Higher quality, and in some cases faster, cleanups than are currently realized, and

4.2.7 A documentation and demonstration that the remedial action is protective of human health, safety, and the environment.

4.3 Risk assessment is a developing science. The scientific approach used to develop the RBSL and SSTL may vary by state and user due to regulatory requirements and the use of alternative scientifically based methods.

4.4 Activities described in this guide should be conducted by a person familiar with current risk and exposure assessment methodologies.

4.5 In order to properly apply the RBCA process, the user should avoid the following:

4.5.1 Use of Tier 1 RBSLs as mandated remediation standards rather than screening levels,

4.5.2 Restriction of the RBCA process to Tier 1 evaluation only and not allowing Tier 2 or Tier 3 analyses,

4.5.3 Placing arbitrary time constraints on the corrective action process; for example, requiring that Tiers 1, 2, and 3 be completed within 30-day time periods that do not reflect the actual urgency of and risks posed by the site,

4.5.4 Use of the RBCA process only when active remediation is not technically feasible, rather than a process that is applicable during all phases of corrective action,

4.5.5 Requiring the user to achieve technology-based remedial limits (for example, asymptotic levels) prior to requesting the approval for the RBSL or SSTL,

4.5.6 The use of predictive modelling that is not supported by available data or knowledge of site conditions,

4.5.7 Dictating that corrective action goals can only be achieved through source removal and treatment actions, thereby restricting the use of exposure reduction options, such as engineering and institutional controls,

4.5.8 The use of unjustified or inappropriate exposure factors,

4.5.9 The use of unjustified or inappropriate toxicity parameters,

4.5.10 Neglecting aesthetic and other criteria when determining RBSLs or SSTLs,

4.5.11 Not considering the effects of additivity when screening multiple chemicals,

4.5.12 Not evaluating options for engineering or institutional controls, exposure point(s), compliance point(s), and carcinogenic risk levels before submitting remedial action plans,

4.5.13 Not maintaining engineering or institutional controls, and

4.5.14 Requiring continuing monitoring or remedial action at sites that have achieved the RBSL or SSTL.

5. Tiered Approach to Risk-Based Corrective Action (RBCA) at Petroleum Release Sites

5.1 RBCA is the integration of site assessment, remedial action selection, and monitoring with USEPA-recommended risk and exposure assessment practices. This creates a process by which corrective action decisions are made in a consistent manner that is protective of human health and the environment.

5.2 The RBCA process is implemented in a tiered approach, involving increasingly sophisticated levels of data collection and analysis. The assumptions of earlier tiers are replaced with site-specific data and information. Upon evaluation of each tier, the user reviews the results and recommendations and decides whether more site-specific analysis is warranted.

5.3 *Site Assessment*—The user is required to identify the sources of the chemical(s) of concern, obvious environmental impacts (if any), any potentially impacted humans and environmental receptors (for example, workers, residents, water bodies, and so forth), and potentially significant transport pathways (for example, ground water flow, utilities, atmospheric dispersion, and so forth). The site assessment will also include information collected from historical records and a visual inspection of the site.

5.4 *Site Classification*—Sites are classified by the urgency of need for initial response action, based on information collected during the site assessment. Associated with site classifications are initial response actions that are to be implemented simultaneously with the RBCA process. Sites should be reclassified as actions are taken to resolve concerns or as better information becomes available.

5.5 *Tier 1 Evaluation*—A look-up table containing screening level concentrations is used to determine whether site conditions satisfy the criteria for a quick regulatory closure or warrant a more site-specific evaluation. Ground water, soil, and vapor concentrations may be presented in this table for a range of site descriptions and types of petroleum products ((for example, gasoline, crude oil, and so forth). The look-up table of RBSL is developed in Tier 1 or, if a look-up table has been previously developed and determined to be applicable to the site by the user, then the existing RBSLs are used in the Tier 1 process. Tier 1 RBSLs are typically derived for standard exposure scenarios using current RME and toxicological parameters as recommended by the USEPA. These values may change as new methodologies and parameters are developed. Tier 1 RBSLs may be presented as a range of values, corresponding to a range of risks or property uses.

5.6 *Tier 2 Evaluation*—Tier 2 provides the user with an option to determine SSTLs and point(s) of compliance. It is important to note that both Tier 1 RBSL and Tier 2 SSTLs are based on achieving similar levels of protection of human health and the environment (for example, 10^{-4} to 10^{-6} risk levels). However, in Tier 2 the non-site-specific assumptions and point(s) of exposure used in Tier 1 are replaced with site-specific data and information. Additional site-assessment data may be needed. For example, the Tier 2 SSTL can be derived from the same equations used to calculate the Tier 1 RBSL, except that site-specific parameters are used in the calculations. The additional site-specific data may support alternate fate and transport analysis. At other sites, the Tier 2 analysis may involve applying Tier 1 RBSLs at more probable point(s) of exposure. Tier 2 SSTLs are consistent with USEPA-recommended practices.

5.7 *Tier 3 Evaluation*—Tier 3 provides the user with an option to determine SSTLs for both direct and indirect pathways using site-specific parameters and point(s) of exposure and compliance when it is judged that Tier 2 SSTLs should not be used as target levels. Tier 3, in general, can be a substantial incremental effort relative to Tiers 1 and 2, as the evaluation is much more complex and may include additional site assessment, probabilistic evaluations, and sophisticated chemical fate/transport models.

5.8 *Remedial Action*—If the concentrations of chemical(s) of concern at a site are above the RBSL or SSTL at the point(s) of compliance or source area, or both, and the user determines that the RBSL or SSTL should be used as remedial action target levels, the user develops a remedial action plan in order to reduce the potential for adverse impacts. The user may use remediation processes to reduce concentrations of the chemical(s) of concern to levels below or equal to the target levels or to achieve exposure reduction (or elimination) through institutional controls discussed in Appendix X4, or through the use of engineering controls, such as capping and hydraulic control.

6. Risk-Based Corrective Action (RBCA) Procedures

6.1 The sequence of principal tasks and decisions associated with the RBCA process are outlined on the flowchart shown in Fig. 1. Each of these actions and decisions is discussed as follows.

6.2 *Site Assessment*—Gather the information necessary for site classification, initial response action, comparison to the RBSL, and determining the SSTL. Site assessment may be conducted in accordance with Guide E 1599. Each successive tier will require additional site-specific data and information that must be collected as the RBCA process

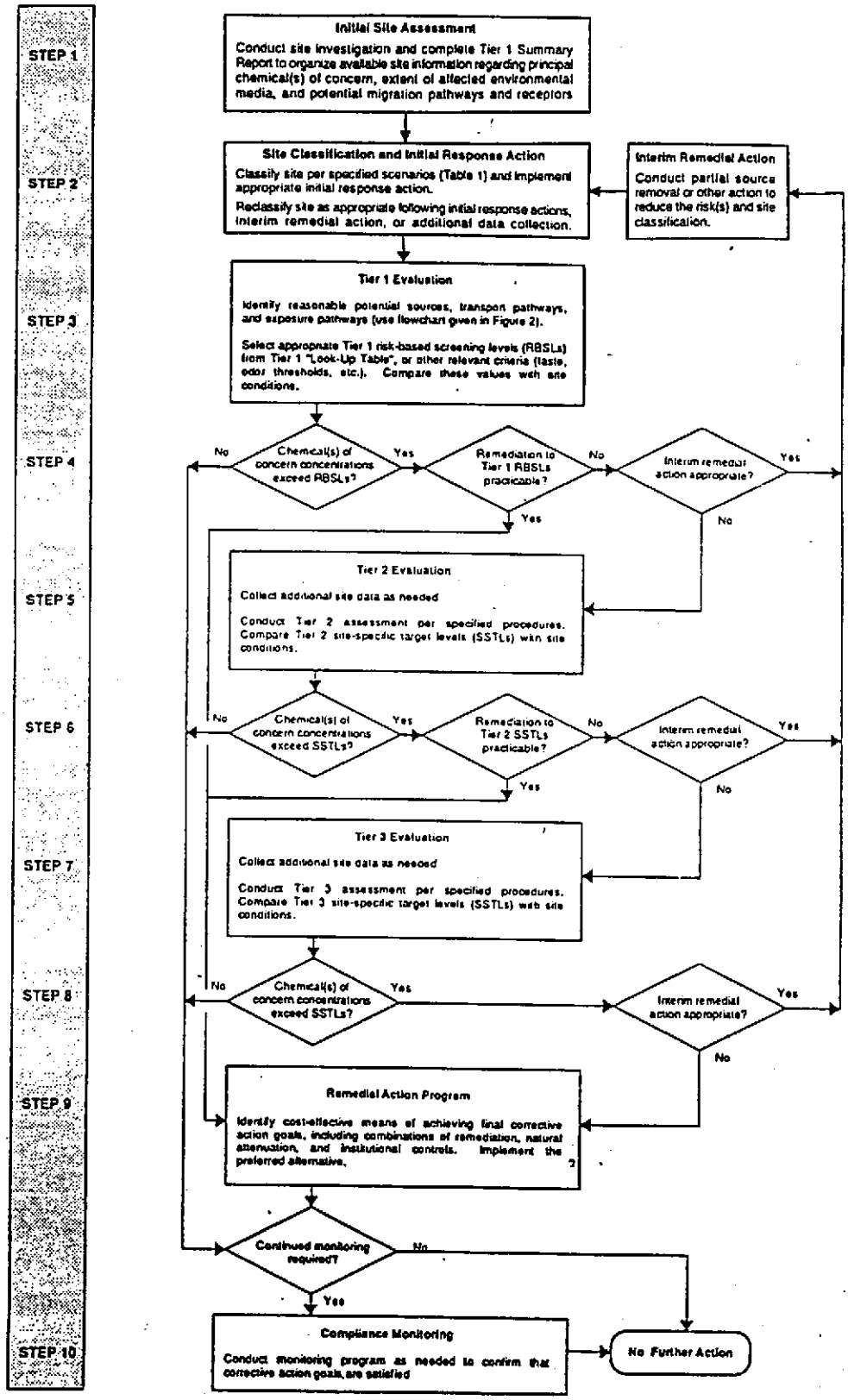


FIG. 1 Risk-Based Corrective Action Process Flowchart

proceeds. The user may generate site-specific data and information or estimate reasonable values for key physical characteristics using soil survey data and other readily available information. The site characterization data should be summarized in a clear and concise format.

6.2.1 The site assessment information for Tier 1 evaluation may include the following:

6.2.1.1 A review of historical records of site activities and past releases;

6.2.1.2 Identification of chemical(s) of concern;

6.2.1.3 Location of major sources of the chemical(s) of concern;

6.2.1.4 Location of maximum concentrations of chemical(s) of concern in soil and ground water;

6.2.1.5 Location of humans and the environmental receptors that could be impacted (point(s) of exposure);

6.2.1.6 Identification of potential significant transport and exposure pathways (ground water transport, vapor migration through soils and utilities, and so forth);

6.2.1.7 Determination of current or potential future use of the site and surrounding land, ground water, surface water, and sensitive habitats;

6.2.1.8 Determination of regional hydrogeologic and geologic characteristics (for example, depth to ground water, aquifer thickness, flow direction, gradient, description of confining units, and ground water quality); and

6.2.19 A qualitative evaluation of impacts to environmental receptors.

6.2.2 In addition to the information gathered in 6.2.1, the site assessment information for Tier 2 evaluation may include the following:

6.2.2.1 Determination of site-specific hydrogeologic and geologic characteristics (for example, depth to ground water, aquifer thickness, flow direction, gradient, description of confining units, and ground water quality);

6.2.2.2 Determination of extent of chemical(s) of concern relative to the RBSL or SSTL, as appropriate;

6.2.2.3 Determination of changes in concentrations of chemical(s) of concern over time (for example, stable, increasing, and decreasing); and

6.2.2.4 Determination of concentrations of chemical(s) of concern measured at point(s) of exposure (for example, dissolved concentrations in nearby drinking water wells or vapor concentrations in nearby conduits or sewers).

6.2.3 In addition to the information gathered in 6.2.1 and 6.2.2, the site assessment information for Tier 3 evaluation includes additional information that is required for site-specific modeling efforts.

6.3 *Site Classification and Initial Response Action*—As the user gathers data, site conditions should be evaluated and an initial response action should be implemented, consistent with site conditions. This process is repeated when new data indicate a significant change in site conditions. Site urgency classifications are presented in Table 1, along with example classification scenarios and potential initial responses. *Note that the initial response actions given in Table 1 may not be applicable for all sites. The user should select an option that best addresses the short-term health and safety concerns of the site while implementing the RBCA process.*

6.3.1 The classification and initial response action scheme given in Table 1 is an example. It is based on the current and projected degree of hazard to human health and the environment. This is a feature of the process that can be customized by the user. "Classification 1" sites are associated with immediate threats to human health and the environment; "Classification 2" sites are associated with short-term (0 to 2-year) threats to human health, safety, and the environment; "Classification 3" sites are associated with long-term (greater than 2-year) threats to human health, safety, and the environment; "Classification 4" sites are associated with no reasonable potential threat to human health or to the environment.

6.3.2 Associated with each classification scenario in Table 1 is an initial response action; the initial response actions are implemented in order to eliminate any potential immediate impacts to human health and the environment as well as to minimize the potential for future impacts that may occur as the user proceeds with the RBCA process. Note that initial response actions do not always require active remediation; in many cases the initial response action is to monitor or further assess site conditions to ensure that risks posed by the site do not increase above acceptable levels over time. The initial response actions given in Table 1 are examples, and the user is free to implement other alternatives.

6.3.3 The need to reclassify the site should be evaluated when additional site information is collected that indicates a significant change in site conditions or when implementation of an interim response action causes a significant change in site conditions.

6.4 *Development of a Tier 1 Look-Up Table of RBSL*—If a look-up table is not available, the user is responsible for developing the look-up table. If a look-up table is available, the user is responsible for determining that the RBSLs in the look-up table are based on currently acceptable methodologies and parameters. The look-up table is a tabulation for potential exposure pathways, media (for example, soil, water, and air), a range of incremental carcinogenic risk levels (10E-4 to 10E-6 are often evaluated as discussed in Appendix X1) and hazard quotients equal to unity, and potential exposure scenarios (for example, residential, commercial, industrial, and agricultural) for each chemical(s) of concern.

6.4.1 The RBSLs are determined using typical, non-site-specific values for exposure parameters and physical parameters for media. The RBSLs are calculated according to methodology suggested by the USEPA. For each exposure scenario, the RBSLs are based on current USEPA RME parameters and current toxicological information given in Refs (2, 3) or peer-reviewed source(s). Consequently, the RBSL look-up table is updated when new methodologies and parameters are developed. For indirect pathways, fate and transport models can be used to predict RBSLs at a source area that corresponds to exposure point concentrations. An example of the development of a Tier 1 Look-Up Table and RBSL is given in Appendix X2. *Figure 2 and Appendix X2 are presented solely for the purpose of providing an example development of the RBSL, and the values should not be viewed as proposed RBSLs.*

6.4.2 Appendix X2 is an example of an abbreviated Tier 1 RBSL Look-Up Table for compounds of concern associated with petroleum releases. The exposure scenarios selected in the example case are for residential and industrial/commercial scenarios characterized by USEPA RME parameters for

TABLE 1 Example Site Classification and Initial Response Actions[A]

Criteria and Prescribed Scenarios	Example Initial Response Actions[B]
1. Immediate threat to human health, safety, or sensitive environmental receptors	Notify appropriate authorities, property owners, and potentially affected parties, and only evaluate the need to
• Explosive levels, or concentrations of vapors that could cause acute health effects, are present in a residence or other building.	• Evacuate occupants and begin abatement measures such as subsurface ventilation or building pressurization.
• Explosive levels of vapors are present in subsurface utility system(s), but no building or residences are impacted.	• Evacuate immediate vicinity and begin abatement measures such as ventilation.
• Free-product is present in significant quantities at ground surface, on surface water bodies, in utilities other than water supply lines, or in surface water runoff.	• Prevent further free-product migration by appropriate containment measures, institute free-product recovery, and restrict area access.
• An active public water supply well, public water supply line, or public surface water intake is impacted or immediately threatened.	• Notify user(s), provide alternate water supply, hydraulically control contaminated water, and treat water at point-of-use.
• Ambient vapor/particulate concentrations exceed concentrations of concern from an acute exposure or safety viewpoint.	• Install vapor barrier (capping, foams, and so forth), remove source, or restrict access to affected area.
• A sensitive habitat or sensitive resources (sport fish, economically important species, threatened and endangered species, and so forth) are impacted and affected.	• Minimize extent of impact by containment measures and implement habitat management to minimize exposure.
2. Short-term (0 to 2 years) threat to human health, safety, or sensitive environmental receptors	Notify appropriate authorities, property owners, and potentially affected parties, and only evaluate the need to
• There is potential for explosive levels, or concentrations of vapors that could cause acute effects, to accumulate in a residence or other building.	• Assess the potential for vapor migration (through monitoring/ modeling) and remove source (if necessary), or install vapor migration barrier.
• Shallow contaminated surface soils are open to public access, and dwellings, parks, playgrounds, day-care centers, schools, or similar use facilities are within 500 ft (152 m) of those soils.	• Remove soils, cover soils, or restrict access.
• A non-potable water supply well is impacted or immediately threatened.	• Notify owner/user and evaluate the need to install point-of-use water treatment, hydraulic control, or alternate water supply.
• Ground water is impacted, and a public or domestic water supply well producing from the impacted aquifer is located within two-years projected ground water travel distance down gradient of the known extent of chemical(s) concern.	• Institute monitoring and then evaluate if natural attenuation is sufficient, or if hydraulic control is required.
• Ground water is impacted, and a public or domestic water supply well producing from a different interval is located within the known extent of chemicals of concern.	• Monitor ground water well quality and evaluate if control is necessary to prevent vertical migration to the supply well.
• Impacted surface water, storm water, or ground water discharges within 500 ft (152 m) of a sensitive habitat or surface water body used for human drinking water or contact recreation.	• Institute containment measures, restrict access to areas near discharge, and evaluate the magnitude and impact of the discharge.
3. Long-term (>2 years) threat to human health, safety, or sensitive environmental receptors	Notify appropriate authorities, property owners, and potentially affected parties, and only evaluate the need to
• Subsurface soils (>3 ft (0.9.m) BGS) are significantly impacted, and the depth between impacted soils and the first potable aquifer is less than 50 ft (15 m).	• Monitor ground water and determine the potential for future migration of the chemical(s) concerns to the aquifer.
• Ground water is impacted, and potable water supply wells producing from the impacted interval are located >2 years ground water travel time from the dissolved plume.	• Monitor the dissolved plume and evaluate the potential for natural attenuation and the need for hydraulic control.
• Ground water is impacted, and non-potable water supply wells producing from the impacted interval are located >2 years ground water travel time from the dissolved plume.	• Identify water usage of well, assess the effect of potential impact, monitor the dissolved plume, and evaluate whether natural attenuation or hydraulic control are appropriate control measures.
• Ground water is impacted, and non-potable water supply wells that do not produce from the impacted interval are located within the known extent of chemical(s) of concern.	• Monitor the dissolved plume, determine the potential for vertical migration, notify the user, and determine if any impact is likely.
• Impacted surface water, storm water, or ground water discharges within 1500 ft (457 m) of a sensitive habitat or surface water body used for human drinking water or contact recreation.	• Investigate current impact on sensitive habitat or surface water body, restrict access to area of discharge (if necessary), and evaluate the need for containment/control measures.
• Shallow contaminated surface soils are open to public access, and dwellings, parks, playgrounds, day-care centers, schools, or similar use facilities are more than 500 ft (152 m) of those soils.	• Restrict access to impact soils.
4. No demonstrable long-term threat to human health or safety or sensitive environmental receptors	Notify appropriate authorities, property owners, and potentially affected parties, and only evaluate the need to
Priority 4 scenarios encompass all other conditions not described in Priorities 1, 2, and 3 and that are consistent with the priority description given above. Some examples are as follows:	
• Non-potable aquifer with no existing local use impacted.	• Monitor ground water and evaluate effect of natural attenuation on dissolved plume migration.
• Impacted soils located more than 3 ft (0.9 m) BGS and greater than 50 ft (15 m) above nearest aquifer.	• Monitor ground water and evaluate effect of natural attenuation on leachate migration.
• Ground water is impacted, and non-potable wells are located down gradient outside the known extent of the chemical(s) of concern, and they produce from a nonimpacted zone.	• Monitor ground water and evaluate effect of natural attenuation on dissolved plume migration.

[A] Johnson, D. C., DeVaull, G. E., Ettinger, R. A., MacDonald, R. L. M., Stanley, C. C., Westby, T. S., and Conner, J., "Risk-Based Corrective Action: Tier 1 Guidance Manual," Shell Oil Co., July 1993.

[B] Note that these are potential initial response actions that may not be appropriate for all sites. The user is encouraged to select options that best address the short-term health and safety concerns of the site, while the RBCA process progresses.

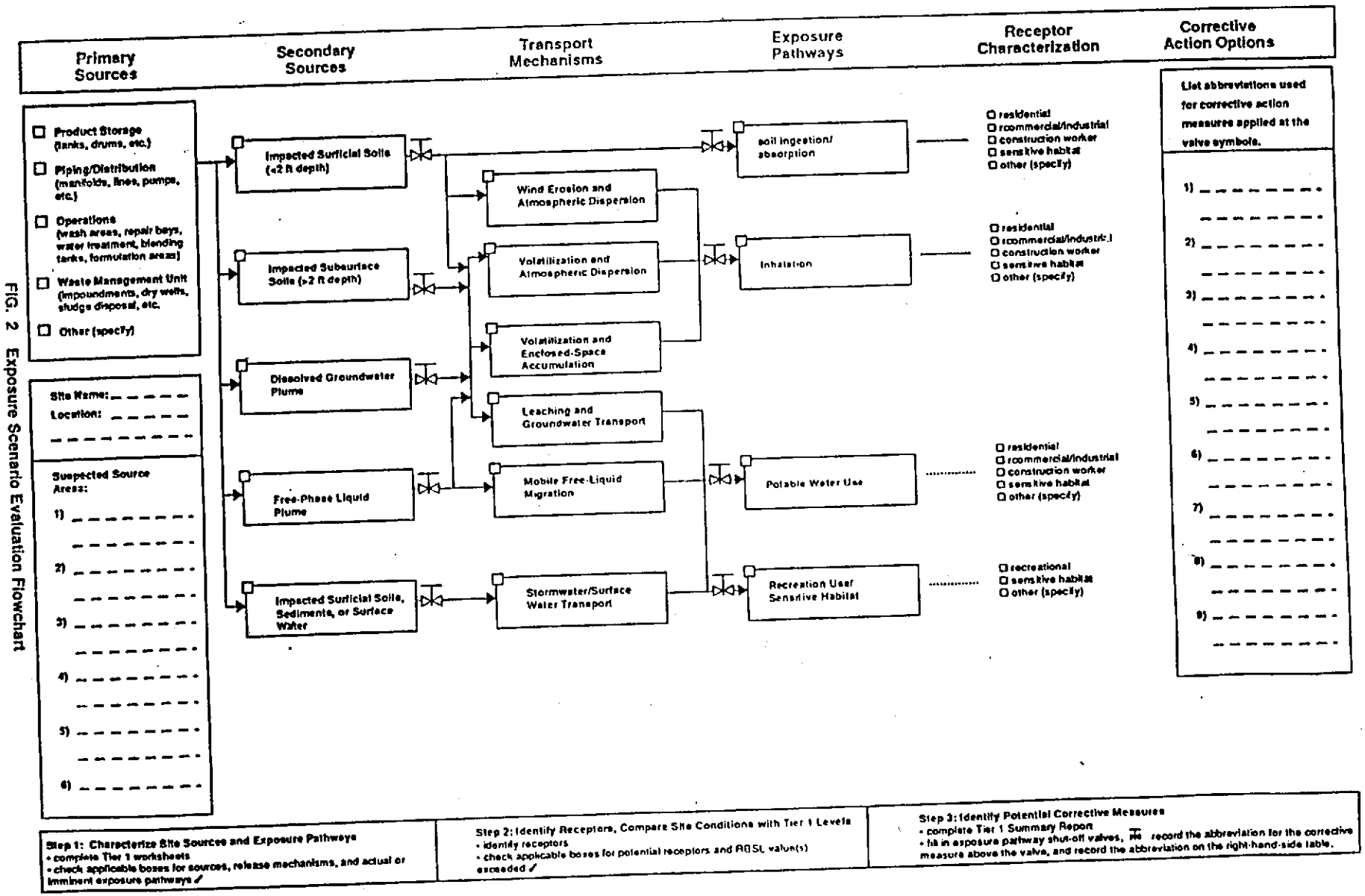


FIG. 2 Exposure Scenario Evaluation Flowchart

adult males. The assumptions and methodology used in deriving the example are discussed in Appendix X2. Note that not all possible exposure pathways are considered in the derivation of the example. *The user should always review the assumptions and methodology used to derive values in a look-up table to make sure that they are consistent with reasonable exposure scenarios for the site being considered as well as currently accepted methodologies.* The value of creating a look-up table is that users do not have to repeat the exposure calculations for each site encountered. The look-up table is only altered when RME parameters, toxicological information, or recommended methodologies are updated. Some states have compiled such tables for direct exposure pathways that, for the most part, contain identical values (as they are based on the same assumptions). Values for the cross-media pathways (for example, volatilization and leaching), when available, often differ because these involve coupling exposure calculations with predictive equations for the fate and transport of chemicals in the environment. As yet, there is little agreement in the technical community concerning non-site-specific values for the transport and fate model parameters, or the choice of the models themselves. *Again, the reader should note that the example is presented here only as an abbreviated example of a Tier 1 RBSL Look-Up Table for typical compounds of concern associated with petroleum products.*

6.4.3 *Use of Total Petroleum Hydrocarbon Measurements*—Various chemical analysis methods commonly referred to as total petroleum hydrocarbons (TPHs) are often used in site assessments. These methods usually determine the total amount of hydrocarbons present as a single number and give no information on the types of hydrocarbon present. The TPHs should not be used for risk assessment because the general measure of TPH provides insufficient information about the amounts of individual chemical(s) of concern present.

6.5 *Comparison of Site Conditions with Tier 1 Risk-Based Screening Levels (RBSL)*—In Tier 1, the point(s) of exposure and point(s) of compliance are assumed to be located within close proximity to the source area(s) or the area where the highest concentrations of the chemical(s) of concern have been identified. Concentrations of the chemical(s) of concern measured at the source area(s) identified at the site should be compared to the look-up table RBSL. If there is sufficient site assessment data, the user may opt to compare RBSLs with statistical limits (for example, upper confidence levels) rather than maximum values detected. Background concentrations should be considered when comparing the RBSLs, to the site concentrations as the RBSLs may sometimes be less than background concentrations. Note that additivity of risks is not explicitly considered in the Tier 1 evaluation, as it is expected that the RBSLs are typically for a limited number of chemical(s) of concern considered at most sites. Additivity may be addressed in Tier 2 and Tier 3 analyses. To accomplish the Tier 1 comparison:

6.5.1 Select the potential exposure scenario(s) (if any) for the site. Exposure scenarios are determined based on the site assessment information described in 6.2;

6.5.2 Based on the impacted media identified, determine the primary sources, secondary sources, transport mechanisms, and exposure pathways;

6.5.3 Select the receptors (if any) based on current and anticipated future use. Consider land use restrictions and surrounding land use when making this selection.

6.5.4 Identify the exposure scenarios where the measured concentrations of the chemical(s) of concern are above the RBSL.

6.6 *Exposure Evaluation Flowchart*—During a Tier 1 evaluation, the risk evaluation flowchart presented in Fig. 2 may be used as a tool to guide the user in selecting appropriate exposure scenarios based on site assessment information. This worksheet may also be used in the evaluation of remedial action alternatives. To complete this flowchart:

6.6.1 Characterize site sources and exposure pathways, using the data summarized from Tier 1 to customize the risk evaluation flowchart for the site by checking the small checkbox for every relevant source, transport mechanism, and exposure pathway.

6.6.2 Identify receptors, and compare site conditions with Tier 1 levels: For each exposure pathway selected, check the receptor characterization (residential, commercial, and so forth) where the concentrations of the chemical(s) of concern are above the RBSL. Consider land use restrictions and surrounding land use when making this selection. Do not check any boxes if there are no receptors present, or likely to be present, or if institutional controls prevent exposure from occurring and are likely to stay in place.

6.6.3 Identify potential remedial action measures. Select remedial action options to reduce or eliminate exposure to the chemical(s) of concern.

6.6.4 The exposure evaluation flowchart (Fig. 2) can be used to graphically portray the effect of the Tier 1 remedial action. Select the Tier 1 remedial action measure or measures (shown as valve symbols) that will break the lines linking sources, transport mechanisms, and pathways leading to the chemical(s) of concern above the RBSL. Adjust the mix of remedial action measures until no potential receptors have concentrations of chemical(s) of concerns above the RBSL with the remedial action measures in place. Show the most likely Tier 1 remedial action measure(s) selected for this site by marking the appropriate valve symbols on the flowchart and recording a remedial action measure on the right-hand-side of this figure.

6.7 *Evaluation of Tier Results*—At the conclusion of each tier evaluation, the user compares the target levels (RBSLs or SSTLs) to the concentrations of the chemical(s) of concern at the point(s) of compliance.

6.7.1 If the concentrations of the chemical(s) of concern exceed the target levels at the point(s) of compliance, then either remedial action, interim remedial action, or further tier evaluation should be conducted.

6.7.1.1 *Remedial Action*—A remedial action program is designed and implemented. This program may include some combination of source removal, treatment, and containment technologies, as well as engineering and institutional controls. Examples of these include the following: soil venting, bioventing, air sparging, pump and treat, and natural attenuation/passive remediation. When concentrations of chemical(s) of concern no longer exceed the target levels at the point of compliance, then the user may elect to move to 6.7.3.

6.7.1.2 *Interim Remedial Action*—If achieving the desired risk reduction is impracticable due to technology or resource limitations, an interim remedial action, such as removal or treatment of "hot spots," may be conducted to address the most significant concerns, change the site classification, and facilitate reassessment of the tier evaluation.

6.7.1.3 *Further Tier Evaluation*—If further tier evaluation is warranted, additional site assessment information may be collected to develop SSTLs under a Tier 2 or Tier 3 evaluation. Further tier evaluation is warranted when:

(*1*) The basis for the RBSL values (for example, geology, exposure parameters, point(s) of exposure, and so forth) are not representative of the site-specific conditions; or

(*2*) The SSTL developed under further tier evaluation will be significantly different from the Tier 1 RBSL or will significantly modify the remedial action activities; or

(*3*) Cost of remedial action to RBSLs will likely be greater than further tier evaluation and subsequent remedial action.

6.7.2 If the concentrations of chemicals of concern at the point of compliance are less than the target levels, but the user is not confident that data supports the conclusion that concentrations will not exceed target levels in the future, then the user institutes a monitoring plan to collect data sufficient to confidently conclude that concentrations will not exceed target levels in the future. When this data is collected, the user moves to 6.7.3.

6.7.3 If the concentrations of chemicals of concern at the point of compliance are less than target levels, and the user is confident that data supports the conclusion that concentrations will not exceed target levels in the future, then no additional corrective action activities are necessary, and the user has completed the RBCA process. In practice, this is often accompanied by the issuing of a no-further-action letter by the oversight regulatory agency.

6.8 *Tier 2*—Tier 2 provides the user with an option to determine the site-specific point(s) of compliance and corresponding SSTL for the chemical(s) of concern applicable at the point(s) of compliance and source area(s). Additional site assessment data may be required; however, the incremental effort is typically minimal relative to Tier 1. If the user completes a Tier 1 evaluation, in most cases, only a limited number of pathways, exposure scenarios, and chemical(s) of concern are considered in the Tier 2 evaluation since many are eliminated from consideration during the Tier 1 evaluation.

6.8.1 In Tier 2, the user:

6.8.1.1 Identifies the indirect exposure scenarios to be addressed and the appropriate site-specific point(s) of compliance. A combination of assessment data and predictive modeling results are used to determine the SSTL at the source area(s) or the point(s) of compliance, or both; or

6.8.1.2 Applies Tier 1 RBSL Look-Up Table values for the direct exposure scenarios at reasonable point(s) of exposure (as opposed to the source area(s) as is done in Tier 1). The SSTLs for source area(s) and point(s) of compliance can be determined based on the demonstrated and predicted attenuation (reduction in concentration with distance) of compounds that migrate away from the source area(s).

6.8.1.3 An example of a Tier 2 application is illustrated in Appendix X5.

6.8.2 Tier 2 of the RBCA process involves the development of SSTL based on the measured and predicted attenuation of the chemical(s) of concern away from the source area(s) using relatively simplistic mathematical models. The SSTLs for the source area(s) are generally not equal to the SSTL for the point(s) of compliance. The predictive equations are characterized by the following:

6.8.2.1 The models are relatively simplistic and are often algebraic or semianalytical expressions;

6.8.2.2 Model input is limited to practicably attainable site-specific data or easily estimated quantities (for example, total porosity, soil bulk density); and

6.8.2.3 The models are based on descriptions of relevant physical/chemical phenomena. Most mechanisms that are neglected result in predicted concentrations that are greater than those likely to occur (for example, assuming constant concentrations in source area(s)). Appendix X3 discusses the use of predictive models and presents models that might be considered for Tier 2 evaluation.

6.8.3 *Tier 2 Evaluation*—Identify the exposure scenarios where the measured concentrations of the chemical(s) of concern are above the SSTL at the point(s) of compliance, and evaluate the tier results in accordance with 6.7.

6.9 *Tier 3*—In a Tier 3 evaluation, SSTLs for the source area(s) and the point(s) of compliance are developed on the basis of more sophisticated statistical and contaminant fate and transport analyses, using site-specific input parameters for both direct and indirect exposure scenarios. Source area(s) and the point(s) of compliance SSTLs are developed to correspond to concentrations of chemical(s) of concern at the point(s) of exposure that are protective of human health and the environment. Tier 3 evaluations commonly involve collection of significant additional site information and completion of more extensive modeling efforts than is required for either a Tier 1 or Tier 2 evaluation.

6.9.1 Examples of Tier 3 analyses include the following:

6.9.1.1 The use of numerical ground water modeling codes that predict time-dependent dissolved contaminant transport under conditions of spatially varying permeability fields to predict exposure point(s) of concentrations;

6.9.1.2 The use of site-specific data, mathematical models, and Monte Carlo analyses to predict a statistical distribution of exposures and risks for a given site; and

6.9.1.3 The gathering of sufficient data to refine site-specific parameter estimates (for example, biodegradation rates) and improve model accuracy in order to minimize future monitoring requirements.

6.9.2 *Tier 3 Evaluation*—Identify the exposure scenarios where the measured concentrations of the chemical(s) of concern are above the SSTL at the point(s) of compliance, and evaluate the tier results in accordance with 6.7 except that a tier upgrade (6.7.5) is not available.

6.10 *Implementing the Selected Remedial Action Program*—When it is judged by the user that no further assessment is necessary, or practicable, a remedial alternatives evaluation should be conducted to confirm the most cost-effective option for achieving the final remedial action target levels (RBSLs or SSTLs, as appropriate). Detailed design specifications may then be developed for installation and operation of the selected measure. The remedial action must continue until such time as monitoring indicates that

concentrations of the chemical(s) of concern are not above the RBSL or SSTL, as appropriate, at the points of compliance or source area(s), or both.

6.11 *RBCA Report*—After completion of the RBCA activities, a RBCA report should be prepared and submitted to the regulatory agency. The RBCA report should, at a minimum, include the following:

6.11.1 An executive summary;

6.11.2 A site description;

6.11.3 A summary of the site ownership and use;

6.11.4 A summary of past releases or potential source areas;

6.11.5 A summary of the current and completed site activities;

6.11.6 A description of regional hydrogeologic conditions;

6.11.7 A description of site-specific hydrogeologic conditions;

6.11.8 A summary of beneficial use;

6.11.9 A summary and discussion of the risk assessment (hazard identification, dose response assessment, exposure assessment, and risk characterization), including the methods and assumptions used to calculate the RBSL or SSTL, or both;

6.11.10 A summary of the tier evaluation;

6.11.11 A summary of the analytical data and the appropriate RBSL or SSTL used;

6.11.12 A summary of the ecological assessment;

6.11.13 A site map of the location;

6.11.14 An extended site map to include local land use and ground water supply wells;

6.11.15 Site plan view showing location of structures, aboveground storage tanks, underground storage tanks, buried utilities and conduits, suspected/confirmed sources, and so forth;

6.11.16 Site photos, if available;

6.11.17 A ground water elevation map;

6.11.18 Geologic cross section(s); and

6.11.19 Dissolved plume map(s) of the chemical(s) of concern.

6.12 *Monitoring and Site Maintenance*—In many cases, monitoring is necessary to demonstrate the effectiveness of implemented remedial action measures or to confirm that current conditions persist or improve with time. Upon completion of this monitoring effort (if required), no further action is required. In addition, some measures (for example, physical barriers such as capping, hydraulic control, and so forth) require maintenance to ensure integrity and continued performance.

6.13 *No Further Action and Remedial Action Closure*—When RBCA RBSLs or SSTLs have been demonstrated to be achieved at the point(s) of compliance or source area(s), or both, as appropriate, and monitoring and site maintenance are no longer required to ensure that conditions persist, then no further action is necessary, except to ensure that institutional controls (if any) remain in place.

APPENDIXES

(Nonmandatory Information)

X1. PETROLEUM PRODUCTS CHARACTERISTICS: COMPOSITION, PHYSICAL AND CHEMICAL PROPERTIES, AND TOXICOLOGICAL ASSESSMENT SUMMARY

X1.1 *Introduction:*

X1.1.1 Petroleum products originating from crude oil are complex mixtures of hundreds to thousands of chemicals; however, practical limitations allow us to focus only on a limited subset of key components when assessing the impact of petroleum fuel releases to the environment. Thus, it is important to have a basic understanding of petroleum properties, compositions, and the physical, chemical, and toxicological properties of some compounds most often identified as the key chemicals or chemicals of concern.

X1.1.2 This appendix provides a basic introduction to the physical, chemical, and toxicological characteristics of petroleum products (gasoline, diesel fuel, jet fuel, and so forth)[5] and other products focussed primarily towards that information which is most relevant to assessing potential impacts due to releases of these products into the subsurface. Much of the information presented is summarized from the references listed at the end of this guide. For specific topics, the reader is referred to the following sections of this appendix:

X1.1.2.1 *Composition of Petroleum Fuels*—See X1.2.

X1.1.2.2 *Physical, Chemical, and Toxicological Properties of Petroleum Fuels*—See X1.3.

X1.1.2.3 *Chemical of Concern*—See X1.4.

X1.1.2.4 *Toxicity of Petroleum Hydrocarbons*—See X1.5.

X1.1.2.5 *Profiles of Select Compounds*—See X1.6.

X1.2 *Composition of Petroleum Products:*

X1.2.1 Most petroleum products are derived from crude oil by distillation, which is a process that separates compounds by volatility. Crude oils are variable mixtures of thousands of chemical compounds, primarily hydrocarbons; consequently, the petroleum products themselves are also variable mixtures of large numbers of components. The biggest variations in composition are from one type of product to another (for example, gasoline to motor oil); however, there are even significant variations within different samples of the same product type. For example, samples of gasoline taken from the same fuel dispenser on different days, or samples taken from different service stations, will have different compositions. These variations are the natural result of differing crude oil sources, refining processes and conditions, and kinds and amount of additives used.

[5] "Alternative products," or those products not based on petroleum hydrocarbons (or containing them in small amounts), such as methanol or M85, are beyond the scope of the discussion in this appendix.

X1.2.2 *Components of Petroleum Products*—The components of petroleum products can be generally classified as either hydrocarbons (organic compounds composed of hydrogen and carbon only) or as non-hydrocarbons (compounds containing other elements, such as oxygen, sulfur, or nitrogen). Hydrocarbons make up the vast majority of the composition of petroleum products. The non-hydrocarbon compounds in petroleum products are mostly hydrocarbon-like compounds containing minor amounts of oxygen, sulfur, or nitrogen. Most of the trace levels of metals found in crude oil are removed by refining processes for the lighter petroleum products.

X1.2.3 *Descriptions and Physical Properties of Petroleum Products*—In order to simplify the description of various petroleum products, boiling point ranges and carbon number (number of carbon atoms per molecule) ranges are commonly used to describe and compare the compositions of various petroleum products. Table X1.1 summarizes these characteristics for a range of petroleum products. Moving down the list from gasoline, increases in carbon number range and boiling range and decreases in volatility (denoted by increasing flash point) indicate the transition to "heavier products." Additional descriptions of each of these petroleum products are provided as follows.

X1.2.4 *Gasoline*—Gasoline is composed of hydrocarbons and "additives" that are blended with the fuel to improve fuel performance and engine longevity. The hydrocarbons fall primarily in the C4 to C12 range. The lightest of these are highly volatile and rapidly evaporate from spilled gasoline. The C4 and C5 aliphatic hydrocarbons rapidly evaporate from spilled gasoline (hours to months, depending primarily on the temperature and degree of contact with air). Substantial portions of the C6 and heavier hydrocarbons also evaporate, but at lower rates than for the lighter hydrocarbons.

X1.2.4.1 Figure X1.1 shows gas chromatograms of a fresh gasoline and the same gasoline after simulated weathering; air was bubbled through the gasoline until 60 % of its initial volume was evaporated. In gas chromatography, the mixture is separated into its components, with each peak representing different compounds. Higher molecular weight components appear further to the right along the *x*-axis. For reference, positions of the *n*-aliphatic hydrocarbons are indicated in Fig. X1.1. The height of, and area under, each peak are measures of how much of that component is present in the mixture. As would be expected by their higher volatilities, the lighter hydrocarbons (up to about C7) evaporate first and are greatly reduced in the weathered gasoline. The gas chromatogram of a fuel oil is also shown for comparison.

X1.2.4.2 The aromatic hydrocarbons in gasoline are primarily benzene (C_6H_6), toluene (C_7H_8), ethylbenzene (C_8H_{10}), and xylenes (C_8H_{10}); these are collectively referred to as "BTEX." Some heavier aromatics are present also, including low amounts of polyaromatic hydrocarbons (PAHs). Aromatics typically comprise about 10 to 40 % of gasoline.

X1.2.4.3 Oxygenated compounds ("oxygenates") such as alcohols (for example, methanol or ethanol) and ethers (for example, methyl tertiarybutyl ether—MTBE) are sometimes added to gasoline as octane boosters and to reduce carbon monoxide exhaust emissions. Methyl tertiarbutyl ether has been a common additive only since about 1980.

X1.2.4.4 Leaded gasoline, which was more common in the past, contained lead compounds added as octane boosters. Tetraethyl lead (TEL) is one lead compound that was commonly used as a gasoline additive. Other similar compounds were also used. Sometimes mixtures of several such compounds were added. Because of concerns over atmospheric emissions of lead from vehicle exhaust, the EPA has reduced the use of leaded gasolines. Leaded gasolines were phased out of most markets by 1989.

X1.2.4.5 In order to reduce atmospheric emissions of lead, lead "scavengers" were sometimes added to leaded gasolines. Ethylene dibromide (EDB) and ethylene dichloride (EDC) were commonly used for this purpose.

X1.2.5 *Kerosene and Jet Fuel*—The hydrocarbons in kerosene commonly fall into the C11 to C13 range, and distill at approximately 150 to 250°C. Special wide-cut (that is, having broader boiling range) kerosenes and low-flash kerosenes are also marketed. Both aliphatic and aromatic hydrocarbons are present, including more multi-ring compounds and kerosene.

X1.2.5.1 Commercial jet fuels JP-8 and Jet A have similar compositions to kerosene. Jet fuels JP-4 and JP-5 are wider cuts used by the military. They contain lighter distillates and have some characteristics of both gasoline and kerosene.

X1.2.5.2 Aromatic hydrocarbons comprise about 10 to 20 % of kerosene and jet fuels.

X1.2.6 *Diesel Fuel and Light Fuel Oils*—Light fuel oils include No. 1 and No. 2 fuel oils, and boil in the range from 160 to 400°C. Hydrocarbons in light fuel oils and diesel fuel typically fall in the C10 to C20 range. Because of their higher molecular weights, constituents in these products are less volatile, less water soluble, and less mobile than gasoline- or kerosene-range hydrocarbons.

X1.2.6.1 About 25 to 35 % of No. 2 fuel oil is composed of aromatic hydrocarbons, primarily alkylated benzenes and naphthalenes. The BTEX concentrations are generally low.

X1.2.6.2 No. 1 fuel oil is typically a straight run distillate.

X1.2.6.3 No. 2 fuel oil can be either a straight run distillate, or else is produced by catalytic cracking (a process in which larger molecules are broken down into smaller ones). Straight run distillate No. 2 is commonly used for home heating fuel, while the cracked product is often used for industrial furnaces and boilers. Both No. 1 and No. 2 fuel oils are sometimes used as blending components for jet fuel or diesel fuel formulations.

X1.2.7 *Heavy Fuel Oils*—The heavy fuel oils include Nos. 4, 5, and 6 fuel oils. They are sometimes referred to as "gas oils" or "residual fuel oils." These are composed of hydrocarbons ranging from about C19 to C25 and have a boiling range from about 315 to 540°C. They are dark in color and considerably more viscous than water. They typically contain 15 to 40 % aromatic hydrocarbons, dominated by alkylated phenanthrenes and naphthalenes. Polar compounds containing nitrogen, sulfur, or oxygen may comprise 15 to 30 % of the oil.

X1.2.7.1 No. 6 fuel oil, also called "Bunker Fuel" or "Bunker C," is a gummy black product used in heavy industrial applications where high temperatures are available to fluidize the oil. Its density is greater than that of water.

X1.2.7.2 Nos. 4 and 5 fuel oils are commonly produced by blending No. 6 fuel oil with lighter distillates.

X1.2.8 *Motor Oils and Other Lubricating Oils*—Lubricating oils and motor oils are predominately comprised of compounds in the C20 to C45 range and boil at approximately 425 to 540°C. They are enriched in the most complex molecular fractions found in crude oil, such as cycloparaffins and PNAs having up to three rings or more. Aromatics may make up to 10 to 30 % of the oil. Molecules containing nitrogen, sulfur, or oxygen are also common. In addition, used automative crankcase oils become enriched with PNAs and certain metals.

X1.2.8.1 These oils are relatively viscous and insoluble in ground water and relatively immobile in the subsurface.

X1.2.8.2 Waste oil compositions are even more difficult to predict. Depending on how they are managed, waste oils may contain some portion of the lighter products in addition to heavy oils. Used crankcase oil may contain wear metals from engines. Degreasing solvents (gasoline, naphtha, or light chlorinated solvents, or a combination thereof) may be present in some wastes.

X1.3 *Physical, Chemical, and Toxicological Characteristics of Petroleum Products:*

X1.3.1 *Trends in Physical/Chemical Properties of Hydrocarbons*—In order to better understand the subsurface behavior of hydrocarbons it is helpful to be able to recognize trends in important physical properties with increasing number of carbon atoms. These trends are most closely followed by compounds with similar molecular structures, such as the straight-chained, single-bonded aliphatic hydrocarbons. In general, as the carbon number (or molecule size) increases, the following trends are observed:

X1.3.1.1 Higher boiling points (and melting points),

X1.3.1.2 Lower vapor pressure (volatility),

X1.3.1.3 Greater density,

X1.3.1.4 Lower water solubility, and

X1.3.1.5 Stronger adhesion to soils and less mobility in the subsurface.

X1.3.2 Table X1.2 lists physical, chemical, and toxicological properties for a number of hydrocarbons found in petroleum products. In general:

X1.3.2.1 Aliphatic petroleum hydrocarbons with more than ten carbon atoms are expected to be immobile in the subsurface, except when dissolved in nonaqueous phase liquids (NAPLs), due to their low water solubilities, low vapor pressures, and strong tendency to adsorb to soil surfaces.

X1.3.2.2 Aromatic hydrocarbons are more water soluble and mobile in water than aliphatic hydrocarbons of similar molecular weight.

X1.3.2.3 Oxygenates generally have much greater water solubilities than hydrocarbons of similar molecular weight, and hence are likely to be the most mobile of petroleum fuel constituents in leachate and ground water. The light alcohols, including methanol and ethanol, are completely miscible with water in all proportions.

X1.3.3 *Properties of Mixtures*—It is important to note that the partitioning behavior of individual compounds is affected by the presence of other hydrocarbons in the subsurface. The maximum dissolved and vapor concentrations achieved in the subsurface are always less than that of any pure compound, when it is present as one of many constituents of a petroleum fuel. For example, dissolved benzene concentrations in ground water contacting gasoline-impacted soils rarely exceed 1 to 3 % of the ~1800-mg/L pure component solubility of benzene.

X1.3.4 *Trends in Toxicological Properties of Hydrocarbons*—A more detailed discussion of toxicological assessment is given in X1.5 (see also Appendix X3), followed by profiles for select chemicals found in petroleum products given in X1.6. Of the large number of compounds present in petroleum products, aromatic hydrocarbons (BTEX, PAHs, and so forth) are the constituents that human and aquatic organisms tend to be most sensitive to (relative to producing adverse health impacts).

X1.4 *Chemicals of Concern for Risk Assessments:*

X1.4.1 It is not practicable to evaluate every compound present in a petroleum product to assess the human health or environmental risk from a spill of that product. For this reason, risk management decisions are generally based on assessing the potential impacts from a select group of "indicator" compounds. It is inherently assumed in this approach that a significant fraction of the total potential impact from all chemicals is due to the chemicals of concern. The selection of chemicals of concern is based on the consideration of exposure routes, concentrations, mobilities, toxicological properties, and aesthetic characteristics (taste, odor, and so forth). Historically, the relatively low toxicities and dissolved-phase mobilities of aliphatic hydrocarbons have made these chemicals of concern of less concern relative to aromatic hydrocarbons. When additives are present in significant quantities, consideration should also be given to including these as chemicals of concern.

X1.4.2 Table X1.3 identifies chemicals of concern most often considered when assessing impacts of petroleum products, based on knowledge of their concentration in the specific fuel, as well as their toxicity, water solubility, subsurface mobility, aesthetic characteristics, and the availability of sufficient information to conduct risk assessments. The chemicals of concern are identified by an "X" in the appropriate column.

X1.5 *Toxicity of Petroleum Hydrocarbons:*

X1.5.1 The following discussion gives a brief overview of origin of the toxicity parameters (reference doses (RfDs)), and slope factors (SFs), a justification for common choices of chemicals of concern and then, in X1.6, a brief summary of the toxicological, physical, and chemical parameters associated with these chemicals of concern.

X1.5.2 *How Toxicity Is Assessed: Individual Chemicals Versus Mixtures*—The toxicity of an individual chemical is typically established based on dose-response studies that estimate the relationship between different dose levels and the magnitude of their adverse effects (that is, toxicity). The dose-response data is used to identify a "safe dose" or a toxic level for a particular adverse effect. For a complex mixture of chemicals, the same approach can be used. For example, to evaluate the toxicity of gasoline, a "pure" reference gasoline would be evaluated instead of the individual chemical. This "whole-product" approach to toxicity assessment is strictly applicable only to mixtures identical to the evaluated mixture; gasolines with compositions different from the reference gasoline might have toxicities similar to the reference, but some differences would be expected. In addition, as the composition of gasoline released to the environment changes

through natural processes (volatilization, leaching, biodegradation), the toxicity of the remaining portion may change also.

X1.5.3 An alternative to the "whole-product" approach for assessing the toxicity of mixtures is the "individual-constituent" approach. In this approach, the toxicity of each individual constituent (or a selected subset of the few most toxic constituents, so-called chemicals of concern) is separately assessed and the toxicity of the mixture is assumed to be the sum of the individual toxicities using a hazard index approach. This approach is often used by the USEPA; however, it is inappropriate to sum hazard indices unless the toxicological endpoints and mechanisms of action are the same for the individual compounds. In addition, the compounds to be assessed must be carefully selected based on their concentrations in the mixture, their toxicities, how well their toxicities are known, and how mobile they are in the subsurface. Lack of sufficient toxicological information is often an impediment to this procedure.

X1.5.4 *Use of TPH Measurements in Risk Assessments*—Various chemical analysis methods commonly referred to as TPH are often used in site assessments. These methods usually determine the total amount of hydrocarbons present as a single number, and give no information on the types of hydrocarbon present. Such TPH methods may be useful for risk assessments where the whole product toxicity approach is appropriate. However in general, *TPH should not be used for "individual constituent" risk assessments because the general measure of TPH provides insufficient information about the amounts of individual compounds present.*

X1.5.5 *Toxicity Assessment Process*—Dose-response data are used to identify a "safe dose" or toxic level for a particular observed adverse effect. Observed adverse effects can include whole body effects (for example, weight loss, neurological observations), effects on specific body organs, including the central nervous system, teratogenic effects (defined by the ability to produce birth defects), mutagenic effects (defined by the ability to alter the genes of a cell), and carcinogenic effects (defined by the ability to produce malignant tumors in living tissues). Because of the great concern over risk agents which may produce incremental carcinogenic effects, the USEPA has developed weight-of-evidence criteria for determining whether a risk agent should be considered carcinogenic (see Table X1.2).

X1.5.6 Most estimates of a "safe dose" or toxic level are based on animal studies. In rare instances, human epidemiological information is available on a chemical. Toxicity studies can generally be broken into three categories based on the number of exposures to the risk agent and the length of time the study group was exposed to the risk agent. These studies can be described as follows:

X1.5.6.1 *Acute Studies*—Acute studies typically use one dose or multiple doses over a short time frame (24 h). Symptoms are usually observed within a short time frame and can vary from weight loss to death.

X1.5.6.2 *Chronic Studies*—Chronic studies use multiple exposures over an extended period of time, or a significant fraction of the animal's (typically two years) or the individual's lifetime. The chronic effects of major concern are carcinogenic, mutagenic, and teratogenic effects. Other chronic health effects such as liver and kidney damage are also important.

X1.5.6.3 *Subchronic Studies*—Subchronic studies use multiple or continuous exposures over an extended period (three months is the usual time frame in animal studies). Observed effects include those given for acute and chronic studies.

X1.5.6.4 Ideally, safe or acceptable doses are calculated from chronic studies, although, due to the frequent paucity of chronic data, subchronic studies are used.

X1.5.6.5 For noncarcinogens, safe doses are based on no observed adverse effect levels (NOAELs) or lowest observed adverse effect levels (LOAELs) from the studies.

X1.5.6.6 Acceptable doses for carcinogens are determined from mathematical models used to generate dose-response curves in the low-dose region from experimentally determined dose-response curves in the high-dose region.

X1.5.7 Data from the preceding studies are used to generate reference doses (RfDs), reference concentrations (RfCs), and slope factors (SFs) and are also used in generating drinking water maximum concentration levels (MCLs) and goals (MCLGs), health advisories (HAs), and water quality criteria. These terms are defined in Table X1.4 and further discussed in X3.6.

X1.5.8 *Selection of Chemicals of Concern*—The impact on human health and the environment in cases of gasoline and middle distillate contamination of soils and ground water can be assessed based on potential receptor (that is, aquatic organisms, human) exposure to three groups of materials: light aromatic hydrocarbons, PAHs, and in older spills, lead. Although not one of the primary contaminants previously described, EDB and EDC were used as lead scavengers in some leaded gasolines and may be considered chemicals of concern, when present.

X1.5.9 The light aromatics, benzene, toluene, xylenes, and ethylbenzene have relatively high water solubility and sorb poorly to soils. Thus, they have high mobility in the environment, moving readily through the subsurface. When released into surface bodies of water, these materials exhibit moderate to high acute toxicity to aquatic organisms. Although environmental media are rarely contaminated to the extent that acute human toxicity is an issue, benzene is listed by the USEPA as a Group A Carcinogen (known human carcinogen) and, thus, exposure to even trace levels of this material is considered significant.

TABLE X1.1 Generalized Chemical and Physical Characterization of Petroleum Products

	Predominant Carbon No. Range	Boiling Range, °C	Flash Point,[A] °C
Gasoline	C4 to C12	25 to 215	−40
Kerosene and Jet Fuels	C11 to C13	150 to 250	<21,[B] 21 to 55,[C] >55[D]
Diesel Fuel and Light Fuel Oils	C10 to C20	160 to 400	>35
Heavy Fuel Oils	C19 to C25	315 to 540	>50
Motor Oils and Other Lubricating Oils	C20 to C45	425 to 540	>175

[A] Typical values.
[B] Jet-B, AVTAG and JP-4.
[C] Kerosene, Jet A, Jet A-1, JP-8 and AVTUR.
[D] AVCAT and JP-5.

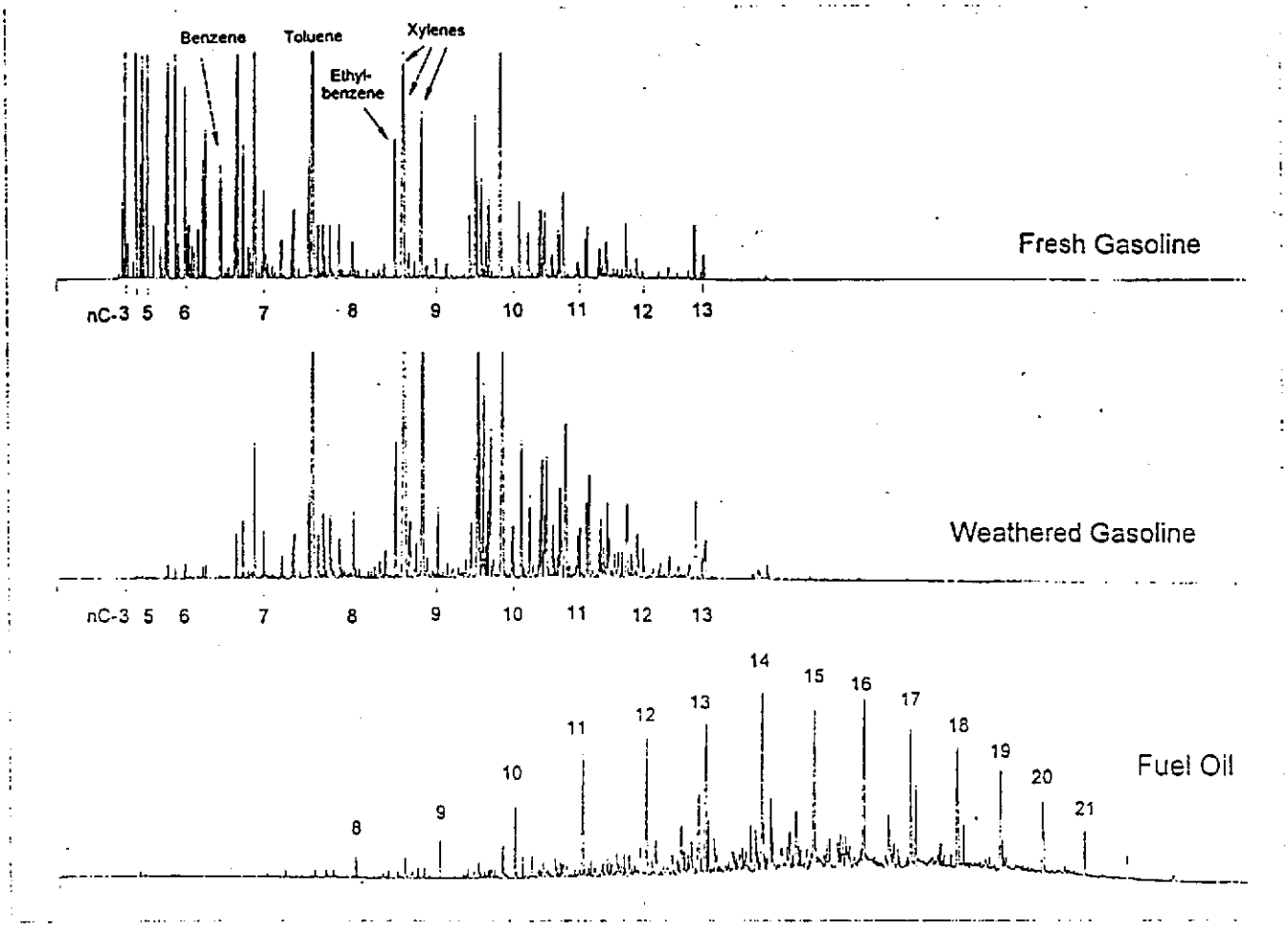


FIG. X1.1 Gas Chromatograms of Some Petroleum Fuels

X1.5.10 Polycyclic aromatics can be broken into two categories: naphthalenes and methylnaphthalenes (diaromatics) have moderate water solubility and soil sorption potential and, thus, their movement through the subsurface tends to be less than monoaromatics, but substantial movement can still occur. When released into surface bodies of water, these materials have moderate to high toxicity to aquatic organisms. The PAHs with three or more condensed rings have very low solubility (typically less than 1 mg/L) and sorb strongly to soils. Thus, their movement in the subsurface is minimal. Several members in the group of three to six-ring PAHs are known or suspected carcinogens and, thus, exposure to low concentrations in drinking water or through the consumption of contaminated soil by children is significant. In addition, materials containing four to six-ring PAHs are poorly biodegradable and, coupled with the potential to bioaccumulate in tissues of aquatic organisms, these materials have the potential to bioconcentrate (be found at levels in living tissue far higher than present in the general surroundings) in the environment.

X1.5.11 Although almost totally eliminated from use in gasolines in the United States, lead is found associated with older spills. Lead was typically added to gasoline either as tetraethyl or tetramethyl lead and may still be found in its original form in areas containing free product. Typically outside the free product zones, these materials have decomposed into inorganic forms of lead. Lead is a neurotoxin and lead in the blood of children has been associated with reduced intellectual development. The ingestion by children of lead-contaminated soils is an exposure route of great concern, as is the consumption of lead-contaminated drinking water. Ethylene dibromide and ethylene dichloride, used as lead scavengers in gasolines, are of concern because of their high toxicity (potential carcinogens) and their high mobility in the environment.

X1.5.12 In summary, benzene and benzo(a)pyrene (and in some cases EDB and EDC) are chemicals of concern because of their carcinogenicity. Other PAHs may also be grouped with B(a)P because of uncertainties in their carcinogenicity and because they may accumulate (bioconcentrate) in living tissue.

X1.5.13 *Toxicity and Physical/Chemical Properties for Chemicals of Concern*—A summary of health effects and physical/chemical properties for a number of chemicals of concern is provided in Table X1.2. This table provides toxicological data from a variety of sources, regardless of data quality. A refined discussion for selected chemicals of concern is given as follows. The reader is cautioned that this information is only current as of the dates quoted, and the sources quoted may have been updated, or more recent information may be available in the peer-reviewed literature.

TABLE X1.2 Chemical and Toxicological Properties of Selected Hydrocarbons

Compounds	Weight of Evidence Class[A]	Oral RfD, mg/kg-day	Inhalation RfC, mg/m³	Oral Slope Factor,[A] mg/kg-day⁻¹	Drinking Water MCL,[A] mg/L	Solubility,[B] mg/L	Octanol/Water Partition Coefficient,[B] log K_{ow}	Organic Carbon Adsorption Coefficient,[B] log K_{oc}
Benzene	A	[E]	[E,G]	0.029[G]	0.005	1750	2.13	1.58
Toluene	D	0.2[A]	0.4[A]	...	1	535	2.65	2.13
Ethylbenzene	D	0.1[A]	1[A]	...	0.7	152	3.13	1.98
Xylenes	D	2[A]	0.3[C,E]	...	10.0	198	3.26	2.38
n-Hexane	[E]	0.06[C], 0.6[D]	0.2[D]	...	...	13[L]	...	...
MTBE	...	[E]	3[A]	...	...	48 000[M]	1.06–1.30[N]	1.08[O]
MEK	D	0.6[A]	1[A]	...	[I]	268 000	0.26	0.65
MIBK	...	0.05[C], 0.5[D]	0.08[C,E], 0.8[D]	...	...	...	...	...
Methanol	...	0.5[A]	[E]	...	...	...	...	...
Ethanol	...	...	...	...	...	1 000 000	−0.032	0.34
TBA	...	...	...	...	...	...	...	...
Lead	B2	...	...	...	0.015[J]	...	...	...
EDC	B2	...	...	0.091	0.006	8 520	1.48	1.15
EDB	B2	...	[E]	85	0.00006	4 300	1.76	1.64
PNAs:								
Pyrene	D	0.03[A]	...	...	...	0.132	4.88	4.58
Benzo(a)pyrene	B2	...	...	7.3	0.0002[K]	0.00120	5.98	5.59
Anthracene	D	0.3[A]	...	...	...	0.0450	4.45	4.15
Phenanthrene	D	...	...	...	...	1.00	4.46	4.15
Naphthalene	D[E]	0.004[C], 0.04[D]	...	...	...	31.0[L]	3.28[L]	3.11[P]
Chrysene	B2	...	...	1.15[N]	0.0002	0.00180	5.61	5.30
Benzo(k)fluoranthene	B2	...	...	...	0.0002[K]	0.430	6.06	5.74
Fluorene	D	0.04[A]	...	...	...	1.69	4.20	3.86
Fluoranthene	D	0.04[A]	...	...	...	0.206	4.90	4.58
Benzo(g,h,i)perylene	D	...	...	...	...	0.000700	6.51	6.20
Benzo(b)fluoranthene	B2	...	...	...	0.0002[K]	0.0140	6.06	5.74
Benz(a)anthracene	B2	...	...	...	0.0002[K]	0.00670	5.60	6.14

[A] See Ref (2).
[B] See Ref (4).
[C] Chronic effect. See Ref (5).
[D] Subchronic effect. See Ref (5).
[E] The data is pending in the EPA-IRIS database.
[F] The data has been withdrawn in the EPA-IRIS database.
[G] The inhalation unit risk for benzene is 8.3×10^{-3} $(mg/m^3)^{-1}$. The drinking water unit is 8.3×10^{-4} (mg/L).
[H] See Ref (6). Health-based criteria for carcinogenic polycyclic aromatic compounds (PAHs) with the exception of dibenzo(a,h)anthracene are set at one tenth of the level of benzo(a)pyrene due to their recognized lesser potency.
[I] Listed in the January 1991 Drinking Water Priority List and may be subject to future regulation (56 FR 1470, 01/14/91).
[J] USEPA, May 1993, Office of Drinking Water. 15 µg/L is an action level; standard for tap water.
[K] Proposed standard.
[L] See Ref (7).
[M] See Ref (8).
[N] See Ref (9).
[O] Estimation Equation (from (10)):
(1) $\log K_{oc} = -0.55 \log S + 3.64$, where S = water solubility (mg/L)
(2) $\log K_{oc} = 0.544 \log P + 1.377$
[P] See Ref (11).

X1.5.13.1 The RfD or SF values are generally obtained from a standard set of reference tables (for example, Integrated Risk Information System, IRIS (2), or the Health Effects Assessment Summary Tables, HEAST (3)). Except as noted, the toxicity evaluations that follow were taken from IRIS (2) because these are EPA-sanctioned evaluations. The information in IRIS (2), however, has typically only been peer-reviewed within the EPA and may not always have support from the external scientific community. The information in IRIS may also be subject to error (as exampled by recent revisions in the slope factor for B(a)P and RfC for MTBE).

X1.5.13.2 HEAST (3) is a larger database than IRIS (2) and is often used as a source of health effects information. Whereas the information in IRIS (2) has been subject to data quality review, however, the information in the HEAST (3) tables has not. The user is expected to consult the original assessment documents to appreciate the strengths and limitations of the data in HEAST (3). Thus, care should be exercised in using the values in HEAST (3).

TABLE X1.3 Commonly Selected Chemicals of Concern for Petroleum Products

	Unleaded Gasoline	Leaded Gasoline	Kerosene/ Jet Fuels	Diesel/ Light Fuel Oils	Heavy Fuel Oils
Benzene	X	X	X	...	...
Toluene	X	X	X	...	...
Ethylbenzene	X	X	X	...	...
Xylene	X	X	X	...	...
MTBE, TBA, MEK, MIBK, methanol, ethanol	when suspected[A]	when suspected[A]	...	...	...
Lead, EDC, EDB	...	X	...	...	...
PNAs[B]	...	...	X	X	X

[A] For example, when these compounds may have been present in the spilled gasoline. These additives are not present in all gasolines.
[B] A list of selected PNAs for consideration is presented in Table X1.2.

X1.5.13.3 References for the physical/chemical properties

are provided in Table X1.2. All Henry's law constants quoted in text are from Ref (11) except MTBE which is from estimation: $H = (V_p)(MW)/760(S)$, where MW is the molecular weight, $V_p = 414$ mmHg at 100°F, and $S = 48\,000$ mg/L.

X1.6 *Profiles of Select Compounds:*

X1.6.1 *Benzene:*

X1.6.1.1 *Toxicity Summary*—Based on human epidemiological studies, benzene has been found to be a human carcinogen (classified as a Group A carcinogen, known human carcinogen by the USEPA). An oral slope factor of 2.9×10^{-2} (mg/kg/day)$^{-1}$ has been derived for benzene based on the observance of leukemia from occupational exposure by inhalation. The USEPA has set a drinking water maximum contaminant level (MCL) at 5 µg/L. The maximum contaminant level goal (MCLG) for benzene is set at zero.

X1.6.1.2 Although the EPA does not usually set long-term drinking water advisories for carcinogenic materials (no exposure to carcinogens is considered acceptable), a ten-day drinking water health advisory for a child has been set at 0.235 mg/L based on hematological impairment in animals. The EPA is in the process of evaluating noncancer effects and an oral RfD for benzene is pending.

X1.6.1.3 In situations in which both aquatic life and water are consumed from a particular body of water, a recommended EPA water quality criterion is set at 0.66 µg/L. When only aquatic organisms are consumed, the criterion is 40 µg/L. These criteria were established at the one-in-one-million risk level (that is, the criteria represent a one-in-one-million estimated incremental increase in cancer risk over a lifetime).

X1.6.1.4 *Physical/Chemical Parameter Summary*—Benzene is subject to rapid volatilization (Henry's law constant = 5.5×10^{-3} m^3-atm/mol) under common above-ground environmental conditions. Benzene will be mobile in soils due to its high water solubility (2.75×10^6 µg/L) and relatively low sorption to soil particles (log $K_{oc} = 1.92$) and, thus, has the potential to leach into ground water. Benzene has a relatively low log K_{ow} value (2.12) and is biodegradable. Therefore, it is not expected to bioaccumulate. In laboratory tests, when a free gasoline phase was in equilibrium with water, typical benzene concentrations in water ranged from 2.42×10^4 to 1.11×10^5 µg/L.

X1.6.2 *Toluene:*

X1.6.2.1 *Toxicity Summary*—Using data from animal studies, the USEPA has set an oral RfD for toluene at 0.2 mg/kg/day. In converting a NOAEL from an animal study, in which the critical effect observed was changes in liver and kidney weights, an uncertainty factor of 1000 and a modifying factor of 1 were used. The EPA has assigned an overall medium level of confidence in the RfD because, although the principal study was well performed, the length of the study corresponded to only subchronic rather than a chronic evaluation, and reproductive aspects were lacking. Based on the RfD and assuming 20 % exposure from drinking water, the EPA has set both drinking water MCL and MCLG of 1000 µg/L. Drinking water health advisories range from 1 mg/L (lifetime equivalent to the RfD) to 20 mg/L (one-day advisory for a child).

X1.6.2.2 In situations in which both aquatic life and water are consumed from a particular body of water, the recommended water quality criterion is set at 1.43×10^4 µg/L. When only aquatic organisms are consumed, the criterion is 4.24×10^5 µg/L.

X1.6.2.3 An inhalation RfC of 0.4 mg/m^3 was derived based on neurological effects observed in a small worker population. An uncertainty factor of 300 and a modifying factor of 1 were used to convert the lowest observed adverse effect level (LOAEL) to the RfC. The overall confidence in the RfC was established as medium because of the use of a LOAEL and because of the paucity of exposure information.

X1.6.2.4 *Physical/Chemical Parameter Summary*—Toluene is expected to volatilize rapidly, under common above-ground environmental conditions, due to its relatively high Henry's law constant (6.6×10^{-3} m^3-atm/mol). It will be mobile in soils based on an aqueous solubility of 5.35×10^5 µg/L and relatively poor sorption to soils (estimated log $K_{oc} = 2.48$) and, hence, has a potential to leach into ground water. Toluene has a relatively low log K_{ow} (2.73) and is biodegradable. Bioaccumulation of toluene is, therefore, expected to be negligible. In laboratory tests, when a free gasoline phase was in equilibrium with water, typical toluene concentrations in water ranged from 3.48×10^4 to 8.30×10^4 µg/L.

X1.6.3 *Xylenes:*

X1.6.3.1 *Toxicity Summary*—Using data from animal studies, the USEPA has set an oral RfD for xylenes at 2.0 mg/kg/day. In converting a NOAEL from the animal study, in which the critical effects observed were hyperactivity, decreased body weight, and increased mortality (among male rats), an uncertainty factor of 100 and a modifying factor of 1 were used. The EPA has assigned an overall medium level of confidence in the RfD because, although the principal study was well designed and performed, supporting chemistry was not performed. A medium level of confidence was also assigned to the database. Based on the RfD and assuming 20 % exposure from drinking water, the EPA has set both drinking water MCL and MCLG of 10 000 g/L. Drinking water health advisories of 10 mg/L (lifetime, adult) and 40 mg/L (one-day, ten-day, and long-term child) are quoted by the EPA's Office of Drinking Water. No USEPA ambient water criteria are available for xylenes at this time. Evaluation of an inhalation RfC is pending.

X1.6.3.2 *Physical/Chemical Parameter Summary*—Xylenes are expected to rapidly volatilize under common above-ground environmental conditions based on their Henry's law constants (for *o*-xylene, $H = 5.1 \times 10^{-3}$ m^3-atm/mol). Xylenes have a moderate water solubility (1.46 to 1.98 × 10^5 µg/L) (pure compound) as well as moderate capacities to sorb to soils (estimated log K_{oc} 2.38 to 2.79) and, therefore, they will be mobile in soils and may leach into ground water. Xylenes are biodegradable, and with log K_{ow} values in the range from 2.8 to 3.3, they are not expected to bioaccumulate.

X1.6.4 *Ethylbenzene:*

X1.6.4.1 *Toxicity Summary*—Using data from animal studies, the USEPA has set an oral RfD for ethylbenzene at 0.1 mg/kg/day. In converting a NOAEL from the animal study, in which the critical effects observed were liver and kidney toxicity, an uncertainty factor of 1000 and a modifying factor of 1 were used. The EPA has assigned an overall

TABLE X1.4 Weight of Evidence Criteria for Carcinogens

Category	Criterion
A	Human carcinogen, with sufficient evidence from epidemiological studies
B1	Probable human carcinogen, with limited evidence from epidemiological studies
B2	Probable human carcinogen, with sufficient evidence from animal studies and inadequate evidence or no data from epidemiological studies
C	Possible human carcinogen, with limited evidence from animal studies in the absence of human data
D	Not classifiable as to human carcinogenicity, owing to inadequate human and animal evidence
E	Evidence of noncarcinogenicity for humans, with no evidence of carcinogenicity in at least two adequate animal tests in different species, or in both adequate animal and epidemiological studies

low level of confidence in the RfD because the study was poorly designed and confidence in the supporting database is also low. Based on the RfD and assuming 20 % exposure from drinking water, the EPA has set both drinking water MCL and MCLG of 700 µg/L. Drinking water health advisories range from 700 µg/L (lifetime equivalent to the RfD) to 32 mg/L (one-day advisory for a child). In situations in which both aquatic life and water are consumed from a particular body of water, a recommended ambient water criterion is set at 1400 µg/L. When only aquatic organisms are consumed, the criterion is 3280 µg/L. An inhalation RfC of 1 mg/m^3 was derived based on developmental toxicity effects observed in rats and rabbits. An uncertainty factor of 300 and a modifying factor of 1 were used to convert the NOAEL to the RfC. Both the study design and database were rated low and, thus, the overall confidence in the RfC was established as low.

X1.6.4.2 *Physical/Chemical Parameter Summary*—Ethylbenzene has a relatively high Henry's law constant (8.7 × 10^{-3} m^3-atm/mol) and, therefore, can rapidly volatilize under common above-ground environmental conditions. Based on its moderate water solubility (1.52 × 10^5 µg/L) and moderate capacity to sorb to soils (estimated log K_{oc} = 3.04), it will have moderate mobility in soil and may leach into ground water. In laboratory tests, when a free gasoline phase was in equilibrium with water, typical combined ethylbenzene and xylenes concentrations in water ranged from 1.08 × 10^4 to 2.39 × 10^4 µg/L, due to partitioning effects. Ethylbenzene has a moderate low K_{ow} value (3.15) and is biodegradable. Therefore, it is not expected to bioaccumulate. In laboratory tests, when a free gasoline phase was in equilibrium with water, typical combined ethylbenzene and xylenes concentrations in water ranged from 1.08 × 10^4 to 2.39 × 10^4 µg/L.

X1.6.5 *Naphthalenes:*

X1.6.5.1 *Toxicity Summary*—In general, poisoning may occur by ingestion of large doses, inhalation, or skin adsorption of naphthalene. It can cause nausea, headache, diaphoresis, hematuria, fever, anemia, liver damage, vomiting, convulsions, and coma. Methylnaphthalenes are presumably less acutely toxic than naphthalene. Skin irritation and skin photosensitization are the only effects reported in man. Inhalation of the vapor may cause headache, confusion, nausea, and sometimes vomiting. The environmental concerns with naphthalenes are primarily attributed to effects on aquatic organisms. As a consequence, the EPA has not set any human health criteria for these materials (that is, there is no RfD or RfC, no drinking water MCL or MCLG or ambient water quality criteria). A risk assessment to define a RfD for these materials is presently under review by the EPA. Drinking water health advisories range from 20 µg/L (lifetime, adult) to 500 µg/L (one-day advisory for a child).[6]

X1.6.5.2 *Physical/Chemical Parameter Summary: Naphthalene*—Naphthalene has a relatively high Henry's law constant (1.15 × 10^{-3} m^3-atm/mol) and, thus, has the capacity to volatilize rapidly under common above-ground environmental conditions. It has a moderate water solubility (3.10 × 10^4 µg/L) and log K_{oc} (3.11) and has the potential to leach to ground water. A moderate log K_{ow} value of 3.01 has been reported, but because naphthalene is very biodegradable, it is unlikely to bioconcentrate to a significant degree.

X1.6.5.3 *Methylnaphthalenes*—Henry's law constants (2.60 × 10^{-4} m^3-atm/mol and 5.18 × 10^{-4} m^3-atm/mol for 1- and 2-methylnaphthalene, respectively) suggest that these materials have the potential to volatilize under common above-ground environmental conditions. 1-Methylnaphthalene exhibits a water solubility similar to naphthalene (2.60 × 10^4 µg/L to 2.8 × 10^4 µg/L). However, solubility decreases with increasing alkylation (dimethylnaphthalenes: 2.0 × 10^3 µg/L to 1.1 × 10^4 µg/L, 1,4,5-trimethylnaphthalene: 2.0 × 10^3 µg/L). These materials are, therefore, expected to be slightly mobile to relatively immobile in soil (for example, log K_{oc} is in the range from 2.86 to 3.93 for 1- and 2-methylnaphthalenes). In aquatic systems, methylnaphthalenes may partition from the water column to

[6] Office of Water, USEPA, Washington, DC.

TABLE X1.5 Definitions of Important Toxicological Characteristics

Reference Dose—A reference dose is an estimate (with an uncertainty typically spanning an order of magnitude) of a daily exposure (mg/kg/day) to the general human population (including sensitive subgroups) that is likely to be without an appreciable risk of deleterious effects during a lifetime of exposure.

Reference Concentration—A reference concentration is an estimate (with an uncertainty spanning perhaps an order of magnitude) of a continuous exposure to the human population (including sensitive subgroups) that is likely to be without appreciable deleterious effects during a lifetime.

Slope Factor—The slope of the dose-response curve in the low-dose region. When low-dose linearity cannot be assumed, the slope factor is the slope of the straight line from zero dose to the dose at 1 % excess risk. An upper bound on this slope is usually used instead of the slope itself. The units of the slope factor are usually expressed as (mg/kg/day)$^{-1}$.

Drinking Water MCLs and MCLGs—Maximum contaminant levels (MCLs) are drinking water standards established by the EPA that are protective of human health. However, these standards take into account the technological capability of attaining these standards. The EPA has, therefore, also established MCL goals (MCLGs) which are based only on the protection of human health. The MCL standards are often used as clean-up criteria.

Drinking Water Health Advisories—The Office of Drinking Water provides health advisories (HAs) as technical guidance for the protection of human health. They are not enforceable federal standards. The HA's are the concentration of a substance in drinking water estimated to have negligible deleterious effects in humans, when ingested for specified time periods.

Water Quality Criteria—These criteria are not rules and they do not have regulatory impact. Rather, these criteria present scientific data and guidance of the environmental effects of pollutants which can be useful to derive regulatory requirements based on considerations of water quality impacts.

organic matter contained in sediments and suspended solids. Methylnaphthalenes have high log K_{ow} values (greater than 3.5) and have the potential to bioaccumulate. They do, however, exhibit a moderate degree of biodegradation, which typically decreases with increased alkylation.

X1.6.6 *Three to Six-Ringed PAHs*—The most significant health effect for this class of compounds is their carcinogenicity, which is structure-dependent. Anthracene and phenanthrene have not been shown to cause cancer in laboratory animals. The available data does not prove pyrene to be carcinogenic to experimental animals. On the other hand, benz[a]-anthracene, benzo[a]pyrene, dibenz[a,h]anthracene, and 7,12-dimethylbenz[a]-anthracene have been shown to be carcinogenic in laboratory animals. B(a)P and pyrene are discussed in X1.6.7 and X1.6.8 as representatives of carcinogenic and noncarcinogenic effects of this class.

X1.6.7 *Benzo(a)pyrene (BaP):*

X1.6.7.1 *Toxicity Summary*—Based on animal data, B(a)P has been classified as a probable human carcinogen (B2 carcinogen) by the USEPA. A range of oral slope factors from 4.5 to 11.7 $(mg/kg/day)^{-1}$ with a geometric mean of 7.3 $(mg/kg/day)^{-1}$ has been derived for B(a)P based on the observance of tumors of the forestomach and squamous cell carcinomas in mice. The data was considered less than optimal but acceptable (note that the carcinogenicity assessment for B(a)P may change in the near future pending the outcome of an on-going EPA review). The EPA has proposed a drinking water MCL at 0.2 µg/L (based on the analytical detection limits). The MCLG for B(a)P is set at zero. In situations in which both aquatic life and water are consumed from a particular body of water, a recommended EPA water quality criterion is set at 2.8×10^{-3} µg/L. When only aquatic organisms are consumed, the criterion is 3.11×10^{-2} µg/L.

X1.6.7.2 *Physical/Chemical Parameter Summary*—When released to water, PAHs are not subject to rapid volatilization (Henry's law constants are on the order of 1.0×10^{-4} m^3-atm/mol or less) under common environmental conditions. They have low aqueous solubility values and tend to sorb to soils and sediments and remain fixed in the environment. Three ring members of this group such as anthracene and phenanthrene have water solubilities on the order of 1000 µg/L. The water solubilities decrease substantially for larger molecules in the group, for example, benzo[a]pyrene has a water solubility of 1.2 µg/L. The log K_{ow} values for PAHs are on the order of 4.3 and greater, which suggests that PAHs will be expected to adsorb very strongly to soil. The PAHs with more than three rings generally have high log K_{ow} values (6.06 for benzo[a]pyrene), have poor biodegradability characteristics and may bioaccumulate.

X1.6.8 *Pyrene:*

X1.6.8.1 *Toxicity Summary*—Using data from animal studies, the USEPA has set an oral RfD for pyrene at 3×10^{-2} mg/kg/day. In converting a NOAEL from the animal study, in which the critical effects observed were kidney toxicity, an uncertainty factor of 3000 and a modifying factor of 1 were used. The EPA has assigned an overall low level of confidence in the RfD because although the study was well-designed, confidence in the supporting database is low. No drinking water MCLs or health advisories have been set. In situations in which both aquatic life and water are consumed from a particular body of water, a recommended EPA water quality criterion is set at 2.8×10^{-3} µg/L. When only aquatic organisms are consumed, the criterion is 3.11×10^{-2} µg/L.

X1.6.8.2 *Physical/Chemical Parameter Summary*—Refer to X1.6.7.2 for BaP. Also see Table X1.2.

X1.6.9 *MTBE:*

X1.6.9.1 *Toxicity Summary*—Using data from animal studies, the USEPA has set an inhalation RfC for MTBE at 3 mg/m^3. In converting a NOAEL from the animal study, in which the critical effects observed included increased liver and kidney weight and increased severity of spontaneous renal lesions (females), increased prostration (females) and swollen pericolar tissue, an uncertainty factor of 100 and a modifying factor of 1 were used. The EPA has assigned an overall medium level of confidence in the RfC because although the study was well-designed, some information on the chemistry was lacking. The confidence in the supporting database is medium to high. No drinking water MCLs or ambient water quality criteria have been set. However, a risk assessment, which may define a RfD for this material, is presently under review by EPA. Drinking water health advisories range from 40 µg/L (lifetime, adult) to 3000 µg/L (one-day advisory for a child).[6]

X1.6.9.2 *Physical/Chemical Parameter Summary*—The Henry's law constant for MTBE is estimated to be approximately 1.0×10^{-3} m^3-atm/mol. It is, therefore, expected to have the potential to rapidly volatilize under common above-ground environmental conditions. It is very water soluble (water solubility is 4.8×10^7 µg/L), and with a relatively low capacity to sorb to soils (estimated log K_{ow} = 1.08), MTBE will migrate at the same velocity as the water in which it is dissolved in the subsurface. The log K_{ow} value has been estimated to be between 1.06 and 1.30, indicating MTBE's low bioaccumulative potential. It is expected to have a low potential to biodegrade, but no definitive studies are available.

X1.6.10 *Lead:*

X1.6.10.1 *Toxicity Summary—(The following discussion is for inorganic lead—not the organic forms of lead (tetraethyllead, tetramethyllead) that were present in petroleum products.)* A significant amount of toxicological information is available on the health effects of lead. Lead produces neurotoxic and behavioral effects particularly in children. However, the EPA believes that it is inappropriate to set an RfD for lead and its inorganic compounds because the agency believes that some of the effects may occur at such low concentrations as to suggest no threshold. The EPA has also determined that lead is a probable human carcinogen (classified as B2). The agency has chosen not to set a numeric slope factor at this time, however, because it is believed that standard procedures for doing so may not be appropriate for lead. At present, the EPA has set an MCLG of zero but has set no drinking water (MCL) or health advisories because of the observance of low-level effects, the overall Agency goal of reducing total lead exposure and because of its classification as a B2 carcinogen. An action of level of 15 µg/L has been set for water distribution systems (standard at the tap). The recommended EPA water quality criterion for consumption of both aquatic life and water is set at 50 µg/L.

X1.6.10.2 *Physical/Chemical Parameter Summary*—Organic lead additive compounds are volatile (estimated Henry's law constant for tetraethyl lead = 7.98×10^{-2} m^3-atm/mol) and may also sorb to particulate matter in the air. Tetraethyl lead has an aqueous solubility of 800 µg/L and an estimated log K_{ow} of 3.69 and, therefore, should not be very mobile in the soil. It decomposes to inorganic lead in dilute aqueous solutions and in contact with other environmental media. In free product (gasoline) plumes, however, it may remain unchanged. Inorganic lead compounds tightly bind to most soils with minimal leaching under natural conditions. Aqueous solubility varies depending on the species involved. The soil's capacity to sorb lead is correlated with soil pH, cation exchange capacity, and organic matter. Lead does not appear to bioconcentrate significantly in fish but does in some shellfish, such as mussels. Lead is not biodegradable.

X1.7 *Discussion of Acceptable Risk* (12)—Beginning in the late 1970s and early 1980s, regulatory agencies in the United States and abroad frequently adopted a cancer risk criteria of one-in-one-million as a negligible (that is, of no concern) risk when fairly large populations might be exposed to a suspect carcinogen. Unfortunately, theoretical increased cancer risks of one-in-one-million are often incorrectly portrayed as serious public health risks. As recently discussed by Dr. Frank Young (13), the current commissioner of the Food and Drug Administration (FDA), this was not the intent of such estimates:

X1.7.1 In applying the de minimis concept and in setting other safety standards, the FDA has been guided by the figure of "one-in-one-million." Other Federal agencies have also used a one-in-one-million increased risk over a lifetime as a reasonable criterion for separating high-risk problems warranting agency attention from negligible risk problems that do not.

X1.7.2 The risk level of one-in-one-million is often misunderstood by the public and the media. It is not an actual risk, that is, we do not expect one out of every million people to get cancer if they drink decaffeinated coffee. Rather, it is a mathematical risk based on scientific assumptions used in risk assessment. The FDA uses a conservative estimate to ensure that the risk is not understated. We interpret animal test results conservatively, and we are extremely careful when we extrapolate risks to humans. When the FDA uses the risk level of one-in-one-million, it is confident that the risk to humans is virtually nonexistent.

X1.7.3 In short, a "one-in-one-million" cancer risk estimate, which is often tacitly assumed by some policy-makers to represent a trigger level for regulatory action, actually represents a level of risk that is so small as to be of negligible concern.

X1.7.4 Another misperception within the risk assessment arena is that all occupational and environmental regulations have as their goal a theoretical maximum cancer risk of 1 in 1 000 000. Travis, et al (14) recently conducted a retrospective examination of the level of risk that triggered regulatory action in 132 decisions. Three variables were considered: (*1*) individual risk (an upper-bound estimate of the probability at the highest exposure), (*2*) population risk (an upper-limit estimate of the number of additional incidences of cancer in the exposed population), and (*3*) population size. The findings of Travis, et al (14) can be summarized as follows:

X1.7.4.1 Every chemical with an individual lifetime risk above 4×10^{-3} received regulation. Those with values below 1×10^{-6} remained unregulated.

X1.7.4.2 For small populations, regulatory action never resulted for individual risks below 1×10^{-4}.

X1.7.4.3 For potential effects resulting from exposures to the entire United States population, a risk level below 1×10^{-6} never triggered action; above 3×10^{-4} always triggered action.

X1.7.5 Rodricks, et al (15) also evaluated regulatory decisions and reached similar conclusions. In decisions relating to promulgation of National Emission Standards for Hazardous Air Pollutants (NESHAPS), the USEPA has found the maximum individual risks and total population risks from a number of radionuclide and benzene sources too low to be judged significant. Maximum individual risks were in the range from 3.6×10^{-5} to 1.0×10^{-3}. In view of the risks deemed insignificant by USEPA, Rodricks, et al (15) noted that 1×10^{-5} (1 in 100 000) appears to be in the range of what USEPA might consider an insignificant average lifetime risk, at least where aggregate population risk is no greater than a fraction of a cancer yearly.

X1.7.6 Recently, final revisions to the National Contingency Plan (16) have set the acceptable risk range between 10^{-4} and 10^{-6} at hazardous waste sites regulated under CERCLA. In the recently promulgated *Hazardous Waste Management System Toxicity Characteristics Revisions* (17), the USEPA has stated that:

> "For drinking water contaminants, EPA sets a reference risk range for carcinogens at 10^{-6} excess individual cancer risk from lifetime exposure. Most regulatory actions in a variety of EPA programs have generally targeted this range using conservative models which are not likely to underestimate the risk."

X1.7.7 Interestingly, the USEPA has selected and promulgated a single risk level of 1 in 100 000 (1×10^{-5}) in the *Hazardous Waste Management System Toxicity Characteristics Revisions* (17). In their justification, the USEPA cited the following rationale:

> The chosen risk level of 10^{-5} is at the midpoint of the reference risk range for carcinogens (10^{-4} to 10^{-6}) generally used to evaluate CERCLA actions. Furthermore, by setting the risk level at 10^{-5} for TC carcinogens, EPA believes that this is the highest risk level that is likely to be experienced, and most if not all risks will be below this level due to the generally conservative nature of the exposure scenario and the underlying health criteria. For these reasons, the Agency regards a 10^{-5} risk level for Group A, B, and C carcinogens as adequate to delineate, under the Toxicity Characteristics, wastes that clearly pose a hazard when mismanaged."

X1.7.8 When considering these limits it is interesting to note that many common human activities entail annual risks greatly in excess of one-in-one-million. These have been discussed by Grover Wrenn, former director of Federal Compliance and State Programs at OSHA, as follows:

X1.7.9 State regulatory agencies have not uniformly adopted a one-in-one-million (1×10^{-6}) risk criterion in making environmental and occupational decisions. The states of Virginia, Maryland, Minnesota, Ohio, and Wisconsin have employed or proposed to use the one-in-one-hundred-thousand (1×10^{-5}) level of risk in their risk management decisions (18). The State of Maine Department of Human Services (DHS) uses a lifetime risk of one in one

hundred thousand as a reference for non-threshold (carcinogenic) effects in its risk management decisions regarding exposures to environmental contaminants (19). Similarly, a lifetime incremental cancer risk of one in one hundred thousand is used by the Commonwealth of Massachusetts as a cancer risk limit for exposures to substances in more than one medium at hazardous waste disposal sites (20). This risk limit represents the total cancer risk at the site associated with exposure to multiple chemicals in all contaminated media. The State of California has also established a level of risk of one in one hundred thousand for use in determining levels of chemicals and exposures that pose no significant risks of cancer under the Safe Drinking Water and Toxic Enforcement Act of 1986 (Proposition 65) (21). Workplace air standards developed by the Occupational Safety and Health Administration (OSHA) typically reflect theoretical risks of one in one thousand (1×10^{-3}) or greater (15).

X1.7.10 Ultimately, the selection of an acceptable and de minimis risk level is a policy decision in which both costs and benefits of anticipated courses of action should be thoroughly evaluated. However, actuarial data and risk estimates of common human activities, regulatory precedents, and the relationship between the magnitude and variance of background and incremental risk estimates all provide compelling support for the adoption of the de minimis risk level of 1×10^{-5} for regulatory purposes.

X1.7.11 In summary, U.S. Federal and state regulatory agencies have adopted a one-in-one-million cancer risk as being of negligible concern in situations where large populations (for example, 200 million people) are involuntarily exposed to suspect carcinogens (for example, food additives). When smaller populations are exposed (for example, in occupational settings), theoretical cancer risks of up to 10^{-4} (1 in 10 000) have been considered acceptable.

X2. DEVELOPMENT OF RISK-BASED SCREENING LEVELS (RBSLs) APPEARING IN SAMPLE LOOK-UP TABLE X2.1

X2.1 *Introduction:*

X2.1.1 This appendix contains the equations and parameters used to construct the example "Look-Up" (Table X2.1). This table was prepared solely for the purpose of presenting an example Tier 1 matrix of RBSLs, and these values should not be viewed, or misused, as proposed remediation "standards." The reader should note that not all possible pathways have been considered and a number of assumptions concerning exposure scenarios and parameter values have been made. These should be reviewed for appropriateness before using the listed RBSLs as Tier 1 screening values.

X2.1.2 The approaches used to calculate RBSLs appearing in Table X2.1 are briefly discussed as follows for exposure to vapors, ground water, surficial soils, and subsurface soils by means of the following pathways:

X2.1.2.1 Inhalation of vapors,

X2.1.2.2 Ingestion of ground water,

X2.1.2.3 Inhalation of outdoor vapors originating from dissolved hydrocarbons in ground water,

X2.1.2.4 Inhalation of indoor vapors originating from dissolved hydrocarbons in ground water,

X2.1.2.5 Ingestion of surficial soil, inhalation of outdoor vapors and particulates emanating from surficial soils, and dermal absorption resulting from surficial soil contact with skin,

X2.1.2.6 Inhalation of outdoor vapors originating from hydrocarbons in subsurface soils,

X2.1.2.7 Inhalation of indoor vapors originating from subsurface hydrocarbons, and

X2.1.2.8 Ingestion of ground water impacted by leaching of dissolved hydrocarbons from subsurface soils.

X2.1.3 For the pathways considered, approaches used in this appendix are consistent with guidelines contained in Ref (26).

X2.1.4 The development presented as follows focuses only on human-health RBSLs for chronic (long-term) exposures.

X2.1.4.1 In the case of compounds that have been classified as carcinogens, the RBSLs are based on the general equation:

$$\textit{risk} = \textit{average lifetime intake}\ [\text{mg/kg-day}] \times \textit{potency factor}\ [\text{mg/kg-day}]^{-1}$$

where the intake depends on exposure parameters (ingestion rate, exposure duration, and so forth), the source concentration, and transport rates between the source and receptor. The potency factor is selected after reviewing a number of sources, including the USEPA Integrated Risk Information System (IRIS) (2) database, USEPA Health Effects Assessment Summary Tables (HEAST) (3), and peer-reviewed sources. The RBSL values appearing in Table X2.1 correspond to probabilities of adverse health effects ("risks") in the range from 10^{-6} to 10^{-4} resulting from the specified exposure. Note that this risk value does not reflect the probability for the specified exposure scenario to occur. Therefore, the actual potential risk to a population for these RBSLs is lower than the 10^{-6} to 10^{-4} range.

X2.1.4.2 In the case of compounds that have not been classified as carcinogens, the RBSLs are based on the general equation:

$$\textit{hazard quotient} = \textit{average intake}\ [\text{mg/kg-day}] / \textit{reference dose}\ [\text{mg/kg-day}]$$

where the intake depends on exposure parameters (ingestion rate, exposure duration, and so forth), the source concentration, and transport rates between the source and receptor. The reference dose is selected after reviewing a number of sources, including the USEPA Integrated Risk Information System (IRIS) (2) database, USEPA Health Effects Assessment Summary Tables (HEAST) (3), and peer-reviewed sources. The RBSL values appearing in Table X2.1 correspond to hazard quotients of unity resulting from the specified exposure. Note that this hazard quotient value does not reflect the probability for the specified exposure scenario to occur. Therefore, the actual potential impact to a population for these RBSLs is lower than a hazard quotient of unity.

X2.1.5 Tables X2.2 through X2.7 summarize the equa-

TABLE X2.1 Example Tier 1 Risk-Based Screening Level (RBSL) Look-up Table[A]

NOTE—This table is presented here only as an example set of Tier 1 RBSLs. It is not a list of proposed standards. The user should review all assumptions prior to using any values. Appendix X2 describes the basis of these values.

Exposure Pathway	Receptor Scenario	Target Level	Benzene	Ethylbenzene	Toluene	Xylenes (Mixed)	Napthalenes	Benzo (a)pyrene
Air								
Indoor air screening levels for inhalation exposure, $\mu g/m^3$	residential	cancer risk = 1E-06	3.92E-01					1.86E-03
		cancer risk = 1E-04	3.92E+01					1.86E-01
		chronic HQ = 1		1.39E+03	5.56E+02	9.73E+03	1.95E+01	
	commercial/ industrial	cancer risk = 1E-06	4.93E-01					2.35E-03
		cancer risk = 1E-04	4.93E+01					2.35E-01
		chronic HQ = 1		1.46E+03	5.84E+02	1.02E+04	2.04E+01	
Outdoor air screening levels for inhalation exposure, $\mu g/m^3$	residential	cancer risk = 1E-06	2.94E-01					1.40E-03
		cancer risk = 1E-04	2.94E+01					1.40E-01
		chronic HQ = 1		1.04E+03	4.17E+02	7.30E+03	1.46E+01	
	commercial/ industrial	cancer risk = 1E-06	4.93E-01					2.35E-03
		cancer risk = 1E-04	4.93E+01					2.35E-01
		chronic HQ = 1		1.46E+03	5.84E+02	1.02E+04	2.04E+01	
OSHA TWA PEL, $\mu g/m^3$			3.20E+03	4.35E+05	7.53E+05	4.35E+06	5.00E+04	2.00E+02[A]
Mean odor detection threshold, $\mu g/m^3$ [B]			1.95E+05		6.00E+03	8.70E+04	2.00E+02	
National indoor background concentration range, $\mu g/m^3$ [C]			3.25E+00 to 2.15E+01	2.20E+00 to 9.70E+00	9.60E-01 to 2.91E+01	4.85E+00 to 4.76E+01		
Soil								
Soil volatilization to outdoor air, mg/kg	residential	cancer risk = 1E-06	2.72E-01					RES[D]
		cancer risk = 1E-04	2.73E+01					RES
		chronic HQ = 1		RES	RES	RES	RES	
	commercial industrial	cancer risk = 1E-06	4.57E-01					RES
		cancer risk = 1E-04	4.57E+01					RES
		chronic HQ = 1		RES	RES	RES	RES	
Soil-vapor intrusion from soil to buildings, mg/kg	residential	cancer risk = 1E-06	5.37E-03					RES
		cancer risk = 1E-04	5.37E-01					RES
		chronic HQ = 1		4.27E+02	2.06E+01	RES	4.07E+01	
	commercial/ industrial	cancer risk = 1E-06	1.09E-02					RES
		cancer risk = 1E-04	1.09E+00					RES
		chronic HQ = 1		1.10E+03	5.45E+01	RES	1.07E+02	
Surficial soil (0 to 3 ft) (0 to 0.9 m) ingestion/ dermal/ inhalation, mg/kg	residential	cancer risk = 1E-06	5.82E+00					1.30E-01
		cancer risk = 1E-04	5.82E+02					1.30E+01
		chronic HQ = 1		7.83E+03	1.33E+04	1.45E+06	9.77E+02	
	commercial/ industrial	cancer risk = 1E-06	1.00E+01					3.04E-01
		cancer risk = 1E-04	1.00E+03					3.04E+01
		chronic HQ = 1		1.15E+04	1.87E+04	2.06E+05	1.90E+03	
Soil-leachate to protect ground water ingestion target level, mg/kg		MCLs	2.93E-02	1.10E+02	1.77E+01	3.05E+02	N/A	9.42E+00
	residential	cancer risk = 1E-06	1.72E-02					5.90E-01
		cancer risk = 1E-04	1.72E+00					RES
		chronic HQ = 1		5.75E+02	1.29E+02	RES	2.29E+01	
	commercial/ industrial	cancer risk = 1E-06	5.78E-02					1.85E+00
		cancer risk = 1E-04	5.78E+00					RES
		chronic HQ = 1		1.61E+03	3.61E+02	RES	6.42E+01	
Ground Water								
Ground water volatilization to outdoor air, mg/L	residential	cancer risk = 1E-06	1.10E+01					>S[E]
		cancer risk = 1E-04	1.10E+03					>S
		chronic HQ = 1		>S	>S	>S	>S	
	commercial/ industrial	cancer risk = 1E-06	1.84E+01					>S
		cancer risk = 1E-04	>S					>S
		chronic HQ = 1		>S	>S	>S	>S	
Ground water ingestion, mg/L		MCLs	5.00E-03	7.00E-01	1.00E+00	1.00E+01	N/A	2.00E-04
	residential	cancer risk = 1E-06	2.94E-03					1.17E-05
		cancer risk = 1E-04	2.94E-01					1.17E-03
		chronic HQ = 1		3.65E+00	7.30E+00	7.30E+01	1.46E-01	
	commercial/ industrial	cancer risk = 1E-06	9.87E-03					3.92E-05
		cancer risk = 1E-04	9.87E-01					>S
		chronic HQ = 1		1.02E+01	2.04E+01	>S	4.09E-01	
Ground water—vapor intrusion from ground water to buildings, mg/L	residential	cancer risk = 1E-06	2.38E-02					>S
		cancer risk = 1E-04	2.38E+00					>S
		chronic HQ = 1		7.75E+01	3.28E+01	>S	4.74E+00	
	commercial/ industrial	cancer risk = 1E-06	7.39E-02					>S
		cancer risk = 1E-04	7.39E+00					>S
		chronic HQ = 1		>S	6.50E+01	>S	1.23E+01	

[A] As benzene soluble coal tar pitch volatiles.
[B] See Ref (22).
[C] See Refs (23-25).
[D] RES—Selected risk level is not exceeded for pure compound present at any concentration.
[E] >S—Selected risk level is not exceeded for all possible dissolved levels (≤ pure component solubility).

tions and parameters used to prepare the example look-up Table X2.1. The basis for each of these equations is discussed in X2.2 through X2.10.

X2.2 *Air—Inhalation of Vapors (Outdoors/Indoors)*—In this case chemical intake results from the inhalation of vapors. It is assumed that vapor concentrations remain constant over the duration of exposure, and all inhaled chemicals are absorbed. Equations appearing in Tables X2.2 and X2.3 for estimating RBSLs for vapor concentrations in the breathing zone follow guidance given in Ref (26). Should the calculated RBSL exceed the saturated vapor concentration for any individual component, "$>P_{vap}$" is entered in the table to indicate that the selected risk level or hazard quotient cannot be reached or exceeded for that compound and the specified exposure scenario.

X2.3 *Ground Water—Ingestion of Ground Water*—In this case chemical intake results from ingestion of ground water. It is assumed that the dissolved hydrocarbon concentrations remain constant over the duration of exposure. Equations appearing in Tables X2.2 and X2.3 for estimating RBSLs for drinking water concentrations follow guidance given in Ref (26) for ingestion of chemicals in drinking water. Should the calculated RBSL exceed the pure component solubility for any individual component, ">S" is entered in the table to indicate that the selected risk level or hazard quotient cannot be reached or exceeded for that compound and the specified exposure scenario (unless free-phase product is mixed with the ingested water).

TABLE X2.2 Equations Used to Develop Example Tier 1 Risk-Based Screening Level (RBSLs) Appearing in "Look-Up" Table X2.1—Carcinagenic Effects[A]

NOTE—See Tables X2.4 through X2.7 for definition of parameters.

Medium	Exposure Route	Risk-Based Screening Level (RBSL)
Air	inhalation[B]	$RBSL_{air}\left[\frac{\mu g}{m^3\text{-}air}\right] = \frac{TR \times BW \times AT_c \times 365\frac{days}{years} \times 10^3\frac{\mu g}{mg}}{SF_i \times IR_{air} \times EF \times ED}$
Ground water	ingestion (potable ground water supply only)[B]	$RBSL_w\left[\frac{mg}{L\text{-}H_2O}\right] = \frac{TR \times BW \times AT_c \times 365\frac{days}{years}}{SF_o \times IR_w \times EF \times ED}$
Ground water[C]	enclosed-space (indoor) vapor inhalation[D]	$RBSL_w\left[\frac{mg}{L\text{-}H_2O}\right] = \frac{RBSL_{air}\left[\frac{\mu g}{m^3\text{-}air}\right]}{VF_{wesp}} \times 10^{-3}\frac{mg}{\mu g}$
Ground water[C]	ambient (outdoor) vapor inhalation[D]	$RBSL_w\left[\frac{mg}{L\text{-}H_2O}\right] = \frac{RBSL_{air}\left[\frac{\mu g}{m^3\text{-}air}\right]}{VF_{wamb}} \times 10^{-3}\frac{mg}{\mu g}$
Surficial soil	ingestion of soil, inhalation of vapors and particulates, and dermal contact[B]	$RBSL_s\left[\frac{\mu g}{kg\text{-}soil}\right] = \frac{TR \times BW \times AT_c \times 365\frac{days}{years}}{EF \times ED\left[\left(SF_o \times 10^{-6}\frac{kg}{mg} \times (IR_{soil} \times RAF_o + SA \times M \times RAF_d)\right) + (SF_i \times IR_{air} \times (VF_{ss} + VF_{pi}))\right]}$ For surficial and excavated soils (0 to 1 m)
Subsurface soil[C]	ambient (outdoor) vapor inhalation[D]	$RBSL_s\left[\frac{mg}{kg\text{-}soil}\right] = \frac{RBSL_{air}\left[\frac{\mu g}{m^3\text{-}air}\right]}{VF_{samb}} \times 10^{-3}\frac{mg}{\mu g}$
Subsurface soil[C]	enclosed space (indoor) vapor inhalation[D]	$RBSL_s\left[\frac{mg}{kg\text{-}soil}\right] = \frac{RBSL_{air}\left[\frac{\mu g}{m^3\text{-}air}\right]}{VF_{sesp}} \times 10^{-3}\frac{mg}{\mu g}$
Subsurface soil[C]	leaching to ground water[D]	$RBSL_s\left[\frac{mg}{kg\text{-}soil}\right] = \frac{RBSL_w\left[\frac{mg}{L\text{-}H_2O}\right]}{LF_{sw}}$

[A] Note that all RBSL values should be compared with thermodynamic partitioning limits, such as solubility levels, maximum vapor concentrations, and so forth. If a RBSL exceeds the relevant partitioning limit, this is an indication that the selected risk or hazard level will never be reached or exceeded for that chemical and the selected exposure scenario.

[B] Screening levels for these media based on other considerations (for example, aesthetic, background levels, environmental resource protection, and so forth) can be derived with these equations by substituting the selected target level for $RBSL_{air}$ or $RBSL_w$ appearing in these equations.

[C] These equations are based on Ref (26).

[D] These equations simply define the "cross-media partitioning factors," VF_i and LF_{sw}.

TABLE X2.3 Equations Used to Develop Example Tier 1 Risk-Based Screening Level (RBSLs) Appearing in "Look-Up" Table X2.1—Noncarcinogenic Effects[A]

NOTE—See Tables X2.4 through X2.7 for definition of parameters.

Medium	Exposure Route	Risk-Based Screening Level (RBSL)
Air	inhalation[B]	$RBSL_{air}\left[\frac{\mu g}{m^3\text{-}air}\right] = \frac{THQ \times RfD_i \times BW \times AT_n \times 365\ \frac{days}{years} \times 10^3\ \frac{\mu g}{mg}}{IR_{air} \times EF \times ED}$
Ground water	ingestion (potable ground water supply only)[B]	$RBSL_w\left[\frac{mg}{L\text{-}H_2O}\right] = \frac{THQ \times RfD_o \times BW \times AT_n \times 365\ \frac{days}{years}}{IR_w \times EF \times ED}$
Ground water[C]	enclosed-space (indoor) vapor inhalation[D]	$RBSL_w\left[\frac{mg}{L\text{-}H_2O}\right] = \frac{RBSL_{air}\left[\frac{\mu g}{m^3\text{-}air}\right]}{VF_{wesp}} \times 10^{-3}\ \frac{mg}{\mu g}$
Ground water[C]	ambient (outdoor) vapor inhalation[D]	$RBSL_w\left[\frac{mg}{L\text{-}H_2O}\right] = \frac{RBSL_{air}\left[\frac{\mu g}{m^3\text{-}air}\right]}{VF_{wamb}} \times 10^{-3}\ \frac{mg}{\mu g}$
Surficial soil	ingestion of soil, inhalation of vapors and particulates, and dermal contact[B]	$RBSL_s\left[\frac{\mu g}{kg\text{-}soil}\right] = \frac{THQ \times BW \times AT_n \times 365\ \frac{days}{years}}{EF \times ED\left[\frac{\left(10^{-6}\ \frac{kg}{mg} \times (IR_{soil} \times RAF_o + SA \times M \times RAF_d)\right)}{RfD_o} + \frac{(IR_{air} \times (VF_{ss} + VF_{ps}))}{RfD_i}\right]}$ For surficial and excavated soils (0 to 1 m)
Subsurface soil[C]	ambient (outdoor) vapor inhalation[D]	$RBSL_s\left[\frac{mg}{kg\text{-}soil}\right] = \frac{RBSL_{air}\left[\frac{\mu g}{m^3\text{-}air}\right]}{VF_{samb}} \times 10^{-3}\ \frac{mg}{\mu g}$
Subsurface soil[C]	enclosed space (indoor) vapor inhalation[D]	$RBSL_s\left[\frac{mg}{kg\text{-}soil}\right] = \frac{RBSL_{air}\left[\frac{\mu g}{m^3\text{-}air}\right]}{VF_{sesp}} \times 10^{-3}\ \frac{mg}{\mu g}$
Subsurface soil[C]	leaching to ground water[D]	$RBSL_s\left[\frac{mg}{kg\text{-}soil}\right] = \frac{RBSL_w\left[\frac{mg}{L\text{-}H_2O}\right]}{LF_{sw}}$

[A] Note that all RBSL values should be compared with thermodynamic partitioning limits, such as solubility levels, maximum vapor concentrations, and so forth. If a RBSL exceeds the relevant partitioning limit, this is an indication that the selected risk or hazard level will never be reached or exceeded for that chemical and the selected exposure scenario.

[B] Screening levels for these media based on other considerations (for example, aesthetic, background levels, environmental resource protection, and so forth) can be derived with these equations by substituting the selected target level for $RBSL_{air}$ or $RBSL_w$ appearing in these equations.

[C] These equations are based on Ref (26).

[D] These equations simply define the "cross-media partitioning factors," VF_i and LF_{sw}.

X2.4 *Ground Water—Inhalation of Outdoor Vapors:*

X2.4.1 In this case chemical intake is a result of inhalation of outdoor vapors which originate from dissolved hydrocarbons in ground water located some distance below ground surface. Here the goal is to determine the dissolved hydrocarbon RBSL that corresponds to the target RBSL for outdoor vapors in the breathing zone, as given in Tables X2.3 and X2.4. If the selected target vapor concentration is some value other than the RBSL for inhalation (that is, odor threshold or ecological criterion), this value can be substituted for the $RBSL_{air}$ parameter appearing in the equations given in Tables X2.2 and X2.3.

X2.4.2 A conceptual model for the transport of chemicals from ground water to ambient air is depicted in Fig. X2.1. For simplicity, the relationship between outdoor air and dissolved ground water concentrations is represented in Tables X2.2 and X2.3 by the "volatilization factor," VF_{wamb} [(mg/m³-air)/(mg/L-H_2O)], defined in Table X2.5. It is based on the following assumptions:

X2.4.2.1 A constant dissolved chemical concentration in ground water,

X2.4.2.2 Linear equilibrium partitioning between dissolved chemicals in ground water and chemical vapors at the ground water table,

X2.4.2.3 Steady-state vapor- and liquid-phase diffusion through the capillary fringe and vadose zones to ground

TABLE X2.4 Exposure Parameters Appearing in Tables X2.2 and X2.3

Parameters	Definitions, Units	Residential	Commercial/Industrial
AT_c	averaging time for carcinogens, years	70 years	70 years[A]
AT_n	averaging time for noncarcinogens, years	30 years	25 years[A]
BW	adult body weight, kg	70 kg	70 kg[A]
ED	exposure duration, years	30 years	25 years[A]
EF	exposure frequency, days/years	350 days/year	250 days/year[A]
IR_{soil}	soil ingestion rate, mg/day	100 mg/day	50 mg/day[A]
IR_{air}-indoor	daily indoor inhalation rate, m^3/day	15 m^3/day	20 m^3/day[A]
IR_{air}-outdoor	daily outdoor inhalation rate, m^3/day	20 m^3/day	20 m^3/day[A]
IR_w	daily water ingestion rate, L/day	2 L/day	1 L/day[A]
LF_{sw}	leaching factor, (mg/L-H_2O)/(mg/kg-soil)—see Table X2.5	chemical-specific	chemical-specific
M	soil to skin adherence factor, mg/cm^2	0.5	0.5[B]
RAF_d	dermal relative absorption factor, volatiles/PAHs	0.5/0.05	0.5/0.05[B]
RAF_o	oral relative absorption factor	1.0	1.0
$RBSL_i$	risk-based screening level for media i, mg/kg-soil, mg/L-H_2O, or µg/m^3-air	chemical-, media-, and exposure route-specific	chemical-, media-, and exposure route-specific
RfD_i	inhalation chronic reference dose, mg/kg-day	chemical-specific	chemical-specific
RfD_o	oral chronic reference dose, mg/kg-day	chemical-specific	chemical-specific
SA	skin surface area, cm^2/day	3160	3160[A]
SF_i	inhalation cancer slope factor, (mg/kg-day)$^{-1}$	chemical-specific	chemical-specific
SF_o	oral cancer slope factor, (mg/kg-day)$^{-1}$	chemical-specific	chemical-specific
THQ	target hazard quotient for individual constituents, unitless	1.0	1.0
TR	target excess individual lifetime cancer risk, unitless	for example, 10^{-6} or 10^{-4}	for example, 10^{-6} or 10^{-4}
VF_i	volatilization factor, (mg/m^3-air)/(mg/kg-soil) or (mg/m^3-air)/(mg/L-H_2O)—see Table X2.5	chemical- and media-specific	chemical- and media-specific

[A] See Ref (27).
[B] See Ref (28).

surface,

X2.4.2.4 No loss of chemical as it diffuses towards ground surface (that is, no biodegradation), and

X2.4.2.5 Steady well-mixed atmospheric dispersion of the emanating vapors within the breathing zone as modeled by a "box model" for air dispersion.

X2.4.3 Should the calculated $RBSL_w$ exceed the pure component solubility for any individual component, ">S" is entered in the table to indicate that the selected risk level or hazard quotient cannot be reached or exceeded for that compound and the specified exposure scenario.

X2.5 *Ground Water—Inhalation of Enclosed-Space (Indoor) Vapors:*

X2.5.1 In this case chemical intake results from the inhalation of vapors in enclosed spaces. The chemical vapors originate from dissolved hydrocarbons in ground water located some distance below ground surface. Here the goal is to determine the dissolved hydrocarbon RBSL that corresponds to the target RBSL for vapors in the breathing zone, as given in Tables X2.2 and X2.3. If the selected target vapor concentration is some value other than the RBSL for inhalation (that is, odor threshold or ecological criterion), this value can be substituted for the $RBSL_{air}$ parameter appearing in the equations given in Tables X2.2 and X2.3.

X2.5.2 A conceptual model for the transport of chemicals from ground water to indoor air is depicted in Fig. X2.2. For simplicity, the relationship between enclosed-space air and dissolved ground water concentrations is represented in Tables X2.2 and X2.3 by the "volatilization factor" VF_{wesp} [(mg/m^3-air)/(mg/L-H_2O)] defined in Table X2.5. It is based on the following assumptions:

X2.5.2.1 A constant dissolved chemical concentration in ground water,

X2.5.2.2 Equilibrium partitioning between dissolved chemicals in ground water and chemical vapors at the ground water table,

X2.5.2.3 Steady-state vapor- and liquid-phase diffusion through the capillary fringe, vadose zone, and foundation cracks,

X2.5.2.4 No loss of chemical as it diffuses towards ground surface (that is, no biodegradation), and

X2.5.2.5 Steady, well-mixed atmospheric dispersion of the emanating vapors within the enclosed space, where the convective transport into the building through foundation cracks or openings is negligible in comparison with diffusive transport.

X2.5.3 Should the calculated $RBSL_w$ exceed the pure component solubility for any individual component, ">S" is entered in the table to indicate that the selected risk level or hazard quotient cannot be reached or exceeded for that compound and the specified exposure scenario.

X2.6 *Surficial Soils—Ingestion, Dermal Contact, and Vapor and Particulate Inhalation:*

X2.6.1 In this case it is assumed that chemical intake results from a combination of intake routes, including: ingestion, dermal absorption, and inhalation of both particulates and vapors emanating from surficial soil.

X2.6.2 Equations used to estimate intake resulting from ingestion follow guidance given in Ref (26) for ingestion of chemicals in soil. For this route, it has been assumed that surficial soil chemical concentrations and intake rates remain constant over the exposure duration.

X2.6.3 Equations used to estimate intake resulting from dermal absorption follow guidance given in Ref (26) for dermal contact with chemicals in soil. For this route, it has been assumed that surficial soil chemical concentrations and absorption rates remain constant over the exposure duration.

X2.6.4 Equations used to estimate intake resulting from the inhalation of particulates follow guidance given in Ref (26) for inhalation of airborne chemicals. For this route, it has been assumed that surficial soil chemical concentrations, intake rates, and atmospheric particulate concentrations remain constant over the exposure duration.

X2.6.5 Equations used to estimate intake resulting from

the inhalation of airborne chemicals resulting from the volatilization of chemicals from surficial soils follow guidance given in Ref (26) for inhalation of airborne chemicals.

X2.6.6 A conceptual model for the volatilization of chemicals from surficial soils to outdoor air is depicted in Fig. X2.3. For simplicity, the relationship between outdoor air and surficial soil concentrations is represented in Tables X2.2 and X2.3 by the "volatilization factor" VF_{ss} [(mg/m³-air)/(mg/kg-soil)] defined in Table X2.5. It is based on the following assumptions:

X2.6.6.1 Uniformly distributed chemical throughout the depth 0—d (cm) below ground surface,

X2.6.6.2 Linear equilibrium partitioning within the soil matrix between sorbed, dissolved, and vapor phases, where

TABLE X2.5 Volatilization Factors (VF_i), Leaching Factor (LF_{sw}), and Effective Diffusion Coefficients (D_i^{eff})

Symbol	Cross-Media Route (or Definition)	Equation
VF_{wesp}	Ground water → enclosed-space vapors	$VF_{wesp}\left[\frac{(mg/m^3\text{-}air)}{(mg/L\text{-}H_2O)}\right] = \frac{H\left[\frac{D_{ws}^{eff}/L_{GW}}{ER\,L_B}\right]}{1+\left[\frac{D_{ws}^{eff}/L_{GW}}{ER\,L_B}\right]+\left[\frac{D_{ws}^{eff}/L_{GW}}{(D_{crack}^{eff}/L_{crack})\eta}\right]} \times 10^3\,\frac{L}{m^3}$ [A]
VF_{wamb}	Ground water → ambient (outdoor) vapors	$VF_{wamb}\left[\frac{(mg/m^3\text{-}air)}{(mg/L\text{-}H_2O)}\right] = \frac{H}{1+\left[\frac{U_{air}\delta_{air}L_{GW}}{WD_{ws}^{eff}}\right]} \times 10^3\,\frac{L}{m^3}$ [B]
VF_{ss}	Surficial soils → ambient air (vapors)	$VF_{ss}\left[\frac{(mg/m^3\text{-}air)}{(mg/kg\text{-}soil)}\right] = \frac{2W\rho_s}{U_{air}\delta_{air}}\sqrt{\frac{D_s^{eff}H}{\pi[\theta_{ws}+k_s\rho_s+H\theta_{as}]T}} \times 10^3\,\frac{cm^3\text{-}kg}{m^3\text{-}g}$ [C] or: $VF_{ss}\left[\frac{(mg/m^3\text{-}air)}{(mg/kg\text{-}soil)}\right] = \frac{W\rho_s d}{U_{air}\delta_{air}T} \times 10^3\,\frac{cm^3\text{-}kg}{m^3\text{-}g}$; whichever is less [D]
VF_p	Surficial soils → ambient air (particulates)	$VF_p\left[\frac{(mg/m^3\text{-}air)}{(mg/kg\text{-}soil)}\right] = \frac{P_e W}{U_{air}\delta_{air}} \times 10^3\,\frac{cm^3\text{-}kg}{m^3\text{-}g}$ [E]
VF_{samb}	Subsurface soils → ambient air	$VF_{samb}\left[\frac{(mg/m^3\text{-}air)}{(mg/kg\text{-}soil)}\right] = \frac{H\rho_s}{[\theta_{ws}+k_s\rho_s+H\theta_{as}]\left(1+\frac{U_{air}\delta_{air}L_S}{D_s^{eff}W}\right)} \times 10^3\,\frac{cm^3\text{-}kg}{m^3\text{-}g}$ [F]
VF_{sesp}	Subsurface soil → enclosed-space vapors	$VF_{sesp}\left[\frac{(mg/m^3\text{-}air)}{(mg/kg\text{-}soil)}\right] = \frac{\frac{H\rho_s}{[\theta_{ws}+k_s\rho_s+H\theta_{as}]}\left[\frac{D_s^{eff}/L_S}{ER\,L_B}\right]}{1+\left[\frac{D_s^{eff}/L_S}{ER\,L_B}\right]+\left[\frac{D_S^{eff}/L_s}{(D_{crack}^{eff}/L_{crack})\eta}\right]} \times 10^3\,\frac{cm^3\text{-}kg}{m^3\text{-}g}$ [A]
LF_{sw}	Subsurface soils → ground water	$LF_{sw}\left[\frac{(mg/L\text{-}H_2O)}{(mg/kg\text{-}soil)}\right] = \frac{\rho_s}{[\theta_{ws}+k_s\rho_s+H\theta_{as}]\left(1+\frac{U_{gw}\delta_{gw}}{IW}\right)} \times 10^0\,\frac{cm^3\text{-}kg}{L\text{-}g}$ [B]
D_s^{eff}	Effective diffusion coefficient in soil based on vapor-phase concentration	$D_s^{eff}\left[\frac{cm^2}{s}\right] = D^{air}\frac{\theta_{as}^{3.33}}{\theta_T^2} + D^{wat}\frac{1}{H}\frac{\theta_{ws}^{3.33}}{\theta_T^2}$ [A]
D_{crack}^{eff}	Effective diffusion coefficient through foundation cracks	$D_{crack}^{eff}\left[\frac{cm^2}{s}\right] = D^{air}\frac{\theta_{acrack}^{3.33}}{\theta_T^2} + D^{wat}\frac{1}{H}\frac{\theta_{wcrack}^{3.33}}{\theta_T^2}$ [A]
D_{cap}^{eff}	Effective diffusion coefficient through capillary fringe	$D_{cap}^{eff}\left[\frac{cm^2}{s}\right] = D^{air}\frac{\theta_{acap}^{3.33}}{\theta_T^2} + D^{wat}\frac{1}{H}\frac{\theta_{wcap}^{3.33}}{\theta_T^2}$ [A]
D_{ws}^{eff}	Effective diffusion coefficient between ground water and soil surface	$D_{ws}^{eff}\left[\frac{cm^2}{s}\right] = (h_{cap}+h_v)\left[\frac{h_{cap}}{D_{cap}^{eff}}+\frac{h_v}{D_s^{eff}}\right]^{-1}$ [A]
C_s^{sat}	Soil concentration at which dissolved pore-water and vapor phases become saturated	$C_s^{sat}\left[\frac{mg}{kg\text{-}soil}\right] = \frac{S}{\mu_s} \times [H\theta_{as}+\theta_{ws}+k_s\rho_s] \times 10^0\,\frac{L\text{-}g}{cm^3\text{-}kg}$ [F]

[A] See Ref (29).
[B] See Ref (30).
[C] See Ref (31).
[D] Based on mass balance.
[E] See Ref (32).
[F] See Ref (33).

TABLE X2.6 Soil, Building, Surface, and Subsurface Parameters Used in Generating Example Tier 1 RBSLs

NOTE—See X2.10 for justification of parameter selection.

Parameters	Definitions, Units	Residential	Commercial/Industrial
d	lower depth of surficial soil zone, cm	100 cm	100 cm
D^{air}	diffusion coefficient in air, cm^2/s	chemical-specific	chemical-specific
D^{wat}	diffusion coefficient in water, cm^2/s	chemical-specific	chemical-specific
ER	enclosed-space air exchange rate, L/s	0.00014 s^{-1}	0.00023 s^{-1}
f_{oc}	fraction of organic carbon in soil, g-C/g-soil	0.01	0.01
H	henry's law constant, $(cm^3\text{-}H_2O)/(cm^3\text{-air})$	chemical-specific	chemical-specific
h_{cap}	thickness of capillary fringe, cm	5 cm	5 cm
h_v	thickness of vadose zone, cm	295 cm	295 cm
I	infiltration rate of water through soil, cm/years	30 cm/year	30 cm/year
k_{oc}	carbon-water sorption coefficient, $cm^3\text{-}H_2O/g\text{-}C$	chemical-specific	chemical-specific
k_s	soil-water sorption coefficient, $cm^3\text{-}H_2O/g\text{-soil}$	$f_{oc} \times k_{oc}$	$f_{oc} \times k_{oc}$
L_B	enclosed-space volume/infiltration area ratio, cm	200 cm	300 cm
L_{crack}	enclosed-space foundation or wall thickness, cm	15 cm	15 cm
L_{GW}	depth to ground water = $h_{cap} + h_v$, cm	300 cm	300 cm
L_S	depth to subsurface soil sources, cm	100 cm	100 cm
P_e	particulate emission rate, $g/cm^2\text{-}s$	6.9×10^{-14}	6.9×10^{-14}
S	pure component solubility in water, $mg/L\text{-}H_2O$	chemical-specific	chemical-specific
U_{air}	wind speed above ground surface in ambient mixing zone, cm/s	225 cm/s	225 cm/s
U_{gw}	ground water Darcy velocity, cm/year	2500 cm/year	2500 cm/year
W	width of source area parallel to wind, or ground water flow direction, cm	1500 cm	1500 cm
δ_{air}	ambient air mixing zone height, cm	200 cm	200 cm
δ_{gw}	ground water mixing zone thickness, cm	200 cm	200 cm
η	areal fraction of cracks in foundations/walls, $cm^2\text{-cracks}/cm^2\text{-total area}$	0.01 $cm^2\text{-cracks}/cm^2\text{-total area}$	0.01 $cm^2\text{-cracks}/cm^2\text{-total area}$
θ_{acap}	volumetric air content in capillary fringe soils, $cm^3\text{-air}/cm^3\text{-soil}$	0.038 $cm^3\text{-air}/cm^3\text{-soil}$	0.38 $cm^3\text{-air}/cm^3\text{-soil}$
θ_{acrack}	volumetric air content in foundation/wall cracks, $cm^3\text{-air}/cm^3$ total volume	0.26 $cm^3\text{-air}/cm^3$ total volume	0.26 $cm^3\text{-air}/cm^3$ total volume
θ_{as}	volumetric air content in vadose zone soils, $cm^3\text{-air}/cm^3\text{-soil}$	0.26 $cm^3\text{-air}/cm^3\text{-soil}$	0.26 $cm^3\text{-air}/cm^3\text{-soil}$
θ_T	total soil porosity, $cm^3/cm^3\text{-soil}$	0.38 $cm^3/cm^3\text{-soil}$	0.38 $cm^3/cm^3\text{-soil}$
θ_{wcap}	volumetric water content in capillary fringe soils, $cm^3\text{-}H_2O/cm^3\text{-soil}$	0.342 $cm^3\text{-}H_2O/cm^3\text{-soil}$	0.342 $cm^3\text{-}H_2O/cm^3\text{-soil}$
θ_{wcrack}	volumetric water content in foundation/wall cracks, $cm^3\text{-}H_2O/cm^3$ total volume	0.12 $cm^3\text{-}H_2O/cm^3$ total volume	0.12 $cm^3\text{-}H_2O/cm^3$ total volume
θ_{ws}	volumetric water content in vadose zone soils, $cm^3\text{-}H_2O/cm^3\text{-soil}$	0.12 $cm^3\text{-}H_2O/cm^3\text{-soil}$	0.12 $cm^3\text{-}H_2O/cm^3\text{-soil}$
ρ_s	soil bulk density, g-soil/cm^3-soil	1.7 g/cm^3	1.7 g/cm^3
τ	averaging time for vapor flux, s	7.88×10^8 s	7.88×10^8 s

the partitioning is a function of constant chemical- and soil-specific parameters,

X2.6.6.3 Diffusion through the vadose zone,

X2.6.6.4 No loss of chemical as it diffuses towards ground surface (that is, no biodegradation), and

X2.6.6.5 Steady well-mixed atmospheric dispersion of the emanating vapors within the breathing zone as modeled by a "box model" for air dispersion.

X2.6.7 In the event that the time-averaged flux exceeds that which would occur if all chemical initially present in the surficial soil zone volatilized during the exposure period, then the volatilization factor is determined from a mass balance assuming that all chemical initially present in the surficial soil zone volatilizes during the exposure period.

X2.7 *Subsurface Soils—Inhalation of Outdoor Vapors:*

X2.7.1 In this case chemical intake is a result of inhalation of outdoor vapors which originate from hydrocarbons contained in subsurface soils located some distance below ground surface. Here the goal is to determine the RBSL for subsurface soils that corresponds to the target RBSL for outdoor vapors in the breathing zone, as given in X2.2. If the selected target vapor concentration is some value other than

TABLE X2.7 Chemical-Specific Properties Used in the Derivation Example Tier 1 RBSLs

Chemical	CAS Number	M_w, g/mol	H, $L\text{-}H_2O/L\text{-air}$	D^{air}, cm^2/s	D^w, cm^2/s	$\log(K_{oc})$, L/kg	$\log(K_{ow})$, L/kg
Benzene	71-43-2	78[A]	0.22[A]	0.093[A]	1.1×10^{-5}[A]	1.58[A]	2.13[A]
Toluene	108-88-3	92[A]	0.26[A]	0.085[A]	9.4×10^{-6}[D]	2.13[A]	2.65[A]
Ethyl benzene	100-41-4	106[A]	0.32[A]	0.076[A]	8.5×10^{-6}[D]	1.98[A]	3.13[A]
Mixed xylenes	1330-20-7	106[A]	0.29[A]	0.072[D]	8.5×10^{-6}[D]	2.38[A]	3.26[A]
Naphthalene	91-20-3	128[A]	0.049[A]	0.072[D]	9.4×10^{-6}[A]	3.11[A]	3.28[A]
Benzo(a)pyrene	50-32-8	252[C]	5.8×10^{-6}[B]	0.050[D]	5.8×10^{-6}[D]	5.59[E]	5.98[B]

Chemical	CAS Number	SF_o, kg-day/mg	SF_i, kg-day/mg	RfD_o, mg/kg-day	RfD_i, mg/kg-day
Benzene	71-43-2	0.029[F]	0.029[F]	...	...
Toluene	108-88-3	...	...	0.2[F]	0.11[F]
Ethyl benzene	100-41-4	...	...	0.1[F]	0.29[F]
Mixed xylenes	1330-20-7	...	...	2.0[F]	2.0[F]
Naphthalene	91-20-3	...	...	0.004[G]	0.004[G]
Benzo(a)pyrene	50-32-8	7.3[F]	6.1[F]	...	...

[A] See Ref (34).
[B] See Ref (35).
[C] See Ref (7).
[D] Diffusion coefficient calculated using the method of Fuller, Schettler, and Giddings, from Ref (11).
[E] Calculated from K_{ow}/K_{oc} correlation: $\log(K_{oc}) = 0.937 \log(K_{ow}) - 0.006$, from Ref (11).
[F] See Ref (2).
[G] See Ref (3).

the RBSL for inhalation (that is, odor threshold or ecological criterion), this value can be substituted for the $RBSL_{air}$ parameter appearing in the equations given in Tables X2.2 and X2.3.

X2.7.2 A conceptual model for the transport of chemicals from subsurface soils to ambient air is depicted in Fig. X2.4. For simplicity, the relationship between outdoor air and soil concentrations is represented in Tables X2.2 and X2.3 by the "volatilization factor," VF_{samb} [(mg/m^3-air)/(kg-soil)], defined in Table X2.5. It is based on the following assumptions:

X2.7.2.1 A constant chemical concentration in subsurface soils,

X2.7.2.2 Linear equilibrium partitioning within the soil matrix between sorbed, dissolved, and vapor phases, where the partitioning is a function of constant chemical- and soil-specific parameters,

X2.7.2.3 Steady-state vapor- and liquid-phase diffusion through the vadose zone to ground surface,

X2.7.2.4 No loss of chemical as it diffuses towards ground surface (that is, no biodegradation), and

X2.7.2.5 Steady well-mixed atmospheric dispersion of the emanating vapors within the breathing zone as modeled by a "box model" for air dispersion.

X2.7.3 Should the calculated $RBSL_s$ exceed the value for which the equilibrated vapor and dissolved pore-water phases become saturated, C_s^{sat} [mg/kg-soil] (see Table X2.5 for calculation of this value), "RES" is entered in the table to indicate that the selected risk level or hazard quotient cannot be reached or exceeded for that compound and the specified exposure scenario (even if free-phase product or precipitate is present in the soil).

X2.8 *Subsurface Soils—Inhalation of Enclosed-Space (Indoor) Vapors:*

X2.8.1 In this case chemical intake is a result of inhalation of enclosed-space vapors which originate from hydrocarbons contained in subsurface soils located some distance below ground surface. Here the goal is to determine the RBSL for subsurface soils that corresponds to the target RBSL for indoor vapors, as given in Tables X2.2 and X2.3. If the selected target vapor concentration is some value other than the RBSL for inhalation (that is, odor threshold or

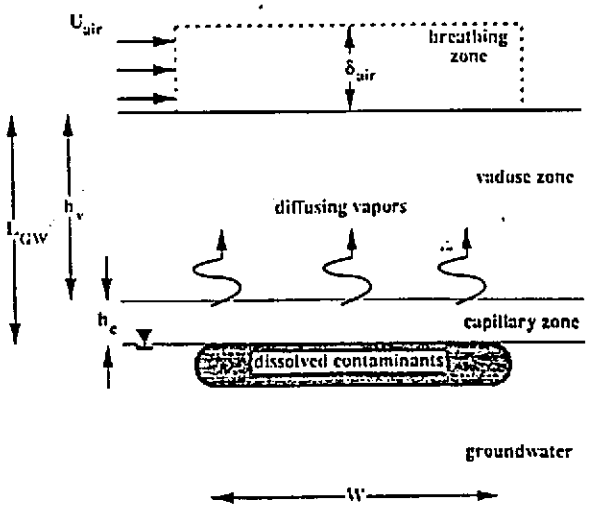


FIG. X2.1 Volatilization from Ground Water to Ambient Air

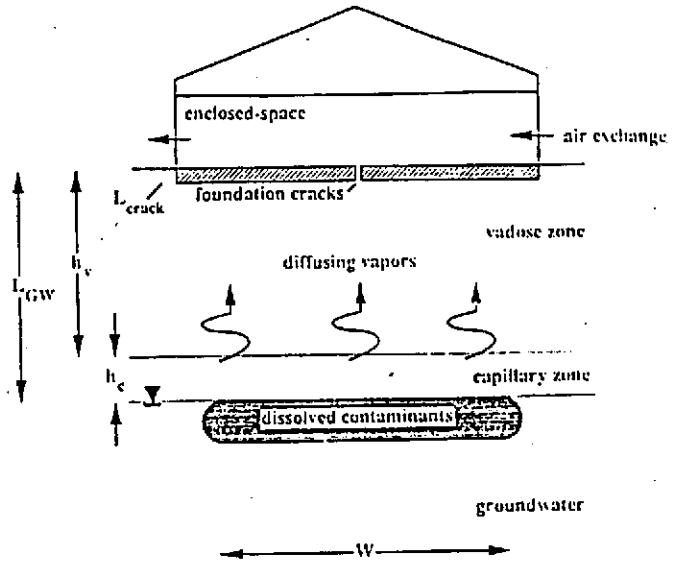


FIG. X2.2 Volatilization from Ground Water to Enclosed-Space Air

ecological criterion), this value can be substituted for the $RBSL_{air}$ parameter appearing in the equations given in Tables X2.2 and X2.3.

X2.8.2 A conceptual model for the transport of chemicals from subsurface soils to enclosed spaces is depicted in Fig. X2.5. For simplicity, the relationship between indoor air and soil concentrations is represented in Tables X2.2 and X2.3 by the "volatilization factor," VF_{sesp} [(mg/m^3-air)/(kg-soil)], defined in Table X2.5. It is based on the following assumptions:

X2.8.2.1 A constant chemical concentration in subsurface soils,

X2.8.2.2 Linear equilibrium partitioning within the soil matrix between sorbed, dissolved, and vapor phases, where the partitioning is a function of constant chemical- and soil-specific parameters,

X2.8.2.3 Steady-state vapor- and liquid-phase diffusion through the vadose zone and foundation cracks,

X2.8.2.4 No loss of chemical as it diffuses towards ground surface (that is, no biodegradation), and

X2.8.2.5 Well-mixed atmospheric dispersion of the emanating vapors within the enclosed space.

X2.8.3 Should the calculated $RBSL_s$ exceed the value C_s^{sat} [mg/kg-soil] for which the equilibrated vapor and dissolved pore-water phases become saturated (see Table X2.5 for calculation of this value), "RES" is entered in the table to indicate that the selected risk level or hazard

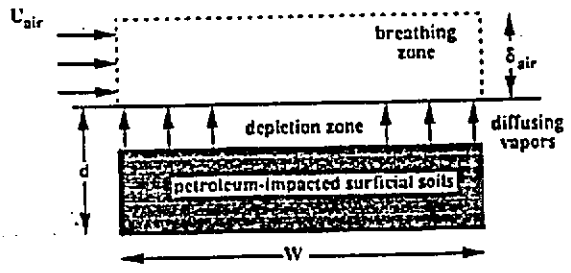


FIG. X2.3 Volatilization from Surficial Soils

quotient cannot be reached or exceeded for that compound and the specified exposure scenario (even if free-phase product or precipitate is present in the soil).

X2.9 *Subsurface Soils—Leaching to Ground Water:*

X2.9.1 In this case chemical intake is a result of chemicals leaching from subsurface soils, followed by inhalation of enclosed-space vapors, inhalation of outdoor vapors, or ingestion of ground water as discussed in X2.1 through X2.3. Here the goal is to determine the RBSL for subsurface soils that corresponds to the target RBSLs for the inhalation or ingestion routes. If the selected target ground water concentration is some value other than an RBSL for ground water (that is, odor threshold or ecological criterion), this value can be substituted for the $RBSL_w$ parameter appearing in the equations given in Tables X2.2 and X2.3.

X2.9.2 A conceptual model for the leaching of chemicals from subsurface soils to ground water is depicted in Fig. X2.6. For simplicity, the relationship between ground water and soil concentrations is represented in Tables X2.2 and X2.3 by the "leaching factor," LF_{sw} [(mg/L-H_2O)/ (mg/kg-soil)], defined in Table X2.5. It is based on the following assumptions:

X2.9.2.1 A constant chemical concentration in subsurface soils,

X2.9.2.2 Linear equilibrium partitioning within the soil matrix between sorbed, dissolved, and vapor phases, where the partitioning is a function of constant chemical- and soil-specific parameters,

X2.9.2.3 Steady-state leaching from the vadose zone to ground water resulting from the constant leaching rate I [cm/s],

X2.9.2.4 No loss of chemical as it leaches towards ground water (that is, no biodegradation), and

X2.9.2.5 Steady well-mixed dispersion of the leachate within a ground water "mixing zone."

X2.9.3 Should the calculated $RBSL_s$ exceed the value for which the equilibrated vapor and dissolved pore-water phases become saturated (see Table X2.5 for calculation of this value), "RES" is entered in the table to indicate that the selected risk level or hazard quotient cannot be reached or exceeded for that compound and the specified exposure scenario (even if free-phase product or precipitate is present in the soil).

X2.9.4 In some regulatory programs, "dilution attenuation factors" (DAFs) are currently being proposed based on

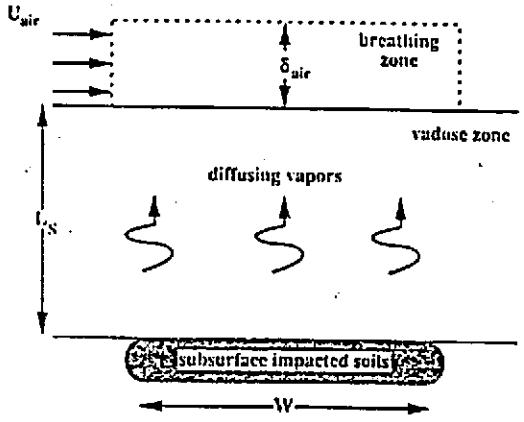


FIG. X2.4 Volatilization from Subsurface Soils to Ambient Air

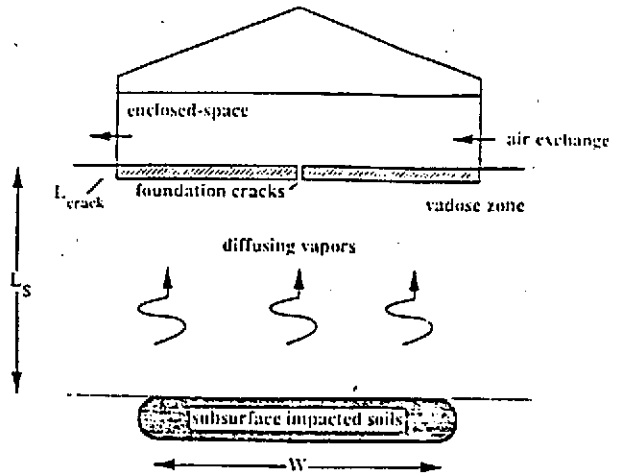


FIG. X2.5 Volatilization from Subsurface Soils to Enclosed-Space Air

fate and transport modeling results. A DAF is typically defined as the ratio of a target ground water concentration divided by the source leachate concentration, and is inherently very similar to the leachate factor, LF_{sw}, discussed here. The difference between these two terms is that LF_{sw} represents the ratio of the target ground water concentration divided by the source area soil concentration. Should a regulatory program already have a technically defensible DAF value, it can be equated to a leachate factor by the following expression:

$$LF_{sw} = \frac{DAF \times \rho_s}{[\theta_{ws} + k_s \rho_s + H\theta_{as}]} \times 10^0$$

where the parameters are defined in Table X2.6.

X2.10 *Parameter Values:*

X2.10.1 Table X2.4 lists exposure parameters used to calculate the RBSLs appearing in sample Look-Up Table X2.1. All values given are based on adult exposures only. With the exception of the dermal exposure parameters (SA, M, and RAF_d), the values given are reasonable maximum exposure (RME) values presented in Ref (27) and are regarded as upper bound estimates for each individual exposure parameter.

X2.10.2 The skin surface area, SA = 3160 cm^2/day, is based on the average surface area of the head, hands, and

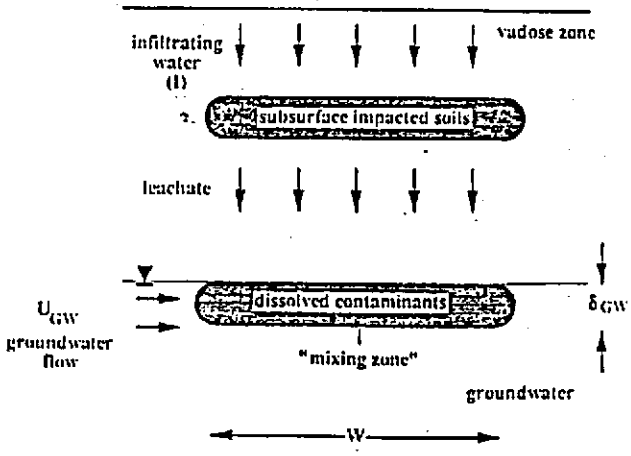


FIG. X2.6 Leaching from Subsurface Soils to Ground Water

forearms for adult males given in Ref (27). The soil-to-skin adherence factor, M [mg/cm^2], and dermal relative absorption factor, RAF_d [mg-absorbed/mg-applied], are based on guidance issued by Ref (28).

X2.10.3 Soil properties are based on typical values for sandy soils and are consistent with values given in Ref (30).

X2.10.4 Physical dimensions are consistent with the scale of typical underground fuel tank releases.

X2.10.5 Particulate emission rates were estimated by the approach presented by Cowherd, et al (32). It was assumed that the mode of the surficial soil size distribution was 2 mm, the erosion potential was unlimited, there was no vegetative cover, and the mean average annual wind speed was 4 m/s.

X2.10.6 The chemical-specific parameters used are defined in Table X2.7.

X2.10.7 In this development, surficial soils are defined as those soils present within 1 m of ground surface. Subsurface soil RBSLs are based on assumed source depths of 1 m. Ground water is assumed to be located 3 m below ground surface.

X2.10.8 Once again, the reader is reminded that the parameter (and corresponding RBSL) values are presented here as examples only, and are not intended to be used as standards. At best, the parameters presented are reasonable values based on current information and professional judgment. The reader should review and verify all assumptions prior to using any of the example RBSLs as screening level values.

X3. USE OF PREDICTIVE MODELING IN THE RISK-BASED CORRECTIVE ACTION PROCESS

X3.1 *Scope:*

X3.1.1 Predictive modeling is a valuable tool that can provide information to the risk management process. In a RBCA, modeling is used to predict the location and concentration contaminants and to interpret, or extrapolate, site characterization data, historical monitoring data, and toxicological information. In addition, predictive modeling may be used in evaluation of remedial alternatives and in evaluating compliance targets in monitoring plans. This appendix discusses the following:

X3.1.1.1 Significance and use of predictive modeling in the RBCA process;

X3.1.1.2 Interpretation of predictive modeling results;

X3.1.1.3 Procedures for predictive migration models; and

X3.1.1.4 Procedures for exposure, risk, and dose-response assessment.

X3.1.2 This appendix is not intended to be all inclusive. Each predictive model is unique and may require additional procedures in its development and application. All such additional analyses should be documented in the RBCA process.

X3.2 *Referenced Documents:*

X3.2.1 *ASTM Standards:*

D 653 Terminology Relating to Soil, Rock, and Contained Fluids[7]

D 5447 Guide for Application of a Ground-Water Flow Model to a Site-Specific Problem[8]

D 5490 Guide for Comparing Ground-Water Flow Model Simulations to Site-Specific Information[8]

E 943 Terminology Relating to Biological Effects and Environmental Fate[9]

E 978 Practice for Evaluating Environmental Fate Models of Chemicals[9]

D 5609 Guide for Defining Boundary Conditions in Ground-Water Flow Modeling[8]

D 5610 Guide for Defining Initial Conditions in Ground-Water Flow Modeling[8]

D 5611 Guide for Conducting a Sensitivity Analysis for a Ground-Water Flow Model Application[8]

X3.3 *Terminology:*

X3.3.1 *Definitions*—For definitions of terms used in this appendix, see Terminologies D 653 and E 943.

X3.3.2 *Descriptions of Terms Specific to This Appendix:*

X3.3.2.1 *analytical model*—a model that uses mathematical solutions to governing equations that are continuous in space and time and applicable to the flow and transport process.

X3.3.2.2 *application verification*—using the set of parameter values and boundary conditions from a calibrated model to approximate acceptably a second set of field data measured under similar conditions.

DISCUSSION—Application verification is to be distinguished from code verification, which refers to software testing, comparison with analytical solutions, and comparison with other similar codes to demonstrate that the code represents its mathematical foundation.

X3.3.2.3 *boundary condition*—a mathematical expression of a state of the physical system that constrains the equations of the mathematical model.

X3.3.2.4 *calibration (model application)*—the process of refining the model representation of the fluid and media properties and boundary conditions to achieve a desired degree of correspondence between the model simulation and observations of the real system.

X3.3.2.5 *code validation*—the process of determining how well a modeling code's theoretical foundation and computer implementation describe actual system behavior in terms of the "degree of correlation" between calculated and independently observed cause-and-effect responses of the prototype fluid flow system (for example, research site or laboratory experiment) for which the code has been developed.

X3.3.2.6 *code verification*—the procedure aimed at establishing the completeness, consistency, correctness, and accuracy of modeling software with respect to its design criteria by evaluating the functionality and operational characteristics of the code and testing embedded algorithms and data transfers through execution of problems for which indepen-

[7] *Annual Book of ASTM Standards*, Vol 04.08.
[8] *Annual Book of ASTM Standards*, Vol 04.09.
[9] *Annual Book of ASTM Standards*, Vol 11.04.

dent benchmarks are available.

X3.3.2.7 *computer code (computer program)*—the assembly of numerical techniques, bookkeeping, and control language that represents the model from acceptance of input data and instructions to delivery of output.

X3.3.2.8 *conceptual model*—an interpretation or working description of the characteristics and dynamics of the physical system.

TABLE X3.1 Example Screening Level Transport Models

Description	Mathematical Approximation	Parameters
Dissolved Phase Transport:		$C(x)$ = dissolved hydrocarbon concentration along centerline (x, y = 0, z = 0) of dissolved plume [g/cm³-H_2O]
Maximum transport rate $u_{d,max}$ [cm/day] of dissolved plume	$u_{d,max} = \frac{K_s i}{\theta_s R_c}$	C_{source} = dissolved hydrocarbon concentration in dissolved plume source area [g/cm³-H_2O]
		i = ground water gradient [cm/cm]
		K_s = saturated hydraulic conductivity [cm/day]
		k_s = sorption coefficient [(g/g-soil)/(g/cm³-H_2O)]
Minimum time $\tau_{d,min}$ [d] for leading edge of dissolved plume to travel distance, L [cm]	$\tau_{d,min} = \frac{L}{u_{d,max}}$	L = distance downgradient [cm]
		R_c = retardation factor = $[1 + k_s\rho_s/\theta_s]$
		S_w = source width (perpendicular to flow in the horizontal plane) [cm]
		S_d = source width (perpendicular to flow in the vertical plane) [cm]
Steady-state attenuation [(g/cm³-H_2O)/(g/cm³-H_2O)] along the centerline (x, y = 0, z = 0) of a dissolved plume	$\frac{C(x)}{C_{source}} = \exp\left\{\frac{x}{2\alpha_x}\left[1 - \sqrt{\left(1 + \frac{4\lambda\alpha_x}{u}\right)}\right]\right\} \cdot \left(erf\left[\frac{S_w}{4\sqrt{\alpha_y x}}\right]\right)\left(erf\left[\frac{S_d}{4\sqrt{\alpha_z x}}\right]\right)$ where: $u = K_s i/\theta_s$	u = specific discharge [cm/day]
		$u_{d,max}$ = maximum transport rate of dissolved plume [cm/day]^A
		x = distance along centerline from downgradient edge of dissolved plume source zone [cm]
		y = depth below water table [cm]
		z = lateral distance away from dissolved plume centerline [cm]
		α_x = longitudinal dispersivity [cm] ≈ 0.10 x
		α_y = transverse dispersivity [cm] ≈ $\alpha_x/3$
		α_z = vertical dispersivity [cm] ≈ $\alpha_x/20$
		λ = first-order degradation constant [d^{-1}]
		θ_s = volumetric water content of saturated zone [cm³-H_2O/cm³-soil]
		ρ_s = soil bulk density [g-soil/cm³-soil]
		$\tau_{d,min}$ = minimum convective travel time of dissolved hydrocarbons to distance L [d]^A
		$erf(\eta)$ = error function evaluated for value η
Immiscible Phase Transport:		C_{soil} = total soil hydrocarbon concentration [g/g-soil]
Maximum depth D_{max} [cm] of immiscible phase penetration	$D_{max} = \frac{V_{spill}}{\theta_R \pi R_{spill}^2}$	$C_{v,eq}$ = equilibrium vapor concentration [g/cm³-vapor]^A
		$C_{w,eq}$ = equilibrium dissolved concentration [g/cm³-H_2O]^A
		D_{max} = maximum depth of immiscible phase penetration [cm]^A
Equilibrium Partitioning:		H = Henry's Law Constant [(g/cm³-vapor)/(g/cm³-H_2O)]
Vapor Concentration:		k_s = sorption coefficient [(g/g-soil)/(g/cm³-H_2O)]
$C_{v,eq}$ [g/cm³-*vapor*]		M_w = molecular weight [g/mol]
Maximum vapor concentration above dissolved hydrocarbons	$C_{v,eq} = HC_{w,eq}$	P_v^i = vapor pressure of compound i [atm]
Maximum vapor concentration when immiscible hydrocarbon is present	$C_{v,eq} = \frac{x_i P_v^i M_w}{RT}$	R = gas constant = 82 cm³-atm/mol-K
		R_{spill} = radial extent of hydrocarbon impact [cm]
		S_i = pure component solubility [g/cm³-H_2O]
		T = absolute temperature [K]
Maximum vapor concentrations in soil pores (no immiscible phase present)	$C_{v,eq} = \frac{HC_{soil}\rho_s}{[\theta_w + k_s\rho_s + H\theta_v]}$	V_{spill} = volume of hydrocarbon released [cm³]
		x_i = mol fraction of component i
		θ_R = volumetric residual content of hydrocarbon under drainage conditions [cm³-hydrocarbon/cm³-soil]
		θ_w = volumetric content of soil pore water [cm³-H_2O/cm³-soil]
		θ_v = volumetric content of soil vapor [cm³-vapor/cm³-soil]
Dissolved Concentration:		π = 3.1416
$C_{w,eq}$ [g/cm³-H_2O]		ρ_s = soil bulk density [g-soil/cm³-soil]
Maximum dissolved concentration when immiscible hydrocarbon is present	$C_{w,eq} = x_i S_i$	(C_{soil}) = concentration at which immiscible phase forms in soil [g/g-soil]^A
Maximum dissolved concentration in soil pores (no immiscible phase present)	$C_{w,eq} = \frac{C_{soil}\rho_s}{[\theta_w + k_s\rho_s + H\theta_v]}$	D^{air} = pure component diffusion coefficient in air [cm²/day]
Equilibrium Partioning:		D^{eff} = effective diffusion coefficient for combined vapor and solute transport, expressed as a vapor phase diffusion coefficient (no immiscible hydrocarbon present outside of source area) [cm²/day]^A
Soil Concentrations [g/g-soil]:		
Soil concentration [C_{soil}] [g/g-soil] at which immiscible hydrocarbon phase forms in soil matrix	$(C_{soil}) = \frac{S_i}{\rho_s}[\theta_w + k_s\rho_s + H\theta_v]$	D^w = pure component diffusion coefficient in water [cm²/day]
		H = Henry's Law Constant [(g/cm³-vapor)/(g/cm³-H_2O)]
		k_s = sorption coefficient [(g/g-soil)/(g/cm³-H_2O)]
Vapor Phase Transport:		k_v = permeability to vapor flow [cm²]
Effective porous media diffusion coefficient D^{eff} [cm²/day] for combined vapor and solute transport, expressed as a vapor phase diffusion coefficient (no immiscible hydrocarbon present outside of source area)	$D^{eff} = \frac{\theta_v^{3.33}}{\theta_T} D^{air} + \frac{1}{H}\frac{\theta_w^{3.33}}{\theta_T} D^w$	L = distance [cm]
		R_v = porous media "retardation" factor (no immiscible hydrocarbon present outside of source area)
		S_i = pure component solubility [g/cm³-H_2O]
		$u_{v,max}$ = maximum convective transport rate of vapors [cm/day]^A
		∇P = vapor phase pressure gradient [g/cm²-s²]
Porous media "retardation" factor R_v (no immiscible hydrocarbon present outside of source area)	$R_v = \left[\frac{\theta_w}{H} + \frac{k_s\rho_s}{H} + \theta_v\right]$	θ_w = volumetric content of soil pore water [cm³-H_2O/cm³-soil]

TABLE X3.1 *Continued*

Description	Mathematical Approximation
Maximum convective transport rate $u_{v,max}$ [cm/day] of vapors	$u_{v,max} = \frac{1}{R_v}\frac{k_v}{\mu_v}\nabla P$
Minimum time $\tau_{v,min}$ [d] for vapors to travel a distance L [cm] from source area by convection[A]	$\tau_{c,min} = \frac{L}{u_{v,max}}$
Minimum time $\tau_{v,min}$ [d] for vapors to travel a distance L [cm] from source area by diffusion	$\tau_{d,min} = \frac{L^2}{(D^{eff}/R_v)}$
Vapor Emissions from Subsurface Vapor Sources to Open Surfaces:	
Maximum diffusive vapor flux F_{max} [g/cm²-day] from subsurface vapor source located a distance d [cm] below ground surface (steady-state, constant source)	$F_{max} = D^{eff}\frac{C_{v,eq}}{d}$
Maximum time-averaged diffusive vapor flux $<F_{max}>$ [g/cm²-day] from subsurface soils over period from time = 0 to time = τ, single-component immiscible phase present	$<F_{max}> = \frac{\rho_s C_{soil}}{\tau}\left\{\sqrt{\left[d^2 + \frac{2C_{v,eq}D^{eff}\tau}{\rho_s C_{soil}}\right]} - d\right\}$
Maximum combined convective and diffusive vapor flux F_{max} [g/cm²-day] from subsurface vapor source located a distance d [cm] below ground surface	$F_{max} = R_v u_{v,max} C_{v,eq} - \frac{R_v u_{v,max} C_{v,eq}}{\left[1 - \exp\left(\frac{R_v u_{v,max} d}{D^{eff}}\right)\right]}$
Vapor Emissions from Surface Soils to Open Spaces:	
Maximum time-averaged diffusive vapor flux $<F_{max}>$ [g/cm²-day] from surface soils over period from time = 0 to time = τ, single-component immiscible phase present	$<F_{max}> = \rho_s C_{soil}\sqrt{\frac{2C_{v,eq}D^{eff}}{\rho_s C_{soil}\tau}}$
Maximum time-averaged diffusive vapor flux $<F_{max}>$ [g/cm²-day] from surface soils over period from time = 0 to time = τ, no immiscible phase present	$<F_{max}> = 2\rho_s C_{soil}\sqrt{\frac{D^{eff}}{\pi R_v \tau}}$
Maximum time-averaged diffusive vapor flux $<F_{max}>$ [g/cm²-day] from surface soils over period from time = 0 to time = τ, volatile components from relatively nonvolatile immiscible phase (for example, benzene from gasoline)	$<F_{max}> = \frac{2D^{eff}\left(\frac{x_i P_i^v M_{w,i}}{RT}\right)}{\sqrt{\pi\alpha\tau}}$
	where:
	$\alpha = \frac{D^{eff}}{\theta_v + \frac{\rho_s RT(C_{soil}/M_{w,T})}{P_i^v}}$

Parameters		
θ_v	=	volumetric content of soil vapor [cm³-vapor/cm³-soil]
θ_T	=	total volumetric content of pore space in soil matrix [cm³/cm³-soil]
μ_v	=	vapor viscosity [g/cm-s]
ρ_s	=	soil bulk density [g-soil/cm³-soil]
$\tau_{c,min}$	=	minimum time for vapors to travel a distance L [cm] by convection [day][A]
$\tau_{d,min}$	=	minimum time for vapors to travel a distance L [cm] by diffusion [day][A]
C_{soil}	=	total soil hydrocarbon concentration [g/g-soil]
$C_{v,eq}$	=	equilibrium vapor concentration [g/cm³-vapor][A]
d	=	distance below ground surface to top of hydrocarbon vapor source [cm]
D^{eff}	=	effective diffusion coefficient for combined vapor and solute transport, expressed as a vapor phase diffusion coefficient (no immiscible hydrocarbon present outside of source area) [cm²/day][A]
R_v	=	porous media "retardation" factor (no immiscible hydrocarbon present outside of source area)[A]
$u_{v,max}$	=	maximum convective transport rate $u_{v,max}$ of vapors [cm/day][A]
ρ_s	=	soil bulk density [g-soil/cm³-soil]
τ	=	averaging time [s]
A_B	=	total area of enclosed space exposed to vapor intrusion (area of foundation) [cm²]
A_{crack}	=	area of foundation through which vapors are transported (area of cracks, open seams, and so forth) [cm²]
C_{soil}	=	total soil hydrocarbon concentration [g/g-soil]
$C_{v,eq}$	=	equilibrium vapor concentration [g/cm³-vapor][A]
d	=	distance between foundation/walls and hydrocarbon vapor source [cm]
D^{eff}	=	effective diffusion coefficient through soil for combined vapor and solute transport, expressed as a vapor phase diffusion coefficient (no immiscible hydrocarbon present outside of source area) [cm²/day][A]
D^{crack}	=	effective diffusion coefficient through foundation cracks [cm²/day][A]
L_{crack}	=	thickness of foundation/wall [cm]
$M_{w,i}$	=	molecular weight of i [g/mol]
$M_{w,T}$	=	average molecular weight of the hydrocarbon mixture [g/mol]
P_i^v	=	vapor pressure of pure component i [atm]
Q_B	=	volumetric flow rate of air within enclosed space [cm³/s]
Q_{soil}	=	volumetric infiltration flow rate of soil gas into enclosed space [cm³/s]
R	=	gas constant = 82 atm-cm³/mol-K
R_v	=	porous media "retardation" factor[A]
T	=	absolute temperature [K]
x_i	=	mol fraction of component i
θ_v	=	volumetric content of soil vapor [cm³-vapor/cm³-soil]
ρ_s	=	soil bulk density [g-soil/cm³-soil]
π	=	3.1416
τ	=	averaging time [s]
$C_{w,eq}$	=	equilibrium dissolved concentration in leachate source area [g/cm³-H_2O][A]
E_B	=	enclosed space air exchange rate [l/d]
E_{max}	=	vapor emission rate into enclosed space [g/day][A]
F	=	vapor flux [g/cm²-day][A]
i	=	ground water gradient [cm/cm]
K_s	=	saturated hydraulic conductivity [cm/day]
L	=	downwind length of vapor emissions source area [cm]
M	=	ground water mixing zone thickness [cm]
q_i	=	water infiltration rate [cm/day]

X3.3.2.9 *ground water flow model*—application of a mathematical model to represent a site-specific ground water flow system.

X3.3.2.10 *mathematical model*—mathematical equations expressing the physical system and including simplifying assumptions. The representation of a physical system by mathematical expressions from which the behavior of the system can be deduced with known accuracy.

X3.3.2.11 *migration model*—application of a mathematical model to represent a site-specific fluid flow system.

X3.3.2.12 *model*—an assembly of concepts in the form of mathematical equations that portray understanding of a natural phenomenon.

X3.3.2.13 *sensitivity (model application)*—the degree to

TABLE X3.1 *Continued*

Description	Mathematical Approximation	Parameters
Vapor Emissions to Enclosed Spaces: Maximum vapor emission rate E_{max} [g/cm²-d] to enclosed spaces from subsurface vapor sources located a distance d [cm] away from the enclosed spaces	$E_{max} = Q_B C_{v,eq} \left(\frac{D^{eff} A_B}{Q_B d}\right) \exp\left(\frac{Q_{soil} L_{crack}}{D^{crack} A_{crack}}\right) \Big/ \left[\exp\left(\frac{Q_{soil} L_{crack}}{D^{crack} A_{crack}}\right) + \left(\frac{D^{eff} A_B}{Q_{soil} d}\right)\left(\exp\left(\frac{Q_{soil} L_{crack}}{D^{crack} A_{crack}}\right) - 1\right)\right]$	u_w = wind speed [cm/day] V_B = volume of enclosed space [cm³] W = width of impacted soil zone [cm] δ = height of breathing zone [cm]
Hydrocarbon Vapor Dispersion:		
Ambient hydrocarbon vapor concentration resulting from area vapor source $C_{outdoor}$ [g/cm³]	$C_{outdoor} = \frac{FL}{u_w \delta}$	
Enclosed space vapor concentration C_{indoor} [g/cm³]	$C_{indoor} = \frac{E_{max}}{V_B E_B}$	
Leachate Transport: *Leaching Impact on Ground Water:* Ground water source area concentration C_{source} [g/cm³-H_2O] resulting from leaching through vadose zone hydrocarbon-impacted soils	$C_{source} = C_{w,eq} \frac{q_i W}{(K_s i M + q_i W)}$	
Ground water source area concentraiton C_{source} [g/cm³-H_2O] resulting from hydrocarbon-impacted soils in direct contact with ground water	$C_{source} = C_{w,eq}$	

[A] Equation for this parameter given in this table.

TABLE X3.2 Reported Degradation Rates for Petroleum Hydrocarbons

Reference	Source of Data	Chemical Decay Rates (day⁻¹, [half-life days])							
		Benzene	Toluene	Ethyl-Benzene	Xylenes	O-Xylene	MTBE	Naphthalene	Benzo (a)Pyrene
Barker, et al[A]	Borden Aquifer, Canada	0.007 [99]	0.011 [63]	...	...	0.014 [50]	...	...	...
Kemblowski[B]	Eastern Florida Aquifer	0.0085 [82]	...	...	...	...	...	...	...
Chiang, et al[C]	Northern Michigan Aquifer	0.095 [7]	...	...	...	...	...	...	...
Wilson, et al[D]	Traverse City, MI Aquifer	0.007 to 0.024 [99] to [29]	0.067 [10]	...	0.004 to 0.014 [173] to [50]	...	...	...	...
Howard, et al[E]	Literature	0.0009 [730] to 0.069 [10]	0.025 [28] to 0.099 [7]	0.003 [228] to 0.116 [6]	0.0019 [365] to 0.0495 [14]	...	0.0019 [365] to 0.0666 [8]	0.0027 [255]	0.0007 [1058] to 0.0061 [114]

[A] See Ref (36).
[B] See Ref (37).
[C] See Ref (38).
[D] See Ref (39).
[E] See Ref (40).

which the model result is affected by changes in a selected model input representing fluid and media properties and boundary conditions.

X3.3.2.14 *simulation*—in migration modeling, one complete execution of a fluid flow modeling computer program, including input and output.

DISCUSSION—for the purposes of this appendix, a simulation refers to an individual modeling run. However, simulation is sometimes also used broadly to refer to the process of modeling in general.

X3.4 *Significance and Use:*

X3.4.1 Predictive modeling is significant in many phases of RBCA, including the following:

X3.4.1.1 Determining the potential urgency of response based on estimated migration and attenuation rates of compounds of concern,

X3.4.1.2 Determining the extent of corrective action based on estimated migration and attenuation rates of compounds of concern,

TABLE X3.3 Results of Exponential Regression for Concentration Versus Time[A]

Site	Compound	k, % per day
Campbell, CA[7]	benzene	1.20
	ethylbenzene	0.67
	xylene	1.12
	benzene	0.42
Palo Alto, CA	benzene	0.30
Virginia Beach, VA	PCE	0.46
	TCE	0.30
Montrose County, CO	benzene	0.42
Provo, UT	benzene	0.23
San Jose, CA	benzene	0.16
	benzene	0.10
Chemical facility	toluene	0.39
	PCE	0.34
	TCE	0.26

[A] Source: Ref (41).

X3.4.1.3 Establishing relationships between administered doses and adverse impacts to humans and sensitive environmental receptors, and

X3.4.1.4 Determining RBSLs concentrations at points of exposure.

X3.4.2 Examples of predictive modeling uses in the RBCA process include the following:

X3.4.2.1 The prediction of contaminant concentration distributions for future times based on historical trend data, as in the case of ground water transport modeling,

X3.4.2.2 The recommendation of sampling locations and sampling frequency based on current interpretation and future expectations of contaminant distributions, as in the design of ground water monitoring networks,

X3.4.2.3 The design of corrective action measures, as in the case of hydraulic control systems, and

X3.4.2.4 The calculation of site-specific exposure point concentrations based on assumed exposure scenarios, as in the case of direct exposure to surficial soils.

X3.4.3 Predictive modeling is not used in the RBCA process as a substitute for validation of site-specific data.

X3.5 *Interpretation of Predictive Modeling Results:*

X3.5.1 Predictive models are mathematical approximations of real processes, such as the movement of chemicals in the subsurface, the ingestion of chemicals contained in drinking water, and adverse impacts to human health and environmental resources resulting from significant exposures. One key step towards evaluating model results is to assess the accuracy and uncertainty, and to verify the model used.

X3.5.2 The accuracy of modeling-based predictions is evaluated using a post audit and is dependent upon a number of factors, including the following:

X3.5.2.1 The approximations used when describing the real system by mathematical expressions,

X3.5.2.2 The model setup, that is, the input parameters (for example, boundary conditions) used to generate the results, and

X3.5.2.3 The mathematical methods used to solve the governing equations (for example, user selection of numerical solution methods, expansion approximations, numerical parameters, and so forth).

X3.5.3 Predictive modeling results are always subject to some degree of uncertainty. It is important to quantify this uncertainty to properly interpret the results. Many times this is done with a sensitivity analysis in which the user identifies those parameters that most significantly influence the results. If most of all of the parameters do not produce "sensitivity," then the model may need to be reevaluated because it is possible that the key parameters are missing from the model.

X3.5.4 A postaudit may be performed to determine the accuracy of the predictions. While model calibration and verification demonstrate that the model accurately simulates past behavior of the system, the postaudit tests whether the model can predict future system behavior. Postaudits are normally performed several years after the initial assessment and corrective action.

X3.5.5 In the RBCA process, "conservative" is an important criterion of predictive modeling. In the initial evaluation, Tier 1, the most conservative approach, is used, which provides a worst case scenario for potential exposure and risk. Models that, because of their simplicity, neglect factors that yield conservative results are used. Input may include conservative values such as the USEPA RME values. When a more rigorous approach is warranted, such as in Tier 2 of the RBCA process, conservative values are often used, but in conjunction with a more reasonable case scenario. This level requires more specific information about the site and may involve the use of either simple or moderately complex mathematical models. It may involve the use of most likely exposure scenario (that is, USEPA MLE values). This information is used to set conservative corrective action objectives that are still regarded as overly protective. At some sites a comprehensive assessment is required (Tier 3) where SSTLs are determined using a site-specific transport and exposure model and, in some cases, parameter distributions. Tier 3 provides the most realistic evaluation of potential exposure and risk.

X3.6 *Types of Predictive Migration and Risk Assessment Models:*

X3.6.1 Predictive models typically used in the RBCA process can be grouped into two broad categories:

X3.6.1.1 Migration models, and

X3.6.1.2 Exposure, risk, and dose-response assessment models.

X3.6.2 The determination of Tier 1 RBSLs or Tiers 2 and 3 SSTLs generally involves the use of combinations of both types of models. A more detailed description of each type of model is given in X3.7 and X3.8.

X3.7 *Procedures for Predictive Migration Models:*

X3.7.1 Migration (fate and transport) models predict the movement of a petroleum release through soil, ground water, or air, or combination thereof, over time. Most models focus on specific phenomena (for example, ground water transport) and vary in complexity, depending on assumptions made during model development. In RBCA, simplistic screening-level migration models are utilized in Tiers 1 and 2, while more complex models are utilized in Tier 3.

X3.7.2 References to many simplistic models suitable for screening-level evaluations for a number of pathways relevant to hydrocarbon contaminant releases are listed in Table X3.1. Most of the screening-level migration models have a simple mathematical form and are based on multiple limiting assumptions rather than on actual phenomena. For example, a simple model is the use of estimated ground water flow velocity to assess the travel time between the leading edge of a dissolved hydrocarbon plume and a ground water well. The travel time is approximated by the following:

$$[\text{distance to well (ft)}/\text{flow velocity (ft/years)}] = \text{travel time (years)}$$

X3.7.2.1 In the case of a relatively light compound such as benzene dissolved in ground water, the flow velocity may best be equated with the ground water flow velocity. Heavier compounds such as naphthalene may be retarded so that a flow velocity lower than the ground water velocity may be used. If miscible liquids are present on the ground water surface, such as gasoline, the liquid flow velocity may actually exceed the ground water velocity.

X3.7.3 The use of more complex models is not precluded in the RBCA process; however, given limited data and assumptions that must be made, many complex numerical

models reduce to the analytical expressions given in Table X3.1.

X3.7.4 *Migration Model Data Requirements*—Predictive migration models require input of site-specific characteristics. Those most commonly required for various simplistic models include the following:

X3.7.4.1 Soil bulk density (for a typical soil: ≈ 1.7 g/cm^3),

X3.7.4.2 Total soil porosity (for a typical soil: ≈ 0.38 cm^3/cm^3),

X3.7.4.3 Soil moisture content can be conservatively estimated in many cases. It is approximately equal to the total soil porosity beneath the water table, and typically >0.05 cm^3-H_2O/cm^3-soil in the vadose zone; this can be a critical input parameter in the case of diffusion models and may require site-specific determination unless conservative values are used,

X3.7.4.4 Fraction organic matter in soil particles (=0.00d − 0.01: sandy soil is often conservatively assumed); this can also be a critical parameter requiring site-specific determination unless conservative values are used),

X3.7.4.5 Hydraulic conductivity (generally site-specific determination required),

X3.7.4.6 Ground water gradient and flow direction (requires site-specific determination), and

X3.7.4.7 First-order decay-rate (generally requires site-specific calibration as models are very sensitive to this parameter); see Tables X3.2 and X3.3 and Ref (41) for a summary of measured values currently available from the literature. The data in Table X3.3 include retardation and dispersion as well as natural biodegradation in attenuation rates measured. However, sensitivity studies indicate that natural biodegradation is the dominant factor. The sensitivity studies use Ref (42). According to these sensitivity studies, an order of magnitude increase in natural biodegradation rate is 3.5 times as effective as an order of magnitude increase in retardation and 12 times as effective as an order of magnitude increase in dispersion in attenuating concentration over distance. Therefore, approximately 80 % of the attenuation shown in the Ref (41) data can be attributed to natural biodegradation.

X3.7.4.8 A similar analysis of the sensitivity of attenuation parameters for the vapor transport pathway also indicates that natural biodegradation is the predominant attenuation mechanism (43). Soil geology is not considered an attenuation mechanism directly, but is a stronger determinant of how far contamination travels than even natural biodegradation. Gasoline contamination does not travel very far in clay (less than 30 ft (9 m)) according to the vapor transport model (43).

X3.7.5 Depending on the models selected, other information may be required, such as meteorological information (wind speed, precipitation, temperature), soil particle size distributions, and nearby building characteristics.

X3.7.6 In most cases, measurements of the attenuation (decrease in concentrations) of compounds with distance away from the contaminant source area will be required to calibrate and verify the predictive capabilities of the selected models. The amount of data required varies depending on the following:

X3.7.6.1 The model code used,

X3.7.6.2 The model's sensitivity to changes in input parameters, and

X3.7.6.3 The contribution of the pathway of concern to the total incremental exposure and risk.

X3.7.7 Generally, site-specific physical and chemical properties for the most sensitive parameters are required for migration models to obtain accurate results. However, instead of site-specific data, conservative values selected from the literature may be used with appropriate caution.

3.7.8 *Migration Modeling Procedure*—The procedure for applying a migration model includes the following steps: definition of study objectives, development of a conceptual model, selection of a computer code or algorithm, construction of the model, calibration of the model and performance of sensitivity analysis, making predictive simulations, documentation of the modeling process, and performing a postaudit. These steps are generally followed in order; however, there is substantial overlap between steps, and previous steps are often revisited as new concepts are explored or as new data are obtained. The iterative modeling approach may also require the reconceptualization of the problem. The basic modeling steps are discussed as follows.

X3.7.8.1. *Modeling Objectives*—Modeling objectives must first be identified (that is, the questions to be answered by the model). The objectives aid in determining the level of detail and accuracy required in the model simulation. Complete and detailed objectives would ideally be specified prior to any modeling activities. Objectives may include interpreting site characterization and monitoring data, predicting future migration, determining corrective action requirements, or predicting the effect of proposed corrective action measures.

X3.7.8.2 *Conceptual Model*—A conceptual model of a subsurface contaminant release, such as a hydrocarbon release from an underground tank, is an interpretation or working description of the characteristics and dynamics of the physical system. The purpose of the conceptual model is to consolidate site and regional data into a set of assumptions and concepts that can be evaluated quantitatively. Development of the conceptual model requires the collection and analysis of physical data pertinent to the system under investigation.

(*1*) The conceptual model identifies and describes important aspects of the physical system, including the following: geologic and hydrologic framework; media type (for example, fractured or porous); physical and chemical processes; and hydraulic, climatic, and vapor properties. The conceptual model is described in more detail for ground water flow systems in Guide D 5447.

(*2*) Provide an analysis of data deficiencies and potential sources of error with the conceptual model. The conceptual model usually contains areas of uncertainty due to the lack of field data. Identify these areas and their significance to the conceptual model evaluated with respect to project objectives.

X3.7.8.3 *Computer Code Selection*—Computer code selection is the process of choosing the appropriate software algorithm, or other analysis technique, capable of simulating the characteristics of the physical system, as identified in the conceptual model. The types of codes generally used in the RBCA process are analytical and numerical models. The selected code should be appropriate to fit the available data

and meet the modeling objectives. The computer code must also be tested for the intended use and be well documented.

(*1*) Analytical models are generally based on assumptions of uniform properties and regular geometries. Advantages include quick setup and execution. Disadvantages include, in many cases, that analytical models are so simplistic that important aspects of a given system are neglected.

(*2*) Numerical models allow for more complex heterogeneous systems with distributed properties and irregular geometries. Advantages include the flexibility to simulate more complex physical systems and natural parameter variability. Disadvantages include that the approach is often very time-intensive and may require much more data and information to be collected.

(*3*) Other factors may also be considered in the decision-making process, such as the model analyst's experience and those described as follows for model construction process; factors such as dimensionality will determine the capabilities of the computer code required for the model.

X3.7.8.4 *Model Construction*—Model construction is the process of transforming the conceptual model into a mathematical form. The model typically consists of two parts, the data set and the computer code. The model construction process includes building the data set used by the computer code. Fundamental components of a migration model are dimensionality, discretization, boundary and initial conditions, contaminant, and media properties.

X3.7.8.5 *Model Calibration*—Calibration of a model is the process of adjusting input for which data are not available within reasonable ranges to obtain a match between observed and simulated values. The range over which model parameters and boundary conditions may be varied is determined by data presented in the conceptual model. In the case where parameters are well characterized by field measurements, the range over which that parameter is varied in the model should be consistent with the range observed in the field. The degree of fit between model simulations and field measurements can be quantified using statistical techniques.

(*1*) In practice, model calibration is frequently accomplished through trial-and-error adjustment of the model's input data to match field observations. The calibration process continues until the degree of correspondence between the simulation and the physical system is consistent with the objectives of the project.

(*2*) Calibration of a model is evaluated through analysis of residuals. A residual is the difference between the observed and simulated variable. Statistical tests and illustrations showing the distribution of residuals are described for ground water flow models in Guide D 5490.

(*3*) Calibration of a model to a single set of field measurements does not guarantee a unique solution. To minimize the likelihood of nonuniqueness, the model should be tested to a different set of boundary conditions or stresses. This process is referred to as application verification. If there is poor correspondence to a second set of field data, then additional calibration or data collection are required. Successful verification of an application results in a higher degree of confidence in model predictions. A calibrated but unverified model may still be used to perform predictive simulations when coupled with a sensitivity analysis.

X3.7.8.6 *Sensitivity Analysis*—Sensitivity analysis is a quantitative method of determining the effect of parameter variation on model results. Two purposes of a sensitivity analysis are (*1*) to quantify the uncertainty in the calibrated model caused by uncertainty in the estimates of parameters, stresses, and boundary conditions, and (*2*) to identify the model inputs that have the most influence on model calibration and predictions.

(*1*) Sensitivity of a model parameter is often expressed as the relative rate of change of a selected model calculation during calibration with respect to that parameter. If a small change in the input parameter or boundary condition causes a significant change in the output, the model is sensitive to that parameter or boundary condition.

(*2*) Whether a given change in the model calibration is considered significant or insignificant is a matter of judgment. However, changes in the model's conclusions are usually able to be characterized objectively. For example, if a model is used to determine whether a contaminant is captured by a potable supply well, then the computed concentration is either detectable or not at the location. If, for some value of the input that is being varied, the model's conclusions are changed but the change in model calibration is insignificant, then the model results may be invalid because, over the range of that parameter in which the model can be considered calibrated, the conclusions of the model change. More information regarding conducting a sensitivity analysis for a ground water flow model application is presented in Guide D 5611.

X3.7.8.7 *Model Predictions*—Once these steps have been conducted, the model is used to satisfy the modeling objectives. Predictive simulations should be documented with appropriate illustrations, as necessary, in the model report.

X3.8 *Procedures for Risk, Exposure, and Dose-Response Assessment Models:*

X3.8.1 "Exposure models" are used to estimate the chemical uptake, or dose, while "risk assessment models" are used to relate human health or ecological impacts to the uptake of a chemical. Risk and exposure assessment models are often combined to calculate a target exposure point concentration of a compound in air, water, or soil.

X3.8.1.1 In the case of compounds that have been classified as carcinogens, exposure and risk assessment models are generally linked by the expression:

$$\textit{risk} = \textit{average lifetime intake}\ [\text{mg/kg-day}] \times \textit{slope factor}\ [\text{mg/kg-day}]^{-1}$$

where the intake depends on exposure parameters (ingestion rate, exposure duration, and so forth) and the concentration at point-of-exposure. The slope factor (sometimes called the "potency factor") is itself based on a model and set of underlying assumptions, which are discussed as follows.

X3.8.1.2 In the case of compounds that have not been classified as carcinogens, exposure and risk assessment models are generally linked by the expression:

$$\textit{hazard quotient} = \textit{average intake}\ [\text{mg/kg-day}]/\textit{reference dose}\ [\text{mg/kg-day}]$$

where the intake depends on exposure parameters (ingestion rate, exposure duration, and so forth) and the concentration at point-of-exposure. The reference dose is itself based on a

model and set of underlying assumptions, which are discussed as follows.

X3.8.2 *Toxicity Assessment: Dose-Response Models*—Toxicity assessments use dose-estimates of a "safe dose" or toxic level based on animal studies. In some instances, human epidemiological information is available on a chemical. Toxicologists generally make two assumptions about the effects of risk agents at the low concentrations typical of environmental exposures:

X3.8.2.1 Thresholds exist for most biological effects; in other words, for noncarcinogenic, nongenetic toxic effects, there are doses below which no adverse effects are observed in a population of exposed individuals, and

X3.8.2.2 No thresholds exist for genetic damage or incremental carcinogenic effects. Any level of exposure to the genotoxic or carcinogenic risk agent corresponds to some non-zero increase in the likelihood of inducing genotoxic or incremental carcinogenic effects.

X3.8.3 The first assumption is widely accepted in the scientific community and is supported by empirical evidence. The threshold value for a chemical is often called the NOAEL. Scientists usually estimate NOAELs from animal studies. An important value that typically results from a NOAEL or LOAEL value is the RfD. A reference dose is an estimate (with an uncertainty typically spanning an order of magnitude) of a daily exposure (mg/kg/day) to the general human population (including sensitive subgroups) that is likely to be without an appreciable risk of deleterious effects during a lifetime of exposure. The RfD value is derived from the NOAEL or LOAEL by application of uncertainty factors (UF) that reflect various types of data used to estimate RfDs and an additional modifying factor (MF), which is based on a professional judgment of the quality of the entire database of the chemical. The oral RfD, for example, is calculated from the following equation:

$$RfD = \frac{NOAEL}{(UF \times MF)}$$

X3.8.4 The second assumption regarding no threshold effects for genotoxic or carcinogenic agents is more controversial but has been adopted by the USEPA. For genotoxic and carcinogenic agents, extrapolations from high experimental doses to low doses of environmental significance require the use of mathematical models to general low dose-response curves. It should be noted that although the EPA uses the linear multi-state model to describe incremental carcinogenic effect, there is no general agreement in the scientific community that this is the appropriate model to use.

X3.8.5 The critical factor determined from the dose-response curve is the slope factor (SF), which is the slope of the dose-response curve in the low-dose region. The units of the slope factor are expressed as $(mg/kg\text{-}day)^{-1}$ and relate a given environmental intake to the risk of additional incidence of cancer above background.

X3.8.6 The RfD or SF values are generally obtained from a standard set of reference tables (for example, Ref (2) or Ref (3)). It is important to note that the information in IRIS has typically only been peer-reviewed within the EPA and may not always have support from the external scientific community. Whereas the information in IRIS has been subject to agency-wide data quality review, the information in the HEAST tables has not. The user is expected to consult the original assessment documents to appreciate the strengths and limitations of the data in HEAST. Thus, care should be exercised in using the values in HEAST. Some state and local agencies have toxicity factors they have derived themselves or preferences for factors to use if neither IRIS nor HEAST lists a value. Values for a range of hydrocarbons typically of interest are presented in Table X3.1.

X3.8.7 It is important to note that in extrapolating the information obtained in animal studies to humans, a number of conservative assumptions are made.

X3.8.7.1 For noncarcinogens, an arbitrary system of default safety and uncertainty factors, as discussed (in multiples of ten), is used to convert observations, in animals to estimates in humans.

X3.8.7.2 For carcinogens, some of the most important assumptions include: (*1*) the results of the most sensitive animal study are used to extrapolate to humans, (*2*) in general, chemicals with any incremental carcinogenic activity in animals are assumed to be potential human carcinogens, and (*3*) no threshold exists for carcinogens.

X3.8.8 The uncertainty in the RfD and SF values are often neglected in deference to single point values which are then typically summarized in databases such as IRIS and HEAST and assumptions described are risk management policy decisions made by the USEPA. These assumptions are not explicitly defined and further obscure the conservatism in the safe dose estimate. Thus, care must be exercised in interpreting results which have as a basis these conservative toxicity evaluations.

X3.8.9 *Exposure Assessment Modeling*—The goal of exposure assessment modeling is to estimate the chemical uptake that occurs when a receptor is exposed to compounds present in their environment. In principal, the process for developing and using migration models presented in X3.7 is directly applicable to exposure assessment modeling. In this case the user:

X3.8.9.1 Develops a conceptual model by identifying significant exposure pathways and receptors,

X3.8.9.2 Selects a model to describe the contact rate and subsequent uptake of the chemical(s),

X3.8.9.3 Performs a sensitivity analysis to identify critical parameters,

X3.8.9.4 Selects appropriate exposure parameters (breathing rates, and so forth),

X3.8.9.5 Generates estimates of exposure and uptake, and

X3.8.9.6 Assesses the uncertainty in the estimates.

X3.8.10 There are differences between the process outlined in X3.7 and that which can be practically applied to exposure assessment modeling. For example, with the exception of exposures and impacts to environmental resources, it is difficult to calibrate exposure assessment models unless very expensive epidemiological studies are conducted.

X3.8.11 Typically, the models used to estimate uptake are simplistic algebraic expressions, such as those contained in Ref (27). Application of these equations is illustrated in Appendix X2.

X3.8.12 In many cases, exposure parameter values are available in Ref (27), but other more recent information is also available in peer-reviewed publications, and all sources

should be carefully reviewed. While point values are often selected for simplicity, statistical distributions for many of the exposure parameters are readily available for Tier 3 analyses.

X3.8.13 It is common for USEPA RME values to be used in exposure assessment calculation, as is done for the example Tier 1 Look-Up Table discussed in Appendix X2. The RME value is generally defined as a statistical upper limit of available data (generally 85 to 90 % of all values are less than the RME value). Therefore, by consistently selecting and multiplying conservative RME values the user models a scenario that is very improbable and always more conservative than the "true" RME exposure scenario. Thus, great care must be exercised, when using combinations of these default values in risk assessments, to avoid a gross overestimation of exposure for a specific site.

X3.9 *Report*—The purpose of the model report is to communicate findings, to document the procedures and assumptions inherent in the study, and to provide detailed information for peer review. The report should be a complete document allowing reviewers and decision makers to formulate their own opinion as to the credibility of the model. The report should describe all aspects of the modeling study outlined in this appendix.

X4. INSTITUTIONAL CONTROLS

X4.1 *Introduction:*

X4.1.1 The purpose of this appendix is to provide a review of generally used institutional controls. For purposes of this appendix, "institutional controls" are those controls that can be used by responsible parties and regulatory agencies in remedial programs where, as a part of the program, certain concentrations of the chemical(s) of concern will remain on site in soil or ground water, or both. Referenced in this appendix are examples of programs from California, Connecticut, Illinois, Indiana, Iowa, Massachusetts, Michigan, Missouri, and New Jersey. In addition, federal programs, such as Superfund settlements and RCRA closure plans have used the following techniques described for some years as a mechanism to ensure that exposure to remaining concentrations of chemical(s) of concern is reduced to the degree necessary.

X4.1.2 The types of institutional controls discussed in this appendix are as follows:

X4.1.2.1 Deed restrictions, or restrictive covenants,

X4.1.2.2 Use restrictions (including well restriction areas),

X4.1.2.3 Access controls,

X4.1.2.4 Notice, including record notice, actual notice, and notice to government authorities,

X4.1.2.5 Registry act requirements,

X4.1.2.6 Transfer act requirements, and

X4.1.2.7 Contractual obligations.

X4.1.3 Institutional controls for environmental remedial programs vary in both form and content. Agencies and landowners can invoke various authorities and enforcement mechanisms, both public and private, to implement any one or a combination of the controls. For example, a state could adopt a statutory mandate (see X4.2) requiring the use of deed restrictions (see X4.3) as a way of enforcing use restrictions (see X4.4) and posting signage (a type of access control, see X4.5). Thus, the institutional controls listed as follows are often used as overlapping strategies, and this blurs the distinctions between them.

X4.2 *Statutory Mandates*—Some states' emergency response programs mandate post-remediation institutional controls and impose civil penalties for noncompliance. The schemes vary from state to state, but all impose obligations on landowners to use one or more institutional controls listed in this appendix.

X4.3 *Deed Restrictions:*

X4.3.1 Deed restrictions place limits and conditions on the use and conveyance of land. They serve two purposes: (*1*) informing prospective owners and tenants of the environmental status of the property and (*2*) ensuring long-term compliance with the institutional controls that are necessary to maintain the integrity of the remedial action over time. Restraining the way someone can use their land runs counter to the basic assumptions of real estate law, so certain legal rules must be satisfied in order to make a deed restriction binding and enforceable.

X4.3.2 There are four requirements for a promise in a deed restriction (also called a "restrictive covenant") to be held against current and subsequent landowners: (*1*) a writing, (*2*) intention by both original parties that particular restrictions be placed on the land in perpetuity, (*3*) "privity of estate," and (*4*) that the restrictions "touch and concern the land."

X4.3.2.1 The first requirement is that of a writing. It is a rule of law that conveyances of land must be documented in a writing. The same rule holds for deed restrictions affecting land. Ideally, a deed restriction used as an institutional control would be written down with particularity and then recorded in the local land records office, in much the same fashion as the documentation and recordation of a sale of land. Parties may also encounter the requirement that the deed restriction be executed "under seal," a legal formality that has been abandoned in most states.

X4.3.2.2 The second requirement is that the deed restriction should precisely reflect what the parties' intentions are in regard to the scope and the duration of the restrictions. Explicitly stating in the deed restriction that the parties intend the restriction to "run with the land" (that is, last forever and bind subsequent owners) is strongly recommended.

X4.3.2.3 The third requirement, privity of estate, arises from a concern that only persons with a certain relationship to the land should be able to enforce a deed restriction. Normally, deed restrictions are promises between the buyer and the seller or between neighbors; therefore, the state or a third party may not enforce a deed restriction. However, even in states that require privity of estate, this concern is addressed if the landowner took the land with knowledge that the restrictions existed and might be enforced by these third parties. Thus, it is also strongly recommended that the deed

restriction explicitly state that the state environmental authority may enforce the restriction. Recording of the deed restriction serves as notice to anyone who later purchases or acquires an interest in the land. Therefore, privity of estate should not be a barrier to state enforcement of the deed restriction if the proper steps are taken.

X4.3.2.4 Finally, a deed restriction is only enforceable if the promise "touches and concerns the land." A rough rule of thumb to decide this point is whether the landowner's legal interest in the land is decreased in value due to the deed restriction. If the land is devalued in this way, then the restriction could be said to "touch and concern the land." Note that the focus of the inquiry is on the land itself; promises that are personal in nature and merely concern human activities that happen to take place on the land are least likely to be enforceable. Thus, any deed restriction used as an institutional control should be written so that it centers on the land and the use of the land.

X4.3.3 Due to the potential enforcement hurdles encountered by a governmental agency in enforcing a deed restriction, it may be appropriate for an individual state to seek statutory and regulatory amendments to ensure that such authority exits in regard to all deed restrictions for environmental purposes.

X4.3.4 Remedies for noncompliance with deed restrictions comes in two forms: (*1*) persons or agencies may sue to obtain a court order (injunction) requiring compliance or (*2*) if the state statute allows for it, the state's attorney general can seek enforcement of civil penalties, such as fines, for noncompliance.

X4.3.5 A state program can require a landowner to continue monitoring activities and to allow state environmental officials access to the site to monitor compliance with institutional controls. These arrangements may have to be put in a deed restriction in order to run with the land from owner to owner, but responsible parties can also be required to sign a contract making these promises. Of course, almost every state has authority to issue administrative orders to accomplish some or all of these arrangements.

X4.3.6 The preceding arrangements can also set out procedures that will be followed if some emergency requires that the remediation site be disturbed. If, for example, underground utility lines must be repaired, the landowner would follow this protocol for handling the soil and alerting the state authority.

X4.4 *Use Restrictions:*

X4.4.1 Use restrictions are usually the heart of what is in a deed restriction. Use restrictions describe appropriate and inappropriate uses of the property in an effort to perpetuate the benefits of the remedial action and ensure property use that is consistent with the applicable cleanup standard. Such techniques also prohibit any person from making any use of the site in a manner that creates an unacceptable risk of human or environmental exposure to the residual concentrations of chemical(s) of concern.

X4.4.2 Use restrictions address uses that may disturb a containment cap or any unremediated soils under the surface or below a building. A prohibition on drinking on-site (or off-site by means of well restriction areas discussed as follows) ground water may also be appropriate.

X4.4.3 As an example, a program may allow a restriction of record to include one or more of the following:

X4.4.3.1 Restriction on property use;

X4.4.3.2 Conditioning the change of use from nonresidential on compliance with all applicable cleanup standards for a residential property;

X4.4.3.3 Restricting access; or

X4.4.3.4 Restricting disturbance of department-approved remedial effects.

X4.4.4 Well restriction areas can be a form of institutional control by providing notice of the existence of chemical(s) of concern in ground water, and by prohibiting or conditioning the construction of wells in that area.

X4.4.4.1 This technique preserves the integrity of any ground water remedial action by prohibiting or conditioning the placement and use of any or all types of wells within the area.

X4.4.4.2 Well restrictions of this nature would be subject to agency approval and public notice, and may include the restriction on constructing or locating any wells within a particular designated area. Notice of the well restriction is recorded on the land records and with various health officials and municipal officials. The restrictions can only be released upon a showing that the concentrations of the chemical(s) of concern in the well restriction area is remediated in accordance with state standards.

X4.5 *Access Controls:*

X4.5.1 Another subset of institutional controls is the control of access to any particular site. The state uses the following criteria to determine the appropriate level and means of access control:

X4.5.1.1 Whether the site is located in a residential or mixed use neighborhood;

X4.5.1.2 Proximity to sensitive land-use areas including day-care centers, playgrounds, and schools; and

X4.5.1.3 Whether the site is frequently traversed by neighbors.

X4.5.2 Access can be controlled by any of the following: fencing and gates, security, or postings or warnings.

X4.6 *Notice*—Regulations of this type generally provide notice of specific location of chemical(s) of concern on the site, and disclose any restrictions on access, use, and development of part or all of the contaminated site to preserve the integrity of the remedial action.

X4.6.2 *Record Notice:*

X4.6.2.1 Some states require that sites having releases of hazardous waste file a notice on the land records providing to any subsequent purchaser of the property information regarding the past or current activities on the site.

X4.6.2.2 The record notice requirement may be broad; the program may require any property subject to a response action to obtain a professional opinion and then prepare and record a Grant of Environmental Restriction that is supported by that opinion.

X4.6.2.3 The record notice requirement can be ancillary to a transfer act (see X4.8), in which case recording of an environmental statement is only required in conjunction with a land transaction.

X4.6.3 *Actual Notice:*

X4.6.3.1 States may require direct notice of environmental information to other parties to a land transaction.

These laws protect potential buyers and tenants, and they also help ensure that use restrictions and other institutional controls are perpetuated.

X4.6.3.2 Actual notice of an environmental defect or failure to provide notice may give a party the right to cancel the transaction and result in civil penalties. For example, landlords and sellers who do not give notice as required by the state may be liable for actual damages plus fines. Nonresidential tenants who fail to notify landowners of suspected or actual hazardous substance releases can have their leases canceled and are subject to fines.

X4.6.4 *Notice to Government Authorities*—Parties to a land transaction may also be required to file the environmental statement with various environmental authorities. Notice to the government may be required before the transaction takes place.

X4.7 *Registry Act Requirements:*

X4.7.1 Some states have registry act programs that provide for the maintenance of a registry of hazardous waste disposal sites and the restriction of the use and transfer of listed sites.

X4.7.2 A typical registry act provides that the state environmental agency establish and maintain a registry of all real property which has been used for hazardous substance disposal either illegally or before regulation of hazardous waste disposal began in that state.

X4.7.3 The state agency is responsible for investigating potential sites for inclusion on the registry. The registry includes the location of the site and a listing of the hazardous wastes on the property, and may also include a classification of the level of health or environmental danger presented by the conditions on the property. The state agency may be required to perform detailed inspections of the site to determine its priority relative to other registered sites.

X4.7.4 Owners of sites proposed for inclusion on the registry have rights of hearing and appeal, and owners of sites on the registry have rights to modify or terminate their listing. In some cases, the owner of a site proposed for inclusion on the registry may obtain the withdrawal of the proposed registration by entering into a consent agreement with the state. Such a consent agreement establishes a timetable and responsibility for remedial action.

X4.7.5 When a site appears on the state registry, the owner must comply with regulatory requirements in regard to use and transfer of the site. The use of a site listed on the registry may not be changed without permission of the state agency. In negotiations for a conveyance of a registered site, the owner may be obligated to disclose the registration early in the process, and permission of the state agency may be required to convey a registered property. Under other schemes, permission to convey is not required, but the seller must notify the state agency of the transaction.

X4.7.6 Finally, registry acts require that the listing of a property on a hazardous materials site registry be recorded in the records of the appropriate locality so that the registration will appear in the chain of title.

X4.8 *Transfer Act Requirements:*

X4.8.1 Some states have transfer act programs that require full evaluation of all environmental issues before or after the transfer occurs. It may be that within such program, institutional controls can be established by way of consent order, administrative order, or some other technique that establishes implementation and continued responsibility for institutional controls.

X4.8.2 A typical transfer act imposes obligations and confers rights on parties to a land transaction arising out of the environmental status of the property to be conveyed. Transfer acts impose information obligations on the seller or lessor of a property (see X4.6.3). That party must disclose general information about strict liability for cleanup costs as well as property-specific information, such as presence of hazardous substances, permitting requirements and status, releases, and enforcement actions and variances.

X4.8.3 Compliance with transfer act obligations in the manner prescribed is crucial for ensuring a successful conveyance. Sometimes the transfer act operates to render a transaction voidable before the transfer occurs. Failure to give notice in the required form and within the time period required or the revelation of an environmental violation or unremediated condition will relieve the transferee and the lender of any obligation to close the transaction, even if a contract has already been executed. Moreover, violation of the transfer act can be the basis for a lawsuit to recover consequential damages.

X4.9 *Contractual Obligations:*

X4.9.1 One system for ensuring the future restriction on use of a site, or the obligation to remediate a site, is to require private parties to restrict use by contract. While this method is often negotiated among private parties, it will be difficult, if not impossible, to institutionalize some control over that process without interfering with the abilities and rights of private parties to freely negotiate these liabilities.

X4.9.2 Another avenue is for the landowner or responsible party to obligate itself to the state by contract. The state may require a contractual commitment from the party to provide long-term monitoring of the site, use restrictions, and means of continued funding for remediation.

X4.10 *Continued Financial Responsibility*—Another aspect of institutional controls is the establishment of financial mechanisms by which a responsible party ensures continued funding of remediation measures and assurance to the satisfaction of the state.

X4.11 *References:*

X4.11.1 The following references serve as examples and are current as of the fourth quarter of 1993:

X4.11.1.1 *References for Deed Restrictions:*

24 New Jersey Regulations 400 (1992) (New Jersey Administration Code § 7.26D-8.2 (c) (2))
24 New Jersey Regulations 400-02 (1992) (New Jersey Administration Code §§ 7.26D-8.1–8.4)
24 New Jersey Regulations 401 (1992) (New Jersey Administration Code § 7.26D Appendix A, Model Document, Declaration of Environmental Restrictions and Grant of Ease ment, Item 8)
Illinois Responsible Property Transfer Act § 7(c) (1985)
Massachusetts Regulations Code Title _____ § 40.1071 (2) (1) & (k)
Massachusetts Regulations Code, Title _____ § 40.1071(4)
Michigan Administration Code 299.5719 (3) (e) (1990)
Michigan Rules 299.5719 (2), (3) (d)

X4.11.1.2 *References for Use Restrictions:*

24 New Jersey Regulations 400 (New Jersey Administration Code § 7.26D-8.2 (d))
Michigan Administration Code 299.5719 (3) (a), (b), (g)
New Jersey Regulation 7.26D-8.4

X4.11.1.3 *References for Access Controls:*

Iowa Administration Code r. 133.4 (2) (b)
Michigan Rule 299.4719 (3) (f)
New Jersey Regulations § 7.26D-8.2

X4.11.1.4 *References for Notice:*

California Health and Safety Code § 25359.7 (1981)
Illinois Responsible Property Transfer Act (1985)
Indiana Code §§13-7-22.5-1–22 (1989) ("Indiana Environmental Hazardous Disclosure and Responsible Party Transfer Law")
Massachusetts Regulations Code Title _____ §§ 40.1071-1090 (1993)
Michigan Rule 299.5719 (3) (c)

X4.11.1.5 *References for Registry Act Requirements:*

Iowa Code Ann. §§ 455B.426–455B.432, 455B.411 (1) (1990)
Missouri Code Regulations Title 10, §§ 25-10.010, 25-3.260 (1993)

X4.11.1.6 *References for Transfer Act Requirements:*

Connecticut General Stat. §22a-134 *et seq*
Illinois Responsible Property Transfer Act (1985)
Indiana Code §§ 13-7-22.5-1–22 (1989) ("Indiana Environmental Hazardous Disclosure and Responsible Party Transfer Law")
New Jersey Senate Bill No. 1070, the Industrial Site Recovery Act, amending the environmental cleanup Responsibility Act, N.J.S.A. 13:1K-6 *et seq*
New Jersey Spill Compensation and Control Act, N.J.S.A. 58:10-23.11 *et seq*

X4.11.1.7 *Reference for Contractual Obligations:*

Michigan Rule 299.5719 (2)

X4.11.1.8 *Reference for Continued Financial Responsibility:*

Michigan Rule 299.5719 (2)

X5. EXAMPLE APPLICATIONS OF RISK-BASED CORRECTIVE ACTION

X5.1 *Introduction*—The following examples illustrate the use of RBCA at petroleum release sites. The examples are hypothetical and have been simplified in order to illustrate that RBCA leads to reasonable and protective decisions: nevertheless, they do reflect conditions commonly encountered in practice.

X5.2 *Example 1—Corrective Action Based on Tier 1 Risk-Based Screening Levels:*

X5.2.1 *Scenario*—A release from the underground storage tank (UST), piping, and dispenser system at a service station is discovered during a real estate divestment assessment. It is known that there are petroleum-impacted surficial soils in the area of the tank fill ports; however, the extent to which the soils are impacted is unknown. In the past, both gasoline and diesel have been sold at the facility. The new owner plans to continue operating the service station facility.

X5.2.2 *Site Assessment*—The responsible party completes an initial site assessment focussed on potential source areas (for example, tanks, lines, dispensers) and receptors. Based on historical knowledge that gasoline and diesel have been dispensed at this facility, chemical analyses of soil and ground water are limited to benzene, toluene, ethylbenzene, xylenes, and naphthalene. Site assessment results are summarized as follows:

X5.2.2.1 Field screening instruments and laboratory analyses indicate that the extent of petroleum-impacted soils is confined to the vicinity of the fill ports for the tanks. A tank and line test reveals no leaks; therefore, evidence suggests that soils are impacted due to spills and overfills associated with filling the storage tank,

X5.2.2.2 The current tanks and piping were installed five years ago,

X5.2.2.3 The concrete driveway is highly fractured,

X5.2.2.4 No other sources are present,

X5.2.2.5 The site is underlain by layers of fine to silty sands,

X5.2.2.6 Ground water, which is first encountered at 32 ft (9.7 m) below ground surface, is not impacted,

X5.2.2.7 Maximum depth at which hydrocarbons are detected is 13 ft (3.9 m). Maximum detected soil concentrations are as follows:

Compound	Depth Below Ground Surface, ft (m)	Concentration, mg/kg
Benzene	8 (2.4)	10
Ethylbenzene	4 (1.2)	4
Toluene	6.5 (1.9)	55
Xylenes	3.5 (1.01)	38
Naphthalene	2 (0.6)	17

X5.2.2.8 A receptor survey indicates that two domestic water wells are located within 900 ft (273.6 m) of the source area. One well is located 500 ft (152.4 m) hydraulically down-gradient from the impacted soil zone, the other well is hydraulically up-gradient. Both wells produce water from the first encountered ground water zone.

X5.2.3 *Site Classification and Initial Response Action*—Based on classification scenarios given in Table 1, this site is classified as a Class 3 site because conditions are such that, at worst, it is a long-term threat to human health and environmental resources. The appropriate initial response is to evaluate the need for a ground water monitoring program. At most, this would consist of a single well located immediately down-gradient of the impacted petroleum soils. The responsible party recommends deferring the decision to install a ground water monitoring system until the Tier 1 evaluation is complete, and justifies this recommendation based on no detected ground water impact, the limited extent of impacted soils, and the separation between impacted soils and first-encountered ground water. The regulatory agency concurs with this decision.

X5.2.4 *Development of Tier 1 Look-Up Table of Risk-Based Screening Level (RBSL)*—Assumptions used to derive example Tier 1 RBSL Look-Up Table X2.1 in Appendix X2 are reviewed and presumed valid for this site. A comparison of RBSLs for both pathways of concern indicates that RBSLs associated with the leaching pathway are the most restrictive of the two. As this aquifer is currently being used as a drinking water supply, RBSL values based on meeting drinking water MCLs are selected. In the case of naphthalene, for which there is no MCL, the RBSL value corresponding to a residential scenario and a hazard quotient of unity is used.

X5.2.5 *Exposure Pathway Evaluation*—Based on current and projected future use, the only two potential complete exposure pathways at this site are: (*1*) the inhalation of ambient vapors by on-site workers, or (*2*) the leaching to ground water, ground water transport to the down-gradient drinking-water well, and ingestion of ground water (see Fig. X5.1).

X5.2.6 *Comparison of Site Conditions With Tier 1 RBSLs*—Based on the data given in X5.2.3.7 and the RBSLs given in Look-Up Table X2.1 in Appendix X2, exceedences of Tier 1 RBSLs are noted only for benzene and toluene.

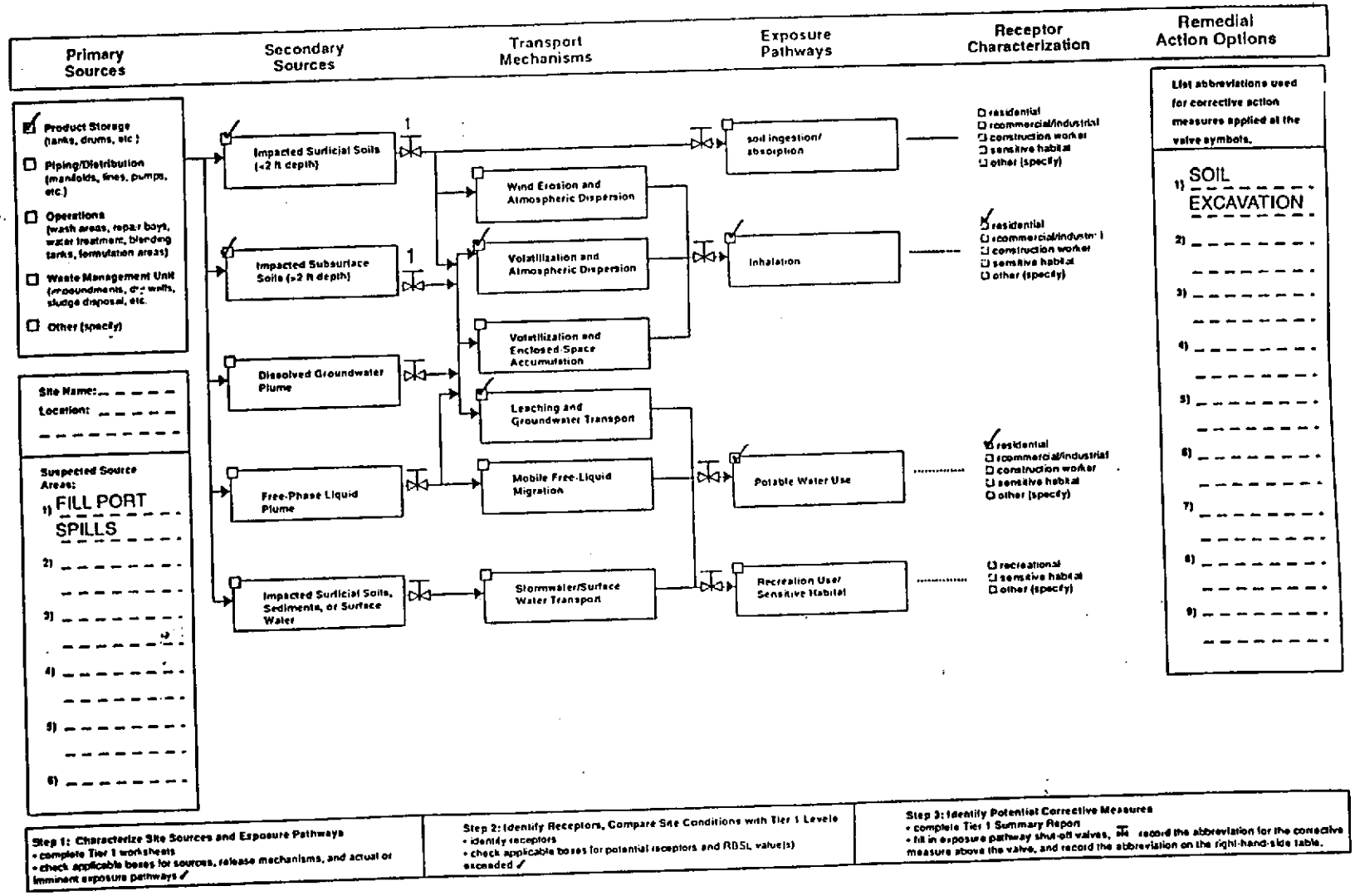


FIG. X5.1 Example 1—Exposure Evaluation Flowchart

X5.2.7 *Evaluation of Tier 1 Results*—The responsible party decides to devise a corrective action plan to meet Tier 1 standards after considering the following factors:

X5.2.7.1 The shallow aquifer is not yet affected,

X5.2.7.2 Quick (relative to rate of chemical migration) removal of the source will eliminate the need for ground water monitoring,

X5.2.7.3 The new owner plans to install new tanks within six months,

X5.2.7.4 Limited excavation of soils to meet Tier 1 criteria could be performed quickly and inexpensively when the tanks are removed, relative to the cost of proceeding to a Tier 2 analysis, and

X5.2.7.5 An excavation proposal will facilitate the real estate deal.

X5.2.8 *Tier 1 Remedial Action Evaluation*—Excavate all impacted soils with concentrations above the Tier 1 RBSLs when the current tanks are replaced. Subsequently resurface the area with new concrete pavement to reduce future infiltration and leaching potential through any remaining impacted soils. It is agreed that ground water monitoring is not necessary and the governing regulatory agency agrees to issue a No Further Action and Closure letter following implementation of the corrective action plan.

X5.3 *Example 2—RBCA Based on Tier 2 Evaluation:*

X5.3.1 *Scenario*—During the installation of new double-contained product transfer lines, petroleum-impacted soils are discovered in the vicinity of a gasoline dispenser at a service station located close to downtown Metropolis. In the past, both gasoline and diesel have been sold at this facility, which has been operating as a service station for more than twenty years.

X5.3.2 *Site Assessment*—The owner completes an initial site assessment focussed on potential source areas (for example, tanks, lines, dispensers) and receptors. Based on historical knowledge that gasoline and diesel have been dispensed at this facility, chemical analyses of soil and ground water are limited to benzene, toluene, ethylbenzene, xylenes, and naphthalene. Results of the site investigation are as follows:

X5.3.2.1 The extent of petroleum-impacted soils is confined to the vicinity of the tanks and dispensers. A recent tank and line test revealed no leaks; therefore, evidence suggests that the releases occurred sometime in the past,

X5.3.2.2 The current tanks, lines, and dispensers were installed three years ago,

X5.3.2.3 The asphalt driveway is competent and not cracked,

X5.3.2.4 Another service station is located hydraulically down gradient, diagonally across the intersection,

X5.3.2.5 The site is underlain by silty sands with a few thin discontinuous clay layers,

X5.3.2.6 Ground water, which is first encountered at 32 ft (9.7 m) below ground surface, is impacted, with highest dissolved concentrations observed beneath the suspected source areas. Dissolved concentrations decrease in all directions away from the source areas, and ground water samples taken hydraulically down gradient from a well located in the center divider of the street (about 100 ft (30.4 m) from the source area) do not contain any detectable levels of dissolved hydrocarbons,

X5.3.2.7 Ground water flow gradient is very shallow, and ground water flow velocities are at most tens of feet per year,

X5.3.2.8 Ground water yield from this aquifer is estimated to be in excess of 5 gal/min (18.9 L/min), and total dissolved solids levels are less than 700 mg/L. Based on this information, this aquifer is considered to be a potential drinking water supply,

X5.3.2.9 A shallow soil gas survey indicates that no detectable levels of hydrocarbon vapors are found in the utility easement running along the southern border of the property, or in soils surrounding the service station kiosk,

X5.3.2.10 Impacted soils extend down to the first encountered ground water. Maximum concentrations detected in soil and ground water are as follows:

Compound	Soil, mg/kg	Ground water, mg/L
Benzene	20	2
Ethylbenzene	4	0.5
Toluene	120	5
Xylenes	100	5.0
Napthalene	2	0.05

X5.3.2.11 A receptor survey indicates that no domestic water wells are located within one-half mile of the site; however, there is an older residential neighborhood located 1200 ft (365.7 m) hydraulically down gradient of the site. Land use in the immediate vicinity is light commercial (for example, strip malls). The site is bordered by two streets and a strip mall parking lot.

X5.3.3 *Site Classification and Initial Response Action*—Based on classification scenarios given in Table 1, this site is classified as a Class 3 site because conditions are such that, at worst, it is a long-term threat to human health and environmental resources. The appropriate initial response is to evaluate the need for a ground water monitoring program. The owner proposes that the ground water monitoring well located hydraulically down gradient in the street divider be used as a sentinel well, and be sampled yearly. The regulatory agency concurs, provided that the well be sampled every six months.

X5.3.4 *Development of Tier 1 Look-Up Table of Risk-Based Screening Level (RBSL) Selection*—Assumptions used to derive example Tier 1 RBSL Look-Up Table X2.1 in Appendix X2 are reviewed and presumed valid for this site. Due to the very low probability of the exposure pathway actually being completed in the future, MCLs are not used and the site owner is able to negotiate Tier 1 RBSLs based on a 10^{-5} risk to human health for carcinogens and hazard quotients equal to unity for the noncarcinogens (based on ground water ingestion).

X5.3.5 *Exposure Pathway Evaluation*—Based on current and projected future use, and the soil gas survey results, there are no potential complete exposure pathways at this site. The down gradient residential neighborhood is connected to a public water supply system, and there is no local use of the impacted aquifer. However, being concerned about future uncontrolled use of the aquifer, the regulatory agency requests that the owner evaluate the ground water transport to residential drinking water ingestion pathway, recognizing that there is a low potential for this to occur (see Fig. X5.2).

X5.3.6 *Comparison of Site Conditions With Tier 1 RBSLs*—Based on the data given in X5.3.2.10 and the RBSLs given in example Look-Up Table X2.1 in Appendix X2,

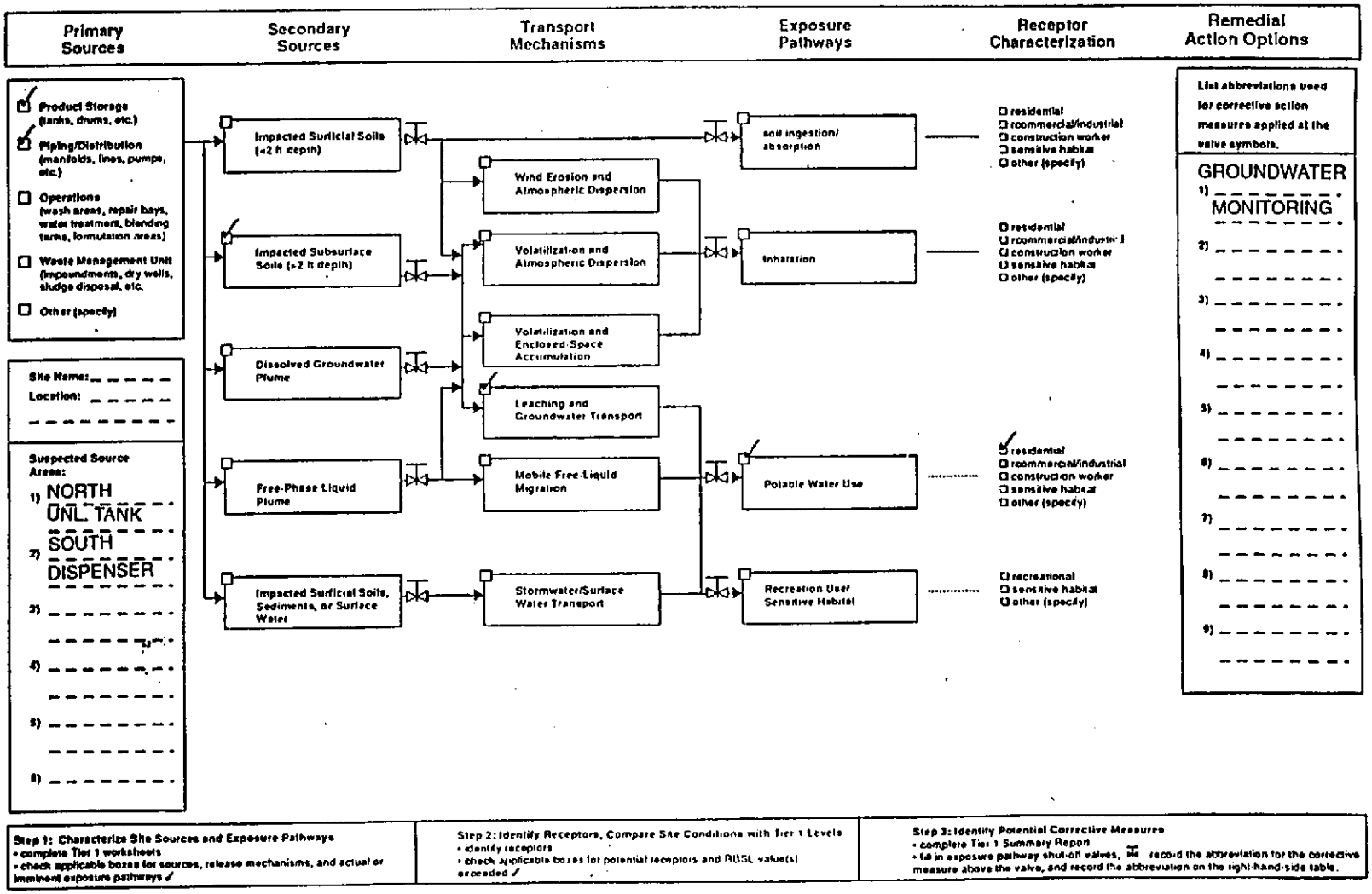


FIG. X5.2 Example 2—Exposure Evaluation Flowchart

exceedences of Tier 1 soil and ground water RBSLs are noted only for benzene.

X5.3.7 *Evaluation of Tier 1 Results*—The responsible party decides to proceed to a Tier 2 evaluation for benzene and the pathway of concern, rather than devise a corrective action plan to meet Tier 1 standards after considering the following factors:

X5.3.7.1 The shallow aquifer is impacted, but the dissolved plume appears to be stable and ground water movement is very slow,

X5.3.7.2 Excavation of soils to meet Tier 1 criteria would be expensive, due to the depth of impacted soils. Excavation would shut down the facility, and require all tanks and new lines to be removed and reinstalled,

X5.3.7.3 Costs for application of other conventional treatment methods, such as vapor extraction and pump and treat, are estimated to exceed $300 000 over the life of the remediation, and

X5.3.7.4 A tier 2 analysis for this site is estimated to require minimal additional data, and is anticipated to result in equally protective, but less costly corrective action.

X5.3.8 *Tier 2 Evaluation*—The owner collects additional ground water monitoring data and verifies that:

X5.3.8.1 No mobile free-phase product is present,

X5.3.8.2 The dissolved plume is stable and ground water concentrations appear to be decreasing with time,

X5.3.8.3 Extent of the dissolved plume is limited to within 50 ft (15.2 m) of the property boundaries,

X5.3.8.4 Dissolved oxygen concentrations are higher outside of the dissolved plume, indicating some level of aerobic biodegradation,

X5.3.8.5 Ground water movement is less than 50 ft/year (15.2 m), and

X5.3.8.6 Simple ground water transport modeling indicates that observations are consistent with expectations for the site conditions.

X5.3.9 *Remedial Action Evaluation*—Based on the demonstration of dissolved plume attenuation with distance, the owner negotiates a corrective action plan based on the following: (*1*) compliance with the Tier 1 RBSLs at the monitoring well located in the street center divider, provided that deed restrictions are enacted to prevent the use of ground water within that zone until dissolved levels decrease below drinking water MCLs, (*2*) deed restrictions are enacted to ensure that site land use will not change significantly, (*3*) continued sampling of the sentinel/compliance ground water monitoring well on a yearly basis, (*4*) should levels exceed Tier 1 RBSLs at that point for any time in the future, the corrective action plan will have to be revised, and (*5*) closure will be granted if dissolved conditions remain stable or decrease for the next two years.

X5.4 *Example 3—RBCA With Emergency Response and In Situ Remediation:*

X5.4.1 *Scenario*—A 5 000-gal (18 925-L) release of super unleaded gasoline occurs from a single-walled tank after repeated manual gaging with a gage stick. Soils are sandy at this site, ground water is shallow, and free-product is observed in a nearby monitoring well within 24 h. The site is located next to an apartment building that has a basement where coin-operated washers and dryers are located for use by the tenants.

X5.4.2 *Site Assessment*—In this case the initial site assessment is conducted rapidly and is focussed towards identifying if immediately hazardous conditions exist. It is known from local geological assessments that the first encountered ground water is not potable, as it is only about 2 ft (0.6 m) thick and is perched on a clay aquitard. Ground water monitoring wells in the area (from previous assessment work) are periodically inspected for the appearance of floating product, and vapor concentrations in the on-site utility corridors are analyzed with an explosimeter. While this flurry of activity begins, a tenant of the apartment building next door informs the station operator that her laundry room/basement has a strong gasoline odor. Explosimeter readings indicate vapor concentrations are still lower than explosive levels, but the investigation team notes that "strong gasoline odors" are present.

X5.4.3 *Site Classification and Initial Response Action*—This limited information is sufficient to classify this site as a Class 2 site (strong potential for conditions to escalate to immediately hazardous conditions in the short term), based on the observed vapor concentrations, size of the release, and geological conditions. The initial response implemented is as follows:

X5.4.3.1 Periodic monitoring of the apartment basement begins to ensure that levels do not increase to the point where evacuation is necessary (either due to explosion or acute health effects). In addition, the fire marshall is notified and building tenants are informed of the activities at the site, potential hazards, and abatement measures being implemented,

X5.4.3.2 A free-product recovery/hydraulic control system is installed to prevent further migration of the mobile liquid gasoline, and

X5.4.3.3 A subsurface vapor extraction system is installed to prevent vapor intrusion to the building.

X5.4.4 *Development of Tier 1 Look-Up Table of Risk-Based Screening Level (RBSL) Selection*—Assumptions used to derive example Tier 1 RBSL Look-Up Table X2.1 in Appendix X2 are reviewed and presumed valid for this site. Target soil and ground water concentrations are determined based on the vapor intrusion scenario. After considering health-based, OSHA PEL, national ambient background, and aesthetic vapor concentrations, target soil levels are based on achieving a 10^{-4} chronic inhalation risk for benzene, and hazard quotients of unity for all other compounds. The agency agrees to base compliance on the volatile monoaromatic compounds in gasoline (benzene, toluene, xylenes, and ethylbenzene), but reserves the right to alter the target levels if aesthetic effects persist in the building basement at the negotiated levels.

X5.4.5 *Exposure Pathway Evaluation*—Given that: (*1*) there is a very low potential for ground water usage, (*2*) a 20-ft (6.1-m) thick aquitard separates the upper perched water from any potential drinking water supplies, and (*3*) the close proximity of the apartment building, the owner proposes focusing on the vapor intrusion—residential inhalation scenario (see Fig. X5.3). The agency concurs, but in order to eliminate potential ground water users as receptors of concern, requests that a down-gradient piezometer be installed in the lower aquifer. The owner concurs.

X5.4.6 *Comparison of Site Conditions With Tier 1*

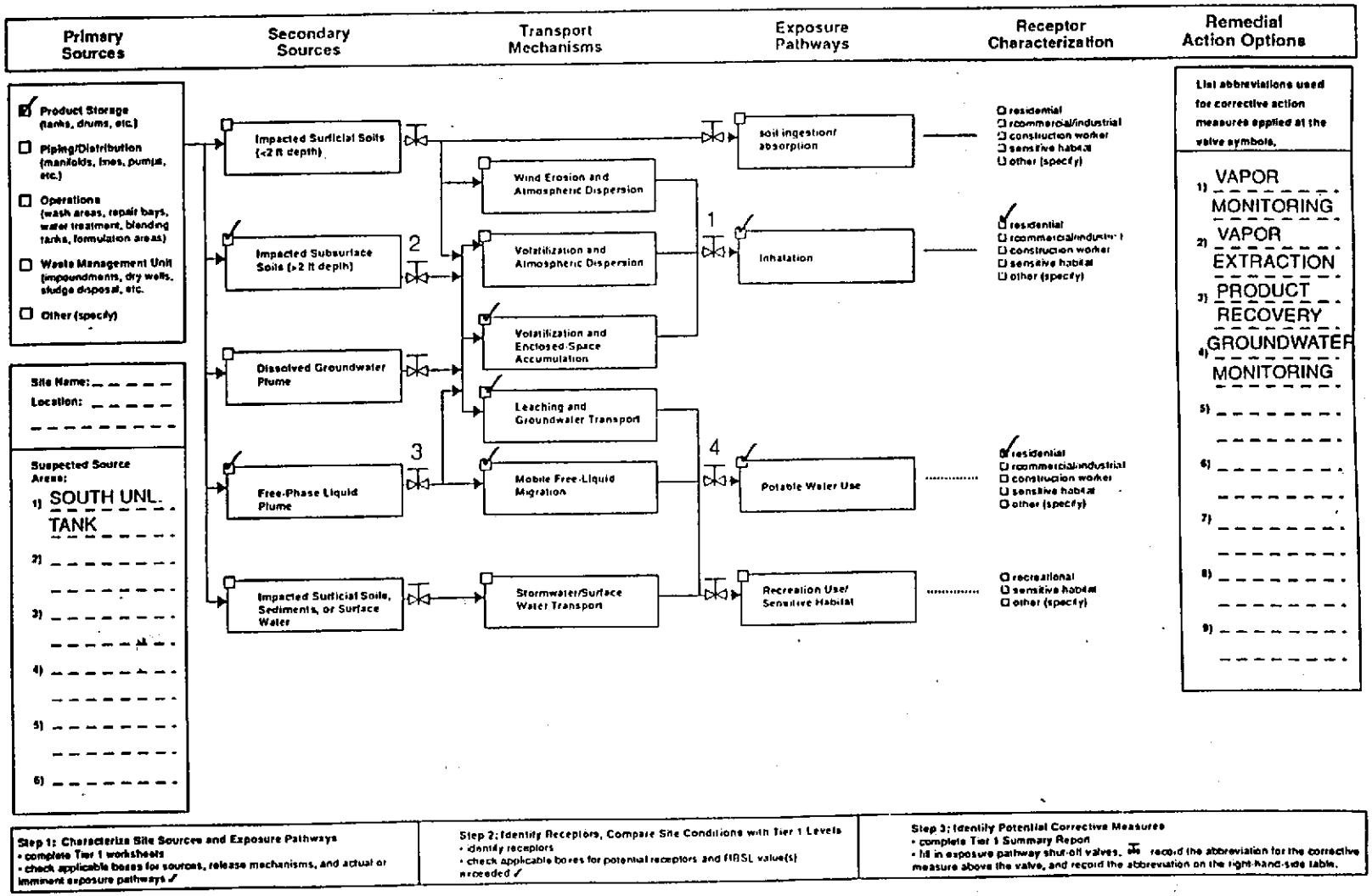


FIG. X5.3 Example 3—Exposure Evaluation Flowchart

RBSLs—While a complete initial site investigation has yet to be conducted, all parties agree that currently the RBSLs are likely to be exceeded.

X5.4.7 *Evaluation of Tier 1 Results*—The owner decides to implement an interim corrective action plan based on Tier 1 RBSLs, but reserves the right to propose a Tier 2 evaluation in the future.

X5.4.8 *Tier 1 Remedial Action Evaluation*—The owner proposes expanding the vapor extraction system to remediate source area soils. In addition he proposes continuing to operate the free-product recovery/hydraulic control system until product recovery ceases. Monitoring of the piezometer placed in the lower aquifer will continue, as well as periodic monitoring of the apartment building basement. Additional assessments will be conducted to ensure that building vapors are not the result of other sources. After some period of operation, when hydrocarbon removal rates decline, a soil and ground water assessment plan will be instituted to collect data to support a Tier 2 evaluation.

X5.5 *Example 4—RBCA Based on Use of a Tier 2 Table Evaluation*—In circumstances where site-specific data are similar among several sites, a table of Tier 2 SSTL values can be created. The following example uses such a table.

X5.5.1 *Scenario*—Petroleum-impacted ground water is discovered in monitoring wells at a former service station. The underground tanks and piping were removed, and the site is now occupied by an auto repair shop.

X5.5.2 *Site Assessment*—The responsible party completes an initial site assessment to determine the extent of hydrocarbon-impacted soil and ground water. Because gasoline was the only fuel dispensed at the site, the assessment focussed on benzene, toluene, ethylene benzene, and xylenes (BTEX) as the chemicals of concern. Site assessment results are summarized as follows:

X5.5.2.1 The area of hydrocarbon-impacted soil is approximately 18 000 ft^2 (1672 m^2) and the depth of soil impaction is less than 5 ft (1.5 m); The plume is off site,

X5.5.2.2 The site is covered by asphalt or concrete,

X5.5.2.3 The site is underlain by clay,

X5.5.2.4 Hydrocarbon-impacted perched ground water is encountered at 1 to 3 ft (0.3 to 0.9 m) below grade. This water is non-potable. The first potable aquifer is located over 100 ft (30 m) below grade and is not impacted. There is no free product,

X5.5.2.5 Maximum detected concentrations are as follows:

Compound	Soil, mg/kg	Ground water, mg/L
Benzene	39	1.8
Toluene	15	4.0
Ethylbenzene	12	0.5
Xylenes	140	9.0

X5.5.2.6 Ground water velocity is 0.008 ft/day (0.0024 m/day) based on slug tests and ground water elevation survey and assumed soil porosity of 50 %,

X5.5.2.7 A receptor survey indicates that the nearest down gradient water well is greater than 1.0 mile (1.6 km) away and the nearest surface water body is 0.5 miles (0.8 km). The distance to the nearest sensitive habitat is greater than 1.0 mile; however, there is a forest preserve frequented by day hikers and picnickers next to the site. The nearest home is 1000 ft (305 m) away. The commercial building on site is 25 ft (7.6 m) from the area of hydrocarbon-impacted soil.

X5.5.3 *Site Classification and Initial Response Action*—Based on the classification scenarios given in Table 1, this site is classified as a Class 4 site, with no demonstrable long-term threat to human health, safety, or sensitive environmental receptors, because the hydrocarbon-impacted soils are covered by asphalt or concrete and cannot be contacted, only non-potable perched water with no existing local use is impacted, and there is no potential for explosive levels or concentrations that could cause acute effects in nearby buildings. The appropriate initial response is to evaluate the need for a ground water monitoring program.

X5.5.4 *Development of Tier 1 Look-Up Table of Risked-Based Screening Level (RBSL)*—The assumptions used to derive the example Tier 1 RBSL Look-Up Table are presumed valid for this site.

X5.5.5 *Exposure Pathway Evaluation*—The complete pathways are ground water and soil volatilization to enclosed spaces and to ambient air, and direct exposure to impacted soil or ground water by construction workers. A comparison of RBSLs for these pathways of concern indicates that

TABLE X5.1 Example 1—Site Classification and Initial Response Actions

Criteria and Prescribed Scenarios	Example Initial Response Actions
3. Long-term (>2 years) threat to human health, safety, or sensitive environmental receptors	Notify appropriate authorities, property owners, and potentially affected parties, and evaluate the need to
• Subsurface soils (>3 ft (0.9 m) BGS) are significantly impacted, and the depth between impacted soils and the first potable aquifer is less than 50 ft (15 m).	• Monitor ground water and determine the potential for future migration of the chemical(s) of concern to the aquifer.
• Ground water is impacted, and potable water supply wells producing from the impacted interval are located >2 years ground water travel time from the dissolved plume.	• Monitor the dissolved plume and evaluate the potential for natural attenuation and the need for hydraulic control.
• Ground water is impacted, and non-potable water supply wells producing from the impacted interval are located >2 years ground water travel time from the dissolved plume.	• Identify water usage of well, assess the effect of potential impact, monitor the dissolved plume, and evaluate whether natural attenuation or hydraulic control are appropriate control measures.
• Ground water is impacted, and non-potable water supply wells that do not produce from the impacted interval are located within the known extent of chemical(s) of concern.	• Monitor the dissolved plume, determine the potential for vertical migration, notify the user, and determine if any impact is likely.
• Impacted surface water, storm water, or ground water discharges within 1500 ft (457 m) of a sensitive habitat or surface water body used for human drinking water or contact recreation.	• Investigate current impact on sensitive habitat or surface water body, restrict access to area of discharge (if necessary), and evaluate the need for containment/control measures.
• Shallow contaminated surface soils are open to public access, and dwellings, parks, playgrounds, day-care centers, schools, or similar-use facilities are more than 500 ft (152 m) of those soils.	• Restrict access to impact soils.

TABLE X5.2 Example 2—Site Classification and Initial Response Actions

Criteria and Prescribed Scenarios	Example Initial Response Actions
3. Long-term (>2 years) threat to human health, safety, or sensitive environmental receptors	Notify appropriate authorities, property owners, and potentially affected parties, and evaluate the need to
• Subsurface soils (>3 ft (0.9 m) BGS) are significantly impacted, and the depth between impacted soils and the first potable aquifer is less than 50 ft (15 m).	• Monitor ground water and determine the potential for future contaminant migration to the aquifer.
• Ground water is impacted, and potable water supply wells producing from the impacted interval are located >2 years ground water travel time from the dissolved plume.	• Monitor the dissolved plume and evaluate the potential for natural attenuation and the need for hydraulic control.
• Ground water is impacted, and non-potable water supply wells producing from the impacted interval are located >2 years ground water travel time from the dissolved plume.	• Identify water usage of well, assess the effect of potential impact, monitor the dissolved plume, and evaluate whether natural attenuation or hydraulic control are appropriate control measures.
• Ground water is impacted, and non-potable water supply wells that do not produce from the impacted interval are located within the known extent of chemical(s) of concern.	• Monitor the dissolved plume, determine the potential for vertical migration, notify the user, and determine if any impact is likely.
• Impacted surface water, storm water, or ground water discharges within 1500 ft (457 m) of a sensitive habitat or surface water body used for human drinking water or contact recreation.	• Investigate current impact on sensitive habitat or surface water body, restrict access to area of discharge (if necessary), and evaluate the need for containment/control measures.
• Shallow contaminated surface soils are open to public access, and dwellings, parks, playgrounds, day-care centers, schools, or similar-use facilities are more than 500 ft (152 m) of those soils.	• Restrict access to impact soils.

TABLE X5.3 Example 3—Site Classification and Initial Response Actions

Criteria and Prescribed Scenarios	Example Initial Response Actions
2. Short-term (0 to 2 years) threat to human health, safety, or sensitive environmental receptors	Notify appropriate authorities, property owners, and potentially affected parties, and evaluate the need to
• There is potential for explosive levels, or concentrations of vapors that could cause acute effects, to accumulate in a residence or other building.	• Assess the potential for vapor migration (through monitoring/modeling) and remove source (if necessary), or install vapor migration barrier.
• Shallow contaminated surface soils are open to public access, and dwellings, parks, playgrounds, day-care centers, schools, or similar use facilities are within 500 ft (152 m) of those soils.	• Remove soils, cover soils, or restrict access.
• A non-potable water supply well is impacted or immediately threatened.	• Notify owner/user and evaluate the need to install point-of-use water treatment, hydraulic control, or alternate water supply.
• Ground water is impacted, and a public or domestic water supply well producing from the impacted aquifer is located within two-years projected ground water travel distance down gradient of the known extent of chemical(s) of concern.	• Institute monitoring and then evaluate if natural attenuation is sufficient, or if hydraulic control is required.
• Ground water is impacted, and a public or domestic water supply well producing from a different interval is located within the known extent of chemicals of concern.	• Monitor ground water well quality and evaluate if control is necessary to prevent vertical migration to the supply well.
• Impacted surface water, storm water, or ground water discharges within 500 ft (152 m) of a sensitive habitat or surface water body used for human drinking water or contact recreation.	• Institute containment measures, restrict access to areas near discharge, and evaluate the magnitude and impact of the discharge.

RBSLs associated with soil volatilization to an enclosed space are the most restrictive RBSLs.

X5.5.6 *Comparison of Site Conditions with Tier 1 RBSLs*—Based on the data given in X5.5.2 and the RBSLs given in Table X2.1, exceedances of Tier 1 RBSLs are noted for benzene in soil and ground water and toluene for ground water.

X5.5.7 *Evaluation of Tier 1 Results*—The responsible party decided to proceed to a Tier 2 evaluation for the pathways of concern rather than develop a corrective action plan for the following reasons:

X5.5.7.1 Only shallow perched water is impacted, and the dissolved plume is moving very slowly in tight clay,

X5.5.7.2 Excavation of soils to meet Tier 1 criteria would be expensive and would disrupt activities of the on-site business. Off-site excavation would be impractical and may not be able to clean up ground water to Tier 1 criteria,

X5.5.7.3 Other conventional treatment methods, such as pump and treat and vapor extraction, would be relatively ineffective in the heavy clay, and

X5.5.7.4 A Tier 2 evaluation for this site requires no additional data and is expected to be an equally protective but less costly corrective action.

X5.5.8 *Development of a Tier 2 Table of Site-Specific Target Levels (SSTLs)*—The Tier 2 table is similar to the Tier 1 Look-Up Table with the exception that SSTLs for the pathways of concern are presented as functions of both the distance from the source to the receptor and the soil type.

X5.5.8.1 For the pathways considered, approaches for the Tier 2 table are consistent with guidelines contained in Ref (26).

X5.5.8.2 The equations, assumptions, and parameters used to construct the Tier 1 Look-Up Table and Tier 2 table are similar, except as noted as follows:

(*1*) *Ground Water: Ingestion of Ground Water*—A one-dimensional analytical mass balance equation with attenuation mechanisms of retardation, dispersivity, and first-order biological decay (in sandy soil only) was applied in conjunction with the equations in Tables X2.2 and X2.3 to calculate SSTLs. The analytical model is limited to steady-state conditions and longitudinal dispersion. The analytical solution to the mass balance equation is presented in Ref (44).

TABLE X5.4 Example Tier 2 Site-Specific Target Level (SSTL) Table—Soil and Ground Water

	Exposure Pathway	Receptor Scenario	Distance to Source, ft (m)	SSTLs at Source Sandy Soil, Natural Biodegradation Carcinogenic Risk = 1 × 10⁻⁵, HQ = 1				SSTLs at Source Clay Soil, No Natural Biodegradation Carcinogenic Risk = 1 × 10⁻⁵, HQ = 1			
				Benzene	Ethylbenzene	Toluene	Xylene	Benzene	Ethylbenzene	Toluene	Xylene
Soil	Soil vapor intrusion from soil to buildings, mg/kg	residential	10 (3)	0.052	18	11	450	1.7	570	300	9500
			25 (7.6)	0.47	160	160	1.7[A]	65	11[A]	10[A]	RES[B]
			100 (30)	3.1[A]	RES	RES	RES	RES	RES	RES	RES
		commercial/ industrial	10 (3)	0.13	39	24	980	4.3	1200	650	2.0[A]
			25 (7.6)	1.2	340	340	3.6[A]	950	24[A]	22.5[A]	RES
			100 (30)	8.0[A]	RES	RES	RES	RES	RES	RES	RES
	Surficial soil ingestion and dermal, mg/kg	residential		22	5100	5400	280	22	5100	5400	280
		commercial/ industrial		120	9600	1.7[A]	1500	117	9600	1.7[A]	1500
	Soil lechate to protect ground water ingestion target level, mg/kg	residential	0 (0)	0.17	47	130	2200	0.17	47	130	2200
			100 (30)	0.32	88	250	4200	0.20	130	760	RES
			500 (152)	4.0	1200	6300	RES	RES	RES	RES	RES
		commercial/ industrial	0 (0)	0.58	130	350	6200	0.58	130	350	6200
			100 (30)	1.1	250	670	1.2[A]	0.70	380	2100	RES
			500 (152)	13	3300	1.75[A]	RES	RES	RES	RES	RES
Ground Water	Ground water ingestion, mg/L	residential	0	0.029	3.6	7.3	73	0.029	3.6	7.3	73
			100	0.054	6.8	14	140	0.035	10	43	>S[C]
			500	0.68	90	350	>S	>S	>S	>S	>S
		commercial/ industrial	0	0.099	10	20	200	0.099	10	20	200
			100	0.185	19	38	>S	0.12	29	120	>S
			500	2.3	250	>S	>S	>S	>S	>S	>S
	Ground water vapor intrusion from ground water to buildings, mg/L	residential	10	0.11	32	17	510	5.0	>S	>S	>S
			25	0.72	210	160	>S	1200	>S	>S	>S
			100	>S	>S	>S	>S	>S	>S	>S	>S
		commercial/ industrial	10	0.26	70	36	>S	13	>S	>S	>S
			25	1.9	>S	350	>S	>S	>S	>S	>S
			100	>S	>S	>S	>S	>S	>S	>S	>S

[A] Weight percent.
[B] RES—Selected risk level is not exceeded for pure compound present at any concentration.
[C] >S—Selected risk level is not exceeded for all possible dissolved levels.

(2) *Ground Water: Inhalation of Outdoor Vapors*—This pathway was not considered because exposure concentrations were very low.

(3) *Ground Water: Inhalation of Enclosed-Space (Indoor) Vapors*—A one-dimensional mass balance equation following Jury, et al (31) has been used to model vapor transport (43). This model was used in conjunction with the equations in Table X2.2 and X2.3 to calculate SSTLs. The model includes concentration attenuation between the source and the building by partitioning into immobile pore water, adsorption onto soil, and biological degradation (in sandy soil only).

(4) *Subsurface Soils: Inhalation of Outdoor Vapors*—This pathway was not considered because exposure concentrations were very low.

(5) *Subsurface Soils: Inhalation of Enclosed-Space (Indoor) Vapors*—The SSTLs were calculated using the Jury model (31) as discussed in Paragraph (3) of X5.5.8.2.

(6) *Subsurface Soils: Leaching to Ground Water*—The SSTLs were calculated using the one-dimensional mass-balance equation described in Paragraph (1) of X5.5.8.2, in conjunction with the lechate factor, LF_{SU}, as discussed in X2.9.4.1.

(7) All exposure parameter values listed in Table X2.4, soil, building surface, and subsurface parameter values listed in Table X2.6, and chemical-specific properties listed in Table X2.7 have not been changed.

(8) First-order decay rates in sandy soil were assumed to be 0.2 % per day for all BTEX compounds. These rates are considered conservative. Chiang, et al (38) determined that a DO of 2.0 mg/L is required for rapid and complete biodegradation of benzene. Chiang, et al (38) measured a biodegradation rate of 0.95 % per day, and Barker, et al (36) measured a biodegradation rate of 0.6 % per day for benzene. In general, published biodegradation rates range from 0.6 to 1.25 % per day. Chiang, et al (38) also determined that biodegradation rates may be slower and incomplete at DO concentrations below 2.0 mg/L. This is a conservative value since aerobic biodegradation continues at DO concentrations as low as 0.7 mg/L (44).

(9) Clay properties are as follows:

Total soil porosity, cm^3/cm^3	0.05
Volumetric water content, cm^3/cm^3	0.40
Ground water Darcy velocity, cm/s	25

X5.5.8.3 Assumptions used to derive the example Tier 2 SSTL table are reviewed and presumed valid for this site. Due to the very conservative assumptions used to calculate exposure and the small number of people potentially exposed, the Tier 2 SSTLs are based on a 10^{-5} risk to human health for carcinogens and hazard quotients equal to unity for noncarcinogens.

X5.5.9 *Comparison of Site Conditions with Tier 2 Table SSTLs*—Based on the data given in X5.5.2 and the SSTLs given in the example table, no exceedances of Tier 2 soil or ground water SSTLs are noted.

X5.5.10 *Tier 2 Remedial Action Evaluation*—Based on the fact that Tier 2 soil or ground water SSTLs are not exceeded, the responsible party negotiates a corrective action plan based on the following:

X5.5.10.1 Annual compliance monitoring of ground

water at down gradient monitoring wells will be performed to demonstrate decreasing concentrations,

X5.5.10.2 Should levels exceed Tier 2 SSTLs at any of these monitoring points at any future time, the corrective action plan will be reevaluated, and

X5.5.10.3 Closure will be granted if dissolved concentrations remain stable or decrease for the next two years.

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Woodward-Clyde

Engineering & sciences applied to the earth & its environment

April 22, 1996

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Subject: Draft Errata to ASTM RBCA Guidance E 1739-95

Dear Curt and Erik:

It was a pleasure to meet with you in Houston. As promised, I am sending you our draft errata for the 1995 ASTM RBCA guidance. It is my understanding that Erik will share this document with the attendees at the upcoming ASTM meeting on April 25, 1996, as appropriate. Please note that due to time constraints this errata is in a draft format. The following individuals of Woodward-Clyde assisted in the preparation of this document: Fabrice Rodrigues, Jerome Lebegue, and Pierre-Yves Saugy. These individuals also contributed significantly to the development of the Woodward-Clyde RBCA Tier 2 software tools presented to you in Houston. This document was peer reviewed by David Berry.

We look forward to collaborating with you on new developments and applications of the risk-based corrective action.

Sincerely,

Marco Lobascio, R.E.A.
Environmental Engineer

cc: Paul McAllister
Chris Vais
Dennis Takade
Jim Strandberg
Jenifer Heath
Ron Duncan

Enclosures: Draft Errata to ASTM RBCA Guidance E 1739-95

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Draft Errata to ASTM RBCA Guidance E 1739-95

Page 6:

Paragraph "6.2.19" should be corrected to paragraph "6.2.1.9".

In paragraph 6.4, there may be an incorrect appendix reference. The third sentence should be corrected from "(10E-4 to 10E-6 are often evaluated as discussed in Appendix X1)" to "(10E-4 to 10E-6 are often evaluated as discussed in Appendix X2)" as specified in paragraph 1.3.7.

Page 7. Table 1:

Reference in footnote A should be corrected from " Johnson, D.C..." to "Johnson, P.C..."

Page 14:

In paragraph X1.5.5, correct table reference. The last sentence should be corrected from "(see Table X1.2.)" to "(see Table X1.4)"

In paragraph X1.5.7, correct table references. The last sentence should be corrected from "These terms are defined in Table X1.4 and further discussed in X3.6" to "These terms are defined in Table X1.5 and further discussed in X3.8"

Page 16. Table X1.2:

Footnote [F] should be deleted since it is not mentioned in Table X1.2 due to the new values of the oral RfD for MIBK.

Page 17. Text:

In paragraph X1.6.3.1, change the MCL and MCLG value from "10,000 g/L" to "10,000 µg/L".

Page 22. Table X2.1:

Commercial RBSLs for benzene due to soil-vapor intrusion into buildings should be corrected from 1.09E-2 to 1.69E-2 and from 1.09E+0 to 1.69E+0.

RBSLs for surficial soils exceeded saturation for all chemicals except benzene and benzo(a)pyrene. Substitute RES to RBSL for those chemicals. Additionally, it would be very useful to show in the Tier 1 RBSLs lookup table the actual value of the solubility or the soil saturation limits.

Draft Errata to ASTM RBCA Guidance E 1739-95
(continued)

Page 23 and 24:

Change the units for RBSLs (surficial soil pathway) from µg/kg-soil to mg/kg-soil. Also, page 24 equation should have square parentheses after EF x ED at denominator, consistent with the corresponding equation for carcinogenic effects presented in the table of page 23. This expression should be corrected from:

"$$RBSL_s \left[\frac{\mu g}{kg - soil}\right] =$$ "

$$\frac{THQ \times BW \times AT_n \times 365 \frac{days}{years}}{EF \times ED \times \left[\frac{\left(10^{-6} \frac{kg}{mg} \times (IR_{soil} \times RAF_o + SA \times M \times RAF_d)\right)}{RfD_o} + \frac{(IR_{air} \times (VF_{ss} + VF_p))}{RfD_i}\right]}$$

to:

"

$$RBSL_s \left[\frac{mg}{kg - soil}\right] =$$ "

$$\frac{THQ \times BW \times AT_n \times 365 \frac{days}{years}}{EF \times ED \times \left[\frac{\left(10^{-6} \frac{kg}{mg} \times (IR_{soil} \times RAF_o + SA \times M \times RAF_d)\right)}{RfD_o} + \frac{(IR_{air} \times (VF_{ss} + VF_p))}{RfD_i}\right]}$$

Page 24. Text:

In paragraph X2.4.1, correct table reference. The second sentence should be corrected from "...as given in Tables X2.3 and X2.4..." to "...as given in Tables X2.2 and X2.3..."

Page 27. Table X2.6:

Correct value for θ_{acap} (Commercial/Industrial scenario) from 0.38 to 0.038 cm^3-air/cm^3-soil.

Page 27. Text:

In paragraph X2.7.1, correct table reference. The second sentence should be corrected from "...as given in Table X2.2..." to "...as given in Tables X2.2 and X2.3..."

Draft Errata to ASTM RBCA Guidance E 1739-95
(continued)

Page 27. Table X2.7:

We think there is some discrepancy between the inhalation reference doses (RfDi) tabulated in Table X2.7 and the values that were used by ASTM in the RBSL calculation of look-up Table X2.1:

Chemical	*RfD used by ASTM*	*RfD in Table X2.7*
Toluene	0.114	0.11
Ethyl benzene	0.285	0.29

Page 29. Text:

In paragraph X2.9.1, there is an incorrect paragraph reference. The first sentence should be corrected from "...as discussed in X2.1 through X2.3..." to "...as discussed in X2.2 through X2.3...".

In paragraph X2.9.3, the first sentence should be corrected from 'Should the calculated $RBSL_s$ exceed the value for which the equilibrated vapor...." to 'Should the calculated $RBSL_s$ exceed the value C_s^{sat} [mg/kg-soil] for which the equilibrated vapor....".

Page 31. Table X3.1:

For the equation describing the effective porous media diffusion coefficient, change the denominator terms from θ_T to θ_T^2. This expression should be changed from:

$$\text{“}D^{eff} = \frac{\theta_v^{3.33}}{\theta_T} D^{air} + \frac{1}{H}\frac{\theta_w^{3.33}}{\theta_T} D^{w}\text{”}$$

to:

$$\text{“}D^{eff} = \frac{\theta_v^{3.33}}{\theta_T^{2}} D^{air} + \frac{1}{H}\frac{\theta_w^{3.33}}{\theta_T^{2}} D^{w}\text{”}$$

Page 39-40. Text:

Paragraphs "X4.6.2", "X4.6.2.1", "X4.6.2.2", "X4.6.2.3", "X4.6.3", "X4.6.3.1", and "X4.6.3.2" should be corrected to paragraphs "X4.6.1", "X4.6.1.1", "X4.6.1.2", "X4.6.1.3", "X4.6.2", "X4.6.2.1", and "X4.6.2.2" respectively.

Draft Errata to ASTM RBCA Guidance E 1739-95
(concluded)

Page 41. Text:

In paragraph X5.2.3, at the end of the second sentence, there should be added: "(see Table X5.1)", since this table reference does not seem to appear anywhere.

In paragraph X5.2.6, correct paragraph reference. The first sentence should be corrected from "Based on the data given in X5.2.3.7..." to "Based on the data given in X5.2.2.7...".

Page 43. Text:

In paragraph X5.3.3, at the end of the second sentence, there should be added: "(see Table X5.2)", because this table reference does not seem to appear anywhere.

Page 45. Text:

In paragraph X5.4.3, at the end of the first sentence, there should be added: "(see Table X5.3)", because this table reference does not seem to appear anywhere.

Page 49. Text:

In paragraph X5.5.9, a table reference is missing. The first sentence should be corrected from " Based on the data given in X5.5.2 and the SSTLs given in the example table, no exceedances..." to from " Based on the data given in X5.5.2 and the SSTLs given in the example Table X5.4, no exceedances...".

Woodward-Clyde

Engineering & Sciences applied to the earth & its environment

November 10, 1994
7147/1000

George De Vaull
Shell Development Co.
P. O. BOX 1380
Houston, TX 77251-1380

Re: Additional Errata for ASTM ES 38-94

Dear George:

Thanks for sending us the ASTM errata memo. We are using the RBCA approach to estimate risk-based screening levels in soil and groundwater at the Hamilton Air Force Base site in California. We have developed our own spreadsheets, and we have reproduced the look-up table values for Tier I. The purpose of this letter is to provide you with additional errata that we have discovered in trying to reproduce the RBCA look-up Table 4.

- Page 9: RBSLs for surficial soils exceeded saturation for all chemicals except benzene and benzo(a)pyrene. Substitute RES to RBSL for those chemicals.

- Page 24: Equation for RBSLs (surficial soil pathway, noncarcinogenic effects) should have a square parentheses after EF x ED at denominator, consistent with the corresponding equation for carcinogenic effects presented in the table of page 23.

- Page 26: We have found some discrepancy between the inhalation reference doses (RfDi) tabulated in Table X2.6 and the values that were used by ASTM in the RBSL calculation of look-up Table 4:

Chemical	*RfD used by ASTM*	*RfD in Table X2.6*
Toluene	0.114	0.11
Ethyl benzene	0.285	0.29

Attached you'll find a copy of our spreadsheet.

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Woodward-Clyde Consultants
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We find the RBCA process very useful, and we look forward to working with you for its implementation. Please keep us informed of any new development in this matter.

Sincerely,

Marco Lobascio
Assistant Project Engineer

For Bill

Bill Popenuck
Project Engineer

cc: Matt Alix (USACE)
Richard Becker, Michael Wade (CalEPA-DTSC)
Ron Duncan (Oakland)
Dennis Takade (Overland Park)
Atul Salhotra (Houston)

DEVELOPMENT OF RISK-BASED SCREENING LEVELS - TEST CASE
Based on ASTM Guidance ES 38 - 94 and Shell ERRATA Memo

EXPOSURE FACTORS AND OTHER RELEVANT PARAMETERS

EXPOSURE PARAMETER	Units	Default Value	Reference
GLOBAL PARAMETERS			
Averaging Time - Carcinogen	yr	70	ASTM - Guide for RBCA July 1994
Averaging Time - Noncarcinogen	yr	30	ASTM - Guide for RBCA July 1994
Body Weight	kg	70	ASTM - Guide for RBCA July 1994
Exposure Duration	yr	30	ASTM - Guide for RBCA July 1994
Exposure Frequency	days/yr	350	ASTM - Guide for RBCA July 1994
Soil ingestion rate	mg/day	100	ASTM - Guide for RBCA July 1994
Daily Indoor Inhalation Rate	m^3/day	15	ASTM - Guide for RBCA July 1994
Daily Outdoor Inhalation Rate	m^3/day	20	ASTM - Guide for RBCA July 1994
Daily water ingestion rate	L/day	2	ASTM - Guide for RBCA July 1994
Soil skin adherence factor	mg/cm^2	0.5	ASTM - Guide for RBCA July 1994
Oral relative absorption factor	—	1	ASTM - Guide for RBCA July 1994
Dermal relative absorption factor (volatiles)	—	0.5	ASTM - Guide for RBCA July 1994
Dermal relative absorption factor (PAHs)	—	0.05	ASTM - Guide for RBCA July 1994
Skin surface area	cm^2	3160	ASTM - Guide for RBCA July 1994
Target Hazard Quotient for individual constituents	—	1	ASTM - Guide for RBCA July 1994
Target Excess Individual Lifetime Cancer Risk	—	1.00E-06	ASTM - Guide for RBCA July 1994
SOIL, BUILDING, SURFACE AND SUBSURFACE PARAMETERS			
Lower depth of surficial soil zone	cm	100	
Enclosed space air exchange rate	L/s	0.00014	ASTM - Guide for RBCA July 1994
Fraction of organic carbon in soil	g-C/g-soil	0.01	ASTM - Guide for RBCA July 1994
Thickness of capillary fringe	cm	5	ASTM - Guide for RBCA July 1994
Thickness of vadose zone	cm	295	ASTM - Guide for RBCA July 1994
Infiltration rate of water through soil	cm/yr	30	ASTM - Guide for RBCA July 1994
Enclosed space volume/infiltration area	cm	200	ASTM - Guide for RBCA July 1994
Enclosed space foundation/wall thickness	cm	15	ASTM - Guide for RBCA July 1994
Depth to groundwater	cm	300	ASTM - Guide for RBCA July 1994
Depth to subsurface soil sources	cm	100	ASTM - Guide for RBCA July 1994
Particulate emission rate	g/cm^2-s	6.90E-14	ASTM - Guide for RBCA July 1994
Wind speed above ground surface in ambient mixing zon	cm/s	225	ASTM - Guide for RBCA July 1994
Groundwater Darcy velocity	cm/yr	2500	ASTM - Guide for RBCA July 1994
Width of source area parallel to wind or gw flow	cm	1500	ASTM - Guide for RBCA July 1994
Ambient air mixing zone height	cm	200	ASTM - Guide for RBCA July 1994
Groundwater mixing zone height	cm	200	ASTM - Guide for RBCA July 1994
Areal fraction of foundation/walls	cm^2/cm^2	0.01	ASTM - Guide for RBCA July 1994
Volumetric air content in capillary fringe soils	cc/cc	0.038	ASTM - Guide for RBCA July 1994
Volumetric air content in found./wall cracks	cc/cc	0.26	ASTM - Guide for RBCA July 1994
Volumetric air content in vadose zone soils	cc/cc	0.26	ASTM - Guide for RBCA July 1994
Total soil porosity	cc/cc-soil	0.38	ASTM - Guide for RBCA July 1994
Volumetric water content in capillary fringe soils	cc/cc	0.342	ASTM - Guide for RBCA July 1994
Volumetric water content in found./wall cracks	cc/cc	0.12	ASTM - Guide for RBCA July 1994
Volumetric water content in vadose zone soils	cc/cc	0.12	ASTM - Guide for RBCA July 1994
Soil bulk density	g/cc	1.70E+00	ASTM - Guide for RBCA July 1994
Averaging time for vapor flux	sec	9.46E+08	ASTM - Guide for RBCA July 1994

Reference : ASTM Emergency Standard Guide for Risk-Based Corrective Action Applied at Petroleum Release Sites (July, 1994)

DEVELOPMENT OF RISK-BASED SCREENING LEVELS - TEST CASE
Based on ASTM Guidance ES 38 - 94 and Shell ERRATA Memo

CHEMICAL-SPECIFIC TOXICITY PARAMETERS

CHEMICAL	SLOPE FACTOR				REFERENCE DOSE			
	ORAL		INHALATION		ORAL		INHALATION	
	[1/(mg/kg-day)]	ref.	[1/(mg/kg-day)]	ref.	[mg/kg-day]	ref.	[mg/kg-day]	ref.
Benzene	0.029	(a)	0.029	(a)	NA	(a)	NA	(a)
Toluene	NA	(a)	NA	(a)	0.2	(a)	0.11	(a)
Ethylbenzene	NA	(a)	NA	(a)	0.1	(a)	0.29	(a)
Xylene (mixed)	NA	(a)	NA	(a)	2	(a)	2	(a)
Naphthalene	NA	(a)	NA	(a)	0.004	(a)	0.004	(a)
Benzo(a)pyrene	7.3	(a)	6.1	(a)	NA	(a)	NA	(a)

References

(a) As referenced in ASTM Emergency Standard Guide for Risk-Based Corrective Action Applied at Petroleum Release Sites (July, 1994)

CHEMICAL-SPECIFIC FATE AND TRANSPORT PARAMETERS

CHEMICAL	Koc [cm^3/g]	Kd [cm^3/g]	Henry's [atm-m^3/mol]	H [cc-H2O/cc-air]	S [mg/l-water]	Dair [cm^2/s]	Dwater [cm^2/s]
Benzene	38	3.80E-01	0.0055	2.20E-01	1750	0.093	1.10E-05
Toluene	135	1.35E+00	0.0066	2.60E-01	535	0.085	9.40E-06
Ethylbenzene	1288	1.29E+01	0.0079	3.20E-01	152	0.076	8.50E-06
Xylene (mixed)	240	2.40E+00	0.0053	2.90E-01	198	0.072	8.50E-06
Naphthalene	1288	1.29E+01	0.0013	4.90E-02	31	0.072	9.40E-06
Benzo(a)pyrene	389000	3.89E+03	1.40E-09	5.74E-08	0.0012	0.05	5.80E-06

Definition of Parameters

Koc	Organic carbon partition coefficient	S	Solubility
Kd	Soil-water partition coefficient	Dair	Diffusion coefficient in air
H	Normalized Henry's Law Constant	Dwater	Diffusion coefficient in water

References

As referenced in ASTM Emergency Standard Guide for Risk-Based Corrective Action Applied at Petroleum Release Sites (July, 1994)

DEVELOPMENT OF RISK-BASED SCREENING LEVELS - TEST CASE
Based on ASTM Guidance ES 38 - 94 and Shell ERRATA Memo

CHEMICAL-SPECIFIC FATE AND TRANSPORT DIFFUSION PARAMETERS

CHEMICAL	Ds [cm^2/s]	Dcrack [cm^2/s]	Dcap [cm^2/s]	Dws [cm^2/s]	Csat [mg/kg]	LFsw [mg/L/mg/kg]
Benzene	7.26E-03	7.26E-03	2.17E-05	1.11E-03	8.47E+02	1.71E-01
Toluene	6.63E-03	6.63E-03	1.80E-05	9.31E-04	7.81E+02	5.65E-02
Ethylbenzene	5.93E-03	5.93E-03	1.50E-05	7.82E-04	1.98E+03	6.35E-03
Xylene (mixed)	5.62E-03	5.62E-03	1.50E-05	7.77E-04	4.98E+02	3.28E-02
Naphthalene	5.62E-03	5.62E-03	4.66E-05	1.88E-03	4.02E+02	6.37E-03
Benzo(a)pyrene	6.05E-01	6.05E-01	1.96E+01	6.14E-01	4.67E+00	2.12E-05

Definition of Parameters

Ds	Effective diffusion coefficient in soil based on vapor-phase concentration
Dcrack	Effective diffusion coefficient through foundation cracks
Dcap	Effective diffusion coefficient through capillary fringe
Dws	Effective diffusion coefficient between groundwater and soil surface
Csat	Soil concentration at which dissolved pore-water and vapor phases become saturated
LFsw	Leachate factor from subsurface soils to groundwater

CHEMICAL-SPECIFIC FATE AND TRANSPORT VOLATILIZATION FACTORS

CHEMICAL	VOLATILIZATION FACTORS						
	VFwesp [mg/m^3-air/mg/L-H2O]	VFwamb [mg/m^3-air/mg/L-H2O]	VFas1 [mg/m^3-air/mg/kg-soil]	VFas2 [mg/m^3-air/mg/kg-soil]	VFp [mg/m^3-air/mg/kg-soil]	VFsamb [mg/m^3-air/mg/kg-soil]	VFsesp [mg/m^3-air/mg/kg-soil]
Benzene	1.65E-02	2.71E-05	9.16E-05	5.99E-06	2.30E-12	1.10E-03	7.36E-02
Toluene	1.69E-02	2.69E-05	5.48E-05	5.99E-06	2.30E-12	3.94E-04	2.64E-02
Ethylbenzene	1.80E-02	2.78E-05	1.93E-05	5.99E-06	2.30E-12	4.87E-05	3.26E-03
Xylene (mixed)	1.59E-02	2.51E-05	4.06E-05	5.99E-06	2.30E-12	2.16E-04	1.45E-02
Naphthalene	4.10E-03	1.02E-05	7.35E-06	5.99E-06	2.30E-12	7.08E-06	4.74E-04
Benzo(a)pyrene	6.82E-07	3.92E-09	4.76E-09	5.99E-06	2.30E-12	2.97E-12	1.96E-10

Definition of Factors

VFwesp	Volatilization factor from groundwater to enclosed-space vapors
VFwamb	Volatilization factor from groundwater to ambient (outdoor) vapors
VFas	Volatilization factor from surficial soils to ambient air (vapors)
VFp	Volatilization factor from surficial soils to ambient air (particulates)
VFsamb	Volatilization factor from surficial soils to ambient air
VFsesp	Volatilization factor from soil to enclosed-space vapors

DEVELOPMENT OF RISK-BASED SCREENING LEVELS - TEST CASE
Based on ASTM Guidance ES 38 - 94 and Shell ERRATA Memo

ADULT RESIDENTIAL - INGESTION OF WATER

CHEMICAL	CHEMICAL CONCENTRATION IN WATER [mg/l]		RBSLs [mg/l]	ASTM Value [mg/l]
	CARCINOGENIC EFFECTS	NONCARCINOGENIC EFFECTS		
Benzene	2.94E-03	N/A	2.94E-03	2.94E-03
Toluene	N/A	7.30E+00	7.30E+00	7.30E+00
Ethylbenzene	N/A	3.65E+00	3.65E+00	3.65E+00
Xylene (mixed)	N/A	7.30E+01	7.30E+01	7.30E+01
Naphthalene	N/A	1.46E-01	1.46E-01	1.46E-01
Benzo(a)pyrene	1.17E-05	N/A	1.17E-05	1.17E-05

N/A Not Applicable

ADULT RESIDENTIAL - SOIL INGESTION

CHEMICAL	CHEMICAL CONCENTRATION IN SOIL [mg/kg]		RBSLs [mg/kg]	ASTM Value [mg/l]
	CARCINOGENIC EFFECTS	NONCARCINOGENIC EFFECTS		
Benzene	5.87E+01	N/A	5.87E+01	N/A
Toluene	NA	6.26E+04	6.26E+04	N/A
Ethylbenzene	NA	3.13E+04	3.13E+04	N/A
Xylene (mixed)	NA	6.26E+05	6.26E+05	N/A
Naphthalene	NA	1.25E+03	1.25E+03	N/A
Benzo(a)pyrene	2.33E-01	N/A	2.33E-01	N/A

N/A Not Applicable

DEVELOPMENT OF RISK-BASED SCREENING LEVELS - TEST CASE
Based on ASTM Guidance ES 38 - 94 and Shell ERRATA Memo

ADULT RESIDENTIAL - AIR INHALATION (INDOOR)

CHEMICAL	CHEMICAL CONCENTRATION IN AIR [ug/m^3]		RBSLs [ug/m^3]	ASTM Value [ug/m^3]
	CARCINOGENIC EFFECTS	NONCARCINOGENIC EFFECTS		
Benzene	3.92E-01	N/A	3.92E-01	3.92E-01
Toluene	N/A	5.55E+02	5.55E+02	5.56E+02
Ethylbenzene	N/A	1.39E+03	1.39E+03	1.39E+03
Xylene (mixed)	N/A	9.73E+03	9.73E+03	9.73E+03
Naphthalene	N/A	1.95E+01	1.95E+01	1.95E+01
Benzo(a)pyrene	1.86E-03	N/A	1.86E-03	1.86E-03

N/A Not Applicable

ADULT RESIDENTIAL - AIR INHALATION (OUTDOOR)

CHEMICAL	CHEMICAL CONCENTRATION IN AIR [ug/m^3]		RBSLs [ug/m^3]	ASTM Value [mg/l]
	CARCINOGENIC EFFECTS	NONCARCINOGENIC EFFECTS		
Benzene	2.94E-01	N/A	2.94E-01	2.94E-01
Toluene	N/A	4.16E+02	4.16E+02	4.17E+02
Ethylbenzene	N/A	1.04E+03	1.04E+03	1.04E+03
Xylene (mixed)	N/A	7.30E+03	7.30E+03	7.30E+03
Naphthalene	N/A	1.46E+01	1.46E+01	1.46E+01
Benzo(a)pyrene	1.40E-03	N/A	1.40E-03	1.40E-03

N/A Not Applicable

DEVELOPMENT OF RISK-BASED SCREENING LEVELS - TEST CASE
Based on ASTM Guidance ES 38 - 94 and Shell ERRATA Memo

ADULT RESIDENTIAL - INDOOR VAPOR INHALATION GROUNDWATER

CHEMICAL	CHEMICAL CONCENTRATION IN WATER (mg/L)		RBSLs (mg/L)	ASTM Value (mg/L)
	CARCINOGENIC EFFECTS	NONCARCINOGENIC EFFECTS		
Benzene	2.38E-01	N/A	2.38E-02	2.38E-02
Toluene	N/A	3.28E+01	3.28E+01	3.28E+01
Ethylbenzene	N/A	7.72E+01	7.72E+01	7.75E+01
Xylene (mixed)	N/A	6.14E+02	1.98E+02 *	N/A
Naphthalene	N/A	4.75E+00	4.75E+00	4.74E+00
Benzo(a)pyrene	2.73E+00	N/A	1.20E-03 *	>S

N/A Not Applicable
* Indicates RBSL exceeded pure component water solubility and hence water solubility is listed as RBSL

TABLE 11
ADULT RESIDENTIAL - OUTDOOR VAPOR INHALATION GROUNDWATER

CHEMICAL	CHEMICAL CONCENTRATION IN WATER (mg/L)		RBSLs (mg/L)	ASTM Value (mg/l)
	CARCINOGENIC EFFECTS	NONCARCINOGENIC EFFECTS		
Benzene	1.08E+01	N/A	1.08E+01	1.10E+01
Toluene	N/A	1.55E+04	5.35E+02 *	>S
Ethylbenzene	N/A	3.74E+04	1.52E+02 *	>S
Xylene (mixed)	N/A	2.91E+05	1.98E+02 *	>S
Naphthalene	N/A	1.43E+03	3.10E+01 *	>S
Benzo(a)pyrene	3.56E+02	N/A	1.20E-03 *	>S

N/A Not Applicable
* Indicates RBSL exceeded pure component water solubility and hence water solubility is listed as RBSL

DEVELOPMENT OF RISK-BASED SCREENING LEVELS - TEST CASE
Based on ASTM Guidance ES 38 - 94 and Shell ERRATA Memo

ADULT RESIDENTIAL - INDOOR VAPOR INHALATION
SUBSURFACE SOILS

CHEMICAL	CHEMICAL CONCENTRATION IN SOIL [mg/kg]		RBSLs [mg/kg]	ASTM Value [mg/kg]
	CARCINOGENIC EFFECTS	NONCARCINOGENIC EFFECTS		
Benzene	5.32E-03	N/A	5.32E-03	5.37E-03
Toluene	N/A	2.10E+01	2.10E+01	2.08E+01
Ethylbenzene	N/A	4.26E-02	4.26E+02	4.27E+02
Xylene (mixed)	N/A	6.73E+02	4.98E+02 *	RES
Naphthalene	N/A	4.10E+01	4.10E+01	4.07E+01
Benzo(a)pyrene	9.48E+03	N/A	4.67E+00 *	RES

N/A Not Applicable
* Indicates RBSL exceeded saturated soil concentration and hence saturated soil concentration is listed as RBSL

ADULT RESIDENTIAL - OUTDOOR VAPOR INHALATION
SUBSURFACE SOILS

CHEMICAL	CHEMICAL CONCENTRATION IN SOIL [mg/kg]		RBSLs [mg/kg]	ASTM Value [mg/l]
	CARCINOGENIC EFFECTS	NONCARCINOGENIC EFFECTS		
Benzene	2.67E-01	N/A	2.67E-01	2.72E-01
Toluene	N/A	1.06E+03	7.81E+02 *	RES
Ethylbenzene	N/A	2.14E+04	1.98E+03 *	RES
Xylene (mixed)	N/A	3.38E+04	4.98E+02 *	RES
Naphthalene	N/A	2.06E+03	4.02E+02 *	RES
Benzo(a)pyrene	4.70E+05	N/A	4.67E+00 *	RES

N/A Not Applicable
* Indicates RBSL exceeded saturated soil concentration and hence saturated soil concentration is listed as RBSL

DEVELOPMENT OF RISK-BASED SCREENING LEVELS - TEST CASE
Based on ASTM Guidance ES 38 - 94 and Shell ERRATA Memo

ADULT RESIDENTIAL - LEACHING TO GROUNDWATER
SUBSURFACE SOIL

CHEMICAL	CHEMICAL CONCENTRATION IN SOIL (mg/kg)		RBSLs (mg/kg)	ASTM Value (mg/l)
	CARCINOGENIC EFFECTS	NONCARCINOGENIC EFFECTS		
Benzene	1.72E-02	N/A	1.72E-02	1.72E-02
Toluene	N/A	1.29E+02	1.29E+02	1.29E+02
Ethylbenzene	N/A	5.75E+02	5.75E+02	5.75E+02
Xylene (mixed)	N/A	2.22E+03	4.98E+02 *	RES
Naphthalene	N/A	2.29E+01	2.29E+01	2.29E+01
Benzo(a)pyrene	5.50E-01	N/A	5.50E-01	5.50E-01

N/A Not Applicable
* Indicates RBSL exceeded saturated soil concentration and hence saturated soil concentration is listed as RBSL

ADULT RESIDENTIAL - SURFICIAL SOILS
SOIL INGESTION, DERMAL CONTACT AND INHALATION OF VAPORS AND PARTICULATES

CHEMICAL	CHEMICAL CONCENTRATION IN SOIL (mg/kg)		RBSLs (mg/kg)	ASTM Value (mg/kg)
	CARCINOGENIC EFFECTS	NONCARCINOGENIC EFFECTS		
Benzene	5.82E+00	N/A	5.82E+00	5.82E+00
Toluene	N/A	1.33E+04	7.81E+02 *	1.33E+04
Ethylbenzene	N/A	7.83E+03	1.98E+03 *	7.83E+03
Xylene (mixed)	N/A	1.45E+05	4.98E+02 *	1.45E+05
Naphthalene	N/A	9.77E+02	4.02E+02 *	9.77E+02
Benzo(a)pyrene	1.30E-01	N/A	1.30E-01	1.30E-01

N/A Not Applicable
* Indicates RBSL exceeded saturated soil concentration and hence saturated soil concentration is listed as RBSL

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SUBJECT: ERRATA FOR ASTM ES 38-94 (July '94)

MESSAGE:

If you do not receive all pages, please call back as soon as possible.

PAGES (INCLUDING COVER PAGE): 6

SD-32 (REV. 5-78)

Shell Development Company
Interoffice Memorandum
SEPTEMBER 12, 1994

FROM: G.E. DEVAULL AND R.A. ETTINGER

TO: DISTRIBUTION

SUBJECT: ASTM ES 38-94 ERRATA

We have reviewed the ASTM Emergency Standard Guide for Risk-Based Corrective Action Applied at Petroleum Release Sites. The following errors in the document were noted.

Page 1 Text

In paragraph 1.3, there are incorrect section references. The second sentence in this paragraph should read:

For those interested only in becoming familiar with RBCA, the short main body of text provides a brief overview of the RBCA process (see Section 3), and then presents RBCA procedures in a step-by-step fashion (see Section 4) followed by a discussion of ways in which the process can be misapplied (see Section 5).

page 7 Table 3

Reference in footnote A should be corrected from "Johnson, D.C..." to "Johnson, P.C..."

Page 9 Table 4:

Look-up values in table differ from those calculated using methodology discussed in Appendix X2, due to typographical errors and parameter value errors in Appendix X2 (discussed later) and differences in application of equations relative to discussion. Revised values are as follows:

The total soil diffusivity through the soil column rather than the crack diffusivity had previously been used in calculating indoor air screening levels. Revising this to use the correct effective crack diffusivity produces the following changes to Table 4:

Pathway: Groundwater Volatilization to Indoor Air:

Chemical	Exposure Scenario	Carcinogen/ Chronic	Target Risk/ Hazard Quotient	RBSL (mg/kg)
Benzene	Residential	Cancer Risk	1E-6	2.38E-2
Benzene	Residential	Cancer Risk	1E-4	2.38E+0
Ethylbenzene	Residential	Chronic	HQ = 1	7.75E+1
Toluene	Residential	Chronic	HQ = 1	3.28E+1
Napthalene	Residential	Chronic	HQ = 1	4.74E+0
Benzene	Comm/Indust	Cancer Risk	1E-6	7.39E-2
Benzene	Comm/Indust	Cancer Risk	1E-4	7.39E+0
Toluene	Comm/Indust	Chronic	HQ = 1	8.50E+1
Napthalene	Comm/Indust	Chronic	HQ = 1	1.23E+1

Changing log10(Koc) for ethylbenzene from 1.98 to 3.11 (as discussed later) produces the following changes to table 4:

Pathway: Soil Leaching to Goundwater:

Chemical	Exposure Scenario	Carcinogen/ Chronic	Target Risk/ Hazard Quotient	RBSL (mg/kg)
Ethylbenzene	Residential	Chronic	HQ = 1	5.75E+2
Ethylbenzene	Comm/Indust	Chronic	HQ = 1	1.61E+3
Ethylbenzene	MCL			1.10E+2

Pathway: Soil Volatilization to Indoor Air:

Chemical	Exposure Scenario	Carcinogen/ Chronic	Target Risk/ Hazard Quotient	RBSL (mg/kg)
Ethylbenzene	Residential	Chronic	HQ = 1	4.27E+2
Ethylbenzene	Comm/Indust	Chronic	HQ = 1	1.10E+3

page 16 Table X1.2

Footnotes C and D both refer to Reference (7). The oral RfD for n-hexane has two different values that are refered to this same reference. The value for the oral RfD in HEAST, 1992 is 0.06.

The last hydrocarbon in this table should be changed from Benz(a)anthracene to Benzo(a)anthracene.

page 22 Table X2.1

The last term in the relation for VF_{wesp} should be changed from 10^{-3} L/m^3 to 10^3 L/m^3.

The last term in the relation for VF_{wamb} should be changed from 10^{-3} L/m^3 to 10^3 L/m^3.

In the expression for LF_{sw}, the units should be changed from 1-H_2O to L-H_2O.

In the expressions for D_s^{eff}, D_{crack}^{eff}, and D_{cap}^{eff} the terms $\theta_T^{3.33}$ in the denominators should be changed to θ_T^2.

page 23 Table X2.2

In the last expression for subsurface soil - leaching to ground water, the term $RBSL_{wi}$ should be changed to $RBSL_w$.

page 24 Table X2.3

In the last expression for subsurface soil - leaching to ground water, the term $RBSL_{wi}$ should be changed to $RBSL_w$.

pages 24-25 Text

The references to Table X2.1 should be changed to Table 4. (Note that there is one reference in each of the following paragraphs: X2.1.4.1, .2.1.4.2, and X2.1.5

page 25 Text

In paragraph X2.1.5, the first sentence should be changed to "Tables X2.1 through X2.6 ..."

page 25 Table X2.5

ER - residental and commercial/industrial values do not round-off to exactly 12/day and 20/day

Change units on infiltration rate, I, to cm/yr (3 occurrences).

Change units on k_{oc} to (cm^3-H_2O/g-C).

Change units of k_s to (cm^3-H_2O/g-soil).

Correct definition of depth to ground water, L_{GW}, to $h_{cap} + h_v$.

Change units on ground water Darcy velocity, U_{gw}, to cm/yr (3 occurrences).

Correct value for θ_{acap} (Commercial/Industrial scenario) to 0.038 cm^3-air/cm^3-soil.

Correct value for τ (Commercial/Industrial scenario) to 7.88×10^8 s.

Page 26 Table X2.6

The benzo(a)pyrene Henry's law coefficient as given (1.4E-9) is in units of atm-m^3/mol. This converts to H = 5.8E-8 in units of L-H2O/L-air at a temperature of 293 K.

The cited ethylbenzene organic carbon partition coefficient of 1.98 traces to Chiou, C.T., et al., 1983: Env. Sci. Tech., 17, (4), p.227, and is for organic matter, not organic carbon. Recommend replacing with Koc = 3.11 (ref. 22) or the same Koc value as in Table X1.2.

Equation in footnote E should be changed

from $\log(K_{oc}) = 0.937 \log(K_{oc}) - 0.006$

to $\log(K_{oc}) = 0.937 \log(K_{ow}) - 0.006$

page 29 Text

In paragraph X2.10.1, first sentence change reference from Table X2.1 to Table 4.

page 31 Table X3.1

For the equation for steady-state attenuation, raise the quantity $(1 + 4 \lambda \alpha_x / u)$ to the 0.5 power (i.e., take the square root of this quantity).

For the equation describing the effective porous media diffusion coefficient, change the denominator terms from $\theta_T^{3.33}$ to θ_T^2.

page 33 Table X3.1

Change the dimensions for W from "z" to "cm"

In the event that additional errata are discovered upon further review of this document, we will inform you of any necessary changes.

G.E. DeVaull

R.A. Ettinger

SEPTEMBER 14, 1994

FROM: R.A. ETTINGER AND J.B. GUSTAFSON

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SUBJECT: ADDITIONAL ERRATA TO ASTM ES 38-94

The following errata have been discovered in addition to those documented in the September 12, 1994 memo.

Page 19 Text

In paragraph 1.6.1.3, change the MCL and MCLG value from "10 000 g/L" to "10 000 µg/L".

Page 27 Text

In paragraph 2.6.6, first sentence, change from "ground water" to "surficial soils".

Page 34 Text

The last sentence in paragraph X3.6.1.1 is not continuous with paragraph X3.6.1.2. Change "that are discussed as follows:" to "which are discussed below."

Page 35 Text

In paragraph 3.6.9 change reference to 6.5 to X3.5.

Page 2 of Errata sheet dated September 12, 1994.

In the first RBSL table for Pathway: Groundwater Volatilization to Indoor Air, the RBSL units should be changed from mg/kg to mg/L.

APPENDIX C

Spreadsheet Calculations of Tier 2 SSTLs

DEVELOPMENT OF TIER 2 SITE SPECIFIC TARGET LEVELS (SSTLs)
Based on ASTM RBCA Guidance E 1739-95 Nov. 1995
Residential Exposure Scenario
EXPOSURE FACTORS AND OTHER RELEVANT PARAMETERS

PARAMETER	Units	Input Value	Reference
EXPOSURE PARAMETERS			
Averaging Time for Carcinogens	yr	70	ASTM 1995 - Guide for RBCA
Averaging Time for Noncarcinogens	yr	30	ASTM 1995 - Guide for RBCA
Body Weight Adult	kg	70	ASTM 1995 - Guide for RBCA
Body Weight Child	kg	15	DTSC 1994 - PEA Guidance
Exposure Duration Adult	yr	24	ASTM 1995 - Guide for RBCA
Exposure Duration Child	yr	6	DTSC 1994 - PEA Guidance
Exposure Frequency	days/yr	350	ASTM 1995 - Guide for RBCA
Soil ingestion rate Adult	mg/day	100	ASTM 1995 - Guide for RBCA
Soil ingestion rate Child	mg/day	200	DTSC 1994 - PEA Guidance
Daily Indoor Inhalation Rate Adult	m^3/day	15	ASTM 1995 - Guide for RBCA
Daily Indoor Inhalation Rate Child	m^3/day	15	DTSC 1994 - PEA Guidance
Daily Outdoor Inhalation Rate Adult	m^3/day	1.7	equivalent to two hour/day exposure
Daily Outdoor Inhalation Rate Child	m^3/day	0.8	equivalent to two hour/day exposure
Daily water ingestion rate Adult	L/day	2	ASTM 1995 - Guide for RBCA
Daily water ingestion rate Child	L/day	1	DTSC 1994 - PEA Guidance
Soil to skin adherence factor	mg/cm^2	0.5	ASTM 1995 - Guide for RBCA
Dermal relative absorption factor (volatiles)	---	0.5	ASTM 1995 - Guide for RBCA
Dermal relative absorption factor (PAHs)	---	0.05	ASTM 1995 - Guide for RBCA
Oral relative absorption factor	---	1	ASTM 1995 - Guide for RBCA
Skin surface area Adult	cm^2	3,160	ASTM 1995 - Guide for RBCA
Skin surface area Child	cm^2	2,000	DTSC 1994 - PEA Guidance
Target Hazard Quotient for individual constituents	---	1	ASTM 1995 - Guide for RBCA
Target Excess Individual Lifetime Cancer Risk	---	1.0E-5	ASTM 1995 - Guide for RBCA
CONTAMINANT FATE AND TRANSPORT PARAMETERS			
Lower depth of surficial soil zone	cm	100	ASTM 1995 - Guide for RBCA
Enclosed space air exchange rate	1/sec	0.00014	ASTM 1995 - Guide for RBCA
Fraction of organic carbon in soil	g-C/g-soil	0.01	ASTM 1995 - Guide for RBCA
Thickness of capillary fringe	cm	5	ASTM 1995 - Guide for RBCA
Thickness of vadose zone	cm	295	ASTM 1995 - Guide for RBCA
Infiltration rate of water through soil	cm/yr	30	ASTM 1995 - Guide for RBCA
Enclosed space volume/infiltration area	cm	200	ASTM 1995 - Guide for RBCA
Enclosed space foundation/wall thickness	cm	15	ASTM 1995 - Guide for RBCA
Depth to groundwater	cm	300	ASTM 1995 - Guide for RBCA
Depth to subsurface soil sources	cm	100	ASTM 1995 - Guide for RBCA
Particulate emission rate	g/cm^2-s	1.5E-09	selected to correspond to 50 $\mu g/m^3$
Wind speed above ground surface in ambient mixing zone	cm/s	225	ASTM 1995 - Guide for RBCA
Groundwater Darcy velocity	cm/yr	2500.0	ASTM 1995 - Guide for RBCA
Width of source area parallel to wind or gw flow	cm	1500	ASTM 1995 - Guide for RBCA
Ambient air mixing zone height	cm	200	ASTM 1995 - Guide for RBCA
Groundwater mixing zone height	cm	200	ASTM 1995 - Guide for RBCA
Areal fraction of cracks in foundation/walls	cm^2/cm^2	0.01	ASTM 1995 - Guide for RBCA
Volumetric air content in capillary fringe soils	cc/cc	0.038	ASTM 1995 - Guide for RBCA
Volumetric air content in found./wall cracks	cc/cc	0.26	ASTM 1995 - Guide for RBCA
Volumetric air content in vadose zone soils	cc/cc	0.26	ASTM 1995 - Guide for RBCA
Total soil porosity	cc/cc-soil	0.38	ASTM 1995 - Guide for RBCA
Volumetric water content in capillary fringe soils	cc/cc	0.342	ASTM 1995 - Guide for RBCA
Volumetric water content in found./wall cracks	cc/cc	0.12	ASTM 1995 - Guide for RBCA
Volumetric water content in vadose zone soils	cc/cc	0.12	ASTM 1995 - Guide for RBCA
Soil bulk density	g/cc	1.7	ASTM 1995 - Guide for RBCA
Averaging time for vapor flux	sec	7.88E+8	ASTM 1995 - Guide for RBCA

Reference : ASTM 1995. Standard Guide for Risk-Based Corrective Action Applied at Petroleum Release Sites. E 1739-95. November.

Residential Exposure Scenario
CHEMICAL-SPECIFIC TOXICITY PARAMETERS

CHEMICAL	SLOPE FACTOR				REFERENCE DOSE			
	ORAL		INHALATION		ORAL		INHALATION	
	[1/(mg/kg-day)]	ref.	[1/(mg/kg-day)]	ref.	[mg/kg-day]	ref.	[mg/kg-day]	ref.
Benzene	1.1E-1	cal/epa	1.1E-1	cal/epa	1.7E-3	r	1.7E-3	n
Toluene	na	ASTM	na	ASTM	2.0E-1	ASTM	1.1E-1	ASTM
Ethylbenzene	na	ASTM	na	ASTM	1.0E-1	ASTM	2.9E-1	ASTM
Xylene (mixed)	na	ASTM	na	ASTM	2.0E+0	ASTM	2.0E+0	ASTM
Naphthalene	na	ASTM	na	ASTM	4.0E-2	n	4.0E-2	r
Benzo(a)pyrene	7.3E+0	ASTM	7.3E+0	ASTM	na	ASTM	na	ASTM
MTBE	na	--	na	--	5.0E-3	n	8.6E-1	i

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References

ASTM = Standard Guide for Risk-Based Corrective Action Applied at Petroleum Release Sites (ASTM E 1739-95, November, 1995).

(i,n,x,r,h) = As referenced in US EPA Region IX Preliminary Remediation Goals (PRGs) 1996. ✓

cal/epa = Cal/EPA Memorandum on California Cancer Potency Factors: Update 11/94

na = Not Applicable/Not Available.

Residential Exposure Scenario
CHEMICAL-SPECIFIC FATE AND TRANSPORT PARAMETERS

CHEMICAL	Koc [cm^3/g]	H [atm-m^3/mol]	H' = H/RT [--]	Solubility [mg/L]	Dair [cm^2/sec]	Dwater [cm^2/sec]	ABS [--]
Benzene	6.5E+1	5.5E-3	2.3E-1	1.8E+3	9.3E-2	1.10E-5	0.5
Toluene	1.4E+2	6.6E-3	2.7E-1	5.4E+2	8.5E-2	9.40E-6	0.5
Ethylbenzene	2.2E+2	7.9E-3	3.2E-1	1.5E+2	7.6E-2	8.50E-6	0.5
Xylene (mixed)	2.4E+2	5.3E-3	2.2E-1	2.0E+2	8.7E-2	8.50E-6	0.5
Naphthalene	1.3E+3	1.3E-3	5.3E-2	3.1E+1	7.2E-2	9.40E-6	0.05
Benzo(a)pyrene	3.9E+5	1.4E-9	5.7E-8	1.2E-3	5.0E-2	5.80E-6	0.05
MTBE	1.2E+1	5.4E-4	2.2E-2	5.1E+4	1.0E-1	1.10E-5	0.5

Definitions of Parameters
Koc = Organic carbon partition coefficient
H = Henry's Law constant
Dair = Diffusion coefficient in air
Dwater = Diffusion coefficient in water
ABS = Dermal Absorption Factor

References

Basics of Pump and Treat Groundwater Remediation Technology. EPA Office of Research and Development. EPA/600/8-90/003. March 1990.
US EPA Region IX Preliminary Remediation Goals (PRGs) 1996.
ASTM Standard Guide for Risk-Based Corrective Action Applied at Petroleum Release Sites (November, 1995).

Residential Exposure Scenario
CHEMICAL-SPECIFIC FATE AND TRANSPORT DIFFUSION PARAMETERS

CHEMICAL	Ds [cm^2/s]	Dcrack [cm^2/s]	Dcap [cm^2/s]	Dws [cm^2/s]	Csat [mg/kg]	Kd [cm^3/g]
Benzene	7.26E-3	7.26E-3	2.15E-5	1.10E-3	1.32E+3	6.50E-1
Toluene	6.63E-3	6.63E-3	1.77E-5	9.19E-4	7.82E+2	1.35E+0
Ethylbenzene	5.93E-3	5.93E-3	1.49E-5	7.79E-4	3.53E+2	2.20E+0
Xylene (mixed)	6.79E-3	6.79E-3	1.88E-5	9.71E-4	4.96E+2	2.40E+0
Naphthalene	5.62E-3	5.62E-3	4.36E-5	1.79E-3	4.02E+2	1.29E+1
Benzo(a)pyrene	6.05E-1	6.05E-1	1.96E+1	6.14E-1	4.67E+0	3.89E+3
MTBE	7.81E-3	7.81E-3	1.10E-4	3.60E-3	9.89E+3	1.20E-1

Definitions of Parameters
Ds = Effective diffusion coefficient in soil based on vapor-phase concentration
Dcrack = Effective diffusion coefficient through foundation cracks
Dcap = Effective diffusion coefficient through capillary fringe
Dws = Effective diffusion coefficient between groundwater and soil surface
Csat = Saturated soil concentration

Residential Exposure Scenario
CHEMICAL-SPECIFIC FATE AND TRANSPORT VOLATILIZATION FACTORS

CHEMICAL	VOLATILIZATION FACTORS							
	VFwesp [mg/m^3-air/ mg/L-H2O]	VFwamb [mg/m^3-air/ mg/L-H2O]	VFss1 [mg/m^3-air/ mg/kg-soil]	VFss2 [mg/m^3-air/ mg/kg-soil]	VFp [mg/m^3-air/ mg/kg-soil]	VFsamb [mg/m^3-air/ mg/kg-soil]	VFsesp [mg/m^3-air/ mg/kg-soil]	LFsw [mg/L/ mg/kg]
Benzene	1.68E-2	2.75E-5	8.14E-5	7.19E-6	5.00E-8	7.22E-4	4.84E-2	1.09E-1
Toluene	1.75E-2	2.76E-5	6.12E-5	7.19E-6	5.00E-8	4.09E-4	2.74E-2	5.65E-2
Ethylbenzene	1.81E-2	2.81E-5	5.03E-5	7.19E-6	5.00E-8	2.76E-4	1.85E-2	3.56E-2
Xylene (mixed)	1.46E-2	2.35E-5	4.24E-5	7.19E-6	5.00E-8	1.96E-4	1.32E-2	3.30E-2
Naphthalene	4.38E-3	1.06E-5	8.40E-6	7.19E-6	5.00E-8	7.70E-6	5.16E-4	6.37E-3
Benzo(a)pyrene	6.82E-7	3.92E-9	5.22E-9	7.19E-6	5.00E-8	2.97E-12	1.96E-10	2.12E-5
MTBE	2.87E-3	8.84E-6	5.22E-5	7.19E-6	5.00E-8	2.97E-4	1.99E-2	4.26E-1

Definitions of Factors

VFwesp = Volatilization factor from groundwater to enclosed-space vapors
VFwamb = Volatilization factor from groundwater to ambient (outdoor) vapors
VFss = Volatilization factor from surficial soils to ambient air (vapors)
VFp = Volatilization factor from surficial soils to ambient air (particulates)
VFsamb = Volatilization factor from subsurface soils to ambient air
VFsesp = Volatilization factor from subsurface soils to enclosed space vapors
LFsw = Leaching factor from subsurface soils to ground water

Residential Exposure Scenario
SUMMARY OF TARGET LEVELS FOR SOIL EXPOSURE PATHWAYS

CHEMICAL	SOIL TARGET LEVELS (1,2)			
	Surficial Soil [mg/kg]	Indoor Soil Emiss. [mg/kg]	Outdoor Soil Emiss. [mg/kg]	Leaching to GW (MCL) [mg/kg]
Benzene	1.1E+1	1.2E-2	1.0E+1	2.6E-2
Toluene	7.8E+2 *	2.2E+1	7.8E+2 *	1.0E+1
Ethylbenzene	3.5E+2 *	8.0E+1	3.5E+2 *	1.1E+1
Xylene (mixed)	5.0E+2 *	5.0E+2 *	5.0E+2 *	1.7E+2
Naphthalene	4.0E+2 *	4.0E+2 *	4.0E+2 *	1.8E-2
Benzo(a)pyrene	6.2E-1	4.7E+0 *	4.7E+0 *	4.7E+0 *
MTBE	5.6E+2	2.2E+2	9.9E+3 *	4.0E-2

* Indicates SSTL exceeded pure component soil saturation limit and hence saturation is listed as SSTL

na = Not Applicable/Not Available

(1) Calculated using the equations in ASTM RBCA guidance. Target risk concentrations are corresponding to a cancer risk of one in 100000 or a non-carcinogenic hazard quotient of unity for the exposure pathway being evaluated.

(2) The SSTL is the lower of the target risk concentrations for carcinogenic and non-carcinogenic effect, unless they exceed soil saturation of water solubility, in which case the SSTL is set at saturation or solubility concentration.

Residential Exposure Scenario

SUMMARY OF TARGET LEVELS FOR WATER EXPOSURE PATHWAYS

CHEMICAL	MCL [mg/L]	SHALLOW GROUNDWATER TARGET LEVELS (1,2)		
		Water Ingestion [mg/L]	Outdoor GW Emissions [mg/L]	Indoor GW Emissions [mg/L]
Benzene	5.0E-3	6.1E-3	1.8E+3 *	3.5E-2
Toluene	1.0E+0	1.6E+1	5.4E+2 *	3.4E+1
Ethylbenzene	7.0E-1	7.8E+0	1.5E+2 *	8.2E+1
Xylene (mixed)	1.0E+1	1.6E+2	2.0E+2 *	2.0E+2 *
Naphthalene	2.0E-4	3.1E+0	3.1E+1 *	3.1E+1 *
Benzo(a)pyrene	2.0E-4	9.2E-5	1.2E-3 *	1.2E-3 *
MTBE	3.0E-2	3.9E-1	5.1E+4 *	1.6E+3

* Indicates SSTL exceeded pure component water solubility and hence water solubility is listed as SSTL

na = Not Applicable/Not Available

(1) Calculated using the equations in ASTM RBCA guidance. Target risk concentrations are corresponding to a cancer risk of one in 100000 or a non-carcinogenic hazard quotient of unity for the exposure pathway being evaluated.

(2) The SSTL is the lower of the target risk concentrations for carcinogenic and non-carcinogenic effect, unless they exceed soil saturation of water solubility, in which case the SSTL is set at saturation or solubility concentration.

Residential Exposure Scenario
SUMMARY OF TARGET LEVELS FOR AIR EXPOSURE PATHWAYS

CHEMICAL	AIR TARGET LEVELS (1,2)	
	Indoor Inhalation [mg/m^3]	Outdoor Inhalation [mg/m^3]
Benzene	6.0E-1	7.3E+0
Toluene	5.9E+2	1.1E+4
Ethylbenzene	1.5E+3	2.7E+4
Xylene (mixed)	1.0E+4	1.9E+5
Naphthalene	2.1E+2	3.8E+3
Benzo(a)pyrene	9.0E-3	1.1E-1
MTBE	4.5E+3	8.0E+4

* Indicates SSTL exceeded pure component water solubility and hence water solubility is listed as SSTL

na = Not Applicable/Not Available

(1) Calculated using the equations in ASTM RBCA guidance. Target risk concentrations are corresponding to a cancer risk of one in 100000 or a non-carcinogenic hazard quotient of unity for the exposure pathway being evaluated.

(2) The SSTL is the lower of the target risk concentrations for carcinogenic and non-carcinogenic effect, unless they exceed soil saturation of water solubility, in which case the SSTL is set at saturation or solubility concentration.

DEVELOPMENT OF TIER 2 SITE SPECIFIC TARGET LEVELS (SSTLs)
Based on ASTM RBCA Guidance E 1739-95 Nov. 1995
Commercial Exposure Scenario
EXPOSURE FACTORS AND OTHER RELEVANT PARAMETERS

PARAMETER	Units	Input Value	Reference
EXPOSURE PARAMETERS			
Averaging Time for Carcinogens	yr	70	ASTM 1995 - Guide for RBCA
Averaging Time for Noncarcinogens	yr	25	ASTM 1995 - Guide for RBCA
Body Weight Adult	kg	70	ASTM 1995 - Guide for RBCA
Exposure Duration Adult	yr	25	ASTM 1995 - Guide for RBCA
Exposure Frequency	days/yr	250	ASTM 1995 - Guide for RBCA
Soil ingestion rate Adult	mg/day	100	ASTM 1995 - Guide for RBCA
Daily Indoor Inhalation Rate Adult	m^3/day	15	ASTM 1995 - Guide for RBCA
Daily Outdoor Inhalation Rate Adult	m^3/day	20	ASTM 1995 - Guide for RBCA
Daily water ingestion rate Adult	L/day	2	ASTM 1995 - Guide for RBCA
Soil to skin adherence factor	mg/cm^2	0.5	ASTM 1995 - Guide for RBCA
Dermal relative absorption factor (volatiles)	---	0.5	ASTM 1995 - Guide for RBCA
Dermal relative absorption factor (PAHs)	---	0.05	ASTM 1995 - Guide for RBCA
Oral relative absorption factor	---	1	ASTM 1995 - Guide for RBCA
Skin surface area Adult	cm^2	3,160	ASTM 1995 - Guide for RBCA
Target Hazard Quotient for individual constituents	---	1	ASTM 1995 - Guide for RBCA
Target Excess Individual Lifetime Cancer Risk	---	1.0E-5	ASTM 1995 - Guide for RBCA
CONTAMINANT FATE AND TRANSPORT PARAMETERS			
Lower depth of surficial soil zone	cm	100	ASTM 1995 - Guide for RBCA
Enclosed space air exchange rate	1/sec	0.00023	ASTM 1995 - Guide for RBCA
Fraction of organic carbon in soil	g-C/g-soil	0.01	ASTM 1995 - Guide for RBCA
Thickness of capillary fringe	cm	5	ASTM 1995 - Guide for RBCA
Thickness of vadose zone	cm	295	ASTM 1995 - Guide for RBCA
Infiltration rate of water through soil	cm/yr	30	ASTM 1995 - Guide for RBCA
Enclosed space volume/infiltration area	cm	300	ASTM 1995 - Guide for RBCA
Enclosed space foundation/wall thickness	cm	15	ASTM 1995 - Guide for RBCA
Depth to groundwater	cm	300	ASTM 1995 - Guide for RBCA
Depth to subsurface soil sources	cm	100	ASTM 1995 - Guide for RBCA
Particulate emission rate	g/cm^2-s	1.5E-09	selected to correspond to 50 $\mu g/m^3$
Wind speed above ground surface in ambient mixing zone	cm/s	225	ASTM 1995 - Guide for RBCA
Groundwater Darcy velocity	cm/yr	2500.0	ASTM 1995 - Guide for RBCA
Width of source area parallel to wind or gw flow	cm	1500	ASTM 1995 - Guide for RBCA
Ambient air mixing zone height	cm	200	ASTM 1995 - Guide for RBCA
Groundwater mixing zone height	cm	200	ASTM 1995 - Guide for RBCA
Areal fraction of cracks in foundation/walls	cm^2/cm^2	0.0005	corresponding to a 50-fold reduction factor
Volumetric air content in capillary fringe soils	cc/cc	0.038	ASTM 1995 - Guide for RBCA
Volumetric air content in found./wall cracks	cc/cc	0.26	ASTM 1995 - Guide for RBCA
Volumetric air content in vadose zone soils	cc/cc	0.26	ASTM 1995 - Guide for RBCA
Total soil porosity	cc/cc-soil	0.38	ASTM 1995 - Guide for RBCA
Volumetric water content in capillary fringe soils	cc/cc	0.342	ASTM 1995 - Guide for RBCA
Volumetric water content in found./wall cracks	cc/cc	0.12	ASTM 1995 - Guide for RBCA
Volumetric water content in vadose zone soils	cc/cc	0.12	ASTM 1995 - Guide for RBCA
Soil bulk density	g/cc	1.7	ASTM 1995 - Guide for RBCA
Averaging time for vapor flux	sec	7.88E+8	ASTM 1995 - Guide for RBCA

Reference : ASTM 1995. Standard Guide for Risk-Based Corrective Action Applied at Petroleum Release Sites. E 1739-95. November.

Commercial Exposure Scenario
CHEMICAL-SPECIFIC TOXICITY PARAMETERS

CHEMICAL	SLOPE FACTOR				REFERENCE DOSE			
	ORAL		INHALATION		ORAL		INHALATION	
	[1/(mg/kg-day)]	ref.	[1/(mg/kg-day)]	ref.	[mg/kg-day]	ref.	[mg/kg-day]	ref.
Benzene	1.1E-1	cal/epa	1.1E-1	cal/epa	1.7E-3	r	1.7E-3	n
Toluene	na	ASTM	na	ASTM	2.0E-1	ASTM	1.1E-1	ASTM
Ethylbenzene	na	ASTM	na	ASTM	1.0E-1	ASTM	2.9E-1	ASTM
Xylene (mixed)	na	ASTM	na	ASTM	2.0E+0	ASTM	2.0E+0	ASTM
Naphthalene	na	ASTM	na	ASTM	4.0E-2	n	4.0E-2	r
Benzo(a)pyrene	7.3E+0	ASTM	7.3E+0	ASTM	na	ASTM	na	ASTM
MTBE	na	--	na	--	5.0E-3	n	8.6E-1	i

References
ASTM = Standard Guide for Risk-Based Corrective Action Applied at Petroleum Release Sites (ASTM E 1739-95, November, 1995).
(i,n,x,r,h) = As referenced in US EPA Region IX Preliminary Remediation Goals (PRGs) 1996.
cal/epa = Cal/EPA Memorandum on California Cancer Potency Factors: Update 11/94
na = Not Applicable/Not Available.

Commercial Exposure Scenario
CHEMICAL-SPECIFIC FATE AND TRANSPORT PARAMETERS

CHEMICAL	Koc [cm^3/g]	H [atm-m^3/mol]	H' = H/RT [--]	Solubility [mg/L]	Dair [cm^2/sec]	Dwater [cm^2/sec]	ABS [--]
Benzene	6.5E+1	5.5E-3	2.3E-1	1.8E+3	9.3E-2	1.10E-5	0.5
Toluene	1.4E+2	6.6E-3	2.7E-1	5.4E+2	8.5E-2	9.40E-6	0.5
Ethylbenzene	2.2E+2	7.9E-3	3.2E-1	1.5E+2	7.6E-2	8.50E-6	0.5
Xylene (mixed)	2.4E+2	5.3E-3	2.2E-1	2.0E+2	8.7E-2	8.50E-6	0.5
Naphthalene	1.3E+3	1.3E-3	5.3E-2	3.1E+1	7.2E-2	9.40E-6	0.05
Benzo(a)pyrene	3.9E+5	1.4E-9	5.7E-8	1.2E-3	5.0E-2	5.80E-6	0.05
MTBE	1.2E+1	5.4E-4	2.2E-2	5.1E+4	1.0E-1	1.10E-5	0.5

Definitions of Parameters
Koc = Organic carbon partition coefficient
H = Henry's Law constant
Dair = Diffusion coefficient in air
Dwater = Diffusion coefficient in water
ABS = Dermal Absorption Factor

References

Basics of Pump and Treat Groundwater Remediation Technology. EPA Office of Research and Development. EPA/600/8-90/003. March 1990.
US EPA Region IX Preliminary Remediation Goals (PRGs) 1996.
ASTM Standard Guide for Risk-Based Corrective Action Applied at Petroleum Release Sites (November, 1995).

Commercial Exposure Scenario
CHEMICAL-SPECIFIC FATE AND TRANSPORT DIFFUSION PARAMETERS

CHEMICAL	Ds [cm^2/s]	Dcrack [cm^2/s]	Dcap [cm^2/s]	Dws [cm^2/s]	Csat [mg/kg]	Kd [cm^3/g]
Benzene	7.26E-3	7.26E-3	2.15E-5	1.10E-3	1.32E+3	6.50E-1
Toluene	6.63E-3	6.63E-3	1.77E-5	9.19E-4	7.82E+2	1.35E+0
Ethylbenzene	5.93E-3	5.93E-3	1.49E-5	7.79E-4	3.53E+2	2.20E+0
Xylene (mixed)	6.79E-3	6.79E-3	1.88E-5	9.71E-4	4.96E+2	2.40E+0
Naphthalene	5.62E-3	5.62E-3	4.36E-5	1.79E-3	4.02E+2	1.29E+1
Benzo(a)pyrene	6.05E-1	6.05E-1	1.96E+1	6.14E-1	4.67E+0	3.89E+3
MTBE	7.81E-3	7.81E-3	1.10E-4	3.60E-3	9.89E+3	1.20E-1

Definitions of Parameters
Ds = Effective diffusion coefficient in soil based on vapor-phase concentration
Dcrack = Effective diffusion coefficient through foundation cracks
Dcap = Effective diffusion coefficient through capillary fringe
Dws = Effective diffusion coefficient between groundwater and soil surface
Csat = Saturated soil concentration

Commercial Exposure Scenario
CHEMICAL-SPECIFIC FATE AND TRANSPORT VOLATILIZATION FACTORS

CHEMICAL	VOLATILIZATION FACTORS							LFsw
	VFwesp [mg/m^3-air/ mg/L-H2O]	VFwamb [mg/m^3-air/ mg/L-H2O]	VFss1 [mg/m^3-air/ mg/kg-soil]	VFss2 [mg/m^3-air/ mg/kg-soil]	VFp [mg/m^3-air/ mg/kg-soil]	VFsamb [mg/m^3-air/ mg/kg-soil]	VFsesp [mg/m^3-air/ mg/kg-soil]	[mg/L/ mg/kg]
Benzene	7.42E-4	2.75E-5	8.14E-5	7.19E-6	5.00E-8	7.22E-4	1.04E-3	1.09E-1
Toluene	8.09E-4	2.76E-5	6.12E-5	7.19E-6	5.00E-8	4.09E-4	5.91E-4	5.65E-2
Ethylbenzene	8.62E-4	2.81E-5	5.03E-5	7.19E-6	5.00E-8	2.76E-4	3.99E-4	3.56E-2
Xylene (mixed)	6.66E-4	2.35E-5	4.24E-5	7.19E-6	5.00E-8	1.96E-4	2.84E-4	3.30E-2
Naphthalene	1.40E-4	1.06E-5	8.40E-6	7.19E-6	5.00E-8	7.70E-6	1.11E-5	6.37E-3
Benzo(a)pyrene	1.66E-8	3.92E-9	5.22E-9	7.19E-6	5.00E-8	2.97E-12	4.29E-12	2.12E-5
MTBE	8.17E-5	8.84E-6	5.22E-5	7.19E-6	5.00E-8	2.97E-4	4.29E-4	4.26E-1

Definitions of Factors

VFwesp = Volatilization factor from groundwater to enclosed-space vapors
VFwamb = Volatilization factor from groundwater to ambient (outdoor) vapors
VFss = Volatilization factor from surficial soils to ambient air (vapors)
VFp = Volatilization factor from surficial soils to ambient air (particulates)
VFsamb = Volatilization factor from subsurface soils to ambient air
VFsesp = Volatilization factor from subsurface soils to enclosed space vapors
LFsw = Leaching factor from subsurface soils to ground water

Commercial Exposure Scenario
SUMMARY OF TARGET LEVELS FOR SOIL EXPOSURE PATHWAYS

CHEMICAL	SOIL TARGET LEVELS (1,2)			
	Surficial Soil [mg/kg]	Indoor Soil Emiss. [mg/kg]	Outdoor Soil Emiss. [mg/kg]	Leaching to GW (MCL) [mg/kg]
Benzene	2.5E+1	1.7E+0	1.8E+0	2.6E-2
Toluene	7.8E+2 *	7.8E+2 *	7.8E+2 *	1.0E+1
Ethylbenzene	3.5E+2 *	3.5E+2 *	3.5E+2 *	1.1E+1
Xylene (mixed)	5.0E+2 *	5.0E+2 *	5.0E+2 *	1.7E+2
Naphthalene	4.0E+2 *	4.0E+2 *	4.0E+2 *	1.8E-2
Benzo(a)pyrene	2.2E+0	4.7E+0 *	4.7E+0 *	4.7E+0 *
MTBE	5.7E+2	9.9E+3 *	9.9E+3 *	4.0E-2

* Indicates SSTL exceeded pure component soil saturation limit and hence saturation is listed as SSTL
na = Not Applicable/Not Available
(1) Calculated using the equations in ASTM RBCA guidance. Target risk concentrations are corresponding to a cancer risk of one in 100000 or a non-carcinogenic hazard quotient of unity for the exposure pathway being evaluated.
(2) The SSTL is the lower of the target risk concentrations for carcinogenic and non-carcinogenic effect, unless they exceed soil saturation of water solubility, in which case the SSTL is set at saturation or solubility concentration.

Commercial Exposure Scenario
SUMMARY OF TARGET LEVELS FOR WATER EXPOSURE PATHWAYS

CHEMICAL	MCL [mg/L]	SHALLOW GROUNDWATER TARGET LEVELS (1,2)		
		Water Ingestion [mg/L]	Outdoor GW Emissions [mg/L]	Indoor GW Emissions [mg/L]
Benzene	5.0E-3	1.3E-2	4.7E+1	2.3E+0
Toluene	1.0E+0	1.0E+1	5.4E+2 *	5.4E+2 *
Ethylbenzene	7.0E-1	5.1E+0	1.5E+2 *	1.5E+2 *
Xylene (mixed)	1.0E+1	1.0E+2	2.0E+2 *	2.0E+2 *
Naphthalene	2.0E-4	2.0E+0	3.1E+1 *	3.1E+1 *
Benzo(a)pyrene	2.0E-4	2.0E-4	1.2E-3 *	1.2E-3 *
MTBE	3.0E-2	2.6E-1	5.1E+4 *	5.1E+4 *

* Indicates SSTL exceeded pure component water solubility and hence water solubility is listed as SSTL

na = Not Applicable/Not Available

(1) Calculated using the equations in ASTM RBCA guidance. Target risk concentrations are corresponding to a cancer risk of one in 100000 or a non-carcinogenic hazard quotient of unity for the exposure pathway being evaluated.

(2) The SSTL is the lower of the target risk concentrations for carcinogenic and non-carcinogenic effect, unless they exceed soil saturation of water solubility, in which case the SSTL is set at saturation or solubility concentration.

Commercial Exposure Scenario
SUMMARY OF TARGET LEVELS FOR AIR EXPOSURE PATHWAYS

CHEMICAL	AIR TARGET LEVELS (1,2)	
	Indoor Inhalation [mg/m^3]	Outdoor Inhalation [mg/m^3]
Benzene	1.7E+0	1.3E+0
Toluene	7.8E+2	5.8E+2
Ethylbenzene	1.9E+3	1.5E+3
Xylene (mixed)	1.4E+4	1.0E+4
Naphthalene	2.7E+2	2.0E+2
Benzo(a)pyrene	2.6E-2	2.0E-2
MTBE	5.8E+3	4.4E+3

* Indicates SSTL exceeded pure component water solubility and hence water solubility is listed as SSTL
na = Not Applicable/Not Available
(1) Calculated using the equations in ASTM RBCA guidance. Target risk concentrations are corresponding to a cancer risk of one in 100000 or a non-carcinogenic hazard quotient of unity for the exposure pathway being evaluated.
(2) The SSTL is the lower of the target risk concentrations for carcinogenic and non-carcinogenic effect, unless they exceed soil saturation of water solubility, in which case the SSTL is set at saturation or solubility concentration.

DEVELOPMENT OF TIER 2 SITE SPECIFIC TARGET LEVELS (SSTLs)
Based on ASTM RBCA Guidance E 1739-95 Nov. 1995
Construction Exposure Scenario
EXPOSURE FACTORS AND OTHER RELEVANT PARAMETERS

PARAMETER	Units	Input Value	Reference
EXPOSURE PARAMETERS			
Averaging Time for Carcinogens	yr	70	ASTM 1995 - Guide for RBCA
Averaging Time for Noncarcinogens	yr	25	ASTM 1995 - Guide for RBCA
Body Weight Adult	kg	70	ASTM 1995 - Guide for RBCA
Exposure Duration Adult	yr	0.5	six month exposure duration
Exposure Frequency	days/yr	250	ASTM 1995 - Guide for RBCA
Soil ingestion rate Adult	mg/day	100	ASTM 1995 - Guide for RBCA
Daily Indoor Inhalation Rate Adult	m^3/day	15	ASTM 1995 - Guide for RBCA
Daily Outdoor Inhalation Rate Adult	m^3/day	20	ASTM 1995 - Guide for RBCA
Daily water ingestion rate Adult	L/day	2	ASTM 1995 - Guide for RBCA
Soil to skin adherence factor	mg/cm^2	0.5	ASTM 1995 - Guide for RBCA
Dermal relative absorption factor (volatiles)	---	0.5	ASTM 1995 - Guide for RBCA
Dermal relative absorption factor (PAHs)	---	0.05	ASTM 1995 - Guide for RBCA
Oral relative absorption factor	---	1	ASTM 1995 - Guide for RBCA
Skin surface area Adult	cm^2	3,160	ASTM 1995 - Guide for RBCA
Target Hazard Quotient for individual constituents	---	1	ASTM 1995 - Guide for RBCA
Target Excess Individual Lifetime Cancer Risk	---	1.0E-5	ASTM 1995 - Guide for RBCA
CONTAMINANT FATE AND TRANSPORT PARAMETERS			
Lower depth of surficial soil zone	cm	100	ASTM 1995 - Guide for RBCA
Enclosed space air exchange rate	1/sec	0.00014	ASTM 1995 - Guide for RBCA
Fraction of organic carbon in soil	g-C/g-soil	0.01	ASTM 1995 - Guide for RBCA
Thickness of capillary fringe	cm	5	ASTM 1995 - Guide for RBCA
Thickness of vadose zone	cm	295	ASTM 1995 - Guide for RBCA
Infiltration rate of water through soil	cm/yr	30	ASTM 1995 - Guide for RBCA
Enclosed space volume/infiltration area	cm	200	ASTM 1995 - Guide for RBCA
Enclosed space foundation/wall thickness	cm	15	ASTM 1995 - Guide for RBCA
Depth to groundwater	cm	300	ASTM 1995 - Guide for RBCA
Depth to subsurface soil sources	cm	100	ASTM 1995 - Guide for RBCA
Particulate emission rate	g/cm^2-s	1.5E-09	selected to correspond to 50 $\mu g/m^3$
Wind speed above ground surface in ambient mixing zone	cm/s	225	ASTM 1995 - Guide for RBCA
Groundwater Darcy velocity	cm/yr	2500.0	ASTM 1995 - Guide for RBCA
Width of source area parallel to wind or gw flow	cm	1500	ASTM 1995 - Guide for RBCA
Ambient air mixing zone height	cm	200	ASTM 1995 - Guide for RBCA
Groundwater mixing zone height	cm	200	ASTM 1995 - Guide for RBCA
Areal fraction of cracks in foundation/walls	cm^2/cm^2	0.01	ASTM 1995 - Guide for RBCA
Volumetric air content in capillary fringe soils	cc/cc	0.038	ASTM 1995 - Guide for RBCA
Volumetric air content in found./wall cracks	cc/cc	0.26	ASTM 1995 - Guide for RBCA
Volumetric air content in vadose zone soils	cc/cc	0.26	ASTM 1995 - Guide for RBCA
Total soil porosity	cc/cc-soil	0.38	ASTM 1995 - Guide for RBCA
Volumetric water content in capillary fringe soils	cc/cc	0.342	ASTM 1995 - Guide for RBCA
Volumetric water content in found./wall cracks	cc/cc	0.12	ASTM 1995 - Guide for RBCA
Volumetric water content in vadose zone soils	cc/cc	0.12	ASTM 1995 - Guide for RBCA
Soil bulk density	g/cc	1.7	ASTM 1995 - Guide for RBCA
Averaging time for vapor flux	sec	7.88E+8	ASTM 1995 - Guide for RBCA

Reference : ASTM 1995. Standard Guide for Risk-Based Corrective Action Applied at Petroleum Release Sites. E 1739-95. November.

Construction Exposure Scenario
CHEMICAL-SPECIFIC TOXICITY PARAMETERS

CHEMICAL	SLOPE FACTOR				REFERENCE DOSE			
	ORAL		INHALATION		ORAL		INHALATION	
	[1/(mg/kg-day)]	ref.	[1/(mg/kg-day)]	ref.	[mg/kg-day]	ref.	[mg/kg-day]	ref.
Benzene	1.1E-1	cal/epa	1.1E-1	cal/epa	1.7E-3	r	1.7E-3	n
Toluene	na	ASTM	na	ASTM	2.0E-1	ASTM	1.1E-1	ASTM
Ethylbenzene	na	ASTM	na	ASTM	1.0E-1	ASTM	2.9E-1	ASTM
Xylene (mixed)	na	ASTM	na	ASTM	2.0E+0	ASTM	2.0E+0	ASTM
Naphthalene	na	ASTM	na	ASTM	4.0E-2	n	4.0E-2	r
Benzo(a)pyrene	7.3E+0	ASTM	7.3E+0	ASTM	na	ASTM	na	ASTM
MTBE	na	--	na	--	5.0E-3	n	8.6E-1	i

References
ASTM = Standard Guide for Risk-Based Corrective Action Applied at Petroleum Release Sites (ASTM E 1739-95, November, 1995).
(i,n,x,r,h) = As referenced in US EPA Region IX Preliminary Remediation Goals (PRGs) 1996.
cal/epa = Cal/EPA Memorandum on California Cancer Potency Factors: Update 11/94
na = Not Applicable/Not Available.

Construction Exposure Scenario
CHEMICAL-SPECIFIC FATE AND TRANSPORT PARAMETERS

CHEMICAL	Koc [cm^3/g]	H [atm-m^3/mol]	H' = H/RT [--]	Solubility [mg/L]	Dair [cm^2/sec]	Dwater [cm^2/sec]	ABS [--]
Benzene	6.5E+1	5.5E-3	2.3E-1	1.8E+3	9.3E-2	1.10E-5	0.5
Toluene	1.4E+2	6.6E-3	2.7E-1	5.4E+2	8.5E-2	9.40E-6	0.5
Ethylbenzene	2.2E+2	7.9E-3	3.2E-1	1.5E+2	7.6E-2	8.50E-6	0.5
Xylene (mixed)	2.4E+2	5.3E-3	2.2E-1	2.0E+2	8.7E-2	8.50E-6	0.5
Naphthalene	1.3E+3	1.3E-3	5.3E-2	3.1E+1	7.2E-2	9.40E-6	0.05
Benzo(a)pyrene	3.9E+5	1.4E-9	5.7E-8	1.2E-3	5.0E-2	5.80E-6	0.05
MTBE	1.2E+1	5.4E-4	2.2E-2	5.1E+4	1.0E-1	1.10E-5	0.5

Definitions of Parameters
Koc = Organic carbon partition coefficient
H = Henry's Law constant
Dair = Diffusion coefficient in air
Dwater = Diffusion coefficient in water
ABS = Dermal Absorption Factor

References

Basics of Pump and Treat Groundwater Remediation Technology. EPA Office of Research and Development. EPA/600/8-90/003. March 1990.
US EPA Region IX Preliminary Remediation Goals (PRGs) 1996.
ASTM Standard Guide for Risk-Based Corrective Action Applied at Petroleum Release Sites (November, 1995).

Construction Exposure Scenario
CHEMICAL-SPECIFIC FATE AND TRANSPORT DIFFUSION PARAMETERS

CHEMICAL	Ds [cm^2/s]	Dcrack [cm^2/s]	Dcap [cm^2/s]	Dws [cm^2/s]	Csat [mg/kg]	Kd [cm^3/g]
Benzene	7.26E-3	7.26E-3	2.15E-5	1.10E-3	1.32E+3	6.50E-1
Toluene	6.63E-3	6.63E-3	1.77E-5	9.19E-4	7.82E+2	1.35E+0
Ethylbenzene	5.93E-3	5.93E-3	1.49E-5	7.79E-4	3.53E+2	2.20E+0
Xylene (mixed)	6.79E-3	6.79E-3	1.88E-5	9.71E-4	4.96E+2	2.40E+0
Naphthalene	5.62E-3	5.62E-3	4.36E-5	1.79E-3	4.02E+2	1.29E+1
Benzo(a)pyrene	6.05E-1	6.05E-1	1.96E+1	6.14E-1	4.67E+0	3.89E+3
MTBE	7.81E-3	7.81E-3	1.10E-4	3.60E-3	9.89E+3	1.20E-1

Definitions of Parameters
Ds = Effective diffusion coefficient in soil based on vapor-phase concentration
Dcrack = Effective diffusion coefficient through foundation cracks
Dcap = Effective diffusion coefficient through capillary fringe
Dws = Effective diffusion coefficient between groundwater and soil surface
Csat = Saturated soil concentration

Construction Exposure Scenario
CHEMICAL-SPECIFIC FATE AND TRANSPORT VOLATILIZATION FACTORS

CHEMICAL	VOLATILIZATION FACTORS							LFsw [mg/L/ mg/kg]
	VFwesp [mg/m^3-air/ mg/L-H2O]	VFwamb [mg/m^3-air/ mg/L-H2O]	VFss1 [mg/m^3-air/ mg/kg-soil]	VFss2 [mg/m^3-air/ mg/kg-soil]	VFp [mg/m^3-air/ mg/kg-soil]	VFsamb [mg/m^3-air/ mg/kg-soil]	VFsesp [mg/m^3-air/ mg/kg-soil]	
Benzene	1.68E-2	2.75E-5	8.14E-5	7.19E-6	5.00E-8	7.22E-4	4.84E-2	1.09E-1
Toluene	1.75E-2	2.76E-5	6.12E-5	7.19E-6	5.00E-8	4.09E-4	2.74E-2	5.65E-2
Ethylbenzene	1.81E-2	2.81E-5	5.03E-5	7.19E-6	5.00E-8	2.76E-4	1.85E-2	3.56E-2
Xylene (mixed)	1.46E-2	2.35E-5	4.24E-5	7.19E-6	5.00E-8	1.96E-4	1.32E-2	3.30E-2
Naphthalene	4.38E-3	1.06E-5	8.40E-6	7.19E-6	5.00E-8	7.70E-6	5.16E-4	6.37E-3
Benzo(a)pyrene	6.82E-7	3.92E-9	5.22E-9	7.19E-6	5.00E-8	2.97E-12	1.96E-10	2.12E-5
MTBE	2.87E-3	8.84E-6	5.22E-5	7.19E-6	5.00E-8	2.97E-4	1.99E-2	4.26E-1

Definitions of Factors

VFwesp = Volatilization factor from groundwater to enclosed-space vapors
VFwamb = Volatilization factor from groundwater to ambient (outdoor) vapors
VFss = Volatilization factor from surficial soils to ambient air (vapors)
VFp = Volatilization factor from surficial soils to ambient air (particulates)
VFsamb = Volatilization factor from subsurface soils to ambient air
VFsesp = Volatilization factor from subsurface soils to enclosed space vapors
LFsw = Leaching factor from subsurface soils to ground water

Construction Exposure Scenario
SUMMARY OF TARGET LEVELS FOR SOIL EXPOSURE PATHWAYS

CHEMICAL	SOIL TARGET LEVELS (1,2)			
	Surficial Soil [mg/kg]	Indoor Soil Emiss. [mg/kg]	Outdoor Soil Emiss. [mg/kg]	Leaching to GW (MCL) [mg/kg]
Benzene	1.3E+3	1.8E+0	9.0E+1	2.6E-2
Toluene	7.8E+2 *	7.8E+2 *	7.8E+2 *	1.0E+1
Ethylbenzene	3.5E+2 *	3.5E+2 *	3.5E+2 *	1.1E+1
Xylene (mixed)	5.0E+2 *	5.0E+2 *	5.0E+2 *	1.7E+2
Naphthalene	4.0E+2 *	4.0E+2 *	4.0E+2 *	1.8E-2
Benzo(a)pyrene	4.7E+0 *	4.7E+0 *	4.7E+0 *	4.7E+0 *
MTBE	9.9E+3 *	9.9E+3 *	9.9E+3 *	4.0E-2

* Indicates SSTL exceeded pure component soil saturation limit and hence saturation is listed as SSTL

na = Not Applicable/Not Available

(1) Calculated using the equations in ASTM RBCA guidance. Target risk concentrations are corresponding to a cancer risk of one in 100000 or a non-carcinogenic hazard quotient of unity for the exposure pathway being evaluated.

(2) The SSTL is the lower of the target risk concentrations for carcinogenic and non-carcinogenic effect, unless they exceed soil saturation of water solubility, in which case the SSTL is set at saturation or solubility concentration.

Construction Exposure Scenario
SUMMARY OF TARGET LEVELS FOR WATER EXPOSURE PATHWAYS

CHEMICAL	MCL [mg/L]	SHALLOW GROUNDWATER TARGET LEVELS (1,2)		
		Water Ingestion [mg/L]	Outdoor GW Emissions [mg/L]	Indoor GW Emissions [mg/L]
Benzene	5.0E-3	6.5E-1	1.8E+3 *	5.2E+0
Toluene	1.0E+0	5.1E+2	5.4E+2 *	5.4E+2 *
Ethylbenzene	7.0E-1	1.5E+2 *	1.5E+2 *	1.5E+2 *
Xylene (mixed)	1.0E+1	2.0E+2 *	2.0E+2 *	2.0E+2 *
Naphthalene	2.0E-4	3.1E+1 *	3.1E+1 *	3.1E+1 *
Benzo(a)pyrene	2.0E-4	1.2E-3 *	1.2E-3 *	1.2E-3 *
MTBE	3.0E-2	1.3E+1	5.1E+4 *	5.1E+4 *

* Indicates SSTL exceeded pure component water solubility and hence water solubility is listed as SSTL
na = Not Applicable/Not Available
(1) Calculated using the equations in ASTM RBCA guidance. Target risk concentrations are corresponding to a cancer risk of one in 100000 or a non-carcinogenic hazard quotient of unity for the exposure pathway being evaluated.
(2) The SSTL is the lower of the target risk concentrations for carcinogenic and non-carcinogenic effect, unless they exceed soil saturation of water solubility, in which case the SSTL is set at saturation or solubility concentration.

Construction Exposure Scenario
SUMMARY OF TARGET LEVELS FOR AIR EXPOSURE PATHWAYS

CHEMICAL	AIR TARGET LEVELS (1,2)	
	Indoor Inhalation [mg/m^3]	Outdoor Inhalation [mg/m^3]
Benzene	8.7E+1	6.5E+1
Toluene	3.9E+4	2.9E+4
Ethylbenzene	9.7E+4	7.3E+4
Xylene (mixed)	6.8E+5	5.1E+5
Naphthalene	1.4E+4	1.0E+4
Benzo(a)pyrene	1.3E+0	9.8E-1
MTBE	2.9E+5	2.2E+5

* Indicates SSTL exceeded pure component water solubility and hence water solubility is listed as SSTL
na = Not Applicable/Not Available
(1) Calculated using the equations in ASTM RBCA guidance. Target risk concentrations are corresponding to a cancer risk of one in 100000 or a non-carcinogenic hazard quotient of unity for the exposure pathway being evaluated.
(2) The SSTL is the lower of the target risk concentrations for carcinogenic and non-carcinogenic effect, unless they exceed soil saturation of water solubility, in which case the SSTL is set at saturation or solubility concentration.

APPENDIX D Example Calculations of Tier 2 SSTLs

TABLE. EXAMPLE CALCULATION OF BENZENE SSTL

Chemical: Benzene (Based on Carcinogenic Risk)
Exposure Pathway : Indoor inhalation of vapors from groundwater
Exposure scenario : Commercial

SSTLw [mg/L] = SSTLair [mg/m3] x 10-3 [mg/mg] / VFwesp

SSTLair [mg/m3] = TR x ATc x 365 [days/year] x 1000 [mg/mg] / [SFi x EF x (ED_{child} x $IR_{air,child}$ / BW_{child} + ED_{adult} x $IR_{air,adult}$ / BW_{adult})]
(ASTM RBCA Guidance E 1739 - 95, p. 23, formula 1)
SSTLair [mg/m3] = 1E-5 x 70 x 365 x 1000 / [1.00E-1 x 250 x (0 x 15 / 15 + 25 x 15 / 70)]
SSTLair [mg/m3] = 1.91E+0

VF_{wesp} = H' x $D_{eff,ws}$ x 1000 [L/m^3] / (L_{GW} x ER x L_B) / { 1 + $D_{eff,ws}$ / (L_{GW} x ER x L_B) + $D_{eff,ws}$ x L_{crack} /($D_{eff,crack}$ x L_{GW} x η) }

$D_{eff,ws}$ [cm^2/s] = (h_{cap} + h_v) x (h_{cap} / $D_{eff,cap}$ + h_v / $D_{eff,s}$)-1

$D_{eff,cap}$ [cm^2/s] = D_{air} x $\theta_{acap}^{3.33}$ / θ_T^2 + D_{wat} x $\theta_{wcap}^{3.33}$ / (H' x θ_T^2)
$D_{eff,cap}$ [cm^2/s] = 0.093 x (0.038)^3.33 / (0.38)^2 + 1.10E-5 x (0.342)^3.33 / (2.20E-1 x (0.38)^2)
$D_{eff,cap}$ [cm^2/s] = 2.17E-5

$D_{eff,s}$ [cm^2/s] = D_{air} x $\theta_{as}^{3.33}$ / θ_T^2 + D_{wat} x $\theta_{ws}^{3.33}$ / (H' x θ_T^2)
$D_{eff,s}$ [cm^2/s] = 0.093 x (0.26)^3.33 / (0.38)^2 + 1.10E-5 x (0.12)^3.33 / (2.20E-1 x (0.38)^2)
$D_{eff,s}$ [cm^2/s] = 7.26E-3

$D_{eff,ws}$ [cm^2/s] = (5 + 295) x (5 / 2.17E-5 + 295 / 7.26E-3)^(-1)
$D_{eff,ws}$ [cm^2/s] = 1.11E-3

$D_{eff,crack}$ [cm^2/s] = D_{air} x $\theta_{acrack}^{3.33}$ / θ_T^2 + D_{wat} x $\theta_{wcrack}^{3.33}$ / (H' x θ_T^2)
$D_{eff,crack}$ [cm^2/s] = 0.093 x (0.26)^3.33 / (0.38)^2 + 1.10E-5 x (0.12)^3.33 / (2.20E-1 x (0.38)^2)
$D_{eff,crack}$ [cm^2/s] = 7.26E-3

VF_{wesp} = 2.20E-1 x 7.26E-3 x 1000 / (300 x 0.00023 x 300) /
{ 1 + 7.26E-3 /(300 x 0.00023 x 300) + 7.26E-3 x 15 / (7.26E-3 x 300 x 0.0005)}
VF_{wesp} = 7.24E-4

SSTLw [mg/L] = 1.91E+0 x 1E-3 / 7.24E-4
SSTLw [mg/L] = 2.64E+0

APPENDIX E

ASTM RBCA Equations

1 RISK-BASED SCREENING LEVEL (RBSLs) – CARCINOGENIC EFFECTS

1.1 DEFINITION OF PARAMETERS

AT_c	=	Averaging time for carcinogens [years]
BW_{child}	=	Child body weight [kg]
BW_{adult}	=	Adult body weight [kg]
BW	=	Adult body weight [kg]
ED_{child}	=	Exposure duration of child [years]
ED_{adult}	=	Exposure duration of adult [years]
ED	=	Exposure duration of adult[years]
EF	=	Exposure frequency [days/year]
$IR_{soil,child}$	=	Soil ingestion rate for child [mg/day]
$IR_{soil,adult}$	=	Soil Ingestion rate for adult [mg/day]
IR_{soil}	=	Soil ingestion rate for adult[mg/day]
$IR_{air,child}$ - *indoor*	=	Daily indoor inhalation rate for child [m^3/day]
$IR_{air,adult}$ - *indoor*	=	Daily indoor inhalation rate for adult [m^3/day]
IR_{air} - *indoor*	=	Daily indoor inhalation rate for adult [m^3/day]
$IR_{air,child}$ - *outdoor*	=	Daily outdoor inhalation rate for child [m^3/day]
$IR_{air,adult}$ - *outdoor*	=	Daily outdoor inhalation rate for adult [m^3/day]
IR_{air} - *outdoor*	=	Daily outdoor inhalation rate for adult [m^3/day]
$IR_{w,child}$	=	Daily water ingestion rate for child [L/day]
$IR_{w,adult}$	=	Daily water ingestion rate for adult [L/day]
IR_w	=	Daily water ingestion rate for adult [L/day]
LF_{sw}	=	Leaching factor from subsurface soils to ground water [(mg/L-H_2O)/(mg/kg-soil)]
M	=	Soil to skin adherence factor [mg/cm^2]
RAF_d	=	Dermal relative absorption factor [volatiles/PAHs]
RAF_o	=	Oral relative absorption factor [---]

$RBSL_{air}$	=	Risk-based screening level for air [µg/m^3-air]
$RBSL_s$	=	Risk-based screening level for soil [µg/kg-soil or mg/kg-soil]
$RBSL_w$	=	Risk-based screening level for water [mg/L-H_2O]
SA_{child}	=	Child skin surface area [cm^2/day]
SA_{adult}	=	Adult skin surface area [cm^2/day]
SA	=	Adult skin surface area [cm^2/day]
SF_i	=	Inhalation cancer slope factor [(mg/kg-day)$^{-1}$]
SF_o	=	Oral cancer slope factor [(mg/kg-day)$^{-1}$]
TR	=	Target excess individual lifetime cancer risk [---]
VF_p	=	Volatilization factor from surficial soils to ambiant air (particulates) [(mg/ m^3-air)/(mg/kg-soil)]
VF_{samb}	=	Volatilization factor from subsurface soils to ambient air [(mg/m^3-air)/(mg/kg-soil)]
VF_{sesp}	=	Volatilization factor from subsurface soils to enclosed-space vapors [(mg/m^3-air)/(mg/kg-soil)]
VF_{ss}	=	Volatilization factor from surficial soils to ambiant air (vapors) [(mg/m^3-air)/(mg/kg-soil)]
VF_{wamb}	=	Volatilization factor from ground water to ambient (outdoor) vapors [(mg/m^3-air)/(mg/L-H_2O)]
VF_{wesp}	=	Volatilization factor from ground water to enclosed-space vapors [(mg/m^3-air)/(mg/L-H_2O)]

1.2 EQUATIONS

Risk-Based Screening Level for inhalation of air

The Risk-Based Screening Level for this route is estimated using:

For adults:

$$RBSL_{air}\left[\frac{\mu g}{m^3 - air}\right] = \frac{TR \times BW \times AT_c \times 365 \ \frac{days}{years} \times 10^3 \frac{\mu g}{mg}}{SF_i \times IR_{air} \times EF \times ED} \quad (1)$$

For children and adults:

$$RBSL_{air} = \frac{TR \times AT_c \times 365 \times 10^3}{SF_i \times EF}\left(\frac{1}{\left(\frac{ED_{child} \times IR_{air,child}}{BW_{child}} + \frac{ED_{adult} \times IR_{air,adult}}{BW_{adult}}\right)}\right) \quad (2)$$

Risk-Based Screening Level for ingestion of potable ground water

The Risk-Based Screening Level for this route is estimated using:

For adults:

$$RBSL_w\left[\frac{mg}{L - H_2O}\right] = \frac{TR \times BW \times AT_c \times 365 \ \frac{days}{years}}{SF_o \times IR_w \times EF \times ED} \quad (3)$$

For children and adults:

$$RBSL_w = \frac{TR \, x \, AT_c \; x \, 365}{SF_o \; x \; EF} \left(\frac{1}{\left(\frac{ED_{child} \; x \, IR_{w,child}}{BW_{child}} + \frac{ED_{adult} \; x \, IR_{w,adult}}{BW_{adult}} \right)} \right) \quad (4)$$

Risk-Based Screening Level for inhalation of enclosed-space (indoor) vapors from ground water

The Risk-Based Screening Level for this route is estimated using:

$$RBSL_w \left[\frac{mg}{L - H_2O} \right] = \frac{RBSL_{air} \left[\frac{\mu g}{m^3 - air} \right]}{VF_{wesp}} \; x \; 10^{-3} \; \frac{mg}{\mu g} \quad (5)$$

Risk-Based Screening Level for inhalation of ambient (outdoor) vapors from ground water

The Risk-Based Screening Level for this route is estimated using:

$$RBSL_w \left[\frac{mg}{L - H_2O} \right] = \frac{RBSL_{air} \left[\frac{\mu g}{m^3 - air} \right]}{VF_{wamb}} \; x \; 10^{-3} \; \frac{mg}{\mu g} \quad (6)$$

Risk-Based Screening Level for ingestion of soil, inhalation of vapors and particulates, and dermal contact from surficial soil

The Risk-Based Screening Level for this route is estimated using:

For adults:

$$RBSL_s \left[\frac{\mu g}{kg - soil}\right] =$$

$$\frac{TR \; x \; BW \; x \; AT_c \; x \; 365 \; \frac{days}{years}}{EF \; x \; ED \; x \left[\left(SF_o \; x \; 10^{-6} \frac{kg}{mg} \; x \; (IR_{soil} \; x \; RAF_o \; + \; SA \; x \; M \; x \; RAF_d)\right) + (SF_i \; x \; IR_{air} \; x \; (VF_{as} \; + \; VF_p))\right]} \quad (7)$$

For children and adults:

$$RBSL_s =$$

$$\frac{TR \; x \; AT_c \; x \; 365}{EF \; x \left\{\begin{array}{l} \frac{ED_{child}}{BW_{child}} \; x \left[\left(SF_o \; x \; 10^{-6} \; x \; (IR_{soil,child} \; x \; RAF_o + SA_{child} \; x \; M \; x \; RAF_d)\right) + (SF_i \; x \; IR_{air,child} \; x \; (VF_{ss} + VF_p))\right] + \\ + \frac{ED_{adult}}{BW_{adult}} \; x \left[\left(SF_o \; x \; 10^{-6} \; x \; (IR_{soil,adult} \; x \; RAF_o + SA_{adult} \; x \; M \; x \; RAF_d)\right) + (SF_i \; x \; IR_{air,adult} \; x \; (VF_{ss} + VF_p))\right] \end{array}\right\}} \quad (8)$$

Risk-Based Screening Level for inhalation of ambient (outdoor) vapors from subsurface soil

The Risk-Based Screening Level for this route is estimated using:

$$RBSL_s \left[\frac{mg}{kg-soil}\right] = \frac{RBSL_{air}\left[\frac{\mu g}{m^3-air}\right]}{VF_{samb}} \; x \; 10^{-3} \; \frac{mg}{\mu g} \qquad (9)$$

Risk-Based Screening Level for inhalation of enclosed-space (indoor) vapors from subsurface soil

The Risk-Based Screening Level for this route is estimated using:

$$RBSL_s \left[\frac{mg}{kg-soil}\right] = \frac{RBSL_{air}\left[\frac{\mu g}{m^3-air}\right]}{VF_{sesp}} \; x \; 10^{-3} \; \frac{mg}{\mu g} \qquad (10)$$

Risk-Based Screening Level for leaching to ground water from subsurface soil

The Risk-Based Screening Level for this route is estimated using:

$$RBSL_s \left[\frac{mg}{kg-soil}\right] = \frac{RBSL_w\left[\frac{mg}{L-H_2O}\right]}{LF_{sw}} \qquad (11)$$

2 RISK-BASED SCREENING LEVEL (RBSLs) – NONCARCINOGENIC EFFECTS

2.1 DEFINITION OF PARAMETERS

AT_n	=	Averaging time for non-carcinogens [years]
BW_{child}	=	Child body weight [kg]
BW_{adult}	=	Adult body weight [kg]
BW	=	Adult body weight [kg]
ED_{child}	=	Exposure duration of child [years]
ED_{adult}	=	Exposure duration of adult [years]
ED	=	Exposure duration [years]
EF	=	Exposure frequency [days/year]
$IR_{soil.child}$	=	Soil ingestion rate for child [mg/day]
$IR_{soil.adult}$	=	Soil Ingestion rate for adult [mg/day]
IR_{soil}	=	Soil ingestion rate for adult [mg/day]
$IR_{air.child}$ - *indoor*	=	Daily indoor inhalation rate for child [m^3/day]
$IR_{air.adult}$ - *indoor*	=	Daily indoor inhalation rate for adult [m^3/day]
IR_{air} - *indoor*	=	Daily indoor inhalation rate for adult [m^3/day]
$IR_{air,child}$ - *outdoor*	=	Daily outdoor inhalation rate for child [m^3/day]
$IR_{air.adult}$ - *outdoor*	=	Daily outdoor inhalation rate for adult [m^3/day]
IR_{air} - *outdoor*	=	Daily outdoor inhalation rate for adult [m^3/day]
$IR_{w,child}$	=	Daily water ingestion rate for child [L/day]
$IR_{w,adult}$	=	Daily water ingestion rate for adult [L/day]
IR_w	=	Daily water ingestion rate for adult [L/day]
LF_{sw}	=	Leaching [(mg/L-H_2O)/(mg/kg-soil)]
M	=	Soil to skin adherence factor [mg/cm^2]
RAF_d	=	Dermal relative absorption factor [volatiles/PAHs]
RAF_o	=	Oral relative absorption factor [---]

$RBSL_{air}$	=	Risk-based screening level for air [µg/m^3-air]
$RBSL_s$	=	Risk-based screening level for soil [µg/kg-soil or mg/kg-soil]
$RBSL_w$	=	Risk-based screening level for water [mg/L-H_2O]
RfD_i	=	Inhalation chronic reference dose [mg/kg-day]
RfD_o	=	Oral chronic reference dose[mg/kg-day]
SA_{child}	=	Child skin surface area for child [cm^2/day]
SA_{adult}	=	Adult skin surface area for adult [cm^2/day]
SA	=	Adult skin surface area [cm^2/day]
SF_i	=	Inhalation cancer slope factor [(mg/kg-day)$^{-1}$]
SF_o	=	Oral cancer slope factor [(mg/kg-day)$^{-1}$]
THQ	=	Target hazard quotient for individual constituents [---]
VF_p	=	Volatilization factor from surficial soils to ambiant air (particulates) [(mg/ m^3-air)/(mg/kg-soil)]
VF_{samb}	=	Volatilization factor from subsurface soils to ambient [(mg/m^3-air)/(mg/kg-soil)]
VF_{sesp}	=	Volatilization factor from subsurface soils to enclosed-space vapors [(mg/m^3-air)/(mg/kg-soil)]
VF_{ss}	=	Volatilization factor from surficial soils to ambiant air (vapors) [(mg/m^3-air)/(mg/kg-soil)]
VF_{wamb}	=	Volatilization factor from ground water to ambient (outdoor) vapors [(mg/m^3-air)/(mg/L-H_2O)]
VF_{wesp}	=	Volatilization factor from ground water to enclosed-space vapors [(mg/m^3-air)/(mg/L-H_2O)]

2.2 EQUATIONS

Risk-Based Screening Level for inhalation of air

The Risk-Based Screening Level for this route is estimated using:

For adults:

$$RBSL_{air}\left[\frac{\mu g}{m^3 - air}\right] = \frac{THQ \times RfD_i \times BW \times AT_n \times 365 \frac{days}{years} \times 10^3 \frac{\mu g}{mg}}{IR_{air} \times EF \times ED} \quad (12)$$

For children and adults:

$$RBSL_{air} = \frac{THQ \times RfD_i \times AT_n \times 365 \times 10^3}{EF}\left(\frac{1}{\left(\frac{ED_{child} \times IR_{air,child}}{BW_{child}} + \frac{ED_{adult} \times IR_{air,adult}}{BW_{adult}}\right)}\right) \quad (13)$$

Risk-Based Screening Level for ingestion of potable ground water

The Risk-Based Screening Level for this route is estimated using:

For adults:

$$RBSL_w\left[\frac{mg}{L - H_2O}\right] = \frac{THQ \times RfD_o \times BW \times AT_n \times 365 \frac{days}{years}}{IR_w \times EF \times ED} \quad (14)$$

For children and adults:

$$RBSL_w = \frac{THQ \; x \; RfD_o \; x \; AT_n \; x \; 365}{EF} \left(\frac{1}{\left(\frac{ED_{child} \; x \; IR_{w,child}}{BW_{child}} + \frac{ED_{adult} \; x \; IR_{w,adult}}{BW_{adult}} \right)} \right) \quad (15)$$

Risk-Based Screening Level for inhalation of enclosed-space (indoor) vapors from ground water

The Risk-Based Screening Level for this route is estimated using:

$$RBSL_w \left[\frac{mg}{L - H_2O} \right] = \frac{RBSL_{air} \left[\frac{\mu g}{m^3 - air} \right]}{VF_{wesp}} \; x \; 10^{-3} \; \frac{mg}{\mu g} \quad (16)$$

Risk-Based Screening Level for inhalation of ambient (outdoor) vapors from ground water

The Risk-Based Screening Level for this route is estimated using:

$$RBSL_w \left[\frac{mg}{L - H_2O} \right] = \frac{RBSL_{air} \left[\frac{\mu g}{m^3 - air} \right]}{VF_{wamb}} \; x \; 10^{-3} \; \frac{mg}{\mu g} \quad (17)$$

Risk-Based Screening Level for ingestion of soil, inhalation of vapors and particulates, and dermal contact from surficial soil

The Risk-Based Screening Level for this route is estimated using:

For adults:

$$RBSL_s \left[\frac{\mu g}{kg - soil}\right] =$$

$$\frac{THQ \; x \; BW \; x \; AT_n \; x \; 365 \; \frac{days}{years}}{EF \; x \; ED \; x \left[\frac{\left(10^{-6} \frac{kg}{mg} \; x \; (IR_{soil} \; x \; RAF_o \; + \; SA \; x \; M \; x \; RAF_d)\right)}{RfD_o} + \frac{(IR_{air} \; x \; (VF_{ss} \; + \; VF_p))}{RfD_i}\right]} \qquad (18)$$

For children and adults:

$$RBSL_s \; =$$

$$\frac{THQ \; x \; AT_n \; x \; 365}{EF \; x \left\{\frac{ED_{child}}{BW_{child}} \left[\frac{\left(10^{-6} \; x \; (IR_{soil,child} \; x \; RAF_o \; + \; SA_{child} \; x \; M \; x \; RAF_d)\right)}{RfD_o} + \frac{(IR_{air,child} \; x \; (VF_{ss} \; + \; VF_p))}{RfD_i}\right] + \right.} \qquad (19)$$

$$\left. + \frac{ED_{adult}}{BW_{adult}} \left[\frac{\left(10^{-6} \; x \; (IR_{soil,adult} \; x \; RAF_o \; + \; SA_{adult} \; x \; M \; x \; RAF_d)\right)}{RfD_o} + \frac{(IR_{air,adult} \; x \; (VF_{ss} \; + \; VF_p))}{RfD_i}\right]\right\}$$

Risk-Based Screening Level for inhalation of ambient (outdoor) vapors from subsurface soil

The Risk-Based Screening Level for this route is estimated using:

$$RBSL_s \left[\frac{mg}{kg-soil}\right] = \frac{RBSL_{air}\left[\frac{\mu g}{m^3-air}\right]}{VF_{samb}} \; x \; 10^{-3} \; \frac{mg}{\mu g} \qquad (20)$$

Risk-Based Screening Level for inhalation of enclosed-space (indoor) vapors from subsurface soil

The Risk-Based Screening Level for this route is estimated using:

$$RBSL_s \left[\frac{mg}{kg-soil}\right] = \frac{RBSL_{air}\left[\frac{\mu g}{m^3-air}\right]}{VF_{sesp}} \; x \; 10^{-3} \; \frac{mg}{\mu g} \qquad (21)$$

Risk-Based Screening Level for leaching to ground water from subsurface soil

The Risk-Based Screening Level for this route is estimated using:

$$RBSL_s \left[\frac{mg}{kg-soil}\right] = \frac{RBSL_w\left[\frac{mg}{L-H_2O}\right]}{LF_{sw}} \qquad (22)$$

3 EQUATIONS OF VOLATILIZATION FACTORS (VF_i), LEACHING FACTOR (LF_{sw}), AND EFFECTIVE DIFFUSION COEFFICIENTS (D_i^{eff})

3 1 DEFINITION OF PARAMETERS

d	=	Lower depth of surficial soil zone [cm]
D^{air}	=	Diffusion coefficient in air [cm^2/s]
D^{wat}	=	diffusion coefficient in water [cm^2/s]
ER	=	Enclosed-space air exchange rate [L/s]
f_{oc}	=	Fraction of organic carbon in soil [g-C/g-soil]
H	=	henry's law constant [cm^3-H_2O]/[cm^3-air]
h_{cap}	=	Thickness of capillary fringe [cm]
h_v	=	Thickness of vadose zone [cm]
I	=	Infiltration rate of water through soil [cm/yr]
k_{oc}	=	Carbon-water sorption coefficient [cm^3-H_2O/g-C]
k_s	=	Soil-Water sorption coefficient [cm^3-H_2O/g-soil]
L_B	=	Enclosed-space volume/infiltration area ratio [cm]
L_{crack}	=	Enclosed-space foundation of wall thickness [cm]
L_{GW}	=	Depth to groundwater = $h_{cap} + h_v$ [cm]
L_s	=	Depth to subsurface soil sources [cm]
P_e	=	Particulate emission rate [g/cm^2-s]
S	=	Pure component solubility in water [mg/L-H_2O]
U_{air}	=	Wind speed above ground surface in ambient mixing zone [cm/s]
U_{gw}	=	Ground water Darcy velocity [cm/yr]
W	=	Width of source area parallel to wind, or ground water flow direction [cm]
δ_{air}	=	Ambient air mixing zone height [cm]

δ_{gw}	=	Ground water mixing zone thickness [cm]
η	=	Areal fraction of cracks in foundations/walls [cm^2-cracks/cm^2-total area]
θ_{acap}	=	Volumetric air content in capillary fringe soils [cm^3-air/cm^3-soil]
θ_{acrack}	=	Volumetric air content in foundation/wall cracks [cm^3-air/ cm^3-total volume]
θ_{as}	=	Volumetric air content in vadose zone soils [cm^3-air/cm^3-soil]
θ_T	=	Total soil porosity [cm^3/ cm^3-soil]
θ_{wcap}	=	Volumetric water content in capillary fringe soils [cm^3-H_2O/ cm^3-soil]
θ_{wcrack}	=	Volumetric water content in foundation/wall cracks [cm^3-H_2O/ cm^3-total volume]
θ_{ws}	=	Volumetric water content in vadose zone soils [cm^3-H_2O/ cm^3-soil]
ρ_s	=	Soil bulk density [g-soil/ cm^3-soil]
τ	=	Averaging time for vapor flux [s]

3.2 EQUATIONS

Volatilization factor from ground water to enclosed-space vapors

(23)

Volatilization factor from ground water to ambient (outdoor) vapors

$$VF_{wamb}\left[\frac{(mg/m^3-air)}{(mg/L-H_2O)}\right] = \frac{H}{1+\left[\frac{U_{air}\ x\ \delta_{air}\ x\ L_{GW}}{W\ x\ D_{ws}^{eff}}\right]}\ x\ 10^3\ \frac{L}{m^3} \quad (24)$$

Volatilization factor from surficial soils to ambient air (vapors)

$$VF_{ss}\left[\frac{(mg/m^3\text{ - air})}{(mg/kg-soil}\right] = \frac{2\ x\ W\ x\ \rho_s}{U_{air}\ x\ \delta_{air}}\sqrt{\frac{D_s^{eff}\ x\ H}{\pi\ x\left[\theta_{ws}+k_s\ x\ \rho_s+H\ x\ \theta_{as}\right]x\ \tau}}\ x\ 10^3\ \frac{cm^3-kg}{m^3-g} \quad (25)$$

or:

$$VF_{ss}\left[\frac{(mg/m^3\text{ - air})}{(mg/kg-soil}\right] = \frac{W\ x\ \rho_s\ x\ d}{U_{air}\ x\ \delta_{air}}\ x\ 10^3\ \frac{cm^3-kg}{m^3-g}\text{; whichever is less} \quad (26)$$

Volatilization factor from surficial soils to ambient air (particulates)

$$VF_p\left[\frac{(mg/m^3\text{ - air})}{(mg/kg-soil}\right] = \frac{P_e\ x\ W}{U_{air}\ x\ \delta_{air}}\ x\ 10^3\ \frac{cm^3-kg}{m^3-g} \quad (27)$$

Volatilization factor from surficial soils to ambient air

$$VF_{samb}\left[\frac{(mg/m^3\text{ - air})}{(mg/kg-soil}\right] = \frac{H\ x\ \rho_s}{\left[\theta_{ws}+k_s\ x\ \rho_s+H\ x\ \theta_{as}\right]\text{x}\left(1+\frac{U_{air}\ x\ \delta_{air}\ x\ L_S}{D_s^{eff}\ x\ W}\right)}\ x\ 10^3\ \frac{cm^3-kg}{m^3-g} \quad (28)$$

Volatilization factor from surficial soil to enclosed-space vapors

$$VF_{sesp}\left[\frac{(mg/m^3\text{ - air})}{(mg/kg-soil}\right] = \frac{\dfrac{H\,x\,\rho_s}{\left[\theta_{ws}+k_s\;x\,\rho_s+H\,x\,\theta_{as}\right]}\;x\left[\dfrac{D_s^{eff}\;/\;L_S}{ER\,x\,L_B}\right]}{1+\left[\dfrac{D_s^{eff}\;/\;L_S}{ER\,x\,L_B}\right]+\left[\dfrac{D_s^{eff}\;/\;L_S}{(D_{crack}^{eff}\;/\;L_{crack})\,x\,\eta}\right]}\;x\;10^3\;\frac{cm^3-kg}{m^3-g} \qquad (29)$$

Leaching factor from subsurface soils to ground water

$$LF_{sw}\left[\frac{(mg/L-H_2O)}{(mg/kg-soil}\right] = \frac{\rho_s}{\left[\theta_{ws}+k_s\;x\,\rho_s+H\,x\,\theta_{as}\right]x\left(1+\dfrac{U_{gw}\,x\,\delta_{gw}}{I\,x\,W}\right)}\;x\;10^0\;\frac{cm^3-kg}{L-g} \qquad (30)$$

Effective diffusion coefficient in soil based on vapor-phase concentration

$$D_s^{eff}\left[\frac{cm^2}{s}\right] = D^{air}\;x\;\frac{\theta_{as}^{3.33}}{\theta_T^2}\;+\;D^{wat}\;x\;\frac{1}{H}\;x\;\frac{\theta_{ws}^{3.33}}{\theta_T^2} \qquad (31)$$

Effective diffusion coefficient through foundation cracks

$$D_{crack}^{eff}\left[\frac{cm^2}{s}\right] = D^{air}\;x\;\frac{\theta_{acrack}^{3.33}}{\theta_T^2}\;+\;D^{wat}\;x\;\frac{1}{H}\;x\;\frac{\theta_{wcrack}^{3.33}}{\theta_T^2} \qquad (32)$$

Effective diffusion coefficient through capillary fringe

$$D_{cap}^{eff}\left[\frac{cm^2}{s}\right] = D^{air}\ x\ \frac{\theta_{acap}^{3.33}}{\theta_T^2} + D^{wat}\ x\ \frac{1}{H}\ x\ \frac{\theta_{wcap}^{3.33}}{\theta_T^2} \quad (33)$$

Effective diffusion coefficient between ground water and soil surface

$$D_{ws}^{eff}\left[\frac{cm^2}{s}\right] = (\ h_{cap} + h_v\ )\ x\left[\frac{h_{cap}}{D_{cap}^{eff}} + \frac{h_v}{D_s^{eff}}\right]^{-1} \quad (34)$$

Soil concentration at which dissolved pore-water and vapor phases become saturated

$$C_s^{sat}\left[\frac{mg}{kg-soil}\right] = \frac{S}{\rho_s}\ x\left[\theta_{ws} + k_s\ x\ \rho_s + H\ x\ \theta_{as}\right] x\ 10^0\ \frac{L-g}{cm^3-kg} \quad (35)$$

TABLE. PARAMETERS FOR EXPOSURE AND CONTAMINANT FATE TRANSPORT MODELING

EXPOSURE PARAMETERS				
Parameters	**Definitions**	**Units**	**Residential**	**Commercial/Industrial**
AT_c	**Averaging time for carcinogens**	years	70	70
AT_n	**Averaging time for noncarcinogens**	years	30	25
BW	**Adult body weight**	kg	70	70
ED	**Exposure duration of adult**	years	30	25
EF	**Exposure frequency**	days/years	350	250
IR_{soil}	**Soil ingestion rate for adult**	mg/day	100	50
IR_{air}-$indoor$	**Daily indoor inhalation rate of adult**	m^3/day	15	20
IR_{air}-$outdoor$	**Daily outdoor inhalation rate of adult**	m^3/day	20	20
IR_w	**Daily water ingestion rate for adult**	L/day	2	1
LF_{sw}	**Leaching factor**	(mg/L-H_2O)/(mg/kg-soil)	Chemical-specific	Chemical-specific
M	**Soil to skin adherence factor**	mg/cm^2	0.5	0.5
RAF_d	**Dermal relative absorption factor (volatiles/PAHs)**	---	0.5/ 0.05	0.5/ 0.05
RAF_o	**Oral relative absorption factor**	---	1.0	1.0
$RBSL_i$	**Risk-Based screening level for media i**	mg/kg-soil, mg/L-H_2O, or mg/m^3-air	Chemical-, media-, and exposure route-specific	Chemical-, media-, and exposure route-specific
$RFDi$	**Inhalation chronic reference dose**	mg/kg-day	Chemical-specific	Chemical-specific
RFD_o	**Oral chronic reference dose**	mg/kg-day	Chemical-specific	Chemical-specific
SA	**Adult skin surface area**	cm^2/day	3160	3,160
SF_i	**Inhalation cancer slope factor**	(mg/kg-day)$^{-1}$	Chemical-specific	Chemical-specific
SF_o	**Oral cancer slope factor**	(mg/kg-day)$^{-1}$	Chemical-specific	Chemical-specific
THQ	**Target hazard quotient for individual constituents**	---	1.0	1.0
TR	**Target excess individual lifetime cancer risk**	---	10^{-6} to 10^{-4}	10^{-6} to 10^{-4}
VF_i	**Volatilization factor**	(mg/m^3-air)/(mg/kg-soil) or (mg/m^3-air)/(mg/L-H_2O)	Chemical- and media-specific	Chemical- and media-specific

CONTAMINANT FATE AND TRANSPORT PARAMETERS				
Parameters	**Definitions**	**Units**	**Residential**	**Commercial/Industrial**
d	**Lower depth of surficial soil zone**	cm	100	100
D^{air}	**Diffusion coefficient in air**	cm^2/s	Chemical-specific	Chemical-specific
D^{water}	**Diffusion coefficient in water**	cm^2/s	Chemical-specific	Chemical-specific
ER	**Enclosed-space air exchange rate**	L/sec	0.00014	0.00023
f_{oc}	**Fraction of organic carbon in soil**	g-C/g-soil	0.01	0.01
H	**Henry's law constant**	(cm^3-H_2O)/(cm^3-air)	Chemical-specific	Chemical-specific
h_{cap}	**Thickness of capillary fringe**	cm	5	5
h_v	**Thickness of vadose zone**	cm	295	295
I	**Infiltration rate of water through soil**	cm/year	30	30
k_{oc}	**Carbon-water sorption coefficient**	cm^3-H_2O/g-C	Chemical-specific	Chemical-specific
k_s	**Soil-water sorption coefficient**	cm^3-H_2O/g-soil	f_{oc} x k_{oc}	f_{oc} x k_{oc}
L_B	**Enclosed-space volume/infiltration area ratio**	cm	200	300
L_{crack}	**Enclosed-space foundation or wall thickness**	cm	15	15
L_{GW}	**Depth to groundwater = h_{cap} + h_v**	cm	300	300
L_s	**Depth to subsurface soil sources**	cm	100	100
P_e	**Particulate emission rate**	g/cm^2-s	6.9 x 10^{-14}	6.9 x 10^{-14}
S	**Pure component solubility in water**	mg/L-H_2O	Chemical-specific	Chemical-specific
U_{air}	**Wind speed above ground surface in ambient mixing zone**	cm/s	225	225
U_{gw}	**Groundwater Darcy velocity**	cm/year	2500	2500
W	**Width of source area parallel to wind, or gw flow direction**	cm	1500	1500
δ_{air}	**Ambient air mixing zone height**	cm	200	200
δ_{gw}	**Ground water mixing zone thickness**	cm	200	200
η	**Areal fraction of cracks in foundation/walls**	cm^2-cracks/cm^2-total area	0.01	0.01
θ_{icap}	**Volumetric air content in capillary fringe soils**	cm^3-air/cm^3-soil	0.038	0.038
θ_{icrack}	**Volumetric air content in foundation/wall cracks**	cm^3-air/cm^3 total volume	0.26	0.26
θ_{iv}	**Volumetric air content in vadose zone soils**	cm^3-air/cm^3-soil	0.26	0.26
θ_T	**Total soil porosity**	cm^3/cm^3-soil	0.38	0.38
θ_{wcap}	**Volumetric water content in capillary fringe soils**	cm^3-H_2O/cm^3-soil	0.342	0.342

θ_{wcrack}	**Volumetric water content in foundation/wall cracks**	cm^3-H_2O/cm^3,total volume	0.12	0.12
θ_{ws}	**Volumetric water content in vadose zone soils**	cm^3-air/cm^3-soil	0.12	0.12
ρ_s	**Soil bulk density**	g-soil/cm^3-soil	1.7	1.7
τ	**Averaging time for vapor flux**	sec	7.88×10^8	7.88×10^8

Reference : ASTM Emergency Standard Guide for Risk-Based Corrective Action Applied at Petroleum Release Sites (September, 1995)