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TRANSMITTAL

DATE: July 20, 2009 REFERENCE NO.: 240612
PROJECT NAME: 1784 150th Avenue, San Leandro

TO: Jerry Wickham
Alameda County Health Care Services Agency
1131 Harbor Bay Parkway, Suite 250
Alameda, California 94502

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QUANTITY	DESCRIPTION
1	Feasibility Study/Corrective Action Plan

As Requested For Review and Comment
 For Your Use _____

COMMENTS:

If you have any questions regarding the content of this document, please contact Peter Schaefer at (510) 420-3319.

Copy to: Denis Brown, Shell Oil Products US, 20945 S. Wilmington Avenue, Carson, CA 90810
City of San Leandro, Environmental Division, 835 East 14th Street, San Leandro, CA 94577

Completed by: Peter Schaefer Signed: *Peter Schaefer*

Filing: Correspondence File



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Re: Shell-branded Service Station
1784 150th Avenue
San Leandro, California
SAP Code 136019
Incident No. 98996068
Agency Case No. RO0000367

Dear Mr. Wickham:

The attached document is provided for your review and comment. Upon information and belief, I declare, under penalty of perjury, that the information contained in the attached document is true and correct.

If you have any questions or concerns, please call me at (707) 865-0251.

Sincerely,

A handwritten signature in black ink, appearing to read "Denis L. Brown", is written over a horizontal line.

Denis L. Brown
Project Manager



FEASIBILITY STUDY/CORRECTIVE ACTION PLAN

**SHELL-BRANDED SERVICE STATION
1784 150TH AVENUE
SAN LEANDRO, CALIFORNIA**

**SAP CODE 136019
INCIDENT NO. 98996068
ACEH FILE NO. RO0000367**

JULY 20, 2009

REF. NO. 240612 (8)

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**Prepared by:
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1.0 INTRODUCTION

Conestoga-Rovers & Associates (CRA), submits this *Feasibility Study/Corrective Action Plan* (FS/CAP) on behalf of Equilon Enterprises LLC dba Shell Oil Products US (Shell) for the referenced site. Preparation of this FS/CAP was requested in Alameda County Health Care Services Agency's (ACHCSA's) April 21, 2009 letter. This FS/CAP complies with California Code of Regulations, Title 23, Division 3, Chapter 16, Underground Storage Tank Regulations.

2.0 SITE BACKGROUND

The site is an operating Shell-branded service station located at the southern corner of 150th Avenue and Freedom Avenue in San Leandro, California (Figure 1). The area surrounding the site is mixed commercial and residential. The site layout (Figure 2) includes a station building, two dispenser islands, and three fuel underground storage tanks (USTs). One waste oil UST was removed from the site on May 25, 2006. There are currently 16 on-site and 8 off-site groundwater monitoring wells and four on-site and one off-site soil vapor probes. A summary of previous work performed at the site is provided in Appendix A.

2.1 SITE GEOLOGY AND HYDROGEOLOGY

2.1.1 LOCAL GEOLOGY

The site is located at the base of the Berkeley Hills on the eastern edge of the East Bay Plain Groundwater Basin. Sediments beneath the site are Quaternary alluvial deposits derived from sedimentary and igneous rocks of the Diablo Range. The site is intersected by the Hayward Fault Zone. The site is underlain by low estimated permeability sediments (clay) with interspersed sediments of moderate permeability. During recent investigations, soil consisted of silty clay, clayey silts, and clayey sandy silt interlayered with sands and gravels to the total explored depth of 40 feet below grade (fbg).

2.1.2 SOIL TYPES

Hollow-stem auger and geoprobe borings showed that the site is underlain by a layer of dark brown to black, soft, damp, sandy silt/silty clay with gravel (ML/CL) of low to moderate plasticity and low to moderate estimated permeability, to an approximate depth of 5 fbg. Beneath lies a brown to dark brown silty clay (CL) to approximately 13 fbg. Silty sand/sandy silt (SM/ML) is present to the total explored depth of 45 fbg, with gravel (GC/GM/GP) interbedded above and below 25 fbg.

Soil types encountered in the cone penetration testing (CPT) borings consisted predominantly of silt, clayey silt, and sandy silt (ML) with increasing interbedded silty sand (SM), and cemented sand and sand (SP) below 25 fbg to the total depth explored of 75 fbg. Cross sections of the site are presented in Figures 3 and 4, and monitoring well, boring, and CPT logs are presented in Appendix B.

2.1.3 GROUNDWATER ELEVATION AND GRADIENT

Groundwater depths have ranged between 17 and 30 fbg on site and between approximately 4 and 14 fbg in off-site well MW-4. Water level measurements have not shown a consistent or reliable groundwater flow direction, although the most frequent groundwater flow direction since 1999 has been to the north-northwest. Groundwater gradients have ranged from 0.0008 ft/ft to 0.017 ft/ft. Groundwater is typically 20 to 30 fbg. The high level of variability in groundwater levels and gradient is likely partially due to the hilly local topography. In addition, an underpass of the MacArthur Freeway (I-580) located directly across Freedom Avenue (up groundwater gradient) from the site likely intercepts high groundwater levels and causes additional variation.

3.0 EXTENT OF GASOLINE CONSTITUENTS

No specific fuel release has been documented at this site. Historically, the highest gasoline constituent concentrations in soil and groundwater have been detected in the vicinity of the dispensers, product piping, and UST complex in the southwestern portion of the site. Separate-phase hydrocarbons (SPH) have previously been detected in former wells MW-1 and MW-2 and in well MW-3. Elevated concentrations of total petroleum hydrocarbons as gasoline (TPHg), benzene, toluene, ethylbenzene, xylenes (BTEX), methyl tertiary butyl ether (MTBE), and tertiary butyl alcohol (TBA) have been detected in all wells except MW-4, MW-6, and MW-9. Low TPHg and BTEX concentrations have been detected sporadically in MW-4, MW-6, and MW-9.

3.1 GASOLINE CONSTITUENT DISTRIBUTION IN SOIL

Elevated concentrations of petroleum constituents in the vadose zone soils have been found beneath dispensers and product piping, in boring SB-23 from 5 fbg to groundwater, and at lower concentrations around the tank complex in borings B-19, B-21, and B-21. Some vadose zone impact is also apparent at offsite boring MW-12. The other borings installed both on and off this site have not indicated vadose zone soil impact. The soil impact observed is at the soil/water interface which is more representative of groundwater impact. Thus, impacted soil is adequately delineated and appears to be in close proximity to the fueling equipment at this site. Historical soil analytical data summary tables are included in Appendix C. Sample locations are shown on Figure 2.

3.1.1 TPHG AND BENZENE

The highest TPHg and benzene concentrations detected historically were 4,100 milligram per kilogram (mg/Kg) and 11 mg/Kg, respectively, at pipe way sampling location P-4 in 2005. Concentrations of 848 mg/Kg TPHg and 1.38 mg/Kg benzene were detected in the soil sample from 24 fbg in offsite soil boring SB-24/MW-12 in 2006. As stated above, the concentrations in SB-24/MW-1 appear to be associated with dissolved hydrocarbons at the interface between the vadose zone and groundwater (smear zone). Figure 5 presents a TPHg isoconcentration contour map for soil samples within the smear zone (from 20 to 30 fbg). TPHg and benzene concentrations in shallow soils (less than 20 fbg) that exceed San Francisco Bay Regional Water Quality Control Board (RWQCB) Environmental Screening Levels (ESLs) for shallow soils where

groundwater is not a source of drinking water (residential land use) are all within the site. Within the site TPHg and/or benzene detections in soils extend to the smear zone in samples from well borings near the dispensers and UST complex. Detections of TPHg and benzene below the smear zone are likely due to groundwater impacts.

3.1.2 MTBE

MTBE was detected at concentrations up to 1.4 mg/Kg in soil samples collected adjacent to the UST complex and dispensers. The highest MTBE concentrations in soil were detected at approximately 24.5 fbg in well boring MW-11 in 2003 and at 2 fbg at sample location Disp-C during 1997 dispenser upgrades. The vertical extent of MTBE in soil has been defined by non-detect concentrations in deeper soil samples.

3.2 GASOLINE CONSTITUENT DISTRIBUTION IN GROUNDWATER

Horizontally, dissolved petroleum hydrocarbon and fuel oxygenate constituents are adequately defined by borings MW-5, BH-7, MW-4, MW-13, SB-13, BH-5, and SB-12 to the west, northwest, and north of the site. Further delineation of dissolved hydrocarbons and oxygenates is provided by SB-17, SB-18, MW-3, and MW-10 to the south, southeast, and east. Vertically, MW-9 and borings CPT-5 and CPT-6 delineate the extent of dissolved hydrocarbons and oxygenates to the northwest, southwest, and southeast. Historical groundwater analytical data is included in Appendix D.

3.2.1 TPHG AND BENZENE

The horizontal and vertical extent of TPHg and benzene has been defined. Up to 790,000 microgram per liter ($\mu\text{g/L}$) TPHg and 36,000 $\mu\text{g/L}$ benzene have historically been detected in former wells MW-1 and MW-2, respectively. The current maximum concentrations are in the vicinity of the UST complex with 92,000 $\mu\text{g/L}$ TPHg in well MW-11 and 2,500 $\mu\text{g/L}$ benzene in well EW-1. Piezometer P-3B contained a concentration of 5,700 $\mu\text{g/L}$ benzene in the fourth quarter of 2009, but is not included in the groundwater monitoring program. Figures 6 and 7 present current groundwater isoconcentration contour maps for TPHg and benzene, respectively. TPHg and benzene concentrations have historically been near or below laboratory reporting limits in down gradient wells MW-4, MW-6, and MW-9. CPT borings drilled in 2007 all showed that TPHg and benzene levels declined with depth.

3.2.2 MTBE

The vertical and horizontal extent of MTBE in groundwater has been defined, and MTBE concentrations currently demonstrate a stable to declining trend. Historically, up to 32,000 µg/L MTBE has been detected in former well MW-2, located northwest of the UST complex. Up to 8.50 µg/L MTBE has been detected in down gradient well MW-12, located across 150th Avenue from the site. The maximum concentration of MTBE detected during the first quarter 2009 was 390 µg/L in well EW-1. Again, piezometer P-1B contained a concentration of 1,300 µg/L MTBE in the fourth quarter of 2008, but is not included in the groundwater monitoring program. Figure 8 presents a current groundwater isoconcentration contour map for MTBE.

3.2.3 TBA

The presence of TBA is likely the result of MTBE degradation. The vertical and horizontal extent of TBA in groundwater has been defined, and TBA concentrations show a stable to slight declining trend over the period during which TBA concentrations have been monitored. TBA has only been detected in wells former wells MW-1 and MW-2, and in well MW-11 with a high concentration of 18,000 µg/L TBA detected in MW-11, located northwest of the UST complex. The distribution of TBA is correlated to the areas with the highest historic MTBE detections (near the former UST complex). During the second and third quarters of 2008, which is the most recent TBA data available, TBA was detected only in former well MW-1 at a concentration of 4,100 µg/L.

4.0 SENSITIVE RECEPTOR SURVEY (SRS)

Cambria Environmental Technology, Inc. (Cambria) conducted an SRS in 2003. No basements were found within 200 feet of the site, nor were any surface waters or sensitive habitats found within 500 feet of the site. No educational or childcare facilities were found within 1,000 feet of the site. The Fairmont Hospital Campus, located at 15400 Foothill Boulevard, is located 1,100 feet from the site, just outside the SRS target radius.

In 1992, Weiss and Associates (Weiss) reviewed the California Department of Water Resources (DWR) and Alameda County records to identify water wells within a ½-mile radius of the site. A total of 21 wells were identified: 12 monitoring wells, 8 irrigation wells, and 1 domestic well. No municipal wells were identified. Weiss concluded that groundwater is not a source of local drinking water. Cambria updated the well survey in 2003, but did not find any additional wells.

The closest identified water well potentially used for drinking water is a well installed in 1952, listed as a domestic well, and located at the Fairmont Hospital, approximately 2,445 feet east-southeast of the site. The well is reportedly 138 feet deep and is screened between 62 and 95 fbg. The well status and operation frequency are unknown. Due to the well location relative to the site and the observed groundwater flow directions, it is unlikely that this well is threatened by groundwater impacts.

The nearest surface water body is San Francisco Bay, which is about 6 miles to the west. Therefore, surface water is not threatened by groundwater impacts.

Soil vapor sampling results from September 2008 detected concentrations of TPHg, benzene, ethylbenzene, and xylenes exceeding RWQCB ESLs for residential land use.

4.1 SUMMARY OF CURRENT SITE CONDITIONS

Based on site investigations conducted to date, site conditions can be summarized as follows:

- Soil types encountered during drilling consisted predominantly of sandy silt/silty clay with gravel (ML/CL), silty clay (CL), with silty sand/sandy silt (SM/ML) and interbedded gravel (GC/GM/GP) increasing below 25 fbg to the total depth explored of 75 fbg.

- Elevated MTBE, TBA, TPHg, and benzene concentrations have been detected in soil and groundwater beneath the site. The vertical and horizontal extent of these constituents has been generally defined. Gasoline constituent concentrations are generally stable.
- A total of 21 wells were identified within a 1/2-mile radius of the site: 12 monitoring wells, 8 irrigation wells, and 1 domestic well. It is unlikely that the domestic well is threatened by groundwater from the site.
- In off-site soil vapor probe SVP-5, soil vapor TPHg concentrations exceeded residential and commercial land use RWQCB ESLs in two of the six sampling events. Ethylbenzene concentrations exceeded residential and commercial land use RWQCB ESLs during the September 15, 2008 sampling event. Benzene and xylenes concentrations exceeded residential land use RWQCB ESLs during the September 15, 2008 event. Soil vapor samples were collected on January 17, 2009 following CRA's November 2008 multi-phase extraction (MPE) pilot test. Soil vapors did not exceed RWQCB ESLs for this sample set. Soil vapor intrusion to residential indoor air may have been mitigated by the MPE pilot test, but remains a concern.

5.0 CORRECTIVE ACTION PLAN (CAP)

5.1 CLEANUP OBJECTIVES

CAP cleanup objectives are typically based on one or more of the following criteria:

- Department of Toxic Substances Control primary or secondary maximum contaminant level for drinking water, if applicable;
- RWQCB ESLs;
- Risk-based cleanup levels established by risk assessment or risk-based corrective action guidelines,
- Current closure guidelines from the regulatory agencies, such as the California State Water Resources Control Board criteria for low-risk groundwater cases, or
- Application of Best Available Technology based on remediation system operation data that demonstrate low, asymptotic levels have been achieved for chemical concentrations in extracted vapor and/or groundwater.

5.2 SOIL CLEANUP GOALS

For the purpose of this CAP, CRA assumes that the gasoline constituents detected in soil may pose a risk to groundwater quality, human health, and/or the environment. Review of current and historical soil data indicates that the primary potential health risk is intrusion of soil vapor into residential indoor air. Since shallow soil impacts exceeding residential ESLs are limited to the site, impacted soils and soil vapors do not appear to be a threat to the down gradient residences.

Since on-site soils are the remaining concern, CRA proposes using the RWQCB ESLs for commercial land use as the soil clean-up goals for this site. Although significant reductions in gasoline constituent concentrations in soil can be attained by various remedial alternatives, attainment of the proposed soil cleanup goals may prove to be technically or economically infeasible. Thus, soil cleanup will be limited to that which is technically or economically feasible.

5.3 GROUNDWATER CLEANUP GOALS

The site resides within the Santa Clara Valley East Bay Plain hydrologic unit (#2-9.04) according to the Department of Water Resources Bulletin 118. The RWQCB's January 18, 2007 *Water Quality Control Plan for the San Francisco Bay Basin* (Basin Plan) designates this unit as a beneficial drinking water source. Furthermore, the site lays within a Groundwater Management Zone "A" per the RWQCB's June 18, 2009 *The East Bay Plain Groundwater Basin, Beneficial Use Evaluation Report* (East Bay Plain Report), Section 17.9. For this zone designation, remedial strategies should be focused on actively maintaining or restoring groundwater quality to drinking water quality objectives. These areas historically supported a municipal beneficial use prior to the 1930's and likely could, with proper management, be used as a limited municipal source of drinking water in the future.

However, the East Bay Plain Report further states, "Within Zone A, there are also areas that may warrant less aggressive remediation on a case-by-case basis. As a mechanism to both recognize that the shallow groundwater is unlikely to be used for drinking water, but still safe guard the deeper aquifers for future drinking water supply uses, a less aggressive remediation strategy is recommended." Per Section 17.10, "There are groundwater pollution plumes that may warrant less aggressive remediation on a case-by-case basis. In general aggressive cleanup may not be warranted when the plume is shallow, concentrations are declining and no beneficial uses are threatened. The goal of the proposed Less Aggressive Remediation Approach is to outline 'basin specific' situations where less aggressive remediation may be acceptable."

Groundwater impacts at this site meet the criteria above (underlined) with exception to the declining concentration trends. It is expected that declining concentration trends will be achieved as a result of active remediation. At that point, this site will fully meet the criteria above. Given these conditions, CRA proposes using RWQCB non-drinking water ESLs as the groundwater cleanup goals. As with the attainment of soil cleanup goals described above, remediating to the proposed groundwater cleanup goals will likely prove technically or economically infeasible. Therefore, groundwater cleanup will be limited to that which is technically or economically feasible.

5.4 SUMMARY

The primary drivers for remediation are vadose zone soil impacts that leach to groundwater and create a vapor intrusion risk, and elevated hydrocarbon concentrations in groundwater.

The objective of remediation is to implement the most cost-effective remediation approach to protect human health and sensitive receptors. The ESLs listed below are proposed as cleanup goals for soil and groundwater. As stated above, attainment of these goals may not be technically or economically feasible. The goal of any remediation alternative proposed in this CAP will be to remove petroleum hydrocarbon mass from the subsurface to the extent practicable and mitigate human health risk. The constituents of concern (COCs), current maximum concentrations, and the proposed cleanup goals, based on RWQCB guidelines for fuel releases, are as follows:

COC	Soil		Groundwater	
	Concentration (a)	ESLs (b)	Concentration (c)	ESL (d)
	mg/Kg	mg/Kg	µg/L	µg/L
TPHg	4,100	180	92,000	210
Benzene	11	2.0	2,500	46
Toluene	83	9.3	11,000	130
Ethylbenzene	48	4.7	4,000	43
Xylenes	280	11	30,000	100
MTBE	1.4	8.4	390	1,800
TBA	0.177	110	4,100	18,000

Notes:

- (a) COC concentrations in soil based on highest detected concentrations in soil samples collected onsite. Offsite soil samples were not considered for this evaluation.
- (b) Deep Soil ESLs for commercial land use where groundwater is not a current or potential source of drinking water as summarized in Table D of the RWQCB Interim Final November 2007 document *Screening For Environmental Concerns at Sites with Contaminated Soil and Groundwater (Revised May 2008)*.
- (c) COC concentrations in groundwater based on highest detected during the first quarter 2009 sampling event, except for TBA which was last analyzed in the second and third quarters of 2008.
- (d) Groundwater ESLs for commercial sites where groundwater is not a current or potential source of drinking water as summarized in Table D of the RWQCB Interim Final November 2007 document *Screening For Environmental Concerns at Sites with Contaminated Soil and Groundwater (Revised May 2008)*.

Bold designates exceedances to the respective ESLs.

6.0 REMEDIAL ALTERNATIVES DISCUSSION AND APPROACH

The proposed remediation objective is based on a combination of the above criteria. The remediation objective is to implement the most cost-effective remedial approach to protect human health, groundwater quality, and other sensitive receptors. Given the site conditions, the site-specific objectives are to:

- Reduce potential risk of soil vapor intrusion to indoor air at down gradient residences;
- Reduce COCs in the identified source areas soils;
- Mitigate further COC impact to groundwater;
- Reduce COCs in groundwater;
- Continue the groundwater monitoring program to monitor water quality; and
- Establish a contingency plan to expedite or enhance remediation, if necessary.

Remediation alternatives reviewed in this CAP address these five objectives. Remedial alternatives were selected to address TPHg and BTEX in soil and TPHg, BTEX, MTBE, and TBA in groundwater.

The remedial technologies selected for evaluation include MPE, air sparging with soil vapor extraction (AS/SVE), in-situ chemical oxidation (ISCO), and monitored natural attenuation (MNA). Each of these alternatives are discussed below and evaluated on the basis of technical feasibility and cost effectiveness.

6.1 REMEDIAL ALTERNATIVES

6.1.1 MPE

MPE is the process of applying high vacuum through an airtight well seal to simultaneously extract soil vapors from the vadose zone and groundwater from the saturated zone. Extended dewatering of the saturated zone combined with vapor extraction can more effectively remediate residual gasoline hydrocarbons in the source area. In addition, the vacuum applied with MPE can increase the groundwater yield from wells completed in low permeability formations. Furthermore, groundwater extraction may provide hydraulic control of the hydrocarbon plume and reduce contaminant migration.

A positive displacement blower or liquid-ring pump may be used to create the high vacuum needed to extract groundwater and soil vapors simultaneously. Alternatively, a submersible groundwater pump can be used to extract groundwater, while a blower or liquid-ring pump is used solely to extract soil vapors. The extraction device is supplemented with a soil vapor treatment (oxidizer or carbon adsorption) system. Extracted groundwater is treated and discharged to the local sanitary sewer or storm drain with the appropriate authorization, or off-hauled to a disposal facility.

6.1.1.1 FEASIBILITY AND COST-EFFECTIVENESS

A pilot test was performed in November 2008 to determine the effectiveness of MPE. It was determined that the contaminated smear zone could not be adequately dewatered. Therefore, MPE is not recommended for this site and a cost estimate has not been prepared.

6.1.1.2 RECOMMENDATION

CRA does not recommend MPE as it can not sufficiently remove submerged hydrocarbons.

6.1.2 AS/SVE

Air sparge (AS) is an in-situ remedial technology that reduces concentrations of volatile constituents that are adsorbed to soils and dissolved in groundwater. This technology, which is also known as "in-situ air stripping" and "in-situ volatilization," involves the injection of contaminant-free air into the subsurface saturated zone, enabling a phase transfer of hydrocarbons from a dissolved state to the vapor phase. The vapor is then vented through the unsaturated zone. Air sparging is most often used together with soil vapor extraction (SVE), but it can also be used with other remedial technologies. When AS is combined with SVE, the SVE system creates a negative pressure in the unsaturated zone through a series of extraction wells to control the vapor plume migration. This combined system is called AS/SVE. SVE has also been a common technology used to remediate vadose zone soils. The applied negative pressure moves air through and strips (via volatilization) hydrocarbons from vadose zone soils. If air emissions need to be treated, extracted soil vapors are typically abated using an oxidizer or granular activated carbon (GAC).

Five AS wells and one SVE well would be installed. Additionally, monitoring wells P-1A, P-2A, P-3A, and P-4A would be used for SVE. Compressed air would be pumped into the AS wells and a blower would extract the volatilized vapors from the SVE wells. Vapor abatement would consist of either a thermal/catalytic oxidizer or a series of GAC vessels. A groundwater treatment system consisting of silt filters and GAC vessels would process water entrained with the extracted soil vapors before discharging the water to the sanitary sewer. Alternatively, the water could be containerized and hauled off site for treatment/disposal.

6.1.2.1 FEASIBILITY AND COST-EFFECTIVENESS

AS would likely be effective at volatilizing the submerged hydrocarbons; however, vapor recovery may be limited by intermittent silty-clay lenses found near and above the smear zone. SVE would likely be effective at reducing source area hydrocarbon mass already in the vadose zone, as the MPE pilot test indicated a reasonable vapor-phase radius of influence could be achieved.

Installation of the AS and SVE wells would cost approximately \$30,000. The system design, permitting, and installation would cost approximately \$70,000 assuming an oxidizer from Shell's existing stock is used. The annual operational cost is estimated at \$55,000. Assuming two years of AS/SVE operation and one year of low flow AS operation (at \$25,000 per year), the total cost is \$135,000. Quarterly monitoring during system design, operation, and two-year rebound monitoring over a five-year period would cost approximately \$60,000 at \$10,000 per year. System demo would cost \$30,000. The site closure request and well destructions are estimated at approximately \$40,000. The total cost for implementing AS/SVE is estimated at \$365,000.

6.1.2.2 RECOMMENDATION

SVE would be effective at removing vadose-zone impacts and mitigating the vapor intrusion risk. However, soil heterogeneities may inhibit the ability to adequately recover sparge vapors. An AS pilot test is necessary to verify if sufficient air can be injected into and distributed through the formation, and also recovered by SVE.

6.1.3 ISCO

ISCO is a remedial method that utilizes a strong oxidizing agent in order to promote a chemical reaction with organic compounds within the subsurface environment. During the reaction, the oxidizing agent breaks the carbon bonds in unsaturated compounds and converts the compounds into non-hazardous compounds such as CO₂ and water. Another benefit of ISCO is the production of dissolved oxygen (DO), which subsequently accelerates the naturally-occurring hydrocarbon biodegradation rate.

Common oxidizing agents include Fenton's reagents (hydrogen peroxide (H₂O₂) and ferrous iron (Fe⁺²) solution), persulfate (S₂O₈²⁻), and ozone (O₃).

6.1.3.1 FENTON'S REAGENT INJECTION

Injection of Fenton's Reagent, in the presence of metals that are commonly found in the subsurface, produces a hydroxyl radical that is a strong oxidizer and ultimately oxidizes hydrocarbons to water and carbon dioxide. This reaction is strongly exothermic and results in increased soil and groundwater temperatures when used in-situ.

Recommendation: Due to the exothermic nature of the reaction and the proximity of fuel equipment near the source/target area, Fenton's Reagent has been dropped from consideration.

6.1.3.2 PERSULFATE INJECTION

Persulfate is commonly applied as sodium persulfate to effectively buffer the pH. Hydrogen peroxide is mixed with the sodium persulfate to catalyze the persulfate radical into the sulfate radical which has a greater electrode potential. Persulfate is more persistent than H₂O₂ or ozone, and will have a greater radius of influence in highly permeable soils¹.

Feasibility and Cost-Effectiveness: The most practical approach for sodium persulfate injection would be gravity feeding sodium persulfate into eight new injection wells in the vicinity of the former waste oil tank and the existing USTs.

¹ Interstate Technology Regulatory Council, Technical and Regulatory Guidance for In Situ Chemical Oxidation of Contaminated Soil and Groundwater, Second Edition, January 2005

Based on the estimated hydrocarbon mass, the natural oxidant demand, and the radius of influence, three injection events injecting approximately 6,500 pounds (lbs) of sodium persulfate and 1,000 lbs of hydrogen peroxide per event would be adequate to oxidize the hydrocarbons within 10-feet of the injection wells.

Bench scale testing is estimated to cost \$10,000. It would cost approximately \$40,000 to install the proposed injection wells. The three injection events would cost approximately \$345,000. Monitoring until closure would cost approximately \$40,000 at \$10,000 per year. The site closure request and well destructions would cost an estimated \$40,000. The total estimated cost to implement ISCO with sodium persulfate is \$475,000.

Recommendation: Though persulfate would effectively oxidize the submerged hydrocarbons, the injection chemicals and labor costs are excessive relative to the other considered technologies. Additionally, persulfate injection does not address the vadose-zone remedial objectives: (1) reduce the potential risk to current and future on-site and off-site occupants, and (2) reduce COCs in source area soils. CRA does not recommend persulfate injection as it can not satisfactorily achieve all the objectives.

6.1.3.3 OZONE INJECTION

Ozone is the tri-atomic, highly reactive, relatively unstable form of oxygen, with a short half-life of approximately 2 minutes in ambient air conditions, and 20 minutes in the aqueous phase. In the aqueous phase, dissolved ozone can directly oxidize contaminants, degrade to the hydroxyl radical (which in turn can oxidize benzene), or degrade to dissolved oxygen, which can enhance natural biodegradation of contaminants. Ozone is 12.5 times more soluble in water than oxygen, which allows it to dissolve in water at substantially higher concentrations than pure oxygen. An ozone sparging system would utilize an ozone-generating system, an oxygen generating system, sparge injection points, SVE wells, SVE system (as discussed in the AS/SVE section above), and trenched conveyance piping.

Ozone can react strongly with subsurface utilities, and safety concerns for its use at an active service station should be considered. Strong oxidation processes such as those produced by ozone injection into earth materials have the potential to generate ancillary compounds that can dissolve into groundwater. These compounds may include trivalent and pentavalent arsenic, trivalent and hexavalent chromium, bromide, bromate, iron and manganese. Although published studies suggest that these reactive

byproducts are short-lived, a bench study is typically required before implementation of this alternative.

Feasibility and Cost Effectiveness: The most practical approach for ozone injection at this site would be injection into eight new injection wells in the vicinity of the former waste oil tank and the existing USTs.

Based on the estimated hydrocarbon mass, the natural oxidant demand, and the radius of influence, the ozone injection system would need to operate for approximately 12 to 18 months injecting into 8 wells to adequately oxidize the hydrocarbons within 10-feet of the injection wells. The ozone injection system would be supplemented with a SVE system to maintain a negative subsurface pressure to inhibit vapor migration and remove hydrocarbon mass from impacted vadose zone soils. The SVE system would extract from four existing SVE wells and one new SVE well.

An ozone bench-test would cost approximately \$10,000. It would cost approximately \$40,000 to install the proposed injection and SVE wells. The system design, permitting, and installation would cost approximately \$105,000 assuming an oxidizer from Shell's existing stock is used. The annual operational cost is estimated at \$55,000. Assuming one and a half years of operation, the total cost is \$82,500. Quarterly monitoring during system design, operation, and two-year rebound monitoring over a four and a half year period would cost approximately \$45,000 at \$10,000 per year. System demo would cost \$30,000. The site closure request and well destructions are estimated at approximately \$45,000. The total cost for implementing ozone injection/SVE is estimated at \$357,500.

Recommendation: As previously stated, SVE would be effective at removing vadose-zone impacts and mitigating the vapor intrusion risk. Ozone can be injected to target and oxidize the submerged hydrocarbons. However, it is uncertain if sufficient ozone mass can be injected into and adequately distributed through the formation. The ozone sparge system operates such that sparge vapors are not created as with AS, but ozone systems are generally more complex and more commonly operationally problematic. Similar to AS, AS pilot testing is necessary to verify if sufficient air (or ozone) can be injected into and distributed through the formation.

6.1.4 MNA

MNA consists of allowing hydrocarbons to biodegrade naturally and implementing a long-term groundwater monitoring plan. Decreasing concentration trends are the primary indicators of natural attenuation of hydrocarbons in groundwater. Secondary indicators such as DO concentrations, oxidation-reduction potential, alkalinity, and nitrate, sulfate, and ferrous iron concentrations are also used to evaluate the existence of and the potential for natural attenuation.

6.1.4.1 FEASIBILITY AND COST-EFFECTIVENESS

MNA is typically a low-cost alternative if cleanup levels can be met in a relatively short and/or acceptable timeframe. Given the current COC concentrations in groundwater, the timeframe to achieve cleanup levels by MNA would be unreasonable. Additionally, MNA is inappropriate considering the other project drivers, such as vapor intrusion. Therefore, MNA is only included in this evaluation of alternatives as a baseline comparison. Groundwater monitoring would cost an estimated \$10,000 per year, if MNA was deemed acceptable. Assuming a minimum of 30 years for MNA to achieve the remedial objectives, the total cost for groundwater monitoring is \$300,000. Destruction of existing wells would cost approximately \$35,000. A closure request is estimated at \$3,000; therefore, the total cost to implement MNA is estimated at \$338,000.

6.1.4.2 RECOMMENDATION

Although technically feasible, the anticipated time for current contaminant levels to reach cleanup levels is not a relatively short timeframe, and will likely be unacceptable to ACHCSA. Other project drivers also necessitate active remediation. Therefore, CRA does not recommend that MNA be implemented at this time. MNA should be implemented after another active remediation technology has been implemented and reached its effective limit.

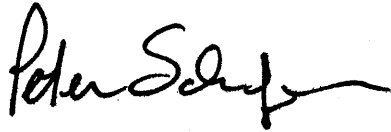
7.0 RECOMMENDATIONS

Alternative	MPE	AS/SVE	ISCO	Ozone w/ SVE	MNA
Pilot/Bench Test	Completed	Not Necessary	\$10,000	\$10,000	NA
Well Installations		\$30,000	\$40,000	\$40,000	NA
Design/Permit/Install*		\$70,000	\$345,000	\$105,000	NA
Annual Operation		\$55,000/\$25,000	NA	\$55,000	NA
Operation Duration		3 years	NA	1.5 years	NA
Total Operation		\$135,000	NA	\$82,500	NA
Annual Groundwater Monitoring		\$10,000	\$10,000	\$10,000	\$10,000
Monitoring Duration		6.0 years	4.0 years	4.5 years	30 years
Total Groundwater Monitoring		\$60,000	\$40,000	\$45,000	\$300,000
System Demolition		\$30,000	NA	\$30,000	NA
Well Destructions/Closure Request		\$40,000	\$40,000	\$45,000	\$38,000
Total Cost-to-Closure		\$365,000	\$475,000	\$357,500	\$338,000
Feasibility	Poor	Fair to Good	Fair	Fair to Good	Good
Effectiveness	Poor	Fair	Fair to Good	Good	Poor
Agency Acceptance	Good	Good	Fair to Good	Fair to Good	Poor
Recommended Alternative		X		X	

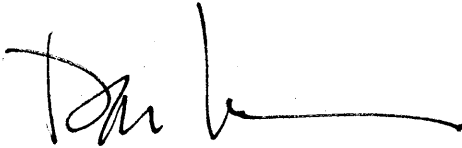
* On year duration assumed for design, permitting, and installation.

MPE and ISCO have been ruled out based on feasibility or cost. Ozone injection with SVE and AS/SVE are comparable in cost. Both approaches appear to be feasible, but have potential limitations. CRA recommends conducting an AS pilot test to verify if sufficient air can be injected into and distributed through the formation, and then recovered by SVE. A helium tracer would be used to confirm air distribution through the formation. The results of the AS pilot test should verify which of these approaches is preferred. Upon approval of the recommendations in this CAP, CRA will prepare a work plan to conduct an AS pilot test. Following the pilot test, CRA will submit an AS pilot test report with a recommendation to implement the preferred alternative.

All of Which is Respectfully Submitted,
CONESTOGA-ROVERS & ASSOCIATES



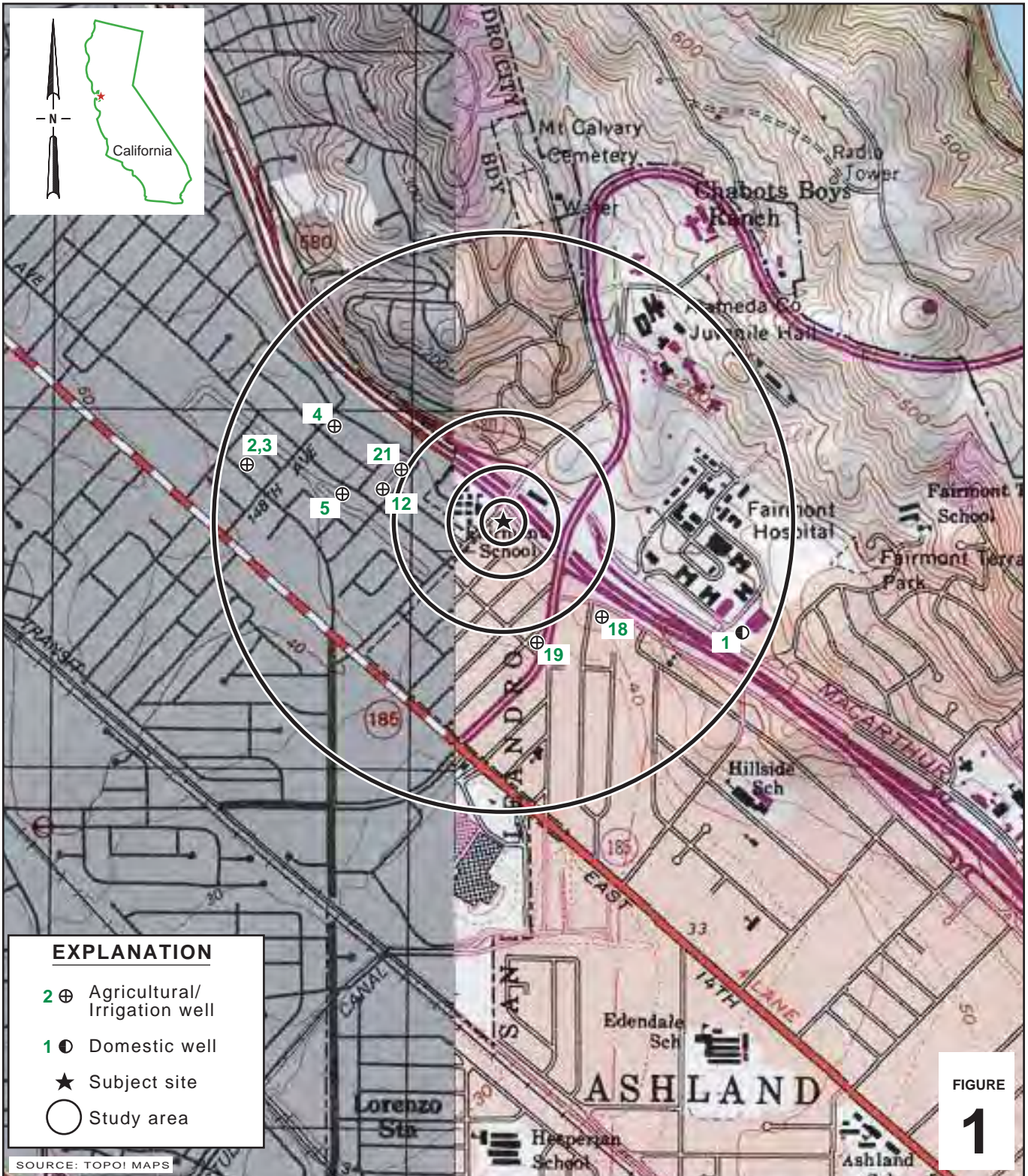
Peter Schaefer, CEG, CHG



Dan Lescure, PE



FIGURES



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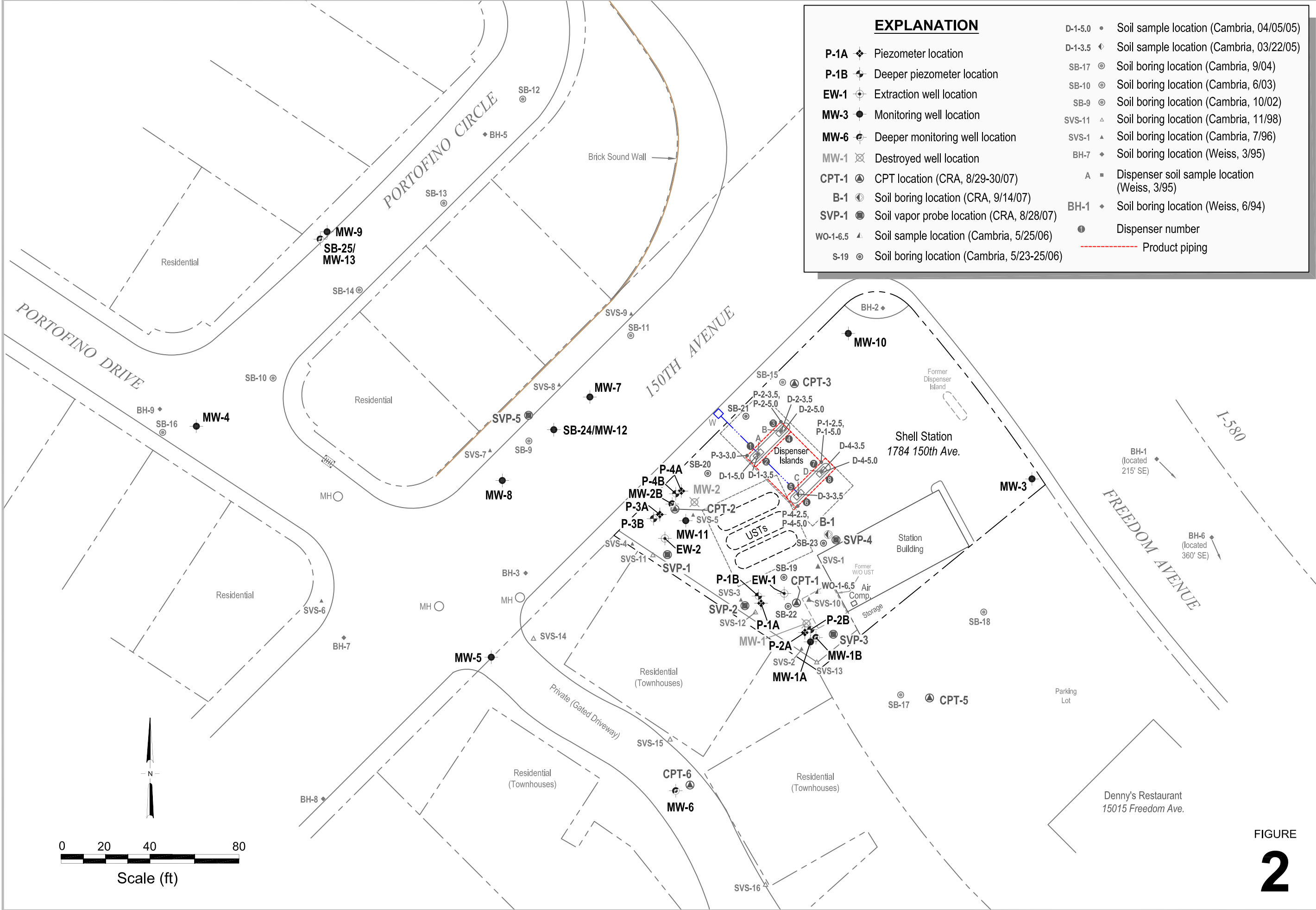
FIGURE 1

Shell-branded Service Station
 1784 150th Avenue
 San Leandro, California



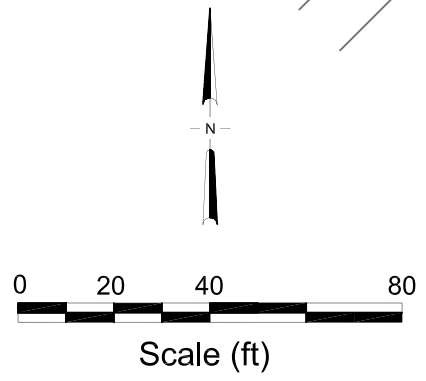
CONESTOGA-ROVERS & ASSOCIATES

Vicinity Map



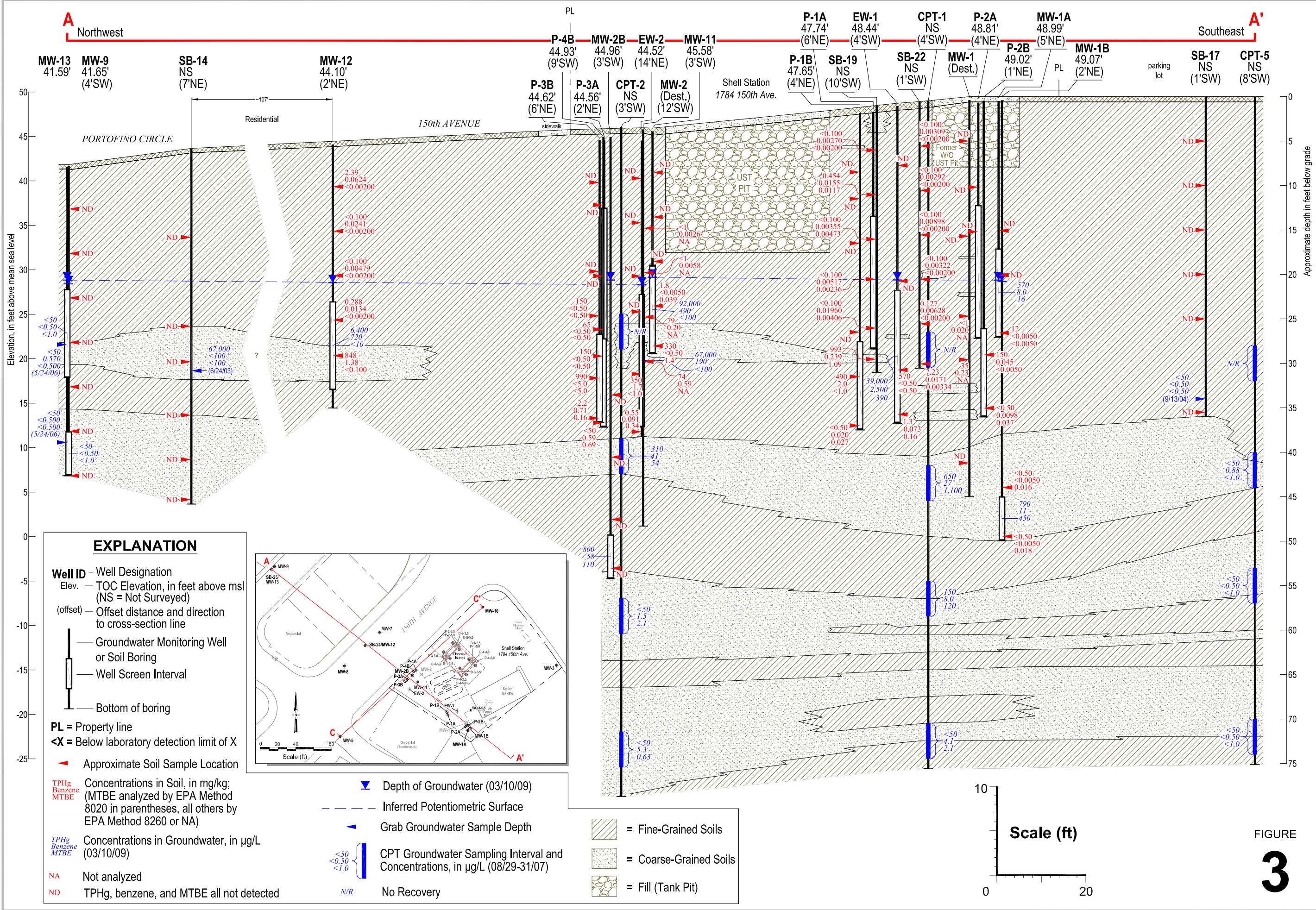
EXPLANATION	
P-1A	◆ Piezometer location
P-1B	⊕ Deeper piezometer location
EW-1	⊕ Extraction well location
MW-3	● Monitoring well location
MW-6	⊕ Deeper monitoring well location
MW-1	⊗ Destroyed well location
CPT-1	⊕ CPT location (CRA, 8/29-30/07)
B-1	⊕ Soil boring location (CRA, 9/14/07)
SVP-1	⊕ Soil vapor probe location (CRA, 8/28/07)
WO-1-6.5	⊕ Soil sample location (Cambria, 5/25/06)
S-19	⊕ Soil boring location (Cambria, 5/23-25/06)
D-1-5.0	⊕ Soil sample location (Cambria, 04/05/05)
D-1-3.5	⊕ Soil sample location (Cambria, 03/22/05)
SB-17	⊕ Soil boring location (Cambria, 9/04)
SB-10	⊕ Soil boring location (Cambria, 6/03)
SB-9	⊕ Soil boring location (Cambria, 10/02)
SVS-11	⊕ Soil boring location (Cambria, 11/98)
SVS-1	⊕ Soil boring location (Cambria, 7/96)
BH-7	◆ Soil boring location (Weiss, 3/95)
A	⊕ Dispenser soil sample location (Weiss, 3/95)
BH-1	◆ Soil boring location (Weiss, 6/94)
●	Dispenser number
---	Product piping

I:\Shell\6-chars\2406--240612-San Leandro 1784 150th\240612-FIGURES\240612 SITE PLAN.DWG



Shell-branded Service Station
 1784 150th Avenue
 San Leandro, California

FIGURE
2



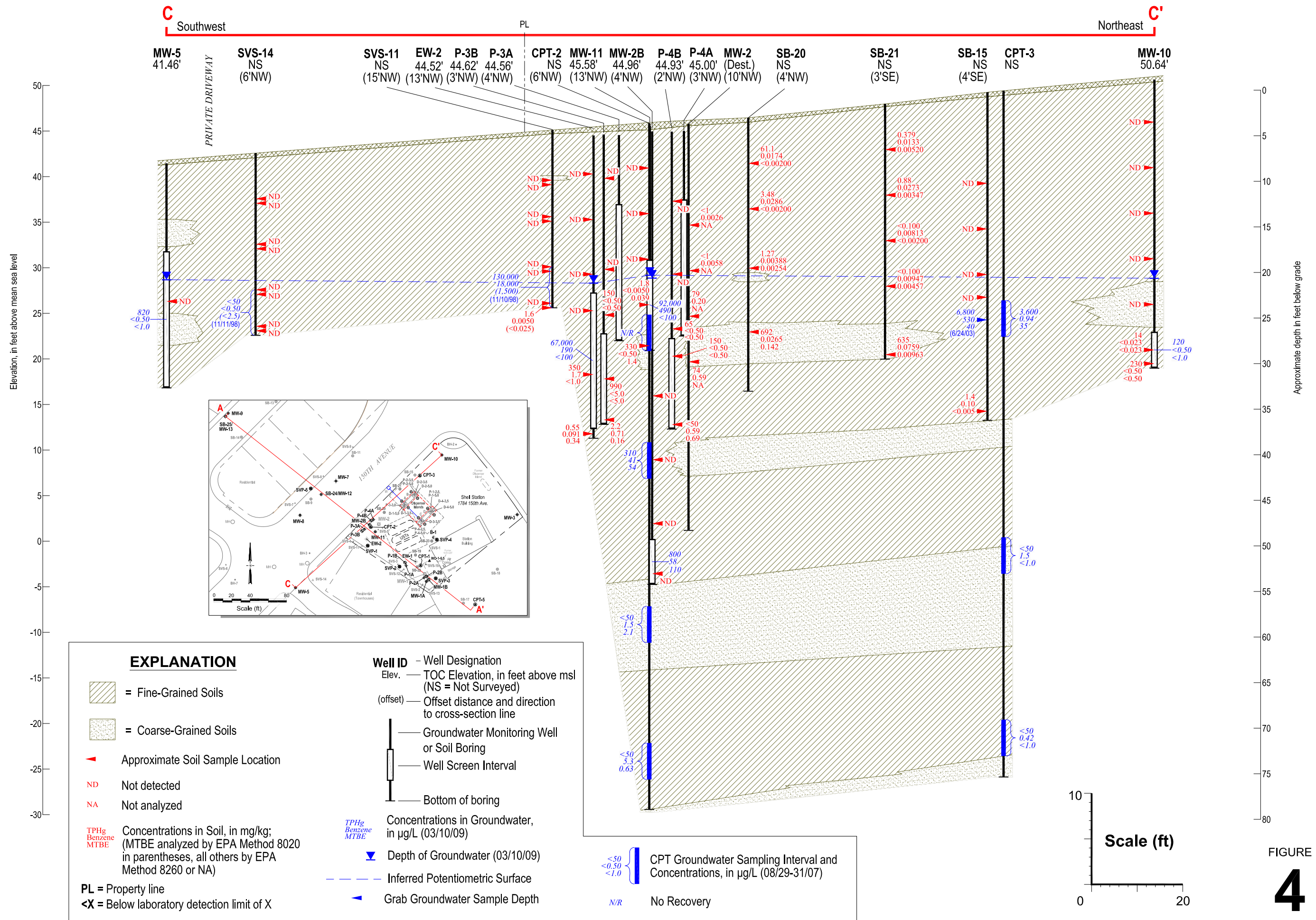
I:\Shell\6-chars\2406--240612-San Leandro 1784 150th\240612-FIGURES\240612 X-SECT A-A' 2009.DWG



Geologic Cross Section A-A'

Shell-branded Service Station

1784 150th Avenue
San Leandro, California



Geologic Cross Section C-C'

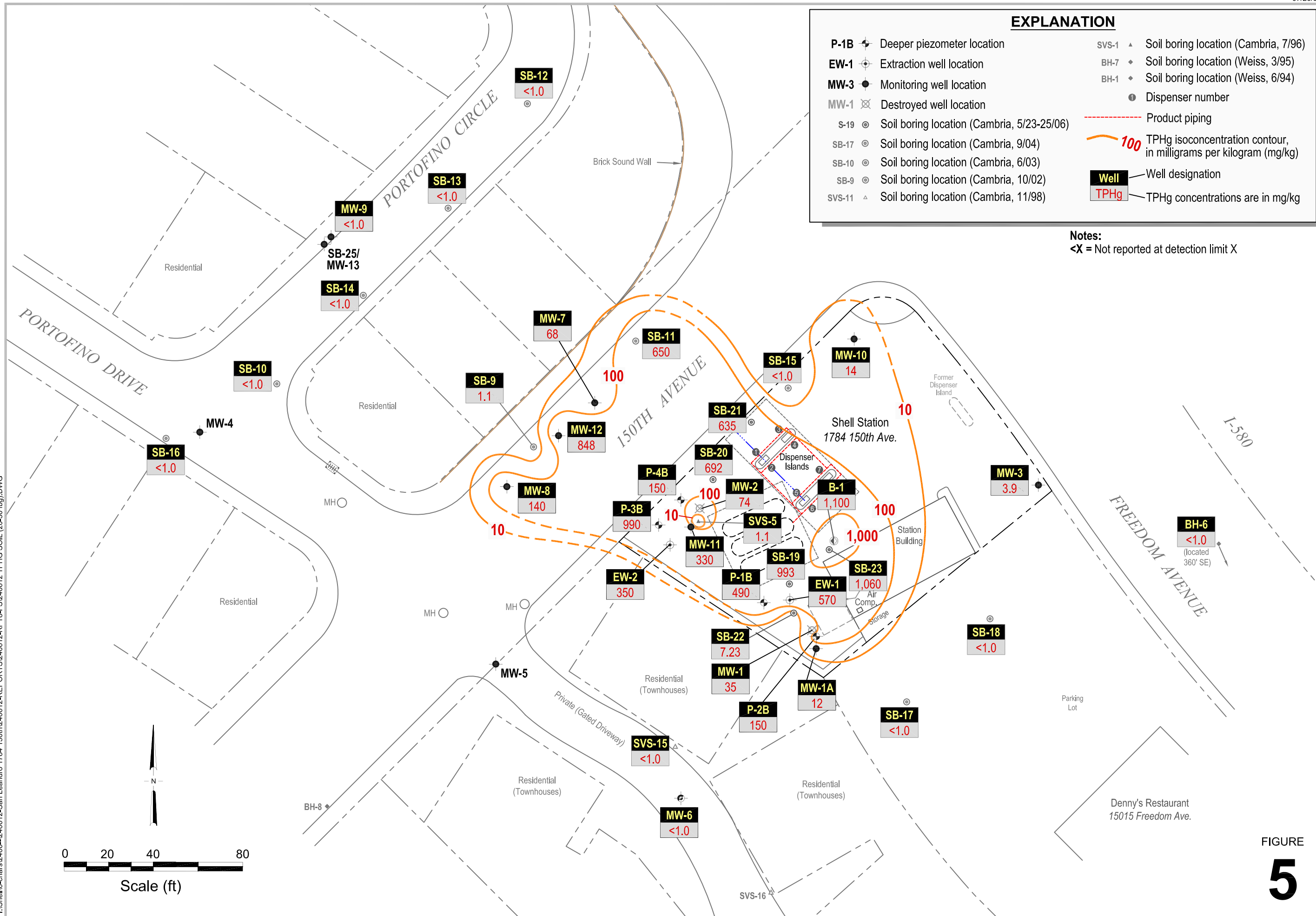


Shell-branded Service Station
 1784 150th Avenue
 San Leandro, California

FIGURE 4

I:\Shell\6-chars\2406--240612-San Leandro 1784 150th\240612-FIGURES\240612 X-SECT C-C' 2009.DWG

I:\Shell\6-chars\2406-1240612-San Leandro 1784 150th\240612-REPORTS\240612-RPT8-FS240612 TPHG SOIL (20-30 fbg).DWG



TPHg in Soil Isoconcentration Map

20 - 30 Feet Below Grade



CONESTOGA-ROVERS & ASSOCIATES

Shell-branded Service Station

1784 150th Avenue
San Leandro, California

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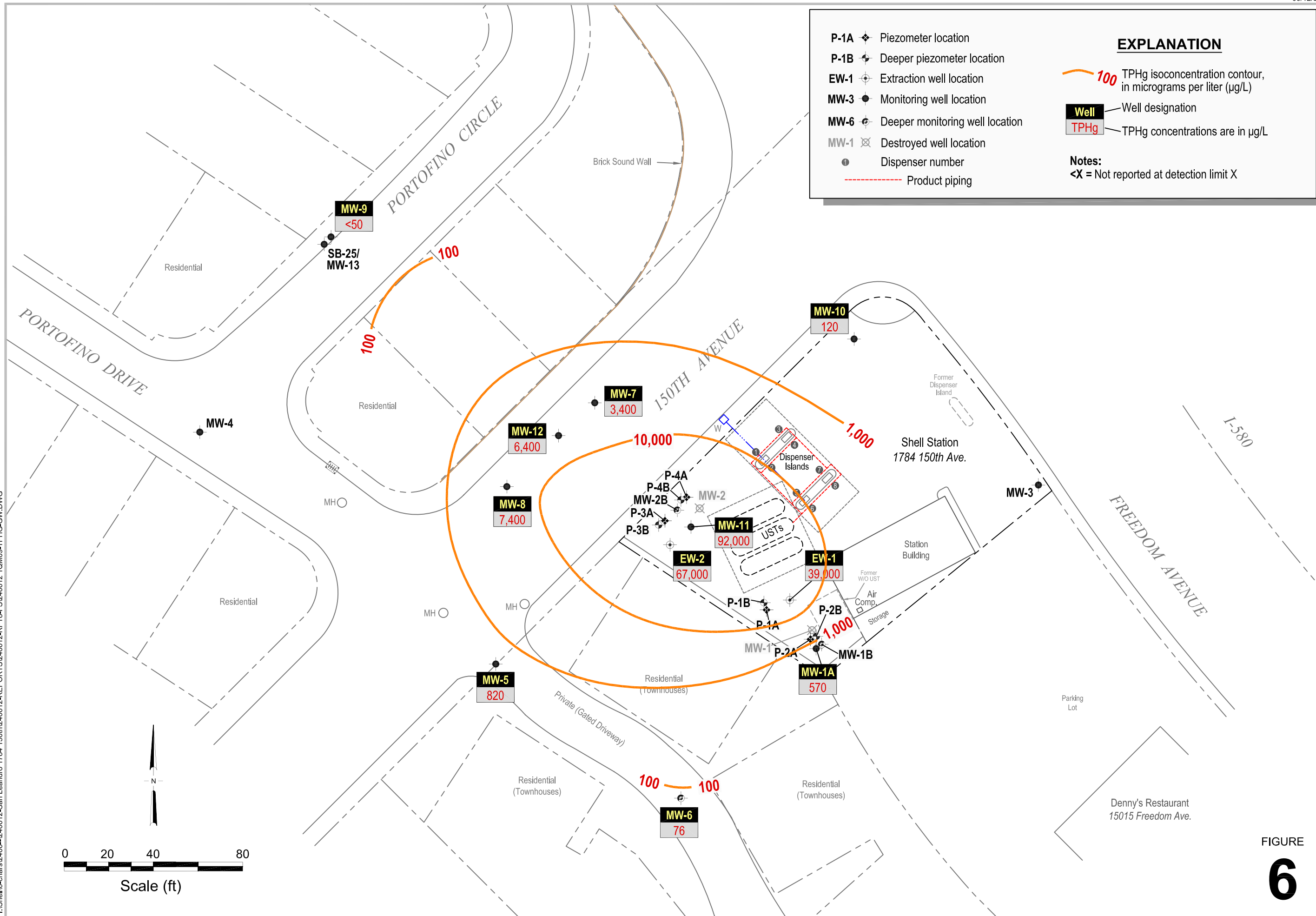
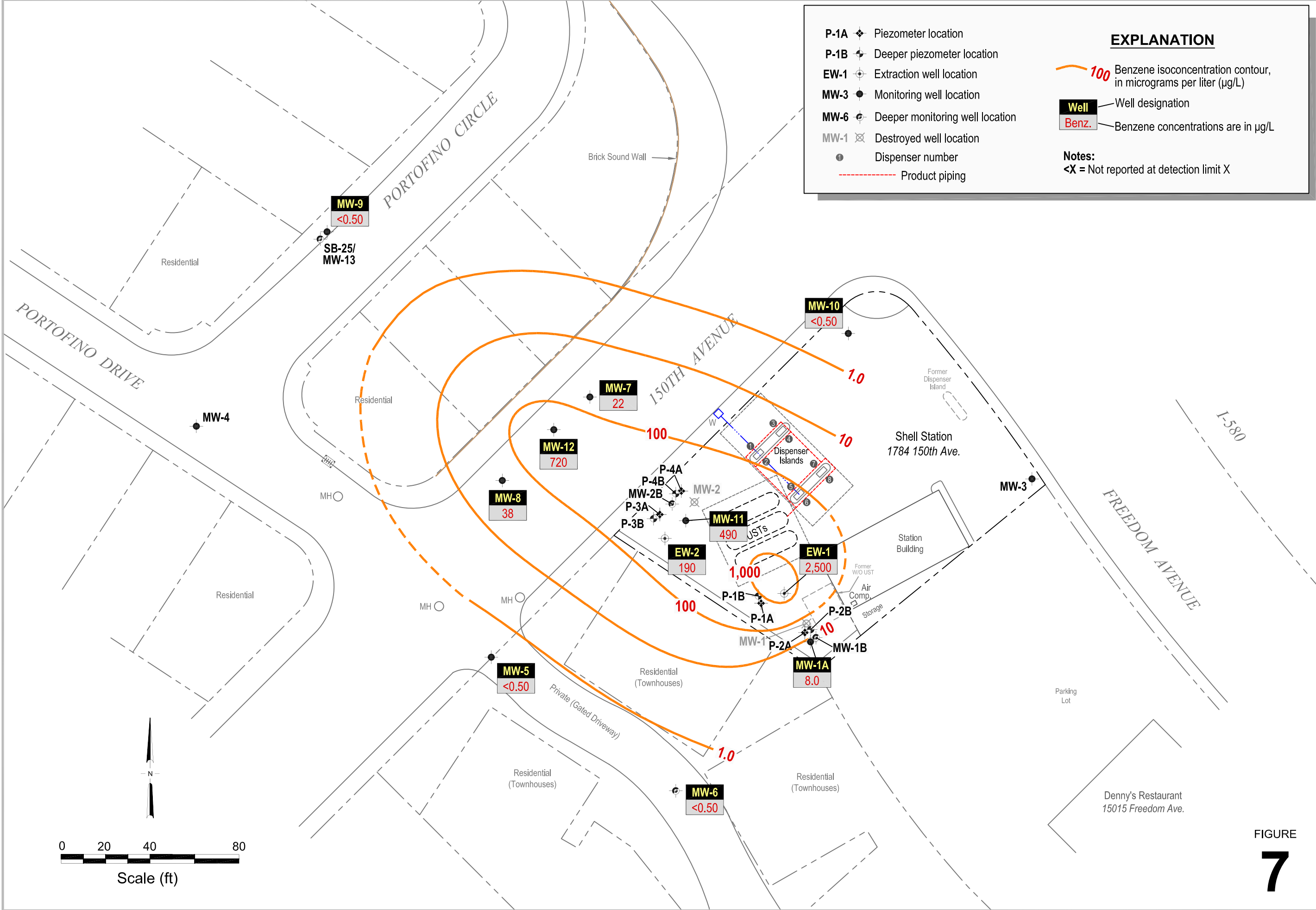


FIGURE 6



EXPLANATION

- P-1A ◆ Piezometer location
- P-1B ◆ Deeper piezometer location
- EW-1 ⊕ Extraction well location
- MW-3 ● Monitoring well location
- MW-6 ⊕ Deeper monitoring well location
- MW-1 ⊗ Destroyed well location
- ① Dispenser number
- - - Product piping

EXPLANATION

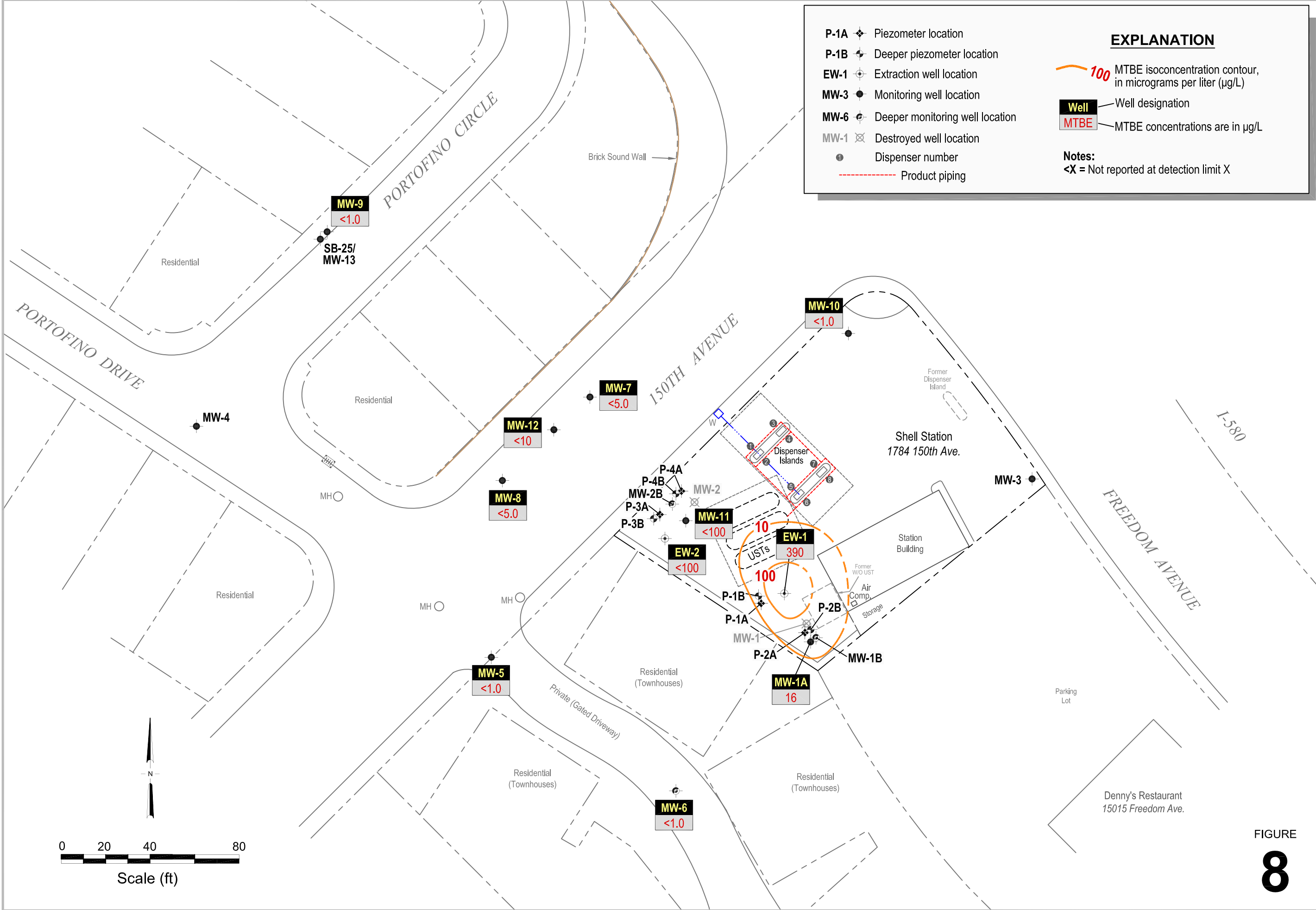
- 100 Benzene isoconcentration contour, in micrograms per liter (µg/L)
- Well Well designation
- Benz. Benzene concentrations are in µg/L

Notes:
 <X = Not reported at detection limit X

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FIGURE 7



EXPLANATION

- P-1A ◆ Piezometer location
- P-1B ◆ Deeper piezometer location
- EW-1 ⊕ Extraction well location
- MW-3 ● Monitoring well location
- MW-6 ⊕ Deeper monitoring well location
- MW-1 ⊗ Destroyed well location
- ① Dispenser number
- - - Product piping

EXPLANATION

- 100 MTBE isoconcentration contour, in micrograms per liter (µg/L)
- Well Well designation
- MTBE MTBE concentrations are in µg/L

Notes:
 <X = Not reported at detection limit X

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FIGURE 8

APPENDIX A

SITE HISTORY

SITE HISTORY

1986 Waste Oil Tank Removal: According to an October 13, 1989 letter from Weiss Associates (Weiss) of Emeryville, California to Shell, Petroleum Engineering of Santa Rosa, California removed a 550-gallon waste-oil tank from the site in November 1986). Blaine Tech Services, Inc. (Blaine) of San Jose, California collected soil samples (Soil #1 and Soil #2) beneath the former tank at 8 and 11 feet below grade (fbg). The soil samples contained up to 196 milligrams per kilogram (mg/kg) oil and grease. The tank pit was over-excavated to a total depth of 16 fbg, but no additional soil samples were collected. Groundwater was not encountered in the tank excavation. A new 550-gallon fiberglass waste-oil tank was installed in the same location.

1990 Well Installation: In March 1990, Weiss advanced soil boring BH-A, which was converted to groundwater monitoring well MW-1, adjacent to the waste-oil tank. In a soil sample collected at 29 fbg, 35 mg/kg total petroleum hydrocarbons as gasoline (TPHg) and 0.23 mg/kg benzene were detected. Details of this investigation are presented in Weiss' July 31, 1990 letter report to Alameda County Department of Environmental Health (ACDEH).

1992 Well Installations: In February 1992, Weiss advanced soil borings BH-B and BH-C, which were converted to monitoring wells MW-2 and MW-3. A soil sample collected near the water table from the boring for well MW-2 (21.5 fbg) contained 79 mg/kg TPHg. Soil samples from boring BH-C, which is located over 100 feet cross-gradient of the tanks, contained up to 68 mg/kg TPHg at 31.5 fbg. Details of this investigation are presented in Weiss' April 27, 1992 letter report to ACDEH.

1992 Well Survey: In 1992, Weiss reviewed the California Department of Water Resources (DWR) and Alameda County records to identify water wells within a 1/2-mile radius of the site. A total of 21 wells were identified: 12 monitoring wells, eight irrigation wells and one domestic well. No municipal wells were identified. The eight irrigation wells and one domestic well are more than 1,000 feet from the site.

1994 Subsurface Investigation: In June 1994, Weiss advanced six soil borings (BH-1 through BH-6) on and off site. No hydrocarbons were detected in soil samples from any borings, except for 0.013 mg/kg benzene in boring BH-3 at 16 fbg. No hydrocarbons were detected in grab groundwater samples from borings BH-1, BH-4, BH-5, and BH-6. The maximum concentrations of 120,000 micrograms per liter ($\mu\text{g}/\text{l}$) TPHg and 25,000 $\mu\text{g}/\text{l}$ benzene were detected in the grab groundwater sample collected from boring BH-3. Details of this investigation are presented in Weiss' October 13, 1994 *Subsurface Investigation* report.

1995 Well Installation: In February and March 1995, Weiss advanced four soil borings (BH-7 through BH-10) and converted BH-10 to monitoring well MW-4. No petroleum hydrocarbons were detected in any of the soil samples. Up to 100 µg/l TPHg and 1.0 µg/l benzene were detected in grab groundwater samples from BH-7 and BH-9. No TPHg or benzene was detected in the grab groundwater sample from BH-10. Groundwater was not encountered in soil boring BH-8. Details of this investigation are presented in Weiss' June 13, 1995 *Subsurface Investigation Report and First Quarter 1995 Monitoring Results*.

1996 Soil Vapor Survey and Soil Sampling: In July 1996, Weiss conducted a subsurface investigation to obtain site-specific data for a risk-based corrective action (RBCA) evaluation of the site. Soil vapor and soil samples were collected from the vadose zone at 10 on- and off-site locations (SVS-1 through SVS-10). The highest soil vapor hydrocarbon concentrations were detected near the northwest corner of the UST complex (sample SVS-5 at 3.0 fbg, which contained 7,600 parts per million by volume [ppmv] benzene). No TPHg, benzene, toluene, ethylbenzene, and xylenes (BTEX), or methyl tertiary-butyl ether (MTBE) was detected in any of the soil samples except for 1.1 ppmv TPHg detected in sample SVS-5 at 18 to 20 fbg. Weiss concluded that depleted oxygen concentrations and elevated carbon dioxide and methane concentrations in the vadose zone indicated that biodegradation was occurring.

1997 RBCA Evaluation: In 1997, Weiss prepared a RBCA evaluation for the site. RBCA analysis results indicated that BTEX, MTBE, 1,2-dichloroethane, and tetrachloroethylene concentrations detected in soil and groundwater beneath the site did not exceed a target risk level of 10^{-5} for residential indoor or outdoor air exposure pathways. However, a risk threshold exceedance was identified associated with ingestion of groundwater from a hypothetical well 25 feet down gradient of the source. Details of this evaluation are presented in Weiss' October 13, 1994 *RBCA Summary Report*.

1997 Dispenser and Turbine Sump Upgrade: The dispensers and turbine sumps at the station were upgraded in December 1997. Cambria Environmental Technology, Inc. (Cambria) collected soil samples Disp-A through Disp-D from beneath the dispenser islands during upgrade activities. Up to 590 mg/kg TPHg (Disp-C at 4.5 fbg), 1.8 mg/kg benzene (Disp-C at 2.0 fbg), and 1.4 mg/kg MTBE (Disp-C at 2.0 fbg) were detected. Details of this investigation are presented in Cambria's March 17, 1998 *Dispenser Soil Sampling* report.

1998 Soil Vapor Survey and Soil Sampling: In November 1998, Cambria conducted a subsurface investigation to obtain site-specific data for an updated RBCA evaluation of

the site. Soil samples, soil vapor samples, and grab groundwater samples were collected from the vadose zone at three on-site and three off-site locations (SVS-11 through SVS-16). In soil vapor, maximum concentrations of 2.7 ppmv TPHg (C5+ hydrocarbons) and 0.17 ppmv TPHg (C2-C4 hydrocarbons) were detected at 10 fbg in borings SVS-14 and SVS-15, respectively. A maximum concentration of 0.0099 ppmv benzene was detected in SVS-16 at 5 fbg. In soil, 1.6 mg/kg TPHg and 0.0050 mg/kg benzene were detected in boring SVS-11 at 19.5 fbg. No TPHg or benzene was detected in any other soil samples. MTBE was reported at 0.029 mg/kg in boring SVS-14 at 19 fbg using EPA Method 8020; however, MTBE was not detected in this sample using EPA Method 8260. TPHg and benzene were detected using EPA Method 8020 in groundwater from borings SVS-11 and SVS-12 at concentrations up to 130,000 µg/l TPHg and 18,000 µg/l benzene. MTBE was reported at a concentration of 1,500 µg/l in boring SVS-11 by EPA Method 8020, but was not confirmed by EPA Method 8260.

1999 RBCA Evaluation: In September 1999, Cambria prepared a RBCA evaluation for the site. Cambria analyzed the following potential exposure pathways: off-site ingestion of groundwater, on-site ingestion of surficial soil, volatilization of benzene from soil or groundwater into on-site or off-site indoor air, and migration of benzene soil vapor to on-site or off-site outdoor air. Results of Tier 1 and Tier 2 RBCA analyses indicated that contaminants within soil and groundwater did not present significant health risks. Details of this evaluation are presented in Cambria's September 17, 1999 *Risk-Based Corrective Action* report.

2001 Off-Site Monitoring Well Installation: Two monitoring wells (MW-5 and MW-6) were installed off site to the southwest. Soil sample results from this investigation indicated only minimal MTBE impact (0.012 mg/kg) to off-site soil southwest of the site. This finding was corroborated by Cambria's 1998 subsurface investigation, in which no TPHg or benzene and only low MTBE concentrations were detected in soil from three borings (SVS-14 through SVS-16) along the private driveway. Details of this investigation are presented in Cambria's December 20, 2001 *Offsite Monitoring Well Installation Report*.

2002-2004 Mobile Groundwater Extraction (GWE): In July 2002, semi-monthly GWE was begun using monitoring well MW-2, and it continued on a monthly basis until March 2004. Beginning in March 2004, monthly GWE was performed using well MW-2 and MW-11 once per month each, so that GWE was conducted twice per month at the site. The GWE frequency was increased to weekly (from both MW-2 and MW-11) beginning in May 2004. Mobile GWE ceased on August 24, 2004. Approximately 19.6 lbs. of TPHg, 3.45 lbs. of benzene, and 5.12 lbs. of MTBE had been removed during these activities.

2002 Off-Site Monitoring Well Installation: Two monitoring wells (MW-7 and MW-8) and one soil boring (SB-9) were installed off-site and northwest of the site in 150th Avenue. Soil sample results collected during this investigation indicated minimal TPHg and BTEX impact to off-site soil northwest of the site. Grab groundwater samples indicated elevated TPHg and benzene concentrations were present in groundwater northwest of the site beneath 150th Avenue. Details of this investigation are presented in Cambria's November 18, 2002 *Offsite Monitoring Well Installation Report*.

2003 Soil and Groundwater Investigation: Six soil borings (SB-10 through SB-14 and SB-16) were advanced to the northwest of the site in both 150th Avenue and Portofino Circle; one boring (SB-15) was advanced on site. Initial groundwater was encountered between 24 and 28 fbg during drilling activities. During the investigation, MTBE was only detected in on-site grab groundwater sample SB-15-W at 40 µg/l. The highest TPHg concentration was detected in SB-14-W at 67,000 µg/l, and the highest benzene concentration was detected in SB-15-W at 530 µg/l. TPHg was detected only in soil samples SB-11-30' and SB-15-36' at concentrations of 650 mg/kg and 1.4 mg/kg, respectively. Benzene was detected only in soil sample SB-15-35' at 0.10 mg/kg. Based on typical groundwater depths in nearby well MW-7, it was determined that samples SB-11-30' and SB-15-36' were saturated, and results may be more indicative of chemical concentrations in groundwater. Details of this investigation are presented in Cambria's August 28, 2003 *Soil and Water Investigation Report and Work Plan*.

2003 Sensitive Receptor Survey (SRS): In October 2003, Cambria completed an SRS at Shell's request. The SRS targeted the following as potential sensitive receptors: basements within 200 feet, surface water and sensitive habitats within 500 feet, hospitals, residential care, and childcare facilities within 1,000 feet, and water wells within ½ mile. No basements, surface water, sensitive habitats, or educational and childcare facilities were identified within the search radius. The Fairmont Hospital campus, located at 15400 Foothill Boulevard, is located approximately 1,100 feet from the site, just outside the target radius of 1,000 feet.

To update the 1992 well survey performed by Weiss, Cambria researched DWR records in September 2003 and located no additional well records for locations within ½ mile of the site. The closest identified water well potentially used for drinking water is a well installed in 1952 and listed as a "domestic well." This well is located at Fairmont Hospital, approximately 2,445 feet east-southeast of the site. The well is reportedly 138 feet deep and has a screened interval between 62 and 95 fbg. The well's status and operation frequency are unknown. Due to the well's distance from the site and the site's

observed groundwater flow directions, it is unlikely that this well would be impacted by groundwater from the site.

2003 Monitoring Well Installation: On November 19 and 20, 2003, Cambria installed on-site and off-site wells MW-9, MW-10, and MW-11. Proposed off-site soil borings were not completed due to access agreement issues. MTBE was detected in two soil samples (MW-11-20' and MW-11-24.5') at concentrations of 0.039 and 1.4 mg/kg, respectively. TPHg was detected in four soil samples (MW-10-30', MW-10-31.5', MW-11-20', and MW-11-24.5') at concentrations of 14, 230, 1.8, and 330 mg/kg, respectively. All soil samples with detectable hydrocarbon and MTBE concentrations were saturated soil samples, so identified results appeared more indicative of chemical concentrations in groundwater than soil. Details of this investigation are presented in Cambria's January 12, 2004 *Soil and Water Investigation and Monitoring Well Installation Report*.

September 2004 Off-Site Investigation: Two soil borings (SB-17 and SB-18) were installed southeast of the site. No TPHg, BTEX, or fuel oxygenates were detected in soil samples from the borings. Grab groundwater samples collected contained up to 55 µg/l TPHg, and no benzene or fuel oxygenates. Results of the investigation are reported in Cambria's December 17, 2004 *Soil and Water Investigation Report*.

2004 Temporary GWE System Installation: On September 13, 2004, Cambria completed installation and began operation of a temporary GWE system. The temporary GWE system was installed as an interim remedial measure to address the elevated petroleum hydrocarbon and MTBE concentrations in groundwater near the west corner of the site. On November 8, 2004, Cambria stopped the temporary GWE system to conduct interim remediation by dual phase extraction (DPE). During these temporary GWE activities approximately 0.448 lbs. of TPHg, 0.036 lbs. of benzene, and 0.121 lbs. of MTBE were removed from the subsurface.

2004 DPE: During the period November 8 through November 13, 2004, DPE was conducted in on-site wells MW-2 and MW-11 as an interim remedial action to reduce hydrocarbon concentrations in groundwater near the western corner of the site and to progress the site toward closure. Based on operating parameters and vapor sample analytical results, the total TPHg, benzene, and MTBE vapor-phase masses removed from well MW-11 are estimated at 165 lbs., 0.291 lbs., and 0.063 lbs., respectively. The total TPHg, benzene, and MTBE vapor-phase masses removed from well MW-2 are estimated at 0.073 lbs., 0.0002 lbs., and 0.001 lbs., respectively. The total TPHg, benzene and MTBE liquid-phase masses removed from wells MW-2 and MW-11 during interim remediation are estimated at 5.31 lbs., 0.193 lbs., and 0.143 lbs., respectively.

2005 Temporary GWE System: Upon completing the interim remedial action, Cambria intended to immediately resume operating the temporary GWE system. However, the restart was delayed due to repaving the site's parking lot. The temporary GWE system operated between January 10 and April 13, 2005. Because detected TPHg and MTBE concentrations were higher in well MW-11 than in well MW-2, MW-11 was chosen for extraction. During these activities, approximately 19.04 lbs. of TPHg, 1.69 lbs. of benzene, and 3.94 lbs. of MTBE were removed from the subsurface. Because of facility upgrades work, Cambria removed the temporary GWE system between March and June 2005. Results of the remediation are reported in Cambria's June 23, 2005 *Interim Remediation Report*.

2005 Fuel System Upgrade: Under contract to Shell, Armer Norman of Pacheco, California replaced the fuel dispensers and piping and upgraded UST sumps between March and May 2005. On March 22 and April 4, 2005, soil samples were collected beneath each of the four dispensers and the product piping joints. TPHg was detected in 11 samples, with a maximum concentration of 4,100 mg/kg in sample P-4-5.0. Benzene was detected in six samples, with a maximum concentration of 11 mg/kg in sample P-4-2.5. MTBE was detected in five samples, with a maximum concentration of 0.18 mg/kg in sample D-1-3.5. Tertiary-butyl alcohol (TBA) was detected in sample D-3-3.5 at a concentration of 0.023 mg/kg. Lead was detected in four samples, with a maximum concentration of 75.7 mg/kg in sample D-1-3.5. Results of the investigation are reported in Cambria's June 1, 2005 *Dispenser and Piping Upgrade Sampling Report*.

2005 Periodic GWE Restart: In September 2005, monthly GWE was re-instated using monitoring well MW-11, and because of the observed presence of SPH in well MW-1, bimonthly extraction from MW-1 was initiated in September 2006. These activities are continued through August 2007 and are reported in the quarterly groundwater monitoring reports.

May 2006 Waste Oil Tank Removal: On May 25, 2006, Wayne Perry, Inc. (Wayne Perry) of Sacramento, California removed one 550-gallon, dual-wall fiberglass waste oil UST. Cambria collected one soil sample (WO-1-6.5) from the sidewall of the UST excavation at a depth of 6.5 fbg. The soil sample contained up to 45 mg/kg oil and grease, 4.3 mg/kg TPHd, 25.4 mg/kg chromium, 7.09 mg/kg lead, 19.0 mg/kg nickel, and 58.4 mg/kg zinc. Based on these concentrations, Shell submitted an Underground Storage Tank Unauthorized Release (Leak)/Site Contamination Report (Unauthorized Release Report) on June 6, 2006. All detections were below SFBRWQCB environmental screening levels for shallow soil (fewer than 3 meters below grade) where groundwater is a current or potential drinking water source for residential land use areas. Based on these results, no

further investigation of waste oil constituents was conducted. Results of the investigation are reported in Cambria's August 4, 2006 *Underground Storage Tank Removal Report*.

May 2006 Subsurface Investigation (SB-19 through SB-25; MW-12 & MW-13): The purpose of this investigation was to determine the vertical and horizontal extent of soil and groundwater impact. Seven soil borings were advanced, two of which were converted to groundwater monitoring wells. Shallow soil samples collected from borings SB-19, SB-20, SB-21, SB-22, and SB-24 did not contain TPHg or BTEX concentrations exceeding applicable published San Francisco Bay Regional Water Quality Control Board environmental screening levels (ESLs). Up to 1,060 mg/kg TPHg and 1.38 µg/l benzene were detected in soil samples collected from the capillary fringe zone in borings SB-19, SB-20, SB-21, SB-23, and SB-24. These detections are considered to be more indicative of groundwater conditions. Fuel oxygenate concentrations were near or below their respective reporting limits in all soil samples collected, and none of the low detections exceeded applicable ESLs. Based on this, the horizontal extent of petroleum hydrocarbons has been defined at the site, and the vertical extent has been defined to the typical groundwater table. TPHg, BTEX, and fuel oxygenate concentrations in grab groundwater samples collected from approximately 20 and 31 fbg in boring SB-25 were also near or below their respective reporting limits. None of the low detections in the grab groundwater samples collected exceed applicable ESLs. Based on this, the vertical extent of petroleum hydrocarbons in groundwater northwest of the site is defined. Results of the investigation are reported in Cambria's July 26, 2006 *Subsurface Investigation Report*.

February 2007 Agency Response with Proposed Future Actions: Cambria responded to ACEH's August 29, 2006 letter which requested updated cross-sections and discussion of other issues. Cambria provided revised cross-sections A-A' and C-C', a discussion of delineation of the extent of petroleum hydrocarbons in soil and groundwater, and a risk evaluation based on these delineations. In addition, Cambria proposed delineation of the vertical extent of petroleum hydrocarbons in groundwater and a shallow soil vapor investigation at the site. The complete report is provided in Cambria's February 17, 2007 *Agency Response with Proposed Future Actions*.

December 2007 Supplemental Subsurface Investigation Report: CRA drilled five cone penetrometer test borings (CPT-1 through CPT-3, CPT-5 and CPT-6) to delineate the vertical extent of petroleum hydrocarbons in groundwater, drilled on hollow-stem auger boring (B-1) to delineate the vertical extent of petroleum hydrocarbons in soil adjacent to the UST complex, and installed and sampled five soil vapor probes (SVP-1 through SVP-5). The investigation was conducted in response to ACEH's July 2, 2007

correspondence which concurred with CRA's February 2007 recommendations. Results of the investigation are reported in CRA's December 19, 2007 *Supplemental Subsurface Investigation Report*.

Shallow soil samples from SVP-1 through SVP-3, and SVP-5 did not contain detectable levels of TPHg, BTEX or MTBE, and the detection in SVP-4 and samples from B-1 were all below the San Francisco Bay Regional Water Quality Control Board (SFBRWQCB) environmental screening levels (ESLs) for shallow and deep soil at residential properties where groundwater is not a potential source of drinking water (Tables B and D of November 2007 ESL document). Data from boring B-1 confirm the presence of residual source material in vadose zone soils in this area, however, the shallower concentrations were lower, and the deepest sample interval (29.5 fbg) was higher when compared with the data collected from nearby boring B-23 in 2006.

Groundwater grab sample analyses were all below the ESLs for sites where groundwater is not a current or potential source of drinking water. Based on the results from this investigation, the horizontal extent of significant petroleum hydrocarbons was determined to be defined at the site, and the vertical extent was found to be confined to the shallower groundwater intervals. The deeper samples obtained from CPT-1 and CPT-3 indicated that the shallower zone (less than 30 fbg) was more impacted than deeper zones.

All soil vapor sample analyses were below ESLs for residential and commercial land use for the BTEX and MTBE constituents, and SVP-2 and SVP-3 were below the ESLs for TPHg. SVP-1, SVP-4, and SVP-5 exceeded the residential ESL and SVP-5 exceeded the commercial ESL for TPHg. Since the groundwater concentrations offsite are lower than those onsite, and since there was impacted vadose zone soil samples near SVP-5 (reported in boring MW-12), it appears that the TPHg concentration in soil gas reflects migration of vapors from shallow impacted soil rather than from the impacted groundwater at depth.

CRA recommended destruction of wells MW-1 and MW-2 due to overly long screen intervals, replacement of well MW-1 with an appropriately screened well in the shallow zone (4-inch diameter well) and a deeper screened well in the within the sandy unit encountered below 40 fbg (2-inch diameter well) and installation of a shallow-zone monitoring well at the location of boring B-1.

Soil Vapor Probe Sampling: CRA resampled soil vapor probes SVP-1 through SVP-3 and SVP-5 in March, May, and September 2008 and in January and July 2009. SVP-4 could not be sampled due to water in the probe's tubing during any of these events and

SVP-5 contained water during the July 2009 event. All soil vapor sample concentrations were below SFBRWQCB ESLs for residential and commercial land use, although some reporting limits were elevated. The TPHg concentrations in SVP-1 and SVP-5 have decreased since the September 25, 2007 sampling event.

2008 Subsurface Investigation: Groundwater monitoring wells (MW-1 and MW-2) were destroyed because their excessive screen length provided a potential conduit to deeper groundwater. Three groundwater monitoring wells (MW-1A, MW-1B, and MW-2B) were installed to replace MW-1 and MW-2. Two DPE wells (EW-1 and EW-2) and eight piezometers (P-1A through P-4A and P-1B through P-4B) were installed for use in groundwater pump tests and a DPE pilot test. Benzene, MTBE, and TBA were not detected at levels above RWQCB ESLs in any of the soil samples collected during this investigation. Only four TPHg detections in soil exceed ESLs (P-3B at 27 fbg, EW-1 at 30 fbg, EW-2 at 27 fbg, and P-1B at 30 fbg). Ethylbenzene and xylenes also exceeded the ESLs in these samples. Toluene was detected at a concentration above the ESL in one sample (P-3B at 27 fbg). Based on the sample depths, these detections may be related to groundwater. This investigation is detailed in CRA's February 5, 2009 *Subsurface Investigation Report*.

2008 Multi-Phase Extraction Pilot Test: CRA conducted aquifer pumping test and a multi-phase extraction test were performed to provide information needed to evaluate the appropriate remedial option to address dissolved-phase petroleum hydrocarbons detected in groundwater. This investigation is detailed in CRA's February 5, 2009 *Aquifer Pumping Test and Multi-Phase Extraction Pilot Test Report*.










Groundwater Monitoring Program: Groundwater quarterly groundwater sampling began in March 1990. Historically, the maximum concentrations of TPHg have been observed in well MW-1 (up to 790,000 µg/l in June 1996); maximum concentrations of benzene have been observed in well MW-2 (up to 36,000 µg/l in March 1993); and maximum concentrations of MTBE have been observed in well MW-2 (up to 32,000 µg/l in February 2002). Separate phase hydrocarbons (SPH) have been observed intermittently in wells MW-1 and MW-2 historically. Since the September 2007 sampling event no more SHP had been observed.

APPENDIX B

BORING LOGS













Boring/Well Log Legend

KEY TO SYMBOLS/ABBREVIATIONS

-  First encountered groundwater
-  Static groundwater
-  Soils logged by hand-auger or air-knife cuttings
-  Soils logged by drill cuttings or disturbed sample
-  Undisturbed soil sample interval
-  Soil sample retained for submittal to analytical laboratory
-  No recovery within interval
-  No recovery within interval
-  Hydropunch or vapor sample screen interval

- PID = Photo-ionization detector or organic vapor meter reading in parts per million (ppm)
- fbg = Feet below grade
- Blow Counts = Number of blows required to drive a California-modified split-spoon sampler using a 140-pound hammer falling freely 30 inches, recorded per 6-inch interval of a total 18-inch sample interval
- (10YR 4/4) = Soil color according to Munsell Soil Color Charts
- msl = Mean sea level
- Soils logged according to the USCS.

UNIFIED SOILS CLASSIFICATION SYSTEM (USCS) SUMMARY

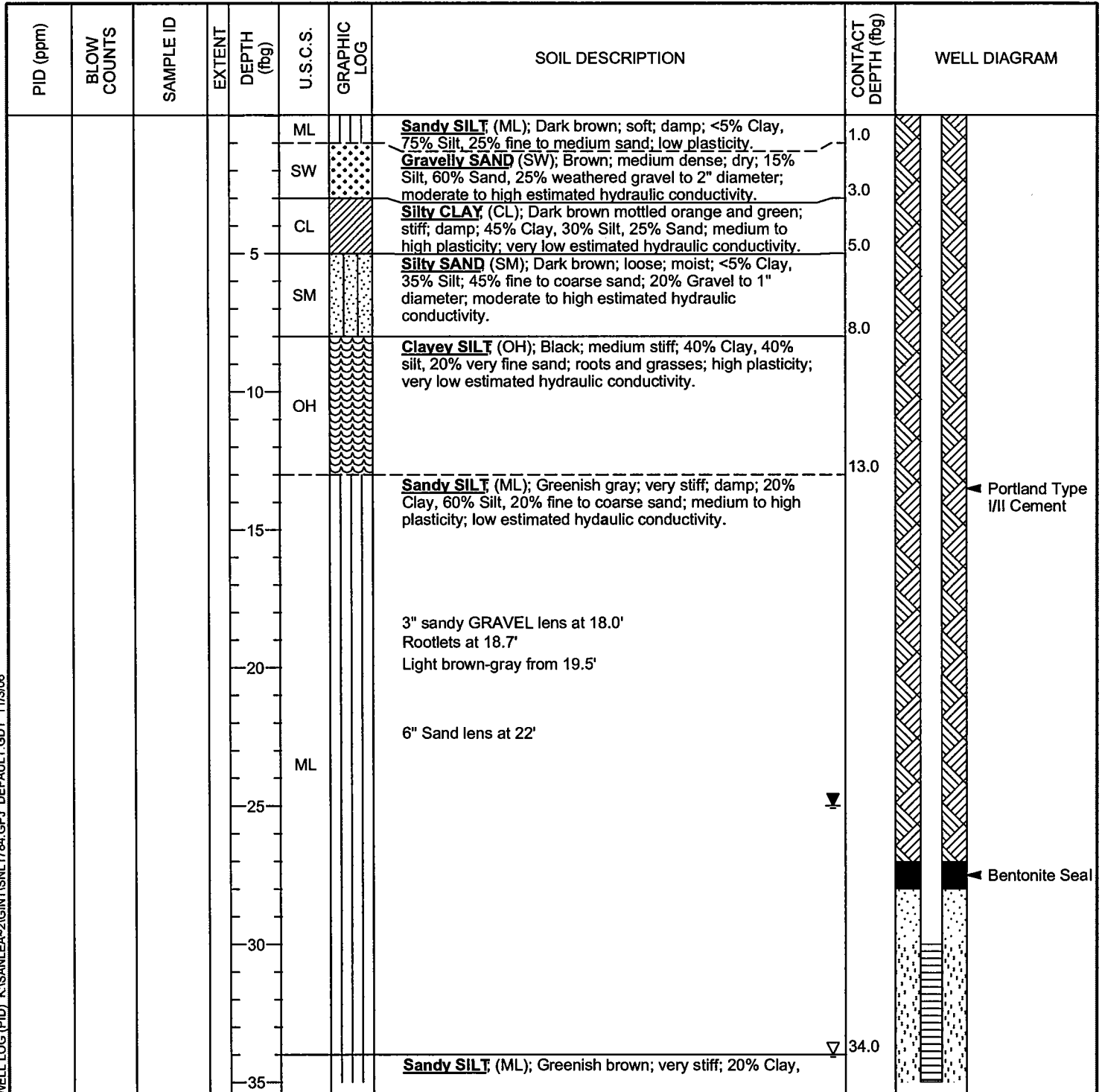
Major Divisions		Graphic	Group Symbol	Typical Description
Coarse-Grained Soils (>50% Sands and/or Gravels)	Gravel and Gravelly Soils		GW	Well-graded gravels, gravel-sand mixtures, little or no fines
			GP	Poorly-graded gravels, gravel-sand mixtures, little or no fines
			GM	Silty gravels, gravel-sand-silt mixtures
			GC	Clayey gravels, gravel-sand-clay mixtures
	Sand and Sandy Soils		SW	Well-graded sands, gravelly sands, little or no fines
			SP	Poorly-graded sands, gravelly sand, little or no fines
SM	Silty sands, sand-silt mixtures			
SC	Clayey sands, sand-clay mixtures			
Fine-Grained Soils (>50% Silts and/or Clays)	Silts and Clays		ML	Inorganic silts, very fine sands, silty or clayey fine sands, clayey silts with slight plasticity
			CL	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays
			OL	Organic silts and organic silty clays of low plasticity
	Silts and Clays		MH	Inorganic silts, micaceous or diatomaceous fine sand or silty soils
			CH	Inorganic clays of high plasticity
			OH	Organic clays of medium to high plasticity, organic silts
Highly Organic Soils			PT	Peat, humus, swamp soils with high organic contents



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 Sonoma, CA 95476
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 Fax: 707-935-6649

BORING/WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	MW-1
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	06-Mar-90
LOCATION	San Leandro, California	DRILLING COMPLETED	06-Mar-90
PROJECT NUMBER	248-0612-008	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Soil Exploration Services	GROUND SURFACE ELEVATION	49.48 ft above msl
DRILLING METHOD	Hollow-stem auger	TOP OF CASING ELEVATION	Not Surveyed
BORING DIAMETER	10"	SCREENED INTERVAL	30 to 45 fbg
LOGGED BY	Karen Sixt	DEPTH TO WATER (First Encountered)	34.0 ft (06-Mar-90) ▽
REVIEWED BY	Richard Weiss; CEG 1112	DEPTH TO WATER (Static)	25.00 ft (08-Mar-90) ▽
REMARKS	Transcribed from original WA log		



WELL LOG (PID) K:\SANLEA-2\GINT\SNL1784.GPJ DEFAULT.GDT 11/3/06

Continued Next Page



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BORING/WELL LOG

CLIENT NAME Shell Oil Products Company (US) BORING/WELL NAME MW-1
 JOB/SITE NAME 1784 150th Avenue DRILLING STARTED 06-Mar-90
 LOCATION San Leandro, California DRILLING COMPLETED 06-Mar-90

Continued from Previous Page

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (ftg)	U.S.C.S.	GRAPHIC LOG	SOIL DESCRIPTION	CONTACT DEPTH (ftg)	WELL DIAGRAM
				40	ML		65% Silt, 15% very fine to medium sand; low to moderate estimated hydraulic conductivity.	45.0	<p>Monterey Sand #3 2"-diam., 0.020" Slotted Schedule 40 PVC</p>
				45					Bottom of Boring @ 45 ft
				50					
				55					
				60					
				65					
				70					
				75					

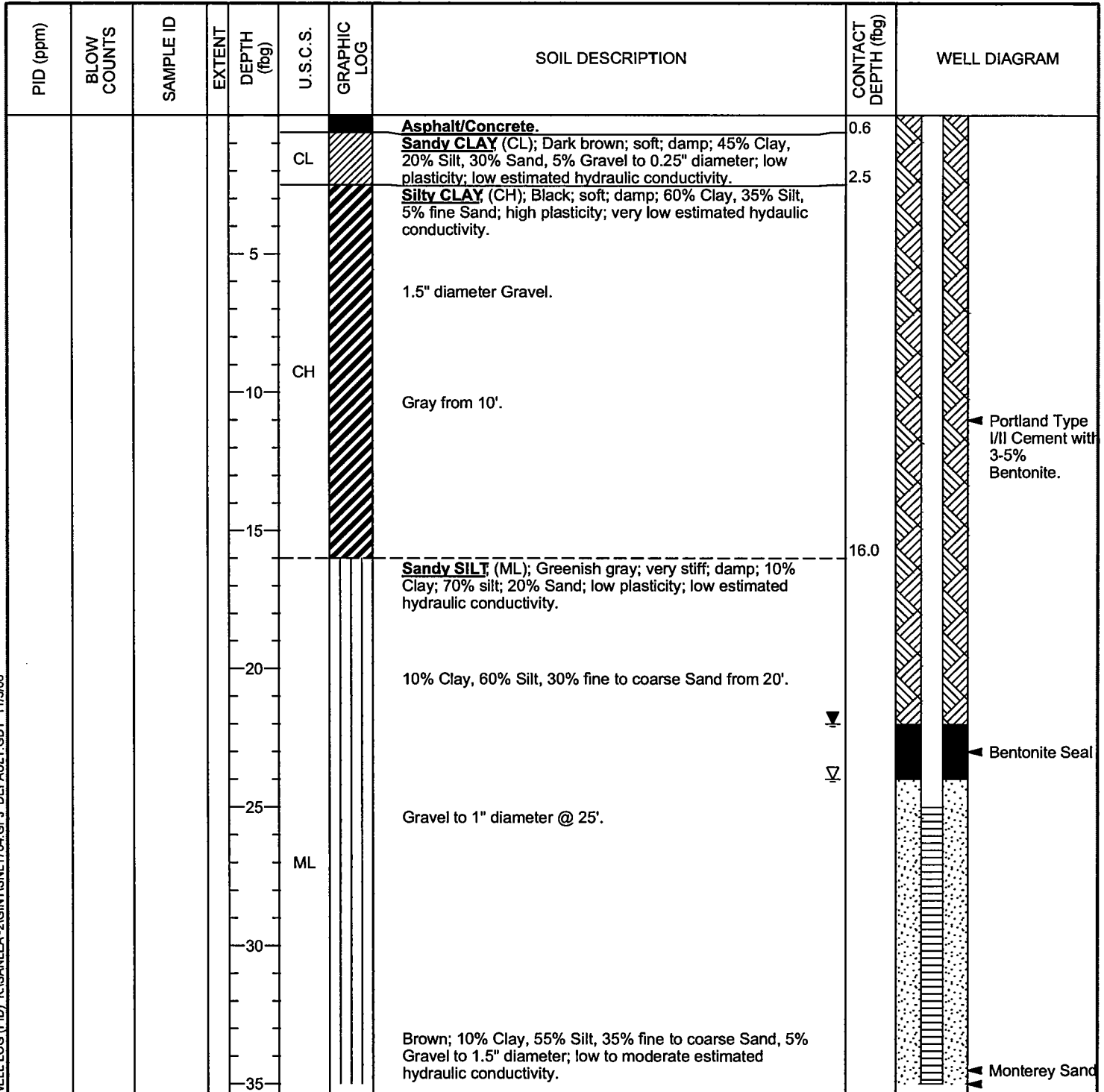
WELL LOG (PID) K:\SANLEA-2\GINT\SNL1784.GPJ DEFAULT.GDT 11/3/06



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BORING/WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	MW-2
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	04-Feb-92
LOCATION	San Leandro, California	DRILLING COMPLETED	04-Feb-92
PROJECT NUMBER	248-0612-008	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Soil Exploration Services	GROUND SURFACE ELEVATION	46.18 ft above msl
DRILLING METHOD	Hollow-stem auger	TOP OF CASING ELEVATION	Not Surveyed
BORING DIAMETER	10"	SCREENED INTERVAL	25 to 45 fbg
LOGGED BY	Tom Fojut	DEPTH TO WATER (First Encountered)	24.0 ft (04-Feb-92) ▾
REVIEWED BY	Joseph P. Theisen; CEG 1645	DEPTH TO WATER (Static)	22.00 ft (13-Feb-92) ▾
REMARKS	Transcribed from original WA log		



WELL LOG (PID) K:\SANLEA-2\GINT\SNL-1784.GPJ DEFAULT.GDT 11/3/06



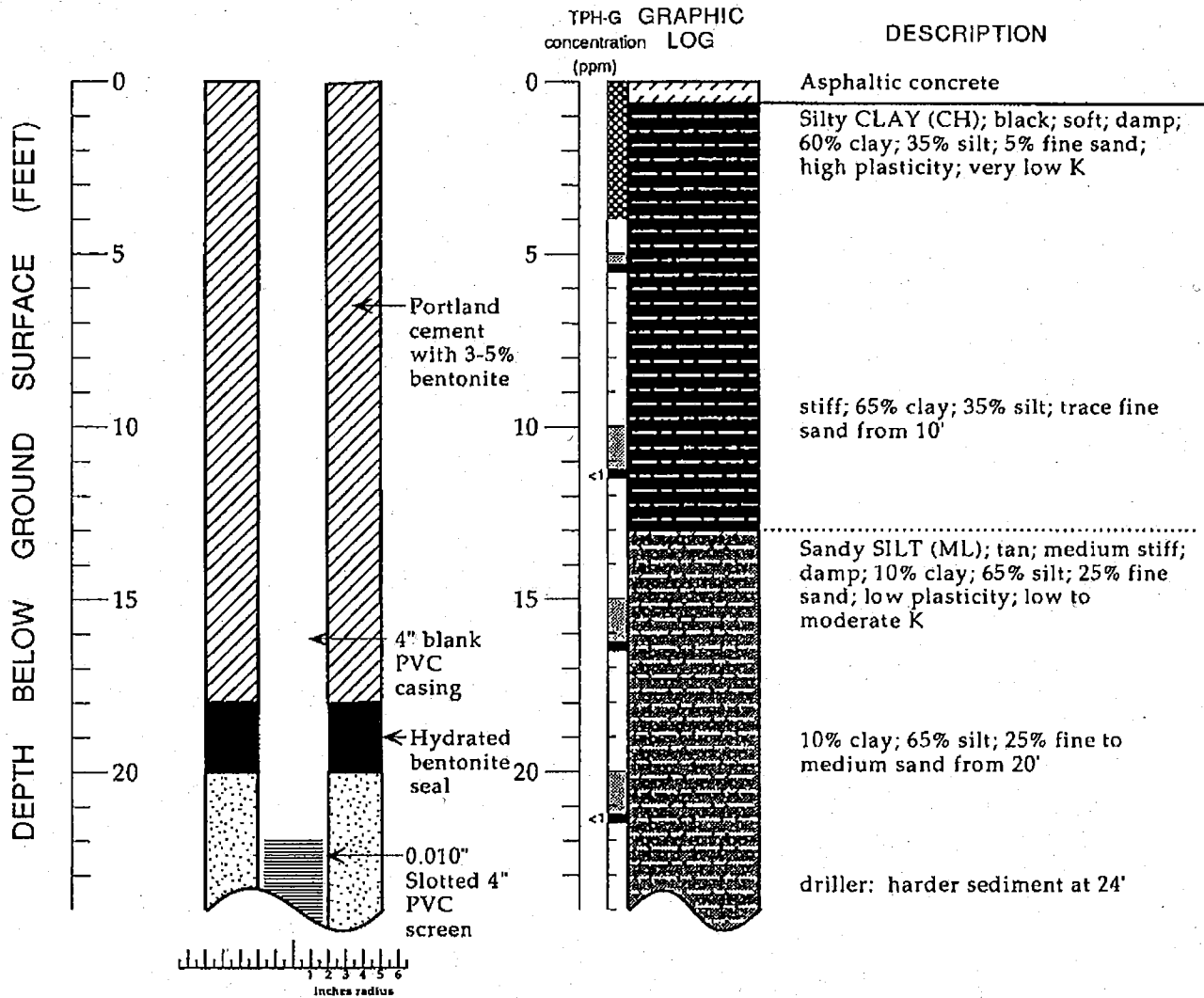
CLIENT NAME Shell Oil Products Company (US) BORING/WELL NAME MW-2
 JOB/SITE NAME 1784 150th Avenue DRILLING STARTED 04-Feb-92
 LOCATION San Leandro, California DRILLING COMPLETED 04-Feb-92

Continued from Previous Page

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (ftg)	U.S.C.S.	GRAPHIC LOG	SOIL DESCRIPTION	CONTACT DEPTH (ftg)	WELL DIAGRAM
				38.0				38.0	# 1/20 4"-diam., 0.010" Slotted Schedule 40 PVC
				40	SM		Silty SAND (SM) ; Brown; dense; wet; 5% Clay, 35% Silt, 45% Sand, 15% Gravel to 1.5" diameter; moderate estimated hydraulic conductivity; Gravel concentrated in layers less than 6" thick.		
				45			5% Clay, 30% Silt, 50% Sand, 15% Gravel to 1.5" diameter from 43'.	45.0	
				50					
				55					
				60					
				65					
				70					
				75					
									Bottom of Boring @ 45 ft

WELL LOG (PID) K:\SANLEA-2\GINT\SNL-1784.GPJ DEFAULT.GDT 11/3/06

WELL MW-3 (BH-C)



EXPLANATION

- Water level during drilling (date)
- Water level (date)
- Contact (dotted where approximate)
- Uncertain contact
- Gradational contact
- Location of recovered drive sample
- Location of drive sample sealed for chemical analysis
- Cutting sample
- K** = Estimated hydraulic conductivity

Logged By: Tom Fojut
 Supervisor: Joseph P. Theisen; CEG 1645
 Drilling Company: Soils Exploration Services, Benicia, CA
 License Number: Lic. #C57-582696
 Driller: Courtney Mossman
 Drilling Method: Hollow-stem auger
 Date Drilled: February 5, 1992
 Well Head Completion: 4" locking well-plug, traffic-rated vault
 Type of Sampler: Split barrel (2" ID)
 Ground Surface Elevation: 52.35 feet above mean sea level
 TPH-G: Total petroleum hydrocarbon as gasoline in soil by modified EPA Method 8015

Boring Log and Well Construction Details - Well MW-3 (BH-C) - Shell Service Station WIC #204-6852-1404 - 1784 150th Avenue, San Leandro, California

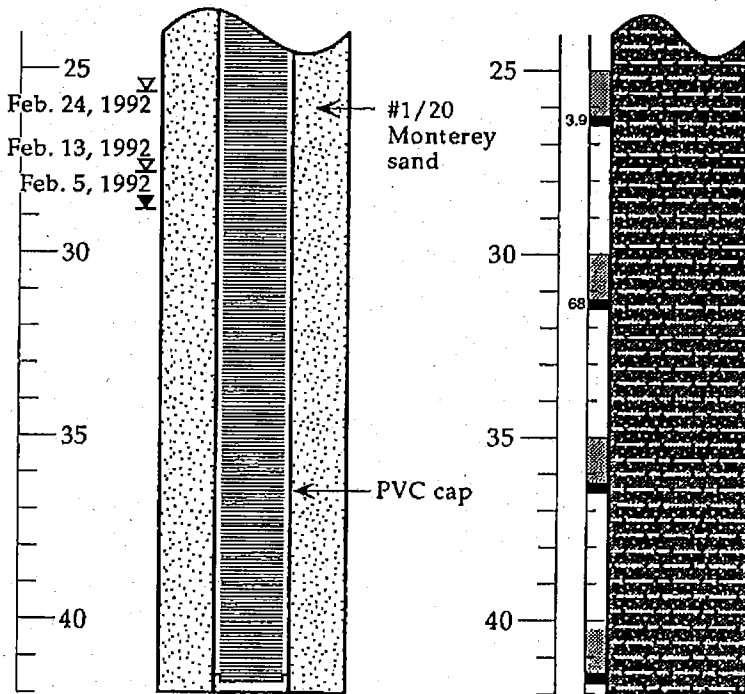


WELL MW-3 (BH-C) (cont.)

TPH-G GRAPHIC
concentration LOG
(ppm)

DESCRIPTION

DEPTH BELOW GROUND SURFACE (FEET)

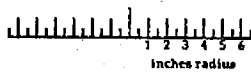


green-gray from 25'

5% clay; 50% silt; 45% medium to coarse sand; moderate K

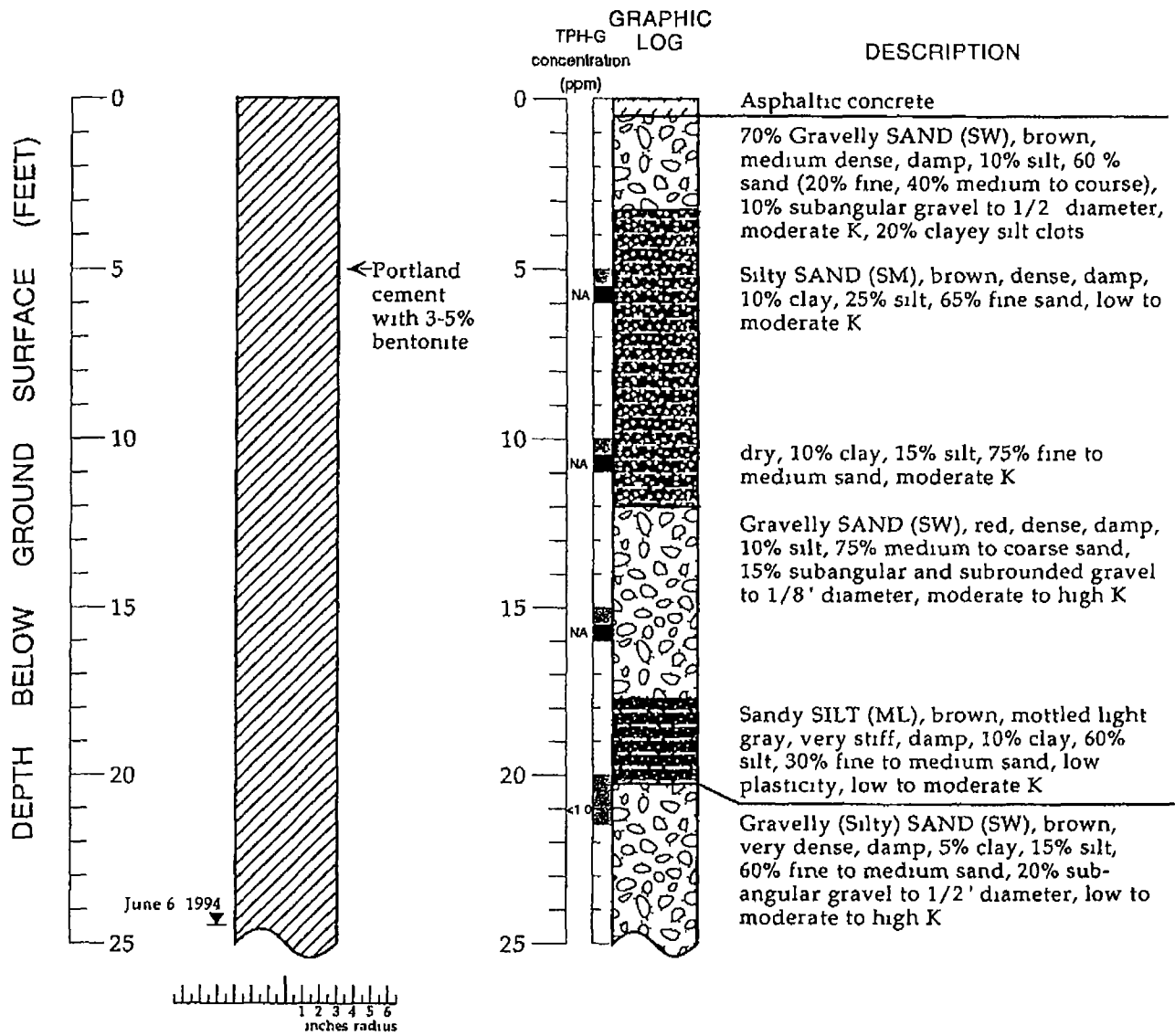
less than 6" thick silty sand lenses from 35'

wet from 36'



Boring Log and Well Construction Details - Well MW-3 (BH-C) - Shell Service Station WIC #204-6852-1404 - 1784 150th Avenue, San Leandro, California

SOIL BORING BH-1



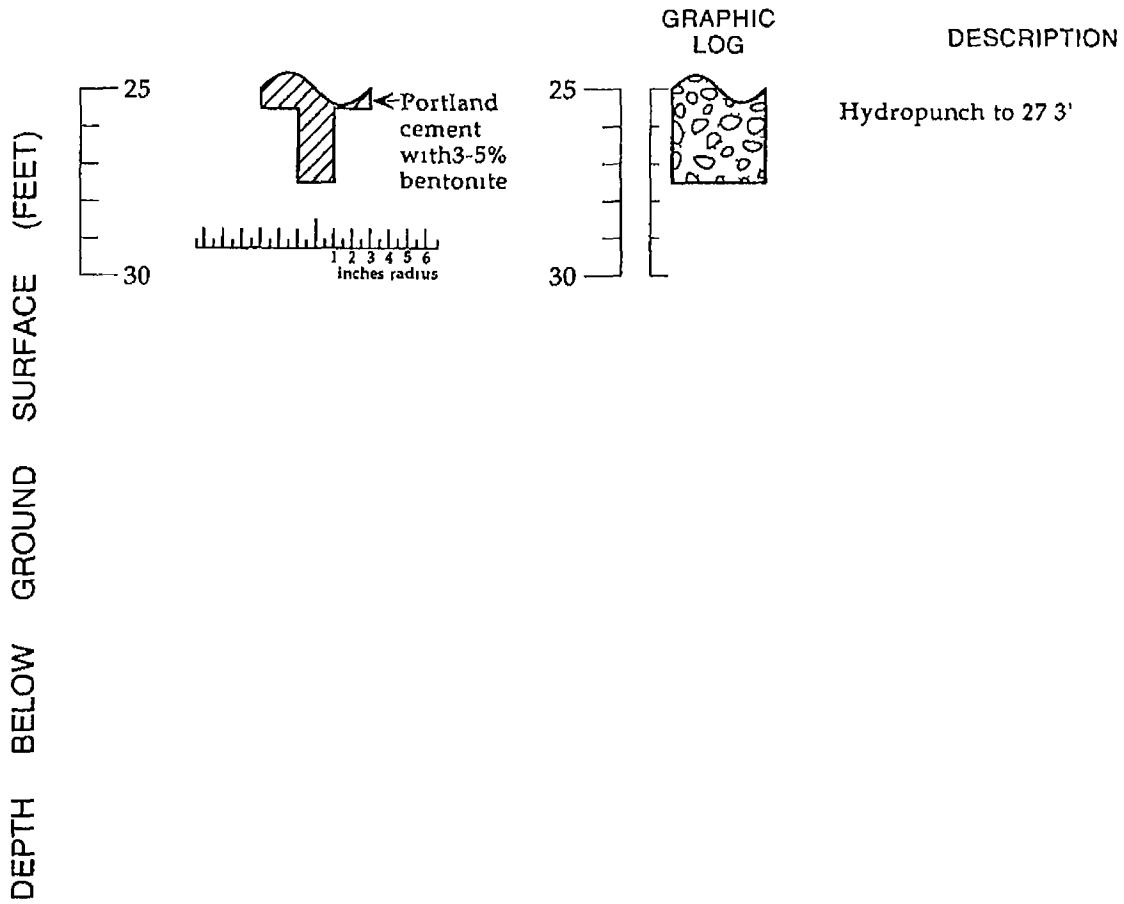
EXPLANATION

- ∇ Water level during drilling (date)
- ∇ Water level (date)
- Contact (dotted where approximate)
- 7-7- Uncertain contact
- //// Gradational contact
- Location of recovered drive sample
- Location of drive sample sealed for chemical analysis
- Cutting sample
- K = Estimated hydraulic conductivity
- NA = Not analyzed

Logged By Jonathan Weingast
 Supervisor James W Carmody, CEG 1576
 Drilling Company Gregg Drilling, Pacheco, CA
 License Number C57-485165
 Driller Mike Braman
 Drilling Method Hollow-stem auger 6"
 Date Drilled June 6, 1994
 Well Head Completion N/A
 Type of Sampler Split spoon (2' ID)
 TPH-G Total petroleum hydrocarbon as gasoline in soil by modified EPA Method 8015

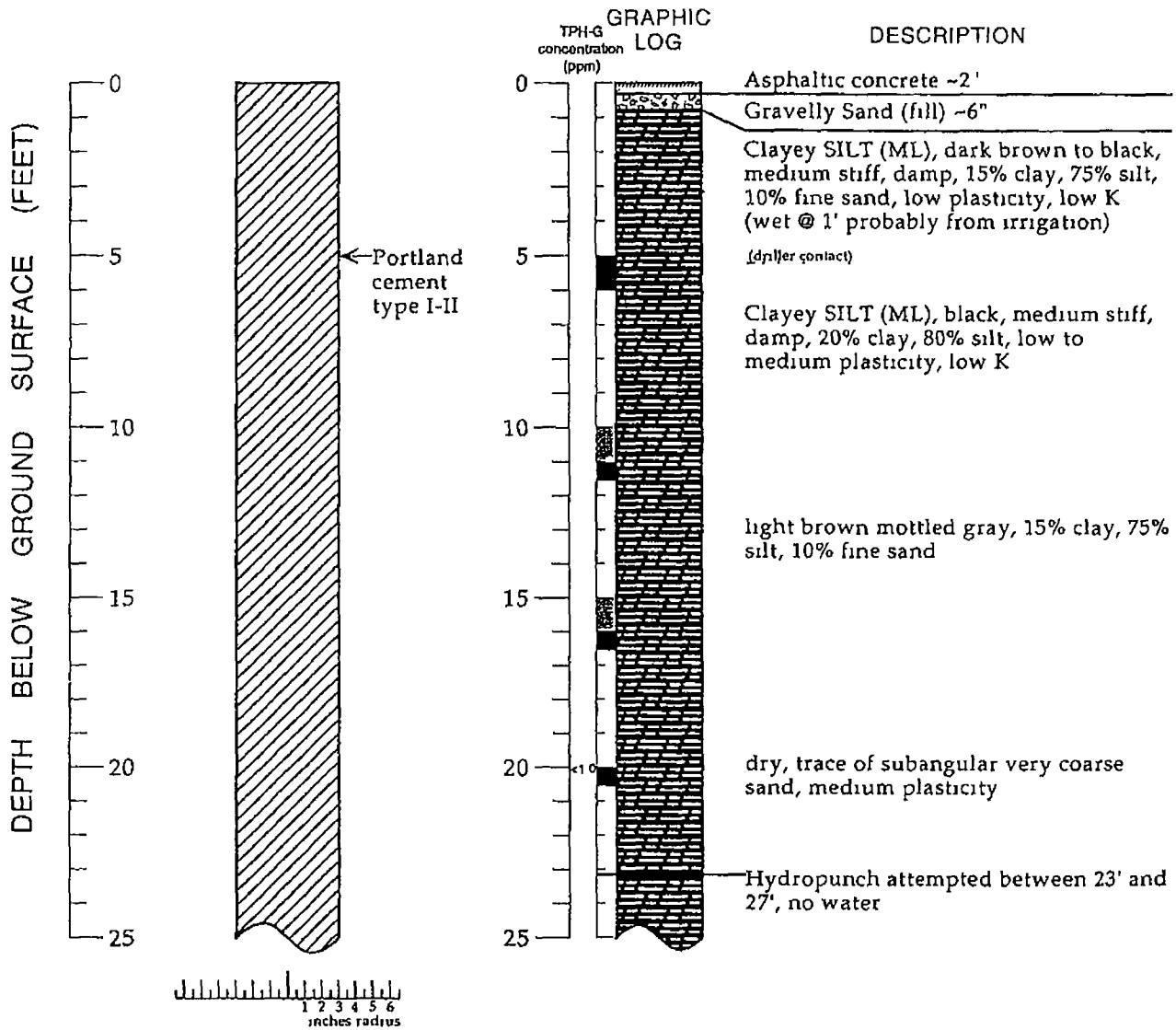
Boring Log Construction Details - BH-1 - Shell Service Station WIC# 204-6852-1404, 1784 150th Avenue, San Leandro, California

SOIL BORING BH-1 (cont)



Boring Log Construction Details - BH-1 - Shell Service Station WIC# 204-6852-1404, 1784 150th Avenue, San Leandro, California

SOIL BORING BH-2

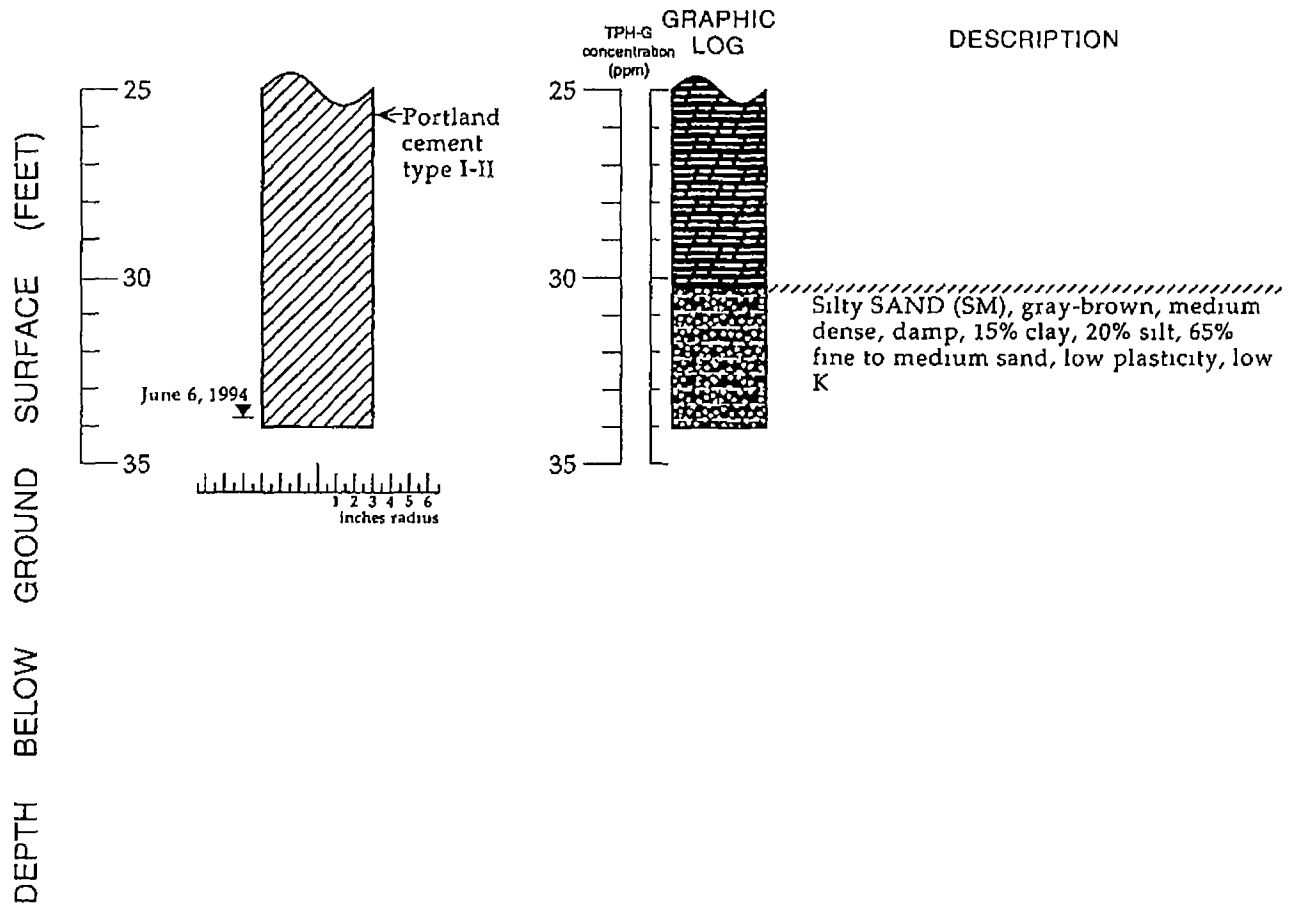


EXPLANATION

<ul style="list-style-type: none"> ▼ Water level during drilling (date) ▽ Water level (date) — Contact (dotted where approximate) - ? - ? - Uncertain contact //// Gradational contact ▨ Location of recovered drive sample ■ Location of drive sample sealed for chemical analysis ▩ Cutting sample K = Estimated hydraulic conductivity 	<ul style="list-style-type: none"> Logged By Jonathan Weingast Supervisor James W Carmody, CEG 1576 Drilling Company Gregg Drilling, Pacheco, CA License Number C57-485165 Driller Mike Braman, Rich Nessinger Drilling Method Hollow-stem auger 6" Date Drilled June 6, 1994 Well Head Completion N/A Type of Sampler Split spoon (2" ID) TPH-G Total petroleum hydrocarbon as gasoline in soil by modified EPA Method 8015
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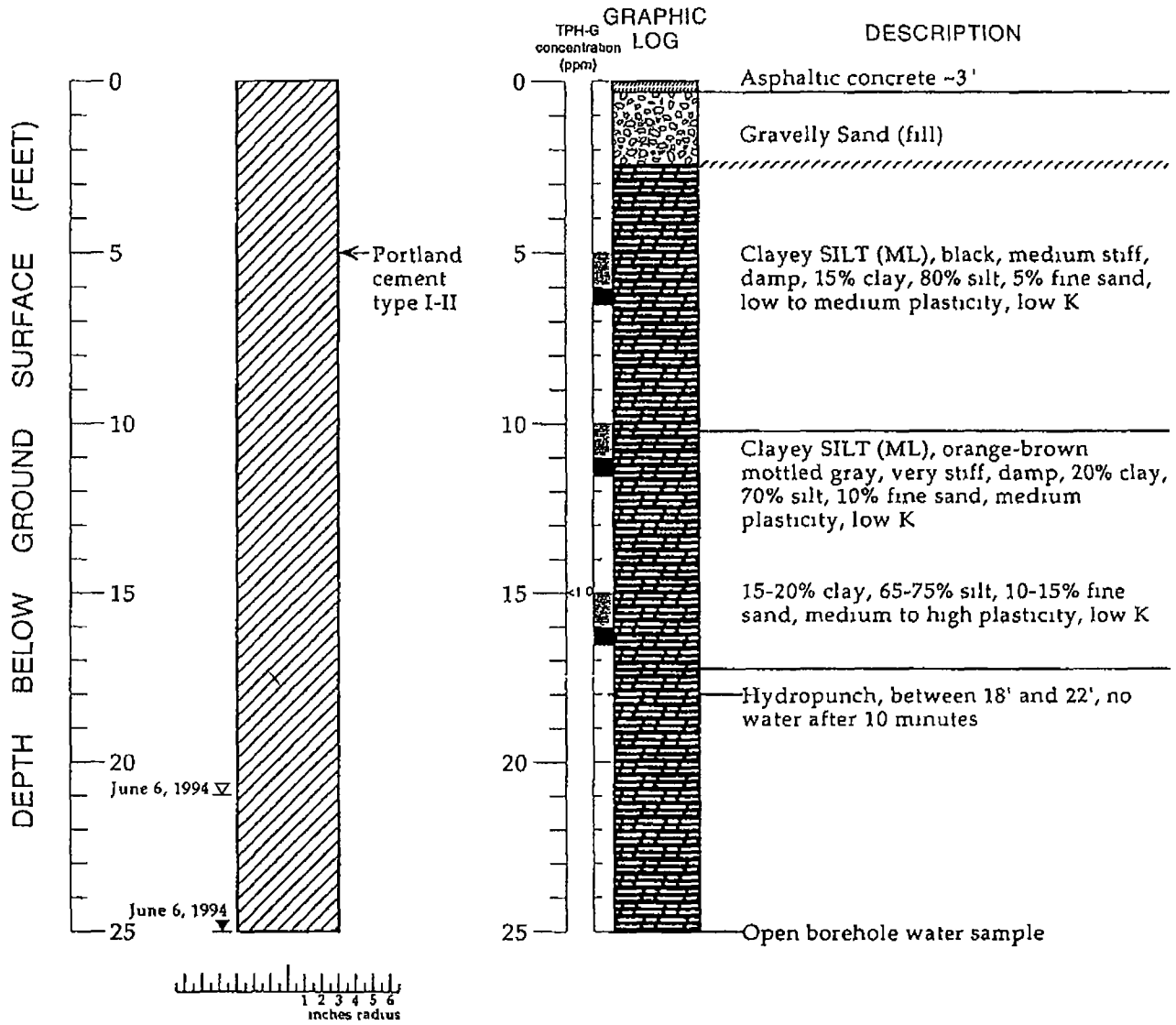
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SOIL BORING BH-2 (cont.)



Boring Log Construction Details - BH-2 - Shell Service Station WIC# 204-6852-1404, 1784 150th Avenue, San Leandro, California

SOIL BORING BH-3

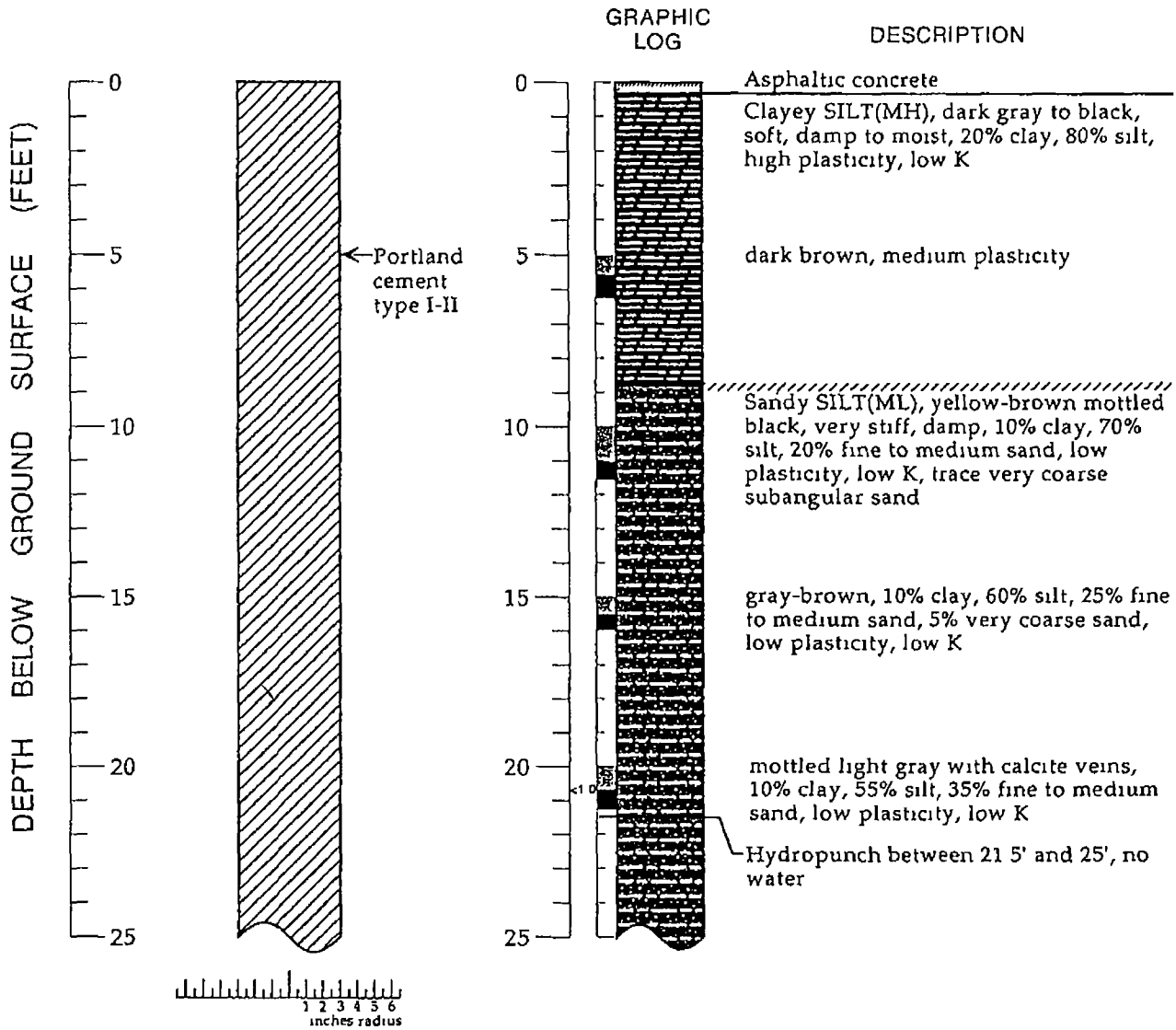


EXPLANATION

▽	Water level during drilling (date)	Logged By	Jonathan Weingast
▽	Water level (date)	Supervisor	James W Carmody, CEG 1576
—	Contact (dotted where approximate)	Drilling Company	Gregg Drilling, Pacheco, CA
- · - · -	Uncertain contact	License Number	C57-485165
////	Gradational contact	Driller	Mike Braman, Rich Nessinger
■	Location of recovered drive sample	Drilling Method	Hollow-stem auger 6'
■	Location of drive sample sealed for chemical analysis	Date Drilled	June 6, 1994
■	Cutting sample	Well Head Completion	N/A
K =	Estimated hydraulic conductivity	Type of Sampler	Split spoon (2" ID)
		TPH-G	Total petroleum hydrocarbon as gasoline in soil by modified EPA Method 8015

Boring Log Construction Details - BH-3 - Shell Service Station WIC# 204-6852 1404, 1784 150th Avenue, San Leandro, California

SOIL BORING BH-4



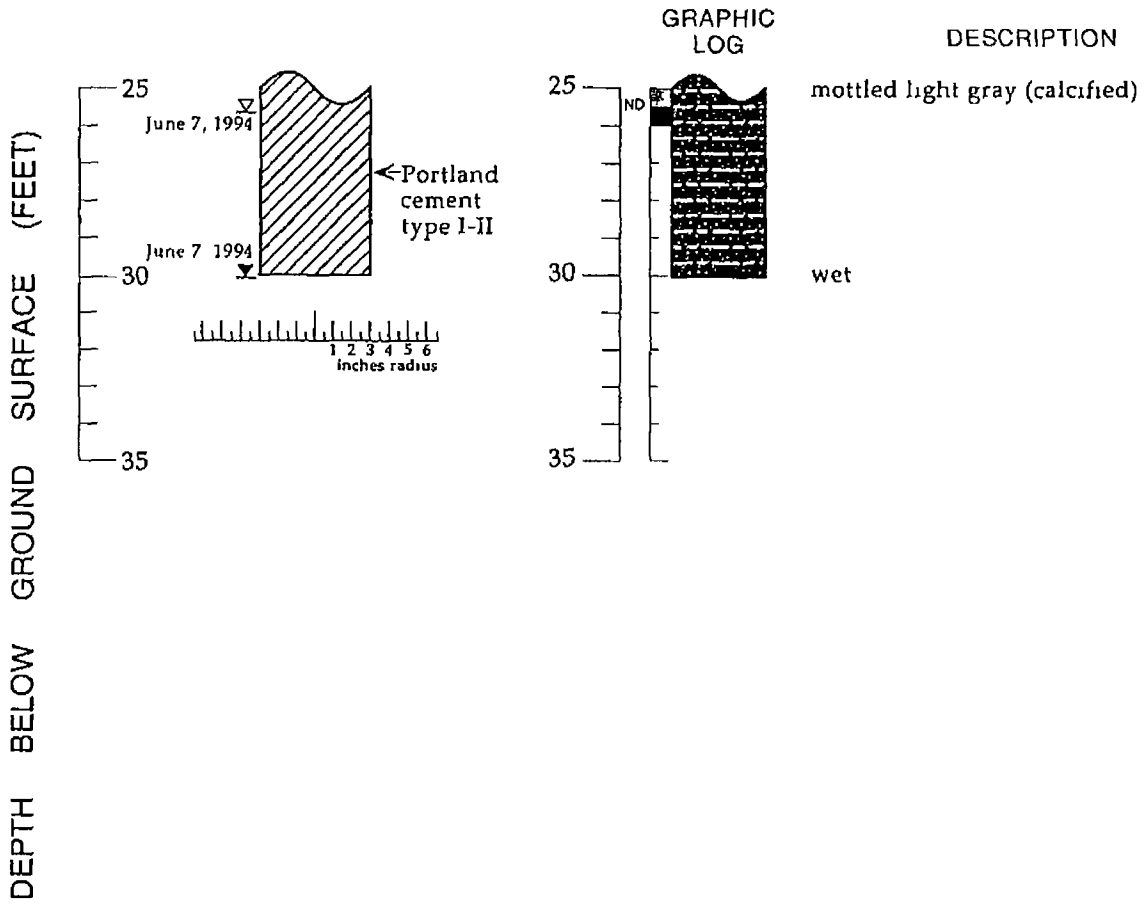
EXPLANATION

- ⊗ Water level during drilling (date)
- ⊘ Water level (date)
- Contact (dotted where approximate)
- ?-?-? Uncertain contact
- //// Gradational contact
- ▨ Location of recovered drive sample
- Location of drive sample sealed for chemical analysis
- ▩ Cutting sample
- K = Estimated hydraulic conductivity

Logged By Jonathan Weingast
 Supervisor James W Carmody, CEG 1576
 Drilling Company Gregg Drilling, Pacheco, CA
 License Number C57-485165
 Driller Mike Braman, Rich Nessinger
 Drilling Method Hollow-stem auger
 Date Drilled June 7, 1994
 Well Head Completion N/A
 Type of Sampler Split spoon (2' ID)
 TPH-G Total petroleum hydrocarbon as gasoline in soil by modified EPA Method 8015

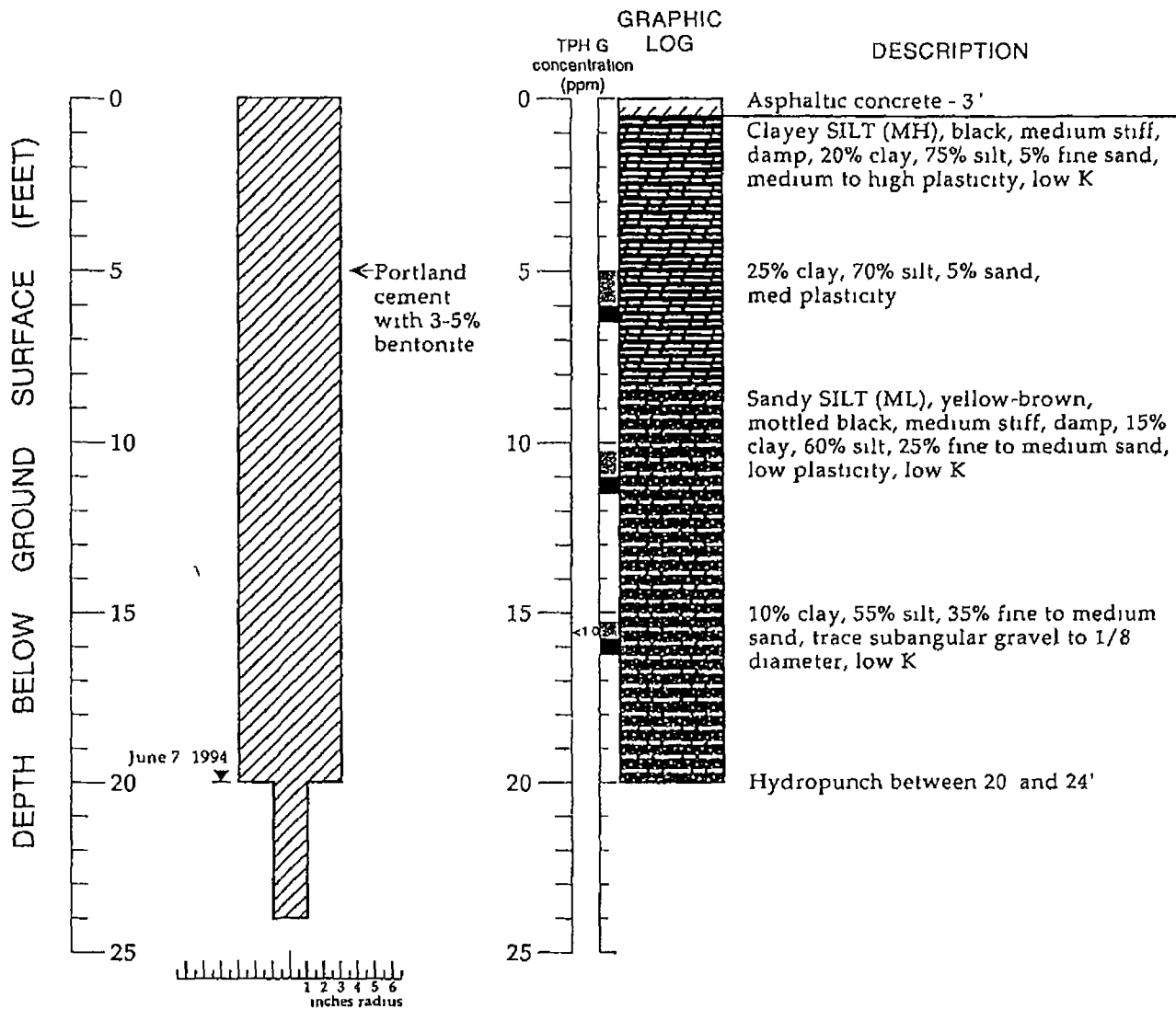
Boring Log Construction Details - BH-4 - Shell Service Station WIC# 204-6852-1404, 1784 150th Avenue, San Leandro, California

SOIL BORING BH-4 (cont.)



Boring Log Construction Details - BH-4 - Shell Service Station WIC# 204-6852-1404, 1784 150th Avenue, San Leandro, California

SOIL BORING BH-5



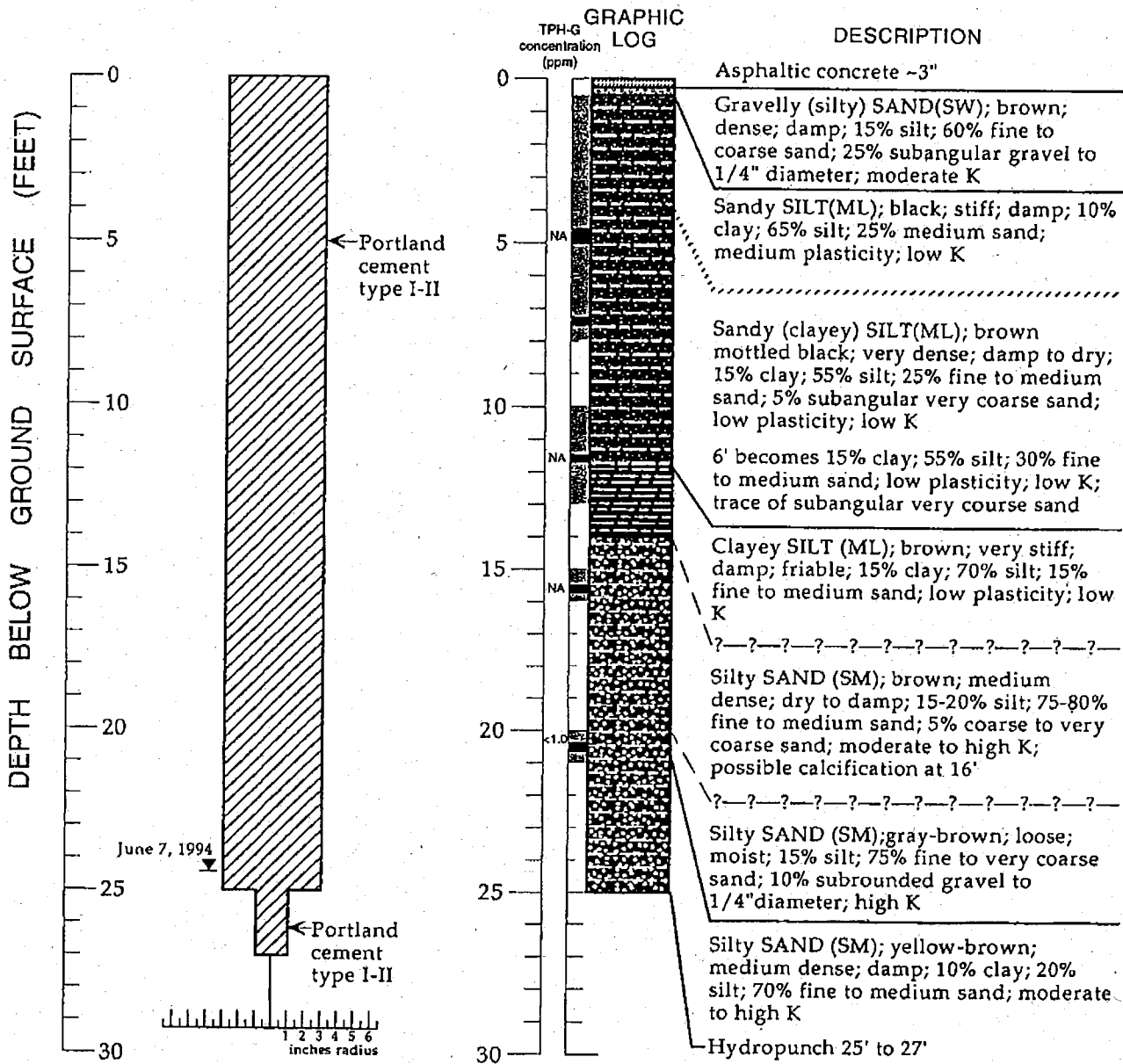
EXPLANATION

- ▼ Water level during drilling (date)
- ▽ Water level (date)
- Contact (dotted where approximate)
- · - · - Uncertain contact
- //// Gradational contact
- Location of recovered drive sample
- Location of drive sample sealed for chemical analysis
- Cutting sample
- K = Estimated hydraulic conductivity

Logged By Jonathan Weingast
 Supervisor James W Carmody, CEG 1576
 Drilling Company Gregg Drilling, Pacheco, CA
 License Number C57-485165
 Driller Mike Braman
 Drilling Method Hollow-stem auger 6"
 Date Drilled June 7, 1994
 Well Head Completion N/A
 Type of Sampler Split spoon (2' ID)
 TPH-G Total Petroleum Hydrocarbons as gasoline in soil by modified EPA Method 8015

Boring Log Construction Details - BH 5 - Shell Service Station WIC# 204-6852-1404, 1784 150th Avenue, San Leandro, California

SOIL BORING BH-6



EXPLANATION

- ▼ Water level during drilling (date)
- ▽ Water level (date)
- Contact (dotted where approximate)
- ?-?-? Uncertain contact
- //// Gradational contact
- ▒ Location of recovered drive sample
- Location of drive sample sealed for chemical analysis
- ▤ Cutting sample
- K = Estimated hydraulic conductivity
- NA = Not analyzed

Logged By: Jonathan Weingast
 Supervisor: James W. Carmody; CEG 1576
 Drilling Company: Gregg Drilling, Pacheco, CA
 License Number: C57-485165
 Driller: Mike Braman, Rich Nessinger
 Drilling Method: Hollow-stem auger 6"
 Date Drilled: June 7, 1994
 Well Head Completion: N/A
 Type of Sampler: Continuous core
 TPH-G: Total petroleum hydrocarbon as gasoline in soil by modified EPA Method 8015

Boring Log Construction Details - BH-6 - Shell Service Station WIC# 204-6852-1404, 1784 150th Avenue, San Leandro, California



Conestoga-Rovers & Associates
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BORING / WELL LOG

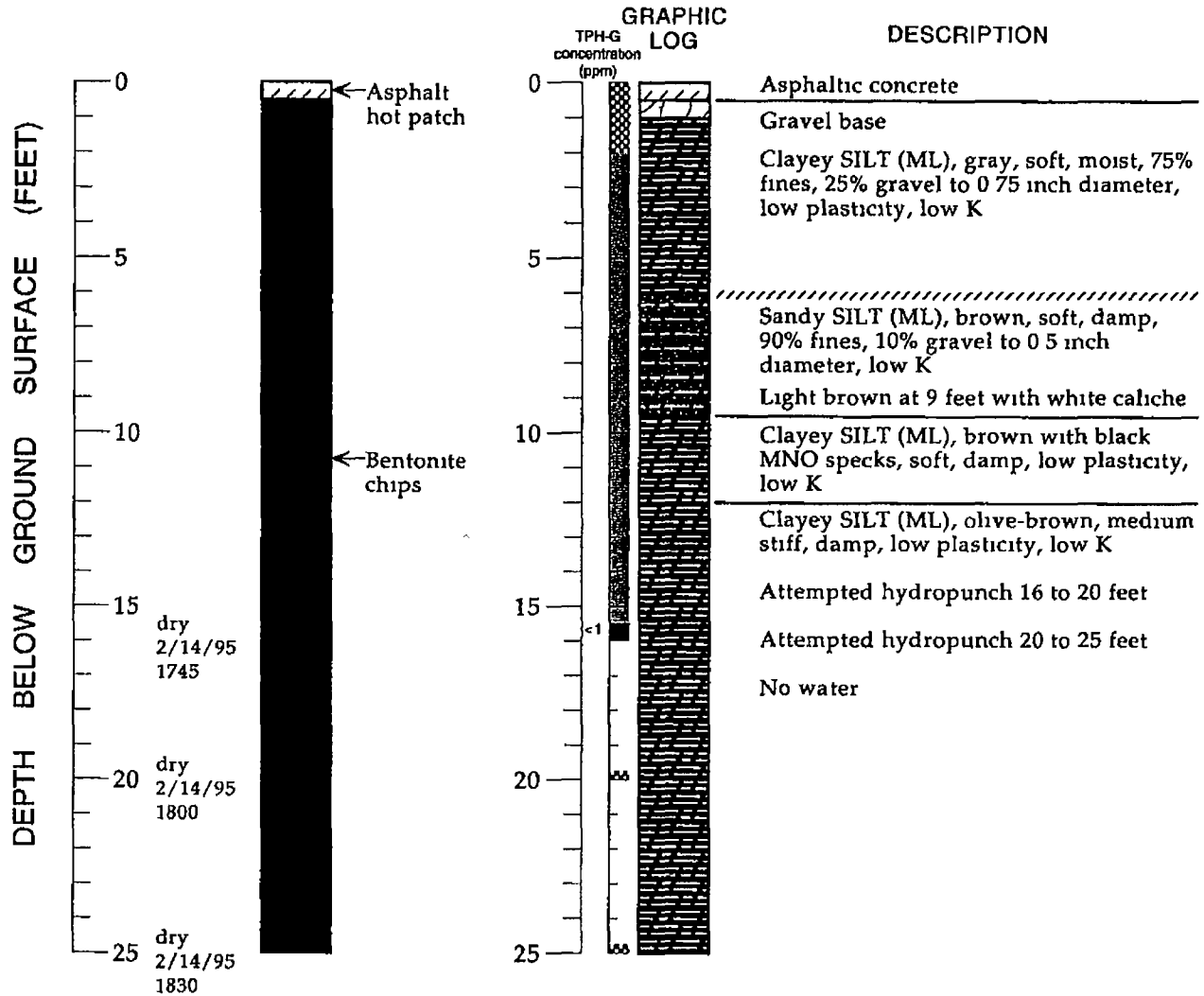
CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	BH-7
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	14-Feb-95
LOCATION	San Leandro, California	DRILLING COMPLETED	14-Feb-95
PROJECT NUMBER	240612	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Vironex	GROUND SURFACE ELEVATION	40.00 ft above msl
DRILLING METHOD	Hydraulic push	TOP OF CASING ELEVATION	NA
BORING DIAMETER	3"	SCREENED INTERVALS	NA
LOGGED BY	Thomas Howard	DEPTH TO WATER (First Encountered)	17.00 fbg
REVIEWED BY	James W. Carmody; CEG 1576	DEPTH TO WATER (Static)	NA
REMARKS	Transcribed from original WA log		

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
							Asphalt and Concrete.	0.6	
							Baserock/Gravel	1.0	
					ML		Sandy, Clayey SILT (ML); Dark gray; medium stiff; damp; 80% fines, 20% very fine to medium Sand; low plasticity; low estimated hydraulic conductivity.		
				5				5.0	
					ML		Clayey SILT (ML); Dark gray; medium stiff; damp, 90% fines, 10% fine Sand; low plasticity; low estimated hydraulic conductivity.		
				10			Light brown at 10' with black specks and white caliche.		
					GM		Silty Sandy GRAVEL (GM); Yellowish brown; medium dense; damp; 20% fines, 30% fine to coarse Sand, 50% sub-angular to sub-rounded Gravel to 0.5" diameter; moderate estimated hydraulic conductivity.	13.0	
					ML		Clayey SILT (ML); Light brown; medium stiff; damp to dry; 90% fines, 10% fine Sand; low plasticity; low estimated hydraulic conductivity.	14.0	
				15				15.0	
					GM		Silty GRAVEL (GM); Light greenish brown; medium dense to very dense; damp to wet; moderate estimated hydraulic conductivity. Attempt hydropunch sample at 17 to 20 fbg, collect water sample.		
				20				20.0	

WELL LOG (PID) \SHELL16-CHARS2406-240612-124CBEB-1NSL-1784.GPJ DEFAULT.GDT 6/10/09

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BH-8

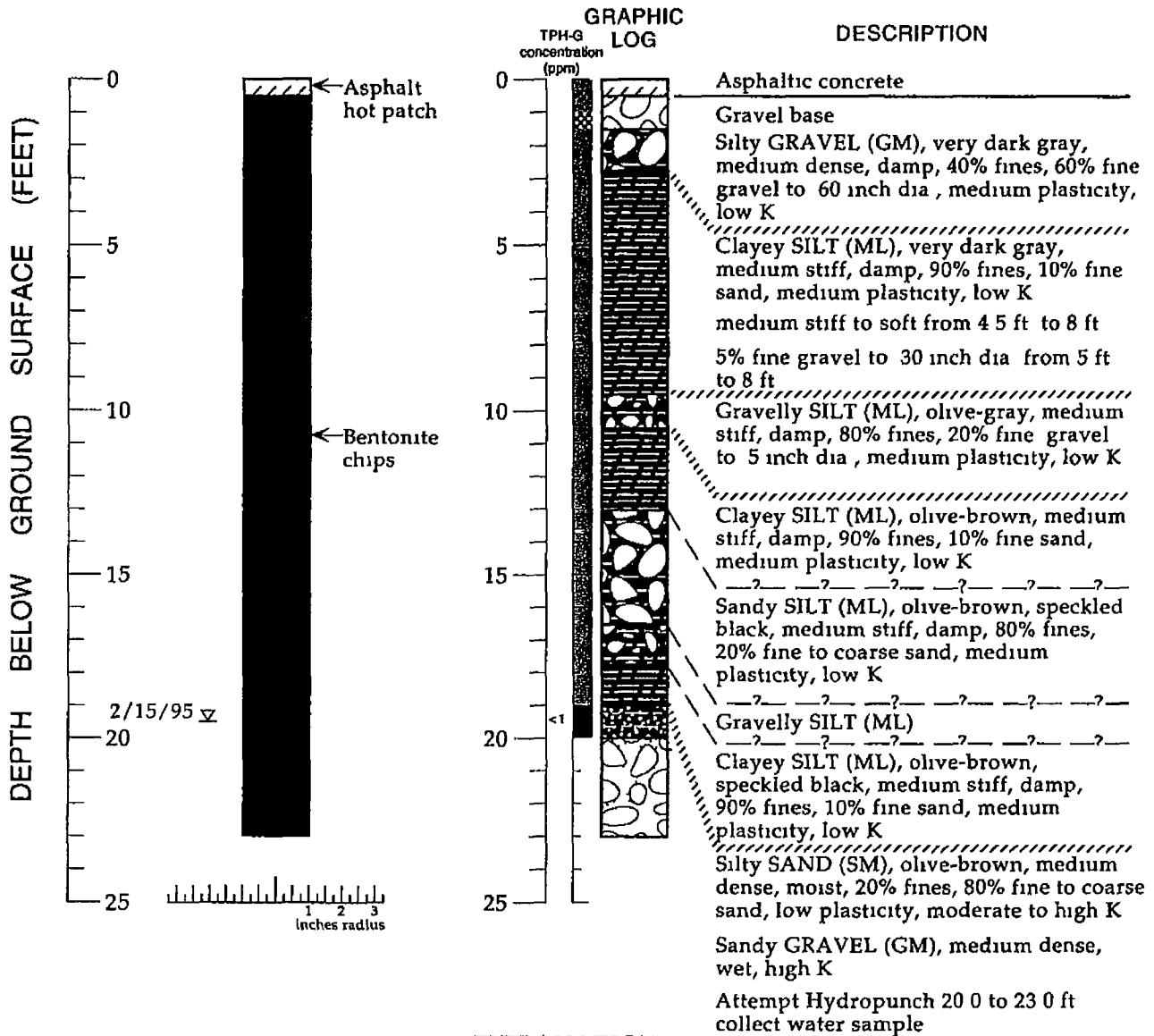


EXPLANATION

▽	Water level during drilling (date)	Logged By	Faith M. Daverin
▽	Water level (date)	Supervisor	James W. Carmody, CEG 1576
—	Contact (dotted where approximate)	Drilling Company	Vironix, Foster City, CA
—?—?	Uncertain contact	License Number	C57-606481
////	Gradational contact	Driller	Tom VanHuizen
▒	Location of recovered drive sample	Drilling Method	GeoProbe
■	Location of drive sample sealed for chemical analysis	Date Drilled	February 14, 1995
⊗	Cutting sample	Well Head Completion	N/A
K =	Estimated hydraulic conductivity	Type of Sampler	California continuous soil and ground water sampler
	Ground Surface Elevation		-40 feet above mean sea level
	TPH-G		Total petroleum hydrocarbon as gasoline in soil by modified EPA Method 8015

Boring Log and Well Construction Details - BH-8 - Shell Service Station WIC #204-6852-1404, 150th Avenue, San Leandro, California

BH-9



EXPLANATION

- ∇ Water level during drilling (date)
- ∇ Water level (date)
- Contact (dotted where approximate)
- ?-?-? Uncertain contact
- //// Gradational contact
- Location of recovered drive sample
- Location of drive sample sealed for chemical analysis
- Cutting sample
- K = Estimated hydraulic conductivity

Logged By Thomas Howard
 Supervisor James W Carmody, CEG 1576
 Drilling Company Vironix, Foster City, CA
 License Number C57-606481
 Driller Tom VanHuizen
 Drilling Method GeoProbe
 Date Drilled February 15, 1995
 Well Head Completion N/A
 Type of Sampler California continuous soil and water sampler
 Ground Surface Elevation ~40 feet above mean sea level
 TPH-G Total petroleum hydrocarbon as gasoline in soil by modified EPA Method 8015

Boring Log and Well Construction Details - BH-9 - Shell Service Station WIC #204-6852-1404, 150th Avenue, San Leandro, California



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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	MW-4
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	03-Mar-95
LOCATION	San Leandro, California	DRILLING COMPLETED	03-Mar-95
PROJECT NUMBER	240612	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	40.08 ft above msl
DRILLING METHOD	Hollow-stem auger	TOP OF CASING ELEVATION	NA
BORING DIAMETER	10"	SCREENED INTERVALS	5 to 17 fbg
LOGGED BY	Faith Daverin	DEPTH TO WATER (First Encountered)	22.00 fbg (03-Mar-95) ▽
REVIEWED BY	James W. Carmody; CEG 1576	DEPTH TO WATER (Static)	9.5 fbg (24-Mar-95) ▽
REMARKS	Transcribed from original WA log		

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
						■	Asphalt/Concrete	0.6	<p>Portland Type I/II Cement with 3-5% Bentonite.</p> <p>Bentonite Seal</p>
						○ ○ ○	Gravel Base	1.6	
				5			Clayey SILT; (ML); Very dark gray; medium stiff; damp; 90% fines, 10% fine sand; low to medium plasticity; low estimated hydraulic conductivity.		<p>2" diam., 0.010" Slotted Schedule 40 PVC</p>
				10	ML				
				15			Moist Clayey SILT; (ML); Brown, speckled black; slightly dense; very wet; 75% fines, 25% fine to coarse sand; low plasticity; low estimated hydraulic conductivity.	14.0	
				18.0	ML		Clayey SILT; (ML); Brown, speckled black; medium stiff; damp; 80% fines, 20% fine to coarse sand, coarsens downward; low plasticity; low estimated hydraulic conductivity.	18.0	<p>Monterey Sand # 1/20</p>
				20					

WELL LOG (PID) I:\SHELL\16-CHARS\2406-1240612-124CBE8-1\SNL1784.GPJ DEFAULT.GDT 6/10/09

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BORING / WELL LOG

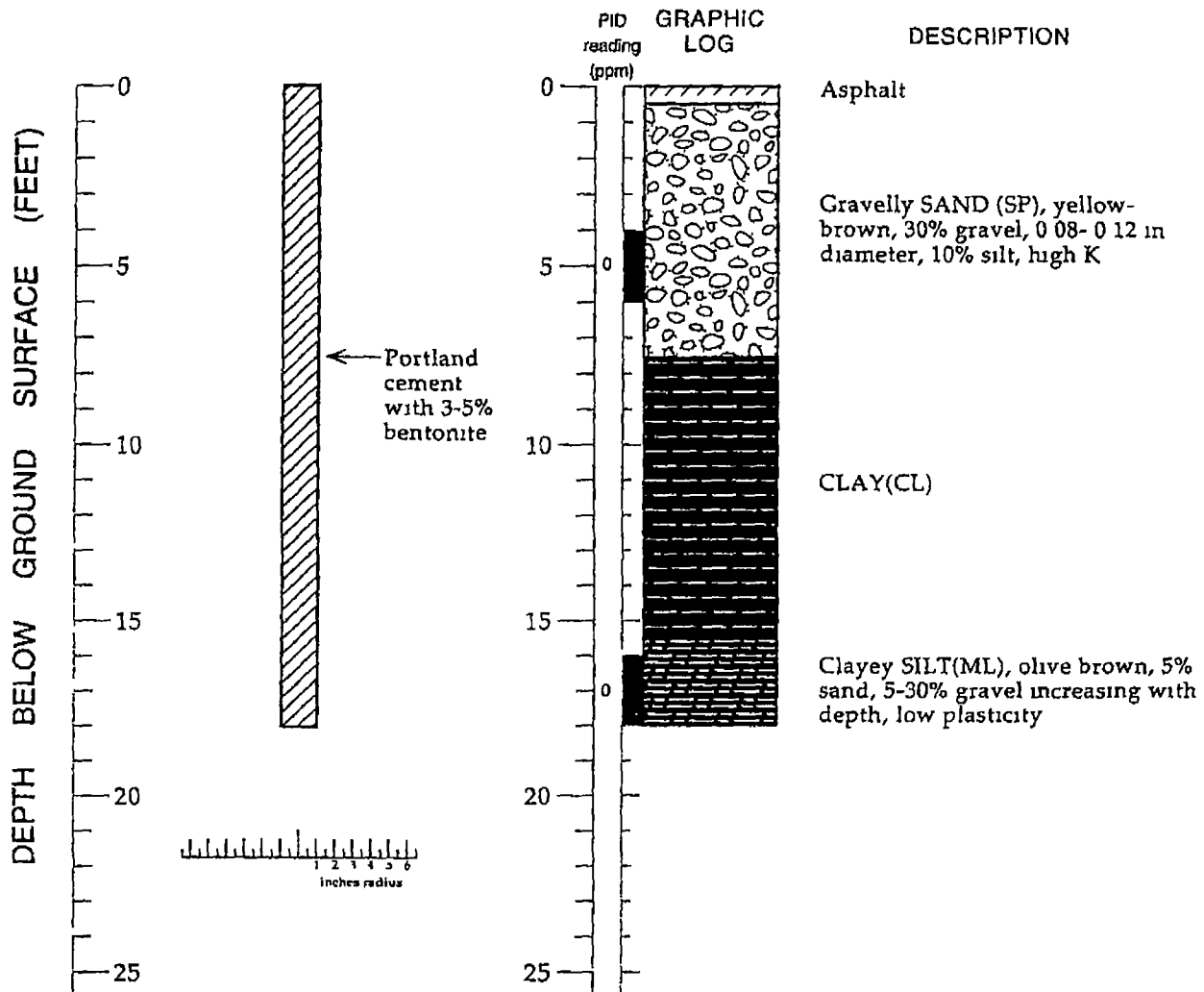
CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	MW-4
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	03-Mar-95
LOCATION	San Leandro, California	DRILLING COMPLETED	03-Mar-95

Continued from Previous Page

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (ftg)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (ftg)	WELL DIAGRAM
					ML				<p>6/6/94</p> <p>Bottom of Boring @ 30 ftg</p>
				23.0	GM		Sandy GRAVEL ; (GM); Brown; medium dense; very moist; 25% fines, 25% medium to coarse Sand, 50% Gravel to 0.25" diameter; moderate to high estimated hydraulic conductivity.	23.0	
				25.5	ML		Sandy SILT (ML); Light brown speckled black; slightly dense; damp to moist; 70% fines, 30% fine to medium Sand; low plasticity; low estimated hydraulic conductivity.	25.5	
				27.0	GM		Sandy GRAVEL ; (GM); Brown; medium dense; very moist; 10% fines, 90% fine to coarse Sand; high estimated hydraulic conductivity.	27.0	
				29.0	SM		Silty SAND ; (SM); Light brown; loose; very wet; 30% Silt, 70% very fine to fine Sand; low plasticity; moderate estimated hydraulic conductivity.	29.0	
				30.0				30.0	

WELL LOG (PID) I:\SHELL16-CHARS\2406-1240612-124CBE8-1\SNL1784.GPJ DEFAULT.GDT 6/10/09

LITHOLOGIC LOG SVS-3



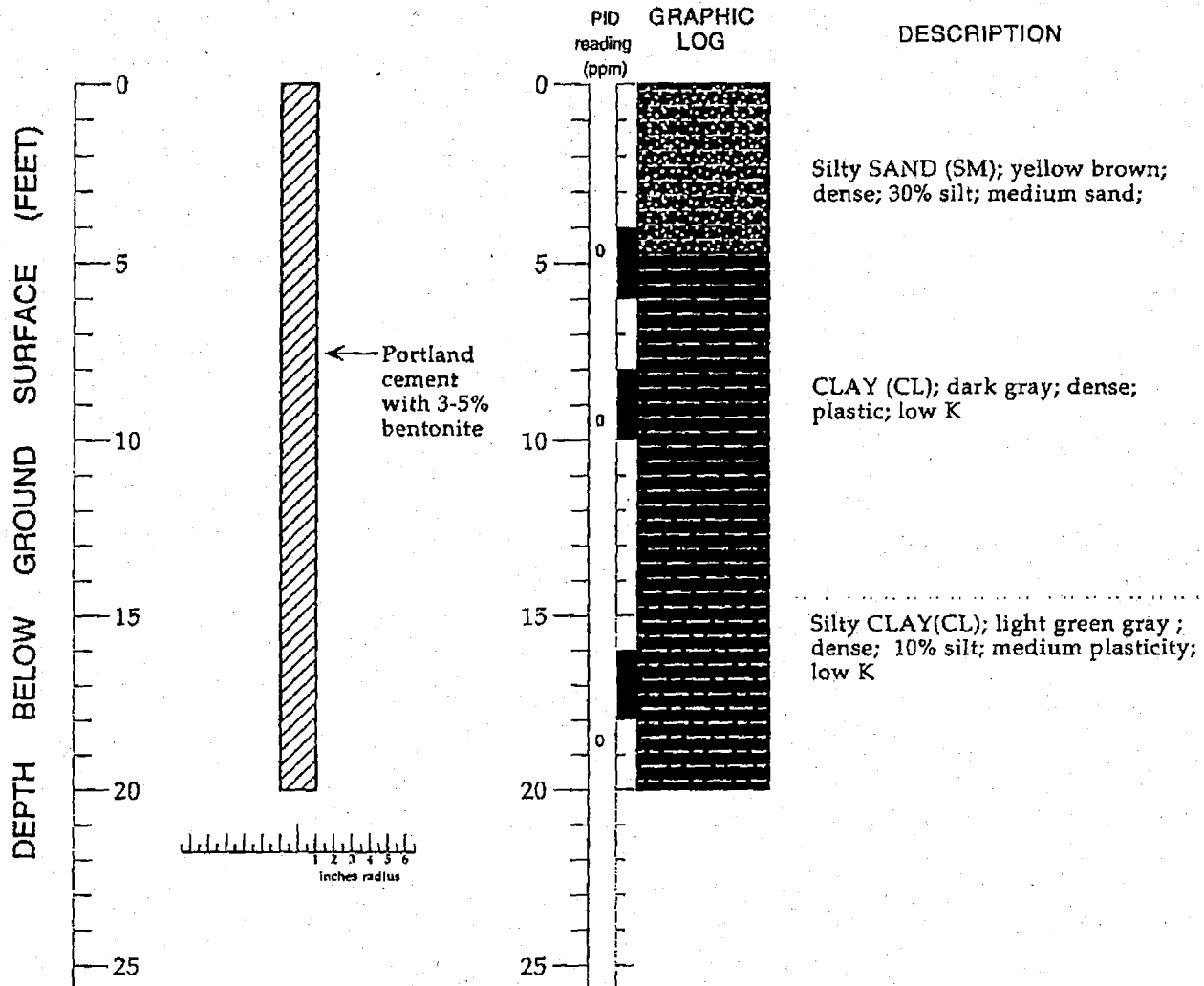
EXPLANATION

- ☒ Water level during drilling (date)
- ☒ Water level (date)
- · — Contact (dotted where approximate)
- ? - ? - Uncertain contact
- //// Gradational contact
- ▨ Location of recovered drive sample
- Location of drive sample sealed for chemical analysis
- ▩ Cutting sample
- K = Estimated hydraulic conductivity

Logged By Chuck Headlee
 Supervisor Jim Carmody, CEG 1576
 Drilling Company Interphase Inc
 License Number C57-485165
 Driller Rick Nessinger
 Drilling Method Geoprobe
 Date Drilled August 18, 1996
 Type of Sampler Geoprobe Sampler
 PID Photoionization detector

Lithographic Log Details - Lithographic Log SVS-3, Shell Service Station WIC# 204-6852-1404, 1784 150th Avenue, San Leandro, California

LITHOLOGIC LOG SVS-5



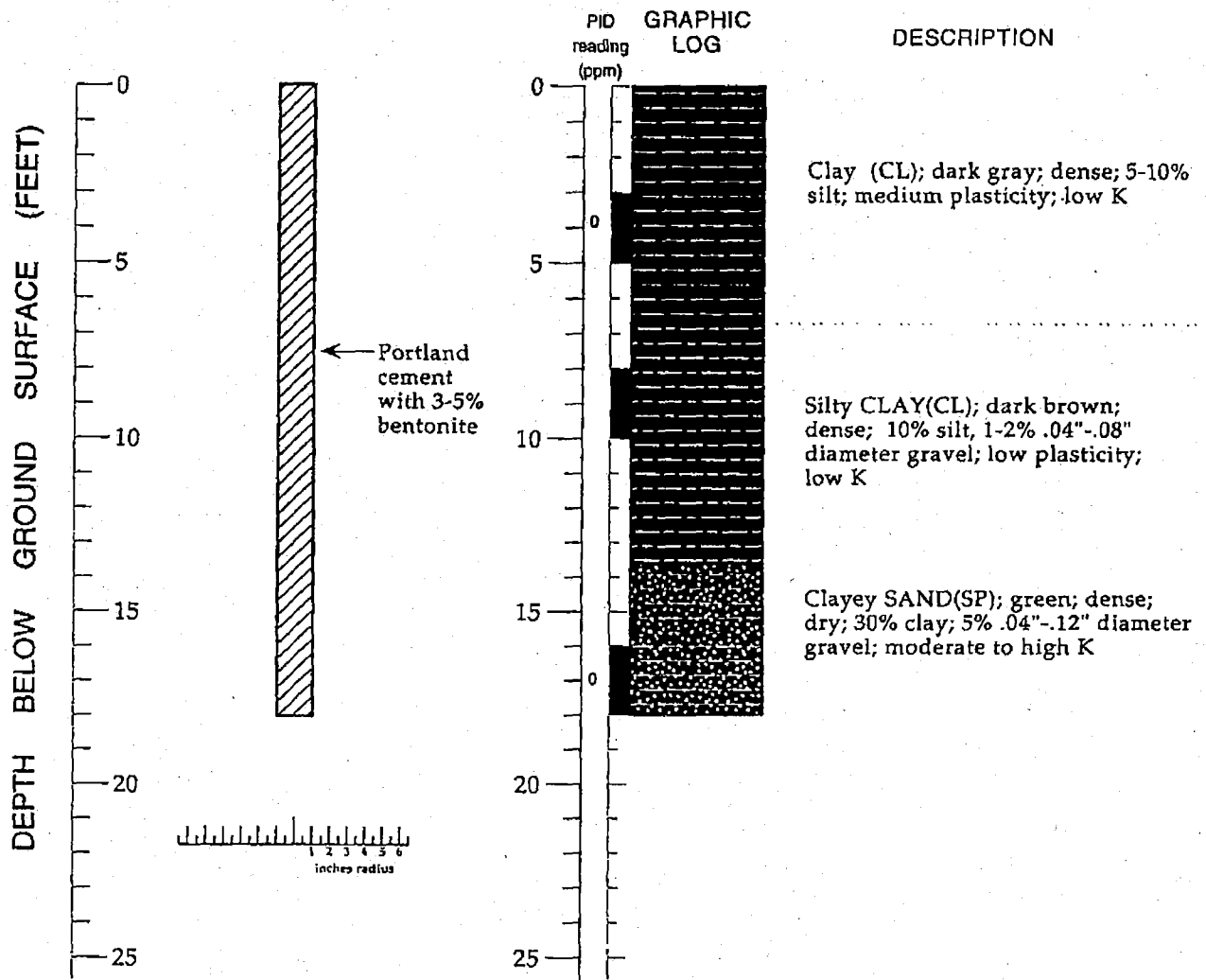
EXPLANATION

- ▼ Water level during drilling (date)
- ∇ Water level (date)
- Contact (dotted where approximate)
- ?-?-? Uncertain contact
- //// Gradational contact
- ▨ Location of recovered drive sample
- Location of drive sample sealed for chemical analysis
- ▩ Cutting sample
- K = Estimated hydraulic conductivity

Logged By: Chuck Headlee
 Supervisor: Jim Carmody, CEG 1576
 Drilling Company: Interphase Inc.
 License Number: C57-606481
 Driller: Rick Nessinger
 Drilling Method: Geoprobe
 Date Drilled: August 18, 1996
 Type of Sampler: Geoprobe Sampler
 PID: Photoionization detector

Lithographic Log Details - Lithographic Log SVS-5, Shell Service Station, WIC#204-6852-1404, 1784 150th Avenue, San Leandro, California

LITHOLOGIC LOG SVS-9



EXPLANATION

- ☒ Water level during drilling (date)
- ☒ Water level (date)
- Contact (dotted where approximate)
- ?-?-? Uncertain contact
- ////// Gradational contact
- ▒ Location of recovered drive sample
- Location of drive sample sealed for chemical analysis
- ▒▒▒▒ Cutting sample
- K = Estimated hydraulic conductivity

Logged By: Chuck Headlee
 Supervisor: Jim Carmody, CEG 1576
 Drilling Company: Interphase Inc.
 License Number: C57-606481
 Driller: Rick Nessinger
 Drilling Method: Geoprobe
 Date Drilled: July 19, 1996
 Type of Sampler: Geoprobe Sampler
 PID: Photionization detector

Lithographic Log Details - Lithographic Log SVS-9, Shell Service Station, WIC#204-6852-1404, 1784 150th Avenue San Leandro, California



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 270 Perkins Street
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BORING/WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	SVS-11
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	10-Nov-98
LOCATION	San Leandro, California	DRILLING COMPLETED	10-Nov-98
PROJECT NUMBER	248-0612-008	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	44.78 ft above msl
DRILLING METHOD	Hydraulic push	TOP OF CASING ELEVATION	Not Surveyed
BORING DIAMETER	2"	SCREENED INTERVAL	NA
LOGGED BY	T. Buggle	DEPTH TO WATER (First Encountered)	NA
REVIEWED BY	D. Ataide	DEPTH TO WATER (Static)	NA
REMARKS	Hand augered to 5' bgs.		

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	SOIL DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM	
							ASPHALT FILL: Road base.	0.4		
					CL		Silty CLAY (CL); Dark brown; dry; 75% clay, 25% silt; low plasticity; low estimated permeability.	3.0		
		SVS-11 @5.5		5	SP		SAND (SAND); Light-brown; dry; 10% silt, 80% sand, 10% gravel; high permeability.	5.0		
					CL		CLAY (CL); black; dry; 90% clay, 5% silt, 5% sand; medium plasticity; low permeability.	5.5		
0		SVS-11 @9.5		10						Portland Type III
					CL		Silty CLAY (CL); grey-green; dry; 60% clay, 30% silty, 10% sand; low plasticity; low permeability.	11.0		
		SVS-11 @15.0		15	CL		Silty Sandy CLAY (CL); grey-green; dry; 60% clay, 20% silty, 20% sand; low plasticity; low permeability.	15.0		
					CL		Silty CLAY (CL); black; dry; 60% clay, 30% silty, 10% sand; low plasticity; low permeability.	17.0		
					CL		Silty Sandy CLAY (CL); grey-green; dry; 60% clay, 20% silty, 20% sand; low plasticity; low permeability.	17.5		
		SVS-11 @19.5		20				19.5		Bottom of Boring @ 19.5 ft
				25						
				30						
				35						

WELL LOG (PID) K:\SANLEA-2\GINTS\NL1784.GPJ DEFAULT.GDT 11/9/06



CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	SVS-14
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	11-Nov-98
LOCATION	San Leandro, California	DRILLING COMPLETED	11-Nov-98
PROJECT NUMBER	248-0612-008	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	41.76 ft above msl
DRILLING METHOD	Hydraulic push	TOP OF CASING ELEVATION	Not Surveyed
BORING DIAMETER	2"	SCREENED INTERVAL	NA
LOGGED BY	T. Buggle	DEPTH TO WATER (First Encountered)	NA
REVIEWED BY	D. Ataide	DEPTH TO WATER (Static)	NA
REMARKS	Hand augered to 5' bgs.		

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	SOIL DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
				0.5			ASPHALT FILL: sand, gravel.	0.5	 Portland Type I/II
		SVS-14 @5.0		5	CL		CLAY ; (CL); black; soft; dry; 90% clay, 10% silt; high plasticity; low estimated permeability. @ 4' - medium-high plasticity.	3.0	
		SVS-14 @10.0		10	CL		@ 8' - black-brown; medium-hard; 80 % clay, 20% silt, medium plasticity; low estimated permeability @ 10' - brown; medium-hard; dry; 70% clay, 20% silt, 5% sand, 5% gravel; low plasticity; low estimated permeability.	12.0	
		SVS-14 @15.0		15	CL		Silty Sandy CLAY (CL); brown-grey; medium-hard; dry; 60% clay, 20% silt, 15% sand, 5% gravel; low plasticity; low estimated permeability.	15.0	
		SVS-14 @19.0		20	CL		Silty CLAY (CL); brown; medium-hard; moist; 70% clay, 25% silt, 5% sand; low plasticity; low estimated permeability. @ 16' 70% clay, 30% silt; low plasticity; low estimated permeability.	20.0	
				25					Bottom of Boring @ 20 ft
				30					
				35					

WELL LOG (PID) K:\SANLEA-2\GINTS\NL1784.GPJ DEFAULT.GDT 11/9/08



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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	SVS-15
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	11-Nov-98
LOCATION	San Leandro, California	DRILLING COMPLETED	11-Nov-98
PROJECT NUMBER	240612	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	41.76 ft above msl
DRILLING METHOD	Hydraulic push	TOP OF CASING ELEVATION	NA
BORING DIAMETER	2"	SCREENED INTERVALS	NA
LOGGED BY	T Buggle	DEPTH TO WATER (First Encountered)	NA
REVIEWED BY	D Ataide	DEPTH TO WATER (Static)	NA
REMARKS	Hand augered to 5' bgs		

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U S C S	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
							ASPHALT	10	
		svs 15 @4.5		5	CL		Silty CLAY (CL) black @ 5' black-brown, soft, dry, 80% clay, 20% silt, medium plasticity, low estimated permeability		
		svs 15 @10		10	CL		@ 9' - grey-green, medium-hard low plasticity, 70% clay, 30% silt		
		svs 15 @15		15	CL		Silty Sandy CLAY, (CL) , grey-brown medium-hard, dry, 60% clay, 20% silt, 20% sand, low plasticity, low estimated permeability @ 13' - grey-brown, 60% clay, 20% silt, 15% sand 5% gravel, medium plasticity	11.0	
		svs 15		20	CL		Silty CLAY (CL) grey-brown medium, dry 60% clay, 20% silt, 10% sand, 10% gravel low plasticity low estimated permeability @ 17' - medium-hard, 70% clay, 20% silt, 10% sand	15.0	

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WELL LOG (PID) 1\SHHELL16 CHARS\2406-1240612-124CBE8-1\SNL1784.GPJ DEFAULT GDT 6/10/09



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BORING / WELL LOG

CLIENT NAME	<u>Shell Oil Products Company (US)</u>	BORING/WELL NAME	<u>SVS-15</u>
JOB/SITE NAME	<u>1784 150th Avenue</u>	DRILLING STARTED	<u>11-Nov-98</u>
LOCATION	<u>San Leandro, California</u>	DRILLING COMPLETED	<u>11-Nov-98</u>

Continued from Previous Page

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U S C S	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
		@19.5						20.5	Bottom of Boring @ 20 fbg

WELL LOG (PID) | 1SHELL16 CHARS2406-1240612-1124CBE8-11SNL1784 GPJ DEFAULT GDT 6/10/09



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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	SVS-16
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	11-Nov-98
LOCATION	San Leandro, California	DRILLING COMPLETED	11-Nov-98
PROJECT NUMBER	240612	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	41.76 ft above msl
DRILLING METHOD	Hydraulic push	TOP OF CASING ELEVATION	NA
BORING DIAMETER	2"	SCREENED INTERVALS	NA
LOGGED BY	T. Buggle	DEPTH TO WATER (First Encountered)	NA
REVIEWED BY	D. Ataide	DEPTH TO WATER (Static)	NA
REMARKS	Hand augered to 5' bgs		

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U S C S	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
				0			ASPHALT	0.5	
				1.5			FILL , road base	1.5	
				5			Silty CLAY , (CL), black, soft, dry, 80% clay, 20% silt, medium plasticity, low estimated permeability		
		SVS 16 @5.0		5			@ 7' - grey-brown, medium, 70 % clay, 20% silt 10% gravel, medium-low plasticity		
				8			@ 8' - black, medium, 80% clay, 20% silt, medium plasticity		
				9			@ 9' - green-brown hard 60 % clay, 25% silt, 10%, 5% gravel, low plasticity low estimated permeability		
		SVS 16 @10.0		10	CL		@ 12' - brown @ 15' Brown-black very hard, 70 % clay 20% silt, 10% sand, low plasticity low estimated permeability		
				15					
		SVS 16 @15.0		15					
				19.0					
									Bottom of Boring @ 19 fbg

WELL LOG (PID) I:\SHELL16 CHARS\2406-1240612-124CBE8-1\SNL1784.GPJ_DEFAULT.GDT 6/10/09

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BORING / WELL LOG

CLIENT NAME	<u>Shell Oil Products Company (US)</u>	BORING/WELL NAME	<u>SVS-16</u>
JOB/SITE NAME	<u>1784 150th Avenue</u>	DRILLING STARTED	<u>11-Nov-98</u>
LOCATION	<u>San Leandro, California</u>	DRILLING COMPLETED	<u>11-Nov-98</u>

Continued from Previous Page

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U S C S	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
							Refusal @ 19'		

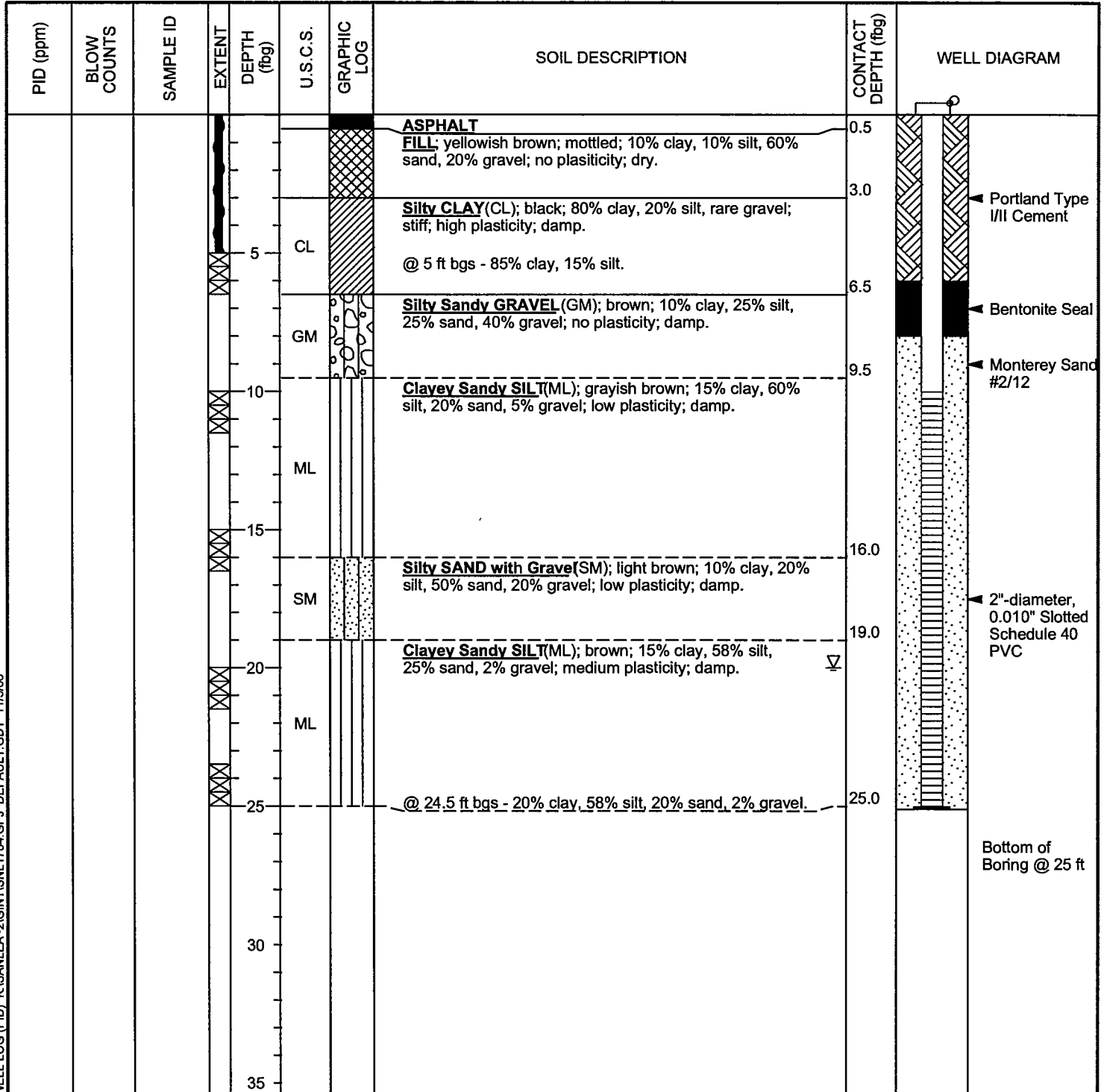
WELL LOG (PID) | \SHELL16 CHARS2406-1240612-124CBE8-1\SNL1784 GPJ DEFAULT GDT 6/10/09



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 270 Perkins Street
 Sonoma, CA 95476
 Telephone: 707-935-4850
 Fax: 707-935-6649

BORING/WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	MW-5
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	24-Oct-01
LOCATION	San Leandro, California	DRILLING COMPLETED	24-Oct-01
PROJECT NUMBER	248-0612-008	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	40.78 ft above msl
DRILLING METHOD	Hollow-stem auger	TOP OF CASING ELEVATION	Not Surveyed
BORING DIAMETER	8"	SCREENED INTERVAL	10 to 25 fbg
LOGGED BY	S. Landsittel	DEPTH TO WATER (First Encountered)	20.0 ft (24-Oct-01) ▽
REVIEWED BY	S. Bork, RG# 5620	DEPTH TO WATER (Static)	NA ▽
REMARKS	Hand augered to 5' bgs. Located at corner of private driveway and 150th Ave. 100' SW of site.		



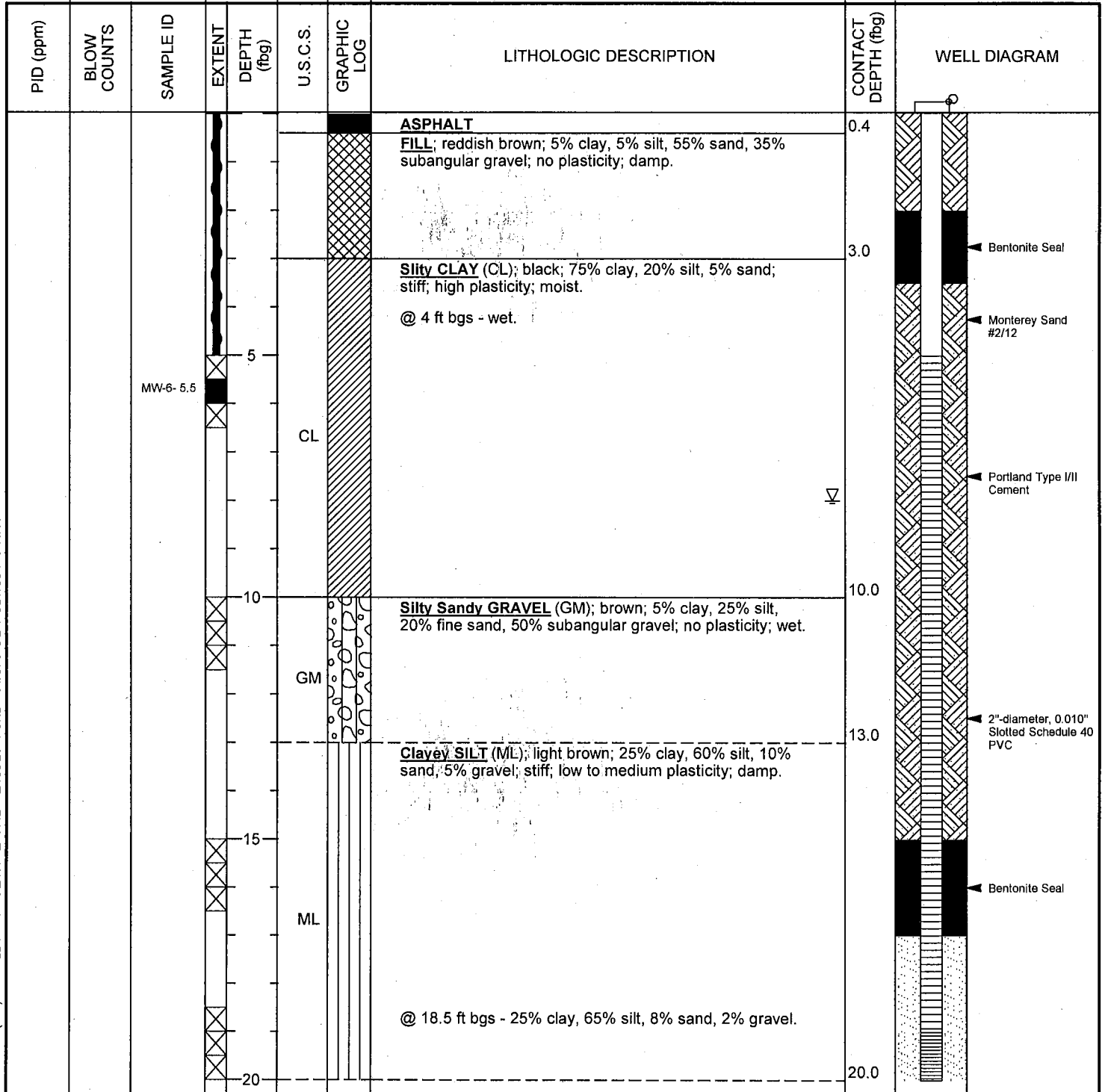
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 5900 Hollis Street, Suite A
 Emeryville, CA 94608
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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	MW-6
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	24-Oct-01
LOCATION	San Leandro, California	DRILLING COMPLETED	24-Oct-01
PROJECT NUMBER	240612	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	41.76 ft above msl
DRILLING METHOD	Hollow-stem auger	TOP OF CASING ELEVATION	NA
BORING DIAMETER	8"	SCREENED INTERVALS	5 to 20 fbg
LOGGED BY	S. Landsittel	DEPTH TO WATER (First Encountered)	8.00 fbg
REVIEWED BY	S. Bork, RG# 5620	DEPTH TO WATER (Static)	NA
REMARKS	Hand augered to 5' bgs. Located in north side of private driveway approximately 70' SW of site and 120' SE of 150th Ave.		



WELL LOG (PID) \\SHELL16-CHARS\2406-1240612-1124CBE8-1NSL1784.GPJ DEFAULT.GDT 6/10/09

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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	MW-6
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	24-Oct-01
LOCATION	San Leandro, California	DRILLING COMPLETED	24-Oct-01

Continued from Previous Page

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (ftg)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (ftg)	WELL DIAGRAM
									<p>Bottom of Boring Montezuma Sand #212109 2" diameter, 0.010" Slotted Schedule 40 PVC</p>

WELL LOG (PID) \SHELL\6-CHARS\2406-1240612-124CBE8-11SNL1784.GPJ DEFAULT.GDT 6/10/09



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BORING/WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	MW-7
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	03-Oct-02
LOCATION	San Leandro, California	DRILLING COMPLETED	03-Oct-02
PROJECT NUMBER	248-0612-008	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	44.86 ft above msl
DRILLING METHOD	Hollow Stem Auger	TOP OF CASING ELEVATION	44.45 ft above msl
BORING DIAMETER	8"	SCREENED INTERVAL	22 to 27 fbg
LOGGED BY	S. Dalie	DEPTH TO WATER (First Encountered)	24.5 ft (03-Oct-02) ▽
REVIEWED BY	M. Derby, PE# 55475	DEPTH TO WATER (Static)	18.88 ft (04-Oct-02) ▽
REMARKS	Hand augered to 5' bgs.		

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (ft)	U.S.C.S.	GRAPHIC LOG	SOIL DESCRIPTION	CONTACT DEPTH (ft)	WELL DIAGRAM
				0.8			Asphalt	0.8	
				2.8	GM		Silty GRAVEL with Sand (GM); 10YR 5/3, brown; loose; dry; 30% Silt, 10% Sand, 60% Clay; no plasticity; no odor; road base.	2.8	
no odor		SB7@5'		5	CL		Silty CLAY (CL); 10YR 2/1, Black; hard; dry; 65% Clay, 35% Silt; very low plasticity; no odor.		
no odor		SB7@10'		10			10YR 4/2, very dark greyish brown; very hard. Clay; Very stiff to hard; dry; 60% Clay, 40% Silt. 10YR 3/2, very dark greyish brown.		Portland Type I/II Cement
		SB7@15'		13.0			SILT with some Clay (ML); 2.5Y 5/2, greyish brown; hard; dry; 2% Clay, 98% Silt; no plasticity; no odor. 10YR 5/2, greyish brown.	13.0	
no odor		SB7@20'		20	ML		Very stiff, brittle; dry; 100% Silt.		Bentonite Seal
		SB7@25'		22.3	GW		Well Graded GRAVEL with Silt and Sand (GW); 5Y 3/2; dark olive grey; loose; moist; 20% Silt, 25% Sand, 55% Gravel; no plasticity; no odor.	22.3	
hydrocarbon odor		SB7@25'		23.0	ML		Clayey SILT with some fine Gravels and Sand (ML); 5Y 3/2, olive grey; medium stiff; moist to wet; 25% Clay, 60% Silt, 5% Sand, 10% Gravel; no plasticity; slight hydrocarbon odor.	23.0	Monterey Sand #2/12
				25.8			Silty GRAVEL with Sand (GM); 5Y 4/2, olive grey; loose; wet to saturated; 30% Silt, 5% Sand, 65% Gravel; no plasticity; "old" hydrocarbon or petroleum odor.	25.8	2"-diameter, 0.010" Slotted Schedule 40 PVC
hydrocarbon odor		SB7@32'		32.0	GM			32.0	
				35					Bottom of Boring @ 32 ft

WELL LOG (PID) SANLEA-2GINTSNL1784.GPJ REFAULT.GDT 11/3/06



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BORING/WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	MW-8
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	04-Oct-02
LOCATION	San Leandro, California	DRILLING COMPLETED	04-Oct-02
PROJECT NUMBER	248-0612-008	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	43.60 ft above msl
DRILLING METHOD	Direct Push/Hollow Stem Auger	TOP OF CASING ELEVATION	43.27 ft above msl
BORING DIAMETER	8"	SCREENED INTERVAL	19 to 24 fbg
LOGGED BY	S. Dalie	DEPTH TO WATER (First Encountered)	21.0 ft (04-Oct-02) ▾
REVIEWED BY	M. Derby, PE# 55475	DEPTH TO WATER (Static)	17.76 ft (04-Oct-02) ▾
REMARKS	Hand augered to 5' bgs.		

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	SOIL DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
				0.8		Asphalt		0.8	
				2.3	GW		Well graded GRAVEL with Sand (GW) ; 10YR 4/2, dark greyish brown; loose; dry; 20% Sand, 80% Gravel; no plasticity; no odor; road base.	2.3	
no odor		MW8@5'		5	CL		Silty CLAY (CL) ; 10YR 2/1, black; medium hard; dry; 80% Clay; 20% Silt; very low plasticity; no odor.		
no odor		MW8@10'		10			10YR 3/1, very dark grey; very hard; dry; 75% Clay, 25% Silt; low plasticity.		
odor		MW8@15'		15	ML		Clayey SILT (ML) ; GLEY, 5GY 5/1; stiff; hard; 10% Clay, 90% Silt; no plasticity.	11.5	
strong hydrocarbon odor		MW8@20'		20			Slightly more Clay; stiff; dry; 20% Clay, 80% Silt; slight staining. GLEY, 5GY 5/1, stained; stiff; dry; 25% Clay, 75% Silt; hydrocarbon odor.	20.8	
strong hydrocarbon odor		MW8@25'		25	GM		Silty GRAVEL with Sand and some Clay (GM) ; GLEY, 5GY 5/1, stained; soft; moist to wet; 5% Clay, 20% Silt, 15% Sand, 60% Gravel; no plasticity; strong hydrocarbon odor.	20.8	
slight hydrocarbon odor				26.0	CL		No Clay; loose; wet to saturated; 15% Silt, 15% Sand, 70% Gravel; no plasticity; strong hydrocarbon odor.	26.0	
				27.5			Silty CLAY (CL) ; 5Y 3/2, olive grey; very hard; dry; 75% Clay, 25% Silt; low plasticity; slight hydrocarbon odor.	27.5	
				30					
				35					

Portland Type I/II Cement

Bentonite Seal

Monterey Sand #2/12
2"-diameter, 0.010" Slotted Schedule 40 PVC

Bottom of Boring @ 27.5 ft

WELL LOG (PID) K:\SANLEA-2\GINTU\1784.GPJ 11/3/06



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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	SB-10
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	23-Jun-03
LOCATION	San Leandro, California	DRILLING COMPLETED	23-Jun-03
PROJECT NUMBER	240612	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	40 88 ft above msl
DRILLING METHOD	Hydraulic push	TOP OF CASING ELEVATION	NA
BORING DIAMETER	2"	SCREENED INTERVALS	NA
LOGGED BY	S Dale	DEPTH TO WATER (First Encountered)	25 00 fbg
REVIEWED BY	M Derby, PE# 55475	DEPTH TO WATER (Static)	13 3 fbg
REMARKS	Hand augered to 5' bgs		

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U S C S	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
				0			Asphalt	0 5	
				5	CL		Silty CLAY (CL) , black, stiff, dry, 80% clay, 20% silt low plasticity	5 0	
				10	ML		Clayey SILT (ML) , black, soft, dry, % clay, % silt, low plasticity	10 5	
1		SB 10 10		10					
				15	CL		CLAY (CL) , black stiff, dry, 100% clay, low plasticity	19 0	
0		SB 10 15 5		15					
				20			Silty CLAY with Gravel (CL) , light olive brown, very stiff dry 65% clay, 10% silt, 5% sand, 15% gravel, low	19 0	

WELL LOG (PID) | |SHELL|6 CHARS|240612-124CBE8-1|SNL|1784 GPJ DEFAULT GDT 6/10/03

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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	SB-10
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	23-Jun-03
LOCATION	San Leandro, California	DRILLING COMPLETED	23-Jun-03

Continued from Previous Page

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U S C S	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
0		SB 10 20 5			CL		plasticity	21 5	 Portland Type I/II Cement 6/23/2005 TPHg = <50 ppb benzene <1 1 ppb MTBE <0 50 ppb
1		SB 10 22			GP GC		Clayey GRAVEL (GP-GC), olive brown, medium dense, damp, 30% clay, 10% sand, 60% gravel no plasticity	23 5	
					SC		Clayey SAND with Gravel (SC), olive brown medium dense damp, 20% clay, 70% sand, 10% gravel, no plasticity	25 0	
1		SB 10 25		25	SW		SAND (SW), olive brown medium dense, wet % clay, % sand % gravel, no plasticity	28 0	
							Silty CLAY with Gravel (CL), olive brown, very stiff dry 60% clay, 30% silt, 10% gravel, low plasticity		
1		SB 10 30		30	CL				
1		SB 10 35		35					
0		SB 10 37			GW		GRAVEL (GW), olive brown loose wet, 5% sand, 95% gravel no plasticity	36 0	
0		SB 10 39 5		40	ML		Sandy SILT with Clay (ML), dark olive brown, soft, moist, 5% clay, 75% silt 20% sand, medium plasticity	38 0	
								40 0	Bottom of Boring @ 40 fbg

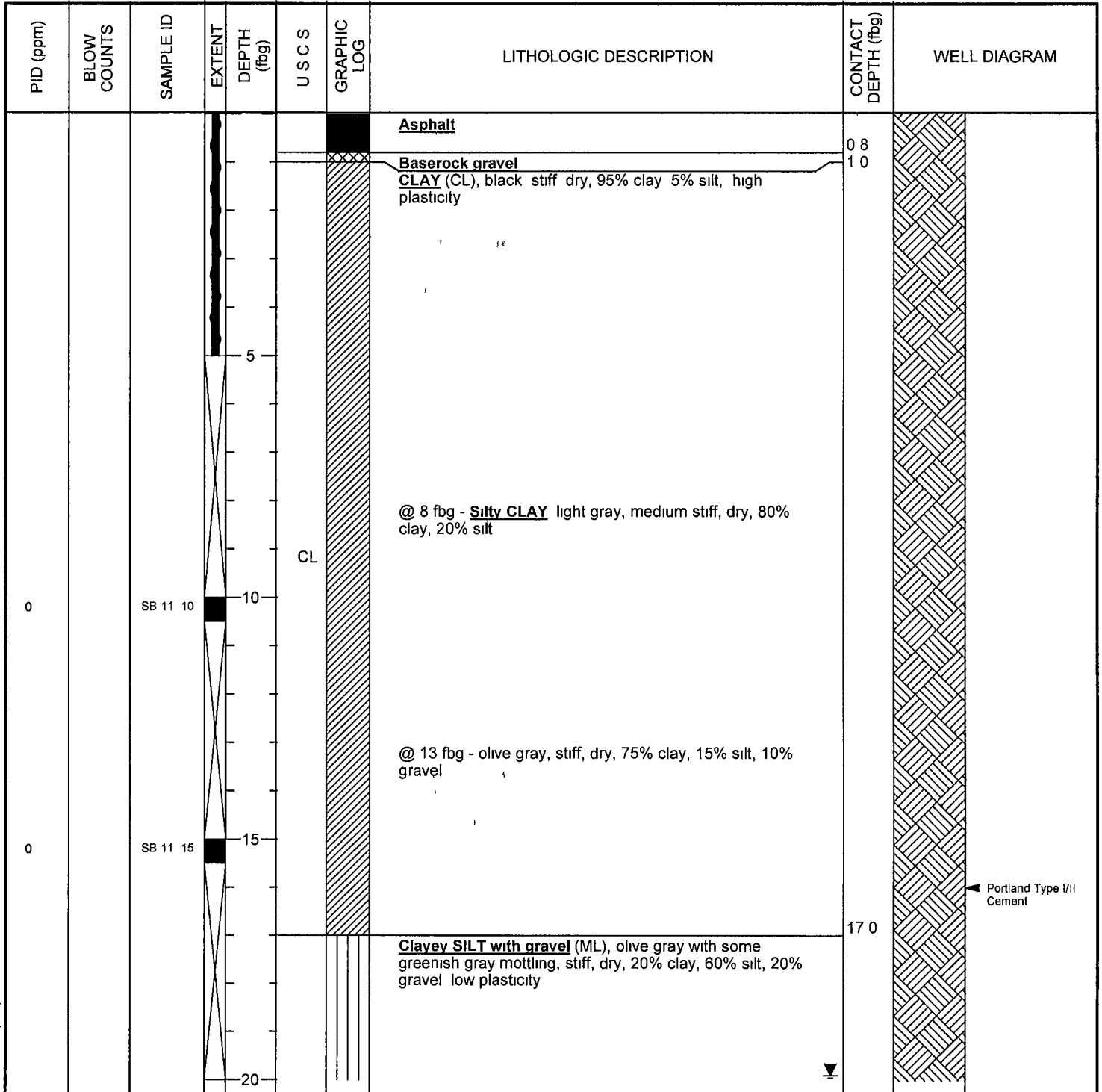
WELL LOG (PID) | \SHELL\6 CHARS\2406-1240612-1124CBE8-1\SNL1784 GP J DEFAULT GDT 6/10/09



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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	SB-11
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	24-Jun-03
LOCATION	San Leandro, California	DRILLING COMPLETED	24-Jun-03
PROJECT NUMBER	240612	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	45.38 ft above msl
DRILLING METHOD	Hydraulic push	TOP OF CASING ELEVATION	NA
BORING DIAMETER	2"	SCREENED INTERVALS	NA
LOGGED BY	S. Dale	DEPTH TO WATER (First Encountered)	28.00 fbg
REVIEWED BY	M. Derby, PE# 55475	DEPTH TO WATER (Static)	19.9 fbg
REMARKS	Hand augered to 5' bgs		



WELL LOG (PID) I:\SHELL\6-CHARS\2406-1240612-1\24CBE8-1\SNL1784.GPJ DEFAULT GDT 6/10/03

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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	SB-11
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	24-Jun-03
LOCATION	San Leandro, California	DRILLING COMPLETED	24-Jun-03

Continued from Previous Page

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U S C S	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
0		SB 11 20			ML				
2		SB 11 24			GP GC		Clayey GRAVEL (GP-GC) olive gray, loose, dry, 20% clay, 80% gravel, no plasticity	23 0	
24		SB 11 25		25	SM		Silty SAND with Gravel (SM) greenish gray, loose, damp, 10% clay, 80% sand, 10% gravel, no plasticity	25 0	
105		SB 11 28			SW		@ 27 9 fbg - wet SAND (SW) , greenish gray loose, wet 100% sand, no plasticity	28 0	
385		SB 11 30		30	GC		Clayey GRAVEL (GC) , greenish gray, medium dense, wet, 20% clay, 80% gravel no plasticity	30 0	
								32 0	
									Bottom of Boring @ 32 fbg

WELL LOG (PID) I | SHELL16 CHARS2406-1240612-1124CBE8-1 | SNL1784 GFJ DEFAULT GDT 6/10/03



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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	SB-12
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	24-Jun-03
LOCATION	San Leandro, California	DRILLING COMPLETED	24-Jun-03
PROJECT NUMBER	240612	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	41.28 ft above msl
DRILLING METHOD	Hydraulic push	TOP OF CASING ELEVATION	NA
BORING DIAMETER	2"	SCREENED INTERVALS	NA
LOGGED BY	S Dale	DEPTH TO WATER (First Encountered)	25.00 fbg
REVIEWED BY	M Derby, PE# 55475	DEPTH TO WATER (Static)	10.8 fbg
REMARKS	Hand augered to 5' bgs		

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT DEPTH (fbg)	U S C S	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
			0			Asphalt	0.5	
			5	ML		Clayey SILT (ML) , black, medium stiff, dry, 45% clay, 55% silt low plasticity	6.5	
1		SB 12 10	10	CL		CLAY (CL) , dark olive brown very stiff, dry, 95% clay, 5% gravel, high plasticity @ 11 fbg - light olive gray 75% clay, 25% silt	16.0	
1		SB 12 15	15	GP GC		Clayey GRAVEL (GP-GC) , light olive gray medium dense, damp, 20% clay, 10% silt, 15% sand, 50% gravel no plasticity	16.0	
			20					

WELL LOG (PID) 1\SHELL6 CHARS2406-1240612-1\24CBE8-1\SNL1784 GPJ DEFAULT GDT 6/10/03

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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	SB-12
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	24-Jun-03
LOCATION	San Leandro, California	DRILLING COMPLETED	24-Jun-03

Continued from Previous Page

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	USCS	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
0		SB 12 20		21.0				21.0	Portland Type I/II Cement
				23.0	ML		Clayey SILT with sand (ML) , light olive gray, medium dense, damp, 30% clay 60% silt, 10% sand, low plasticity		
				25.0	CL		Silty CLAY with Sand (CL) light olive brown medium stiff, damp to moist, 60% clay, 30% silt 10% sand low plasticity		6/24/2005 TPHg = <50 ppb benzene <0.50 ppb MTBE <0.50 ppb
0		SB 12 25		25.0	SC		Clayey SAND (SC) , light olive gray, loose wet, 40% clay, 60% sand, 10% gravel, no plasticity		
				27.0			GRAVEL with sand (GW) , light olive gray, loose, wet, 30% sand, 70% gravel no plasticity		
0		SB 12 30		30.0					
				35.0	GW				
0		SB 12 35		35.0					
				38.0					
				40.0	SW		SAND (SW) light olive gray, loose, wet, 100% sand, no plasticity		
0		SB 12 39.5		40.0					Bottom of Boring @ 40 fbg

WELL LOG (PID) 1\SHELL16 CHARS\2406-1240612-124CBE8-1\SNL1784 GFJ DEFAULT GDT 6/10/03



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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	SB-13
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	25-Jun-03
LOCATION	San Leandro, California	DRILLING COMPLETED	25-Jun-03
PROJECT NUMBER	240612	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	41 18 ft above msl
DRILLING METHOD	Hydraulic push	TOP OF CASING ELEVATION	NA
BORING DIAMETER	2"	SCREENED INTERVALS	NA
LOGGED BY	S Dale	DEPTH TO WATER (First Encountered)	24 00 fbg
REVIEWED BY	M Derby, PE# 55475	DEPTH TO WATER (Static)	NA
REMARKS	Hand augered to 5' bgs		

WELL LOG (PID) 1 \SHELL\US CHARS\2406-1240612-124CBE8-1\SNL1784 GPJ DEFAULT GDT 6/10/09

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT DEPTH (fbg)	U S C S	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
			0			Asphalt	0 5	
			5			Silty CLAY (CL) , black, very stiff, dry, 90% clay, 10% silt, high plasticity		
1		SB 13 10	10	CL		@ 6 5 fbg - 70% clay 30% silt		
			13 5			Clayey SILT with gravel (ML) olive gray, very stiff, dry, 20% clay, 70% silt, 10 % sand, medium plasticity	13 5	
1		SB 13 15	15	ML				
			16 5			Silty CLAY (CL) , light olive gray very stiff dry, 80% clay, 20% silt, high plasticity	16 5	
			20	CL				

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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	SB-13
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	25-Jun-03
LOCATION	San Leandro, California	DRILLING COMPLETED	25-Jun-03

Continued from Previous Page

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U S C S	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
1		SB 13 20						22 0	<p>Portland Type I/II Cement</p> <p>6/23/2005 TPHg = <50 ppb benzene <0 50 ppb MTBE <0 50 ppb</p>
					GP GC		Clayey GRAVEL (GP-GC), olive gray, dense, damp 30% clay, 70% gravel, no plasticity		
1		SB 13 24			SW		SAND (SW), olive brown dense, wet 20% sand 80% gravel, no plasticity	24 0	
1		SB 13 25		25	SC		Clayey SAND (SC), olive gray, dense wet, 40% clay, 60% sand, medium plasticity	25 0	
					ML		Clayey SILT with gravel , (ML), olive gray, dense, wet, 20% clay, 75% silt, 5% gravel, medium plasticity	26 0	
0		SB 13 30		30			Clayey GRAVEL with sand (GP-GC), dark olive gray, loose, wet 15% clay, 20% sand, 65% gravel no plasticity @ 31 fbg - very dense, 25% clay, 20% sand, 55% gravel	30 0	
					GP GC		 @ 34 fbg - medium dense 25% clay, 10% sand, 65% gravel		
0		SB 13 35		35				37 0	
					CL		Silty CLAY with gravel (CL), dark olive gray, very stiff damp to dry 80% clay, 15% silt, 5% gravel high plasticity		
1		SB 13 39 5		40				40 0	Bottom of Boring @ 40 fbg

WELL LOG (PID) | \SHELL\6 CHARS\2406-1240612-124CBEB-1\SNL1784 GPJ DEFAULT.GDT 6/10/09



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BORING/WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	SB-14
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	24-Jun-03
LOCATION	San Leandro, California	DRILLING COMPLETED	24-Jun-03
PROJECT NUMBER	248-0612-008	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	40.98 ft above msl
DRILLING METHOD	Hydraulic push	TOP OF CASING ELEVATION	Not Surveyed
BORING DIAMETER	2"	SCREENED INTERVAL	NA
LOGGED BY	S. Dalie	DEPTH TO WATER (First Encountered)	25.0 ft (24-Jun-03) ▼
REVIEWED BY	M. Derby, PE# 55475	DEPTH TO WATER (Static)	7.85 ft ▼
REMARKS	Hand augered to 5' bgs.		

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	SOIL DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
				0.5			Asphalt Silty CLAY (CL); black; medium stiff; dry; 65% clay, 35% silt; high plasticity.	0.5	<p>Portland Type I/II Cement</p> <p>6/24/2005 TPHg = <67,000 ppb, benzene <100 ppb, MTBE <100 ppb</p>
				5	CL				
0		SB-14-10		10					
				13.0			Gravelly SILT (ML); light olive brown; stiff; dry; 75% silt, 25% gravel; medium plasticity.	13.0	
0		SB-14-15		15	ML		@ 17 fbg - 90% silt, 10% gravel.		
				20.0			Clayey GRAVEL with sand (GP-GC); light olive gray; dense; damp; 30% clay, 10% sand, 60% gravel; no plasticity.	20.0	
1		SB-14-20		20	GP GC				
				22.0			Clayey SAND (SW); light olive gray; medium dense; wet; 30% clay, 70% sand; no plasticity.	22.0	
0		SB-14-24		24	GW				
0		SB-14-25		25	GW		GRAVEL (GW); light olive; very dense; wet; 20% sand, 80% gravel; no plasticity.	25.0	
				26.0			Gravelly SILT with sand (ML); light olive gray; medium dense; wet; 75% silt, 25% gravel; no plasticity.	26.0	
				30.0			GRAVEL with sand (GW); light olive gray; loose; wet; 25% sand, 75% gravel; no plasticity.	30.0	
1		SB-14-30		30	GW				
				34.0			Clayey GRAVEL (GC); light olive gray; very stiff; wet;	34.0	
				35					

WELL LOG (PID) KISANLEA-2IGINTSNL1784.GPJ DEFAULT.GDT 11/03/06

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BORING/WELL LOG

CLIENT NAME Shell Oil Products Company (US) BORING/WELL NAME SB-14
 JOB/SITE NAME 1784 150th Avenue DRILLING STARTED 24-Jun-03
 LOCATION San Leandro, California DRILLING COMPLETED 24-Jun-03

Continued from Previous Page

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	SOIL DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
1		SB-14-35			GC		50% clay, 50% gravel; medium plasticity.	36.5	
					GW		GRAVEL with sand (GW); light olive gray; loose; wet; 20% sand, 80% gravel; no plasticity.		
0		SB-14-39.5		40				40.0	Bottom of Boring @ 40 ft
				45					
				50					
				55					
				60					
				65					
				70					
				75					

WELL LOG (PID) K:\SANLEA-2\GINT\SNL1784.GPJ DEFAULT.GDT 11/3/06



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BORING/WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	SB-15
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	26-Jun-03
LOCATION	San Leandro, California	DRILLING COMPLETED	26-Jun-03
PROJECT NUMBER	248-0612-008	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	47.00 ft above msl
DRILLING METHOD	Hydraulic push	TOP OF CASING ELEVATION	Not Surveyed
BORING DIAMETER	2"	SCREENED INTERVAL	NA
LOGGED BY	S. Dalie	DEPTH TO WATER (First Encountered)	25.0 ft (26-Jun-03)
REVIEWED BY	M. Derby, PE# 55475	DEPTH TO WATER (Static)	24.00 ft
REMARKS	Hand augered to 5' bgs.		

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	SOIL DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
				0.5			Asphalt Silty CLAY (CL); black; soft; dry; 55% clay, 45% silt; high plasticity.	0.5	
2.5				5	CL				
		SB-15-10		10	ML		Clayey SILT (ML); black; soft; dry; 45% clay, 55% silt; high plasticity.	10.0	
1				11.0			Silty CLAY with grave (CL); black; very stiff; dry; 50% clay, 40% silt, 10% gravel; high plasticity.	11.0	
				14			@ 14 fbg - gray; 60% clay, 40% silt.		
		SB-15-15		15	CL				
0				16.5			SILT (ML); olive gray; very stiff; dry; 15% clay; 85% silt; medium plasticity.	16.5	
		SB-15-20		20	GW		GRAVEL (GW); olive gray; loose; dry; 20% sand, 80% gravel; no plasticity.	21.0	
10				23.0			Clayey GRAVEL (GP-GC); olive gray; dense; damp; 30% clay, 70% gravel; medium plasticity.	23.0	
9		SB-15-22.5		23.0					
				25			@ 25 fbtg - wet.		
		SB-15-25		25	GP GC				
25				30.0			Silty SAND (SM); olive gray; medium dense; wet; 10% clay, 20% silt, 70% sand; low plasticity.	30.0	
				32			@ 32 fbg - 10% clay, 25% silt, 55% sand, 10% gravel.		
		SB-15-30		30	SM				
21				34.0			CLAY with grave (CL); olive brown; very stiff; damp;	34.0	
				35					

WELL LOG (PID) K:\SANLEA-2\GINT\SNL1784.GPJ DEFAULT.GDT 11/3/06

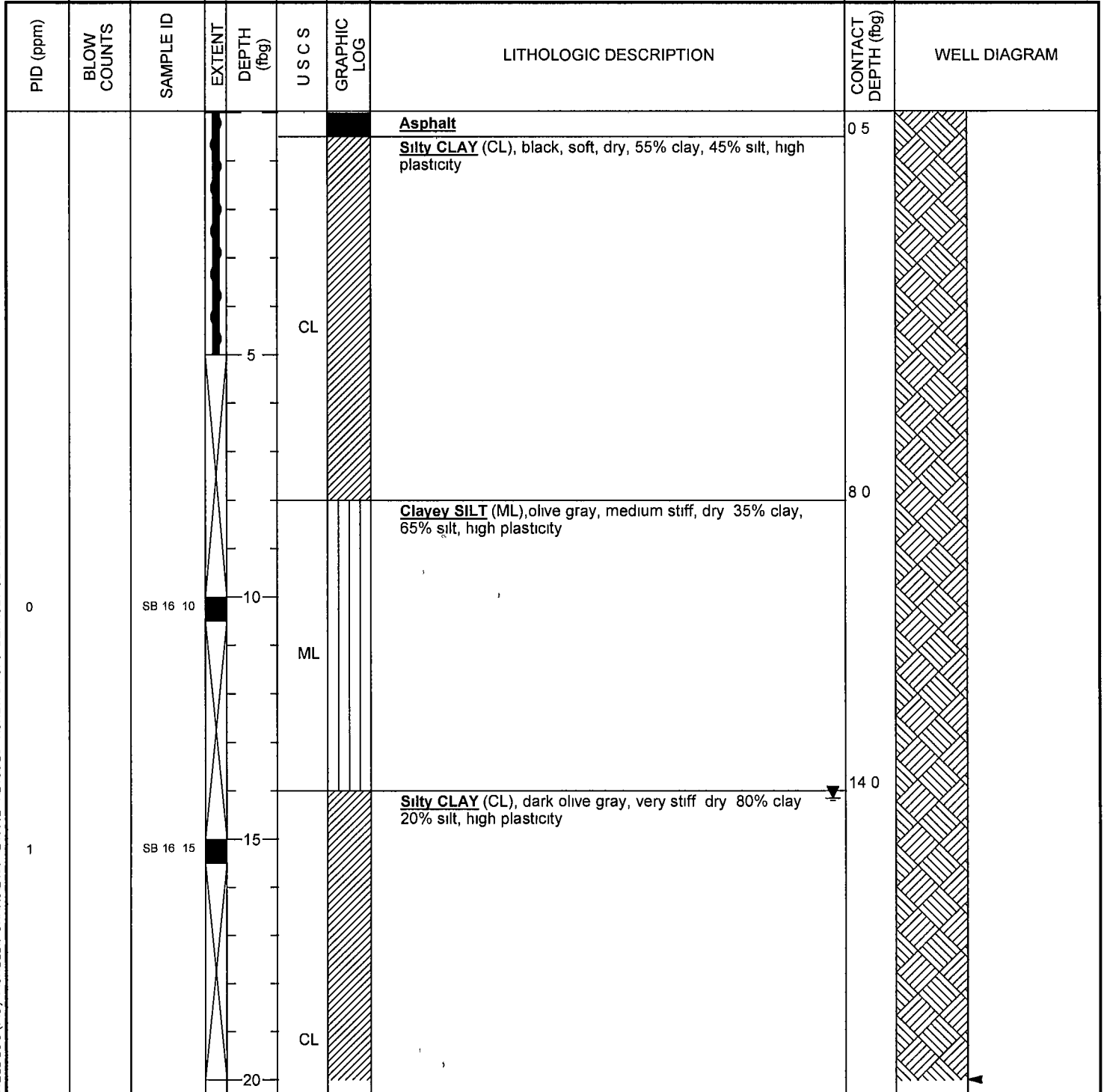
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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	SB-16
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	23-Jun-03
LOCATION	San Leandro, California	DRILLING COMPLETED	23-Jun-03
PROJECT NUMBER	240612	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	40 70 ft above msl
DRILLING METHOD	Hydraulic push	TOP OF CASING ELEVATION	NA
BORING DIAMETER	2"	SCREENED INTERVALS	NA
LOGGED BY	S. Dalie	DEPTH TO WATER (First Encountered)	24 00 fbg
REVIEWED BY	M. Derby, PE# 55475	DEPTH TO WATER (Static)	(23-Jun-03) 14 2 fbg
REMARKS	Hand augered to 5' bgs		



WELL LOG (PID) I:\SHELL16 CHARS\2406-1240612-124CBE8-1\SNL1784.GPJ DEFAULT.GDT 6/10/03

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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	SB-16
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	23-Jun-03
LOCATION	San Leandro, California	DRILLING COMPLETED	23-Jun-03

Continued from Previous Page

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	USCS	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
1		SB 16 20					@ 20 fbg - 70% clay, 20% silt 10% gravel		
0		SB 16 24		24.0	GP GC		Clayey GRAVEL (GP-GC) light olive brown, medium dense, wet 30% clay, 10% sand, 60% gravel, medium plasticity	24.0	
0		SB 16 25		25.5	GW		GRAVEL (GW), light olive brown dense wet, 20% sand, 80% gravel no plasticity	25.5	
				26.5			Silty CLAY (CL), light olive brown, very stiff, damp, 80% clay, 20% silt, high plasticity	26.5	
				28.0	CL			28.0	
0		SB 16 28		29.5	GP GC		Clayey GRAVEL (GP-GC), light olive brown, loose, wet 5% clay, 15% sand 80% gravel low plasticity	29.5	
				30.0			Clayey SILT (ML) dark olive brown, medium stiff damp, 10% clay 90% silt high plasticity	30.0	
				33.0	ML			33.0	
				35.0			GRAVEL (GW) dark olive gray, loose wet, 20% sand 80% gravel, no plasticity	35.0	
1		SB 16 35		36.0				36.0	
				36.0			Clayey GRAVEL (GP-GC) dark olive gray, medium stiff, wet, 40% clay, 20% sand, 40% gravel low plasticity	36.0	
				40.0	GP GC			40.0	
0		SB 16 39.5		40.0				40.0	

WELL LOG (PID) I:\SHELL16 CHARS\2405-1240612-124CBEB-1\SNL1784 GPJ DEFAULT GDT 6/10/09



CLIENT NAME Shell Oil Products Company (US) **BORING/WELL NAME** MW-9
JOB/SITE NAME 1784 150th Avenue **DRILLING STARTED** 19-Nov-03
LOCATION San Leandro, California **DRILLING COMPLETED** 19-Nov-03
PROJECT NUMBER 248-0612-008 **WELL DEVELOPMENT DATE (YIELD)** NA
DRILLER Gregg Drilling **GROUND SURFACE ELEVATION** 41.84 ft above msl
DRILLING METHOD Hollow-stem auger **TOP OF CASING ELEVATION** 41.65 ft above msl
BORING DIAMETER 8" **SCREENED INTERVAL** 30 to 35 fbg
LOGGED BY S. Dalie **DEPTH TO WATER (First Encountered)** 20.0 ft (19-Nov-03)
REVIEWED BY M. Derby, PE# 55475 **DEPTH TO WATER (Static)** 14.78 ft (20-Nov-03)
REMARKS Hand augered to 5 fbg, located in Portofino Circle.

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	SOIL DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
				0.6			Asphalt. CLAY ; (CL); Black; very stiff; dry; 85% clay, 15% silt; low plasticity. CLAY with some small sub angular gravel.	0.6	<p>Portland Type I/II</p> <p>Bentonite Seal</p> <p>Lonestar Sand #2/12 2"-diam., 0.010" Slotted Schedule 40 PVC</p>
0.1		MW-9-5'		5	CL				
0		MW-9-10'		10			Brownish gray; very stiff to hard; dry; 90% clay, 5% silt; no plasticity.		
0.1		MW-9-15'		15	OL		Silty CLAY (OL); Brownish gray; very stiff to hard; dry; 70% clay, 30% silt.	15.0	
				17.5	SC		Clayey SAND (SC); Brownish gray; medium dense; damp; 45% clay, 55% sand; low plasticity.	17.5	
3		MW-9-20'		20	GC		Clayey GRAVEL ; (GC); Brownish gray; medium dense; moist to wet; 25% clay, 5% sand, 70% Gravel.	20.0	
				22.5			CLAY ; (CL); Light brown; very stiff to hard; damp; 95% clay, 5% small gravel.	22.5	
1.8		MW-9-25'		25	CL				
				27.5			Clayey GRAVEL ; (GC); Light brown; very dense; saturated; 45% clay, 55% gravel.	27.5	
0		MW-9-30'		30	GC				
				32.5			Well Graded GRAVEL ; (GW); Light brown; loose; saturated; 25% coarse sand, 75% gravel.	32.5	
				35	GW			35.0	

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BORING/WELL LOG

CLIENT NAME Shell Oil Products Company (US) BORING/WELL NAME MW-9
 JOB/SITE NAME 1784 150th Avenue DRILLING STARTED 19-Nov-03
 LOCATION San Leandro, California DRILLING COMPLETED 19-Nov-03

Continued from Previous Page

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	SOIL DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
0.1		MW-9-34.5'		40 45 50 55 60 65 70 75					Bottom of Boring @ 35 ft

WELL LOG (PID) K:\SANLEA-2\GINTS\NL1784.GPJ DEFAULT.GDT 10/26/06



CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	MW-10
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	20-Nov-03
LOCATION	San Leandro, California	DRILLING COMPLETED	20-Nov-03
PROJECT NUMBER	248-0612-008	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	50.98 ft above msl
DRILLING METHOD	Hollow-stem auger	TOP OF CASING ELEVATION	50.64 ft above msl
BORING DIAMETER	10"	SCREENED INTERVAL	28 to 32 fbg
LOGGED BY	S. Dalie	DEPTH TO WATER (First Encountered)	23.5 ft (20-Nov-03)
REVIEWED BY	M. Derby, PE# 55475	DEPTH TO WATER (Static)	20.00 ft (20-Nov-03)
REMARKS	Hand augered to 5 fbg.		

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	SOIL DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
				0.6			Asphalt.	0.6	<p>Portland Type I/II</p> <p>Bentonite Seal</p> <p>Lonestar Sand #2/12 4"-diam., 0.010" Slotted Schedule 40 PVC</p> <p>Bottom of Boring @ 32 ft</p>
				3.0	GW		Well Graded GRAVEL (GW); Brown; loose; dry; 20% coarse sand, 80% angular gravel.	3.0	
				5			CLAY (CL); Black; very stiff; dry; 100% clay, no fines.		
0		MW-10-5'		5					
				10	CL				
0.1		MW-10-10'		10					
				15			Silty CLAY; gray; very stiff; dry; 30% silt, 70% clay.		
3.5		MW-10-15'		15					
				17.5			Clayey SILT (ML); Light olive gray; very dense; dry; 30% clay, 70% silt.	17.5	
8		MW-10-20'		20	ML				
				22.5			Clayey GRAVEL (GC); Light olive gray; medium dense; moist to wet 30: clay, 70% gravel.	22.5	
24		MW-10-25'		25	GC				
				25.0			Silty GRAVEL (GM); Light olive gray; medium dense; wet; 10% clay, 25% silt, 10% sand, 55% gravel.	25.0	
				27.5			Clayey SILT (ML); Grayish brown; medium dense; wet; 20% clay, 80% silt.	27.5	
111		MW-10-30'		30	ML				
104		MW-10-31.5'		31.5					
				32.0					
				35					

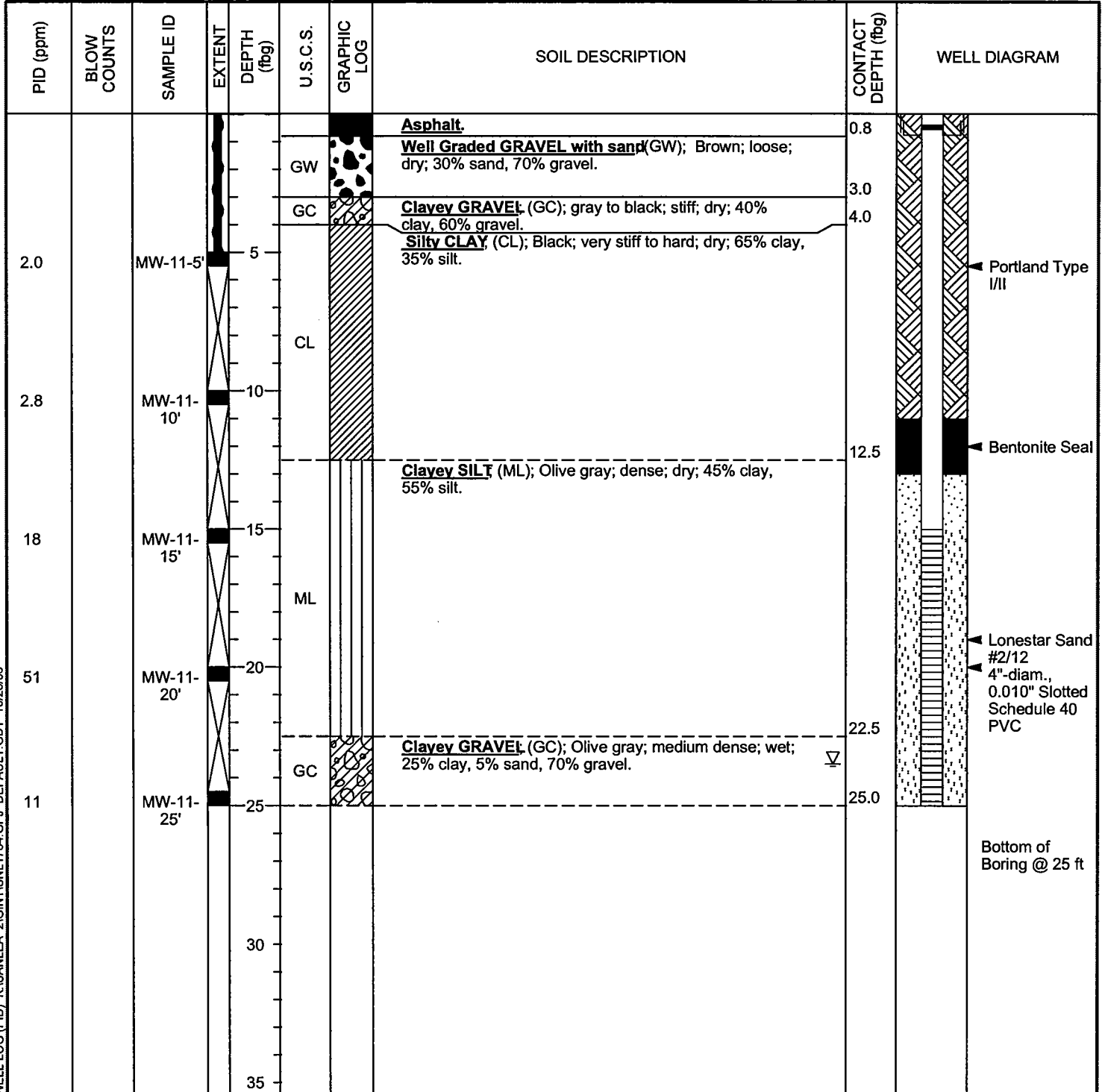
WELL LOG (PID) K:\SANLEA-2\GINTS\NL1784.GPJ DEFAULT.GDT 10/26/06



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BORING/WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	MW-11
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	20-Nov-03
LOCATION	San Leandro, California	DRILLING COMPLETED	20-Nov-03
PROJECT NUMBER	248-0612-008	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	45.94 ft above msl
DRILLING METHOD	Hollow-stem auger	TOP OF CASING ELEVATION	45.58 ft above msl
BORING DIAMETER	10"	SCREENED INTERVAL	15 to 25 fbg
LOGGED BY	S. Dalie	DEPTH TO WATER (First Encountered)	23.5 ft (20-Nov-03)
REVIEWED BY	M. Derby, PE# 55475	DEPTH TO WATER (Static)	NA
REMARKS	Hand augered to 5 fbg.		



WELL LOG (PID) K:\SANLEA-2\GINT\SNL1784.GPJ DEFAULT.GDT 10/26/06



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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	SB-17
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	13-Sep-04
LOCATION	San Leandro, California	DRILLING COMPLETED	13-Sep-04
PROJECT NUMBER	240612	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	NA
DRILLING METHOD	Hydraulic push	TOP OF CASING ELEVATION	NA
BORING DIAMETER	2"	SCREENED INTERVALS	NA
LOGGED BY	S Dalie	DEPTH TO WATER (First Encountered)	34.00 fbg
REVIEWED BY	M Derby, PE# 55475	DEPTH TO WATER (Static)	28.5 fbg (13-Sep-04)
REMARKS	Hand augered to 5 fbg		

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT DEPTH (fbg)	U S C S	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
						Asphalt	0.6	
				GM		Silty GRAVEL with clay, (GM) , Black very stiff, dry, 15% clay, 25% silt, 60% gravel no plasticity	2.5	
		SB 17 5	5	CL		Silty CLAY (CL) , Black, very stiff, dry, 85% clay, 15% silt, low to medium plasticity		
0		SB 17 10	10					
				ML		Sandy SILT (ML) , Olive brown dense, dry, 5% clay, 70% silt, 25% sand, no plasticity	13.5	
0		SB 17 15	15	SM		Silty SAND with Gravel, (SM) , Olive brown, very dense, dry 25% silt, 60% sand 15% gravel no plasticity	15.5	
						Silty CLAY with gravel (CL) Dark olive brown, very stiff dry 70% clay, 20% silt, 10% gravel, no plasticity	18.0	← Portland Type I/II Cement
			20					

WELL LOG (PID) I \SHELL\6 CHARS\2406-1240612-1240612-11SNL1784 GPJ DEFAULT GDT 6/10/09

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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	SB-17
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	13-Sep-04
LOCATION	San Leandro, California	DRILLING COMPLETED	13-Sep-04

Continued from Previous Page

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U S C S	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
0		SB 17 20			CL				
0		SB 17 25		25	ML		Clayey SILT (ML) , Brownish gray very stiff, dry, 60% clay, 30% silt, 10% gravel low plasticity	24 0	
							No recovery	28 0	
0		SB 17 35 5		35	GC		Clayey Gravel with sand (GC) , brownish gray, medium dense, wet 25% clay, 15% sand, 70% gravel, no plasticity	32 0	
								36 0	Bottom of Boring @ 36 fbg

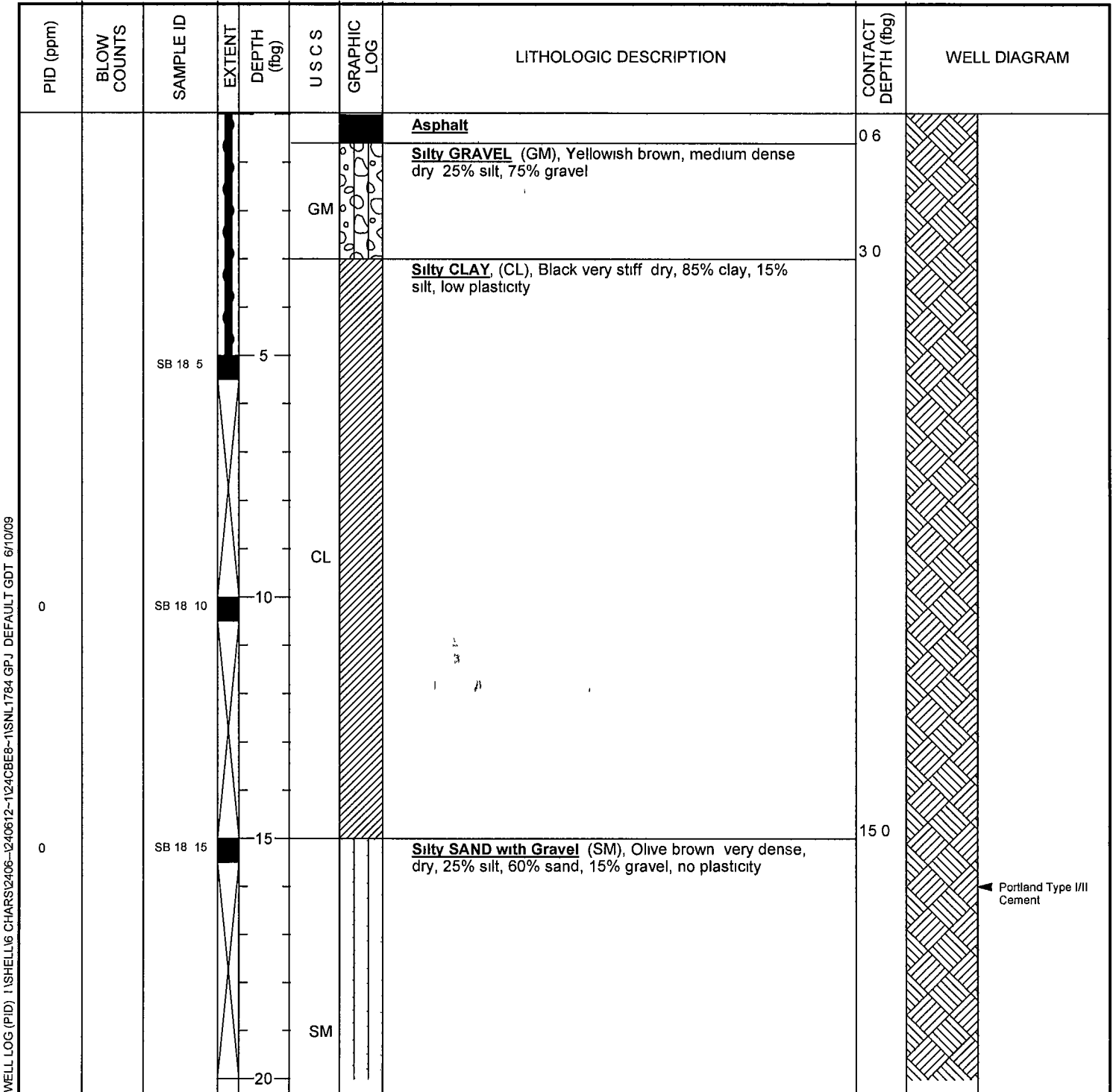
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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	SB-18
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	13-Sep-04
LOCATION	San Leandro, California	DRILLING COMPLETED	13-Sep-04
PROJECT NUMBER	240612	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	NA
DRILLING METHOD	Hydraulic push	TOP OF CASING ELEVATION	NA
BORING DIAMETER	2"	SCREENED INTERVALS	NA
LOGGED BY	S Dale	DEPTH TO WATER (First Encountered)	32 00 fbg (13-Sep-04) ▼
REVIEWED BY	M Derby, PE# 55475	DEPTH TO WATER (Static)	27 6 fbg (13-Sep-04) ▼
REMARKS	Hand augered to 5 fbg		



WELL LOG (PID) 1\SHELL\6 CHARS\2406-1240612-124CBE8-11SNL1784 GPJ DEFAULT.GDT 6/10/09

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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	SB-18
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	13-Sep-04
LOCATION	San Leandro, California	DRILLING COMPLETED	13-Sep-04

Continued from Previous Page

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U S C S	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
0		SB 18 20							
				22.7			Well graded SAND (SW) , Olive medium dense damp 5% clay, 90% sand, no plasticity		
				24.0	SW		No Recovery		
0		SB 18 25		25					
								28.0	
					CL		Silty CLAY (CL) , Olive brown very stiff dry 60% clay, 40% silt, low plasticity		
0		SB 18 30		30				30.3	
							Clayey Gravel with sand (GC) brownish gray, medium dense, wet, 35% clay, 15% sand, 50% gravel, no plasticity		
								32.0	
									Bottom of Boring @ 32 fbg

WELL LOG (PID) I:\SHELL16 CHARS\2406-1240812-124CBE8-1\SNL1784.GPJ DEFAULT GDT 6/10/09



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BORING/WELL LOG

CLIENT NAME Shell Oil Products Company (US) BORING/WELL NAME SB-19
 JOB/SITE NAME 1784 150th Avenue DRILLING STARTED 23-May-06
 LOCATION San Leandro, California DRILLING COMPLETED 24-May-06
 PROJECT NUMBER 248-0612-008 WELL DEVELOPMENT DATE (YIELD) NA
 DRILLER Gregg Drilling GROUND SURFACE ELEVATION Not Surveyed
 DRILLING METHOD Hydraulic push TOP OF CASING ELEVATION Not Surveyed
 BORING DIAMETER 3.25" SCREENED INTERVAL NA
 LOGGED BY B. DeBoer DEPTH TO WATER (First Encountered) 28.0 ft (24-May-06) ▽
 REVIEWED BY A. Cool DEPTH TO WATER (Static) NA ▾

REMARKS Hand augered to 5' bgs.

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (ft)	U.S.C.S.	GRAPHIC LOG	SOIL DESCRIPTION	CONTACT DEPTH (ft)	WELL DIAGRAM
				0.8			ASPHALT	0.8	
				3.0	GW		Well Graded GRAVEL with sand [GW]; 10YR 3/3, brown; dry; 30% sand, 70% gravel.	3.0	
				4.0	SM		Silty SAND with GRAVEL [SM]; 10YR 4/4, dark yellowish brown; dry; 10% clay, 30% silt, 35% medium sand, 25% fine gravel.	4.0	
0		SB-19-5		5.0			Gravelly SILT with sand [ML]; 10YR 4/4, dark yellowish brown; dry; 20% clay, 50% silt, 15% medium sand, 15% fine gravel.	6.0	
				6.0			SILT [ML]; 10YR 4/2, dark grayish brown; dry; 25% clay, 70% silt, 5% medium sand; medium plasticity.	6.0	
0		SB-19-10		10.0				12.0	
				12.0			SILT [ML]; 10YR 4/2, dark grayish brown; dry; 15% clay, 75% silt, 10% medium sand; medium plasticity.	12.0	
18		SB-19-15		15.0	ML		SILT with sand [ML]; GLEY1 4/5G, dark greenish gray; dry; 10% clay, 70 % silt, 20% medium sand; medium plasticity.	15.0	
2		SB-19-19.5		20.0				15.0	
				24.0			SILT with sand [ML]; GLEY1 4/5G, dark greenish gray; moist; 60% silt, 40% medium sand; medium plasticity.	24.0	
33		SB-19-25		25.0				26.0	
				26.0			SILT with sand [ML]; GLEY1 4/5G, dark greenish gray; moist; 80% silt, 20% medium sand; medium plasticity.	26.0	
				28.0	SM		Silty SAND [SM]; 10YR 4/3, brown; wet; 15% silt, 75% coarse sand, 10% fine gravel.	28.0	
86		SB-19-28.5		28.5	ML		SILT with sand [ML]; GLEY1 4/5G, dark greenish gray; moist; 80% silt, 20% medium sand; medium plasticity.	28.8	
				30.0				30.0	
				35.0				35.0	

WELL LOG (PID) K:\SANLEA-2\GINT\SNL1784.GPJ DEFAULT.GDT 11/3/06

Bottom of Boring @ 30 ft



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BORING/WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	SB-20
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	23-May-06
LOCATION	San Leandro, California	DRILLING COMPLETED	25-May-06
PROJECT NUMBER	248-0612-008	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	Not Surveyed
DRILLING METHOD	Hydraulic push	TOP OF CASING ELEVATION	Not Surveyed
BORING DIAMETER	3.25"	SCREENED INTERVAL	NA
LOGGED BY	B. DeBoer	DEPTH TO WATER (First Encountered)	23.0 ft (25-May-06)
REVIEWED BY	A. Cool	DEPTH TO WATER (Static)	NA
REMARKS	Hand augered to 5 fbg		

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	SOIL DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
				0.5			Asphalt SILT [ML]; 10YR 2/1, black; dry; 10% clay, 80% silt, 10% fine sand; medium plasticity.	0.5	
45		SB-20-5		5	ML		SILT [ML]; 10YR 2/1, black; dry; 15% clay, 75% silt, 5% fine sand, 5% fine gravel; medium plasticity.		
22		SB-20-10		10			Sandy SILT [ML]; GLEY1 5/5G, greenish gray; dry; 70% silt, 30% fine sand; low plasticity.	13.0	
				15					
20		SB-20-16.5		17.0	SM		Silty SAND with grave [SM]; 10YR 2/1, black; moist; 20% silt, 65% coarse sand, 15% fine gravel.	18.0	
				20	ML		Sandy SILT [ML]; GLEY1 5/5G, greenish gray; dry; 70% silt, 30% fine sand; low plasticity.		
				23.0				23.0	
108		SB-20-23.5		25	SP SM		Poorly-graded SAND with sil [SP-SM]; GLEY1 5/5G, greenish gray; wet; 10% silt, 80% fine sand; 10% fine gravel; low plasticity.		
				27.0					
				30.0	CL		CLAY [CL]; GLEY1 5/5GY, greenish gray; dry; 70% clay, 30% silt; high plasticity.		
				35					Bottom of Boring @ 30 ft

WELL LOG (PID) K:\SANLEA-2\GINTS\NL1784.GPJ DEFAULT.GDT 11/9/06



CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	SB-21
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	23-May-06
LOCATION	San Leandro, California	DRILLING COMPLETED	24-May-06
PROJECT NUMBER	248-0612-008	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	Not Surveyed
DRILLING METHOD	Hydraulic push	TOP OF CASING ELEVATION	Not Surveyed
BORING DIAMETER	3.25"	SCREENED INTERVAL	NA
LOGGED BY	B. DeBoer	DEPTH TO WATER (First Encountered)	27.0 ft (24-May-06)
REVIEWED BY	A. Cool	DEPTH TO WATER (Static)	NA
REMARKS	Had augered to 5 fbg		

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	SOIL DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
				0.3			Concrete	0.3	
21		SB-21-5		5			SILT [ML]; 10YR 2/1, black; dry; 10% clay, 80% silt, 10% fine sand; medium plasticity.		
16		SB-21-10		10	ML		SILT [ML]; 10YR 2/1, black; dry; 15% clay, 75% silt, 10% fine sand, 10% fine gravel; medium plasticity.	10.0	
10		SB-21-15		15			Sandy SILT [ML]; GLEY1 5/5G, greenish gray; dry; 70% silt, 30% fine sand; low plasticity.	13.0	
27		SB-21-20		20			Silty SAND [SM]; GLEY1 5/5G, greenish gray; moist; 20% silt, 80% fine sand; medium plasticity.	22.0	
124		SB-21-27.5		27.5	SM		Silty SAND [SM]; GLEY1 5/5G, greenish gray; wet; 15% silt, 75% fine sand, 10% fine gravel.	28.0	Bottom of Boring @ 28 ft

WELL LOG (PID) K:\SANLEA-2\GINTS\NL1784.GPJ DEFAULT.GDT 11/3/06



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BORING/WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	SB-22
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	23-May-06
LOCATION	San Leandro, California	DRILLING COMPLETED	25-May-06
PROJECT NUMBER	248-0612-008	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	Not Surveyed
DRILLING METHOD	Hydraulic push	TOP OF CASING ELEVATION	Not Surveyed
BORING DIAMETER	3.25"	SCREENED INTERVAL	NA
LOGGED BY	B. DeBoer	DEPTH TO WATER (First Encountered)	NA
REVIEWED BY	A. Cool	DEPTH TO WATER (Static)	NA
REMARKS	Hand augered to 5' bgs.		

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (ftg)	U.S.C.S.	GRAPHIC LOG	SOIL DESCRIPTION	CONTACT DEPTH (ftg)	WELL DIAGRAM
				0.8			ASPHALT	0.8	
				3.0	GW		Well Graded GRAVEL with sand [GW]; 10YR 4/3, brown; dry; 30% sand, 70% fine gravel.	3.0	
				5.0	SM		Silty SAND with GRAVEL [SM]; 10YR 4/4, dark yellowish brown; dry; 10% clay, 30% silt, 35% medium sand, 25% fine gravel.	5.0	
0		SB-22-5		5			Gravelly SILT with sand [ML]; 10YR 4/4, dark yellowish brown; dry; 20% clay, 50% silt, 15% medium sand, 15% fine gravel.	7.0	
				10			SILT [ML]; 10YR 4/2, dark grayish brown; dry; 25% clay, 70% silt, 5% medium sand; medium plasticity.	10	
0		SB-22-10		10			SILT [ML]; 10YR 4/2, dark grayish brown; dry; 15% clay, 75% silt, 10% medium sand; medium plasticity.	12.0	
				15				15	
0		SB-22-15		15	ML			15	
				20			SILT with sand [ML]; GLEY1 4/5G, dark greenish gray; dry; 10% clay, 70 % silt, 20% medium sand; medium plasticity.	20.0	
0		SB-22-20		20			SILT [ML]; 10YR 5/3, brown; dry; 25% clay, 70% silt, 5% fine sand; medium plasticity.	24.0	
				25				25	
0		SB-22-25		25				25	
				30				30.0	
0		SB-22-29.5		30				30.0	Bottom of Boring @ 30 ft
				35					

WELL LOG (PID) K:\SANLEA-2\GINT\SNL1784.GPJ DEFAULT.GDT 10/26/06



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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	SB-23
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	23-May-06
LOCATION	San Leandro, California	DRILLING COMPLETED	24-May-06
PROJECT NUMBER	240612	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	NA
DRILLING METHOD	Hydraulic push	TOP OF CASING ELEVATION	NA
BORING DIAMETER	3 25"	SCREENED INTERVALS	NA
LOGGED BY	B DeBoer	DEPTH TO WATER (First Encountered)	15 50 fbg
REVIEWED BY	A Cool	DEPTH TO WATER (Static)	NA
REMARKS	Hand augered to 5 fbg		

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U S C S	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
				0			Asphalt	0 5	
74		SB 23 5		5			SILT with sand [ML] , 10YR 4/3, brown, dry 15% clay, 60% silt, 20% fine sand, 5% fine gravel, low plasticity		
					ML		SILT [ML] 10YR 3/1, very dark gray, dry 10% clay 80% silt 10% fine sand, medium plasticity	7 0	
							Sandy SILT with gravel [ML] 10YR 2/1, black moist, 45% silt, 35% fine sand 20% fine gravel	9 0	
98		SB 23 10		10			SILT [ML] , 10YR 2/1, black, dry, 10% clay, 80% silt, 10% fine sand, medium plasticity	10 0	
					GM		Silty GRAVEL with sand [GM] , 10YR 3/1, very dark gray wet, 35% silt, 25% coarse sand, 40% fine gravel	15 0	
58		SB 23 15		15					
					SP SM		Poorly-graded SAND with silt [SP-SM] 10YR 5/4, yellowish brown, moist, 10% silt, 90% fine sand	17 0	
					SM		Silty SAND [SM] 10YR 5/4, yellowish brown dry, 20% silt, 80% fine sand	19 0	
				20				20 0	

WELL LOG (PID) I \SHELL\6 CHARS\2406-1240612-1\24CBE8-1\SNL-1784 GPJ DEFAULT.GDT 6/10/09

Continued Next Page



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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	SB-23
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	23-May-06
LOCATION	San Leandro, California	DRILLING COMPLETED	24-May-06

Continued from Previous Page

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U S C S	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
13		SB 23 20			ML		<u>SILT</u> [ML] 10YR 4/3, brown, dry, 10% clay, 80% silt, 10% fine sand, medium plasticity		
82		SB 23 25		25	SM		<u>Silty SAND</u> [SM], 10YR 5/4, yellowish brown, dry, 20% silt 80% fine sand	24 0	
204		SB 23 29 5		30	ML		<u>SILT</u> [ML], 10YR 2/1, black dry 10% clay, 80% silt, 10% fine sand medium plasticity	26 0	
								30 0	Bottom of Boring @ 30 fbg

WELL LOG (PID) | \SHELL16 CHARS\2406-0240612-1\24CBE8-1\SNL1784 GPJ DEFAULT GDT 6/10/09



CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	MW-12
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	23-May-06
LOCATION	San Leandro, California	DRILLING COMPLETED	26-Feb-06
PROJECT NUMBER	248-0612-008	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	44.46 ft above msl
DRILLING METHOD	Hollow-stem auger	TOP OF CASING ELEVATION	44.10 ft above msl
BORING DIAMETER	8"	SCREENED INTERVAL	18 to 28 fbg
LOGGED BY	B. DeBoer	DEPTH TO WATER (First Encountered)	24.0 ft (26-May-06)
REVIEWED BY	A. Cool	DEPTH TO WATER (Static)	NA
REMARKS	Air Knife to 5 fbg		

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	SOIL DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
				0.6			Asphalt	0.6	<p>Portland Type I/II</p> <p>Bentonite Seal</p> <p>Monterey Sand # 1/20</p> <p>2"-diam., 0.010" Slotted Schedule 40 PVC</p> <p>Bottom of Boring @ 30 ft</p>
				1.6			Baserock	1.6	
				5			SILT [ML]; 10YR 2/1, black; dry; 30% clay, 70% silt; medium plasticity.		
6		SB-24-5		5					
				10					
9		SB-24-10		10					
				12.0	ML		SILT [ML]; 10YR 3/1, very dark gray with green mottling; dry; 40% clay, 60% silt; medium plasticity.	12.0	
				15					
0		SB-24-15		15			SILT [ML]; GLEY1 4/10Y, dark greenish gray; dry; 10% clay, 80% silt, 10% fine sand; low plasticity.	16.0	
				16.0				16.0	
				20					
451		SB-24-20		20			SILT with sand [ML]; GLEY1 4/10Y dark greenish gray; moist; 10% clay, 65% silt, 25% fine sand; medium plasticity.	22.0	
				23.0			SAND with silt and grave [SM]; GLEY1 4/10Y, very dark greenish gray; wet; 15% silt, 65% coarse sand, 20% fine gravel.	23.0	
869		SB-24-24		25	SM			23.0	
				27.0			CLAY [CL]; GLEY1 4/5GY, very dark greenish gray; moist; 60% clay, 40% silt; high plasticity.	27.0	
				27.0	CL			27.0	
419				30				30.0	
				35					

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BORING/WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	SVP-1
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	27-Aug-07
LOCATION	San Leandro, California	DRILLING COMPLETED	28-Aug-07
PROJECT NUMBER	240612	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	Not Surveyed
DRILLING METHOD	Hand Auger	TOP OF CASING ELEVATION	Not Surveyed
BORING DIAMETER	3.5"	SCREENED INTERVAL	4.6 to 4.9 fbg
LOGGED BY	S. Lewis	DEPTH TO WATER (First Encountered)	NA
REVIEWED BY	A. Friel, PG 6452	DEPTH TO WATER (Static)	NA
REMARKS			

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	SOIL DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
					ASPHALT		ASPHALT	0.7	<p>Bentonite Slurry with Pellet Base</p> <p>1/4" - Diameter Teflon Tubing</p> <p>2/16 Sand</p> <p>3" - length Stainless Steel Screen</p> <p>Bottom of Boring @ 5.2 ft</p>
					SM		Silty SAND with Gravel (SM) ; yellowish brown (10YR 5/4); dry to moist; 15% silt, 65% fine to coarse sand, 20% fine gravel. @ 1' - 15% silt, 70% fine to coarse sand, 15% fine gravel.	2.5	
					ML		SILT (ML) ; very dark gray (10YR 3/1); moist; 30% clay, 70% silt; medium plasticity.	5.2	
0.0		SVP-1-4.5'		5					
				10					

WELL LOG (PID) I:\SONOMA-1\SHEISANLEA-2\GINTS\NL1784.GPJ DEFAULT.GDT 10/3/07



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BORING/WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	SVP-2
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	28-Aug-07
LOCATION	San Leandro, California	DRILLING COMPLETED	28-Aug-07
PROJECT NUMBER	240612	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	Not Surveyed
DRILLING METHOD	Hand Auger	TOP OF CASING ELEVATION	Not Surveyed
BORING DIAMETER	3.5"	SCREENED INTERVAL	4.6 to 4.9 fbg
LOGGED BY	S. Lewis	DEPTH TO WATER (First Encountered)	NA
REVIEWED BY	A. Friel, PG 6452	DEPTH TO WATER (Static)	NA
REMARKS			

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	SOIL DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
					ASPHALT		ASPHALT	0.7	<p>Bentonite Slurry with Pellet Base</p> <p>1/4" - Diameter Teflon Tubing</p> <p>2/16 Sand</p> <p>3" - length Stainless Steel Screen</p> <p>Bottom of Boring @ 5.2 ft</p>
					SM		Silty SAND with Gravel (SM) ; olive (5Y 4/3); dry to moist; 15% silt, 60% fine to coarse sand, 25% fine gravel. Silty SAND (SM) ; olive (5Y 4/3); dry; 15% silt, 80% fine to coarse sand, 5% fine gravel.	4.5	
0.0		SVP-2-4.5'		5	ML		SILT (ML) ; very dark grayish brown (10YR 3/2); moist; 15% clay, 80% fine to coarse sand, 5% fine to coarse sand; low plasticity.	5.2	
				10					

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BORING/WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	SVP-3
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	28-Aug-07
LOCATION	San Leandro, California	DRILLING COMPLETED	28-Aug-07
PROJECT NUMBER	240612	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	Not Surveyed
DRILLING METHOD	Hand Auger	TOP OF CASING ELEVATION	Not Surveyed
BORING DIAMETER	3.5"	SCREENED INTERVAL	4.6 to 4.9 fbg
LOGGED BY	S. Lewis	DEPTH TO WATER (First Encountered)	NA
REVIEWED BY	A. Friel, PG 6452	DEPTH TO WATER (Static)	NA
REMARKS			

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	SOIL DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
					ASPHALT		ASPHALT	0.7	<p>Bentonite Slurry with Pellet Base</p> <p>1/4" - Diameter Teflon Tubing</p> <p>2/16 Sand</p> <p>3" - length Stainless Steel Screen</p> <p>Bottom of Boring @ 5.2 ft</p>
					ML		SILT (ML) ; very dark grayish brown (10YR 3/2); moist; 20% clay, 75% silt, 5% fine to coarse sand; low plasticity.	1.0	
					SM		Silty SAND with Gravel (SM) ; light brownish gray (2.5Y 6/2); dry; 15% silt, 70% fine to coarse sand, 15% fine gravel.		
0.0		SVP-3-4.5'		5				5.0	
				10					

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BORING/WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	SVP-4
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	28-Aug-07
LOCATION	San Leandro, California	DRILLING COMPLETED	28-Aug-07
PROJECT NUMBER	240612	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	Not Surveyed
DRILLING METHOD	Hand auger	TOP OF CASING ELEVATION	Not Surveyed
BORING DIAMETER	3.5"	SCREENED INTERVAL	4.6 to 4.9 fbg
LOGGED BY	S. Lewis	DEPTH TO WATER (First Encountered)	2.5 ft (28-Aug-07)
REVIEWED BY	A. Friel, PG 6452	DEPTH TO WATER (Static)	NA
REMARKS			

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	SOIL DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
					CONCRETE		CONCRETE	0.5	<p>Bentonite Slurry with Pellet Base</p> <p>1/4" - Diameter Teflon Tubing</p> <p>2/16 Sand</p> <p>3" - length Stainless Steel Screen</p> <p>Bottom of Boring @ 5.4 ft</p>
6.3					SM		Silty SAND with Gravel (SM) ; light olive brown (2.5Y 5/4); dry to moist; 15% silt, 60% fine to coarse sand, 25% fine gravel. @ 1' - moist. @ 2.5' - wet; perched.	3.0	
623		SVP-4-4.5'			ML		SILT (ML) ; very dark grayish brown (10YR 3/2); moist; 25% clay, 70% silt, 5% fine to coarse sand; medium plasticity. @ 4' - dark greenish gray (10Y 4/1).	5.4	
				10					

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BORING/WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	SVP-5
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	28-Aug-07
LOCATION	San Leandro, California	DRILLING COMPLETED	28-Aug-07
PROJECT NUMBER	240612	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	Not Surveyed
DRILLING METHOD	Hand Auger	TOP OF CASING ELEVATION	Not Surveyed
BORING DIAMETER	3.5"	SCREENED INTERVAL	4.6 to 4.9 fbg
LOGGED BY	S. Lewis	DEPTH TO WATER (First Encountered)	NA
REVIEWED BY	A. Friel, PG 6452	DEPTH TO WATER (Static)	NA

REMARKS

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	SOIL DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
					CONCRETE		CONCRETE	0.5	<p>Bentonite Slurry with Pellet Base</p> <p>1/4" - Diameter Teflon Tubing</p> <p>2/16 Sand</p> <p>3" - length Stainless Steel Screen</p> <p>Bottom of Boring @ 5.2 ft</p>
					SM		Silty SAND with Gravel (SM) ; dark yellowish brown (10YR 3/4); dry to moist; 15% silt, 60% fine to coarse sand, 25% fine gravel.	1.0	
					ML		SILT (ML) ; very dark gray (10YR 3/1); moist; 25% clay, 75% silt; medium plasticity.		
1.4		SVP-5-4.5'		5				5.2	
				10					

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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	B-1
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	14-Sep-07
LOCATION	San Leandro, California	DRILLING COMPLETED	14-Sep-07
PROJECT NUMBER	240612	WELL DEVELOPMENT DATE (YIELD)	NA
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	NA
DRILLING METHOD	Hydraulic push	TOP OF CASING ELEVATION	NA
BORING DIAMETER	2	SCREENED INTERVALS	NA
LOGGED BY	L Goldfinch	DEPTH TO WATER (First Encountered)	NA
REVIEWED BY	A Friel, PG 6452	DEPTH TO WATER (Static)	NA
REMARKS	Hand augered to 5' bgs on 8/28/2007 Located between dispensers & station building		

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (ft)	U S C S	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (ft)	WELL DIAGRAM
							CONCRETE	0.5	
					SM		Silty SAND with Gravel (SM) , reddish brown (2.5Y 5/4) dry to moist, 15% silt, 60% fine to coarse sand, 25% fine gravel	3.0	
					ML		SILT (ML) very dark grayish brown (10YR 3/2), moist, 25% clay, 70% silt, 5% fine to coarse sand, medium plasticity	5.0	
486		B 15		5	ML		Gravelly SILT with Sand (ML) black (2.5Y 2.5/1), wet, 25% clay, 40% silt, 15% fine sand, 20% fine to medium gravel low plasticity	9.0	
78		B 110		10	ML		SILT (ML) , black (2.5Y 2.5/1), moist 30% clay, 65% silt 5% fine sand medium plasticity	12.0	
					ML		SILT with Gravel (ML) , dark gray (2.5Y 4/1), 30% clay, 55% silt, 5% fine sand, 10% fine to medium gravel	16.0	
106.5		B 115		15	ML		Gravelly SILT with Sand (ML) , dark gray (2.5Y 4/1) moist, 10% clay, 35% silt, 25% fine to coarse sand 30% fine to medium gravel, low plasticity	17.0	
83.3					ML		SILT (ML) olive gray (5Y 4/2), dry to moist, 5% clay, 90% silt, 5% fine sand	19.0	
865		B 117			ML		@18' - moist 30% clay, 65% silt, 5% fine sand medium plasticity	19.0	
					ML		SILT with Sand (ML) , olive gray (5Y 5/2) wet 15% clay, 65% silt, 20% fine to medium sand low plasticity	20.0	

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WELL LOG (PID) \1\SHELL116 CHARS\2406-1240612-1124CBE8-1\SNL1784 GPJ DEFAULT GDT 6/10/09



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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	B-1
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	14-Sep-07
LOCATION	San Leandro, California	DRILLING COMPLETED	14-Sep-07

Continued from Previous Page

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U S C S	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
9 289		B 1 2 0					Sandy SILT with Gravel (ML) olive gray (5Y 4/2) dry to moist 65% silt, 20% fine to coarse sand, 15% fine gravel		
1 342					ML	@ 21' - moist, 50% silt, 35% fine to coarse sand, 15% fine gravel	22 0		
5 172					ML	SILT (ML) , dry, 5% clay, 85% silt, 10% fine sand	24 0		
167 1		B 1 2 5		25		SILT with Sand (ML) , dark gray (2 5Y 4/1), moist to wet, 20% clay, 60% silt 15% fine to medium sand, 5% fine gravel			
6 783					ML	@ 27' - olive gray (5Y 5/2) dry, 5% clay, 75% silt, 10% fine to coarse sand, 10% fine gravel @ 28' - dark gray (5Y 4/1), moist to wet 20% clay, 55% silt, 15% fine to coarse sand, 10% fine gravel	29 0		
7 234		B 1 2 9 5		30	ML	SILT (ML) , grayish brown (2 5Y 5/2), dry, 20% clay, 75% silt, 5% fine sand	30 0	Bottom of Boring @ 30 fbg	

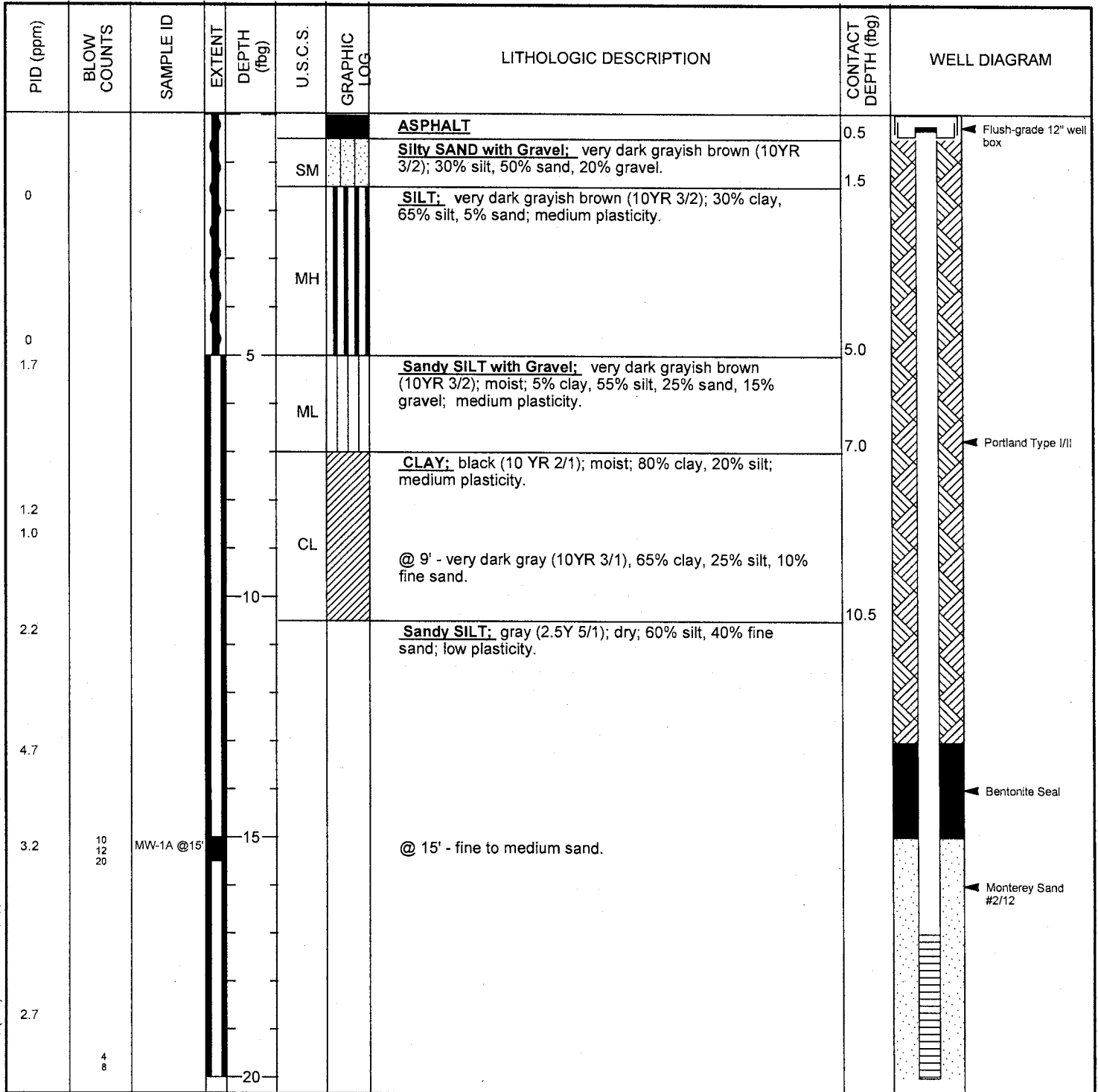
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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	MW-1A
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	26-Aug-08
LOCATION	San Leandro, California	DRILLING COMPLETED	02-Sep-08
PROJECT NUMBER	240612	WELL DEVELOPMENT DATE (YIELD)	15-Sep-08 (16 gallons)
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	49.41 ft above msl
DRILLING METHOD	Hollow-stem auger	TOP OF CASING ELEVATION	48.99 ft above msl
BORING DIAMETER	10"	SCREENED INTERVALS	17 to 27 fbg
LOGGED BY	E. Reinhart-Koylu	DEPTH TO WATER (First Encountered)	NA
REVIEWED BY	P. Schaefer	DEPTH TO WATER (Static)	23.78 fbg (15-Sep-08)
REMARKS	Air knife to 5 fbg		



WELL LOG (PID) I:\SHELL\6-CHARS\2406-1240612-SAN LEANDRO 1784 150TH\240612-GINTS\NL1784.GPJ DEFAULT.GDT. 2/6/09

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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	MW-1A
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	26-Aug-08
LOCATION	San Leandro, California	DRILLING COMPLETED	02-Sep-08

Continued from Previous Page

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
5.1	15 8 17 20	MW-1A @20'					@ 20' - 55% silt, 45% fine to coarse sand.		<p>4"-diam. .020" Slotted Schedule 40 PVC</p>
1.5									
1.3	7 16 19						@ 22' - grayish brown (10 YR 5/2); 70% silt, 30% fine to coarse sand.		
					ML				
				25			@ 25' - fine sand.		
3.5	9 13 13								
2.6	12 25 36								
167	6 12 24	MW-1A @26.5'						27.0	Bottom of Boring @ 27 fbg

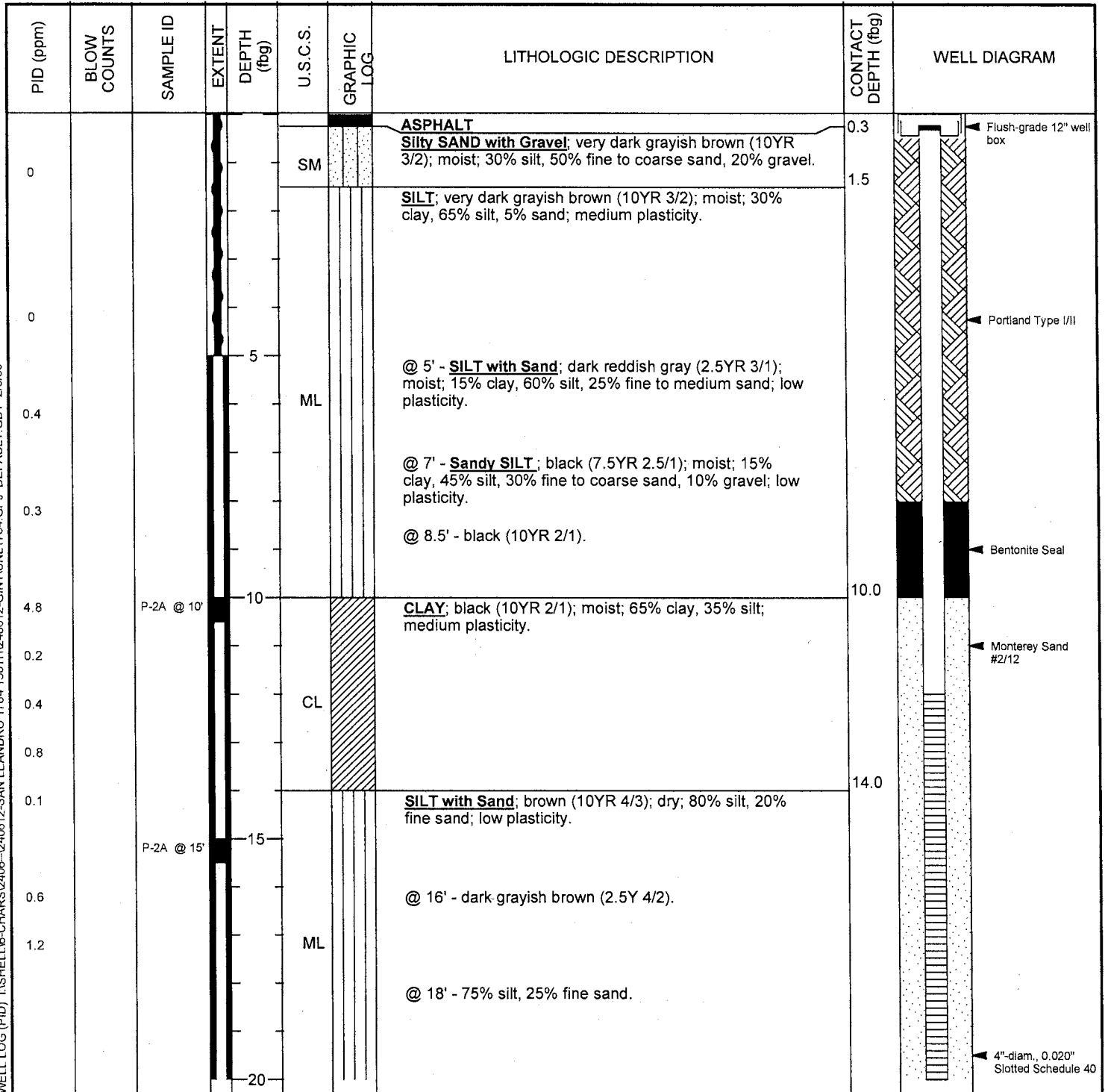
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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	P-2A
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	26-Aug-08
LOCATION	San Leandro, California	DRILLING COMPLETED	02-Sep-08
PROJECT NUMBER	240612	WELL DEVELOPMENT DATE (YIELD)	15-Sep-08 (21 gallons)
DRILLER	Gregg Drilling, C-57 #485165	GROUND SURFACE ELEVATION	49.29 ft above msl
DRILLING METHOD	Hollow-stem auger	TOP OF CASING ELEVATION	48.81 ft above msl
BORING DIAMETER	10"	SCREENED INTERVALS	12 to 27 fbg
LOGGED BY	E. Reinhart-Koylu	DEPTH TO WATER (First Encountered)	NA
REVIEWED BY	P. Schaefer	DEPTH TO WATER (Static)	23.58 fbg (15-Sep-08)
REMARKS	Air knife to 5 fbg		



WELL LOG (PID) I:\SHELL\6-CHARS\2406-1240612-SAN LEANDRO 1784 150TH\240612-GINT\SNL1784.GPJ DEFAULT.GDT 2/6/09

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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	P-2A
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	26-Aug-08
LOCATION	San Leandro, California	DRILLING COMPLETED	02-Sep-08

Continued from Previous Page

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
0.1							Sandy SILT with gravel ; grayish brown (2.5Y 5/2); dry; 55% silt, 30% fine sand, 15% gravel; low plasticity.		
0.6									
0.8							@ 22' - Sandy SILT ; grayish brown (2.5Y 5/2); dry; 65% silt, 35% fine sand; low plasticity.		
0.2					ML				
0				25			@ 25' - dark grayish brown (2.5Y 4/2).		
33.1							@ 26' - dark gray (5Y 4/1); 70% silt, 30% fine sand.	27.0	

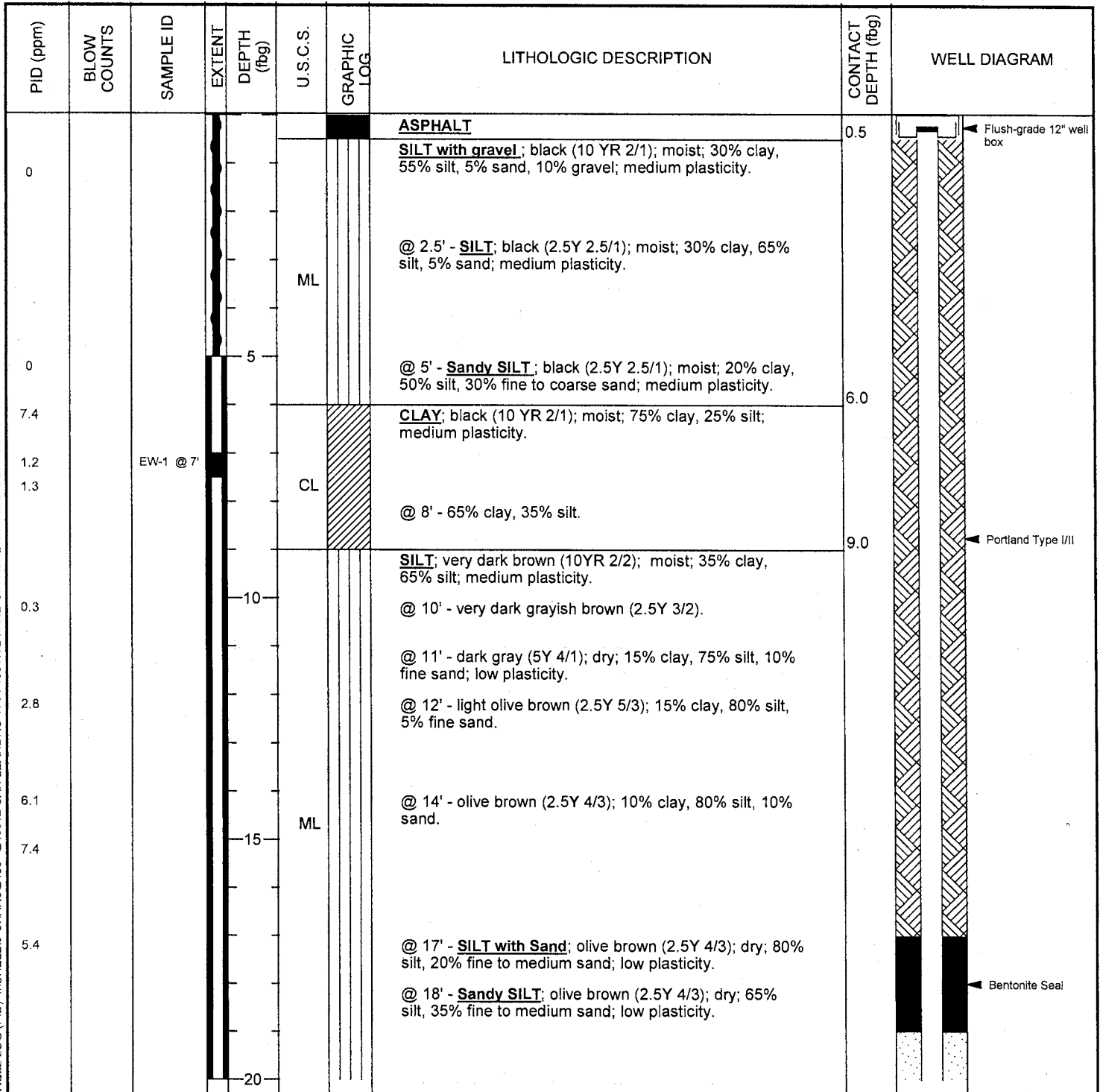
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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	EW-1
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	26-Aug-08
LOCATION	San Leandro, California	DRILLING COMPLETED	03-Sep-08
PROJECT NUMBER	240612	WELL DEVELOPMENT DATE (YIELD)	15-Sep-08 (75 gallons)
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	48.74 ft above msl
DRILLING METHOD	Hollow-stem auger	TOP OF CASING ELEVATION	48.44 ft above msl
BORING DIAMETER	10"	SCREENED INTERVALS	21 to 36 fbg
LOGGED BY	E. Reinhart-Koylu	DEPTH TO WATER (First Encountered)	33.00 fbg (03-Sep-08) ∇
REVIEWED BY	P. Schaefer	DEPTH TO WATER (Static)	23.26 fbg (15-Sep-08) ▼
REMARKS	Air knife to 5 fbg		



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WELL LOG (PID) I:\SHELL\6-CHARS\2406-1240612-SAN LEANDRO 1784 150TH\240612-GINTSNL.1784.GPJ DEFAULT.GDT 2/6/09



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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	EW-1
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	26-Aug-08
LOCATION	San Leandro, California	DRILLING COMPLETED	03-Sep-08

Continued from Previous Page

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
2.2		EW-1 @ 20'					@ 20' - SILT with Sand ; pale yellow (2.5Y 5/4); dry; 5% clay, 60% silt, 25% fine to medium sand, 10% fine gravel; low plasticity.		
4.2									
9.7					ML		@ 22' - Sandy SILT ; dark grayish brown (10YR 4/4); moist; 70% silt, 30% fine sand; medium plasticity.		
							@ 24' - SILT with Sand ; dark grayish brown (10YR 4/4); moist; 75% silt, 25% fine sand; medium plasticity.		
72				25					
137					SM		Silty SAND ; olive gray (5Y 4/2); moist; 20% silt, 80% fine to coarse angular sand.	26.0	
							SILT with Sand ; olive gray (5Y 5/2); moist; 80% silt, 20% fine to medium sand; medium plasticity.	26.5	
294							@ 28' - dark yellowish brown (10YR 4/2); dry.		
360		EW-1 @ 30'		30			@ 30' - brown (10 YR 5/3); dry; 5% clay, 85% silt, 15% sand.		
345					ML		@ 31' - dark gray (5Y 4/1).		
							@ 32' - Sandy SILT ; olive gray (5Y 4/2); moist; 65% silt, 35% fine to medium sand; low plasticity.		
276									
83.7		EW-1 @ 35'		35			@ 35' - dark gray (5Y 4/1).		
19.9							@ 35.5' - olive brown (2.5Y 4/3); dry.	36.0	
									Bottom of Boring @ 36 fbg

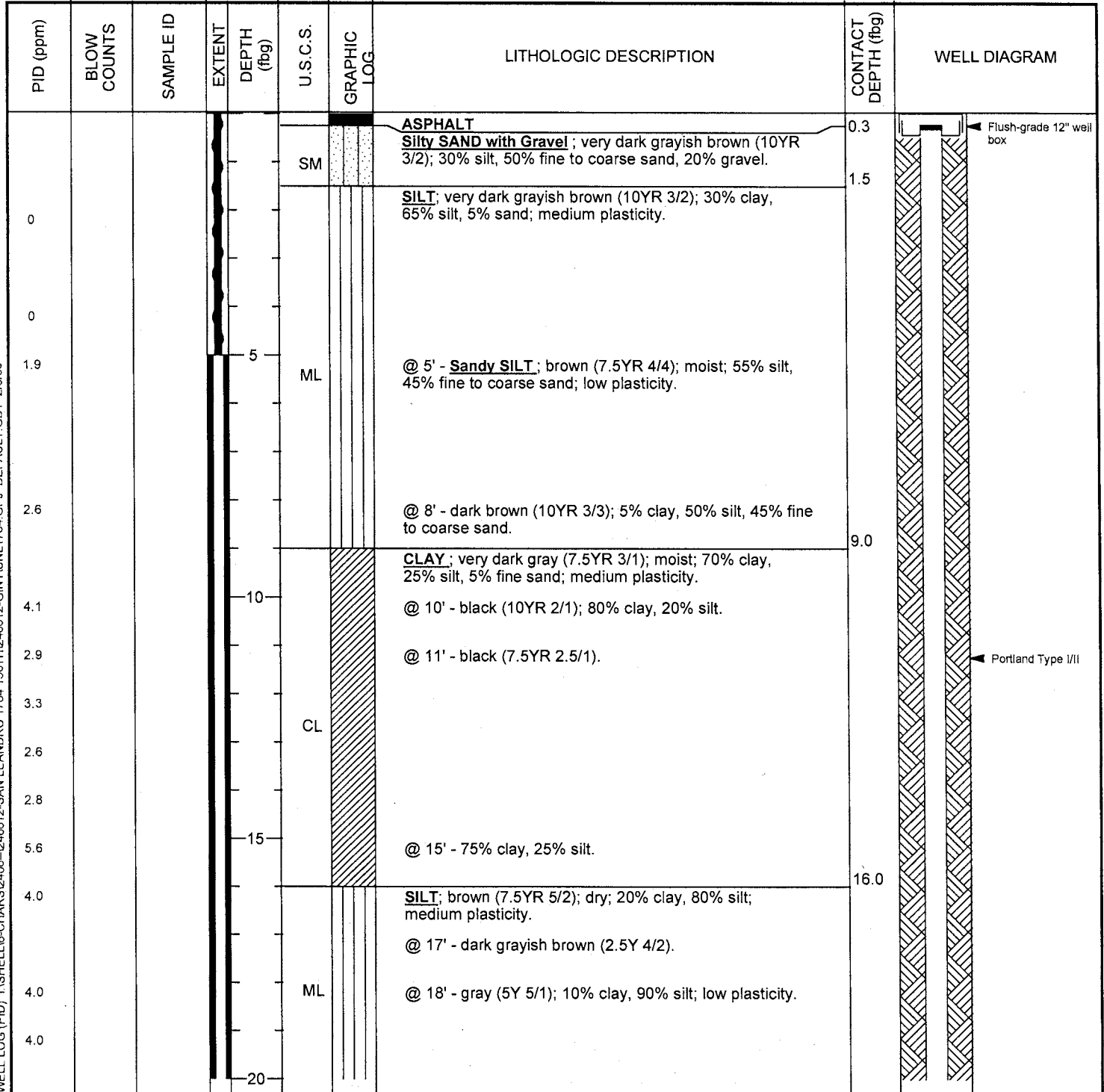
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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	P-2B
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	26-Aug-08
LOCATION	San Leandro, California	DRILLING COMPLETED	03-Sep-08
PROJECT NUMBER	240612	WELL DEVELOPMENT DATE (YIELD)	15-Sep-08 (65 gallons)
DRILLER	Gregg Drilling, C-57 #485165	GROUND SURFACE ELEVATION	49.45 ft above msl
DRILLING METHOD	Hollow-stem auger	TOP OF CASING ELEVATION	49.02 ft above msl
BORING DIAMETER	10"	SCREENED INTERVALS	26 to 36 fbg
LOGGED BY	E. Reinhart-Koylu	DEPTH TO WATER (First Encountered)	NA
REVIEWED BY	P. Schaefer	DEPTH TO WATER (Static)	23.40 fbg (15-Sep-08)
REMARKS	Air knife to 5 fbg		



WELL LOG (PID) I:\SHELL\6-CHARS\2406-12\40612-SAN LEANDRO 1784-150TH\240612-GINT\SNL1784.GPJ DEFAULT.GDT 2/6/09

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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	P-2B
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	26-Aug-08
LOCATION	San Leandro, California	DRILLING COMPLETED	03-Sep-08

Continued from Previous Page

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
2.0						@ 20' - dark gray (10YR 4/1); 5% clay, 85% silt, 10% fine to coarse sand.		
2.6						@ 22' - Sandy SILT ; dark gray (2.5Y 4/1); dry; 60% silt, 35% fine to coarse sand, 5% gravel; low plasticity.		
2.0						@ 23.5' - SILT ; grayish brown (10YR 5/2); dry; 15% clay, 85% silt; low plasticity.		
1.3			25			@ 25' - gray (10YR 5/1); 20% clay, 80% silt.		
18.3						@ 26' - dark grayish brown (2.5Y 4/2).		
92						@ 28' - gray (5Y 5/1); 15% clay, 85% silt.		
490		P-2B @ 29		ML		@ 29' - gray (2.5Y 5/1).		
236			30			@ 30' - SILT with Sand ; gray (10YR 5/1); dry; 5% clay, 75% silt, 20% fine sand; low plasticity.		
17						@ 33' - brown (10YR 5/3); moist; 5% clay, 70% silt, 25% sand; low plasticity.		
27						@ 34' - brown (7.5YR 4/3).		
37						@ 35' - brown (10YR 4/3); 20% clay, 60% silt, 20% fine sand.		
48		P-2B @ 35	35					
							36.0	Bottom of Boring @ 36 fbg

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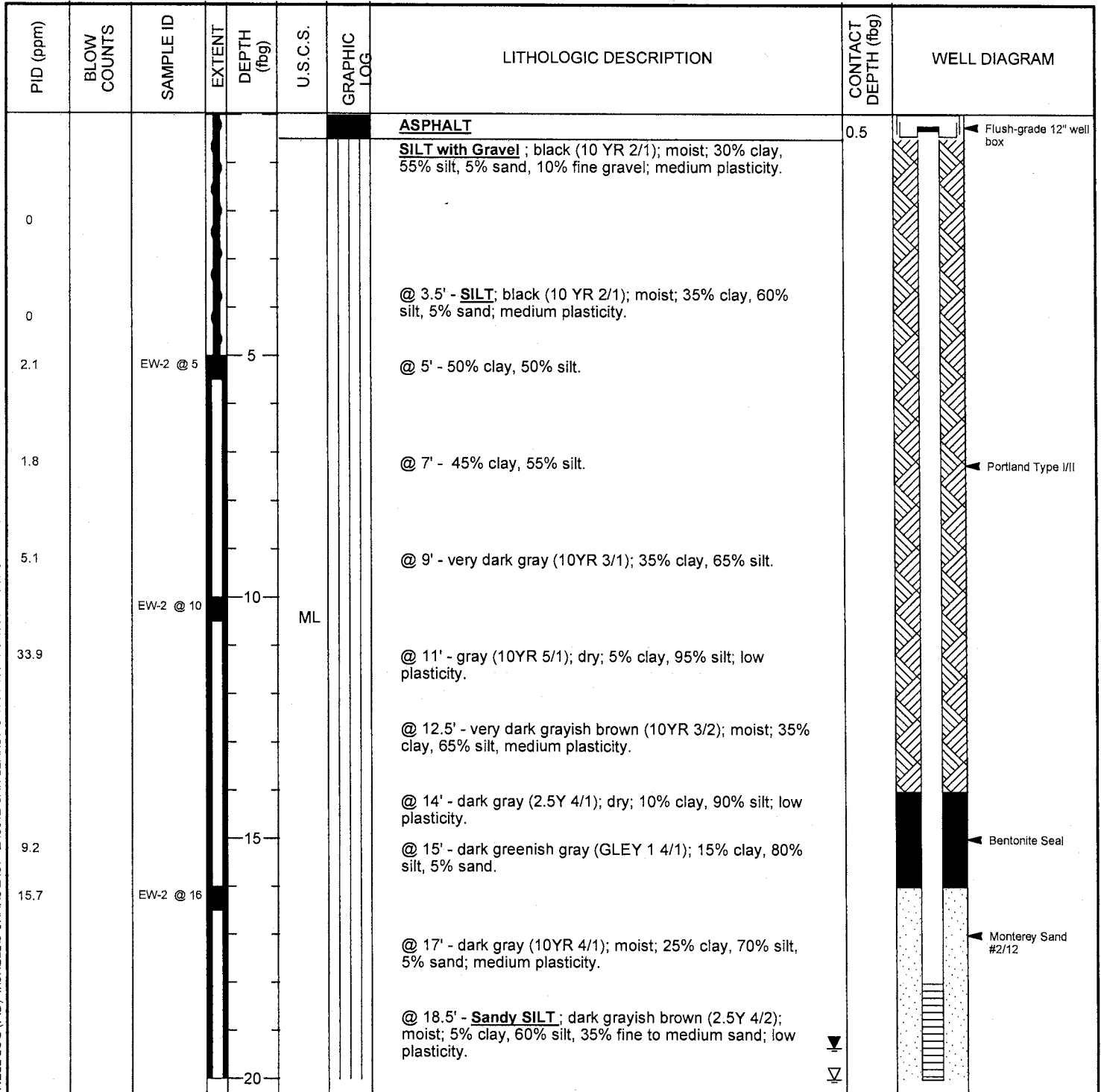


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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	EW-2
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	28-Aug-08
LOCATION	San Leandro, California	DRILLING COMPLETED	04-Sep-08
PROJECT NUMBER	240612	WELL DEVELOPMENT DATE (YIELD)	17-Sep-08 (88 gallons)
DRILLER	Gregg Drilling, C-57 #485165	GROUND SURFACE ELEVATION	45.29 ft above msl
DRILLING METHOD	Hollow-stem auger	TOP OF CASING ELEVATION	44.52 ft above msl
BORING DIAMETER	10"	SCREENED INTERVALS	18 to 33 fbg
LOGGED BY	E. Reinhart-Koylu	DEPTH TO WATER (First Encountered)	20.00 fbg (04-Sep-08) ▼
REVIEWED BY	P. Schaefer	DEPTH TO WATER (Static)	19.35 fbg (15-Sep-08) ▼
REMARKS	Air knife to 5 fbg		

WELL LOG (PID) \\SHELL\6-CHARS\2406-1240612-SAN LEANDRO 1784 150TH\240612-GINT\SNL-1784.GPJ DEFAULT.GDT 2/6/09



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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	EW-2
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	28-Aug-08
LOCATION	San Leandro, California	DRILLING COMPLETED	04-Sep-08

Continued from Previous Page

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
78.1		EW-2 @ 20			ML			21.0	<p>4" diam., 0.020" Slotted Schedule 40 PVC</p>
24.9					SM		@ 21' - Silty SAND ; olive gray (5Y 5/2); wet; 5% clay, 35% silt, 60% angular sand.	23.0	
224					ML		@ 23' - SILT ; olive brown (2.5Y 4/3); moist; 100% silt; low plasticity.	25.0	
225				25	CL		@ 25' - CLAY ; dark gray (5Y 4/1); moist; 65% clay, 35% silt; medium plasticity.	27.0	
357		EW-2 @ 27'					SILT ; dark gray (5Y 4/1); moist; 25% clay, 65% silt, 10% fine to medium sand; low plasticity.		
301				30	ML		@ 29' - pale yellow (2.5Y 5/4); dry; 5% clay, 95% silt. @ 30' - olive brown (2.5Y 4/3); 5% clay, 85% silt, 10% fine sand.		
66.5							@ 33' - SILT with Sand ; olive brown (2.5Y 4/4); moist; 5% clay, 80% silt, 15% fine sand; low plasticity.	34.0	
59.3		EW-2 @ 33.5							Bottom of Boring @ 34 fbg

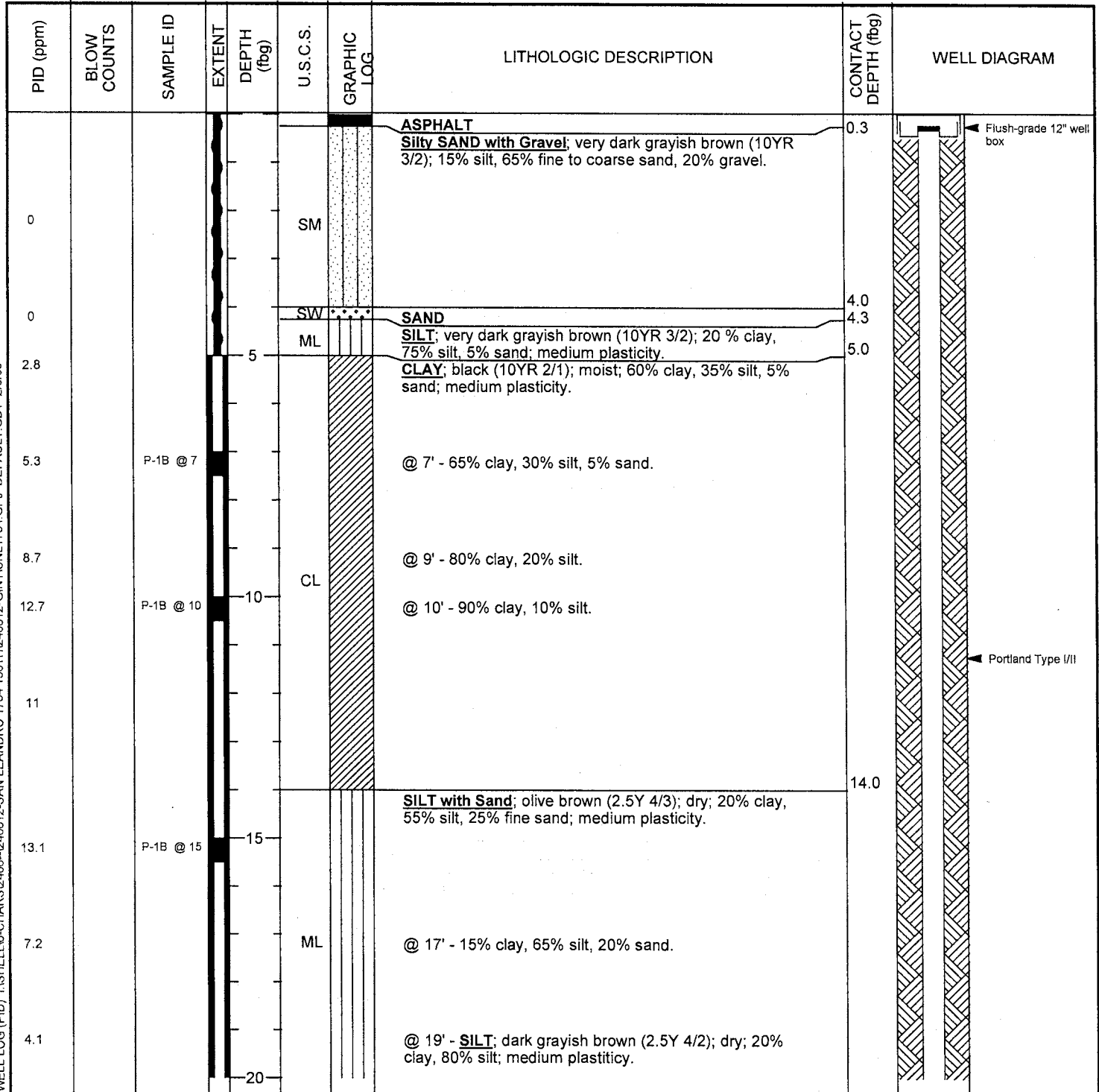
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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	P-1B
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	27-Aug-08
LOCATION	San Leandro, California	DRILLING COMPLETED	04-Sep-08
PROJECT NUMBER	240612	WELL DEVELOPMENT DATE (YIELD)	16-Sep-08 (82 gallons)
DRILLER	Gregg Drilling, C-57 #485165	GROUND SURFACE ELEVATION	47.99 ft above msl
DRILLING METHOD	Hollow-stem auger	TOP OF CASING ELEVATION	47.65 ft above msl
BORING DIAMETER	10"	SCREENED INTERVALS	26 to 36 fbg
LOGGED BY	E. Reinhart-Koylu	DEPTH TO WATER (First Encountered)	34.00 fbg (04-Sep-08) ▼
REVIEWED BY	P. Schaefer	DEPTH TO WATER (Static)	22.50 fbg (15-Sep-08) ▼
REMARKS	Air knife to 5 fbg		



WELL LOG (PID) I:\SHELL\6-CHARS\2406-1240612-SAN LEANDRO 1784 150TH\240612-GINT\SNL1784.GPJ DEFAULT.GDT 2/6/09

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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	P-1B
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	27-Aug-08
LOCATION	San Leandro, California	DRILLING COMPLETED	04-Sep-08

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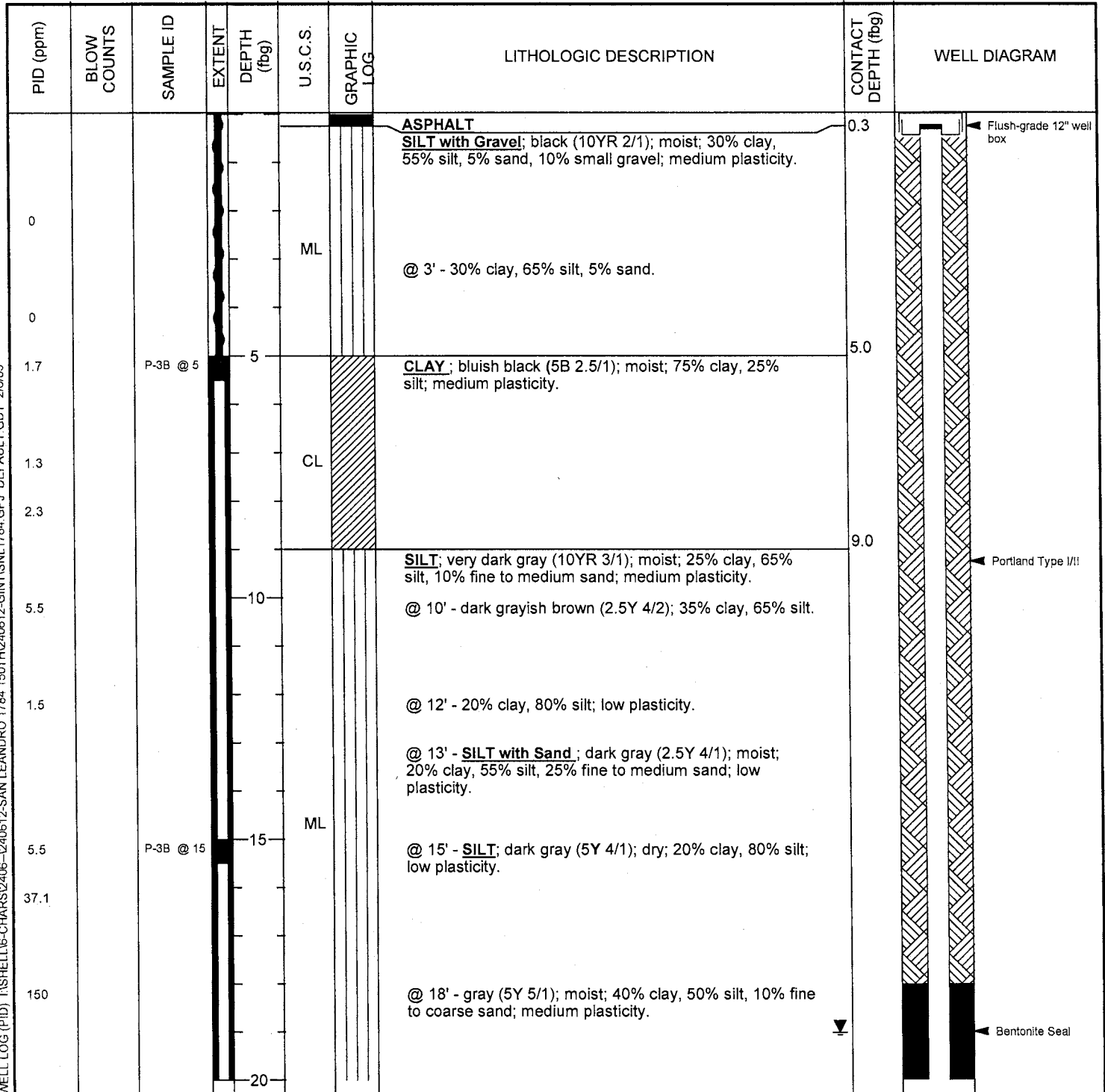
PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
2.1						@ 20' - 15% clay, 85% silt; low plasticity.		
3.8								
122.5		P-1B @ 25	25			@ 26' - 20% clay, 70% silt, 10% fine sand.		
330						@ 27' - moist; 35% clay, 65% silt; medium plasticity.		
263				ML		@ 28' - SILT with Sand ; dark gray (10YR 4/1); dry; 5% clay, 70% silt, 25% fine sand; low plasticity.		
425		P-1B @ 30	30			@ 29' - dark yellowish brown (10YR 4/2);		
126						@ 30' - moist; 80% silt, 20% fine sand.		
92						@ 31' - grayish brown (2.5Y 5/2); dry; 75% silt, 25% fine to medium sand.		
83						@ 32' - SILT ; grayish brown (2.5Y 5/2); moist; 25% clay, 70% silt, 5% sand; low plasticity.		
36.5		P-1B @ 35.5	35.5			@ 34' - SILT with Sand ; dark grayish brown (2.5Y 4/2); moist; 15% clay, 60% silt, 25% fine to medium sand; medium plasticity.	36.0	
								Bottom of Boring @ 36 fbg



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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	P-3B
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	28-Aug-08
LOCATION	San Leandro, California	DRILLING COMPLETED	05-Sep-08
PROJECT NUMBER	240612	WELL DEVELOPMENT DATE (YIELD)	16-Sep-08 (87 gallons)
DRILLER	Gregg Drilling, C-57 #485165	GROUND SURFACE ELEVATION	44.82 ft above msl
DRILLING METHOD	Hollow-stem auger	TOP OF CASING ELEVATION	44.62 ft above msl
BORING DIAMETER	10"	SCREENED INTERVALS	22 to 32 fbg
LOGGED BY	E. Reinhart-Koylu	DEPTH TO WATER (First Encountered)	24.00 fbg (05-Sep-08) ▼
REVIEWED BY	P. Schaefer	DEPTH TO WATER (Static)	19.02 fbg (15-Sep-08) ▼
REMARKS	Air knife to 5 fbg		



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WELL LOG (PID) I:\SHELL\6-CHARS\2406-12\40612-SAN LEANDRO 1784 150TH\240612-GINT\SL1784.GPJ DEFAULT.GDT 2/6/09



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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	P-3B
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	28-Aug-08
LOCATION	San Leandro, California	DRILLING COMPLETED	05-Sep-08

Continued from Previous Page

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
382		P-3B @ 20				@ 20' - dark gray (5Y 4/1).		<p>Monterey Sand #2/12</p> <p>4"-diam., 0.020" Slotted Schedule 40 PVC</p> <p>Bottom of Boring @ 32 fbg</p>
196						@ 22' - brown (7.5YR 4/4); 20% clay, 75% silt, 5% sand.		
95.4						@ 24' - wet; 20% clay, 80% silt.		
122			25	ML		@ 25' - gray (5Y 5/1); dry; 5% clay, 90% silt, 5% sand; low plasticity.		
443		P-3B @ 27				@ 26' - moist.		
248						@ 28' - 10% clay, 80% silt, 10% sand.		
216			30			@ 29' - <u>SILT with Sand</u> ; grayish brown (2.5Y 5/2); dry; 5% clay, 70% silt, 25% fine sand; low plasticity.		
77		P-3B @ 31.5				@ 31' - moist; 15% clay, 60% silt, 25% fine to medium sand.	32.0	

WELL LOG (PID) I:\SHELL\6-CHARS\2406-1240612-SAN LEANDRO 1784 150TH\240612-GINTS\NL1784.GPJ DEFAULT.GDT 2/6/09

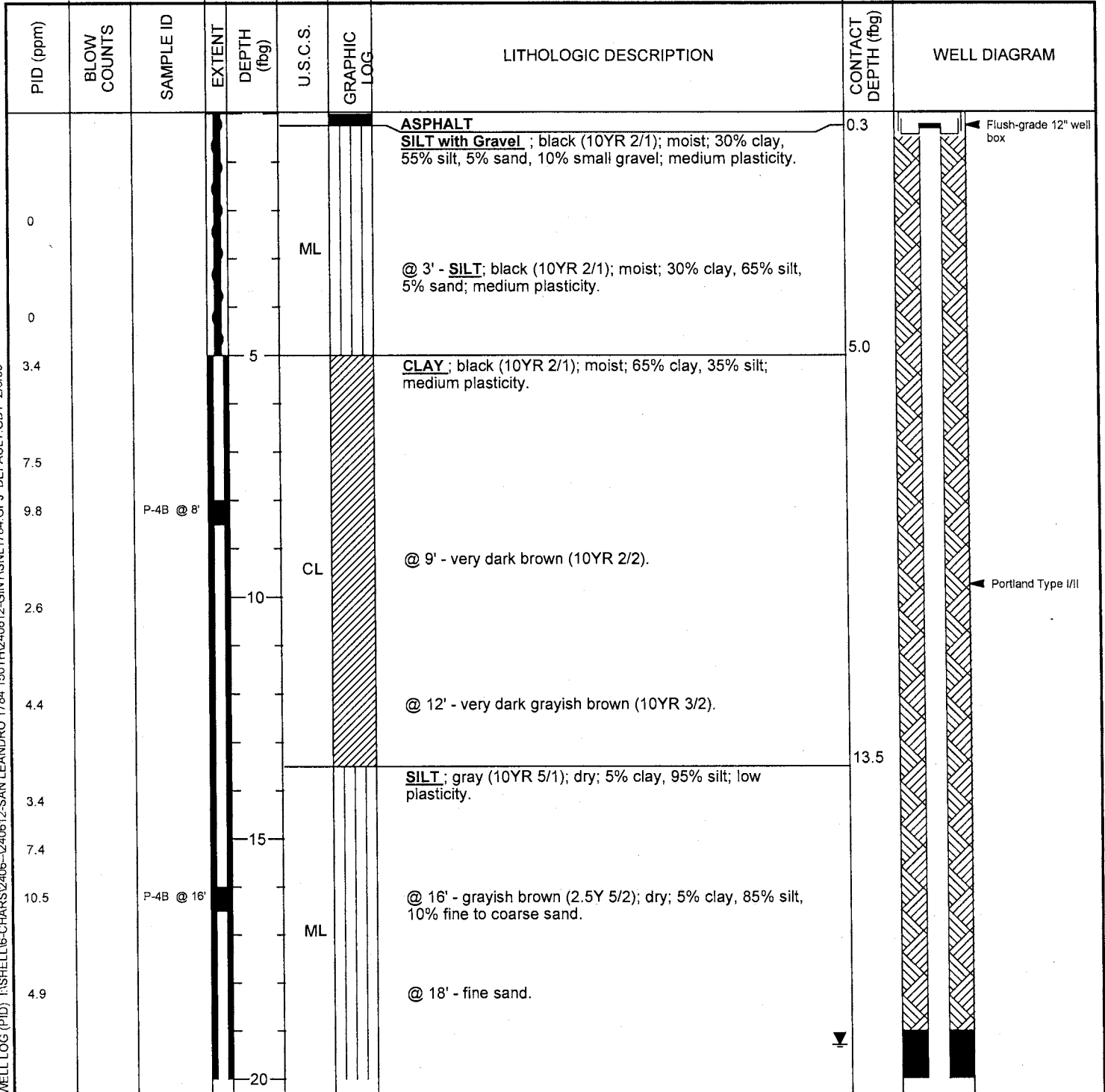


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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	P-4B
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	27-Aug-08
LOCATION	San Leandro, California	DRILLING COMPLETED	05-Sep-08
PROJECT NUMBER	240612	WELL DEVELOPMENT DATE (YIELD)	17-Sep-08 (88 gallons)
DRILLER	Gregg Drilling, C-57 #485165	GROUND SURFACE ELEVATION	45.30 ft above msl
DRILLING METHOD	Hollow-stem auger	TOP OF CASING ELEVATION	44.93 ft above msl
BORING DIAMETER	10"	SCREENED INTERVALS	23 to 33 fbg
LOGGED BY	E. Reinhart-Koylu	DEPTH TO WATER (First Encountered)	NA
REVIEWED BY	P. Schaefer	DEPTH TO WATER (Static)	19.30 fbg (15-Sep-08)
REMARKS	Air knife to 5 fbg		

WELL LOG (PID) I:\SHELL\6-CHARS\2406-1240612-SAN LEANDRO 1784 150TH\240612-GINT\SNL1784.GPJ DEFAULT.GDT 2/6/09



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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	P-4B
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	27-Aug-08
LOCATION	San Leandro, California	DRILLING COMPLETED	05-Sep-08

Continued from Previous Page

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
49.3							@ 20' - Sandy SILT ; dark gray (5Y 4/1); moist; 5% clay, 55% silt, 30% fine sand, 10% small gravel; low plasticity.		
342		P-4B @ 22'					@ 22' - 5% clay, 55% silt, 30% fine to coarse sand, 10% small gravel.		
418							@ 23' - 5% clay, 50% silt, 35% fine to coarse sand, 10% small gravel.		
236									
469		P-4B @ 25'		25			@ 25' - SILT ; dark gray (5Y 4/1); dry; 10% clay, 85% silt, 5% sand; low plasticity.		
419					ML		@ 27' - 30% clay, 70% silt.		
329							@ 28' - 20% clay, 80% silt.		
251				30			@ 30' - SILT with Sand ; olive gray (5Y 5/2); moist; 5% clay, 70% silt, 25% fine to medium sand; low plasticity.		
214									
88		P-4B @ 32.5'						33.0	Bottom of Boring @ 33 fbg

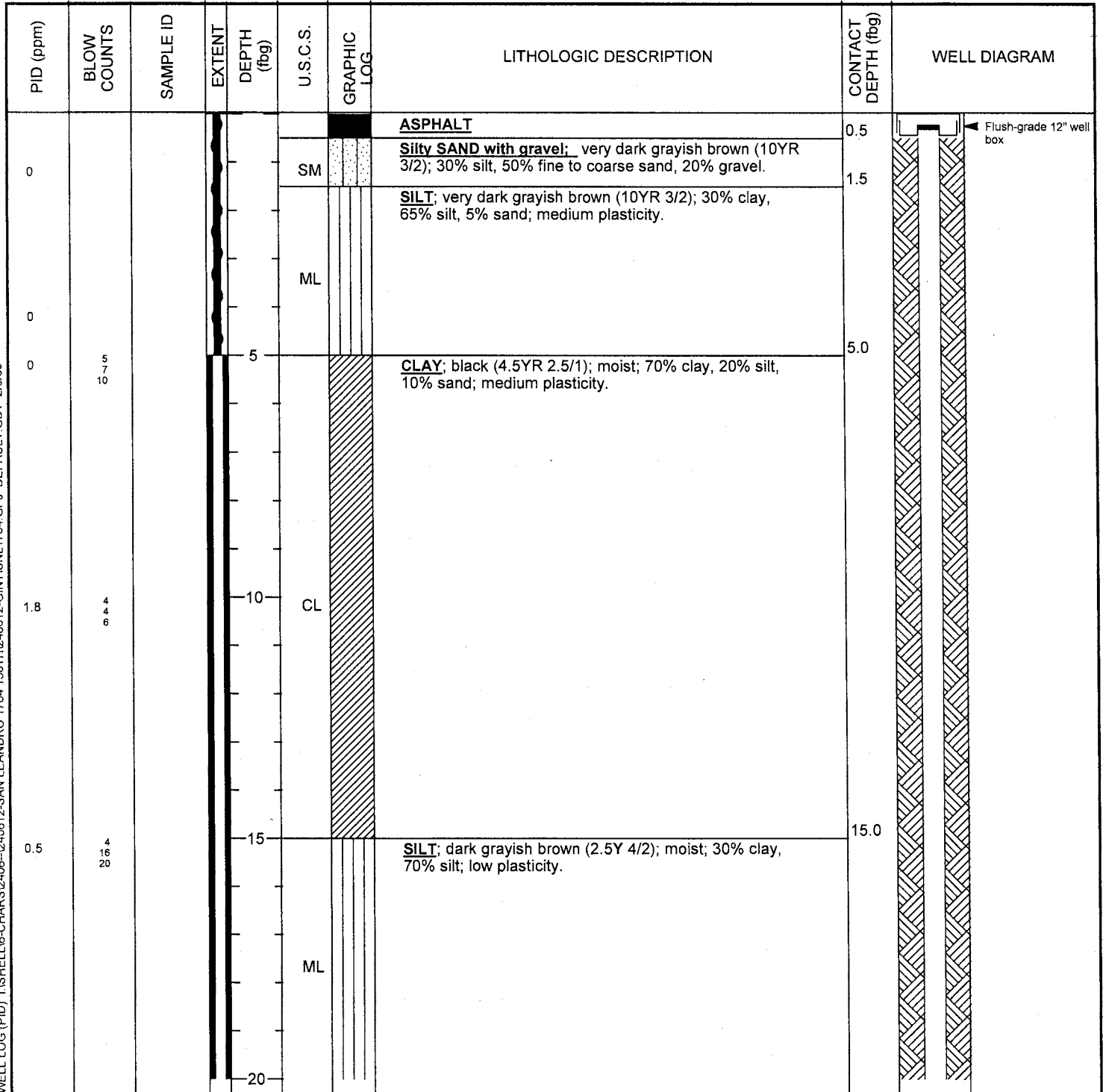
WELL LOG (PID) I:\SHELL\6-CHARS\2406-1240612-SAN LEANDRO 1784 150TH\240612-GINTIS\NL1784.GPJ DEFAULT.GDT 2/6/09



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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	MW-2B
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	26-Aug-08
LOCATION	San Leandro, California	DRILLING COMPLETED	28-Oct-08
PROJECT NUMBER	240612	WELL DEVELOPMENT DATE (YIELD)	31-Oct-08 (189 gallons)
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	45.25 ft above msl
DRILLING METHOD	Hollow-stem auger	TOP OF CASING ELEVATION	44.96 ft above msl
BORING DIAMETER	10"	SCREENED INTERVALS	45 to 50 fbg
LOGGED BY	E. Reinhart-Koylu	DEPTH TO WATER (First Encountered)	23.50 fbg (28-Oct-08)
REVIEWED BY	P. Schaefer	DEPTH TO WATER (Static)	20.20 fbg (31-Oct-08)
REMARKS	Air knife to 5 fbg		



WELL LOG (PID) I:\SHELL\6-CHARS\2406-1240612-SAN LEANDRO 1784 150TH\240612-GINT\SNL1784.GPJ DEFAULT.GDT 2/6/09

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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	MW-2B
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	26-Aug-08
LOCATION	San Leandro, California	DRILLING COMPLETED	28-Oct-08

Continued from Previous Page

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
13.1	11 17 23								
286	14 22 40			25			@ 23.5' - wet.		
463	21 24 27	MW-2B @ 30'		30	ML		@ 25' - olive brown (2.5Y 4/3).		
16.5	10 18 12			35			@ 30' - olive gray (5Y 4/2); moist; 30% clay, 60% silt, 10% fine sand.		
78.3	22 32 50 for 2"	MW-2B @ 37'					@ 35' - SILT with Sand ; olive gray (5Y 4/2); wet; 25% clay, 55% silt, 20% fine to medium sand; medium plasticity.		
7.8	25 31 50 for 2"			40			@ 37' - Sandy SILT ; brown (10YR 4/3); moist; 20% clay, 45% silt, 35% fine sand; medium plasticity.		
8.4	21 50 for 2"						@ 39' - light olive brown (2.5Y 5/4); wet.		
7.7	11 23 30						@ 42' - yellowish brown (10YR 5/4); moist.		

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WELL LOG (PID) I:\SHELL\6-CHARS\2406-1240612-SAN LEANDRO 1784 150TH\240612-GINT\SNL1784.GPJ DEFAULT.GDT 2/6/09



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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	MW-2B
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	26-Aug-08
LOCATION	San Leandro, California	DRILLING COMPLETED	28-Oct-08

Continued from Previous Page

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
13.7	7 17 23	MW-2B @ 44'					@ 44' - dark yellowish brown (10YR 4/4); 25% clay, 45% silt, 30% fine sand.		<p>Monterey Sand #2/12</p> <p>4"-diam., 0.020" Slotted Schedule 40 PVC</p> <p>Bottom of Boring @ 50 fbg</p>
1.7	6 16 25			45			@ 45' - brown (10YR 4/3); 25% clay, 40% silt, 30% fine sand, 5% fine gravel.		
2.7	22 50 for 4"				ML		@ 46' - 25% clay, 40% silt, 30% fine to medium sand, 5% fine gravel.		
3.1		MW-2B @ 49.5'		50				50.0	

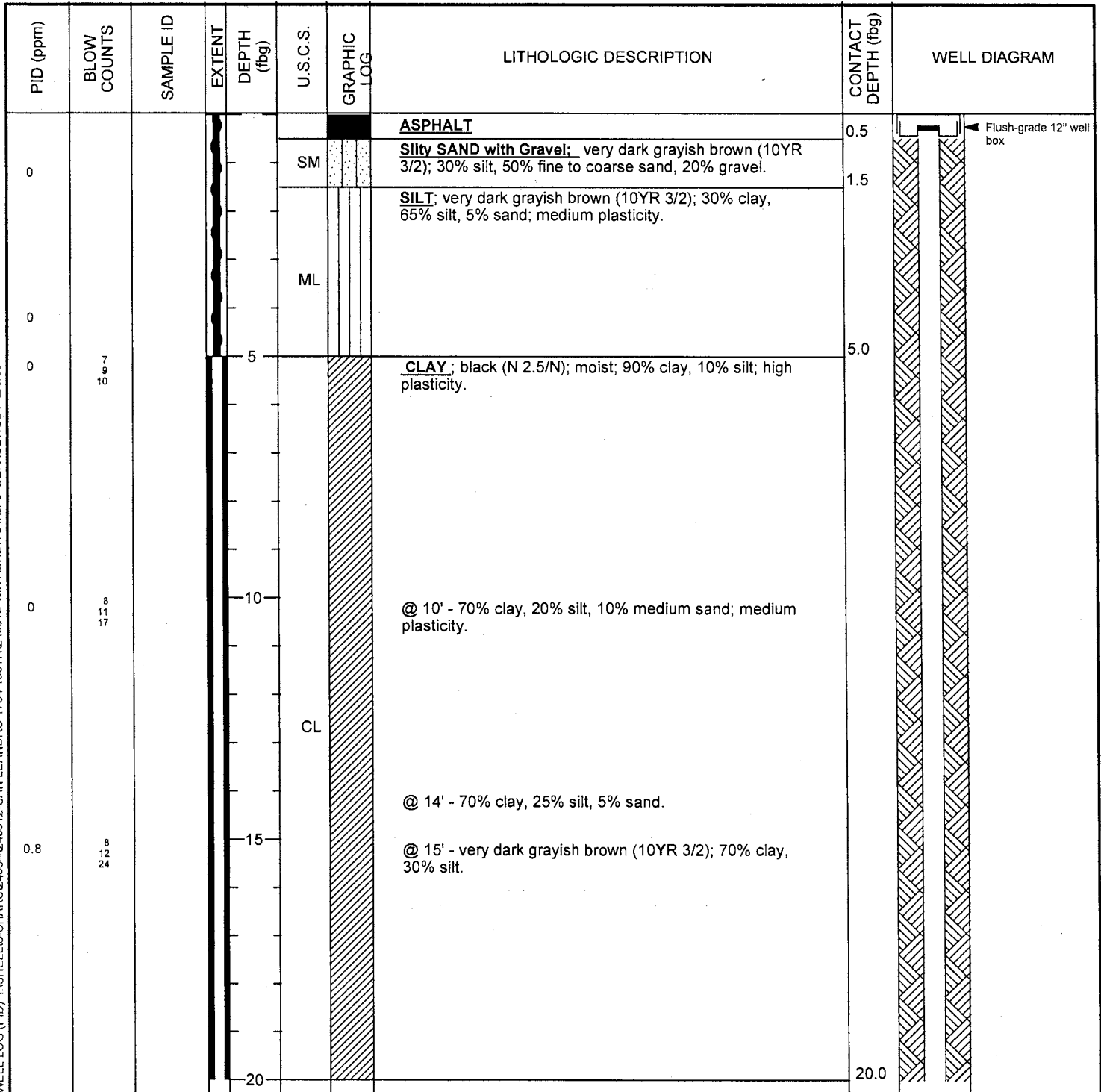
WELL LOG (PID) I:\SHELL\6-CHARS\2406--\240612-SAN LEANDRO 1784 150TH\240612-GINT\SNL1784.GPJ DEFAULT.GDT 2/6/09



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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	MW-1B
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	26-Aug-08
LOCATION	San Leandro, California	DRILLING COMPLETED	29-Oct-08
PROJECT NUMBER	240612	WELL DEVELOPMENT DATE (YIELD)	31-Oct-08 (165 gallons)
DRILLER	Gregg Drilling	GROUND SURFACE ELEVATION	49.52 ft above msl
DRILLING METHOD	Hollow-stem auger	TOP OF CASING ELEVATION	49.07 ft above msl
BORING DIAMETER	10"	SCREENED INTERVALS	45 to 50 fbg
LOGGED BY	E. Reinhart-Koylu	DEPTH TO WATER (First Encountered)	37.00 fbg (29-Oct-08) ▼
REVIEWED BY	P. Schaefer	DEPTH TO WATER (Static)	24.25 fbg (31-Oct-08) ▼
REMARKS	Air knife to 5 fbg		



WELL LOG (PID) I:\SHELL\6-CHARS\2406-1240612-SAN LEANDRO 1784 150TH\240612-GINT\SNL-1784.GPJ DEFAULT.GDT 2/6/09

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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	MW-1B
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	26-Aug-08
LOCATION	San Leandro, California	DRILLING COMPLETED	29-Oct-08

Continued from Previous Page

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (ft)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (ft)	WELL DIAGRAM
0.2	15 18 22						SILT ; olive gray (5Y 4/2); dry; 35% clay, 60% silt, 5% fine sand; low plasticity.		
0.3	20 23 25			25			@25' - Sandy SILT ; olive gray (5Y 4/2); moist; 65% silt, 35% fine to medium sand; low plasticity.		
404	17 19 22			30	ML		@ 30' - 70% silt, 30% sand; medium plasticity.		
4.7	15 16 18			35			@ 35' - SILT ; dark yellowish brown (10YR 4/4); moist; 30% clay, 60% silt, 10% fine sand; low plasticity.		
							@ 37' - wet.		
							Silty SAND ; yellowish brown (10YR 5/4); wet; 5% clay, 35% silt, 60% fine to coarse angular rounded sand.	38.0	
4.2	14 19 27			40	SM				
	3 27 31								
									Bentonite Seal

WELL LOG (PID) I:\SHELL\6-CHARS\2406--1240612-SAN LEANDRO 1784 150TH\240612-GINT\SNL-1784.GPJ DEFAULT GDT: 2/6/09

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BORING / WELL LOG

CLIENT NAME	Shell Oil Products Company (US)	BORING/WELL NAME	MW-1B
JOB/SITE NAME	1784 150th Avenue	DRILLING STARTED	26-Aug-08
LOCATION	San Leandro, California	DRILLING COMPLETED	29-Oct-08

Continued from Previous Page

PID (ppm)	BLOW COUNTS	SAMPLE ID	EXTENT	DEPTH (fbg)	U.S.C.S.	GRAPHIC LOG	LITHOLOGIC DESCRIPTION	CONTACT DEPTH (fbg)	WELL DIAGRAM
6.8	17 50 for 2"	MW-1B @ 44'		45			@ 43' - 30% silt, 65% fine to coarse sand, 5% fine gravel.		<p>Monterey Sand #2/12</p> <p>4"-diam., 0.020" Slotted Schedule 40 PVC</p>
1.5	27 50 for 3"				SM		@ 45' - 45% silt, 50% fine to medium sand, 5% fine gravel.		
0.7	28 18								
0.6	8 10 13	MW-1B @ 49.5'		50				50.0	Bottom of Boring @ 50 fbg

WELL LOG (PID) I:\SHELL\6-CHARS\2406--240612-SAN LEANDRO 1784 150TH\240612-GINT\SNL1784.GPJ DEFAULT.GDT 2/6/09

APPENDIX C

HISTORICAL SOIL DATA

TABLE 1

**HISTORICAL SOIL ANALYTICAL DATA
SHELL-BRANDED SERVICE STATION
1784 150TH STREET, SAN LEANDRO, CALIFORNIA**

Sample ID	Date	Depth (fbg)	TPHg	Benzene	Toluene	Ethyl- benzene	Total Xylenes	MTBE (8020)	MTBE (8260)	TBA	ETBE	DIPE	TAME	1,2-DCA	EDB	Ethanol	TOG	Lead
<u>1986 Waste Oil Tank Removal</u>																		
Soil #1	11/7/1986	8	--	--	--	--	--	--	--	--	--	--	--	--	--	--	196	--
Soil #2	11/11/1986	11	--	--	--	--	--	--	--	--	--	--	--	--	--	--	167.4	--
<u>1990 Monitoring Well Installation</u>																		
MW-1/BH-A ^{a,b}	3/5/1990	5	<1	<0.0025	<0.0025	<0.0025	<0.0025	--	--	--	--	--	--	<0.002	--	--	<50	--
MW-1/BH-A ^{a,b}	3/5/1990	15.7	<1	<0.0025	<0.0025	<0.0025	<0.0025	--	--	--	--	--	--	<0.002	--	--	<50	--
MW-1/BH-A ^{a,b,c}	3/5/1990	24.7	<1	0.020	<0.0025	<0.0025	<0.0025	--	--	--	--	--	--	<0.002	--	--	<50	--
MW-1/BH-A ^a	3/5/1990	29.2	35	0.23	0.20	<0.0025	0.64	--	--	--	--	--	--	0.0064	--	--	<50	--
MW-1/BH-A ^{a,b}	3/5/1990	41.2	<1	<0.0025	<0.0025	<0.0025	<0.0025	--	--	--	--	--	--	<0.002	--	--	<50	--
<u>1992 Monitoring Well Installations</u>																		
MW-2/BH-B ^b	2/4/1992	11.5	<1	0.0026	<0.0025	<0.0025	<0.0025	--	--	--	--	--	--	<0.002	--	--	--	--
MW-2/BH-B	2/4/1992	16.5	<1	0.0058	<0.0025	<0.0025	<0.0025	--	--	--	--	--	--	--	--	--	--	--
MW-2/BH-B ^{b,d}	2/4/1992	21.5	79	0.20	0.60	1.0	4.1	--	--	--	--	--	--	<0.002	--	--	--	--
MW-2/BH-B	2/4/1992	26.5	74	0.59	0.91	1.5	3.9	--	--	--	--	--	--	--	--	--	--	--
MW-3/BH-C ^b	2/5/1992	11.5	<1	0.0042	0.0029	0.0039	<0.0025	--	--	--	--	--	--	<0.002	--	--	--	--
MW-3/BH-C ^b	2/5/1992	21.5	<1	<0.0025	<0.0025	<0.0025	<0.0025	--	--	--	--	--	--	<0.002	--	--	--	--
MW-3/BH-C ^{b,e}	2/5/1992	26.5	3.9	<0.0025	<0.0025	<0.0025	0.0054	--	--	--	--	--	--	<0.002	--	--	--	--
MW-3/BH-C	2/5/1992	31.5	68	<0.05	<0.05	<0.05	0.17	--	--	--	--	--	--	--	--	--	--	--
<u>1994 Subsurface Investigation</u>																		
BH-1-21	6/6/1994	21	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	--	--	--	--	--	--	--	--	--	--
BH-2-20	6/6/1994	20	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	--	--	--	--	--	--	--	--	--	--
BH-3-16 ^t	6/6/1994	16	<1.0	0.013	<0.0050	<0.0050	<0.0050	--	--	--	--	--	--	--	--	--	--	--
BH-4-20.6	6/7/1994	20.6	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	--	--	--	--	--	--	--	--	--	--
BH-5-15.6	6/7/1994	15.6	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	--	--	--	--	--	--	--	--	--	--
BH-6-20.5	6/7/1994	20.5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	--	--	--	--	--	--	--	--	--	--
<u>1995 Monitoring Well Installation</u>																		
BH-7-15.8	2/14/1995	15.8	<1.0	<0.0025	<0.0025	<0.0025	<0.0025	--	--	--	--	--	--	--	--	--	--	--
BH-8-16.0	2/14/1995	16	<1.0	<0.0025	<0.0025	<0.0025	<0.0025	--	--	--	--	--	--	--	--	--	--	--
BH-9-19.5	2/14/1995	19.5	<1.0	<0.0025	<0.0025	<0.0025	<0.0025	--	--	--	--	--	--	--	--	--	--	--
MW-4/BH-10-15.2	3/3/1995	15.2	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	--	--	--	--	--	--	--	--	--	--

TABLE 1

**HISTORICAL SOIL ANALYTICAL DATA
SHELL-BRANDED SERVICE STATION
1784 150TH STREET, SAN LEANDRO, CALIFORNIA**

Sample ID	Date	Depth (fbg)	TPHg	Benzene	Toluene	Ethyl-benzene	Total Xylenes	MTBE (8020)	MTBE (8260)	TBA	ETBE	DIPE	TAME	1,2-DCA	EDB	Ethanol	TOG	Lead
<u>1996 Subsurface Investigation</u>																		
SVS-3	7/18-19/96	16-18	<1.0	<0.005	<0.005	<0.005	<0.005	<0.025	--	--	--	--	--	--	--	--	--	--
SVS-5	7/18-19/96	4-6	<1.0	<0.005	<0.005	<0.005	<0.005	<0.025	--	--	--	--	--	--	--	--	--	--
SVS-5	7/18-19/96	8-10	<1.0	<0.005	<0.005	<0.005	<0.005	<0.025	--	--	--	--	--	--	--	--	--	--
SVS-5	7/18-19/96	18-20	1.1	<0.005	<0.005	<0.005	<0.005	<0.025	--	--	--	--	--	--	--	--	--	--
SVS-9	7/18-19/96	3-5	<1.0	<0.005	<0.005	<0.005	<0.005	<0.025	--	--	--	--	--	--	--	--	--	--
SVS-9	7/18-19/96	8-10	<1.0	<0.005	<0.005	<0.005	<0.005	<0.025	--	--	--	--	--	--	--	--	--	--
SVS-9	7/18-19/96	16-18	<1.0	<0.005	<0.005	<0.005	<0.005	<0.025	--	--	--	--	--	--	--	--	--	--
<u>1997 Dispenser and Turbine Pump Upgrades</u>																		
Disp-A	12/4/1997	2	3.1	<0.005	0.037	0.022	<0.01	0.019	--	--	--	--	--	--	--	--	--	--
Disp-A, 4.5	12/4/1997	4.5	6.3	0.096	0.012	0.46	0.037	0.056	--	--	--	--	--	--	--	--	--	--
Disp-B	12/4/1997	2	130	<1	<1	<1	<2	<1	--	--	--	--	--	--	--	--	--	--
Disp-B, 4.5	12/4/1997	4.5	1.0	0.045	<0.005	0.064	0.32	<0.03	--	--	--	--	--	--	--	--	--	--
Disp-C	12/4/1997	2	190	1.8	2.1	3.6	20	1.4	--	--	--	--	--	--	--	--	--	--
Disp-C, 4.5 ^b	12/4/1997	4.5	590	<0.5	0.98	2.3	3.1	<0.5	--	--	--	--	--	--	--	--	--	--
Disp-D	12/4/1997	2	3.8	0.11	<0.005	0.15	0.17	0.11	--	--	--	--	--	--	--	--	--	--
Disp-D, 4.5	12/4/1997	4.5	1.4	0.027	<0.005	0.036	0.178	0.005	--	--	--	--	--	--	--	--	--	--
<u>1998 Subsurface Investigation</u>																		
SVS-11-5.5	11/10/1998	5.5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	<0.025	--	--	--	--	--	--	--	--	--	--
SVS-11-6	11/10/1998	6	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	<0.025	--	--	--	--	--	--	--	--	--	--
SVS-11-9.5	11/10/1998	9.5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	<0.025	--	--	--	--	--	--	--	--	--	--
SVS-11-10	11/10/1998	10	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	<0.025	--	--	--	--	--	--	--	--	--	--
SVS-11-15	11/10/1998	15	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	<0.025	--	--	--	--	--	--	--	--	--	--
SVS-11-15.5	11/10/1998	15.5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	<0.025	--	--	--	--	--	--	--	--	--	--
SVS-11-19	11/10/1998	19	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	<0.025	--	--	--	--	--	--	--	--	--	--
SVS-11-19.5	11/10/1998	19.5	1.6	0.0050	<0.0050	<0.0050	<0.0050	<0.025	--	--	--	--	--	--	--	--	--	--
SVS-14-5	11/11/1998	5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	<0.025	--	--	--	--	--	--	--	--	--	--
SVS-14-5.5	11/11/1998	5.5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	<0.025	--	--	--	--	--	--	--	--	--	--
SVS-14-10	11/11/1998	10	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	<0.025	--	--	--	--	--	--	--	--	--	--
SVS-14-10.5	11/11/1998	10.5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	<0.025	--	--	--	--	--	--	--	--	--	--
SVS-14-15	11/11/1998	15	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	<0.025	--	--	--	--	--	--	--	--	--	--
SVS-14-15.5	11/11/1998	15.5	<1.0	<0.0050	0.006	<0.0050	<0.0050	<0.025	--	--	--	--	--	--	--	--	--	--

TABLE 1

**HISTORICAL SOIL ANALYTICAL DATA
SHELL-BRANDED SERVICE STATION
1784 150TH STREET, SAN LEANDRO, CALIFORNIA**

Sample ID	Date	Depth (ft)	TPHg	Benzene	Toluene	Ethyl- benzene	Total Xylenes	MTBE (8020)	MTBE (8260)	TBA	ETBE	DIPE	TAME	1,2-DCA	EDB	Ethanol	TOG	Lead
SVS-14-19	11/11/1998	19	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	0.029	<25	--	--	--	--	--	--	--	--	--
SVS-14-19.5	11/11/1998	19.5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	<0.025	--	--	--	--	--	--	--	--	--	--
SVS-15-4.5	11/11/1998	4.5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	<0.025	--	--	--	--	--	--	--	--	--	--
SVS-15-5	11/11/1998	5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	<0.025	--	--	--	--	--	--	--	--	--	--
SVS-15-10	11/11/1998	10	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	<0.025	--	--	--	--	--	--	--	--	--	--
SVS-15-10.5	11/11/1998	10.5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	<0.025	--	--	--	--	--	--	--	--	--	--
SVS-15-15	11/11/1998	15	<1.0	<0.0050	<0.0050	<0.0050	0.013	<0.025	--	--	--	--	--	--	--	--	--	--
SVS-15-15.5	11/11/1998	15.5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	<0.025	--	--	--	--	--	--	--	--	--	--
SVS-15-19.5	11/11/1998	19.5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	<0.025	--	--	--	--	--	--	--	--	--	--
SVS-15-20	11/11/1998	20	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	<0.025	--	--	--	--	--	--	--	--	--	--
SVS-16-5	11/11/1998	5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	<0.025	--	--	--	--	--	--	--	--	--	--
SVS-16-5.5	11/11/1998	5.5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	<0.025	--	--	--	--	--	--	--	--	--	--
SVS-16-10	11/11/1998	10	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	<0.025	--	--	--	--	--	--	--	--	--	--
SVS-16-10.5	11/11/1998	10.5	<1.0	<0.0050	<0.0050	<0.0050	0.0093	0.026	--	--	--	--	--	--	--	--	--	--
SVS-16-15	11/11/1998	15	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	<0.025	--	--	--	--	--	--	--	--	--	--
SVS-16-15.5	11/11/1998	15.5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	<0.025	--	--	--	--	--	--	--	--	--	--
<u>2001 Monitoring Well Installation</u>																		
MW-5-15.5	10/24/2001	15.5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
MW-6-5.5	10/24/2001	5.5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	0.012	--	--	--	--	--	--	--	--	--
<u>2002 Monitoring Well Installation</u>																		
MW7@5'	10/3/2002	5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.5	--	--	--	--	--	--	--	--	--
MW7@10'	10/3/2002	10	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.5	--	--	--	--	--	--	--	--	--
MW7@15'	10/3/2002	15	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.5	--	--	--	--	--	--	--	--	--
MW7@20'	10/3/2002	20	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.5	--	--	--	--	--	--	--	--	--
MW7@25'	10/3/2002	25	11	<0.0050	0.0060	0.086	0.13	--	<0.5	--	--	--	--	--	--	--	--	--
MW7@30'	10/3/2002	30	68	<0.025	0.19	0.89	3.7	--	<0.5	--	--	--	--	--	--	--	--	--
MW7@32'	10/3/2002	32	1.2	<0.0050	0.0069	0.025	0.11	--	<0.5	--	--	--	--	--	--	--	--	--
MW8@5'	10/4/2002	5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.5	--	--	--	--	--	--	--	--	--
MW8@10'	10/4/2002	10	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.5	--	--	--	--	--	--	--	--	--
MW8@15'	10/4/2002	15	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.5	--	--	--	--	--	--	--	--	--

TABLE 1

**HISTORICAL SOIL ANALYTICAL DATA
SHELL-BRANDED SERVICE STATION
1784 150TH STREET, SAN LEANDRO, CALIFORNIA**

Sample ID	Date	Depth (ftg)	TPHg	Benzene	Toluene	Ethyl- benzene	Total Xylenes	MTBE (8020)	MTBE (8260)	TBA	ETBE	DIPE	TAME	1,2-DCA	EDB	Ethanol	TOG	Lead
MW8@20'	10/4/2002	20	1.2	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.5	--	--	--	--	--	--	--	--	--
MW8@25'	10/4/2002	25	140	0.072	0.15	1.5	5.8	--	<0.5	--	--	--	--	--	--	--	--	--
SB9@22	10/4/2002	22	1.1	<0.0050	<0.0050	0.016	0.088	--	<0.5	--	--	--	--	--	--	--	--	--
<u>2003 Subsurface Investigation</u>																		
SB-10-10'	6/23/2003	10	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-10-20'	6/23/2003	20	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-10-22'	6/23/2003	22	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-10-25'	6/23/2003	25	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-10-30	6/23/2003	30	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-10-37'	6/23/2003	37	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-10-39.5'	6/23/2003	39.5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-11-10'	6/24/2003	10	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-11-15'	6/24/2003	15	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-11-20'	6/24/2003	20	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-11-24'	6/24/2003	24	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-11-28'	6/24/2003	28	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-11-30'	6/24/2003	30	650	<0.50	<0.50	3.5	9.9	--	<0.50	--	--	--	--	--	--	--	--	--
SB-12-10'	6/24/2003	10	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-12-20'	6/24/2003	20	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-12-25'	6/24/2003	25	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-12-30'	6/24/2003	30	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-12-35'	6/24/2003	35	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-12-39.5'	6/24/2003	39.5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-13-10'	6/23/2003	10	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-13-20'	6/23/2003	20	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-13-24'	6/23/2003	24	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-13-30'	6/23/2003	30	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-13-35'	6/23/2003	35	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-13-39.5'	6/23/2003	39.5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-14-10'	6/24/2003	10	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--

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**HISTORICAL SOIL ANALYTICAL DATA
SHELL-BRANDED SERVICE STATION
1784 150TH STREET, SAN LEANDRO, CALIFORNIA**

Sample ID	Date	Depth (fbg)	TPHg	Benzene	Toluene	Ethyl- benzene	Total Xylenes	MTBE (8020)	MTBE (8260)	TBA	ETBE	DIPE	TAME	1,2-DCA	EDB	Ethanol	TOG	Lead
SB-14-20'	6/24/2003	20	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-14-24'	6/24/2003	24	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-14-30'	6/24/2003	30	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-14-35'	6/24/2003	35	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-14-39.5'	6/24/2003	39.5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-15-10'	6/26/2003	10	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-15-15'	6/26/2003	15	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-15-20'	6/26/2003	20	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-15-22.5'	6/26/2003	22.5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-15-35'	6/26/2003	35	1.4	0.10	<0.0050	0.030	0.0055	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-16-10'	6/23/2003	10	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-16-20'	6/23/2003	20	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-16-24'	6/23/2003	24	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-16-28'	6/23/2003	28	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-16-35'	6/23/2003	35	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
SB-16-39.5'	6/23/2003	39.5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
<u>2003 Monitoring Well Installation</u>																		
MW-9-5'	11/19/2003	5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
MW-9-10'	11/19/2003	10	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
MW-9-15'	11/19/2003	15	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
MW-9-20'	11/19/2003	20	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
MW-9-25'	11/19/2003	25	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
MW-9-30'	11/19/2003	30	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
MW-9-35'	11/19/2003	35	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
MW-10-5'	11/20/2003	5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
MW-10-10'	11/20/2003	10	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
MW-10-15'	11/20/2003	15	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
MW-10-20'	11/20/2003	20	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
MW-10-25'	11/20/2003	25	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
MW-10-30'	11/20/2003	30	14	<0.023	<0.023	<0.023	<0.023	--	<0.023	--	--	--	--	--	--	--	--	--
MW-10-31.5'	11/20/2003	31.5	230	<0.50	<0.50	2.2	1.5	--	<0.50	--	--	--	--	--	--	--	--	--

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1784 150TH STREET, SAN LEANDRO, CALIFORNIA**

Sample ID	Date	Depth (ftg)	TPHg	Benzene	Toluene	Ethyl- benzene	Total Xylenes	MTBE (8020)	MTBE (8260)	TBA	ETBE	DIPE	TAME	1,2-DCA	EDB	Ethanol	TOG	Lead
MW-11-5'	11/20/2003	5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
MW-11-10'	11/20/2003	10	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
MW-11-15'	11/20/2003	15	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	--	--	--	--	--	--	--	--	--
MW-11-20'	11/20/2003	20	1.8	<0.0050	<0.0050	0.0084	0.013	--	0.039	--	--	--	--	--	--	--	--	--
MW-11-24.5'	11/20/2003	24.5	330	<0.50	1.6	4.8	29	--	1.4	--	--	--	--	--	--	--	--	--
<u>2004 Subsurface Investigation</u>																		
SB-17-5'	9/13/2004	5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.10	<0.0050	<0.10	<0.0050	<0.0050	<0.0050	<0.1	--	--
SB-17-10'	9/13/2004	10	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.10	<0.0050	<0.10	<0.0050	<0.0050	<0.0050	<0.1	--	--
SB-17-15'	9/13/2004	15	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.10	<0.0050	<0.10	<0.0050	<0.0050	<0.0050	<0.1	--	--
SB-17-20'	9/13/2004	20	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.10	<0.0050	<0.10	<0.0050	<0.0050	<0.0050	<0.1	--	--
SB-17-25'	9/13/2004	25	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.10	<0.0050	<0.10	<0.0050	<0.0050	<0.0050	<0.1	--	--
SB-17-35.5'	9/13/2004	35.5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.10	<0.0050	<0.10	<0.0050	<0.0050	<0.0050	<0.1	--	--
SB-18-5'	9/13/2004	5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.10	<0.0050	<0.10	<0.0050	<0.0050	<0.0050	<0.1	--	--
SB-18-10'	9/13/2004	10	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.10	<0.0050	<0.10	<0.0050	<0.0050	<0.0050	<0.1	--	--
SB-18-15'	9/13/2004	15	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.10	<0.0050	<0.10	<0.0050	<0.0050	<0.0050	<0.1	--	--
SB-18-20'	9/13/2004	20	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.10	<0.0050	<0.10	<0.0050	<0.0050	<0.0050	<0.1	--	--
SB-18-25'	9/13/2004	25	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.10	<0.0050	<0.10	<0.0050	<0.0050	<0.0050	<0.1	--	--
SB-18-30'	9/13/2004	30	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.10	<0.0050	<0.10	<0.0050	<0.0050	<0.0050	<0.1	--	--
<u>2005 Dispenser Upgrades</u>																		
D-1-3.5	3/22/2005	3.5	460	0.76	0.17	16	8.1	--	0.18	<0.25	<0.050	<0.050	<0.050	<0.050	<0.050	--	--	75.7
D-1-5.0	4/4/2005	5	330	<0.50	0.75	3.2	0.91	--	<0.50	--	--	--	--	--	--	--	--	--
D-2-3.5	3/22/2005	3.5	1,400	1.6	75	18	170	--	0.066	<0.15	<0.25	<0.25	<0.25	<0.25	<0.25	--	--	2.06
D-2-5.0	4/4/2005	5	<50	<0.50	<0.50	<0.50	0.95	--	<0.50	--	--	--	--	--	--	--	--	--
D-3-3.5	3/22/2005	3.5	30	0.78	0.24	1.8	2.7	--	0.053	0.023	<0.050	<0.050	<0.050	<0.050	<0.050	--	--	5.19
D-4-3.5	3/22/2005	3.5	110	0.52	6.3	1.3	10	--	0.028	<0.25	<0.050	<0.050	<0.050	<0.050	<0.050	--	--	1.89
D-4-5.0	4/4/2005	5	290	<0.50	<0.50	6.3	3.6	--	<0.50	--	--	--	--	--	--	--	--	--
P-1-2.5	4/4/2005	2.5	<50	<0.50	<0.50	<0.50	0.87	--	<0.50	--	--	--	--	--	--	--	--	--
P-1-5.0	4/4/2005	5	69	<0.50	<0.50	1.1	5.0	--	<0.50	--	--	--	--	--	--	--	--	--
P-2-3.5	4/4/2005	3.5	<1.0	<0.0050	<0.0050	<0.0050	<0.0050	--	0.013	--	--	--	--	--	--	--	--	--
P-2-5.0	4/4/2005	5	85	<0.50	<0.50	0.84	0.50	--	<0.50	--	--	--	--	--	--	--	--	--
P-3-3.0	4/4/2005	3	2,300	<1.0	<1.0	<1.0	<1.0	--	<1.0	--	--	--	--	--	--	--	--	--
P-4-2.5	4/4/2005	2.5	3,700	11	83	42	280	--	<1.0	--	--	--	--	--	--	--	--	--

TABLE 1
HISTORICAL SOIL ANALYTICAL DATA
SHELL-BRANDED SERVICE STATION
1784 150TH STREET, SAN LEANDRO, CALIFORNIA

Sample ID	Date	Depth (fbg)	TPHg	Benzene	Toluene	Ethyl-benzene	Total Xylenes	MTBE (8020)	MTBE (8260)	TBA	ETBE	DIPE	TAME	1,2-DCA	EDB	Ethanol	TOG	Lead
P-4-5.0	4/4/2005	5	4,100	10	23	48	240	--	<2.5	--	--	--	--	--	--	--	--	--
<u>2006 Subsurface Investigation</u>																		
SB-19-5	5/23/2006	5	<0.100	0.00270	<0.00200	<0.00200	<0.00500	--	<0.00200	<0.0500	<0.00500	<0.00200	<0.00200	<0.00200	<0.00200	--	--	--
SB-19-10	5/24/2006	10	0.454	0.0155	0.00411	<0.00200	<0.00500	--	0.0117	<0.0500	<0.00500	<0.00200	<0.00200	<0.00200	<0.00200	--	--	--
SB-19-15	5/24/2006	15	<0.100	0.00355	<0.00200	<0.00200	<0.00500	--	0.00473	<0.0500	<0.00500	<0.00200	<0.00200	<0.00200	<0.00200	--	--	--
SB-19-19.5	5/24/2006	19.5	<0.100	0.00517	<0.00200	<0.00200	<0.00500	--	0.00236	<0.0500	<0.00500	<0.00200	<0.00200	<0.00200	<0.00200	--	--	--
SB-19-25	5/24/2006	25	<0.100	0.01960	0.00643	<0.00200	0.00619	--	0.00406	0.0668	<0.00500	<0.00200	<0.00200	<0.00200	<0.00200	--	--	--
SB-19-28.5	5/24/2006	28.5	993	0.239	<0.100	8.52	34.6	--	1.09	<2.50	<0.250	<0.100	<0.100	<0.100	<0.100	--	--	--
SB-20-5	5/23/2006	5	61.1	0.0174	0.00952	0.00798	0.0170	--	<0.00200	0.0740	<0.00500	<0.00200	<0.00200	<0.00200	<0.00200	--	--	--
SB-20-10	5/25/2006	10	3.48	0.0286	0.00982	<0.00200	<0.00500	--	<0.00200	0.0727	<0.00500	<0.00200	<0.00200	<0.00200	<0.00200	--	--	--
SB-20-16.5	5/25/2006	16.5	1.27	0.00388	<0.00200	<0.00200	0.00576	--	0.00254	<0.0500	<0.00500	<0.00200	<0.00200	<0.00200	<0.00200	--	--	--
SB-20-23.5	5/25/2006	23.5	692	0.0265	0.0772	6.48	39.1	--	0.142	0.177	<0.00500	<0.00200	<0.00200	<0.00200	<0.00200	--	--	--
SB-21-5	5/23/2006	5	0.379	0.0133	0.00301	<0.00200	<0.00500	--	0.00520	<0.0500	<0.00500	<0.00200	<0.00200	<0.00200	<0.00200	--	--	--
SB-21-10	5/24/2006	10	0.881	0.0273	0.0102	<0.00200	<0.00500	--	0.00347	<0.0500	<0.00500	<0.00200	<0.00200	<0.00200	<0.00200	--	--	--
SB-21-15	5/24/2006	15	<0.100	0.00813	0.00286	<0.00200	<0.00500	--	<0.00200	<0.0500	<0.00500	<0.00200	<0.00200	<0.00200	<0.00200	--	--	--
SB-21-20	5/24/2006	20	<0.100	0.00947	0.00330	<0.00200	<0.00500	--	0.00457	<0.0500	<0.00500	<0.00200	<0.00200	<0.00200	<0.00200	--	--	--
SB-21-27.5	5/24/2006	27.5	635	0.0759	2.20	5.46	27.5	--	0.00963	<0.0500	<0.00500	<0.00200	<0.00200	<0.00200	<0.00200	--	--	--
SB-22-5	5/23/2006	5	<0.100	0.00309	<0.00200	<0.00200	<0.00500	--	<0.00200	<0.0500	<0.00500	<0.00200	<0.00200	<0.00200	<0.00200	--	--	--
SB-22-10	5/25/2006	10	<0.100	0.00292	<0.00200	<0.00200	<0.00500	--	<0.00200	<0.0500	<0.00500	<0.00200	<0.00200	<0.00200	<0.00200	--	--	--
SB-22-15	5/25/2006	15	<0.100	0.00898	0.00279	<0.00200	<0.00500	--	<0.00200	<0.0500	<0.00500	<0.00200	<0.00200	<0.00200	<0.00200	--	--	--
SB-22-20	5/25/2006	20	<0.100	0.00322	<0.00200	<0.00200	<0.00500	--	<0.00200	<0.0500	<0.00500	<0.00200	<0.00200	<0.00200	<0.00200	--	--	--
SB-22-25	5/25/2006	25	0.127	0.00628	0.00226	<0.00200	<0.00500	--	<0.00200	0.0660	<0.00500	<0.00200	<0.00200	<0.00200	<0.00200	--	--	--
SB-22-29.5	5/25/2006	29.5	7.23	0.0171	<0.00200	0.169	0.167	--	0.00334	<0.0500	<0.00500	<0.00200	<0.00200	<0.00200	<0.00200	--	--	--
SB-23-5	5/23/2006	5	517	0.0654	0.100	3.34	7.71	--	<0.00200	<0.0500	<0.00500	<0.00200	<0.00200	<0.00200	<0.00200	--	--	--
SB-23-10	5/24/2006	10	114	1.49	0.0582	1.22	0.468	--	0.00731	<0.0500	<0.00500	<0.00200	<0.00200	<0.00200	<0.00200	--	--	--
SB-23-15	5/24/2006	15	102	0.458	0.0127	0.790	0.948	--	0.0118	<0.0500	<0.00500	<0.00200	<0.00200	<0.00200	<0.00200	--	--	--
SB-23-20	5/24/2006	20	215	0.0154	0.00805	0.986	5.26	--	0.0490	<0.0500	<0.00500	<0.00200	<0.00200	<0.00200	<0.00200	--	--	--
SB-23-25	5/24/2006	25	1,060	0.498	4.77	8.99	54.3	--	<0.100	<2.50	<0.250	<0.100	<0.100	<0.100	<0.100	--	--	--
SB-23-29.5	5/24/2006	29.5	526	0.716	5.71	4.80	27.9	--	0.326	<0.0500	<0.00500	<0.00200	<0.00200	<0.00200	<0.00200	--	--	--
MW-12/SB-24-5	5/23/2006	5	2.39	0.0624	0.00307	<0.00200	<0.00500	--	<0.00200	<0.0500	<0.00500	<0.00200	<0.00200	<0.00200	<0.00200	--	--	--

TABLE 1

**HISTORICAL SOIL ANALYTICAL DATA
SHELL-BRANDED SERVICE STATION
1784 150TH STREET, SAN LEANDRO, CALIFORNIA**

Sample ID	Date	Depth (fbg)	TPHg	Benzene	Toluene	Ethyl-benzene	Total Xylenes	MTBE (8020)	MTBE (8260)	TBA	ETBE	DIPE	TAME	1,2-DCA	EDB	Ethanol	TOG	Lead
MW-12/SB-24-10	5/26/2006	10	<0.100	0.0241	0.00776	<0.00200	<0.00500	--	<0.00200	<0.0500	<0.00500	<0.00200	<0.00200	<0.00200	<0.00200	--	--	--
MW-12/SB-24-15	5/26/2006	15	<0.100	0.00479	<0.00200	<0.00200	<0.00500	--	<0.00200	<0.0500	<0.00500	<0.00200	<0.00200	<0.00200	<0.00200	--	--	--
MW-12/SB-24-20	5/26/2006	20	0.288	0.0134	0.00609	<0.00200	<0.00500	--	<0.00200	<0.0500	<0.00500	<0.00200	<0.00200	<0.00200	<0.00200	--	--	--
MW-12/SB-24-24	5/26/2006	24	848	1.38	8.16	8.10	41.5	--	<0.100	<2.50	<0.250	<0.100	<0.100	<0.100	<0.100	--	--	--
<u>2007 Subsurface Investigation</u>																		
SVP-1-4.5'	8/28/2007	4.5	<0.50 ⁱ	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.050	<0.010	<0.010	<0.010	<0.0050	<0.0050	--	--	--
SVP-2-4.5'	8/28/2007	4.5	<0.50 ⁱ	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.050	<0.010	<0.010	<0.010	<0.0050	<0.0050	--	--	--
SVP-3-4.5'	8/28/2007	4.5	<0.50 ⁱ	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.050	<0.010	<0.010	<0.010	<0.0050	<0.0050	--	--	--
SVP-4-4.5'	8/28/2007	4.5	150 ^{h,i}	<0.12	0.24	3.8	12.13	--	<0.12	<12	<0.25	<0.25	<0.25	<0.12	<0.12	--	--	--
SVP-5-4.5'	8/28/2007	4.5	<0.50 ⁱ	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.050	<0.010	<0.010	<0.010	<0.0050	<0.0050	--	--	--
B-1-5	9/14/2007	5	55 ⁱ	<0.12	<0.12	0.27	1.0	--	<0.12	--	--	--	--	<0.12	<0.12	--	--	--
B-1-10	9/14/2007	10	24 ⁱ	0.28	0.0094	0.13	0.1156	--	<0.0050	--	--	--	--	<0.0050	<0.0050	--	--	--
B-1-15	9/14/2007	15	6.6 ⁱ	0.038	<0.0050	0.17	0.19	--	<0.0050	--	--	--	--	<0.0050	<0.0050	--	--	--
B-1-17	9/14/2007	17	160 ⁱ	<0.12	<0.12	1.7	6.53	--	<0.12	--	--	--	--	<0.12	<0.12	--	--	--
B-1-20	9/14/2007	20	550 ⁱ	<0.62	<0.62	6.0	30.6	--	<0.62	--	--	--	--	<0.62	<0.62	--	--	--
B-1-25	9/14/2007	25	310 ⁱ	0.38	<0.12	3.5	11.8	--	<0.12	--	--	--	--	<0.12	<0.12	--	--	--
B-1-29.5	9/14/2007	29.5	1,100ⁱ	4.1	15	19	112	--	<0.62	--	--	--	--	<0.62	<0.62	--	--	--
<u>2008 Subsurface Investigation</u>																		
MW-1A@15'	9/2/2008	15	<0.50	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.050	<0.010	<0.010	<0.010	--	--	--	--	--
MW-1A@20'	9/2/2008	20	<0.50	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.050	<0.010	<0.010	<0.010	--	--	--	--	--
MW-1A@26.5'	9/2/2008	26.5	12 ⁱ	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.050	<0.010	<0.010	<0.010	--	--	--	--	--
P-2A@10'	9/2/2008	10	<0.50	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.050	<0.010	<0.010	<0.010	--	--	--	--	--
P-2A@15'	9/2/2008	15	<0.50	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.050	<0.010	<0.010	<0.010	--	--	--	--	--
EW-1@7'	9/3/2008	7	<0.50	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.050	<0.010	<0.010	<0.010	--	--	--	--	--
EW-1@20'	9/3/2008	20	<0.50	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.050	<0.010	<0.010	<0.010	--	--	--	--	--
EW-1@30'	9/3/2008	30	570	<0.50	<0.50	11	18	--	<0.50	<5.0	<1.0	<1.0	<1.0	--	--	--	--	--
EW-1@35'	9/3/2008	35	1.3	0.073	0.015	0.019	0.075	--	0.16	0.13	<0.010	<0.010	<0.010	--	--	--	--	--
P-2B@29'	9/3/2008	29	150	0.045	<0.0050	2.1	5.7	--	<0.0050	<0.050	<0.010	<0.010	<0.010	--	--	--	--	--
P-2B@35'	9/3/2008	35	<0.50	0.0098	<0.0050	<0.0050	<0.0050	--	0.037	0.28	<0.010	<0.010	<0.010	--	--	--	--	--

TABLE 1
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SHELL-BRANDED SERVICE STATION
1784 150TH STREET, SAN LEANDRO, CALIFORNIA

Sample ID	Date	Depth (fbg)	TPHg	Benzene	Toluene	Ethyl-benzene	Total Xylenes	MTBE (8020)	MTBE (8260)	TBA	ETBE	DIPE	TAME	1,2-DCA	EDB	Ethanol	TOG	Lead
EW-2@5'	9/4/2008	5	<0.50	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.050	<0.010	<0.010	<0.010	--	--	--	--	--
EW-2@10'	9/4/2008	10	<0.50	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.050	<0.010	<0.010	<0.010	--	--	--	--	--
EW-2@16'	9/4/2008	16	<0.50	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.050	<0.010	<0.010	<0.010	--	--	--	--	--
EW-2@20'	9/4/2008	20	<50	<0.50	<0.50	<0.50	0.90	--	<0.50	<5.0	<1.0	<1.0	<1.0	--	--	--	--	--
EW-2@27'	9/4/2008	27	350	1.7	<1.0	7.2	18	--	<1.0	<10	<2.0	<2.0	<2.0	--	--	--	--	--
EW-2@33.5'	9/4/2008	33.5	0.55	0.091	<0.0050	0.0095	0.0099	--	0.34 ¹	0.32	<0.010	<0.010	<0.010	--	--	--	--	--
P-1B@7'	9/4/2008	7	<0.50	<0.0050	<0.0050	<0.0050	0.0067	--	<0.0050	<0.050	<0.010	<0.010	<0.010	--	--	--	--	--
P-1B@10'	9/4/2008	10	<0.50	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.050	<0.010	<0.010	<0.010	--	--	--	--	--
P-1B@15'	9/4/2008	15	<0.50	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.050	<0.010	<0.010	<0.010	--	--	--	--	--
P-1B@25'	9/4/2008	25	<0.50	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.050	<0.010	<0.010	<0.010	--	--	--	--	--
P-1B@30'	9/4/2008	30	490	2.0	<1.0	9.1	41	--	<1.0	<10	<2.0	<2.0	<2.0	--	--	--	--	--
P-1B@35.5'	9/4/2008	35.5	<0.50	0.020	0.013	0.0092	0.035	--	0.027	0.064	<0.010	<0.010	<0.010	--	--	--	--	--
P-3B@5'	9/5/2008	5	<0.50	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.050	<0.010	<0.010	<0.010	--	--	--	--	--
P-3B@15'	9/5/2008	15	<0.50	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.050	<0.010	<0.010	<0.010	--	--	--	--	--
P-3B@20'	9/5/2008	20	150	<0.50	0.83	1.8	5.2	--	<0.50	<5.0	<1.0	<1.0	<1.0	--	--	--	--	--
P-3B@27'	9/5/2008	27	990	<5.0	13	21	61	--	<5.0	<50	<10	<10	<10	--	--	--	--	--
P-3B@31.5'	9/5/2008	31.5	2.2	0.71	0.050	0.065	0.21	--	0.16	0.22	<0.010	<0.010	<0.010	--	--	--	--	--
P-4B@8'	9/5/2008	8	<0.50	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.050	<0.010	<0.010	<0.010	--	--	--	--	--
P-4B@16'	9/5/2008	16	<0.50	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.050	<0.010	<0.010	<0.010	--	--	--	--	--
P-4B@22'	9/5/2008	22	65	<0.50	<0.50	0.53	1.3	--	<0.50	<5.0	<1.0	<1.0	<1.0	--	--	--	--	--
P-4B@25'	9/5/2008	25	150	<0.50	0.96	2.7	16	--	<0.50	<5.0	<1.0	<1.0	<1.0	--	--	--	--	--
P-4B@32.5'	9/5/2008	32.5	<50	0.59	<0.50	<0.50	<0.50	--	0.69	<5.0	<1.0	<1.0	<1.0	--	--	--	--	--
MW-2B@30'	10/28/2008	30	<0.50	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.050	<0.010	<0.010	<0.010	--	--	--	--	--
MW-2B@37'	10/28/2008	37	<0.50	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.050	<0.010	<0.010	<0.010	--	--	--	--	--
MW-2B@44'	10/28/2008	44	<0.50	<0.0050	<0.0050	<0.0050	<0.0050	--	<0.0050	<0.050	<0.010	<0.010	<0.010	--	--	--	--	--
MW-2B@49.5'	10/28/2008	49.5	<0.50	<0.0050	<0.0050	0.0052	<0.0050	--	<0.0050	<0.050	<0.010	<0.010	<0.010	--	--	--	--	--
MW-1B@44'	10/28/2008	44	<0.50	<0.0050	<0.0050	0.0052	<0.0050	--	0.016	<0.050	<0.010	<0.010	<0.010	--	--	--	--	--
MW-1B@49.5'	10/28/2008	49.5	<0.50	<0.0050	<0.0050	0.0052	<0.0050	--	0.018	<0.050	<0.010	<0.010	<0.010	--	--	--	--	--
Shallow Soil (≤10 fbg) ESL^k:			180	0.27	9.3	4.7	11	8.4	8.4	110	NA	NA	NA	0.48	0.044	NA	NA	750
Deep Soil (>10 fbg) ESL^k:			180	2.0	9.3	4.7	11	8.4	8.4	110	NA	NA	NA	1.8	1.0	NA	NA	750

TABLE 1

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SHELL-BRANDED SERVICE STATION
1784 150TH STREET, SAN LEANDRO, CALIFORNIA**

Sample ID	Date	Depth (ftg)	TPHg	Benzene	Toluene	Ethyl- benzene	Total Xylenes	MTBE (8020)	MTBE (8260)	TBA	ETBE	DIPE	TAME	1,2-DCA	EDB	Ethanol	TOG	Lead
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Notes:

All results in milligrams per kilograms (mg/kg) unless otherwise indicated.

TPHg = Total petroleum hydrocarbons as gasoline. Before 2001, analyzed by modified EPA Method 8015; from 2001 through present, analyzed by EPA Method 8260B unless otherwise noted.

Benzene, toluene, ethylbenzene, and xylenes analyzed by EPA Method 8260B; before 2001, analyzed by EPA Method 8020.

MTBE = Methyl tertiary-butyl ether analyzed by EPA Method 8020 or EPA Method 8260 (as indicated).

TBA = Tertiary-butyl alcohol analyzed by EPA Method 8260B

DIPE = Di-isopropyl ether analyzed by EPA Method 8260B

ETBE = Ethyl tertiary-butyl ether analyzed by EPA Method 8260B

TAME = Tertiary-amyl methyl ether analyzed by EPA Method 8260B

1,2-DCA = 1,2-dichloroethane analyzed by EPA Method 8260B; prior to 2004, analyzed by EPA Method 8010

EDB = Ethyl di-bromide, analyzed by EPA Method 8260B analyzed by EPA Method 8260B

Ethanol analyzed by EPA Method 8260B

TOG = Total oil and grease analyzed by American Public Health Association Standard Method 503E

Lead analyzed by EPA Method 6010B

ftg = feet below grade

<x = Not detected at reporting limit x

-- = Not analyzed

NA = ESL not published

a = Petroleum oil and grease analyzed by American Public Health Association Standard Method 503E; none detected.

b = Analyzed for halogenated volatile organic compounds by EPA Method 8010; none detected.

c = Total petroleum hydrocarbons as diesel (TPHd) and total petroleum hydrocarbons as motor oil (TPHmo) analyzed by modified EPA Method 8015; none detected.

d = TPHd detected at 23 mg/kg by modified EPA Method 8015; lab characterized detected compounds as hydrocarbons lighter than diesel.

e = TPHd detected at 4.9 mg/kg by modified EPA Method 8015; lab characterized detected compounds as hydrocarbons lighter than diesel.

f = Analyzed for volatile organic compounds by EPA Method 8010; none detected.

g = Sample saturated with perched water from beneath dispenser.

h = The sample chromatographic pattern for TPH does not match the chromatographic pattern of the specified standard. Quantification of the unknown hydrocarbon(s) in the sample was based upon the specified standard.

i = Analyzed by EPA Method 8015B.

j = Analyte was detected at a concentration below the reporting limit and above the laboratory method detection limit. Reported value is estimated.

k = San Francisco Bay Regional Water Quality Control Board commercial/industrial Environmental Screening Level for soil where groundwater is not a source of drinking water (Tables B and D of *Screening for Environmental Concerns at Sites With Contaminated Soil and Groundwater*, California Regional Water Quality Control Board, Interim Final - November 2007 [Revised May 2008]).

APPENDIX D

HISTORICAL GROUNDWATER DATA

Table 2. Historical Grab Groundwater Analytical Data - Shell-branded Service Station, Incident No.98996068, 1784 150th Avenue, San Leandro, California

Sample ID	Sample Date	Depth (fbg)	TPHg	Benzene	Toluene	Ethyl-benzene	Total Xylenes	MTBE	(ppb)						
									TBA	DIPE	ETBE	TAME	1,2 DCA	EDB	Ethanol
1994 Subsurface Investigation															
BH-1	6/6/1994		<50	<0.50	<0.50	<0.50	<0.50	---	---	---	---	---	---	---	
BH-2	6/6/1994		5,200 a	8.8	<0.50	9.1	<0.50	---	---	---	---	---	---	---	
BH-3	6/6/1994		120,000 b	25,000	14,000	3,100	13,000	---	---	---	---	---	---	---	
BH-4	6/7/1994		<50	<0.50	<0.50	<0.50	<0.50	---	---	---	---	---	---	---	
BH-5	6/7/1994		<50	<0.50	<0.50	<0.50	<0.50	---	---	---	---	---	---	---	
BH-6	6/7/1994		<50	<0.50	<0.50	<0.50	<0.50	---	---	---	---	---	---	---	
1995 Monitoring Well Installation															
BH-7-17-W	2/14/1995		100	1.0	1.0	<0.5	<0.5	---	---	---	---	---	---	---	
BH-9-20-W	2/14/1995		90	0.9	0.9	<0.5	<0.5	---	---	---	---	---	---	---	
1998 Subsurface Investigation															
SVS-11-W1	11/10/1998		130,000	18,000	1,800	5,700	31,000	1,500	---	---	---	---	---	---	
SVS-12-W1	11/11/1998		64,000	1,800	770	2,700	17,000	<250	---	---	---	---	---	---	
SVS-14-W1	11/11/1998		<50	<0.50	<0.50	<0.50	<0.50	<2.5	---	---	---	---	---	---	
SVS-15-W1	11/11/1998		<50	<0.50	<0.50	<0.50	0.80	<2.5	---	---	---	---	---	---	
SVS-16-W1	11/11/1998		<50	<0.50	<0.50	<0.50	<0.50	<2.5	---	---	---	---	---	---	
2002 Monitoring Well Installation															
MW7-W	10/3/2002		60,000	59	590	1,900	7,300	<100	---	---	---	---	---	---	
MW8-W	10/4/2002		83,000	810	2,000	3,700	17,000	<500	---	---	---	---	---	---	
SB9-W	10/4/2002		78,000	2,200	8,200	2,300	13,000	<500	---	---	---	---	---	---	
2003 Subsurface Investigation															
SB-10-W	6/23/2003		<50	1.1	0.84	<0.50	1.7	<0.50	<5.0	<2.0	<2.0	<2.0	<0.50	<0.50	
SB-11-W	6/24/2003		75	0.84	0.53	1.5	7.1	<0.50	<5.0	<2.0	<2.0	<2.0	<0.50	<0.50	
SB-12-W	6/24/2003		<50	<0.50	<0.50	<0.50	<1.0	<0.50	<5.0	<2.0	<2.0	<2.0	<0.50	<0.50	
SB-13-W	6/23/2003		<50	0.89	0.52	<0.50	<1.0	<0.50	<5.0	<2.0	<2.0	<2.0	<0.50	<0.50	
SB-14-W	6/24/2003		67,000	<100	280	3,800	16,000	<100	<1000	<400	<400	<400	<100	<100	
SB-15-W	6/26/2003		6,800	530	<25	380	560	40	<250	<100	<100	<100	<25	<25	
SB-16-W	6/23/2003		<50	0.67	<0.50	<0.50	<1.0	<0.50	<5.0	<2.0	<2.0	<2.0	<0.50	<0.50	
2004 Subsurface Investigation															
SB-17-W	9/13/2004		<50	<0.50	4.2	2.0	7.9	<0.50	<5.0	<2.0	<2.0	<2.0	<0.50	<0.50	
SB-18-W	9/13/2004		55	<0.50	5.5	2.5	10.0	<0.50	<5.0	<2.0	<2.0	<2.0	<0.50	<0.50	

Table 2. Historical Grab Groundwater Analytical Data - Shell-branded Service Station, Incident No.98996068, 1784 150th Avenue, San Leandro, California

Sample ID	Sample Date	Depth (fbg)	TPHg	Benzene	Toluene	Ethyl-benzene	Total Xylenes	MTBE	TBA	DIPE	ETBE	TAME	1,2 DCA	EDB	Ethanol
			(ppb)												
2006 Subsurface Investigation															
SB-25W-20	5/24/2006		<50.0	0.570	0.650	1.69	3.28	<0.500	<10.0	<0.500	<0.500	<0.500	2.96	<0.500	---
SB-25W-31	5/24/2006		<50.0	<0.500	<0.500	0.520	<0.500	<0.500	<10.0	<0.500	<0.500	<0.500	3.10	<0.500	---
2007 Subsurface Investigation															
CPT-1-41'-45'	8/30/2007	41-45	650	27	4.3	14	43.4	1,100	430	2.0	<2.0	<2.0	92	<1.0	---
CPT-1-54'-58'	8/31/2007	54-58	<50 d	8.0	0.64 e	2.6	5.39 e	120	<10	<2.0	<2.0	<2.0	97	<1.0	---
CPT-1-70'-74'	8/31/2007	70-74	<50	4.1	0.62 e	1.0	1.97 e	2.1	<10	<2.0	<2.0	<2.0	<0.50	<1.0	---
CPT-2-35'-39'	8/29/2007	35-39	310	41	4.7	12	50	54	<10	<2.0	<2.0	<2.0	11	<1.0	---
CPT-2-53'-57'	8/29/2007	53-57	<50	1.5	0.83 e	1.1	4.7	2.1	<10	<2.0	<2.0	<2.0	13	<1.0	---
CPT-2-68'-72'	8/29/2007	68-72	<50	5.3	1.8	4.2	16.3	0.63 e	<10	<2.0	<2.0	<2.0	<0.50	<1.0	---
CPT-3-23'-27'	8/28/2007	23-27	3,600	0.94	0.32 e	18	8.8	35	11	<2.0	<2.0	<2.0	8.2	<1.0	---
CPT-3-49'-53'	8/29/2007	49-53	<50	1.5	0.51 e	0.43 e	<1.0	<1.0	<10	<2.0	<2.0	<2.0	<0.50	<1.0	---
CPT-3-69'-73'	8/29/2007	69-73	<50	0.42 e	<1.0	<1.0	<1.0	<1.0	<10	<2.0	<2.0	<2.0	<0.50	<1.0	---
CPT-5-41'-45'	8/30/2007	41-45	<50	0.88	0.34 e	<1.0	<1.0	<1.0	<10	<2.0	<2.0	<2.0	<0.50	<1.0	---
CPT-5-54'-57'	8/31/2007	54-57	<50	<0.50	<1.0	<1.0	<1.0	<1.0	<10	<2.0	<2.0	<2.0	6.6	<1.0	---
CPT-5-70'-74'	8/31/2007	70-74	<50	<0.50	<1.0	<1.0	<1.0	<1.0	<10	<2.0	<2.0	<2.0	<0.50	<1.0	---
CPT-6-40'-44'	8/30/2007	40-44	<50	<0.50	<1.0	<1.0	<1.0	<1.0	<10	<2.0	<2.0	<2.0	<0.50	<1.0	---
CPT-6-70'-74'	8/30/2007	70-74	<50	<0.50	<1.0	<1.0	<1.0	20	<10	<2.0	<2.0	<2.0	15	<1.0	---
Groundwater ESL:			500	46	130	290	100	1,800	18,000	N/A	N/A	N/A	200	150	5,000

Abbreviations and Notes:

TPHg = Total petroleum hydrocarbons as gasoline by modified EPA Method 8015 in 1998, and by EPA Method 8260B thereafter

Benzene, toluene, ethylbenzene and total xylenes by EPA Method 8020 in 1998, and by EPA Method 8260B thereafter.

MTBE = Methyl tertiary butyl ether by EPA Method 8020 in 1998 and by EPA Method 8260B thereafter

TBA = Tert-Butyl alcohol, analyzed by EPA Method 8260B

ETBE = Ethyl tert butyl ether, analyzed by EPA Method 8260B

DIPE = Di-isopropyl Ether, analyzed by EPA Method 8260B

TAME = Tert-Amyl methyl ether, analyzed by EPA Method 8260B

1,2-DCA = 1,2-dichloroethane

EDB = Ethyl di-bromide, analyzed by EPA Method 8260B

Ethanol analyzed by EPA Method 8260B

Table 2. Historical Grab Groundwater Analytical Data - Shell-branded Service Station, Incident No.98996068, 1784 150th Avenue, San Leandro, California

Sample ID	Sample Date	Depth (fbg)	TPHg	Benzene	Toluene	Ethyl-benzene	Total Xylenes	MTBE	TBA	DIPE	ETBE	TAME	1,2 DCA	EDB	Ethanol
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ppb = Parts per billion

--- = Not analyzed

a = Chromatogram pattern as weathered gasoline

b = Chromatogram pattern as gasoline

c = San Francisco Bay Regional Water Quality Control Board Environmental Screening Level where groundwater is not a source of drinking water

d = The sample chromatographic pattern for TPH does not match the chromatographic pattern of the specified standard. Quantification of the unknown hydrocarbon(s) in the sample was based upon the specified standard.

e = Analyte was detected at a concentration below the reporting limit and above the laboratory method detection limit. Reported value is estimated.

WELL CONCENTRATIONS
Shell-branded Service Station
1784 150th Avenue
San Leandro, CA

Well ID	Date	TPPH (ug/L)	TEPH (ug/L)	B (ug/L)	T (ug/L)	E (ug/L)	X (ug/L)	MTBE 8020 (ug/L)	MTBE 8260 (ug/L)	DIPE (ug/L)	ETBE (ug/L)	TAME (ug/L)	TBA (ug/L)	1,2- DCA (ug/L)	EDB (ug/L)	TOC (MSL)	Depth to Water (ft.)	GW Elevation (MSL)	SPH Thickness (ft.)	DO Reading (ppm)
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EW-1	09/15/2008	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	48.44	23.26	25.18	NA	NA
EW-1	01/06/2009	43,000	NA	1,600	860	1,500	3,800	NA	500	NA	NA	NA	NA	NA	NA	48.44	22.51	25.93	NA	0.18
EW-1	03/10/2009	39,000	NA	2,500	1,300	1,700	5,300	NA	390	NA	NA	NA	NA	NA	NA	48.44	19.58	28.86	NA	1.21

EW-2	09/15/2008	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	44.52	19.35	25.17	NA	NA
EW-2	01/06/2009	85,000	NA	970	1,400	3,200	20,000	NA	150	NA	NA	NA	NA	NA	NA	44.52	18.63	25.89	NA	0.22
EW-2	03/10/2009	67,000	NA	190	650	3,100	21,000	NA	<100	NA	NA	NA	NA	NA	NA	44.52	16.21	28.31	NA	0.76

MW-1	03/08/1990	510	120	1.5	0.8	<0.5	5.4	NA	NA	NA	NA	NA	NA	NA	NA	49.13	25.29	23.84	NA	NA
MW-1	06/12/1990	390	100	86	1.3	0.7	6.2	NA	NA	NA	NA	NA	NA	NA	NA	49.13	25.85	23.28	NA	NA
MW-1	09/13/1990	100	130	56	0.75	2.4	2.8	NA	NA	NA	NA	NA	NA	NA	NA	49.13	27.49	21.64	NA	NA
MW-1	12/18/1990	480	<50	54	1.7	3.3	3.7	NA	NA	NA	NA	NA	NA	NA	NA	49.13	27.41	21.72	NA	NA
MW-1	03/07/1991	80	<50	266	<0.5	1.2	<1.5	NA	NA	NA	NA	NA	NA	NA	NA	49.13	25.79	23.34	NA	NA
MW-1	06/07/1991	510	<50	130	3.8	6.1	11	NA	NA	NA	NA	NA	NA	NA	NA	49.13	25.64	23.49	NA	NA
MW-1	09/17/1991	330	120 a	67	<0.5	3.0	2.2	NA	NA	NA	NA	NA	NA	NA	NA	49.13	27.54	21.59	NA	NA
MW-1	12/09/1991	140a	80	<0.5	<0.5	1.7	4.7	NA	NA	NA	NA	NA	NA	NA	NA	49.13	27.81	21.32	NA	NA
MW-1	02/13/1992	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	49.13	25.57	23.56	NA	NA
MW-1	02/24/1992	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	49.13	22.83	26.30	NA	NA
MW-1	02/27/1992	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	49.13	23.09	26.04	NA	NA
MW-1	03/01/1992	<50	<50	<0.5	<0.5	<0.5	<0.5	NA	NA	NA	NA	NA	NA	NA	NA	49.13	23.26	25.87	NA	NA
MW-1	06/03/1992	1,500	NA	520	180	72	230	NA	NA	NA	NA	NA	NA	NA	NA	49.13	24.64	24.49	NA	NA
MW-1	09/01/1992	130	NA	16	1.4	1.8	3.4	NA	NA	NA	NA	NA	NA	NA	NA	49.13	26.74	22.39	NA	NA
MW-1	10/06/1992	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	49.13	27.18	21.95	NA	NA
MW-1	11/11/1992	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	49.13	27.99	21.14	NA	NA
MW-1	12/04/1992	150	NA	360	0.7	1.8	2.1	NA	NA	NA	NA	NA	NA	NA	NA	49.13	27.14	21.99	NA	NA
MW-1	01/22/1993	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	49.13	20.09	29.04	NA	NA
MW-1	02/10/1993	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	49.13	24.26	24.87	NA	NA
MW-1	03/03/1993	<50	NA	1.5	<0.5	<0.5	<0.5	NA	NA	NA	NA	NA	NA	NA	NA	49.13	20.50	28.63	NA	NA
MW-1	05/11/1993	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	49.13	21.70	27.43	NA	NA
MW-1	06/17/1993	1,600	NA	340	120	120	440	NA	NA	NA	NA	NA	NA	NA	NA	49.13	22.42	26.71	NA	NA
MW-1	09/10/1993	2,600	NA	670	340	310	730	NA	NA	NA	NA	NA	NA	NA	NA	49.13	24.11	25.02	NA	NA
MW-1	12/13/1993	11,000	NA	470	320	380	2,300	NA	NA	NA	NA	NA	NA	NA	NA	49.13	23.73	25.40	NA	NA
MW-1	03/03/1994	16,000	NA	700	690	480	3,200	NA	NA	NA	NA	NA	NA	NA	NA	49.13	22.08	27.05	NA	NA
MW-1	06/06/1994	7,500	NA	420	280	200	1,000	NA	NA	NA	NA	NA	NA	NA	NA	49.13	23.10	26.03	NA	NA
MW-1	09/12/1994	1,200	NA	110	21	3.3	420	NA	NA	NA	NA	NA	NA	NA	NA	49.13	25.19	23.94	NA	NA

WELL CONCENTRATIONS
Shell-branded Service Station
1784 150th Avenue
San Leandro, CA

Well ID	Date	TPPH (ug/L)	TEPH (ug/L)	B (ug/L)	T (ug/L)	E (ug/L)	X (ug/L)	MTBE 8020 (ug/L)	MTBE 8260 (ug/L)	DIPE (ug/L)	ETBE (ug/L)	TAME (ug/L)	TBA (ug/L)	1,2- DCA (ug/L)	EDB (ug/L)	TOC (MSL)	Depth to Water (ft.)	GW Elevation (MSL)	SPH Thickness (ft.)	DO Reading (ppm)
MW-1	12/19/1994	4,600	NA	470	330	230	1,300	NA	NA	NA	NA	NA	NA	NA	NA	49.13	23.06	26.07	NA	NA
MW-1	02/28/1995	500	NA	59	32	6.8	68	NA	NA	NA	NA	NA	NA	NA	NA	49.13	20.90	28.23	NA	NA
MW-1	03/24/1995	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	49.13	18.28	30.85	NA	NA
MW-1	06/26/1995	5,500	NA	740	420	300	1,800	NA	NA	NA	NA	NA	NA	NA	NA	49.13	20.40	28.73	NA	NA
MW-1	09/13/1995	84,000	NA	1,900	2,600	3,000	14,000	NA	NA	NA	NA	NA	NA	NA	NA	49.13	22.62	26.51	NA	NA
MW-1	12/19/1995	80,000	NA	660	350	170	18,000	NA	NA	NA	NA	NA	NA	NA	NA	49.13	22.10	27.03	NA	NA
MW-1	03/07/1996	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	49.13	18.83	30.34	0.05	NA
MW-1	06/28/1996	270,000	NA	2,800	820	1,000	16,000	<0.5	NA	NA	NA	NA	NA	NA	NA	49.13	21.46	27.67	NA	NA
MW-1 (D)	06/28/1996	790,000	NA	2,200	780	1,000	13,000	15,000	NA	NA	NA	NA	NA	NA	NA	49.13	21.46	27.67	NA	NA
MW-1	09/26/1996	29,000	NA	1,100	260	270	1,900	<1,000	NA	NA	NA	NA	NA	NA	NA	49.13	23.57	25.57	0.01	NA
MW-1	09/26/1996	25,000	NA	1,200	320	240	1,900	<1,000	NA	NA	NA	NA	NA	NA	NA	49.13	NA	NA	NA	NA
MW-1	12/10/1996	13,000	NA	510	240	230	1,200	100	NA	NA	NA	NA	NA	NA	NA	49.13	21.43	27.70	NA	1.0
MW-1 (D)	12/10/1996	8,400	NA	420	130	140	680	81	NA	NA	NA	NA	NA	NA	NA	49.13	21.43	27.70	NA	1.0
MW-1	03/10/1997	4,200	NA	13	8.8	16	74	<12	NA	NA	NA	NA	NA	NA	NA	49.13	20.08	29.05	NA	2.0
MW-1 (D)	03/10/1997	5,100	NA	12	8.9	17	79	<25	NA	NA	NA	NA	NA	NA	NA	49.13	20.08	29.05	NA	2.0
MW-1	06/30/1997	5,700	NA	320	120	140	700	47	NA	NA	NA	NA	NA	NA	NA	49.13	21.68	27.45	NA	1.6
MW-1 (D)	06/30/1997	5,300	NA	300	95	120	580	45	NA	NA	NA	NA	NA	NA	NA	49.13	21.68	27.45	NA	1.6
MW-1	09/12/1997	6,300	NA	120	26	82	260	30	NA	NA	NA	NA	NA	NA	NA	49.13	21.78	27.35	NA	2.1
MW-1 b	12/18/1997	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	49.13	20.78	28.35	NA	1.3
MW-1	02/02/1998	84	NA	5.1	<0.50	<0.50	2.1	2.5	NA	NA	NA	NA	NA	NA	NA	49.13	19.65	29.48	NA	2.0
MW-1	06/24/1998	13,000	NA	3,000	260	410	1,400	<250	NA	NA	NA	NA	NA	NA	NA	49.13	19.65	29.48	NA	2.5
MW-1 (D)	06/24/1998	12,000	NA	3,800	250	47	1,400	710	NA	NA	NA	NA	NA	NA	NA	49.13	19.65	29.48	NA	2.5
MW-1	08/26/1998	3,100	NA	1,200	27	170	50	88	NA	NA	NA	NA	NA	NA	NA	49.13	20.49	28.64	NA	2.1
MW-1	12/23/1998	45,000	NA	5,300	220	1,000	3,600	970	NA	NA	NA	NA	NA	NA	NA	49.13	21.22	27.91	NA	3.8
MW-1	03/01/1999	22,300	NA	2,540	436	753	3,370	<400	NA	NA	NA	NA	NA	NA	NA	49.13	19.27	29.86	NA	1.8
MW-1	06/14/1999	18,800	NA	6,820	210	436	958	1,360	NA	NA	NA	NA	NA	NA	NA	49.13	20.80	28.33	NA	2.2
MW-1	09/28/1999	21,500	NA	7,470	281	467	927	1,800	NA	NA	NA	NA	NA	NA	NA	49.13	22.55	26.58	NA	2.0
MW-1	12/08/1999	22,300	NA	6,140	135	256	367	232	NA	NA	NA	NA	NA	NA	NA	49.13	23.12	26.01	NA	2.1
MW-1	03/14/2000	6,690	NA	1,880	63.5	134	307	460	NA	NA	NA	NA	NA	NA	NA	49.13	18.87	30.26	NA	2.3
MW-1	06/28/2000	8,080	NA	2,690	85.1	149	514	701	NA	NA	NA	NA	NA	NA	NA	49.13	21.12	28.01	NA	2.4
MW-1	09/06/2000	17,800	NA	7,390	212	329	1,270	<1,000	NA	NA	NA	NA	NA	NA	NA	49.13	21.90	27.23	NA	3.0
MW-1	12/14/2000	8,900	NA	4,870	79.2	106	370	1,840	673*	NA	NA	NA	NA	NA	NA	49.13	22.60	26.53	NA	2.0
MW-1	03/05/2001	7,520	NA	2,120	66.0	107	129	668	NA	NA	NA	NA	NA	NA	NA	49.13	20.06	29.07	NA	0.4
MW-1	06/11/2001	30,000	NA	7,400	390	600	2,300	NA	170	NA	NA	NA	NA	NA	NA	49.13	22.39	26.74	NA	1.6
MW-1	09/12/2001	23,000	NA	7,500	120	280	910	NA	320	NA	NA	NA	NA	NA	NA	49.13	23.37	25.76	NA	2.2

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MW-1	12/27/2001	16,000	NA	2,400	190	330	1,500	NA	350	NA	NA	NA	NA	NA	NA	49.13	20.97	28.16	NA	1.3
MW-1	02/27/2002	26,000	NA	6,100	330	510	2,000	NA	210	NA	NA	NA	NA	NA	NA	49.10	20.47	28.63	NA	1.3
MW-1	06/18/2002	29,000	NA	8,100	280	510	1,800	NA	140	NA	NA	NA	NA	NA	NA	49.10	21.99	27.11	NA	2.2
MW-1	09/18/2002	34,000	NA	5,900	350	700	3,000	NA	<250	NA	NA	NA	NA	NA	NA	49.10	23.21	25.89	NA	0.8
MW-1	12/27/2002	7,500	NA	1,200	30	120	410	NA	230	<5.0	<5.0	<5.0	310	31	<5.0	49.10	20.10	29.00	NA	0.6
MW-1	03/05/2003	17,000	NA	1,600	88	400	1,400	NA	230	NA	NA	<10	290	<10	NA	49.10	21.05	28.05	NA	1.7
MW-1	06/24/2003	Well inaccessible		NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	49.10	NA	NA	NA	NA
MW-1	06/25/2003	14,000	NA	5,300	250	440	2,100	NA	100	NA	NA	<200	<500	<50	NA	49.10	21.93	27.17	NA	0.9
MW-1	09/25/2003	33,000	NA	7,700	250	860	3,400	NA	130	NA	NA	<200	<500	<50	NA	49.10	23.21	25.89	NA	1.7
MW-1	12/15/2003	63,000	NA	14,000	360	1,300	3,900	NA	150	NA	NA	<400	<1000	<100	NA	49.10	22.08	27.02	NA	1.5
MW-1	03/04/2004	28,000	NA	8,000	180	640	2,100	NA	79	NA	NA	<200	<500	<50	NA	49.10	19.85	29.25	NA	0.2
MW-1	05/27/2004	33,000	NA	8,700	260	840	2,700	NA	81	NA	NA	<200	<500	<50	NA	49.10	22.15	26.95	NA	0.2
MW-1	09/24/2004	26,000	NA	5,700	210	830	2,900	NA	<50	<200	<200	<200	<500	<50	<50	49.10	23.69	25.41	NA	1.5
MW-1	11/22/2004	100,000	NA	2,500	920	4,100	22,000	NA	130	NA	NA	<200	<500	<50	NA	49.10	23.19	25.91	NA	NA
MW-1	03/02/2005	110,000	NA	1,300	670	4,000	23,000	NA	87	NA	NA	<100	<500	<25	NA	49.10	19.35	29.75	NA	NA
MW-1	06/30/2005	94,000	NA	6,500	1,100	3,900	21,000	NA	900	NA	NA	<1,000	<2,500	<250	NA	49.10	20.64	28.46	NA	0.6
MW-1	09/20/2005	63,000	NA	3,900	540	2,000	14,000	NA	1,100	<800	<800	<800	<2,000	<200	NA	49.10	22.06	27.04	NA	NA
MW-1	12/05/2005	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	49.10	21.90	27.25	0.06	NA
MW-1	03/02/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	49.10	17.54	31.60	0.05	NA
MW-1 (n)	06/29/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	49.10	NA	NA	NA	NA
MW-1 (o)	06/30/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	49.10	20.16	28.97	0.04	NA
MW-1	07/06/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	49.10	20.26	28.86	0.03	NA
MW-1	09/11/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	49.10	21.24	27.91	0.06	NA
MW-1	12/28/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	49.10	20.83	28.30	0.04	NA
MW-1	03/20/2007	43,600	NA	11,900	348	964	1,450	NA	9,180	NA	NA	<200	<10,000	<100	NA	49.10	20.88	28.22	NA	0.26
MW-1	06/01/2007	22,000 q	NA	7,900	120	310	424 r	NA	7,800	NA	NA	NA	NA	NA	NA	49.10	21.93	27.17	NA	0.72
MW-1	06/26/2007	20,000 q	NA	6,700	110	360	730	NA	6,500	NA	NA	<200	2,200	<50	NA	49.10	22.30	26.80	NA	1.33
MW-1	07/19/2007	26,000 q	NA	6,100	92 r	180	523 r	NA	7,100	NA	NA	NA	NA	NA	NA	49.10	22.70	26.40	NA	2.89
MW-1	08/14/2007	44,000 q	NA	6,300	130	910	4,100	NA	6,300	NA	NA	NA	NA	NA	NA	49.10	22.90	26.20	NA	1.9
MW-1	09/11/2007	38,000 q	NA	8,100	140	670	1,770	NA	5,700	<100	<100	<100	3,000	<25	NA	49.10	23.65	25.45	NA	0.84
MW-1	10/26/2007	40,000 q	NA	9,500	120	540	1,370	NA	6,300	NA	NA	NA	NA	NA	NA	49.10	23.04	26.06	NA	0.9
MW-1	11/13/2007	36,000 q	NA	8,400	110	480	1,400	NA	7,100	NA	NA	NA	NA	NA	NA	49.10	22.99	26.11	NA	0.30
MW-1	12/26/2007	33,000 q	NA	8,600	120	550	1,330	NA	5,300	NA	NA	<100	2,500	<25	NA	49.10	22.37	26.73	NA	0.5
MW-1	01/03/2008	42,000 q	NA	9,900	170	810	2,140	NA	5,300	NA	NA	NA	NA	NA	NA	49.10	22.53	26.57	NA	1.63
MW-1	02/21/2008	32,000 q	NA	9,900	540	1,100	2,260	NA	5,500	NA	NA	NA	NA	NA	NA	49.10	20.42	28.68	NA	2.1

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MW-1	03/19/2008	41,000 q	NA	9,900	620	1,300	2,280	NA	5,600	NA	NA	NA	6,900	<50	NA	49.10	21.01	28.09	NA	0.24
MW-1	04/16/2008	53,000	NA	10,000	430	1,100	2,200	NA	5,500	NA	NA	NA	NA	NA	NA	49.10	21.49	27.61	NA	1.70
MW-1	05/29/2008	47,000	NA	9,100	670	1,100	2,270	NA	4,600	NA	NA	NA	NA	NA	NA	49.10	22.17	26.93	NA	1.10
MW-1	06/05/2008	51,000	NA	7,900	660	1,100	2,780	NA	4,600	<200	<200	<200	3,700	<50	NA	49.10	22.31	26.79	NA	0.19
MW-1	07/22/2008	69,000	NA	8,700	510	1,400	3,480	NA	3,100	NA	NA	NA	NA	NA	NA	49.10	23.13	25.98	0.01	1.64
MW-1	09/29/2008	61,000	NA	7,900	560	1,400	2,480	NA	2,300	<200	<200	<200	4,100	<50	NA	49.10	24.04	25.06	NA	0.69
MW-1	Well destroyed		NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
MW-1A	09/15/2008	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	48.99	23.78	25.21	NA	NA
MW-1A	12/19/2008	320	NA	0.54	<1.0	<1.0	<1.0	NA	12	NA	NA	NA	NA	NA	NA	48.99	23.61	25.38	NA	0.38
MW-1A	03/10/2009	570	NA	8.0	<1.0	1.5	1.2	NA	16	NA	NA	NA	NA	NA	NA	48.99	20.15	28.84	NA	1.80
MW-1B	10/31/2008	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	49.07	24.25	24.82	NA	NA
MW-1B	12/19/2008	980	NA	14	<1.0	3.8	15	NA	440	NA	NA	NA	NA	NA	NA	49.07	23.71	25.36	NA	0.42
MW-1B	03/10/2009	790	NA	11	<5.0	<5.0	8.4	NA	450	NA	NA	NA	NA	NA	NA	49.07	20.36	28.71	NA	1.22
MW-2	02/13/1992	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	45.83	22.22	23.61	NA	NA
MW-2	02/24/1992	17,000	2,700 a	6,200	1,600	550	1,900	NA	NA	NA	NA	NA	NA	NA	NA	45.83	19.61	26.22	NA	NA
MW-2	02/27/1992	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	45.83	19.92	25.91	NA	NA
MW-2	03/01/1992	86,000	1,000 a	30,000	34,000	2,300	16,000	NA	NA	NA	NA	NA	NA	NA	NA	45.83	21.11	24.72	NA	NA
MW-2	06/03/1992	87,000	NA	28,000	18,000	2,000	10,000	NA	NA	NA	NA	NA	NA	NA	NA	45.83	21.58	24.25	NA	NA
MW-2	09/01/1992	110,000	NA	21,000	13,000	1,900	7,800	NA	NA	NA	NA	NA	NA	NA	NA	45.83	23.46	22.37	NA	NA
MW-2	10/06/1992	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	45.83	23.99	21.84	NA	NA
MW-2	11/11/1992	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	45.83	24.25	21.58	NA	NA
MW-2	12/04/1992	42,000	NA	15,000	2,400	960	2,900	NA	NA	NA	NA	NA	NA	NA	NA	45.83	23.89	21.94	NA	NA
MW-2	01/22/1993	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	45.83	17.03	28.80	NA	NA
MW-2	02/10/1993	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	45.83	18.08	27.75	NA	NA
MW-2	03/03/1993	160,000	NA	36,000	3,800	32,000	21,000	NA	NA	NA	NA	NA	NA	NA	NA	45.83	17.28	28.55	NA	NA
MW-2 (D)	03/03/1993	150,000	NA	31,000	3,100	20,000	14,000	NA	NA	NA	NA	NA	NA	NA	NA	45.83	17.28	28.55	NA	NA
MW-2	05/11/1993	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	45.83	18.41	27.42	NA	NA
MW-2	06/17/1993	65,000	NA	34,000	15,000	3,200	11,000	NA	NA	NA	NA	NA	NA	NA	NA	45.83	19.06	26.77	NA	NA
MW-2 (D)	06/17/1993	62,000	NA	28,000	14,000	2,700	10,000	NA	NA	NA	NA	NA	NA	NA	NA	45.83	19.06	26.77	NA	NA
MW-2	09/10/1993	72,000	NA	24,000	16,000	2,300	11,000	NA	NA	NA	NA	NA	NA	NA	NA	45.83	20.88	24.95	NA	NA
MW-2 (D)	09/10/1993	71,000	NA	23,000	15,000	2,300	10,000	NA	NA	NA	NA	NA	NA	NA	NA	45.83	20.88	24.95	NA	NA
MW-2	12/13/1993	19,000	NA	5,400	4,900	680	3,100	NA	NA	NA	NA	NA	NA	NA	NA	45.83	20.42	25.41	NA	NA

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MW-2 (D)	12/13/1993	17,000	NA	6,200	5,500	720	3,500	NA	NA	NA	NA	NA	NA	NA	NA	45.83	20.42	25.41	NA	NA
MW-2	03/03/1994	110,000	NA	21,000	24,000	2,000	13,000	NA	NA	NA	NA	NA	NA	NA	NA	45.83	18.48	27.35	NA	NA
MW-2 (D)	03/03/1994	93,000	NA	19,000	22,000	1,800	12,000	NA	NA	NA	NA	NA	NA	NA	NA	45.83	18.48	27.35	NA	NA
MW-2	06/06/1994	10,000	NA	1,900	3,300	2,500	13,000	NA	NA	NA	NA	NA	NA	NA	NA	45.83	20.26	25.57	NA	NA
MW-2 (D)	06/06/1994	99,000	NA	9,900	12,000	2,400	12,000	NA	NA	NA	NA	NA	NA	NA	NA	45.83	20.26	25.57	NA	NA
MW-2	09/12/1994	160,000	NA	22,000	33,000	3,400	23,000	NA	NA	NA	NA	NA	NA	NA	NA	45.83	21.80	24.03	NA	NA
MW-2 (D)	09/12/1994	150,000	NA	23,000	34,000	3,500	23,000	NA	NA	NA	NA	NA	NA	NA	NA	45.83	21.80	24.03	NA	NA
MW-2	12/19/1994	80,000	NA	17,000	16,000	2,300	14,000	NA	NA	NA	NA	NA	NA	NA	NA	45.83	19.66	26.17	NA	NA
MW-2 (D)	12/19/1994	100,000	NA	28,000	26,000	3,400	20,000	NA	NA	NA	NA	NA	NA	NA	NA	45.83	19.66	26.17	NA	NA
MW-2	02/28/1995	100,000	NA	24,000	18,000	2,300	17,000	NA	NA	NA	NA	NA	NA	NA	NA	45.83	17.51	28.32	NA	NA
MW-2 (D)	02/28/1995	100,000	NA	31,000	21,000	3,200	18,000	NA	NA	NA	NA	NA	NA	NA	NA	45.83	17.51	28.32	NA	NA
MW-2	03/24/1995	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	45.83	14.88	30.95	NA	NA
MW-2	06/26/1995	45,000	NA	14,000	12,000	1,500	7,500	NA	NA	NA	NA	NA	NA	NA	NA	45.83	17.58	28.25	NA	NA
MW-2 (D)	06/26/1995	68,000	NA	13,000	11,000	1,800	7,700	NA	NA	NA	NA	NA	NA	NA	NA	45.83	17.58	28.25	NA	NA
MW-2	09/13/1995	110,000	NA	19,000	19,000	2,800	15,000	NA	NA	NA	NA	NA	NA	NA	NA	45.83	19.28	26.55	NA	NA
MW-2 (D)	09/13/1995	120,000	NA	20,000	20,000	2,900	15,000	NA	NA	NA	NA	NA	NA	NA	NA	45.83	19.28	26.55	NA	NA
MW-2	12/19/1995	180,000	NA	18,000	29,000	4,100	24,000	NA	NA	NA	NA	NA	NA	NA	NA	45.83	18.61	27.22	NA	NA
MW-2 (D)	12/19/1995	160,000	NA	18,000	28,000	3,800	24,000	NA	NA	NA	NA	NA	NA	NA	NA	45.83	18.61	27.22	NA	NA
MW-2	03/06/1996	120,000	NA	28,000	15,000	3,900	17,000	NA	NA	NA	NA	NA	NA	NA	NA	45.83	15.41	30.42	NA	NA
MW-2	06/28/1996	96,000	NA	20,000	20,000	4,100	22,000	2,400	NA	NA	NA	NA	NA	NA	NA	45.83	17.84	27.99	NA	NA
MW-2	09/26/1996	87,000	NA	7,600	11,000	2,500	15,000	990	840	NA	NA	NA	NA	NA	NA	45.83	19.60	26.23	NA	NA
MW-2	12/10/1996	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	45.83	18.15	27.88	0.25	NA
MW-2	03/10/1997	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	45.83	17.02	28.97	0.20	NA
MW-2	06/30/1997	57,000	NA	3,600	4,600	1,300	9,700	2,300	NA	NA	NA	NA	NA	NA	NA	45.83	19.42	26.41	NA	2.4
MW-2	09/12/1997	88,000	NA	7,800	8,800	2,600	16,000	3,200	NA	NA	NA	NA	NA	NA	NA	45.83	19.40	26.43	NA	1.7
MW-2 (D)	09/12/1997	90,000	NA	8,300	9,400	2,700	17,000	3,400	NA	NA	NA	NA	NA	NA	NA	45.83	19.40	26.43	NA	1.7
MW-2 b	12/18/1997	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	45.83	17.56	28.27	NA	1.3
MW-2	02/02/1998	<50	NA	0.6	1.9	0.93	6.0	9.3	NA	NA	NA	NA	NA	NA	NA	45.83	18.14	27.69	NA	2
MW-2 (D)	02/02/1998	56	NA	1.0	2.8	1.4	9.3	13	NA	NA	NA	NA	NA	NA	NA	45.83	18.14	27.69	NA	2
MW-2	06/24/1998	20,000	NA	<200	620	560	4,500	<1,000	NA	NA	NA	NA	NA	NA	NA	45.83	16.08	29.75	NA	2.4
MW-2	08/26/1998	22,000	NA	380	1,100	560	4,400	330	NA	NA	NA	NA	NA	NA	NA	45.83	19.25	26.58	NA	NA
MW-2 (D)	08/26/1998	11,000	NA	180	130	290	500	1,400	NA	NA	NA	NA	NA	NA	NA	45.83	19.25	26.58	NA	NA
MW-2	12/23/1998	100,000	NA	4,100	6,500	2,400	16,000	<500	NA	NA	NA	NA	NA	NA	NA	45.83	18.29	27.54	NA	3.8
MW-2	03/01/1999	50,800	NA	3,910	7,480	1,890	13,100	9,620	NA	NA	NA	NA	NA	NA	NA	45.83	22.81	23.02	NA	2.0
MW-2	06/14/1999	4,930	NA	128	270	139	1,040	2,200	2,540*	NA	NA	NA	NA	NA	NA	45.83	18.86	26.97	NA	1.6

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Well ID	Date	TPPH (ug/L)	TEPH (ug/L)	B (ug/L)	T (ug/L)	E (ug/L)	X (ug/L)	MTBE 8020 (ug/L)	MTBE 8260 (ug/L)	DIPE (ug/L)	ETBE (ug/L)	TAME (ug/L)	TBA (ug/L)	1,2- DCA (ug/L)	EDB (ug/L)	TOC (MSL)	Depth to Water (ft.)	GW Elevation (MSL)	SPH Thickness (ft.)	DO Reading (ppm)
MW-2	09/28/1999	16,200	NA	647	1,070	542	4,130	5,320	4,790	NA	NA	NA	NA	NA	NA	45.83	21.41	24.42	NA	1.8
MW-2	12/08/1999	25,700	NA	1,670	2,110	977	6,600	6,190	5,970	NA	NA	NA	NA	NA	NA	45.83	21.89	23.94	NA	1.8
MW-2	03/14/2000	45,100	NA	2,070	4,710	1,920	12,800	16,700	18,300*	NA	NA	NA	NA	NA	NA	45.83	15.57	30.26	NA	2.0
MW-2	06/28/2000	52,100	NA	5,150	4,200	1,880	13,300	15,500	13,500*	NA	NA	NA	NA	NA	NA	45.83	17.79	28.04	NA	1.9
MW-2	09/06/2000	39,500	NA	4,490	3,290	2,100	14,000	18,500	9,060*	NA	NA	NA	NA	NA	NA	45.83	18.65	27.18	NA	3.5
MW-2	12/14/2000	209	NA	3.51	1.11	1.00	64.4	79.4	NA	NA	NA	NA	NA	NA	NA	45.83	19.00	26.83	NA	1.5
MW-2	03/05/2001	38,200	NA	2,010	927	1,250	8,300	13,100	15,400	NA	NA	NA	NA	NA	NA	45.83	16.66	29.17	NA	1.0
MW-2	06/11/2001	50,000	NA	4,400	2,200	1,800	11,000	NA	26,000	NA	NA	NA	NA	NA	NA	45.83	18.93	26.90	NA	1.7
MW-2	09/12/2001	59,000	NA	6,100	2,800	2,300	14,000	NA	21,000	NA	NA	NA	NA	NA	NA	45.83	19.85	25.98	NA	1.6
MW-2	12/27/2001	74,000	NA	8,600	2,500	2,500	17,000	NA	25,000	NA	NA	NA	NA	NA	NA	45.83	17.85	27.98	NA	2.6
MW-2	02/27/2002	70,000	NA	8,100	2,600	2,100	13,000	NA	32,000	NA	NA	NA	NA	NA	NA	45.79	17.15	28.64	NA	2.0
MW-2	06/18/2002	72,000	NA	9,500	3,000	2,200	13,000	NA	29,000	NA	NA	NA	NA	NA	NA	45.79	18.49	27.30	NA	0.6
MW-2	09/18/2002	48,000	NA	7,600	850	1,300	6,300	NA	8,700	NA	NA	NA	NA	NA	NA	45.79	19.95	25.84	NA	1.0
MW-2	12/27/2002	40,000	NA	5,900	1,200	1,400	7,800	NA	19,000	<50	<50	55	10,000	<50	<50	45.79	16.71	29.08	NA	1.0
MW-2	03/05/2003	62,000	NA	13,000	1,400	2,000	7,900	NA	21,000	NA	NA	<50	10,000	<50	NA	45.79	17.72	28.07	NA	1.4
MW-2	06/24/2003	19,000	NA	9,500	530	700	2,900	NA	14,000	NA	NA	<400	6,000	<100	NA	45.79	18.30	27.49	NA	1.4
MW-2	09/25/2003	65,000	NA	24,000	1,500	2,400	9,700	NA	19,000	NA	NA	<1,000	6,400	<250	NA	45.79	20.05	25.74	NA	1.3
MW-2	12/15/2003	67,000	NA	18,000	1,800	1,900	7,200	NA	11,000	NA	NA	<400	3,700	<100	NA	45.79	18.80	26.99	NA	0.1
MW-2	03/04/2004	72,000	NA	27,000	1,200	2,100	7,600	NA	13,000	NA	NA	<400	6,800	<100	NA	45.79	16.75	29.04	NA	0.2
MW-2	05/27/2004	74,000	NA	6,000	2,000	2,500	15,000	NA	19,000	NA	NA	<400	8,500	<100	NA	45.79	18.85	26.94	NA	0.8
MW-2	09/24/2004	<100	NA	<1.0	<1.0	<1.0	<2.0	NA	130	<4.0	<4.0	<4.0	46	19	<1.0	45.79	16.10	29.69	NA	5.1
MW-2	11/22/2004	8,800	NA	1,200	230	350	1,900	NA	2,200	NA	NA	<40	1,300	<10	NA	45.79	19.83	25.96	NA	0.3
MW-2	03/02/2005	960	NA	150	21	30	220	NA	630	NA	NA	<10	460	<2.5	NA	45.79	15.90	29.89	NA	0.5
MW-2	06/30/2005	970	NA	130	19	27	210	NA	320 e	NA	NA	<2.0	220	0.98	NA	45.79	17.14	28.65	NA	0.7
MW-2	09/20/2005	890	NA	320	10	35	190	NA	440	<10	<10	<10	570	<2.5	NA	45.79	18.66	27.13	NA	0.9
MW-2	12/05/2005	690	NA	150	6.1	21	130	NA	450	NA	NA	<5.0	520	<5.0	NA	45.79	18.58	27.21	NA	0.51
MW-2	03/02/2006	11,000 g	NA	2,700 g	150 g	440 g	2,300 g	NA	1,600 g	NA	NA	5.7	3,800 g	<0.50 j	NA	45.79	16.30	29.49	NA	1.2
MW-2 (n)	06/29/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	45.79	NA	NA	NA	NA
MW-2 (o)	06/30/2006	3,870	NA	177	33.1	55.5	311	NA	1,560	NA	NA	4.90	1,180	<0.500	NA	45.79	16.72	29.07	NA	0.58
MW-2	07/06/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	45.79	16.86	28.93	NA	NA
MW-2	09/11/2006	10,700	NA	1,010	134	211	1,280	NA	2,780	<0.500	<0.500	45.7	1,850	<0.500	NA	45.79	17.86	27.93	NA	1.03
MW-2	12/28/2006	29,000	NA	2,600	550	1,000	5,600	NA	2,500	NA	NA	<50	3,300	<12	NA	45.79	17.45	28.34	NA	1.09
MW-2	03/20/2007	57,600	NA	14,200 l	4,150 l	4,310 l	22,400 l	NA	6,240 l	NA	NA	<200 l	<10,000 l	<100 l	NA	45.79	17.28	28.51	NA	0.18
MW-2	06/26/2007	39,000 q	NA	3,400	2,300	2,200	12,900	NA	3,300	NA	NA	<100	3,400	<25	NA	45.79	18.64	27.15	NA	0.30
MW-2	09/11/2007	30,000 q	NA	4,000	2,500	2,500	13,000	NA	2,600	<100	<100	<100	2,600	<25	NA	45.79	19.57	26.22	NA	1.14
MW-2	12/26/2007	43,000 q	NA	6,200	2,200	2,800	17,600	NA	2,200	NA	NA	<50	2,000	<12	NA	45.79	18.78	27.01	NA	3.2
MW-2	03/19/2008	19,000 q	NA	2,400	1,800	1,200	6,000	NA	910	NA	NA	<200	1,000	<50	NA	45.79	17.32	28.47	NA	0.06

WELL CONCENTRATIONS
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1784 150th Avenue
San Leandro, CA

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MW-2	05/29/2008	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	45.79	18.40	27.39	NA	NA
MW-2	06/05/2008	68,000	NA	7,400	2,600	2,800	14,100	NA	2,600	<100	<100	<100	1,800	<25	NA	45.79	18.71	27.08	NA	0.28
MW-2	07/22/2008	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	45.79	19.48	26.31	NA	NA
MW-2	09/29/2008	84,000	NA	2,600	6,900	3,400	19,300	NA	620	<100	<100	<100	<500	<25	NA	45.79	24.50	21.29	NA	1.37
MW-2	Well destroyed		NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
MW-2B	10/31/2008	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	44.96	20.20	24.76	NA	NA
MW-2B	12/19/2008	1,300	NA	43	2.0	<1.0	65	NA	50	NA	NA	NA	NA	NA	NA	44.96	19.60	25.36	NA	0.48
MW-2B	03/10/2009	800	NA	58	1.3	<1.0	4.2	NA	110	NA	NA	NA	NA	NA	NA	44.96	16.10	28.86	NA	0.69
MW-3	02/13/1992	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	51.97	27.97	24.00	NA	NA
MW-3	02/24/1992	4,500	1,300a	97	<5	78	18	NA	NA	NA	NA	NA	NA	NA	NA	51.97	25.60	26.37	NA	NA
MW-3	02/27/1992	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	51.97	25.88	26.09	NA	NA
MW-3	03/01/1992	2,200	440	69	<0.5	<0.5	<0.5	NA	NA	NA	NA	NA	NA	NA	NA	51.97	26.00	25.97	NA	NA
MW-3	06/03/1992	4,100	NA	13	72	44	65	NA	NA	NA	NA	NA	NA	NA	NA	51.97	27.70	24.27	NA	NA
MW-3	09/01/1992	1,900	NA	20	6.8	5.5	<5	NA	NA	NA	NA	NA	NA	NA	NA	51.97	29.46	22.51	NA	NA
MW-3 (D)	09/01/1992	1,900	NA	21	6.6	3.4	<5	NA	NA	NA	NA	NA	NA	NA	NA	51.97	29.46	22.51	NA	NA
MW-3	10/06/1992	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	51.97	30.01	21.96	NA	NA
MW-3	11/11/1992	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	51.97	30.26	21.71	NA	NA
MW-3	12/04/1992	2,400	NA	8.2	<5	<5	<5	NA	NA	NA	NA	NA	NA	NA	NA	51.97	29.93	22.04	NA	NA
MW-3 (D)	12/04/1992	2,100	NA	11	<0.5	5.7	<0.5	NA	NA	NA	NA	NA	NA	NA	NA	51.97	29.93	22.04	NA	NA
MW-3	01/22/1993	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	51.97	22.76	29.21	NA	NA
MW-3	02/10/1993	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	51.97	21.40	30.57	NA	NA
MW-3	03/03/1993	5,100	NA	63	61	75	150	NA	NA	NA	NA	NA	NA	NA	NA	51.97	23.08	28.89	NA	NA
MW-3	05/11/1993	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	51.97	24.51	27.46	NA	NA
MW-3	06/17/1993	4,000	NA	94	140	82	150	NA	NA	NA	NA	NA	NA	NA	NA	51.97	25.21	26.76	NA	NA
MW-3	09/10/1993	3,200	NA	140	12.5	12.5	12.5	NA	NA	NA	NA	NA	NA	NA	NA	51.97	26.95	25.02	NA	NA
MW-3	12/13/1993	6,200	NA	<12.5	<12.5	<12.5	<12.5	NA	NA	NA	NA	NA	NA	NA	NA	51.97	26.52	25.45	NA	NA
MW-3	03/03/1994	4,500	NA	73	<5	<5	<5	NA	NA	NA	NA	NA	NA	NA	NA	51.97	24.50	27.47	NA	NA
MW-3	06/06/1994	3,200	NA	<0.5	<0.5	3.1	<0.5	NA	NA	NA	NA	NA	NA	NA	NA	51.97	26.33	25.64	NA	NA
MW-3	09/12/1994	3,900	NA	<0.5	<0.5	9.6	4.1	NA	NA	NA	NA	NA	NA	NA	NA	51.97	27.98	23.99	NA	NA
MW-3	12/19/1994	2,400	NA	21	22	4.2	2.6	NA	NA	NA	NA	NA	NA	NA	NA	51.97	25.63	26.34	NA	NA
MW-3	02/28/1995	4,000	NA	58	<0.5	7.1	3.5	NA	NA	NA	NA	NA	NA	NA	NA	51.97	23.45	28.52	NA	NA
MW-3	03/24/1995	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	51.97	21.07	30.90	NA	NA
MW-3	06/26/1995	3,900	NA	8.1	<0.5	12	2.4	NA	NA	NA	NA	NA	NA	NA	NA	51.97	23.64	28.33	NA	NA
MW-3	09/13/1995	4,100	NA	58	5.5	5.5	<0.5	NA	NA	NA	NA	NA	NA	NA	NA	51.97	25.40	26.57	NA	NA

WELL CONCENTRATIONS
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Well ID	Date	TPPH (ug/L)	TEPH (ug/L)	B (ug/L)	T (ug/L)	E (ug/L)	X (ug/L)	MTBE 8020 (ug/L)	MTBE 8260 (ug/L)	DIPE (ug/L)	ETBE (ug/L)	TAME (ug/L)	TBA (ug/L)	1,2- DCA (ug/L)	EDB (ug/L)	TOC (MSL)	Depth to Water (ft.)	GW Elevation (MSL)	SPH Thickness (ft.)	DO Reading (ppm)
MW-3	12/19/1995	3,600	NA	<0.5	4.3	2.1	1.1	NA	NA	NA	NA	NA	NA	NA	NA	51.97	24.53	27.44	NA	NA
MW-3	03/07/1996	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	51.97	21.59	30.41	0.04	NA
MW-3	06/28/1996	2,400	NA	55	<0.5	<0.5	11	120	NA	NA	NA	NA	NA	NA	NA	51.97	23.95	28.02	NA	NA
MW-3	09/26/1996	2,500	NA	<5.0	<5.0	<5.0	<5.0	160	NA	NA	NA	NA	NA	NA	NA	51.97	25.89	26.08	NA	NA
MW-3	12/10/1996	1,600	NA	28	4.2	<2.0	3.9	110	NA	NA	NA	NA	NA	NA	NA	51.97	24.22	27.75	NA	0.8
MW-3	03/10/1997	130	NA	<0.50	<0.50	<0.50	1.4	4.2	NA	NA	NA	NA	NA	NA	NA	51.97	23.05	28.92	NA	2.8
MW-3	06/30/1997	1,200	NA	21	2.3	<2.0	<2.0	69	NA	NA	NA	NA	NA	NA	NA	51.97	24.34	27.63	NA	2.3
MW-3	09/12/1997	440	NA	8.3	0.82	<0.50	1.9	3.4	NA	NA	NA	NA	NA	NA	NA	51.97	24.47	27.50	NA	1.9
MW-3 b	12/18/1997	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	51.97	23.54	28.43	NA	0.8
MW-3	02/02/1998	400	NA	9.3	0.68	<0.50	<0.50	9	NA	NA	NA	NA	NA	NA	NA	51.97	21.92	30.05	NA	1.5
MW-3	06/24/1998	<50	NA	<0.50	<0.50	<0.50	<0.50	<2.5	NA	NA	NA	NA	NA	NA	NA	51.97	22.35	29.62	NA	1.9
MW-3	08/26/1998	140	NA	7.4	<0.50	<0.50	2.5	13	NA	NA	NA	NA	NA	NA	NA	51.97	23.45	28.52	NA	1.3
MW-3	12/23/1998	1,200	NA	50	<2.0	<2.0	<2.0	69	NA	NA	NA	NA	NA	NA	NA	51.97	24.01	27.96	NA	4.2
MW-3	03/01/1999	2,550	NA	<0.500	<0.500	<0.500	0.658	32.4	NA	NA	NA	NA	NA	NA	NA	51.97	22.08	29.89	NA	2.0
MW-3	06/14/1999	514	NA	18.1	0.728	<0.500	<0.500	15.9	NA	NA	NA	NA	NA	NA	NA	51.97	23.15	28.82	NA	1.7
MW-3	09/28/1999	1,180	NA	<1.00	<1.00	<1.00	<1.00	<10.0	NA	NA	NA	NA	NA	NA	NA	51.97	25.36	26.61	NA	1.2
MW-3	12/08/1999	1,740	NA	71.5	23.0	24.2	61.3	103	NA	NA	NA	NA	NA	NA	NA	51.97	25.75	26.22	NA	2.0
MW-3	03/14/2000	1,410	NA	5.63	35.6	<5.00	8.41	38.7	NA	NA	NA	NA	NA	NA	NA	51.97	21.64	30.33	NA	2.1
MW-3	06/28/2000	2,460	NA	<5.00	9.48	<5.00	28.4	64.0	NA	NA	NA	NA	NA	NA	NA	51.97	23.84	28.13	NA	2.87
MW-3	09/06/2000	887	NA	<1.00	<1.00	<1.00	<1.00	<10.0	NA	NA	NA	NA	NA	NA	NA	51.97	24.73	27.24	NA	2.0
MW-3	12/14/2000	955	NA	25.4	1.96	<0.500	1.13	10.2	NA	NA	NA	NA	NA	NA	NA	51.97	25.45	26.52	NA	2.1
MW-3	03/05/2001	2,100	NA	4.90	56.5	<2.00	3.62	261	NA	NA	NA	NA	NA	NA	NA	51.97	22.83	29.14	NA	0.8
MW-3	06/11/2001	2,000	NA	1.0	<0.50	<0.50	<0.50	NA	<0.50	NA	NA	NA	NA	NA	NA	51.97	25.20	26.77	NA	0.7
MW-3	09/12/2001	1,500	NA	0.50	0.54	<0.50	1.8	NA	<5.0	NA	NA	NA	NA	NA	NA	51.97	26.15	25.82	NA	1.5
MW-3	12/27/2001	2,100	NA	<0.50	<0.50	<0.50	<0.50	NA	<5.0	NA	NA	NA	NA	NA	NA	51.97	23.67	28.30	NA	1.9
MW-3	02/27/2002	2,300	NA	<0.50	<0.50	<0.50	<0.50	NA	<5.0	NA	NA	NA	NA	NA	NA	51.92	23.23	28.69	NA	1.5
MW-3	06/18/2002	2,000	NA	<0.50	<0.50	<0.50	<0.50	NA	<0.50	NA	NA	NA	NA	NA	NA	51.92	24.74	27.18	NA	2.0
MW-3	09/18/2002	2,600	NA	<0.50	<0.50	<0.50	<0.50	NA	<5.0	NA	NA	NA	NA	NA	NA	51.92	26.05	25.87	NA	1.4
MW-3	12/27/2002	Well inaccessible		NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	51.92	NA	NA	NA	NA
MW-3	03/05/2003	2,300	NA	<0.50	<0.50	<0.50	<0.50	NA	<5.0	NA	NA	<2.0	<50	13	NA	51.92	23.84	28.08	NA	1.3
MW-3	06/24/2003	Well inaccessible		NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	51.92	NA	NA	NA	NA
MW-3	06/25/2003	1,800 c	NA	0.71	<0.50	<0.50	<1.0	NA	0.54	NA	NA	<2.0	<5.0	1.1	NA	51.92	24.48	27.44	NA	1.3
MW-3	09/25/2003	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	51.92	25.99	25.93	NA	NA
MW-3	12/15/2003	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	51.92	24.94	26.98	NA	NA
MW-3	03/04/2004	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	51.92	22.50	29.42	NA	NA

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MW-3	05/27/2004	2,500	NA	<0.50	<0.50	<0.50	<1.0	NA	1.1	NA	NA	<2.0	<5.0	0.82	NA	51.92	24.94	26.98	NA	0.5
MW-3	09/24/2004	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	51.92	26.55	25.37	NA	NA
MW-3	11/22/2004	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	51.92	25.92	26.00	NA	NA
MW-3	03/02/2005	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	51.92	22.12	29.80	NA	NA
MW-3	06/30/2005	3,700	NA	<2.0	2.4	<2.0	<4.0	NA	<2.0	<8.0	<8.0	<8.0	<20	<2.0	NA	51.92	23.31	28.61	NA	1.2
MW-3	09/20/2005	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	51.92	24.78	27.14	NA	NA
MW-3	12/05/2005	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	51.92	24.65	27.27	NA	NA
MW-3	03/02/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	51.92	22.56	29.36	NA	NA
MW-3 (n)	06/29/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	51.92	NA	NA	NA	NA
MW-3 (o)	06/30/2006	1,580	NA	<0.500	<0.500	<0.500	<0.500	NA	<0.500	<0.500	<0.500	<0.500	<10.0	5.95	NA	51.92	22.89	29.03	NA	0.49
MW-3	07/06/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	51.92	22.99	28.93	NA	NA
MW-3	09/11/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	51.92	23.92	28.00	NA	NA
MW-3	12/28/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	51.92	23.68	28.24	NA	NA
MW-3	03/20/2007	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	51.92	23.91	28.01	NA	NA
MW-3	06/26/2007	1,400 q	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	<2.0	<2.0	<2.0	<10	44	NA	51.92	25.10	26.82	NA	1.77
MW-3	09/11/2007	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	51.92	23.41	28.51	NA	NA
MW-3	12/26/2007	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	51.92	25.15	26.77	NA	NA
MW-3	03/19/2008	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	51.92	23.81	28.11	NA	NA
MW-3	06/05/2008	3,600	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	<2.0	<2.0	<2.0	<10	33	NA	51.92	25.08	26.84	NA	0.10
MW-3	09/29/2008	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	51.92	26.85	25.07	NA	NA
MW-3	12/19/2008	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	51.92	26.47	25.45	NA	NA
MW-3	03/10/2009	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	51.92	23.13	28.79	NA	NA
MW-4	03/24/1995	<50	NA	<0.5	<0.5	<0.5	<0.5	NA	NA	NA	NA	NA	NA	NA	NA	40.51	9.16	31.35	NA	NA
MW-4	06/26/1995	<50	NA	<0.5	<0.5	<0.5	<0.5	NA	NA	NA	NA	NA	NA	NA	NA	40.51	12.06	28.45	NA	NA
MW-4	09/13/1995	<50	NA	<0.5	<0.5	<0.5	<0.5	NA	NA	NA	NA	NA	NA	NA	NA	40.51	13.90	26.61	NA	NA
MW-4	12/19/1995	<50	NA	<0.5	<0.5	<0.5	<0.5	NA	NA	NA	NA	NA	NA	NA	NA	40.51	12.90	27.61	NA	NA
MW-4	03/06/1996	<50	NA	<0.5	<0.5	<0.5	<0.5	NA	NA	NA	NA	NA	NA	NA	NA	40.51	9.63	30.88	NA	NA
MW-4	06/28/1996	40	NA	<0.5	0.59	0.97	3.8	26	NA	NA	NA	NA	NA	NA	NA	40.51	12.30	28.21	NA	NA
MW-4	09/26/1996	<50	NA	<0.5	<0.5	<0.5	<0.5	<2.5	NA	NA	NA	NA	NA	NA	NA	40.51	14.12	26.39	NA	NA
MW-4	12/10/1996	<50	NA	<0.5	<0.5	<0.5	<0.5	<2.5	NA	NA	NA	NA	NA	NA	NA	40.51	12.31	28.20	NA	1.2
MW-4	03/10/1997	<50	NA	<0.50	<0.50	<0.50	<0.50	<2.5	NA	NA	NA	NA	NA	NA	NA	40.51	11.34	29.17	NA	NA
MW-4	06/30/1997	<50	NA	<0.50	<0.50	<0.50	<0.50	<2.5	NA	NA	NA	NA	NA	NA	NA	40.51	13.80	26.71	NA	1.9
MW-4	09/12/1997	<50	NA	<0.50	<0.50	<0.50	<0.50	<2.5	NA	NA	NA	NA	NA	NA	NA	40.51	13.99	26.52	NA	1.7
MW-4 b	12/18/1997	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	40.51	12.02	28.49	NA	1.8

WELL CONCENTRATIONS
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Well ID	Date	TPPH (ug/L)	TEPH (ug/L)	B (ug/L)	T (ug/L)	E (ug/L)	X (ug/L)	MTBE 8020 (ug/L)	MTBE 8260 (ug/L)	DIPE (ug/L)	ETBE (ug/L)	TAME (ug/L)	TBA (ug/L)	1,2- DCA (ug/L)	EDB (ug/L)	TOC (MSL)	Depth to Water (ft.)	GW Elevation (MSL)	SPH Thickness (ft.)	DO Reading (ppm)
MW-4	02/02/1998	<50	NA	<0.50	<0.50	<0.50	<0.50	<2.5	NA	NA	NA	NA	NA	NA	NA	40.51	11.23	29.28	NA	1
MW-4	06/24/1998	<50	NA	<0.50	<0.50	<0.50	<0.50	<2.5	NA	NA	NA	NA	NA	NA	NA	40.51	10.58	29.93	NA	1.9
MW-4	08/26/1998	<50	NA	<0.50	<0.50	<0.50	<0.50	<2.5	NA	NA	NA	NA	NA	NA	NA	40.51	11.75	28.76	NA	1.2
MW-4	12/23/1998	<50	NA	0.60	<0.50	<0.50	<0.50	<2.5	NA	NA	NA	NA	NA	NA	NA	40.51	12.41	28.10	NA	4.2
MW-4	03/01/1999	<50.0	NA	<0.500	<0.500	<0.500	<0.500	<2.00	NA	NA	NA	NA	NA	NA	NA	40.51	10.38	30.13	NA	2.1
MW-4	06/14/1999	<50.0	NA	<0.500	<0.500	<0.500	<0.500	<2.50	NA	NA	NA	NA	NA	NA	NA	40.51	11.91	28.60	NA	2.4
MW-4	09/28/1999	<50.0	NA	<0.500	<0.500	<0.500	<0.500	<5.00	NA	NA	NA	NA	NA	NA	NA	40.51	10.19	30.32	NA	2.2
MW-4	12/08/1999	<50.0	NA	<0.500	<0.500	<0.500	<0.500	<2.50	NA	NA	NA	NA	NA	NA	NA	40.51	10.67	29.84	NA	1.8
MW-4	03/14/2000	<50.0	NA	<0.500	<0.500	<0.500	<0.500	<2.50	NA	NA	NA	NA	NA	NA	NA	40.51	9.95	30.56	NA	2.5
MW-4	06/28/2000	<50.0	NA	<0.500	<0.500	<0.500	<0.500	<2.50	NA	NA	NA	NA	NA	NA	NA	40.51	12.22	28.29	NA	0.9
MW-4	09/06/2000	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	40.51	13.17	27.34	NA	3.0
MW-4	12/14/2000	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	40.51	8.65	31.86	NA	NA
MW-4	03/05/2001	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	40.51	11.07	29.44	NA	NA
MW-4	06/11/2001	<50	NA	<0.50	<0.50	<0.50	<0.50	NA	<0.50	NA	NA	NA	NA	NA	NA	40.51	13.62	26.89	NA	1.3
MW-4	09/12/2001	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	40.51	14.61	25.90	NA	NA
MW-4	12/27/2001	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	40.51	12.19	28.32	NA	NA
MW-4	02/27/2002	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	40.45	11.64	28.81	NA	NA
MW-4	06/18/2002	<50	NA	<0.50	<0.50	<0.50	<0.50	NA	<0.50	NA	NA	NA	NA	NA	NA	40.45	13.22	27.23	NA	0.6
MW-4	09/18/2002	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	40.45	14.46	25.99	NA	NA
MW-4	12/27/2002	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	40.45	11.23	29.22	NA	NA
MW-4	03/05/2003	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	40.45	12.22	28.23	NA	NA
MW-4	06/24/2003	57 c	NA	<0.50	<0.50	<0.50	<1.0	NA	12	NA	NA	NA	NA	NA	NA	40.45	12.79	27.66	NA	1.6
MW-4	09/25/2003	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	40.45	14.45	26.00	NA	NA
MW-4	12/15/2003	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	40.45	13.24	27.21	NA	NA
MW-4	03/04/2004	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	40.45	10.93	29.52	NA	NA
MW-4	05/27/2004	<50	NA	<0.50	<0.50	<0.50	<1.0	NA	<0.50	NA	NA	NA	NA	NA	NA	40.45	13.42	27.03	NA	0.5
MW-4	09/24/2004	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	40.45	15.11	25.34	NA	NA
MW-4	11/22/2004	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	40.45	14.42	26.03	NA	NA
MW-4	03/02/2005	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	40.45	10.17	30.28	NA	NA
MW-4	06/30/2005	<50 d	NA	<0.50	<0.50	<0.50	<1.0	NA	<0.50	<2.0	<2.0	<2.0	<5.0	NA	NA	40.45	11.60	28.85	NA	0.8
MW-4	09/20/2005	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	40.45	13.18	27.27	NA	NA
MW-4	12/05/2005	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	40.45	13.08	27.37	NA	NA
MW-4	03/02/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	40.45	10.62	29.83	NA	NA
MW-4 (n)	06/29/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	40.45	NA	NA	NA	NA
MW-4 (o)	06/30/2006	<50.0	NA	<0.500	<0.500	<0.500	<0.500	NA	<0.500	<0.500	<0.500	<0.500	<10.0	NA	NA	40.45	11.20	29.25	NA	0.44

WELL CONCENTRATIONS
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Well ID	Date	TPPH (ug/L)	TEPH (ug/L)	B (ug/L)	T (ug/L)	E (ug/L)	X (ug/L)	MTBE 8020 (ug/L)	MTBE 8260 (ug/L)	DIPE (ug/L)	ETBE (ug/L)	TAME (ug/L)	TBA (ug/L)	1,2- DCA (ug/L)	EDB (ug/L)	TOC (MSL)	Depth to Water (ft.)	GW Elevation (MSL)	SPH Thickness (ft.)	DO Reading (ppm)
MW-4	07/06/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	40.45	11.22	29.23	NA	NA
MW-4	09/11/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	40.45	12.29	28.16	NA	NA
MW-4	12/28/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	40.45	11.71	28.74	NA	NA
MW-4	03/20/2007	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	40.45	11.99	28.46	NA	NA
MW-4	06/26/2007	59 q	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	<2.0	<2.0	<2.0	<10	NA	NA	40.45	13.60	26.85	NA	3.69
MW-4	09/11/2007	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	40.45	11.61	28.84	NA	NA
MW-4	12/26/2007	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	40.45	13.72	26.73	NA	NA
MW-4	03/19/2008	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	40.45	12.19	28.26	NA	NA
MW-4	06/05/2008	<50	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	<2.0	<2.0	<2.0	<10	NA	NA	40.45	13.62	26.83	NA	0.09
MW-4	09/29/2008	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	40.45	15.55	24.90	NA	NA
MW-4	12/19/2008	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	40.45	15.03	25.42	NA	NA
MW-4	03/10/2009	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	40.45	11.55	28.90	NA	NA
MW-5	01/29/2002	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	41.46	12.82	28.64	NA	NA
MW-5	02/27/2002	190	NA	<0.50	<0.50	0.85	1.5	NA	<5.0	NA	NA	NA	NA	NA	NA	41.46	12.85	28.61	NA	1.9
MW-5	06/18/2002	650	NA	1.4	3.0	52	28	NA	<0.50	NA	NA	NA	NA	NA	NA	41.46	13.65	27.81	NA	0.8
MW-5	09/18/2002	390	NA	0.72	0.51	<0.50	<0.50	NA	<5.0	NA	NA	NA	NA	NA	NA	41.46	15.57	25.89	NA	1.1
MW-5	12/27/2002	380	NA	<0.50	<0.50	0.56	<0.50	NA	<0.50	<2.0	<2.0	<2.0	<50	<2.0	<2.0	41.46	12.51	28.95	NA	1.9
MW-5	03/05/2003	290	NA	<0.50	1.7	9.4	22	NA	<5.0	NA	NA	NA	NA	NA	NA	41.46	13.39	28.07	NA	2.6
MW-5	06/24/2003	220	NA	<0.50	1.0	19	1.3	NA	<0.50	NA	NA	NA	NA	NA	NA	41.46	13.91	27.55	NA	1.7
MW-5	09/25/2003	<50	NA	<0.50	<0.50	<0.50	<1.0	NA	<0.50	NA	NA	NA	NA	NA	NA	41.46	15.58	25.88	NA	2.1
MW-5	12/15/2003	200 c	NA	<0.50	<0.50	<0.50	<1.0	NA	<0.50	NA	NA	NA	NA	NA	NA	41.46	14.45	27.01	NA	0.21
MW-5	03/04/2004	170 c	NA	<0.50	<0.50	<0.50	<1.0	NA	<0.50	NA	NA	NA	NA	NA	NA	41.46	12.52	28.94	NA	0.1
MW-5	05/27/2004	<50	NA	<0.50	<0.50	<0.50	<1.0	NA	<0.50	NA	NA	NA	NA	NA	NA	41.46	14.49	26.97	NA	0.5
MW-5	09/24/2004	<50	NA	0.71	<0.50	<0.50	<1.0	NA	<0.50	<2.0	<2.0	<2.0	<5.0	NA	NA	41.46	16.08	25.38	NA	1.7
MW-5	11/22/2004	<50 d	NA	<0.50	<0.50	<0.50	<1.0	NA	<0.50	NA	NA	NA	NA	NA	NA	41.46	15.48	25.98	NA	0.3
MW-5	03/02/2005	190	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	NA	NA	<2.0	<10	<0.50	NA	41.46	11.52	29.94	NA	0.4
MW-5	06/30/2005	3,200	NA	<5.0	25	200	270	NA	<5.0	NA	NA	NA	NA	NA	NA	41.46	12.33	29.13	NA	0.9
MW-5	09/20/2005	310	NA	<0.50	1.3	47	2.5	NA	<0.50	<2.0	<2.0	<2.0	<5.0	NA	NA	41.46	14.36	27.10	NA	0.5
MW-5	12/05/2005	250	NA	<0.50	0.94	26	<0.50	NA	<0.50	NA	NA	NA	NA	NA	NA	41.46	14.25	27.21	NA	0.58
MW-5	03/02/2006	3,000 g	NA	<0.50	17	230 g	390 g	NA	<0.50	NA	NA	NA	NA	NA	NA	41.46	11.87	29.59	NA	0.7
MW-5 (n)	06/29/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	41.46	NA	NA	NA	NA
MW-5 (o)	06/30/2006	729	NA	<0.500	1.00	43.2	21.7	NA	<0.500	NA	NA	NA	NA	NA	NA	41.46	12.49	28.97	NA	0.67
MW-5	07/06/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	41.46	12.58	28.88	NA	NA
MW-5	09/11/2006	<50.0	NA	<0.500	<0.500	<0.500	1.29	NA	<0.500	<0.500	<0.500	<0.500	<10.0	NA	NA	41.46	13.54	27.92	NA	0.78

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MW-5	12/28/2006	330	NA	<0.50	<0.50	8.6	<1.0	NA	<0.50	NA	NA	NA	NA	NA	NA	41.46	13.25	28.21	NA	0.59
MW-5	03/20/2007	358	NA	<0.500	<0.500	<0.500	<1.00	NA	<0.500	NA	NA	NA	NA	NA	NA	41.46	13.28	28.18	NA	0.11
MW-5	06/26/2007	120 q	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	NA	NA	NA	NA	NA	NA	41.46	14.68	26.78	NA	4.72
MW-5	09/11/2007	<50 q	NA	0.19 r	<1.0	<1.0	<1.0	NA	<1.0	<2.0	<2.0	<2.0	<10	NA	NA	41.46	15.57	25.89	NA	0.84
MW-5	12/26/2007	110 q, t	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	NA	NA	NA	NA	NA	NA	41.46	14.76	26.70	NA	0.8
MW-5	03/19/2008	2,000	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	NA	NA	NA	NA	NA	NA	41.46	13.34	28.12	NA	0.31
MW-5	06/05/2008	2,000	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	NA	NA	NA	NA	NA	NA	41.46	14.63	26.83	NA	0.10
MW-5	09/29/2008	830	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	<2.0	<2.0	<2.0	<10	NA	NA	41.46	16.45	25.01	NA	1.13
MW-5	12/19/2008	58	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	NA	NA	NA	NA	NA	NA	41.46	16.04	25.42	NA	0.62
MW-5	03/10/2009	820	NA	<0.50	<1.0	13	10	NA	<1.0	NA	NA	NA	NA	NA	NA	41.46	12.77	28.69	NA	0.37

MW-6	01/29/2002	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	41.50	3.88	37.62	NA	NA
MW-6	01/31/2002	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	41.50	12.43	29.07	NA	NA
MW-6	02/27/2002	<50	NA	<0.50	<0.50	<0.50	<0.50	NA	<5.0	NA	NA	NA	NA	NA	NA	41.50	12.82	28.68	NA	4.1
MW-6	06/18/2002	<50	NA	<0.50	<0.50	<0.50	<0.50	NA	<0.50	NA	NA	NA	NA	NA	NA	41.50	4.26	37.24	NA	3.9
MW-6	09/18/2002	<50	NA	<0.50	<0.50	<0.50	<0.50	NA	<5.0	NA	NA	NA	NA	NA	NA	41.50	5.26	36.24	NA	4.2
MW-6	12/27/2002	<50	NA	<0.50	<0.50	<0.50	<0.50	NA	<0.50	<2.0	<2.0	<2.0	<50	<2.0	<2.0	41.50	12.11	29.39	NA	3.0
MW-6	03/05/2003	<50	NA	<0.50	<0.50	<0.50	<0.50	NA	<5.0	NA	NA	NA	NA	NA	NA	41.50	13.47	28.03	NA	4.9
MW-6	06/24/2003	<50	NA	<0.50	<0.50	<0.50	<1.0	NA	<0.50	NA	NA	NA	NA	NA	NA	41.50	13.71	27.79	NA	5.8
MW-6	09/25/2003	Well inaccessible		NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	41.50	NA	NA	NA	NA
MW-6	12/15/2003	<50	NA	<0.50	<0.50	<0.50	<1.0	NA	<0.50	NA	NA	NA	NA	NA	NA	41.50	13.17	28.33	NA	5.7
MW-6	03/04/2004	<50	NA	<0.50	<0.50	<0.50	<1.0	NA	<0.50	NA	NA	NA	NA	NA	NA	41.50	11.15	30.35	NA	1.0
MW-6	05/27/2004	<50	NA	0.50	<0.50	<0.50	<1.0	NA	<0.50	NA	NA	NA	NA	NA	NA	41.50	13.68	27.82	NA	1.0
MW-6	09/24/2004	<50	NA	<0.50	<0.50	<0.50	<1.0	NA	<0.50	NA	NA	NA	NA	NA	NA	41.50	10.71	30.79	NA	3.1
MW-6	11/22/2004	<50 d	NA	0.65	<0.50	<0.50	<1.0	NA	<0.50	NA	NA	NA	NA	NA	NA	41.50	7.60	33.90	NA	6.5
MW-6	03/02/2005	<100	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	NA	NA	<2.0	<10	<0.50	NA	41.50	6.77	34.73	NA	6.2
MW-6	06/30/2005	<50	NA	<0.50	<0.50	<0.50	<1.0	NA	<0.50	NA	NA	NA	NA	NA	NA	41.50	12.87	28.63	NA	1.2
MW-6	09/20/2005	<50	NA	<0.50	<0.50	<0.50	<1.0	NA	<0.50	NA	NA	NA	NA	NA	NA	41.50	14.16	27.34	NA	5.5
MW-6	12/05/2005	<50	NA	<0.50	<0.50	<0.50	<0.50	NA	<0.50	NA	NA	NA	NA	NA	NA	41.50	14.23	27.27	NA	2.40
MW-6	03/02/2006	58 i	NA	<0.50	<0.50	0.73	1.5	NA	<0.50	NA	NA	NA	NA	NA	NA	41.50	11.40	30.10	NA	1.2
MW-6 (m)	06/29/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	41.50	12.49	29.01	NA	0.41
MW-6 (o)	06/30/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	41.50	12.35	29.15	NA	NA
MW-6 (p)	07/06/2006	<50.0	NA	<0.500	<0.500	<0.500	<0.500	NA	<0.500	NA	NA	NA	NA	NA	NA	41.50	12.66	28.84	NA	0.30
MW-6	09/11/2006	<50.0	NA	<0.500	<0.500	<0.500	0.530	NA	<0.500	NA	NA	NA	NA	NA	NA	41.50	13.33	28.17	NA	1.16
MW-6	12/28/2006	<50	NA	<0.50	<0.50	<0.50	<1.0	NA	<0.50	NA	NA	NA	NA	NA	NA	41.50	13.15	28.35	NA	1.0

WELL CONCENTRATIONS
Shell-branded Service Station
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San Leandro, CA

Well ID	Date	TPPH (ug/L)	TEPH (ug/L)	B (ug/L)	T (ug/L)	E (ug/L)	X (ug/L)	MTBE 8020 (ug/L)	MTBE 8260 (ug/L)	DIPE (ug/L)	ETBE (ug/L)	TAME (ug/L)	TBA (ug/L)	1,2- DCA (ug/L)	EDB (ug/L)	TOC (MSL)	Depth to Water (ft.)	GW Elevation (MSL)	SPH Thickness (ft.)	DO Reading (ppm)
MW-6	03/20/2007	<50.0	NA	<0.500	<0.500	<0.500	<1.00	NA	<0.500	NA	NA	NA	NA	NA	NA	41.50	13.24	28.26	NA	5.60
MW-6	06/26/2007	60 q	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	NA	NA	NA	NA	NA	NA	41.50	14.60	26.90	NA	5.46
MW-6	09/11/2007	<50 q	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	NA	NA	NA	NA	NA	NA	41.50	15.39	26.11	NA	1.16
MW-6	12/26/2007	<50 q	NA	0.27 r	<1.0	<1.0	<1.0	NA	<1.0	NA	NA	NA	NA	NA	NA	41.50	14.69	26.81	NA	3.1
MW-6	03/19/2008	1,500	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	NA	NA	NA	NA	NA	NA	41.50	12.93	28.57	NA	0.30
MW-6	06/05/2008	<50	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	NA	NA	NA	NA	NA	NA	41.50	14.61	26.89	NA	0.09
MW-6	09/29/2008	<50	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	NA	NA	NA	NA	NA	NA	41.50	15.62	25.88	NA	2.26
MW-6	12/19/2008	<50	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	NA	NA	NA	NA	NA	NA	41.50	14.45	27.05	NA	1.82
MW-6	03/10/2009	76	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	NA	NA	NA	NA	NA	NA	41.50	11.58	29.92	NA	0.57
MW-7	10/21/2002	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	44.45	18.90	25.55	NA	NA
MW-7	12/27/2002	49,000	NA	830	980	2,000	5,200	NA	<10	<10	<10	<10	<100	<10	<10	44.45	15.43	29.02	NA	2.1
MW-7	03/05/2003	32,000	NA	370	490	1,600	2,900	NA	<100	NA	NA	NA	NA	NA	NA	44.45	16.34	28.11	NA	2.6
MW-7	06/24/2003	Well inaccessible		NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	44.45	NA	NA	NA	NA
MW-7	09/25/2003	8,700	NA	57	34	450	290	NA	<5.0	NA	NA	NA	NA	NA	NA	44.45	18.36	26.09	NA	1.2
MW-7	12/15/2003	27,000	NA	170	260	1,200	1,500	NA	<10	NA	NA	NA	NA	NA	NA	44.45	17.44	27.01	NA	1.3
MW-7	03/04/2004	13,000	NA	200	190	1,200	1,200	NA	<5.0	NA	NA	NA	NA	NA	NA	44.45	15.45	29.00	NA	0.1
MW-7	05/27/2004	16,000	NA	76	56	860	420	NA	<5.0	NA	NA	NA	NA	NA	NA	44.45	17.50	26.95	NA	0.5
MW-7	09/24/2004	8,400	NA	26	14	340	200	NA	<5.0	<20	<20	<20	<50	NA	NA	44.45	18.94	25.51	NA	1.1
MW-7	11/22/2004	14,000	NA	92	60	790	730	NA	<5.0	NA	NA	NA	NA	NA	NA	44.45	18.47	25.98	NA	0.2
MW-7	03/02/2005	13,000	NA	130	140	740	980	NA	<10	NA	NA	<20	<100	<5.0	NA	44.45	14.53	29.92	NA	0.7
MW-7	06/30/2005	9,900	NA	27	48	380	520	NA	<10	NA	NA	NA	NA	NA	NA	44.45	15.92	28.53	NA	0.9
MW-7	09/20/2005	7,700	NA	30	53	380	570	NA	<5.0	36	<20	<20	<50	NA	NA	44.45	17.28	27.17	NA	1.4
MW-7	12/05/2005	2,900	NA	20	<2.5	270	19	NA	<2.5	NA	NA	NA	NA	NA	NA	44.45	17.40	27.05	NA	0.56
MW-7	03/02/2006	3,900 g	NA	27	31	240 g	190	NA	1.1	NA	NA	NA	NA	NA	NA	44.45	15.00	29.45	NA	0.9
MW-7 (n)	06/29/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	44.45	NA	NA	NA	NA
MW-7 (o)	06/30/2006	10,800	NA	13.8	49.4	474	640	NA	<0.500	NA	NA	NA	NA	NA	NA	44.45	15.35	29.10	NA	0.54
MW-7	07/06/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	44.45	15.41	29.04	NA	NA
MW-7	09/11/2006	7,210	NA	4.38	3.96	188	91.6	NA	<0.500	<0.500	<0.500	<0.500	<10.0	NA	NA	44.45	16.33	28.12	NA	0.82
MW-7	12/28/2006	3,100	NA	4.8	5.2	190	160	NA	<1.0	NA	NA	NA	NA	NA	NA	44.45	16.22	28.23	NA	0.78
MW-7	03/20/2007	5,960	NA	11.3	20.6	223	291	NA	<0.500	NA	NA	NA	NA	NA	NA	44.45	16.26	28.19	NA	1.10
MW-7	06/26/2007	7,900 q	NA	5.3	15	410	459	NA	<5.0	NA	NA	NA	NA	NA	NA	44.45	17.60	26.85	NA	0.83
MW-7	09/11/2007	4,100 q	NA	1.9	0.66 r	130	25.6	NA	<1.0	0.42 r	<2.0	<2.0	<10	NA	NA	44.45	18.63	25.82	NA	0.97
MW-7	12/26/2007	6,100 q	NA	5.9	7.6	290	348	NA	<5.0	NA	NA	NA	NA	NA	NA	44.45	17.72	26.73	NA	1.3
MW-7	03/19/2008	2,700	NA	5.0	2.4	110	97.9	NA	<1.0	NA	NA	NA	NA	NA	NA	44.45	16.36	28.09	NA	0.47

WELL CONCENTRATIONS
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San Leandro, CA

Well ID	Date	TPPH (ug/L)	TEPH (ug/L)	B (ug/L)	T (ug/L)	E (ug/L)	X (ug/L)	MTBE 8020 (ug/L)	MTBE 8260 (ug/L)	DIPE (ug/L)	ETBE (ug/L)	TAME (ug/L)	TBA (ug/L)	1,2- DCA (ug/L)	EDB (ug/L)	TOC (MSL)	Depth to Water (ft.)	GW Elevation (MSL)	SPH Thickness (ft.)	DO Reading (ppm)
MW-7	06/05/2008	6,400	NA	3.8	<5.0	220	253	NA	<5.0	NA	NA	NA	NA	NA	NA	44.45	17.65	26.80	NA	0.09
MW-7	09/29/2008	2,500	NA	1.6	<1.0	40	8.1	NA	<1.0	<2.0	<2.0	<2.0	<10	NA	NA	44.45	19.40	25.05	NA	1.26
MW-7	12/19/2008	5,600	NA	5.4	<5.0	110	97.0	NA	<5.0	NA	NA	NA	NA	NA	NA	44.45	19.17	25.28	NA	2.11
MW-7	03/10/2009	3,400	NA	22	<5.0	94	92	NA	<5.0	NA	NA	NA	NA	NA	NA	44.45	16.21	28.24	NA	1.85
MW-8	10/21/2002	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	43.27	17.70	25.57	NA	NA
MW-8	12/27/2002	30,000	NA	280	220	2,000	5,300	NA	<10	<10	<10	<10	<100	<10	<10	43.27	14.25	29.02	NA	1.2
MW-8	03/05/2003	30,000	NA	220	150	2,100	4,200	NA	<100	NA	NA	NA	NA	NA	NA	43.27	15.36	27.91	NA	1.3
MW-8	06/24/2003	Well inaccessible		NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	43.27	NA	NA	NA	NA
MW-8	09/25/2003	26,000	NA	240	53	1,600	2,600	NA	<50	NA	NA	NA	NA	NA	NA	43.27	17.43	25.84	NA	1.0
MW-8	12/15/2003	38,000	NA	290	140	2,200	5,200	NA	<13	NA	NA	NA	NA	NA	NA	43.27	16.24	27.03	NA	0.4
MW-8	03/04/2004	19,000	NA	180	95	1,400	3,900	NA	<13	NA	NA	NA	NA	NA	NA	43.27	14.63	28.64	NA	0.1
MW-8	05/27/2004	19,000	NA	230	41	1,100	2,200	NA	<13	NA	NA	NA	NA	NA	NA	43.27	16.41	26.86	NA	0.5
MW-8	09/24/2004	21,000	NA	270	42	1,200	2,600	NA	<13	<50	<50	<50	<130	NA	NA	43.27	18.10	25.17	NA	0.7
MW-8	11/22/2004	24,000	NA	200	64	1,400	4,100	NA	<13	NA	NA	NA	NA	NA	NA	43.27	17.28	25.99	NA	1.0
MW-8	03/02/2005	16,000	NA	100	44	890	2,300	NA	<10	NA	NA	<20	<100	<5.0	NA	43.27	13.35	29.92	NA	0.6
MW-8	06/30/2005	19,000	NA	110	41	700	2,100	NA	<10	NA	NA	NA	NA	NA	NA	43.27	14.91	28.36	NA	0.8
MW-8	09/20/2005	10,000	NA	86	25	600	1,400	NA	<10	<40	<40	<40	<100	NA	NA	43.27	16.11	27.16	NA	0.8
MW-8	12/05/2005	9,900	NA	130	16	600	1,300	NA	<10	NA	NA	NA	NA	NA	NA	43.27	16.20	27.07	NA	0.56
MW-8	03/02/2006	13,000 g	NA	130 g	45	790 g	2,000 g	NA	0.54	NA	NA	NA	NA	NA	NA	43.27	14.28	28.99	NA	1.1
MW-8 (n)	06/29/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	43.27	NA	NA	NA	NA
MW-8 (o)	06/30/2006	14,900	NA	71.8	14.1	622	1,390	NA	<0.500	NA	NA	NA	NA	NA	NA	43.27	14.18	29.09	NA	0.50
MW-8	07/06/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	43.27	14.39	28.88	NA	NA
MW-8	09/11/2006	18,700	NA	94.2	11.2	683	1,280	NA	<0.500	<0.500	<0.500	<0.500	<10.0	NA	NA	43.27	15.10	28.17	NA	0.92
MW-8	12/28/2006	9,000	NA	54	7.1	430	980	NA	<2.5	NA	NA	NA	NA	NA	NA	43.27	15.15	28.12	NA	0.93
MW-8	03/20/2007	7,780	NA	40.4	9.21	230	499	NA	0.840	NA	NA	NA	NA	NA	NA	43.27	15.01	28.26	NA	0.11
MW-8	06/26/2007	7,500 q	NA	36	5.5	360	860	NA	<5.0	NA	NA	NA	NA	NA	NA	43.27	16.40	26.87	NA	0.59
MW-8	09/11/2007	10,000 q	NA	55	7.0	420	1,140	NA	<5.0	<10	<10	<10	<50	NA	NA	43.27	17.42	25.85	NA	1.07
MW-8	12/26/2007	10,000 q	NA	54	12 r	490	1,740	NA	<20	NA	NA	NA	NA	NA	NA	43.27	16.61	26.66	NA	1.4
MW-8	03/19/2008	5,800	NA	20	<5.0	200	600	NA	<5.0	NA	NA	NA	NA	NA	NA	43.27	15.30	27.97	NA	0.24
MW-8	06/05/2008	7,600	NA	27	<5.0	240	750	NA	<5.0	NA	NA	NA	NA	NA	NA	43.27	16.53	26.74	NA	0.10
MW-8	09/29/2008	5,600	NA	47	<5.0	120	287	NA	<5.0	<10	<10	<10	<50	NA	NA	43.27	18.13	25.14	NA	1.04
MW-8	12/19/2008	6,900	NA	40	<5.0	110	374	NA	<5.0	NA	NA	NA	NA	NA	NA	43.27	18.01	25.26	NA	0.74
MW-8	03/10/2009	7,400	NA	38	<5.0	210	780	NA	<5.0	NA	NA	NA	NA	NA	NA	43.27	15.45	27.82	NA	2.40

WELL CONCENTRATIONS
Shell-branded Service Station
1784 150th Avenue
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Well ID	Date	TPPH (ug/L)	TEPH (ug/L)	B (ug/L)	T (ug/L)	E (ug/L)	X (ug/L)	MTBE 8020 (ug/L)	MTBE 8260 (ug/L)	DIPE (ug/L)	ETBE (ug/L)	TAME (ug/L)	TBA (ug/L)	1,2- DCA (ug/L)	EDB (ug/L)	TOC (MSL)	Depth to Water (ft.)	GW Elevation (MSL)	SPH Thickness (ft.)	DO Reading (ppm)
MW-9	12/10/2003	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	41.65	15.15	26.50	NA	NA
MW-9	12/15/2003	<50	NA	<0.50	<0.50	<0.50	1.3	NA	2.5	NA	NA	NA	NA	NA	NA	41.65	14.48	27.17	NA	0.9
MW-9	03/04/2004	<50	NA	<0.50	<0.50	<0.50	<1.0	NA	<0.50	NA	NA	NA	NA	NA	NA	41.65	12.15	29.50	NA	0.2
MW-9	05/27/2004	<50	NA	<0.50	<0.50	<0.50	<1.0	NA	<0.50	NA	NA	NA	NA	NA	NA	41.65	14.55	27.10	NA	0.5
MW-9	09/24/2004	<50	NA	<0.50	<0.50	<0.50	<1.0	NA	<0.50	<2.0	<2.0	<2.0	<5.0	NA	NA	41.65	16.37	25.28	NA	1.0
MW-9	11/22/2004	<50 d	NA	<0.50	<0.50	<0.50	<1.0	NA	<0.50	NA	NA	NA	NA	NA	NA	41.65	15.62	26.03	NA	0.3
MW-9	03/02/2005	100	NA	<0.50	<1.0	1.4	3.8	NA	<1.0	NA	NA	<2.0	<10	<0.50	NA	41.65	11.40	30.25	NA	0.4
MW-9	06/30/2005	<50	NA	<0.50	<0.50	<0.50	<1.0	NA	<0.50	NA	NA	NA	NA	NA	NA	41.65	12.70	28.95	NA	1.3
MW-9	09/20/2005	<50	NA	<0.50	<0.50	<0.50	1.8	NA	<0.50	<2.0	<2.0	<2.0	<5.0	NA	NA	41.65	14.38	27.27	NA	1.2
MW-9	12/05/2005	<50	NA	<0.50	<0.50	<0.50	0.65	NA	<0.50	NA	NA	NA	NA	NA	NA	41.65	14.25	27.40	NA	1.13
MW-9	03/02/2006	<50 h	NA	<0.50	<0.50	<0.50 h	<0.50 h	NA	<0.50	NA	NA	NA	NA	NA	NA	41.65	11.87	29.78	NA	0.9
MW-9 (m)	06/29/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	41.65	12.35	29.30	NA	0.55
MW-9 (o)	06/30/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	41.65	12.37	29.28	NA	NA
MW-9 (p)	07/06/2006	<50.0	NA	<0.500	<0.500	<0.500	<0.500	NA	<0.500	NA	NA	NA	NA	NA	NA	41.65	12.46	29.19	NA	0.58
MW-9	09/11/2006	<50.0	NA	<0.500	<0.500	<0.500	<0.500	NA	<0.500	<0.500	<0.500	<0.500	<10.0	NA	NA	41.65	13.42	28.23	NA	0.79
MW-9	12/28/2006	<50	NA	<0.50	<0.50	<0.50	<1.0	NA	<0.50	NA	NA	NA	NA	NA	NA	41.65	13.23	28.42	NA	0.73
MW-9	03/20/2007	<50.0	NA	<0.500	<0.500	<0.500	<1.00	NA	<0.500	NA	NA	NA	NA	NA	NA	41.65	13.35	28.30	NA	1.20
MW-9	06/26/2007	86 q	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	NA	NA	NA	NA	NA	NA	41.65	14.80	26.85	NA	0.91
MW-9	09/11/2007	<50 q	NA	0.15 r	<1.0	<1.0	<1.0	NA	<1.0	<2.0	<2.0	<2.0	<10	NA	NA	41.65	15.70	25.95	NA	1.04
MW-9	12/26/2007	<50 q	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	NA	NA	NA	NA	NA	NA	41.65	14.86	26.79	NA	2.0
MW-9	03/19/2008	<50	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	NA	NA	NA	NA	NA	NA	41.65	13.39	28.26	NA	0.27
MW-9	06/05/2008	<50	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	NA	NA	NA	NA	NA	NA	41.65	14.77	26.88	NA	1.34
MW-9	09/29/2008	<50	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	<2.0	<2.0	<2.0	<10	NA	NA	41.65	16.62	25.03	NA	1.10
MW-9	12/19/2008	<50	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	NA	NA	NA	NA	NA	NA	41.65	16.26	25.39	NA	0.66
MW-9	03/10/2009	<50	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	NA	NA	NA	NA	NA	NA	41.65	13.22	28.43	NA	1.58
MW-10	12/10/2003	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	50.64	24.33	26.31	NA	NA
MW-10	12/15/2003	6,400	NA	3.1	<1.0	33	20	NA	<1.0	NA	NA	<4.0	<10	<1.0	NA	50.64	23.58	27.06	NA	0.3
MW-10	03/04/2004	1,400	NA	1.2	<1.0	16	3.4	NA	<1.0	NA	NA	<4.0	<10	<1.0	NA	50.64	21.20	29.44	NA	0.1
MW-10	05/27/2004	810	NA	<1.0	<1.0	8.3	<2.0	NA	<1.0	NA	NA	<4.0	<10	<1.0	NA	50.64	23.63	27.01	NA	0.5
MW-10	09/24/2004	790	NA	1.2	<1.0	7.3	<2.0	NA	<1.0	<4.0	<4.0	<4.0	<10	<1.0	<1.0	50.64	25.30	25.34	NA	1.5
MW-10	11/22/2004	1,100	NA	1.1	<0.50	17	<1.0	NA	<0.50	NA	NA	<2.0	<5.0	<0.50	NA	50.64	24.62	26.02	NA	0.4
MW-10	03/02/2005	920	NA	0.60	<1.0	3.5	<1.0	NA	<1.0	NA	NA	<2.0	<10	<0.50	NA	50.64	20.72	29.92	NA	0.4
MW-10	06/30/2005	470 f	NA	<0.50	<0.50	1.4	<1.0	NA	<0.50	NA	NA	<2.0	<5.0	<0.50	NA	50.64	21.48	29.16	NA	1.4
MW-10	09/20/2005	420	NA	<0.50	<0.50	1.2	2.1	NA	<0.50	<2.0	<2.0	<2.0	<5.0	<0.50	NA	50.64	23.45	27.19	NA	2.0

WELL CONCENTRATIONS
Shell-branded Service Station
1784 150th Avenue
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Well ID	Date	TPPH (ug/L)	TEPH (ug/L)	B (ug/L)	T (ug/L)	E (ug/L)	X (ug/L)	MTBE 8020 (ug/L)	MTBE 8260 (ug/L)	DIPE (ug/L)	ETBE (ug/L)	TAME (ug/L)	TBA (ug/L)	1,2- DCA (ug/L)	EDB (ug/L)	TOC (MSL)	Depth to Water (ft.)	GW Elevation (MSL)	SPH Thickness (ft.)	DO Reading (ppm)
MW-10	12/05/2005	420	NA	<0.50	<0.50	1.1	<0.50	NA	<0.50	NA	NA	<0.50	<5.0	<0.50	NA	50.64	23.42	27.22	NA	0.97
MW-10	03/02/2006	230 h	NA	<0.50 h	<0.50	0.83 h	<0.50 h	NA	<0.50	NA	NA	<0.50	<5.0 h	<0.50 j	NA	50.64	21.13	29.51	NA	1.1
MW-10 (n)	06/29/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	50.64	NA	NA	NA	NA
MW-10 (o)	06/30/2006	<50.0	NA	<0.500	<0.500	<0.500	<0.500	NA	<0.500	NA	NA	<0.500	<10.0	<0.500	NA	50.64	21.49	29.15	NA	0.37
MW-10	07/06/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	50.64	21.60	29.04	NA	NA
MW-10	09/11/2006	250	NA	<0.500	<0.500	<0.500	<0.500	NA	<0.500	<0.500	<0.500	<0.500	<10.0	<0.500	NA	50.64	22.62	28.02	NA	0.98
MW-10	12/28/2006	Well inaccessible		NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	50.64	NA	NA	NA	NA
MW-10	03/20/2007	158	NA	<0.500	<0.500	<0.500	<1.00	NA	<0.500	NA	NA	<1.00	<50.0	<0.500	NA	50.64	22.30	28.34	NA	0.10
MW-10	06/26/2007	230 q	NA	0.15 r	<1.0	0.43 r	<1.0	NA	<1.0	NA	NA	<2.0	<10	<0.50	NA	50.64	23.75	26.89	NA	1.54
MW-10	09/11/2007	62 q	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	<2.0	<2.0	<2.0	<10	<0.50	NA	50.64	24.78	25.86	NA	0.98
MW-10	12/26/2007	200 q, t	NA	0.15 r	<1.0	0.30 r	<1.0	NA	<1.0	NA	NA	<2.0	<10	<0.50	NA	50.64	23.86	26.78	NA	0.9
MW-10	03/19/2008	170 q	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	NA	NA	<2.0	<10	<0.50	NA	50.64	22.46	28.18	NA	0.10
MW-10	06/05/2008	150	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	<2.0	<2.0	<2.0	<10	<0.50	NA	50.64	23.76	26.88	NA	0.11
MW-10	09/29/2008	130	NA	<0.50	<1.0	<1.0	1.4	NA	<1.0	<2.0	<2.0	<2.0	<10	<0.50	NA	50.64	25.59	25.05	NA	0.91
MW-10	12/19/2008	220	NA	1.6	1.4	1.9	4.3	NA	<1.0	NA	NA	<2.0	<10	<0.50	NA	50.64	22.39	28.25	NA	0.26
MW-10	03/10/2009	120	NA	<0.50	<1.0	<1.0	1.8	NA	<1.0	NA	NA	<2.0	<10	<0.50	NA	50.64	21.79	28.85	NA	0.40
MW-11	12/10/2003	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	45.58	19.10	26.48	NA	NA
MW-11	12/15/2003	110,000	NA	9,900	3,300	3,900	23,000	NA	20,000	NA	NA	<800	18,000	<200	NA	45.58	18.50	27.08	NA	0.3
MW-11	03/04/2004	68,000	NA	5,300	3,000	3,600	23,000	NA	8,300	NA	NA	<200	12,000	<50	NA	45.58	16.67	28.91	NA	0.1
MW-11	05/27/2004	86,000	NA	8,500	3,200	13,000	22,000	NA	25,000	NA	NA	<400	18,000	<100	NA	45.58	18.60	26.98	NA	1.6
MW-11	09/24/2004	63,000	NA	7,200	2,000	3,000	15,000	NA	26,000	<400	<400	<400	17,000	<100	<100	45.58	20.22	25.36	NA	2.2
MW-11	11/22/2004	96,000	NA	7,100	3,700	2,800	15,000	NA	20,000	NA	NA	<400	14,000	<100	NA	45.58	19.56	26.02	NA	0.3
MW-11	03/02/2005	63,000	NA	6,200	6,800	2,200	15,000	NA	16,000	NA	NA	<200	7,800	<50	NA	45.58	15.75	29.83	NA	4.6
MW-11	06/30/2005	100,000	NA	4,200	18,000	3,800	25,000	NA	2,500	NA	NA	<400	3,400	<100	NA	45.58	16.92	28.66	NA	1.0
MW-11	09/20/2005	65,000	NA	3,800	10,000	3,100	19,000	NA	3,900	<400	<400	<400	4,600	<100	NA	45.58	18.43	27.15	NA	NA
MW-11	12/05/2005	69,000	NA	4,000	10,000	3,100	16,000	NA	7,400	NA	NA	<50	4,400	<50	NA	45.58	18.26	27.32	NA	0.70
MW-11	03/02/2006	76,000 g	NA	4,000 g	13,000 g	2,900 g	16,000 g	NA	6,100 g	NA	NA	36	420 k	<0.50 j	NA	45.58	16.13	29.45	NA	0.9
MW-11	04/19/2006	116,000	NA	4,780	12,000	3,280	20,200	NA	5,550	NA	NA	34.6	4,010	<0.500	NA	45.58	15.30	30.28	NA	0.86
MW-11	05/01/2006	129,000	NA	4,180	15,100	3,180	18,700	NA	4,510	NA	NA	28.9	3,130	92.1	NA	45.58	15.43	30.15	NA	0.97
MW-11 (n)	06/29/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	45.58	NA	NA	NA	NA
MW-11 (o)	06/30/2006	119,000	NA	4,420	11,300	2,650	17,200	NA	4,490	NA	NA	22.8	2,700	<0.500	NA	45.58	15.49	30.09	NA	0.49
MW-11	07/06/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	45.58	16.61	28.97	NA	NA
MW-11	07/31/2006	<50.0	NA	4,870	11,400	2,890	20,400	NA	4,880	NA	NA	27.2	3,120	<0.500	NA	45.58	17.00	28.58	NA	0.36
MW-11	08/23/2006	115,000	NA	5,230	8,720	2,680	16,900	NA	4,860	NA	NA	29.6	3,670	<10.0	NA	45.58	17.28	28.30	NA	0.7

WELL CONCENTRATIONS
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Well ID	Date	TPPH (ug/L)	TEPH (ug/L)	B (ug/L)	T (ug/L)	E (ug/L)	X (ug/L)	MTBE 8020 (ug/L)	MTBE 8260 (ug/L)	DIPE (ug/L)	ETBE (ug/L)	TAME (ug/L)	TBA (ug/L)	1,2- DCA (ug/L)	EDB (ug/L)	TOC (MSL)	Depth to Water (ft.)	GW Elevation (MSL)	SPH Thickness (ft.)	DO Reading (ppm)
MW-11	09/11/2006	9,090	NA	5,140	8,400	3,040	17,700	NA	5,310	<0.500	<0.500	134	4,240	<0.500	NA	45.58	17.62	27.96	NA	0.63
MW-11	10/18/2006	193,000	NA	4,930	9,700	3,920	21,000	NA	4,300	NA	NA	<0.500	2,530	<0.500	NA	45.58	18.08	27.50	NA	0.51
MW-11	11/22/2006	3,600	NA	3,600	9,300	2,800	16,000	NA	2,800	NA	NA	<10	4,000	<2.5	NA	45.58	18.06	27.52	NA	0.4
MW-11	12/28/2006	75,000	NA	2,700	9,800	1,900	13,000	NA	2,500	NA	NA	<200	2,500	<50	NA	45.58	17.20	28.38	NA	0.9
MW-11	01/25/2007	68,000	NA	2,900	9,600	2,200	13,000	NA	2,400	NA	NA	<200	2,400	<50	NA	45.58	18.10	27.48	NA	0.7
MW-11	02/19/2007	88,000	NA	3,600	17,000	3,200	20,000	NA	2,200	NA	NA	25	4,000	<5.0	NA	45.58	17.89	27.69	NA	0.2
MW-11	03/20/2007	77,600	NA	3,140	12,800	3,060	17,600	NA	1,930	NA	NA	<200	<10,000	<100	NA	45.58	17.30	28.28	NA	0.38
MW-11	04/05/2007	67,000 q	NA	3,200	9,600	3,200	14,300	NA	1,800	NA	NA	<100	2,900	<25	NA	45.58	17.50	28.08	NA	0.72
MW-11	06/01/2007	65,000 q	NA	3,100	11,000	3,200	17,900	NA	1,700	NA	NA	NA	NA	NA	NA	45.58	18.32	27.26	NA	1.18
MW-11	06/26/2007	52,000 q	NA	2,200	8,000	2,200	13,700	NA	1,300	NA	NA	<200	2,300	<50	NA	45.58	18.70	26.88	NA	0.24
MW-11	07/19/2007	62,000 q	NA	2,500	9,600	2,400	16,300	NA	1,500	NA	NA	NA	NA	NA	NA	45.58	18.10	27.48	NA	3.42
MW-11	08/14/2007	65,000 q	NA	3,000	11,000	3,000	17,600	NA	1,000	NA	NA	NA	NA	NA	NA	45.58	19.30	26.28	NA	1.1
MW-11	09/11/2007	45,000 q	NA	2,000	6,300	2,100	11,900	NA	960	<100	<100	<100	2,100	<25	NA	45.58	19.65	25.93	NA	0.86
MW-11	10/26/2007	58,000 q	NA	2,500	9,300	3,200	17,700	NA	900	NA	NA	NA	NA	NA	NA	45.58	19.42	26.16	NA	1.2
MW-11	11/13/2007	64,000 q	NA	2,400	9,500	3,300	18,000	NA	1,200	NA	NA	NA	NA	NA	NA	45.58	19.34	26.24	NA	0.32
MW-11	12/26/2007	56,000 q	NA	2,300	11,000	3,800	23,400	NA	1,300	NA	NA	<40	1,400	<10	NA	45.58	18.68	26.90	NA	0.9
MW-11	01/03/2008	64,000 q	NA	2,600	10,000	4,400	23,600	NA	1,300	NA	NA	NA	NA	NA	NA	45.58	18.86	26.72	NA	1.65
MW-11	02/21/2008	70,000 q	NA	2,400	9,200	3,700	18,700	NA	440	NA	NA	NA	NA	NA	NA	45.58	16.70	28.88	NA	0.9
MW-11	03/19/2008	65,000 q	NA	2,500	7,700	3,700	19,700	NA	520	NA	NA	<100	810	<25	NA	45.58	17.34	28.26	0.02	0.07
MW-11	04/16/2008	86,000	NA	3,000	8,200	4,500	24,300	NA	280	NA	NA	NA	NA	NA	NA	45.58	17.78	27.80	NA	1.40
MW-11	05/29/2008	70,000	NA	1,900	6,000	3,200	16,500	NA	110	NA	NA	NA	NA	NA	NA	45.58	18.52	27.06	NA	0.43
MW-11	06/05/2008	72,000	NA	1,800	6,700	3,300	18,000	NA	120	<100	<100	<100	<500	<25	NA	45.58	18.63	26.95	NA	0.21
MW-11	07/22/2008	100,000	NA	1,100	9,200	3,800	24,900	NA	<100	NA	NA	NA	NA	NA	NA	45.58	19.41	26.17	NA	1.31
MW-11	09/29/2008	110,000	NA	1,500	10,000	4,300	27,200	NA	210	<100	<100	<100	<500	<25	NA	45.58	20.21	25.37	NA	0.79
MW-11	12/19/2008	110,000	NA	1,000	9,600	3,700	24,600	NA	<100	NA	NA	<200	<1,000	<50	NA	45.58	19.75	25.83	NA	0.52
MW-11	03/10/2009	92,000	NA	490	11,000	4,000	30,000	NA	<100	NA	NA	<200	<1,000	<50	NA	45.58	16.40	29.18	NA	0.50
MW-12	06/26/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	44.10	14.75	29.35	NA	NA
MW-12 (n)	06/29/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	44.10	NA	NA	NA	NA
MW-12 (o)	06/30/2006	95,000	NA	3,930	8,900	2,110	10,400	NA	<0.500	NA	NA	NA	NA	NA	NA	44.10	15.00	29.10	NA	0.62
MW-12	07/06/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	44.10	15.10	29.00	NA	NA
MW-12	09/11/2006	5,110	NA	3,930	3,290	2,710	8,060	NA	8.50	NA	NA	NA	NA	NA	NA	44.10	15.91	28.19	NA	1.09
MW-12	12/28/2006	31,000	NA	2,400	1,100	1,500	2,900	NA	<2.5	NA	NA	NA	NA	NA	NA	44.10	15.85	28.25	NA	0.82
MW-12	03/20/2007	30,100	NA	508	352	341	748	NA	<0.500	NA	NA	NA	NA	NA	NA	44.10	15.81	28.29	NA	1.44
MW-12	06/26/2007	32,000 q	NA	2,700	1,200	2,100	3,700	NA	<20	NA	NA	NA	NA	NA	NA	44.10	17.29	26.81	NA	0.40

WELL CONCENTRATIONS
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San Leandro, CA

Well ID	Date	TPPH (ug/L)	TEPH (ug/L)	B (ug/L)	T (ug/L)	E (ug/L)	X (ug/L)	MTBE 8020 (ug/L)	MTBE 8260 (ug/L)	DIPE (ug/L)	ETBE (ug/L)	TAME (ug/L)	TBA (ug/L)	1,2- DCA (ug/L)	EDB (ug/L)	TOC (MSL)	Depth to Water (ft.)	GW Elevation (MSL)	SPH Thickness (ft.)	DO Reading (ppm)
MW-12	09/11/2007	21,000 q	NA	810	720	860	1,950	NA	<20	NA	NA	NA	NA	NA	NA	44.10	18.08	26.02	NA	1.21
MW-12	12/26/2007	20,000 q	NA	2,000	600	1,400	2,870	NA	<20	NA	NA	NA	NA	NA	NA	44.10	17.44	26.66	NA	1.3
MW-12	03/19/2008	12,000	NA	1,000	460	630	1,490	NA	<20	NA	NA	NA	NA	NA	NA	44.10	15.97	28.13	NA	0.28
MW-12	06/05/2008	22,000	NA	860	530	930	2,340	NA	<10	NA	NA	NA	NA	NA	NA	44.10	17.28	26.82	NA	0.10
MW-12	09/29/2008	23,000	NA	1,800	820	1,300	2,900	NA	<10	NA	NA	NA	NA	NA	NA	44.10	19.10	25.00	NA	0.76
MW-12	12/19/2008	12,000	NA	850	240	530	930	NA	<10	NA	NA	NA	NA	NA	NA	44.10	18.68	25.42	NA	0.47
MW-12	03/10/2009	6,400	NA	720	110	450	570	NA	<10	NA	NA	NA	NA	NA	NA	44.10	15.55	28.55	NA	2.25
MW-13	06/26/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	41.59	12.10	29.49	NA	NA
MW-13 (m)	06/29/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	41.59	12.47	29.12	NA	0.61
MW-13 (o)	06/30/2006	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	41.59	12.25	29.34	NA	NA
MW-13 (p)	07/06/2006	<50.0	NA	<0.500	<0.500	<0.500	<0.500	NA	<0.500	<0.500	<0.500	<0.500	<10.0	<0.500	NA	41.59	12.35	29.24	NA	0.24
MW-13	09/11/2006	<50.0	NA	<0.500	<0.500	<0.500	<0.500	NA	<0.500	NA	NA	NA	NA	NA	NA	41.59	13.33	28.26	NA	1.02
MW-13	12/28/2006	<50	NA	<0.50	<0.50	<0.50	<1.0	NA	<0.50	NA	NA	NA	NA	NA	NA	41.59	13.12	28.47	NA	0.81
MW-13	03/20/2007	<50.0	NA	1.41	2.36	2.20	6.29	NA	<0.500	NA	NA	NA	NA	NA	NA	41.59	13.12	28.47	NA	0.14
MW-13	06/26/2007	58 q	NA	0.20 r	<1.0	<1.0	<1.0	NA	<1.0	NA	NA	NA	NA	NA	NA	41.59	14.68	26.91	NA	0.38
MW-13	09/11/2007	<50 q	NA	0.69	0.30 r	<1.0	<1.0	NA	<1.0	NA	NA	NA	NA	NA	NA	41.59	15.51	26.08	NA	0.92
MW-13	12/26/2007	<50 q	NA	0.24 r	<1.0	<1.0	<1.0	NA	<1.0	NA	NA	NA	NA	NA	NA	41.59	14.74	26.85	NA	1.0
MW-13	03/19/2008	<50	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	NA	NA	NA	NA	NA	NA	41.59	13.28	28.31	NA	0.34
MW-13	06/05/2008	<50	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	NA	NA	NA	NA	NA	NA	41.59	14.65	26.94	NA	0.15
MW-13	09/29/2008	<50	NA	0.53	<1.0	<1.0	<1.0	NA	<1.0	NA	NA	NA	NA	NA	NA	41.59	16.50	25.09	NA	1.59
MW-13	12/19/2008	<50	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	NA	NA	NA	NA	NA	NA	41.59	16.12	25.47	NA	0.49
MW-13	03/10/2009	<50	NA	<0.50	<1.0	<1.0	<1.0	NA	<1.0	NA	NA	NA	NA	NA	NA	41.59	12.75	28.84	NA	1.52
P-1A	09/15/2008	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	47.74	22.49	25.25	NA	NA
P-1A	12/19/2008	13,000	NA	90	24	1,100	893	NA	190	NA	NA	NA	NA	NA	NA	47.74	22.23	25.51	NA	0.54
P-1B	09/15/2008	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	47.65	22.50	25.15	NA	NA
P-1B	12/19/2008	82,000	NA	5,200	3,300	3,000	9,600	NA	1,300	NA	NA	NA	NA	NA	NA	47.65	22.25	25.40	NA	0.66
P-2A	09/15/2008	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	48.81	23.58	25.23	NA	NA
P-2A	12/19/2008	1,900	NA	70	<2.0	19	<2.0	NA	94	NA	NA	NA	NA	NA	NA	48.81	23.49	25.32	NA	3.92
P-2B	09/15/2008	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	49.02	23.40	25.62	NA	NA
P-2B	12/19/2008	7,500	NA	450	<5.0	93	81	NA	410	NA	NA	NA	NA	NA	NA	49.02	23.61	25.41	NA	0.17

WELL CONCENTRATIONS
Shell-branded Service Station
1784 150th Avenue
San Leandro, CA

Well ID	Date	TPPH (ug/L)	TEPH (ug/L)	B (ug/L)	T (ug/L)	E (ug/L)	X (ug/L)	MTBE 8020 (ug/L)	MTBE 8260 (ug/L)	DIPE (ug/L)	ETBE (ug/L)	TAME (ug/L)	TBA (ug/L)	1,2- DCA (ug/L)	EDB (ug/L)	TOC (MSL)	Depth to Water (ft.)	GW Elevation (MSL)	SPH Thickness (ft.)	DO Reading (ppm)
P-3A	09/15/2008	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	44.56	19.21	25.35	NA	NA
P-3A	12/19/2008	64,000	NA	1,900	1,900	3,600	12,300	NA	170	NA	NA	NA	NA	NA	NA	44.56	19.03	25.53	NA	0.37
P-3B	09/15/2008	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	44.62	19.02	25.60	NA	NA
P-3B	12/19/2008	70,000	NA	5,700	2,300	3,300	11,600	NA	1,100	NA	NA	NA	NA	NA	NA	44.62	19.26	25.36	NA	NA
P-4A	09/15/2008	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	45.00	19.95	25.05	NA	NA
P-4A	10/02/2008	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	45.00	19.63	25.37	NA	NA
P-4A	12/19/2008	80,000	NA	330	9,300	3,800	14,300	NA	130	NA	NA	NA	NA	NA	NA	45.00	19.32	25.68	NA	0.76
P-4B	09/15/2008	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	44.93	19.30	25.63	NA	NA
P-4B	12/19/2008	81,000	NA	1,100	5,800	4,000	17,500	NA	390	NA	NA	NA	NA	NA	NA	44.93	19.50	25.43	NA	0.52

WELL CONCENTRATIONS
Shell-branded Service Station
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Well ID	Date	TPPH (ug/L)	TEPH (ug/L)	B (ug/L)	T (ug/L)	E (ug/L)	X (ug/L)	MTBE 8020 (ug/L)	MTBE 8260 (ug/L)	DIPE (ug/L)	ETBE (ug/L)	TAME (ug/L)	TBA (ug/L)	1,2- DCA (ug/L)	EDB (ug/L)	TOC (MSL)	Depth to Water (ft.)	GW Elevation (MSL)	SPH Thickness (ft.)	DO Reading (ppm)
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Abbreviations:

TPPH = Total petroleum hydrocarbons as gasoline by EPA Method 8260B; prior to June 11, 2001, analyzed by EPA Method 8015.

TEPH = Total petroleum hydrocarbons as diesel by modified EPA Method 8015.

BTEX = Benzene, toluene, ethylbenzene, xylenes by EPA Method 8260B; prior to June 11, 2001, analyzed by EPA Method 8020.

MTBE = Methyl tertiary butyl ether

DIPE = Di-isopropyl ether, analyzed by EPA Method 8260

ETBE = Ethyl tertiary butyl ether, analyzed by EPA Method 8260

TAME = Tertiary amyl methyl ether, analyzed by EPA Method 8260

TBA = Tertiary butyl alcohol, analyzed by EPA Method 8260

1,2-DCA = 1,2-dichloroethane, analyzed by EPA Method 8260

EDB = 1,2-dibromomethane or ethylene dibromide, analyzed by EPA Method 8260

TOC = Top of Casing Elevation

SPH = Separate-Phase Hydrocarbons

GW = Groundwater

DO = Dissolved Oxygen

ug/L = Parts per billion

ppm = Parts per million

MSL = Mean sea level

ft. = Feet

<n = Below detection limit

(D) = Duplicate sample

NA = Not applicable

WELL CONCENTRATIONS
Shell-branded Service Station
1784 150th Avenue
San Leandro, CA

Well ID	Date	TPPH (ug/L)	TEPH (ug/L)	B (ug/L)	T (ug/L)	E (ug/L)	X (ug/L)	MTBE 8020 (ug/L)	MTBE 8260 (ug/L)	DIPE (ug/L)	ETBE (ug/L)	TAME (ug/L)	TBA (ug/L)	1,2- DCA (ug/L)	EDB (ug/L)	TOC (MSL)	Depth to Water (ft.)	GW Elevation (MSL)	SPH Thickness (ft.)	DO Reading (ppm)
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Notes:

a = Chromatogram pattern indicates an unidentified hydrocarbon.

b = Samples not analyzed due to laboratory oversight.

c = Hydrocarbon does not match pattern of laboratory's standard.

d = The concentration reported reflects individual or discrete unidentified peaks not matching a typical fuel pattern.

e = Estimated value. The concentration exceeded the calibration of analysis.

f = Quantity of unknown hydrocarbon(s) in sample based on gasoline.

g = Sample was originally analyzed within the EPA recommended hold time. Re-analysis for dilution was performed past the recommended hold time.

h = Sample was originally analyzed within the EPA recommended hold time. Re-analysis for confirmation was performed past the recommended hold time.

i = The result for this hydrocarbon is elevated due to the presence of single analyte peak(s) in the quantitation range.

j = Result was reported with a possible low bias due to the continuing calibration verification falling outside the acceptance criteria.

k = The result was reported with a possible low bias due to the continuing calibration verification falling outside the acceptance criteria.

l = Sample required dilution due to high concentrations of target analyte.

m = Well resampled on July 6, 2006 due to laboratory error.

n = Well not accessed due to equipment malfunction.

o = All wells regauged on June 30, 2006 prior to sampling.

p = Wells resampled for 2Q06 event due to laboratory error.

q = Analyzed by EPA Method 8015B (M).

r = Analyte was detected at a concentration below the reporting limit and above the laboratory method detection limit. Reported value is estimated.

t = the sample chromatographic pattern for TPH does not match the chromatographic pattern of the specified standard. Quantitation of the unknown hydrocarbon(s) in the sample was based upon the specified standard.

* = Sample analyzed out of EPA recommended hold time.

When Separate-Phase Hydrocarbons are present, the groundwater elevation is adjusted using the following formula: $GWE = TOC - DTW + 0.8 * SPH$ thickness.

Site surveyed January 23, 2002 by Virgil Chavez Land Surveying of Vallejo, CA.

Wells MW-7 and MW-8 surveyed by Virgil Chavez Land Surveying of Vallejo, CA

Wells MW-9, MW-10, and MW-11 surveyed December 11, 2003 by Virgil Chavez Land Surveying of Vallejo, CA.

Wells MW-12 and MW-13 surveyed on June 9, 2006 by Virgil Chavez Land Surveying of Vallejo, CA.