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Alameda County Environmental Health



February 25, 2009

Jerry Wickham, P.G., C.E.G., C.HG. Senior Hazardous Materials Specialist ALAMEDA COUNTHY ENVIRONMENTAL HEALTH 1131 Harbor Bay Parkway, Suite 250 Alameda, CA 94502-6577

Bureau Veritas Project No. 33104-004578.00

Subject: Workplan for Additional Subsurface Investigation

Former Lemoine Sausage Factory

630 20th Avenue

Oakland, California 94601

Fuel Leak Case No. RO0000334 and Geotracker ID T0600102114

Dear Mr. Wickham:

Bureau Veritas North America, Inc. (Bureau Veritas) is pleased to present this workplan to conduct an additional subsurface investigation at the subject property. Our workplan was prepared in accordance with the objectives outlined in your letter dated November 12, 2008.

We are ready to commence investigation efforts upon your approval of this workplan. If you have any questions or comments regarding this workplan, please do not hesitate to contact me at (925) 426-2626 or at timothy.bodkin@us.bureauveritas.com.

Sincerely,

Timothy G. Bodkin, C.E.G., R.E.A. II

wiethy & Book

Senior Project Manager

Health, Safety, and Environmental Services

Enclosure

cc: Nanda Thalasila, AIG

Donna Profitt, Bank of America

Heather Bush, Bureau Veritas North America, Inc.

Workplan for Additional Subsurface Investigation

Former Lemoine Sausage Factory 630 29th Avenue Oakland, California 94601

February 25, 2009 33104-004578.00

Prepared for ALAMEDA COUNTY ENVIRONMENTAL HEALTH 1131 Harbor Bay Parkway, Suite 250 Alameda, California 94502-6577



For the benefit of business and people

Bureau Veritas North America, Inc.

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1.0 INTRODUCTION

Bureau Veritas North America, Inc. (Bureau Veritas) has prepared this workplan to conduct an additional subsurface investigation at the Former Lemoine Sausage Factory ("Site), located at 630 29th Avenue in Oakland, California. The workplan has been prepared in accordance with the Alameda County Environmental Health's (ACEH) letter dated November 12, 2008, requiring that additional subsurface investigation be conducted at the Site.

As presented in their letter, ACEH reviewed groundwater monitoring data from Second Quarter 2008, which showed that a plume of dissolved petroleum hydrocarbons extends more than 200 feet in a west-southwest direction from the former UST area at the Site. Total petroleum hydrocarbons as gasoline (TPH-g) and benzene were detected in groundwater at concentrations up to 26,000 and 9,700 micrograms per liter (µg/L), respectively in Second Quarter 2008. Detected concentrations of the TPH-g and benzene exceed California Regional Water Quality Control Board (RWQCB) Environmental Screening Levels (ESLs) for both drinking water and non-drinking water resources. Chlorinated volatile organic compounds (VOCs) also were also detected in groundwater in on-site and off-site areas. The source of the VOCs is unknown.

On the basis of information presented in the ACEH's letter, the objectives of this additional subsurface investigation include:

- Delineating the dissolved petroleum hydrocarbon plume within its central and downgradient portions
- Investigating potential source(s) for the VOCs
- Delineating the lateral extent of coarse-grained soils below the 15-foot depth
- Assessing nearby utility corridors that may serve as contaminant migration pathways
- Evaluating potential vapor intrusion into the existing building on-site

Descriptions of the site background and proposed scope of work supporting the objectives of this additional investigation are provided in the following sections.

2.0 SITE BACKGROUND

The Site is located at the southeast corner of the intersection of 29th Avenue and East 7th Street, in an area primarily zoned light industrial and commercial. The location of the Site is shown on Figure 1. The Site is surrounded by light industrial and commercial facilities to the north and south, the 29th Avenue overpass to the west, and a light industrial/commercial facility and residences to the east. An unpaved, undeveloped lot containing automobile wreckage, miscellaneous equipment, and scrap metal materials is located to the west of the Site. A blacksmith and steel fabrication shop (Mor-Drop) is located further west of the undeveloped lot. Residential areas are located further south and east of the adjacent commercial properties. According to historic maps, machine shops also were formerly located in the adjacent undeveloped lot. An automotive repair facility was formerly located to the south.



The Site is occupied by an approximately 9,262-square foot, L-shaped building formerly used as a sausage factory and cold storage warehouse. The building is a one-story, wood-framed, stucco exterior structure with concrete flooring and a wooden roof. The concrete flooring lies approximately 3.5 feet above street grade within the western and central portions of the building, and lies at ground level within the eastern portion of the building.

During earlier operations at the Site, the interior of the building was divided into a sausage production area, cold storage area, office area, refrigeration machinery room, and employee locker room. Additional refrigeration equipment was formerly present on the roof of the building, as noted during previous investigations. The building is currently subdivided into three tenant spaces. The eastern portion is occupied by an automobile repair and hobby shop. The central portion is occupied by an architectural design and fabrication facility. The western portion is occupied by an art fabricator.

A 1,000-gallon gasoline underground storage tank (UST) and associated piping were formerly located beneath the sidewalk along 7th Street adjacent to the northeast side of the building. The UST was located near the roll-up door on the building. The fuel dispenser for the UST was located in a "cubby hole" adjacent to the building's roll-up door. The location of the former UST is shown on Figure 2.

2.1 UST REMOVAL

In November 1996, the UST and associated piping were removed. Groundwater was encountered at the 5-foot depth during excavation activities. A petroleum hydrocarbon sheen was observed in groundwater that entered the excavation during the UST removal. Seven (7) soil samples (S-1 through S-7) were obtained during UST removal under the direction of ACEH. The soil samples were collected at depths between 5 and 8 feet below ground surface (bgs) beneath the fill ends of the UST and the dispenser. The soil samples were analyzed for TPH-g, methyl tertiary butyl ether (MTBE), benzene, toluene, ethylbenzene, and xylenes (BTEX), and organic lead. Analytical results showed concentrations of these constituents ranging between non-detection and 4,300 milligrams per kilogram (mg/kg). Chemical concentrations detected in soil during the UST removal are shown on Figure 3.

2.2 PREVIOUS INVESTIGATIONS

Since 1997, several investigations and quarterly groundwater monitoring events have been performed at the Site to characterize soil quality and monitor groundwater conditions and quality. To date, this has included ten (10) soil borings (B-1 through B-10) to assess soil and groundwater quality around the vicinity of the former UST excavation and beneath the building footprint, and thirteen (13) groundwater monitoring wells (MW-1 through MW-13) within the uppermost water-bearing zone to characterize groundwater conditions and quality, as well as delineate the extent of impacted groundwater on- and off-site. Previous investigation results suggest the mass of impacted soil is located around the former UST location and beneath a limited portion of the building footprint on the northeast side of the building along East 7th Street. Boring and monitoring well locations are shown on Figure 2. Soil analytical results from Borings B-1 through B-5 are shown on Figure 3. Boring logs and monitoring well construction details from these previous investigations are provided in Appendix A.

In 1999, Clayton Group Services, Inc. (Clayton, now Bureau Veritas) initiated quarterly groundwater monitoring activities at the Site. Since the inception of quarterly monitoring, groundwater flow consistently has been to the west-southwest, and analytical data has shown TPH- and benzene-impacted



groundwater extending across a portion of the Site, as well as off-site to the west. The highest concentrations of TPH-g and benzene have been detected in on-site Wells MW-2 and MW-9, which are both located inside the central portion of the building. Historical groundwater elevation data is presented in Appendix B. Historical groundwater analytical data is presented in Appendix C.

TPH-g and benzene concentrations in groundwater generally have remained within the same order of magnitude over the past several monitoring events. The lateral extent of the groundwater plume is roughly defined by the TPH and benzene concentrations detected in the outermost monitoring wells with the exception of the TPH-g and benzene concentrations detected in the most downgradient well (MW-13), which may be attributable to an off-site source. Groundwater elevations measured during Fourth Quarter 2008 are shown on Figure 4. TPH-g and benzene concentrations detected in groundwater during Fourth Quarter 2008 are shown on Figures 5 and 6, respectively.

VOCs, primarily trichloroethene (TCE), cis-1,2-dichloroethene (cis-1,2-DCE), trans-1,2-DCE, and vinyl chloride (VC), have been detected in some of the wells (MW-8, MW-12, and MW-13) during previous monitoring events. The presence of cis-1,2-DCE, trans-1,2-DCE, and VC in groundwater over the past several monitoring events indicates that natural attenuation of the TCE is occurring. The VOC plume is stable in size and configuration, and has not shown further offsite migration to the west. The source of VOCs in groundwater is unknown and appears to be offsite. TCE and cis-1,2-DCE concentrations detected in groundwater during Fourth Quarter 2008 are shown on Figure 7.

2.2.1 Risk Assessment/Feasibility Study (RA/FS)

In 2001, Clayton performed a risk assessment and feasibility study (RA/FS) to determine site-specific cleanup goals and evaluate potential remedial measures for the Site. The risk assessment was performed at the Tier II level in accordance with the California Code of Regulations Title 22 Division 21 (Title 22), American Society for Testing and Materials (ASTM-E1735) Standard Guide for Risk Based Corrective Action (RBCA) Applied at Petroleum Release Sites (ASTM, 1995), and the Oakland Urban Land Redevelopment Program (OULRP) Guidance Document (COPWA, 2000), as well as in accordance with the City of Oakland's document entitled "Oakland Risk-Based Corrective Action: Technical Background Document" updated January 1, 2000. The risk assessment identified chemicals of concern, primary sources, secondary sources, transport mechanisms and chemical exposure pathways to potential receptors. As part of the RA/FS, a receptor characterization and survey, risk evaluation, and identification of decision analysis-remedial action options were implemented.

The receptor survey determined that no domestic drinking water wells exist within a 2,000-foot radius of the Site, and, therefore, there is no risk of exposure from groundwater consumption downgradient and within 2,000 feet of the Site. Nearby underground utilities, including a storm drain and sanitary sewer, were identified as potential conduits for the transport of impacted groundwater. Appendix D provides a map showing storm drain and sanitary sewer locations. Non-detect concentrations noted in monitoring wells adjacent to the Site indicated that groundwater impact to the utility trenches was unlikely. The Oakland Estuary, located approximately 0.2 miles away to the south southwest between the Oakland and Alameda city limits, also was considered as a point of exposure. During the RA/FS, it was assumed that groundwater was able to enter the Oakland Estuary through natural pathways or via leakage from utility trenches. Upon further review, it was concluded that the Oakland Estuary was not a viable pathway of exposure due to its use as an active marine waterway.



In summary, the results of the risk assessment showed there were no off-site receptors that would be impacted by the Site constituents. Groundwater beneath the Site was not considered to be of beneficial use because it was located adjacent to a sanitary sewer system. Low permeability hydrogeologic conditions also showed that groundwater could not be extracted at sufficient rates for consumption over a prolonged period of time. Furthermore, groundwater beneath the Site is brackish and not suitable for consumption.

2.2.2 Evaluation of Remedial Action Alternatives

In 2004, remedial action alternatives were evaluated for practical consideration, technical applicability, and costs. Three (3) remedial action alternatives were selected for evaluation and included Alternative 1 (building demolition, excavation/disposal, and building reconstruction), Alternative 2 (soil excavation, groundwater extraction via the installation of an interceptor trench with soil vapor extraction); and Alternative 3 (groundwater injection using an Oxygen Release Compound (ORC)). Each alternative was evaluated with regard to implementability, effectiveness, and cost.

This evaluation showed that each of the alternatives could be implemented, with the exception of several elements that were not technically or economically feasible. Such restrictions included the intrusiveness of each alternative relative to the building footprint and tenant occupancy, overall cost, and length of time to achieve a designated site-specific cleanup goal.

Alternative 1 was considered the most likely approach to achieve cleanup goals, but would have been the most intrusive to implement because of completely displacing tenants during remedial activities.

Alternative 1 also would have been the most costly to implement. The approach involved building demolition and removal; excavation and offsite disposal of impacted soils; reuse of clean soil from the upper 6 feet of the excavation as fill; and placement of a limited volume of imported soil. Impacted groundwater would have been extracted and treated during construction dewatering. The time needed to complete Alternative 1 would have been significantly less than for Alternatives 2 or 3.

Alternative 2 also would have required temporary tenant relocation, and would have taken much longer to meet cleanup goals because a more localized area of impacted soil, rather than a larger area, would have been removed. The soil vapor extraction for Alternative 2 would not have been effective because of predominant, fine-grained, low permeability soils occurring within the vadose zone. VOC-impacted groundwater from the off-site source likely would have been captured and brought on-site during implementation of Alternatives 1 or 2.

Considering the intrusive nature, cost prohibition, time constraints, low permeability soil conditions, and necessity to capture of VOC-impacted groundwater from an off-site source associated with Alternatives 1 and 2, it was decided that a pilot test for Alternative 3 (ORC injection) would be conducted.

2.2.3 ORC Injection Pilot Study

In 2005, an ORC injection pilot study was performed at the Site to evaluate its technical feasibility for reducing chemical concentrations in groundwater. Two (2) temporary monitoring wells (T-1 and T-2) were installed and ORC injection borings were drilled. The wells were positioned downgradient of Well MW-9 to evaluate the effects of ORC injection. The injection borings were positioned upgradient of Wells MW-9 and MW-4. Well MW-9 also was utilized for groundwater monitoring purposes during the study.



Following injection, Wells T-1, T-2, and Well MW-9 were sampled three times over a five-month period. Sampling events were interspersed with the quarterly groundwater monitoring schedule. During the earlier RA/FS, bio-assessment test data showed that groundwater beneath the Site contained heterotrophic bacteria capable of degrading organic compounds. Test data also showed that groundwater beneath the Site was anaerobic (oxygen-poor) and lacked essential inorganic nutrients (nitrogen and phosphate). However, ORC injection was selected as a remedial alternative for pilot testing assuming if the oxygen, nitrogen, and phosphate concentrations could be increased, then those elements would potentially stimulate and increase bacteriological activity, thus allowing for biodegradation of the petroleum hydrocarbons.

Test results showed that minimal aerobic biodegradation of petroleum hydrocarbons occurred during the pilot study. No significant declines in hydrocarbon concentrations in groundwater were noted. Biodegradation appeared to occur at an extremely slow rate that would be ineffective for reducing chemical concentrations in a timely manner. On this basis, ORC injection would have been conducted over a much longer time interval, and requiring more injection events, than had been anticipated to achieve cleanup goals.

Based on the pilot study outcome, Alternative 3 was not recommended for implementation at the Site. Low permeability soils beneath the Site also would have limited the effectiveness of multiple ORC injection events and would have likely necessitated re-applications of ORC over smaller areas if the quarterly monitoring analytical results continued to show minimal changes of concentrations over time. Furthermore, none of the TPH-impacted source area would be removed during ORC injection. The length of time to meet site-specific cleanup goals was unknown.

3.0 SUBSURFACE CONDITIONS

Previous investigation results show that the Site is underlain by fine-grained soils containing occasional layers of coarse-grained soils. Subsurface conditions beneath the Site are illustrated on cross sections provided in this workplan. The locations of the cross sections are shown on Figure 8. Cross sections A-A' and B-B' are shown on Figure 9.

Uppermost soils beneath the Site generally consist of sandy clay and clayey silt that extend to depths between 4 and 7 feet bgs. Green-colored staining and hydrocarbon odors were encountered within these units at a depth of about 6 feet bgs at some locations. The coarse grained soils consist of sands, silty sands, and clayey sands that are discontinuous in extent. The sands are present at depths between 4 and 7 feet bgs with thicknesses between 2 and 5.5 feet. The sands are further underlain by silty clay and clayey silt units, which were noted to extend to the termination depths in most borings drilled during previous investigations except for Wells MW-7 and MW-13. Clayey sand was encountered at 14 feet bgs in Boring MW-13 and silty gravel was encountered at 18.5 feet bgs in Boring MW-7. No separate phase hydrocarbon product has been encountered in borings advanced at the Site.

Fill soils were encountered in Borings B-9, B-10, and MW-1, along East 7th Street; this occurs as backfill material for a trench containing the sanitary sewer line. The fill consists of sandy clay with gravel and extends to approximately 8 feet bgs. The sandy clay is underlain by an approximately one-foot thick layer of saturated sand that appears to cover the sanitary sewer line.



Quarterly groundwater monitoring events have shown the depth to groundwater varying between approximately 6 and 9 feet bgs. Fine-grained soils beneath the Site exhibit low permeability. Slow recharge has been noted in borings advanced at the Site, especially while attempting to obtain grab groundwater samples. Monitoring wells also have exhibited slow recharge characteristics, where the monitoring wells have been bailed dry upon removal of a few well casing volumes of water. The thickness of unsaturated vadose zone soils (clayey silt and sandy clay soils) beneath the Site is also limited due to the presence of shallow groundwater. Because of fluctuating groundwater levels, a hydrocarbon "smear zone" appears to be present at depths between approximately 5 and 9 feet bgs.

4.0 SCOPE OF WORK

The scope of work for this investigation is designed to meet objectives presented in Section 1.0 of this Workplan. The scope of work includes drilling and sampling of nineteen (19) borings (SV-1 through SV-3, SVGW-1 through SVGW-4, and B-11 through B-22) for soil vapor, soil, and grab-groundwater sampling purposes, followed by laboratory analyses. Borings SV-1 through SV-3 will be advanced inside the Site building for soil vapor sampling purposes. SVGW-1 through SVGW-4 will be advanced inside the Par-A-Dice Custom tenant space for soil vapor and grab groundwater sampling purposes. Boring B-11 will be advanced inside the Par-A-Dice tenant space to log stratigraphic conditions and define the lateral and vertical extent of a coarse-grained soil zone that was encountered in the bottom of Boring MW-13, located downgradient of the Site. Borings B-12 through B-22 will advanced within the undeveloped land and Mor-Drop facility for soil vapor, soil, and grab-groundwater sampling purposes. Pre-field and field activities are described in the following sections.

4.1 PRE-FIELD ACTIVITIES

4.1.1 Property Access

The borings for this investigation will be advanced inside the Site building, the undeveloped land, and the Mor-Drop facility, as shown on Figure 10. Arrangements for accessing the tenant spaces, undeveloped land, and Mor-Drop facility will be coordinated with the property owners in advance of field activities.

4.1.2 **Permitting**

Permits for the soil vapor/grab groundwater sampling points will be obtained from Alameda County Public Works Agency. Field activities will commence upon receipt of the permits.

4.1.3 Health and Safety Plan

A Health and Safety Plan (HASP) will be prepared for the Site based upon results of previous investigations. The HASP will provide information on the work to be performed, safety precautions, emergency response procedures, nearest hospital information, and on-site personnel responsible for managing emergency situations.

Bureau Veritas will perform the investigation in accordance with the requirements of the State of California General Industry Safety Order 5192 and Title 29 of the Code of Federal Regulations, Section 1910.120 (29 CFR 1910.120). Prior to starting field activities, Bureau Veritas also will conduct "tailgate" safety meetings with field personnel and subcontractors, which will include discussions of the safety



hazards and precautionary measures to be implemented during the course of the field activities. Tailgate safety meetings will be performed on a regular basis, as necessary. A copy of the HASP will be kept onsite during field activities.

During field activities, field personnel will don modified Level D health and safety gear, consisting of gloves, safety glasses, steel-toed boots, and hardhats for protection from overhead drilling equipment. On-site health and safety issues will be the responsibility of the Bureau Veritas Project Manager and Site Health and Safety Officer.

4.1.4 <u>Utility Clearance</u>

Boring locations will be marked with white paint prior to contacting Underground Services Alert (USA). Upon contact, USA will notify local utility companies regarding the upcoming exploration work, who, in turn, will mark the locations of their utilities around designated investigation areas, as appropriate and where accessible. Following the USA clearance, an experienced underground utility locator will be retained by Bureau Veritas to perform a detailed utility clearance to confirm marked underground utility locations, as well as check for the presence of other underground utilities not already marked. Boring locations will be shifted accordingly if underground utilities are found to be located directly beneath or in close proximity to the boring locations.

4.2 FIELD ACTIVITIES

Drilling for the borings will be performed by a qualified, experienced, C-57 licensed drilling company under subcontract to Bureau Veritas. Depending upon the locations, drilling will be accomplished with a limited access or truck-mounted drilling rig using direct push methods. Drilling for Boring B-11 will be accomplished using the same drilling methods with the exception of utilizing dual tube casing for preventing cross contamination from water-bearing zone to another during grab-groundwater sampling. Drilling operations will be supervised by an experienced Bureau Veritas field scientist or geologist under the oversight of a Bureau Veritas California-licensed Certified Engineering Geologist.

The borings will be advanced to depths between 10 and 15 feet bgs except for Boring B-11, which is anticipated to be advanced to a depth of approximately 35 feet bgs. The borings will be continuously cored throughout their entire depths for purposes of lithologic logging and field screening purposes, as well as for soil vapor, soil, and grab-groundwater sample collection. Soils will be retained in acrylic liners lining the inside of the core barrel during each sample drive for selection of samples for laboratory analyses, lithologic logging, and field screening. Recovered soil cores will be examined for soil classification and described on detailed boring logs in general conformance with the Unified Soil Classification System. Additional lithologic descriptions and drilling information, such as physical features, sample recovery, discoloration, odor, etc., will be recorded on the boring logs. Upon completion of drilling, the borings will be backfilled with a bentonite grout.

4.2.1 Soil Vapor Sampling

Soil vapor samples will be collected from each of the borings (SV-1 through SV-3, SVGW-1 through SVGW-4, and B-12 through B-22) in an attempt to locate the source area(s) of VOCs and to evaluate potential vapor intrusion into the existing building at the Site except for Boring B-11. Temporary, nested soil vapor sampling points will be installed at each location for sample collection. Proposed soil vapor



borings will be spatially positioned across the Site, as shown on Figure 10. Soil vapor sampling activities during this investigation will be performed in accordance with the California Department of Toxic Substances Control (DTSC) and RWQCB *Advisory – Active Soil Gas Investigation* guidance dated January 28, 2003.

4.2.1.1. Temporary, Nested Soil Vapor Sampling Point Construction

The borings will be advanced for construction of temporary soil vapor points, which will be installed at a depth of 4 feet. Upon reaching the borehole bottom at each location, the construction of each sampling point will begin by placing approximately 6 inches of clean, dry sand in the borehole bottom along with a temporary soil vapor probe attached to an approximate 5-foot length of inert tubing, both extending to the borehole bottom. After the tubing is set in place, an additional 6 inches of clean, dry sand will be added above the tip of the tubing. Above the sand layer, the borehole annulus will be filled with approximately one foot of dry granular bentonite and then filled with hydrated bentonite chips to grade.

4.2.1.2. Soil Vapor Sample Collection

After an adequate amount of time has been allotted for first soil vapor sampling point to equilibrate, a purge test will be performed to determine the optimal purge volume to be applied to each soil vapor sampling location. The purge test will consist of collecting soil vapor samples from first sample point at one (1), three (3), and seven (7) purge volumes. Sampling apparatus at the ground surface will consist of a combination of inert tubing, Teflon tape, gas-tight syringes, and stainless steel and brass fittings, as necessary. Leak tests also will be conducted at each sampling point using an appropriate chemical compound to determine if leakage is occurring through the sampling apparatus during sample collection. The soil vapor samples will be retained in gas-tight syringes.

Upon retrieval of the soil vapor samples, the syringes will be labeled with appropriate project information, including the project name, project number, sample location and depth, date of sampling, and sampler's name. Chain-of-custody documentation will be completed and accompany the soil vapor samples to the analytical laboratory. The soil vapor samples will be analyzed by a State of California-certified mobile analytical laboratory that will be stationed onsite during sampling activities. The samples will be analyzed for VOCs using EPA Method 8260B. Duplicate soil vapor samples will be obtained during the survey at the rate of one (1) sample per each field day.

Upon completion of soil vapor sampling, the inert tubing will be removed from the borehole. Bentonite seals will be left in the boreholes until re-drilled for soil and/or grab-groundwater sampling purposes.

4.2.2 Soil Sampling

Soil samples will be obtained from the vadose zone in Borings B-12 through B-22 to assess for the presence of VOCs. One (1) soil sample will be obtained from the vadose zone in each boring at about the 5-foot depth for laboratory analyses. Selected sample depths for the laboratory analyses may be modified during field activities, and will be dependent upon drilling conditions and the depth to groundwater. A total of eleven (11) soil samples will be submitted for laboratory analyses.

The soil samples will be retained in acrylic liners lining the inside of the core barrel during each sample drive. After the core barrel is retrieved, the acrylic liner will be examined and cut for selecting and



retaining samples for laboratory analyses. Samples to be submitted for laboratory analyses will be retained using EPA Method 5035 protocol (Encore sampling devices).

After the samples are retrieved from the core barrel and the acrylic liners are examined and cut, the ends of the acrylic tubes will be covered with Teflon tape and sealed with airtight plastic caps. The acrylic tubes will then be labeled with the project name, project number, boring number, sample depth, sampling date/time of sampling, and sampler's initials. The tubes will be placed on crushed ice inside an insulated, pre-chilled cooler for transport to the analytical laboratory. Chain-of-custody (COC) documentation will be completed and accompany the soil samples to the analytical laboratory.

4.2.2.1. Field Screening

Soil samples from each sampling interval in the vadose zone will be retained for headspace testing. Headspace tests will be performed with a photo-ionization detector (PID) for detecting the presence of VOCs. To initiate the headspace testing procedure, soil samples will be removed from the acrylic liners inside the core barrel, placed into labeled plastic bags, and sealed for conducting the tests. After sufficient time has elapsed for vapor build-up inside the bags, the bags will be punctured with the probe tip of the PID to allow for measurement of the headspace. Measurements will be obtained in the parts per million (ppm) range for total VOCs. Results of the headspace tests (PID readings) will be recorded on the boring logs.

4.2.3 Grab-Groundwater Sampling

Upon completion of the soil vapor and/or soil sampling activities, the borings (SVGW-1 through SVGW-4 and B-12 through B-22) will then be advanced into the uppermost water-bearing zone beneath the Site for grab-groundwater sampling purposes. Based upon our knowledge of the site-specific subsurface conditions at the Site, it is anticipated that the borings will be advanced to depths approximately between 10 and 15 feet bgs.

To initiate grab-groundwater sampling, the core barrel from the drilling rig will be pulled a few feet upward to allow for installation of one-inch-diameter PVC casing, which will serve as temporary well casing. The casing will be inserted to the borehole bottom. The lower five feet of the casing will be slotted to allow the introduction of water into the casing.

Sufficient time will be allowed for groundwater to enter the screen for collection of a grab-groundwater sample. Prior to sample collection, the groundwater level will be measured and recorded on the boring log. Grab groundwater samples will be obtained from the temporary well casings using a pre-cleaned, stainless steel bailer or plastic bailer. Upon collection, the samples will be poured from the bailer into appropriate laboratory-supplied containers. The sample containers will be capped/sealed, labeled with identifying project information, and placed into a pre-chilled ice chest for transportation to the analytical laboratory. Chain of custody documentation will accompany the groundwater samples to the laboratory.

Upon sample collection, the temporary well casings will be removed and the borings will be backfilled with either a bentonite grout or neat cement grout in accordance with ACPWA permitting requirements.



4.2.4 Decontamination and Waste Containerization

Drilling and sampling equipment will be steam cleaned or cleaned with a non-phosphate solution prior to drilling each boring. Decontamination of the drilling equipment will be performed at a designated self-contained onsite area. Decontamination wastewater will be pumped from the driller's self-contained unit into Department of Transportation (DOT)-approved 55-gallon waste drums. Soil cuttings generated during drilling activities also will be placed into DOT-approved 55-gallon waste drums. Disposable health and safety gear, if any, worn during field activities also will be placed into 55-gallon waste drums.

The drums will be temporarily stored onsite. Disposition of the waste(s) will be determined upon receipt of the laboratory analytical data.

5.0 LABORATORY ANALYSES

Soil vapor and grab-groundwater samples will be analyzed by State of California-certified analytical laboratories. Soil vapor samples will be analyzed by a mobile analytical laboratory. Grab-groundwater samples will be analyzed by a fixed analytical laboratory. The samples will be analyzed for TPH-g and BTEX using EPA Method 8021B and for VOCs using EPA Method 8260B. Laboratory analyses will be performed over a standard turnaround time of between 5 and 10 business days.

6.0 REPORT PREPARATION

Upon completion of the field activities and receipt of the laboratory analytical data, Bureau Veritas will prepare a technical report, which will include a description of the site conditions, summary of investigative methodologies, analytical results, findings, conclusions, and recommendations. The report also will include tables showing the laboratory analytical results for the various media, figures showing the boring locations and distribution of laboratory analytical results for various media, and appendices for the drilling permits, boring logs, chain-of-custody documentation, and certified analytical results.

7.0 PROJECT SCHEDULE

Pre-field activities for this investigation will commence upon the ACEH's written approval of this workplan. It is anticipated that the pre-field activities through the report preparation phase may take between six and eight weeks to complete. Scheduling of the pre-field field activities through report preparation will be contingent upon arrangement of access into tenant spaces and off-site areas, receipt of drilling permits, subcontractor availability, and receipt of laboratory analyses.



This workplan prepared by:

Twicky & Bother



Timothy G. Bodkin, C.E.G., R.E.A. II

Senior Project Manager

Health, Safety, and Environmental Services

This workplan reviewed by:

Jon A. Rosso, P.E.

Regional Director Health, Safety, and Environmental Services

February 25, 2009

Project No. 33104-004578.00

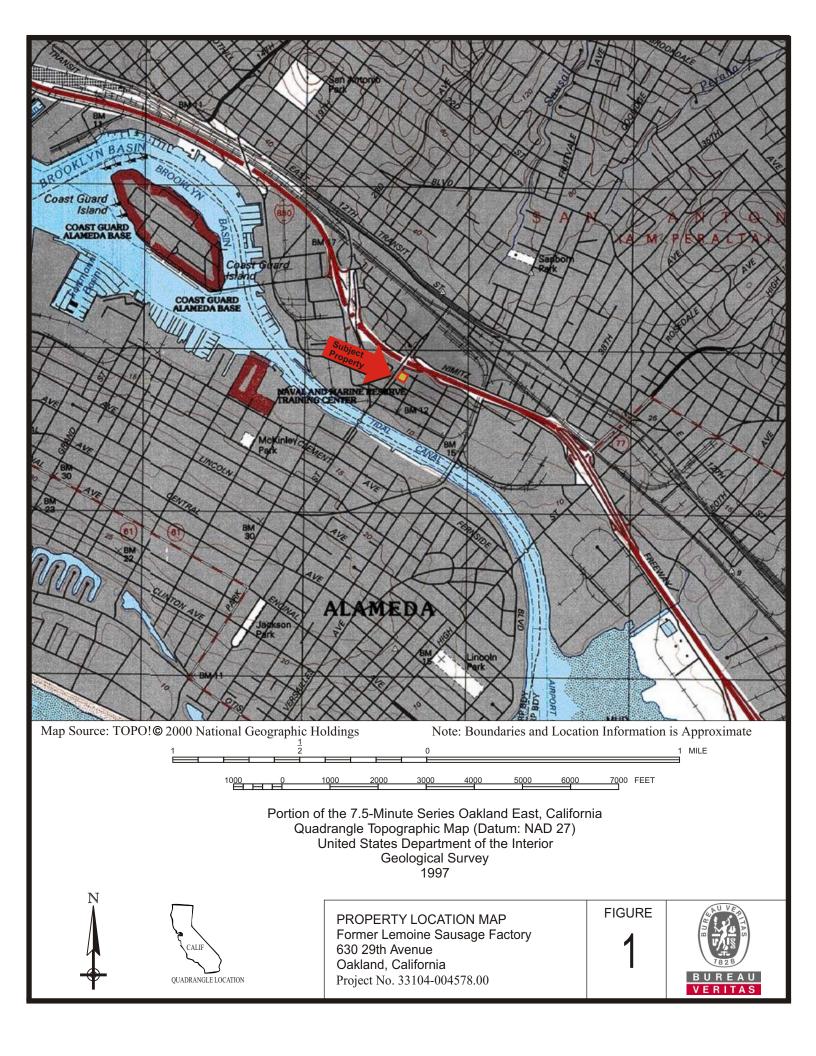


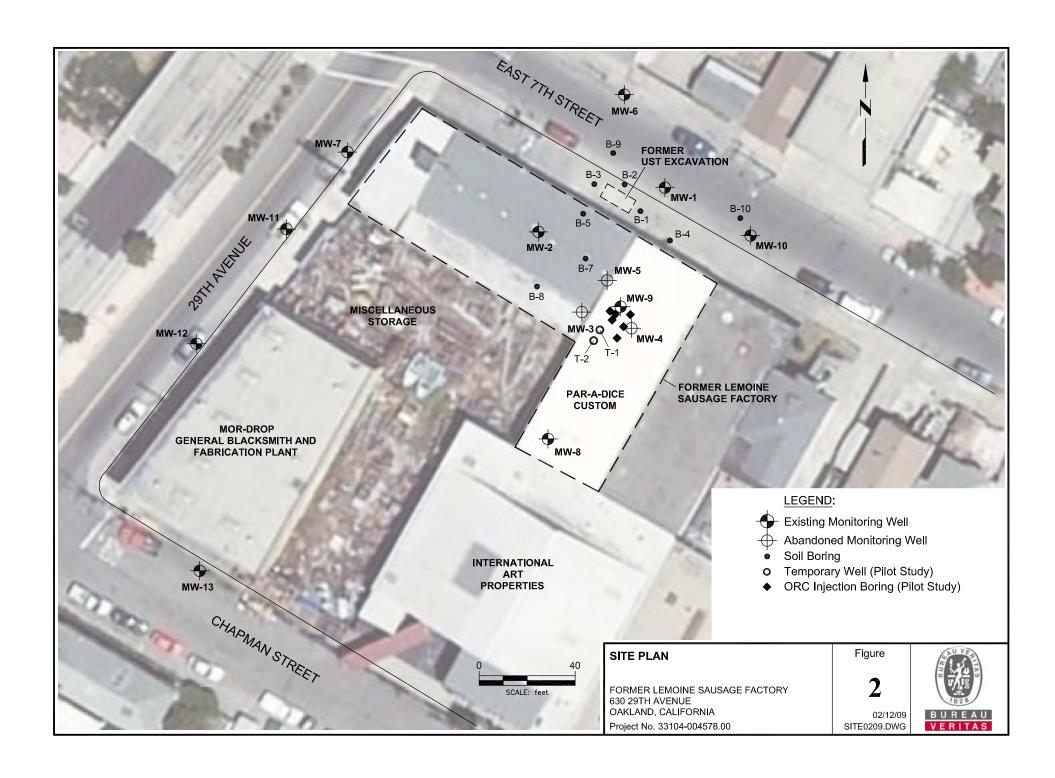
8.0 REFERENCES

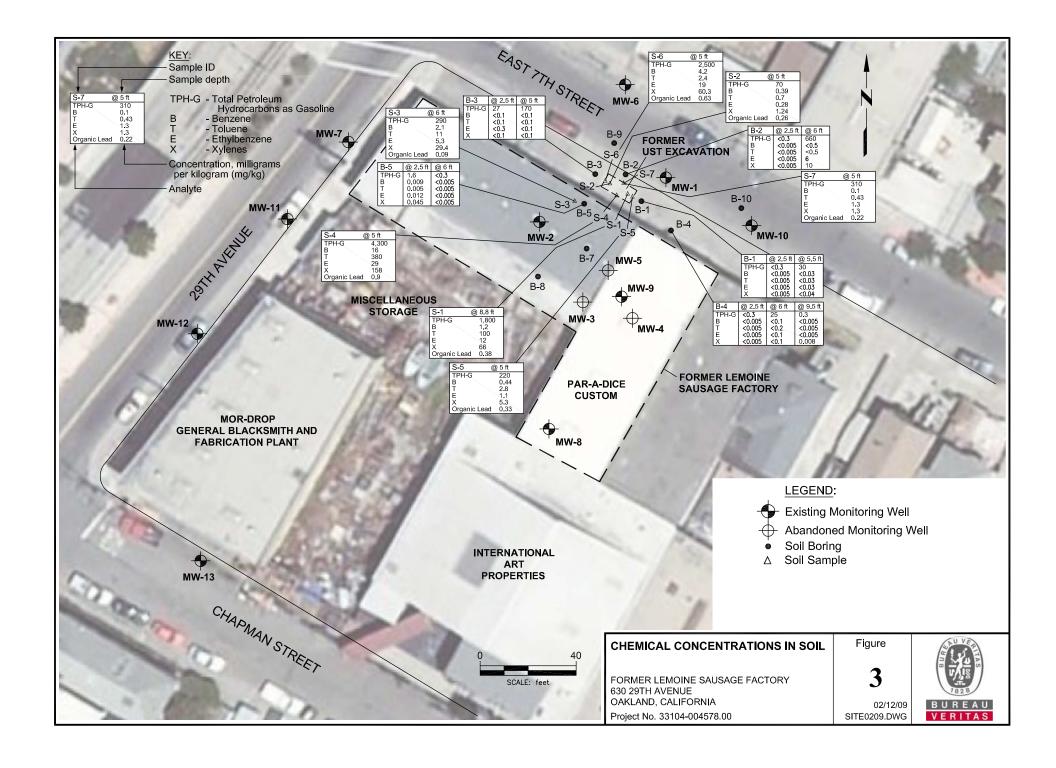
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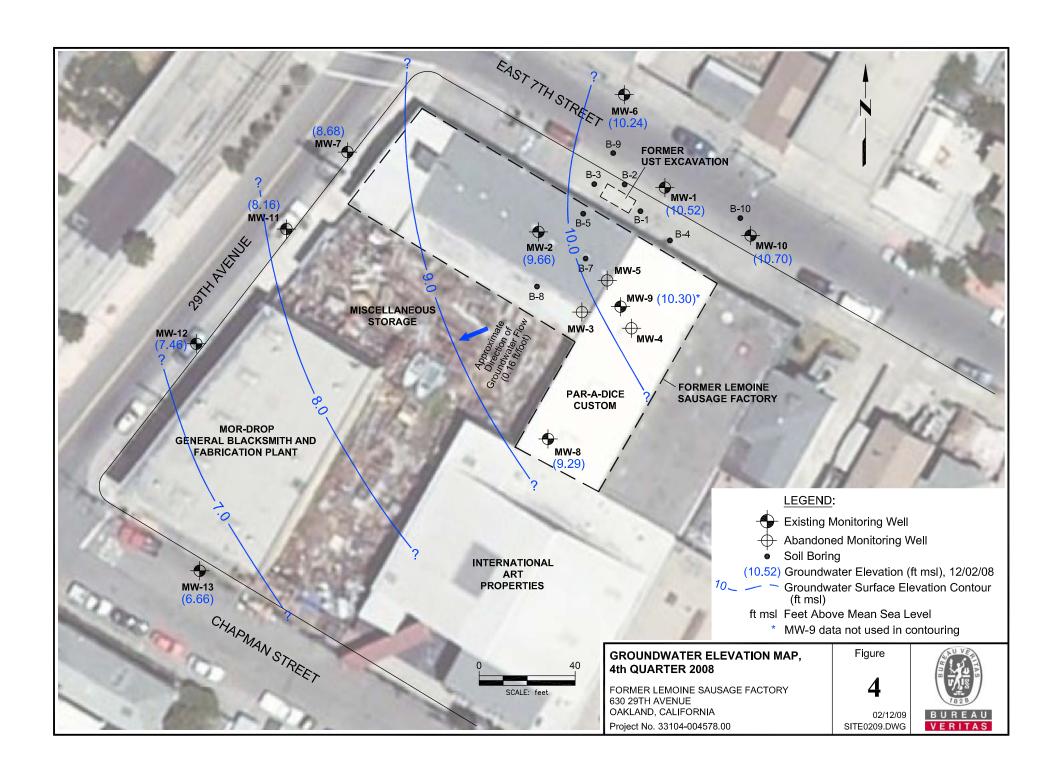


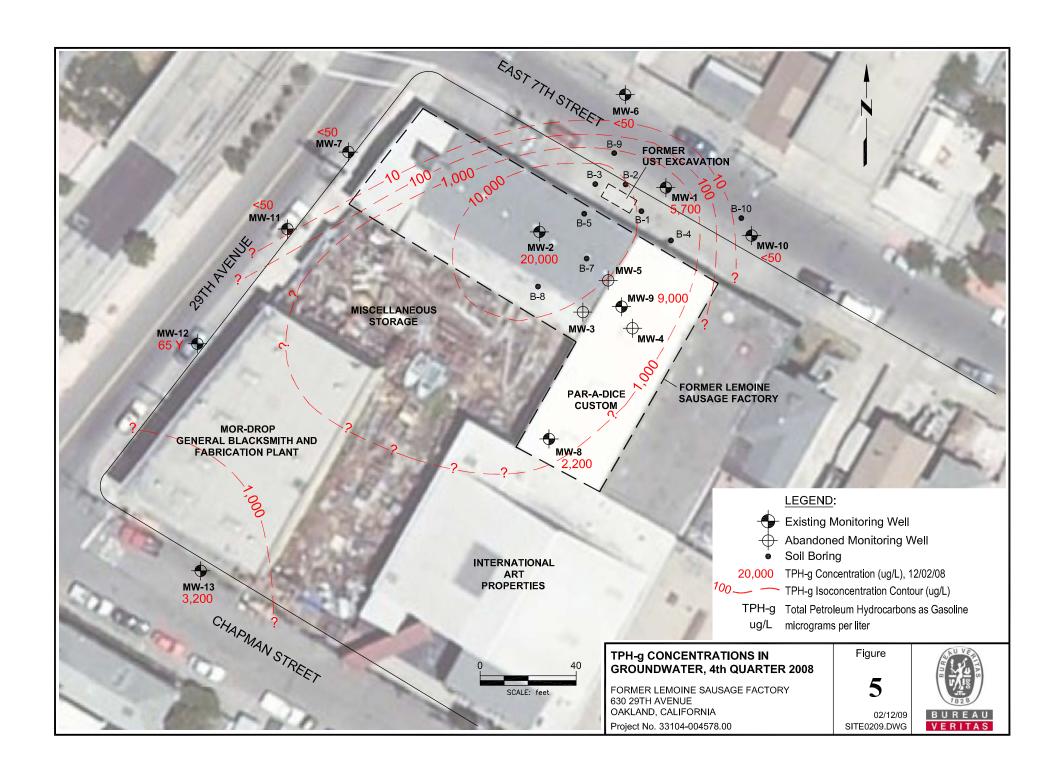
FIGURES

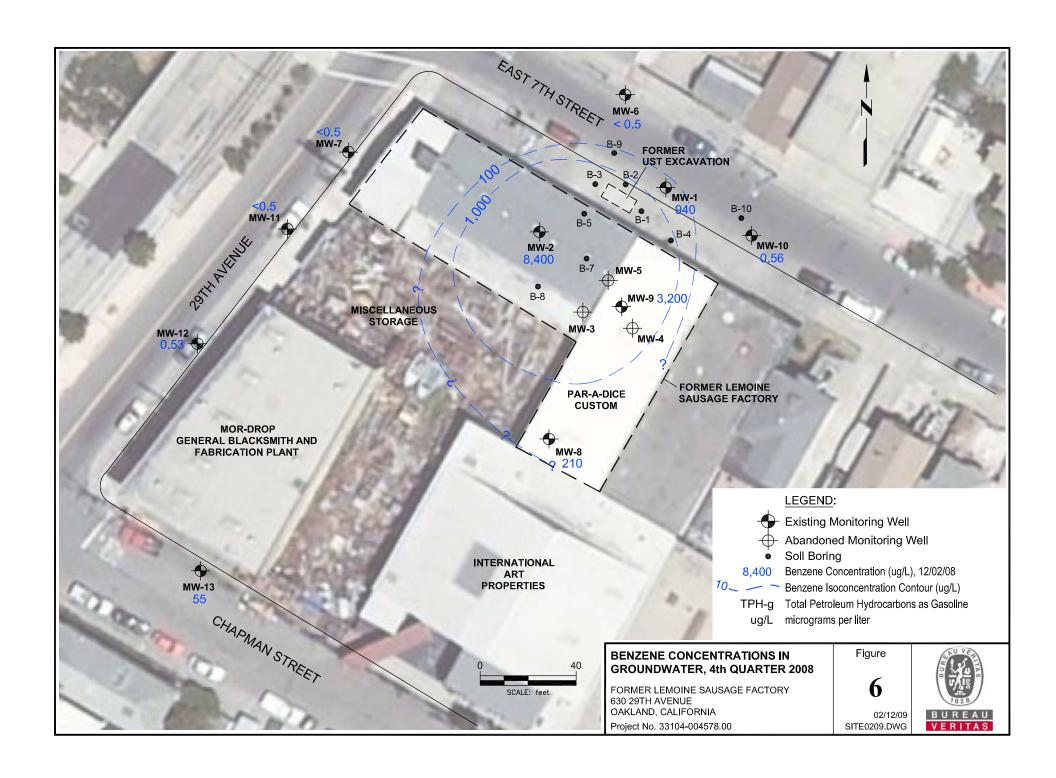


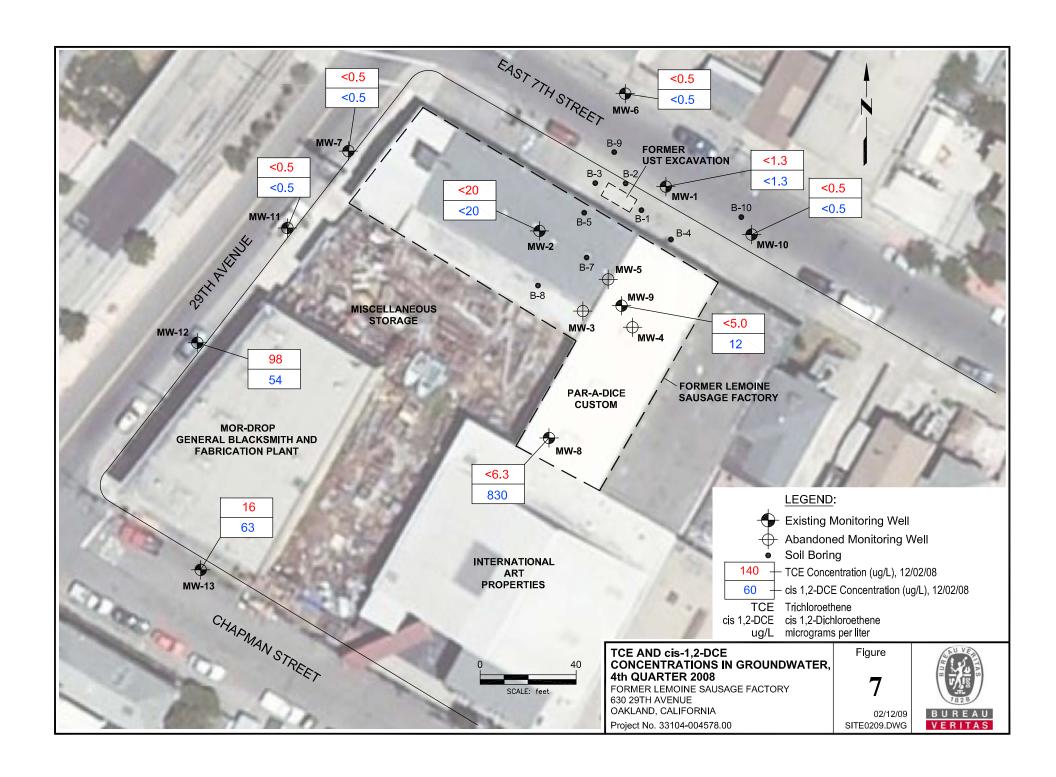


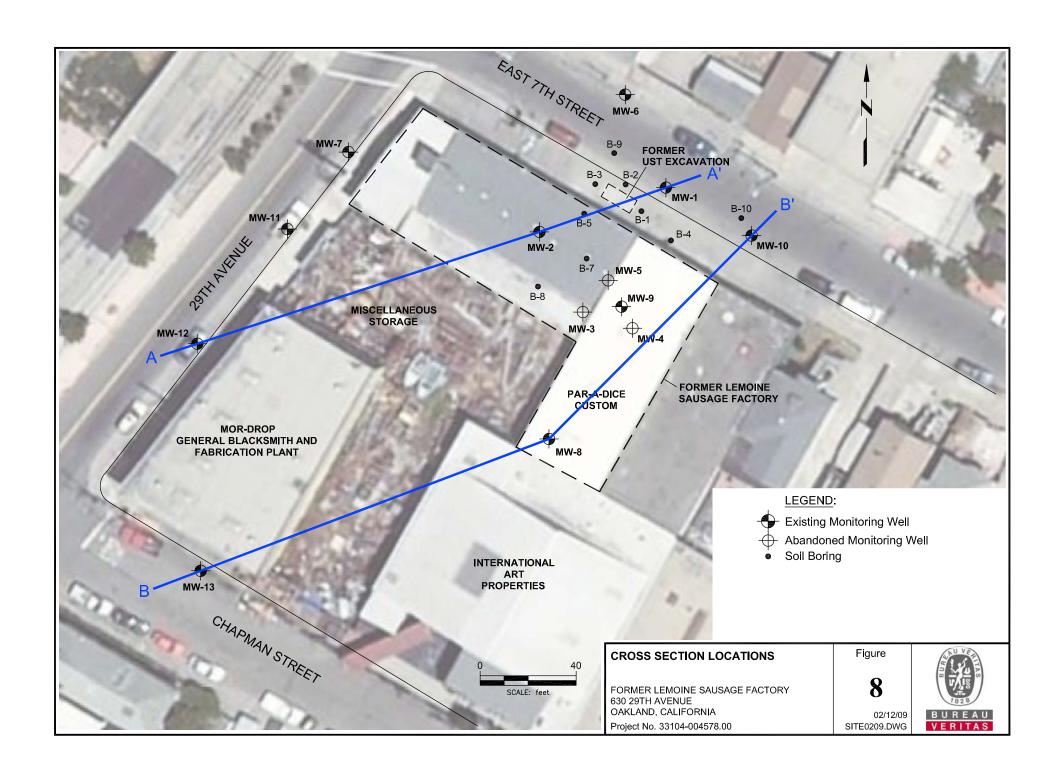


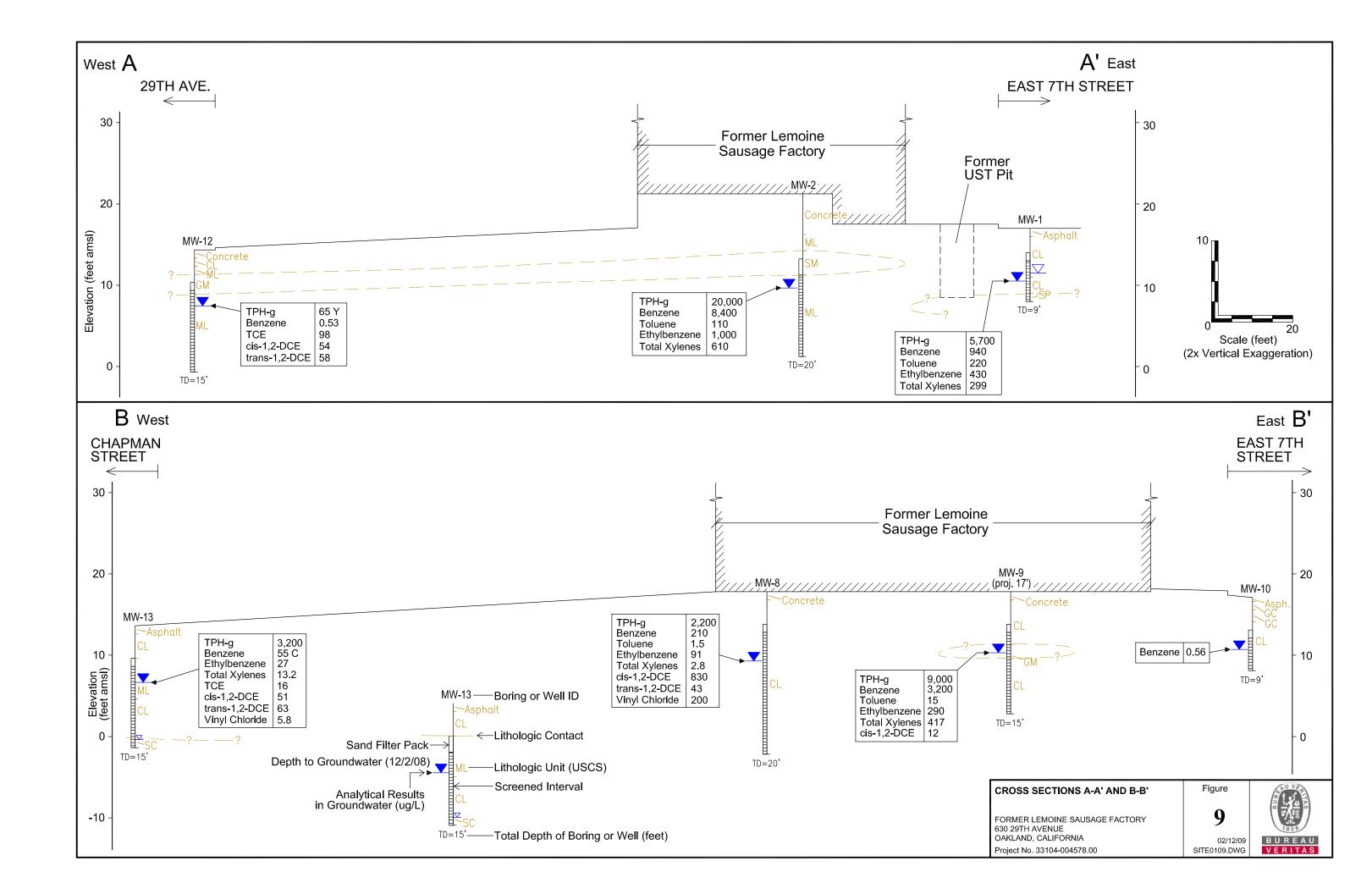


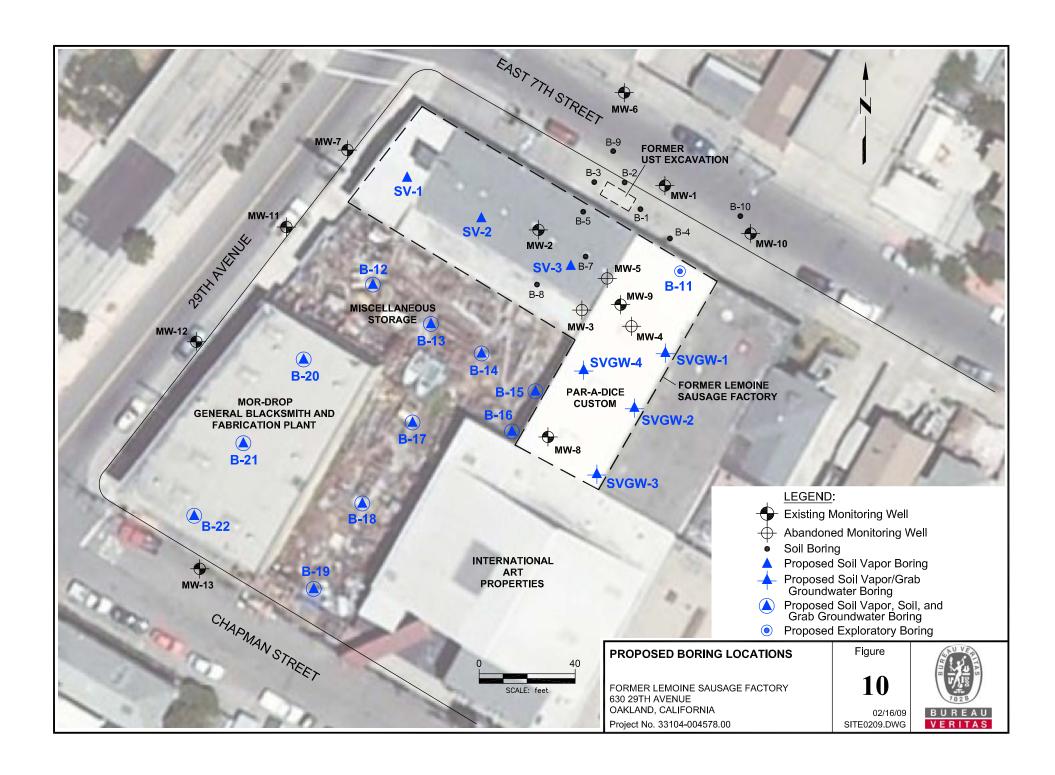














APPENDIX A BORING LOGS AND MONITORING WELL CONSTRUCTION DETAILS

| | | Cla | yto | on | LOG OF BORING B-7 | | | | | | |
|--|--|-----------|---------|---|---|---|---------------|----------------------|-------------------------|--|--|
| | Envi | ronmen | tal Co | nsultants | | | (Page 1 of 1) | | | | |
| SITE INVESTIGATION FORMER LEMOINE SAUSAGE FACTORY 630 29TH AVENUE OAKLAND, CALIFORNIA Clayton Project No.: 70-97066.00 | | | | | Date Started Date Completed Hole Diameter Drilling Method Sampling Method | : 1-27-99 : 1-27-99 : 2 in. : Geoprobe | | Driller Logged By | : Vironex : M. Hanko | | |
| Depth in Feet | Surf. Elev. 18 | nscs | GRAPHIC | | DESCRIPTION | | | | • | | |
| 4 | - 18 - 13 | СС | - | CONCRETE Floo | | | | | | | |
| , The state of the | And the second s | ML SM | | medium stiff, sligh | (0,0,70,30), dark gra tly moist, plastic with gravel (5,60,30,5 , angular 1/4" gravel, | | | | , | | |
| 10 | e de la companya de l | ML | | Clayey SILT (ML) medium stiff, sligh | (0,0,70,30), dark gra tly moist, plastic, HC | y (10YR 3/1), odor in soil | | | | | |
| 20 - Notes: A | rbitrary su | uriace da | tum se | at at 18 feet. | · | | | | | TOTAL CONTRACTOR CONTR | |
| | | | | | | | | | | | |

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| | | Cla | | | LOG OF BORING B-8 | | | | | | | |
|--|--|-----------|---------|--|---|---|--|----------------------|-------------------------|--|--|--|
| | Envi | ronment | al Co | nsultants | | | | | (Page 1 of 1) | | | |
| SITE INVESTIGATION FORMER LEMOINE SAUSAGE FACTORY 630 29TH AVENUE OAKLAND, CALIFORNIA Clayton Project No.: 70-97066.00 | | | | SAGE FACTORY NUE FORNIA | Date Started Date Completed Hole Diameter Drilling Method Sampling Method | : 1-27-99 : 1-27-99 : 2 in. : Geoprobe | | Driller Logged By | : Vironex : M. Hanko | ······································ | | |
| Depth in Feet | Surf. Elev. 18 | nscs | GRAPHIC | | DESCRIPTION | ı | | , | | | | |
| 0 - | - 18 | | | CONCRETE Floo | r | | <u>-</u> | | | | | |
| | | СС | | | | - | | | | | | |
| 5 - | - 13 | ML | | Clayey SILT (ML) medium stiff, sligh | (0,0,70,30), dark gr atly moist, plastic | ay (10YR 3/1), | 100 mm m m m m m m m m m m m m m m m m m | | | | | |
| - | | ML | | Sandy SILT (ML) 4/2), slightly moisi | (0,20,60,20), grayis t, stiff | ħ brown (10YR | | | | | | |
| 10 - | - 8 | CL | | Silty CLAY (CL) (C 4/3), very stiff, slig | 0,25,35,40), yellowis yhtly moist | h brown (10YR | | | | | | |
| 15 | - 3 | | | | | | | | | | | |
| 1 | A provide management | | | | | | | | | ; | | |
| - | ************************************** | | | | | | | | | | | |
| 20 - | | | | | | | | | | | | |
| Notes: A | arbitrary s | urface da | itum s | et a t 18 feet. | | | | | | | | |

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| | Envi | Cla | al Co | nsultants | LOG OF BORING B-9 | | | | | | |
|------------|--|----------------------|---------------------|---------------------------------------|---|--|--|----------------------|-------------------------|--|--|
| | | | | · | | | | | (Page 1 of 1) | | |
| | MER LE 63 OAH | 30 29TH KLAND, | SAU: AVE CALI | SAGE FACTORY | Date Started Date Completed Hole Diameter Drilling Method Sampling Method | : 1-28-99 : 1-28-99 : 2 in. : Geoprobe : | | Driller .ogged By | : Vironex : M. Hanko | | |
| Depth | Surf. | | HIC | | | | interior and the second se | - | | | |
| in Feet | Elev. 18 | nscs | GRAPHIC | | DESCRIPTION | N | | | | | |
| 0 - | - 18 | AS/FL | | Asphalt and Base | | | | | | | |
| - | | | | Sandy CLAY (CL) (10YR 4/2), very s | with gravel (10,30, stiff, <1/4" angular g | 25,35), dark brown ravel | | | | | |
| - | | CL Static water at 3 | | | feet bgs | | | | | | |
| 5 | - 13 | | | | ens at 5.5-6.0 feet b | - | | | | | |
| | | CL | // | (10YR 3/1), very s | rith gravel (10,10,35 stiff,1-inch gravel, st | rong HC odor | | | | | |
| | | SP | | stiff, saturated, str | 0,0,0), dark gray (10 rong HC odor | JYR 3/1), very | | | | | |
| 10 | - 8 | | | Refusal at 9 feet b | | | | | | | |
| | | | | • | | | | | | | |
| 1 | | | | | | | | | | | |
| | | | | | | | | | | | |
| 15 | 3 | | | | | | | | | | |
| _ | ************************************** | | | | | | | | | | |
| | | | | | | | | | | | |
| | | | | | | · | | | | | |
| 20 - | rbitrary s | | | ··· | | | | | | | |

Clayton LOG OF BORING B-10 **Environmental Consultants** (Page 1 of 1) SITE INVESTIGATION Date Started : 1-28-99 Driller : Vironex FORMER LEMOINE SAUSAGE FACTORY Date Completed : 1-28-99 Logged By : M. Hanko 630 29TH AVENUE Hole Diameter : 2 in. OAKLAND, CALIFORNIA Drilling Method : Geoprobe Clayton Project No.: 70-97066.00 Sampling Method GRAPHIC Depth Surf. nscs Elev. DESCRIPTION Feet 18 0 + 18 Asphalt and Base Material AS/FL Sandy CLAY (CL) with gravel (10,30,25,35), dark brown (10YR 4/2), very stiff, <1/4" angular gravel CL Static water at 3.6 feet bgs 5 + 13 saturated gravel lens at 5.5-6.0 feet bgs Silty CLAY (CL) with gravel (10,10,35,45), dark gray (10YR 3/1), very stiff,1-inch gravel, strong HC odor CL SAND (SP) (0,100,0,0), dark gray (10YR 3/1), very stiff, saturated, strong HC odor SP Refusal at 9 feet bgs due to sanitary sewer pipeline. 10 15 \ 3 Notes: Arbitrary surface datum set at 18 feet.

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03-03-1999

Clayton LOG OF BORING MW_1 Environmental Consultants (Page 1 of 1) SITE INVESTIGATION Date Started : 1-28-99 Driller : Viranex FORMER LEMOINE SAUSAGE FACTORY Date Completed ; 1-28-99 Logged By : M. Hanko 630 29TH AVENUE Hole Diameter : 2 in. Surface (Rim) Elevation 16.99 ft.msl OAKLAND, CALIFORNIA **Drilling Method** : Geoprobe Top of Well Casing : 16.69 ft.msl Clayton Project No.: 70-97066.00 Sampling Method Survey By : V. Chavez Well1: MW-1 GRAPHIC Elev.: 16.99 Depth Surf. Elev. USCS DESCRIPTION in Feet 16.99 Cover 0 -Asphalt and Base Material AS/FL Neat Cement 16 Sandy CLAY (CL) with gravel (10,30,25,35), dark brown (10YR 4/2), very stiff, <1/4" angular gravel, saturated gravel lens at 5.5-6.0 feet bgs Blank Bentonite CL 5 #3 Sand 11 3/4-inch Pre-Packed Silty CLAY (CL) with gravel (10,10,35,45), dark gray (10YR 3/1), very stiff,1-inch gravel, strong HC odor 0.020" Slotted CL Screen SAND (SP) (0,100,0,0), dark gray (10YR 3/1), loose, SP saturated, strong HC odor Refusal at 9 feet bgs due to concrete. 10 15 C:\u10ch5\p97066\97066\mv1.bor 20 Notes: 03-03-1999

Clayton LOG OF BORING MW_2 Environmental Consultants (Page 1 of 1) SITE INVESTIGATION Date Started : 1-27-99 Driller : Vironex FORMER LEMOINE SAUSAGE FACTORY Date Completed : 1-27-99 Logged By : M. Hanko 630 29TH AVENUE Hole Diameter : 2 in. Surface (Rim) Elevation 21.24 ft,msl OAKLAND, CALIFORNIA Top of Well Casing Drilling Method : Geoprobe : 20.79 ft.msl Clayton Project No.: 70-97066.00 Sampling Method Survey By : V. Chavez Well1: MW-2 GRAPHIC Elev.: 21.24 Depth Surf. Elev. DESCRIPTION in Feet 21.24 Cover 0 -21 Suspended Slab, various layers of concrete slabs, wood slabs, steel slabs, and rubble CC Neat Cement Blank 5 16 Clayey SILT (ML) (0,0,70,30), dark gray (10YR 3/1), medium stiff, slightly moist, plastic ML Silty SAND (SM) with gravel (5,60,30,5), brown (10YR 5/3), moist, dense, angular 1/4" gravel, fine sand Bentonite SM 10 Clayey SILT (ML) (0,0,70,30), dark gray (10YR 3/1), medium stiff, slightly moist, plastic 11 #3 Sand 3/4-inch Pre-Packed 15 ML 0.020" Slotted 6 Screen C:\rntech5\p97066\97066mv2.txor Notes: Petroleum odor @13' bgs, retained sample @ 13'.

03-04-1999

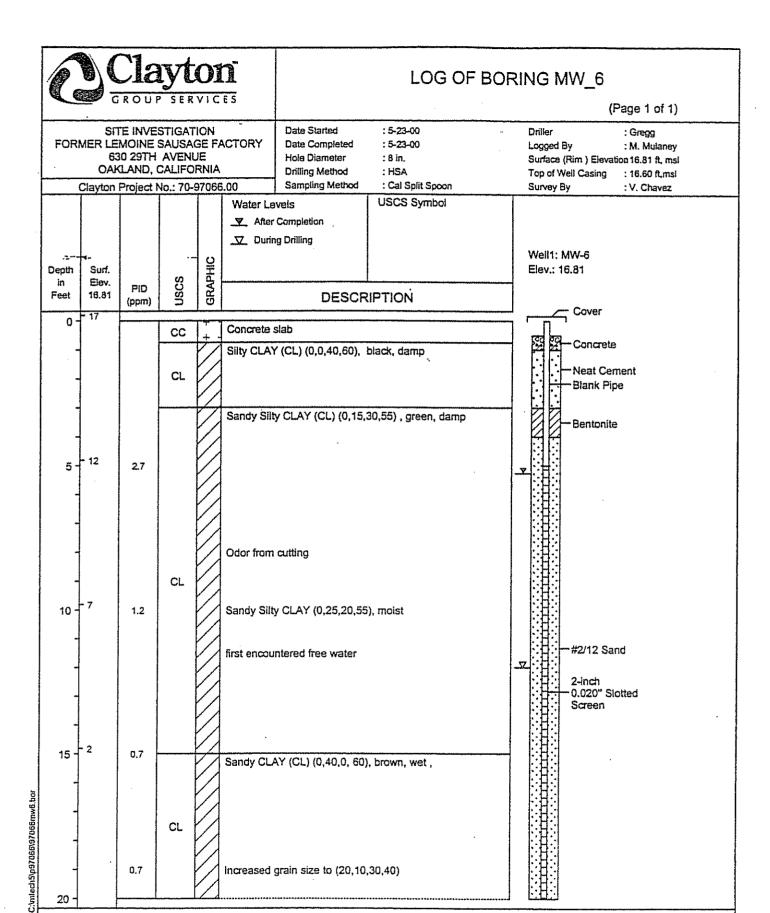
| Env | Clayto | | LOG OF BORING MW_3 | | | | |
|---------------------------------------|--|--|---|--|--|--|--|
| FORMER LE 6 OA | TE INVESTIO MOINE SAU 30 29TH AVI (LAND, CALI Project No.: | SAGE FACTORY ENUE FORNIA | Date Started Date Completed Hole Diameter Drilling Method Sampling Method | : 1-27-99 : 1-27-99 : 2 in. : Geoprobe : | (Page 1 of 1) Driller : Vironex Logged By : M. Hanko Surface (Rim) Elevation 21.30 ft.msl Top of Well Casing : 21.10 ft.msl Survey By : V. Chavez | | |
| Depth Surf. in Elev. Feet 21.30 | USCS | THE CONTRACT OF THE CONTRACT O | DESCRIPTIO | N | Weil1: MW-3 Elev.: 21.3 | | |
| 0 - 21 | CC | Suspended Slab, slabs, steel slabs, | various layers of co and rubble | oncrete slabs, wood | Cover | | |
| 5 - 16 | ML | medium stiff, sligh | | · | Blank | | |
| 10 - 11 | sc | slightly moist, satu warehouse floor |) with gravel, brown rated at 11.5 - 12.5 | 5 feet below the | — Bentonite | | |
| 15 - 6 | ML . | Slity CLAY (CL) (0 stiff to hard, slight | ,5,45,50), light bro ly moist | wn (10YR5/3), very | #3 Sand 3/4-inch Pre-Packed 0.020" Slotted Screen | | |
| 20 - lotes: | | | | | | | |

| En | Cla | | | LOG OF BORING MW_4 (Page 1 of 1) | | | | |
|--------------------------------------|---|----------------------|--|--|--|--|--|--|
| FORMER L | 330 29TH KLAND, | SAUS AVE CALIF | SAGE FACTORY NUE | Date Started Date Completed Hole Diameter Drilling Method Sampling Method | : 1-28-99 : 1-28-99 : 2 in. : Geoprobe : | Driller : Vironex Logged By : M. Hanko Surface (Rim) Elevation: 17.92 ft.msl Top of Well Casing : 17.78 ft.msl Survey By : V. Chavez | | |
| Depth Surf. in Elev Feet 17.92 | Elev. 있 호 | | DESCRIPTION | | V | Well1: MW-4 Elev.: 17.92 | | |
| 0 - 17 | CC | | medium stiff, sligh | (0,0,70,30), dark gi tly moist, plastic | | Blank Neat Cement Bentonite | | |
| 5 - 12 | SC | | Clayey SAND (SC slightly moist, satu |) with gravel, brown rated at 8.5 - 9.5 fe | (10YR 5/3), et bgs | #3 Sand | | |
| 10 - 7 | CL | | Silty CLAY (CL) (0 stiff to hard, slight | ,5,45,50), light brown ight brown is the second sec | wn (10YR5/3), very | 3/4-inch Pre-Packed 0.020" Slotted Screen | | |
| 15 - 2 | | <u> </u> | | | | | | |
| 20 - Notes: | *************************************** | | | | | | | |

Clayton LOG OF BORING MW_5 **Environmental Consultants** (Page 1 of 1) SITE INVESTIGATION Date Started : 1-27-99 Driller : Vironex FORMER LEMOINE SAUSAGE FACTORY Date Completed : 1-27-99 Logged By : M. Hanko 630 29TH AVENUE Hole Diameter : 2 in. Surface (Rim) Elevation not determined OAKLAND, CALIFORNIA **Drilling Method** : Geoprobe Top of Well Casing : 21.12 ft,msl Clayton Project No.: 70-97066.00 Sampling Method Survey By : V. Chavez Well1: MW-5 GRAPHIC Depth Surf. Elev.: 21.5 **DESCRIPTION** Elev. in Feet 21.5 Cover 0 Suspended Slab, various layers of concrete slabs, wood 21 slabs, steel slabs, and rubble CC Neat Cement Clayey SILT (ML) (0,0,70,30), dark gray (10YR 3/1), Blank medium stiff, slightly moist, plastic 5 16 ML Bentonite Silty SAND (SM) with gravel (5,60,30,5), brown (10YR 5/3), moist, dense, angular1/4" gravel, fine sand SM 10 Clayey SILT (ML) (5,10,50,35), stiff, slightly moist, -#3 Sand 11 very plastic 3/4-inch Pre-Packed 0.020" Slotted Screen ML Borehole collapsed from 16 to 14.5 feet bgs prior to installation of casing. 15 6 Notes: Arbitrary surface datum set at 21.5 feet.

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20 Notes: CL

Increased grain size to (20,10,30,40)

0.7

09-18-2000



LOG OF BORING MW_7

(Page 1 of 1)

| SITE INVESTIGATION |
|--------------------------------|
| FORMER LEMOINE SAUSAGE FACTORY |
| 630 29TH AVENUE |
| OAKLAND, CALIFORNIA |

Date Started Date Completed Hole Diameter

: 5-23-00 : 5-23-00 : 8 in.

Driller : Gregg

Logged By : M. Mulaney Surface (Rim) Elevation 15.67 ft, msl Top of Well Casing : 15.47 ft,msi

Drilling Method : HSA Clayton Project No.: 70-97066.00 Sampling Method : Cal Split Spoon Survey By : V. Chavez USCS Symbol Water Levels ▼ After Completion 19 □ During Drilling Well1: MW-7 GRAPHIC Depth Surf. Elev.: 15.67 USCS Élev. in PID Feet 15.67 DESCRIPTION (ppm) Cover 0 Concrete slab CC Concrete Silty CLAY (CL) (0,0,30,70), black, damp CL Neat Cement Sandy Silty CLAY (CL) (0,10,40,55), green, damp Blank Pipe CL Silty CLAY (CL) (0,0,30,70), black, damp Bentonite CL 5 1.7 Pebbly Sandy Silty CLAY (CL) (20,20,10,50), dark green, Sandy Silty CLAY (CL) (0,20,30,50), brown, damp, carbon, root structures 10 2.7 Sandy CLAY (CL), damp #2/12 Sand CL 2-inch 0.020" Slotted Screen 15 0.7 Sandy Silty CLAY (CL) (0,30,10, 60), brown, damp, root structures, green staining Silty Sandy GRAVEL (GC) (60,30,10, 0), brown, 1.7 saturated

20 Notes:

09-18-2000

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LOG OF BORING MW_8

(Page 1 of 1)

| SITE INVESTIGATION |
|--------------------------------|
| FORMER LEMOINE SAUSAGE FACTORY |
| 630 29TH AVENUE |
| OAKLAND, CALIFORNIA |

Date Started

: 5-23-00

Driller

: Gregg

| | 63 OAK | 30 29TH (LAND, (| AVENI CALIFO | LIFORNIA Drilling Method : HSA | | | | Logged By : M. Mulaney Surface (Rim) Elevation 17.83 ft, msl Top of Weil Casing : 17.58 ft, msl |
|-------------|--|---------------------|--|--------------------------------|----------------------------------|--|--|--|
| Depth in | Surf. Elev. | PID | NSCS SOSU | GRAPHIC | Water Le | vels Completion | : Cal Split Spoon USCS Symbol | Survey By : V. Chavez Well1: MW-8 Elev.: 17.83 |
| Feet | 17.83 - 18 | (ppm) | Sn | 8 | | DESCR | IPTION | Cover |
| 0 - | | | cc | + | Concrete s Pebbly Sar green, moi | ndy Silty CLAY (CL |) (25,10,25,40), black and | Concrete Neat Cement Blank Pipe Bentonite |
| 5 1 1 1 1 | - 13 | 6.1 | | | | | | |
| 10 - | - 8 | 6.6 | CL | | Sandy Silty carbon, ro | CLAY (CL) (0,20,3 ot structures, green | 30,50), brown, moist, 1-2 mm staining | 2-inch 0.020" Slotted Screen |
| 15 - | 3 | 48.4 | The state of the s | | mm carbon | | 5,45), light brown, moist, 1 | |
| 20 - | A CONTRACTOR OF THE PARTY OF TH | | | | | | The state of the s | |

Notes:

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|---------------------|--|---|-----------------------------------|------------------------|------|---|--|--|
| | | undv 630 : Oa | vater Ev 29th Ave ikland, (| raluatio enue CA | on | | Date Started : 10/5/01 Date Completed : 10/5/01 Hole Diameter : 8 in. Drilling Method : H.S.A. Sampling Method : Split Spoon | (Page 1 of 1) Driller : Gregg Drilling Logged By : M. Mullaney Top of Well Casing : 17.61 feet, msl Survey By : V. Chavez |
| Depth in Feet | Surf. Elev. 18 | Blow Count | PID (ppm) | Samples | nscs | GRAPHIC | DESCRIPTION | Well1: MW-9 Elev.: 18 |
| | 18 | минициним при | - VA | | CL | | Concrete Silty CLAY (0,0,35,65), Black, Damp. Gravelly silty CLAY (30,0,30,40), Tan, Damp | 8"-Traffic Rated Well Vault set in Concrete Neat Cement Grout Sch40 Blank Pipe Bentonite |
| - | The state of the s | | 0.6 | \boxtimes | | 100000000000000000000000000000000000000 | Silty Clayey GRAVEL (50, 0, 30, 20) green stain and slight HC odor Gravelly Silty CLAY (20,0, 30,50), Tan, moist, HC odor | #2/16 Sand |
| 10 | 8 | Manual 1970 | 2.1 | | CL. | | sandy silty clay (0,15,20,65), Tan, moist, very fine sand | Screen |
| 15 | 3 | | 15.5 | | | <u> </u> | | Bottom Cap |
| Notes: | - | | | | | | | |

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| C | C | | yto | | | | LOG OF BOF | |
|---------------------|----------------------|--|-----------------------------------|-----------------------|-------|---------|--|--|
| | | und 630 Oa | water Ev 29th Avo akland, (| /aluati enue CA | on | | Date Started : 10/5/01 Date Completed : 10/5/01 Hole Diameter : 8 in. Drilling Method : H.S.A. | (Page 1 of 1) Driller : Gregg Drilling Logged By : M. Multaney Top of Well Casing : 16.92 feet, msl Survey By : V. Chavez |
| (| Clayton | Proji | ect No.: | 70-97 | 066.0 | 10 | Sampling Method : Split Spoon | |
| Depth in Feet | Surf. Elev. 17 | Blow Count | PID (ppm) | Samples | USCS | GRAPHIC | DESCRIPTION | Well1: MW-10 Elev.: 17 Cover |
| 0 | - 17 | | | | GC | | Asphalt and baserock Gravelly Silty CLAY (40,0,20,40), Orange brown, damp | 8"-Traffic Rated Well Vault set in Concrete Neat Cement Grout |
| 5 - | - 12 | ANALYSIA ANA | 0.0 | | CL | | Silty CLAY (0,5,35,65), green, damp Gravelly Silty CLAY (30,0,30,40), tan, damp | Sch40 Blank Pipe Bentonite #2/16 Sand 0.010" Slotted Screen |
| 10 - | 7 | The second secon | | | | | Refusal at 9-feet bgs due to concrete. | |
| 15 - | 2 | | | | | | | |
| 20 - | | | | | | ···· | | |
| 20 - Notes: | | | | | | | | |

| C | | | ytc | | | | LOG OF BOR | LOG OF BORING MW-11 | | | |
|---|--|--|--------------|-----------|------|---------|--|---|--|--|--|
| | *** | | | : | | | | (Page 1 of 1) | | | |
| | Former Lemoine Sausage Factory Groundwater Evaluation 630 29th Avenue Oakland, CA Clayton Project No.: 70-97066.00 | | | | | | Date Started : 10/5/01 Date Completed : 10/5/01 Hole Diameter : 8 in. Drilling Method : H.S.A. Sampling Method : Split Spoon | Driller : Gregg Drilling Logged By : M. Mullaney Top of Well Casing : 14.87 feet, msl Survey By : V. Chavez | | | |
| Depth in Feet | Surf. Elev. 15 | Blow Count | PID (ppm) | Samples | nscs | GRAPHIC | DESCRIPTION | Well1: MW-11 Elev.: 15 Cover | | | |
| 0- | - 15 | | | | GP | | Asphalt and baserock | 8"-Traffic Rated Well Vault set in Concrete Neat Cement | | | |
| - | | | | | GМ | a 0 a | Gravelly SILT (40,0,10,50), Orange brown, damp | Grout Sch40 Blank Pipe Bentonite | | | |
| 5 - | - 10 | | 8.8 | | | | Silty CLAY (0,5,35,65), Tan, Damp. | - Bentonile | | | |
| 10 - | 5 | and the state of t | 0.0 | | CL | | Sandy silty CLAY (0,15,15,70), green/gray, moist | | | | |
| 15 - | 0 | | 0.0 | | | | Silty CLAY (0,5,25,70), Brown, moist | Bottom Cap | | | |
| 5.\erm\tantaning_iags\p01447\rm\-11.bot | | WANDERSTEIN STREET STRE | | | | | | | | | |
| Notes: | 1 | <u> </u> | | - Aldrews | | | | | | | |



LOG OF BORING MW-12

(Page 1 of 1)

Former Lemoine Sausage Factory Groundwater Evaluation 630 29th Avenue Oakland, CA Date Started Date Completed : 5-16-02 : 5-16-02

Logged By Top of Well Casing

Driller

: Gregg Drilling : M. Krzeminski

Hole Diameter Drilling Method : 8 in. : H.S.A.

Survey By

: XX.YY feet, msl : V. Chavez

Sampling Method ; Split Spoon Clayton Project No.: 70-97066.01 Well: MW-12 Samples Elev.: 15 Depth Surf. USCS **DESCRIPTION** Elev. Surface Casing Cover Feet 15 15 8"-Traffic Rated Well Vault set in Concrete Concrete and baserock CC CLAY (0,0,0,100) dark brown, stiff, dry. CL Neat Cement Grout Clayey SILT (0,0,80,20), light brown, stiff, dry ML Sch40 Blank Pipe Silty Clayey GRAVEL (70,0,15,15), orange brown, loose, dry. -Bentonite GM 5 10 Clayey SILT (0,0,90,10) greenish grey, dry. \boxtimes #2/12 Sand light brown 0.010" Slotted Screen trace fine sand 10 ML - 5 moist **Bottom Cap** 15-05-20-2002 s:\es\boring_logs\p97066\kW-12.BOR 20 Notes:



LOG OF BORING MW-13

(Page 1 of 1)

Former Lemoine Sausage Factory Groundwater Evaluation 630 29th Avenue Oakland, CA

Date Started Date Completed Hole Diameter

: 5-16-02 : 5-16-02 : 8 in.

Driller Logged By Top of Well Casing

: Gregg Drilling : M, Krzeminski : XX,YY feet, msl

: V. Chavez Survey By

: H.S.A. Drilling Method Sampling Method : Split Spoon Clayton Project No.: 70-97066.01 Well: MW-13 GRAPHIC Depth Surf. Elev.: 15 uscs DESCRIPTION Elev. Surface Casing Cover 15 Feet 0 15 Asphalt and baserock 8"-Traffic Rated AC Well Vault set in Concrete Silty CLAY (0,0,20,80) dark brown, stiff, dry. Neat Cement Grout CL Sch40 Blank Pipe Bentonite Clayey SILT (0,0,90,10), light brown - greenish grey, stiff, dry. 5 10 ML \times #2/12 Sand CLAY (0,0,5,95), greyish green- yelow orange, loose, dry, damp, hydrocarbon odor. 0.010" Slotted Screen 10 5 CL V Clayey SAND (5,80,0,15) greenish grey- yelowish SC orange, saturated, hydrocarbon odor. Bottom Cap 15 0 05-20-2002 s:\es\boring_legs\p97066\MW-13.BOR 20 Notes:



LOG OF **MONITORING WELL**

Project No.: 70-04578.02

Client:

AIG

Location: 630 29th Avenue, Oakland, California

Logged By: P. McLaughlin

Start Date: 8/19/2005

Start Time:

Elevation: N/A Boring Dia.: 7"

BORING NO.

T-1

Finish Date: 8/19/2005

Driller: Exploration Geoservices

Finish Time:

Drill Method: Hollow Stem Auger

Hammer Weight: N/A

Drop:

N/A

| l Richard | | | | | | | | Borehole Completion Data: Boring completed as test well | | | |
|--------------------|--|------------|--|------|---------------------------------|--------------------------|-------|--|--|---|--|
| SAMPLE INTERVAL | SAMPLE RECOVERY (in) | SAMPLE ID. | PID READING (ppm) | TIME | ОЕРТН (ft) | SAMPLE GRAPHIC LOG | uscs | DESCRIPTION | CON Traffic cover with well plug | WELL STRUCTION | |
| <i>W</i> = | (5) E. | 2.5 | | 1.5 | 1 2- 3 4 5 6- | <u>X</u> | ML SM | Concrete Slab, 0.75' thick CLAYEY SILT dark brown, damp, soft SILTY SAND brown, damp, loose, trace fine gravel up to 3/8" dia. SILTY SAND WITH GRAVEL grayish brown, damp, loose, with fine gravel up to 3/4" dia. SILTY SAND light brown, moist, loose, trace fine gravel up to 3/8" dia. | | Portland Type II Neat Cement from 0.5 to 3 feet bgs Bentonite Seal from 3 to 4 feet bgs 2" Blank SCH-40 PVC Riser Casing from 0 to 5 feet bgs Lonestar 2/12 Sand from 4 to 15 feet bgs | |
| | *************************************** | 10.0 | A CONTRACTOR OF THE CONTRACTOR | | 9- 10~ 11~ 12- | | SM | hydrocarbon odor from ~9.0' - 15.0' | | 2-inch diameter PVC Well Screen (0.010-in. Slot) from 5 to 15 feet bgs | |
| | the state of the s | 15.0 | | | 14- 15- 16- 17- 18- | | | EOB at 15 feet bgs No Groundwater Encountered During Drilling. | | : | |



LOG OF MONITORING **WELL**

Project No.: 70-04578.02

Client: AIG

630 29th Avenue, Oakland, California Location:

Logged By: P. McLaughlin

Start Date: 8/19/2005

Start Time:

Elevation: N/A

BORING NO.

T-2

Finish Date: 8/19/2005

Driller: Exploration Geoservices

Finish Time:

Boring Dia.: 7"

Hammer Weight: N/A

Drop:

Drill Method: Hollow Stem Auger N/A

Borehole Completion Data: Boring completed as test well

| | · | | , | | · | , | | | Borehole Completion Data: Boring comple | ted as test we | ·II |
|--------------------|-------------------------|------------|----------------------|---------|------------|-------------------|-----|----------|---|----------------------------------|---|
| SAMPLE INTERVAL | SAMPLE RECOVERY (in) | SAMPLE ID. | PID READING (ppm) | TIME | оертн (п) | SAMPLE GRAPHIC | 90: | nscs | DESCRIPTION | CON Traffic cover with well plug | WELL STRUCTION |
| <i>s</i> ≥ | N EX | S) | <u> </u> | <u></u> | 0 | | | <u> </u> | Concrete Slab, 0.75' thick | Willi Well pidg | |
| | | | | | 4. (| | | ML | CLAYEY SILT dark brown, damp, soft | | – Portland Type II |
| | | 2.5 | | | 3- | X | | SM | SILTY SAND brown, damp, loose, trace fine gravel up to 3/8" dia. | | Neat Cement from 0.5 to 3 feet bgs |
| | | | | | 4- | | | | SILTY SAND WITH GRAVEL grayish brown, damp, loose, with fine gravel up to 3/4" dia. | | - Bentonite Seal from 3 to 4 feet bgs - 2" Blank SCH-40 |
| | | 5.0 | | | 5- 6- | | | SM | | | PVC Riser Casing from 0 to 5 feet bgs |
| | | 7.5 | | | 7 <i>-</i> | X | | | SILTY SAND light brown, moist, loose, trace fine gravel up to 3/8" dia. | | - Lonestar 2/12 Sand from 4 to 15 feet bgs |
| | | 10.0 | | | 10- | X | | SM | hydrocarbon odor from ~9.0' - 15.0' | | – 2-inch diameter PVC Well Screen (0.010-in. Slot) from 5 to 15 feet bgs |
| | | 12.5 | | | 12- | M. | | | | | |
| | | 15.0 | | | 15- | | | | | | |
| | | | | | 16- | | 1.3 | | EOB at 15 feet bgs No Groundwater Encountered During Drilling. | | |
| | | | | | 17- | | | | | | |
| | | | | | 18- | | | | | | |
| | | | | | 19- | | | | | | Page 1 of 1 |



APPENDIX B HISTORICAL GROUNDWATER ELEVATION DATA



| Well | Date | Top of Casing | Depth to | Groundwater |
|----------------|------------|--------------------|--------------|--------------------|
| Identification | Measured | Elevation (ft,msl) | Water (feet) | Elevation (ft,msl) |
| | 0/0// 000 | 40.00 | | 40.00 |
| MW-1 | 2/8/1999 | 16.69 | 3.60 | 13.09 |
| | 6/15/2000 | 16.69 | 4.82 | 11.87 |
| | 9/22/2000 | 16.69 | 6.30 | 10.39 |
| | 12/19/2000 | 16.69 | 5.50 | 11.19 |
| | 3/21/2001 | 16.69 | 4.29 | 12.40 |
| | 6/20/2001 | 16.69 | 5.85 | 10.84 |
| | 9/25/2001 | 16.69 | 6.76 | 9.93 |
| | 12/3/2001 | 16.69 | 4.17 | 12.52 |
| | 3/25/2002 | 16.69 | 2.77 | 13.92 |
| | 6/28/2002 | 16.69 | 5.61 | 11.08 |
| | 9/11/2002 | 16.69 | 6.17 | 10.52 |
| | 12/16/2002 | 16.69 | 3.91 | 12.78 |
| | 3/28/2003 | 16.69 | 4.44 | 12.25 |
| | 6/24/2003 | 16.69 | 5.29 | 11.40 |
| | 9/26/2003 | 16.69 | 6.88 | 9.81 |
| | 12/16/2003 | 16.69 | NM | NM |
| | 4/6/2004 | 16.69 | 3.57 | 13.12 |
| | 6/23/2004 | 16.69 | 5.96 | 10.73 |
| | 9/15/2004 | 16.69 | NM | NM |
| | 12/16/2004 | 16.69 | 4.40 | 12.29 |
| | 3/22/2005 | 16.69 | 3.44 | 13.25 |
| | 6/24/2005 | 16.69 | 4.45 | 12.24 |
| | 9/13/2005 | 16.69 | 6.03 | 10.66 |
| | 12/2/2005 | 16.69 | 4.95 | 11.74 |
| | 3/2/2006 | 16.69 | 3.74 | 12.95 |
| | 6/15/2006 | 16.69 | 4.58 | 12.11 |
| | 9/14/2006 | 16.69 | 5.15 | 11.54 |
| | 1/11/2007 | 16.69 | 4.01 | 12.68 |
| | 4/9/2007 | 16.69 | 4.67 | 12.02 |
| | 9/17/2007 | 16.69 | 6.39 | 10.30 |
| | 12/19/2007 | 16.69 | 5.40 | 11.29 |
| | 3/11/2008 | 16.69 | 4.21 | 12.48 |
| | 6/10/2008 | 16.69 | 5.68 | 11.01 |
| | 9/9/2008 | 16.69 | 6.67 | 10.02 |
| | 12/2/2008 | 16.69 | 6.17 | 10.52 |
| MW-2 | 2/8/1999 | 20.79 | 14.20 | 6.59 |
| 10100-2 | 6/15/2000 | 20.79 | 10.46 | 10.33 |
| | 9/22/2000 | 20.79 | 11.49 | 9.30 |
| | 12/19/2000 | 20.79 | 11.38 | 9.41 |
| | 3/21/2001 | 20.79 | 10.01 | 10.78 |
| | 6/20/2001 | 20.79 | 10.92 | 9.87 |
| | 9/25/2001 | 20.79 | 11.78 | 9.01 |
| | 12/3/2001 | 20.79 | 11.13 | 9.66 |
| | 3/25/2001 | 20.79 | 9.21 | 11.58 |
| | 6/28/2002 | 20.79 | 10.65 | 10.14 |
| | 9/11/2002 | 20.79 | 10.89 | 9.90 |
| | 12/16/2002 | 20.79 | 11.15 | 9.64 |
| | 3/28/2003 | 20.79 | 10.27 | 10.52 |
| | 6/24/2003 | 20.79 | 10.24 | 10.55 |
| | | <u> </u> | 10.47 | 10.00 |
| | 9/26/2003 | 20.79 | 11.20 | 9.59 |



| Well | Date | Top of Casing | Depth to | Groundwater |
|----------------|------------------------|---------------------------|--------------|--------------------|
| Identification | Measured | Elevation (ft,msl) | Water (feet) | Elevation (ft,msl) |
| | 4/0/0004 | 00.70 | 0.40 | 44.00 |
| MW-2 | 4/6/2004 | 20.79 | 9.40 | 11.39 |
| | 6/23/2004 | 20.79 | 11.60 | 9.19 |
| | 9/15/2004 | 20.79 | 10.94 | 9.85 |
| | 12/16/2004 | 20.79 | NM | NM |
| | 3/22/2005 | 20.79 | 9.26 | 11.53 |
| | 6/24/2005 | 20.79 | 10.03 | 10.76 |
| | 9/13/2005 | 20.79 | 10.58 | 10.21 |
| | 12/2/2005 | 20.79 | NM | NM |
| | 3/2/2006 | 20.79 | 9.45 | 11.34 |
| | 6/15/2006 | 20.79 | 9.84 | 10.95 |
| | 9/14/2006 | 20.79 | 10.27 | 10.52 |
| | 1/11/2007 | 20.79 | 10.45 | 10.34 |
| | 4/9/2007 | 20.79 | 10.03 | 10.76 |
| | 9/17/2007 | 20.79 | 10.85 | 9.94 |
| | 12/19/2007 | 20.79 | 10.71 | 10.08 |
| | 3/11/2008 | 20.79 | 9.76 | 11.03 |
| | 6/10/2008 | 20.79 | 10.64 | 10.15 |
| | 9/9/2008 | 20.79 | 11.04 | 9.75 |
| | 12/2/2008 | 20.79 | 11.13 | 9.66 |
| | | | | |
| MW-3 | 2/8/1999 | 21.10 | 7.45 | 13.65 |
| | 6/15/2000 | 21.10 | 10.56 | 10.54 |
| | 9/22/2000 | 21.10 | 15.30 | 5.80 |
| | 12/19/2000 | 21.10 | 9.72 | 11.38 |
| | 3/21/2001 | 21.10 | 8.95 | 12.15 |
| | 6/20/2001 | 21.10 | 10.14 | 10.96 |
| | 9/25/2001 | 21.10 | 10.74 | 10.36 |
| | | itoring program in Octobe | | 10.00 |
| | | | | |
| MW-4 | 2/8/1999 | 17.78 | 4.13 | 13.65 |
| | 6/15/2000 | 17.78 | 6.30 | 11.48 |
| | 9/22/2000 | 17.78 | 6.90 | 10.88 |
| | 12/19/2000 | 17.78 | 6.40 | 11.38 |
| | 3/21/2001 | 17.78 | 5.77 | 12.01 |
| | 6/20/2001 | 17.78 | 6.78 | 11.00 |
| | 9/25/2001 | 17.78 | 7.40 | 10.38 |
| | Removed from mon | itoring program in Octobe | r 2001 | |
| B4347 F | 0/0/4000 | 04.40 | 7.00 | 40.50 |
| MW-5 | 2/8/1999 | 21.12 | 7.62 | 13.50 |
| | 6/15/2000 | 21.12 | 10.36 | 10.76 |
| | 9/22/2000 | 21.12 | 9.99 | 11.13 |
| | 12/19/2000 | 21.12 | 9.99 | 11.13 |
| | 3/21/2001 | 21.12 | 8.68 | 12.44 |
| | 6/20/2001 | 21.12 | 9.90 | 11.22 |
| | 9/25/2001 | 21.12 | 10.34 | 10.78 |
| | Removed from mon | itoring program in Octobe | r 2001 | |
| MW-6 | 6/15/2000 | 16.60 | 5.47 | 11.13 |
| 3 | 9/22/2000 | 16.60 | 6.54 | 10.06 |
| | 12/19/2000 | 16.60 | 5.93 | 10.67 |
| | 3/21/2001 | 16.60 | 5.93 4.70 | 11.90 |
| | | | | |
| | 6/20/2001 9/25/2001 | 16.60 16.60 | 6.13 6.68 | 10.47 9.92 |
| | 9/75/7001 | ID DU | n nă | |



| Well dentification | Date | Top of Casing | Depth to | Groundwater |
|-----------------------|------------|--------------------|--------------|--------------------|
| dentification | Measured | Elevation (ft,msl) | Water (feet) | Elevation (ft,msl) |
| 1W-6 | 12/3/2001 | 16.60 | 4.72 | 11.88 |
| | 3/25/2002 | 16.60 | 3.93 | 12.67 |
| | 6/28/2002 | 16.60 | 5.83 | 10.77 |
| | 9/11/2002 | 16.60 | 5.43 | 11.17 |
| | 12/16/2002 | 16.60 | 3.93 | 12.67 |
| | 3/28/2003 | 16.60 | NM | NM |
| | 6/24/2003 | 16.60 | 5.52 | 11.08 |
| | 9/26/2003 | 16.60 | 6.70 | 9.90 |
| | 12/16/2003 | 16.60 | 4.99 | 11.61 |
| | 4/6/2004 | 16.60 | 4.85 | 11.75 |
| | 6/23/2004 | 16.60 | 5.76 | 10.84 |
| | 9/15/2004 | 16.60 | 6.56 | 10.04 |
| | 12/16/2004 | 16.60 | 4.56 | 12.04 |
| | 3/22/2005 | 16.60 | 3.63 | 12.97 |
| | 6/24/2005 | 16.60 | 4.84 | 11.76 |
| | 9/13/2005 | 16.60 | 6.15 | 10.45 |
| | 12/2/2005 | 16.60 | 5.24 | 11.36 |
| | 3/2/2006 | 16.60 | 3.41 | 13.19 |
| | 6/15/2006 | 16.60 | 5.09 | 11.51 |
| | 9/14/2006 | 16.60 | 5.68 | 10.92 |
| | | | 5.66 4.71 | 11.89 |
| | 1/11/2007 | 16.60 | | |
| | 4/9/2007 | 16.60 16.60 | 5.25 | 11.35 10.04 |
| | 9/17/2007 | | 6.56 | |
| | 12/19/2007 | 16.60 | 5.41 | 11.19 |
| | 3/11/2008 | 16.60 | 4.89 | 11.71 |
| | 6/10/2008 | 16.60 | 6.01 | 10.59 |
| | 9/9/2008 | 16.60 | 6.75 | 9.85 |
| | 12/2/2008 | 16.60 | 6.36 | 10.24 |
| 1W-7 | 12/16/2002 | 15.47 | 5.01 | 10.46 |
| | 12/17/2002 | 15.47 | 6.95 | 8.52 |
| | 12/18/2002 | 15.47 | 6.94 | 8.53 |
| | 12/19/2002 | 15.47 | 6.04 | 9.43 |
| | 12/20/2002 | 15.47 | 6.48 | 8.99 |
| | 12/21/2002 | 15.47 | 7.25 | 8.22 |
| | 12/22/2002 | 15.47 | 6.90 | 8.57 |
| | 12/23/2002 | 15.47 | 5.53 | 9.94 |
| | 12/24/2002 | 15.47 | 7.20 | 8.27 |
| | 12/25/2002 | 15.47 | 7.51 | 7.96 |
| | 12/26/2002 | 15.47 | 6.40 | 9.07 |
| | 3/28/2003 | 15.47 | 5.68 | 9.79 |
| | 6/24/2003 | 15.47 | 6.13 | 9.34 |
| | 9/26/2003 | 15.47 | 7.22 | 8.25 |
| | 12/16/2003 | 15.47 | 5.68 | 9.79 |
| | 4/6/2004 | 15.47 | 5.60 | 9.87 |
| | 6/23/2004 | 15.47 | 6.20 | 9.27 |
| | 9/15/2004 | 15.47 | 6.70 | 8.77 |
| | 12/16/2004 | 15.47 | 5.15 | 10.32 |
| | 3/22/2005 | 15.47 | NM | NM |
| | 6/24/2005 | 15.47 | NM | NM |
| | 9/13/2005 | 15.47 | 6.45 | 9.02 |
| | 12/2/2005 | 15.47 | 5.93 | 9.02 9.54 |
| | | | | |
| | 3/2/2006 | 15.47 | 4.65 | 10.82 |



| Well | Date | Top of Casing | Depth to | Groundwater |
|----------------|------------|--------------------|--------------|--------------------|
| Identification | Measured | Elevation (ft,msl) | Water (feet) | Elevation (ft,msl) |
| BANA/ 7 | C/4E/2006 | 45 47 | E 74 | 0.76 |
| MW-7 | 6/15/2006 | 15.47 | 5.71 | 9.76 |
| | 9/14/2006 | 15.47 | 6.10 | 9.37 |
| | 1/11/2007 | 15.47 | 6.04 | 9.43 |
| | 4/9/2007 | 15.47 | 5.68 | 9.79 |
| | 9/17/2007 | 15.47 | 6.93 | 8.54 |
| | 12/19/2007 | 15.47 | 5.81 | 9.66 |
| | 3/11/2008 | 15.47 | 5.54 | 9.93 |
| | 6/10/2008 | 15.47 | 6.49 | 8.98 |
| | 9/9/2008 | 15.47 | 7.08 | 8.39 |
| | 12/2/2008 | 15.47 | 6.79 | 8.68 |
| MW-8 | 6/15/2000 | 17.58 | 7.14 | 10.44 |
| | 9/22/2000 | 17.58 | 8.33 | 9.25 |
| | 12/19/2000 | 17.58 | 7.71 | 9.87 |
| | 3/21/2001 | 17.58 | 6.40 | 11.18 |
| | 6/20/2001 | 17.58 | 7.96 | 9.62 |
| | 9/25/2001 | 17.58 | 8.89 | 8.69 |
| | 12/3/2001 | 17.58 | 6.58 | 11.00 |
| | 3/25/2001 | 17.58 | 5.40 | 12.18 |
| | 6/28/2002 | 17.58 | | |
| | | | 7.71 | 9.87 |
| | 9/11/2002 | 17.58 | 8.40 | 9.18 |
| | 12/16/2002 | 17.58 | 5.63 | 11.95 |
| | 3/28/2003 | 17.58 | 6.62 | 10.96 |
| | 6/24/2003 | 17.58 | 7.44 | 10.14 |
| | 9/26/2003 | 17.58 | 8.71 | 8.87 |
| | 12/16/2003 | 17.58 | 6.69 | 10.89 |
| | 4/6/2004 | 17.58 | 6.74 | 10.84 |
| | 6/23/2004 | 17.58 | 7.98 | 9.60 |
| | 9/15/2004 | 17.58 | 8.52 | 9.06 |
| | 12/16/2004 | 17.58 | 5.61 | 11.97 |
| | 3/22/2005 | 17.58 | 5.54 | 12.04 |
| | 6/24/2005 | 17.58 | 6.77 | 10.81 |
| | 9/13/2005 | 17.58 | 7.92 | 9.66 |
| | 12/2/2005 | 17.58 | 7.36 | 10.22 |
| | 3/2/2006 | 17.58 | 5.83 | 11.75 |
| | 6/15/2006 | 17.58 | 6.99 | 10.59 |
| | 9/14/2006 | 17.58 | 7.58 | 10.00 |
| | 1/11/2007 | 17.58 | 6.30 | 11.28 |
| | 4/9/2007 | 17.58 | 7.05 | 10.53 |
| | 9/17/2007 | 17.58 | | 9.32 |
| | | 17.58 | 8.26 | 10.63 |
| | 12/19/2007 | | 6.95 | |
| | 3/11/2008 | 17.58 | 6.57 | 11.01 |
| | 6/10/2008 | 17.58 | 7.73 | 9.85 |
| | 9/9/2008 | 17.58 | 8.48 | 9.10 |
| | 12/2/2008 | 17.58 | 8.29 | 9.29 |
| MW-9 | 12/3/2001 | 17.61 | 5.79 | 11.82 |
| | 3/25/2002 | 17.61 | 4.98 | 12.63 |
| | 6/28/2002 | 17.61 | 7.71 | 9.90 |
| | 9/11/2002 | 17.61 | 6.91 | 10.70 |
| | 12/16/2002 | 17.61 | 6.58 | 11.03 |
| | | | 6.08 | |
| | 3/28/2003 | 17.61 | 0.00 | 11.53 |



| Well | Date | Top of Casing | Depth to | Groundwater |
|---------------|------------|--------------------|--------------|--------------------|
| dentification | Measured | Elevation (ft,msl) | Water (feet) | Elevation (ft,msl) |
| /IW-9 | 6/24/2003 | 17.61 | 6.42 | 11.19 |
| | 9/26/2003 | 17.61 | 8.14 | 9.47 |
| | 12/16/2003 | 17.61 | 6.76 | 10.85 |
| | 4/6/2004 | 17.61 | 5.97 | 11.64 |
| | 6/23/2004 | 17.61 | 7.80 | 9.81 |
| | 9/15/2004 | 17.61 | 7.14 | 10.47 |
| | 12/16/2004 | 17.61 | 5.73 | 11.88 |
| | 3/22/2005 | 17.61 | 5.31 | 12.30 |
| | 6/24/2005 | 17.61 | 6.05 | 11.56 |
| | 9/13/2005 | 17.61 | 6.70 | 10.91 |
| | 12/2/2005 | 17.61 | 6.92 | 10.69 |
| | 3/2/2006 | 17.61 | 5.83 | 11.78 |
| | 6/15/2006 | 17.61 | 6.32 | 11.29 |
| | 9/14/2006 | 17.61 | 6.79 | 10.82 |
| | 1/11/2007 | 17.61 | 5.59 | 12.02 |
| | 4/9/2007 | 17.61 | 6.35 | 11.26 |
| | 9/17/2007 | 17.61 | 7.26 | 10.35 |
| | 12/19/2007 | 17.61 | 6.81 | 10.80 |
| | 3/11/2008 | 17.61 | 5.95 | 11.66 |
| | 6/10/2008 | 17.61 | 6.98 | 10.63 |
| | 9/9/2008 | 17.61 | 7.34 | 10.27 |
| | 12/2/2008 | 17.61 | 7.31 | 10.30 |
| MW-10 | 12/3/2001 | 16.92 | 4.22 | 12.70 |
| | 3/25/2002 | 16.92 | 3.00 | 13.92 |
| | 6/28/2002 | 16.92 | 5.65 | 11.27 |
| | 9/11/2002 | 16.92 | 6.16 | 10.76 |
| | 12/16/2002 | 16.92 | 3.74 | 13.18 |
| | 3/28/2003 | 16.92 | 4.54 | 12.38 |
| | 6/24/2003 | 16.92 | 5.40 | 11.52 |
| | 9/26/2003 | 16.92 | 6.98 | 9.94 |
| | 12/16/2003 | 16.92 | 4.94 | 11.98 |
| | 4/6/2004 | 16.92 | 4.54 | 12.38 |
| | 6/23/2004 | 16.92 | 5.96 | 10.96 |
| | 9/15/2004 | 16.92 | 6.86 | 10.06 |
| | 12/16/2004 | 16.92 | 4.45 | 12.47 |
| | 3/22/2005 | 16.92 | 3.56 | 13.36 |
| | 6/24/2005 | 16.92 | 4.58 | 12.34 |
| | 9/12/2005 | 16.92 | 6.08 | 10.84 |
| | 12/2/2005 | 16.92 | 4.94 | 11.98 |
| | 3/2/2006 | 16.92 | 3.90 | 13.02 |
| | 6/15/2006 | 16.92 | 4.74 | 12.18 |
| | 9/14/2006 | 16.92 | 5.27 | 11.65 |
| | 1/11/2007 | 16.92 | 4.37 | 12.55 |
| | 4/9/2007 | 16.92 | 4.81 | 12.11 |
| | 9/17/2007 | 16.92 | 6.48 | 10.44 |
| | 12/19/2007 | 16.92 | 5.21 | 11.71 |
| | 3/11/2008 | 16.92 | 4.60 | 12.32 |
| | 6/10/2008 | 16.92 | 5.77 | 11.15 |
| | 9/9/2008 | 16.92 | 6.71 | 10.21 |
| | 12/2/2008 | 16.92 | 6.22 | 10.70 |



| Well | Date | Top of Casing | Depth to | Groundwater |
|---------------|------------|--------------------|--------------|--------------------|
| dentification | Measured | Elevation (ft,msl) | Water (feet) | Elevation (ft,msl) |
| /IW-11 | 12/3/2001 | 14.87 | 5.67 | 9.20 |
| NVV-11 | 3/25/2001 | 14.87 | 4.68 | 10.19 |
| | 6/28/2002 | 14.87 | 6.35 | 8.52 |
| | 9/11/2002 | 14.87 | 6.91 | 7.96 |
| | 12/16/2002 | 14.87 | 3.92 | 10.95 |
| | 3/28/2003 | 14.87 | 5.17 | 9.70 |
| | 6/24/2003 | 14.87 | 5.86 | 9.01 |
| | 9/26/2003 | 14.87 | 7.16 | 7.71 |
| | 12/16/2003 | 14.87 | 5.61 | 9.26 |
| | 4/6/2004 | 14.87 | 5.49 | 9.38 |
| | 6/23/2004 | 14.87 | 5.68 | 9.19 |
| | 12/16/2004 | 14.87 | 4.69 | 10.18 |
| | 3/22/2005 | 14.87 | 4.20 | 10.16 |
| | 6/24/2005 | 14.87 | 5.41 | 9.46 |
| | | | | |
| | 9/13/2005 | 14.87 14.87 | 6.23 | 8.64 8.42 |
| | 9/15/2005 | | 6.45 | |
| | 12/2/2005 | 14.87 | 5.95 | 8.92 |
| | 3/2/2006 | 14.87 | 4.31 | 10.56 |
| | 6/15/2006 | 14.87 | 5.40 | 9.47 |
| | 9/14/2006 | 14.87 | 5.94 | 8.93 |
| | 1/11/2007 | 14.87 | 5.45 | 9.42 |
| | 4/9/2007 | 14.87 | 5.52 | 9.35 |
| | 9/17/2007 | 14.87 | NM 5.74 | NM 2.10 |
| | 12/19/2007 | 14.87 | 5.74 | 9.13 |
| | 3/11/2008 | 14.87 | 4.82 | 10.05 |
| | 6/10/2008 | 14.87 | 6.17 | 8.70 |
| | 9/9/2008 | 14.87 | 6.98 | 7.89 |
| | 12/2/2008 | 14.87 | 6.71 | 8.16 |
| /IW-12 | 6/28/2002 | 14.05 | 6.13 | 7.92 |
| | 9/11/2002 | 14.05 | 6.82 | 7.23 |
| | 12/16/2002 | 14.05 | 4.94 | 9.11 |
| | 3/28/2003 | 14.05 | 5.08 | 8.97 |
| | 6/24/2003 | 14.05 | 5.73 | 8.32 |
| | 9/26/2003 | 14.05 | 6.94 | 7.11 |
| | 12/16/2003 | 14.05 | 4.99 | 9.06 |
| | 4/6/2004 | 14.05 | 5.04 | 9.01 |
| | 6/23/2004 | 14.05 | 5.78 | 8.27 |
| | 9/15/2004 | 14.05 | 6.43 | 7.62 |
| | 12/16/2004 | 14.05 | 4.34 | 9.71 |
| | 3/22/2005 | 14.05 | 3.50 | 10.55 |
| | 6/24/2005 | 14.05 | 4.9 | 9.15 |
| | 9/12/2005 | 14.05 | 6.11 | 7.94 |
| | 12/2/2005 | 14.05 | 5.13 | 8.92 |
| | 3/2/2006 | 14.05 | 3.83 | 10.22 |
| | 6/15/2006 | 14.05 | 5.18 | 8.87 |
| | 9/14/2006 | 14.05 | 5.86 | 8.19 |
| | 1/11/2007 | 14.05 | 6.97 | 7.08 |
| | 4/9/2007 | 14.05 | 5.31 | 8.74 |
| | 9/17/2007 | 14.05 | 6.59 | 7.46 |
| | 12/19/2007 | | 5.24 | |
| | | 14.05 | | 8.81 |
| | 3/11/2008 | 14.05 | 4.80 | 9.25 |
| | 6/10/2008 | 14.05 | 6.13 | 7.92 |



HISTORICAL GROUNDWATER ELEVATION DATA FORMER LEMOINE SAUSAGE FACTORY 630 29TH AVENUE OAKLAND, CALIFORNIA

| Well Identification | Date Measured | Top of Casing Elevation (ft,msl) | Depth to Water (feet) | Groundwater Elevation (ft,msl) |
|------------------------|------------------|-------------------------------------|--------------------------|-----------------------------------|
| MW-12 | 9/9/2008 | 14.05 | 6.84 | 7.21 |
| IVI VV - 1 Z | 12/2/2008 | 14.05 | 6.59 | 7.46 |
| MW-13 | 6/28/2002 | 13.39 | 6.21 | 7.18 |
| | 9/11/2002 | 13.39 | 6.66 | 6.73 |
| | 12/16/2002 | 13.39 | 3.90 | 9.49 |
| | 3/28/2003 | 13.39 | 5.34 | 8.05 |
| | 6/24/2003 | 13.39 | 5.99 | 7.40 |
| | 9/26/2003 | 13.39 | 6.99 | 6.40 |
| | 12/16/2003 | 13.39 | 5.01 | 8.38 |
| | 4/6/2004 | 13.39 | 5.35 | 8.04 |
| | 6/23/2004 | 13.39 | 6.12 | 7.27 |
| | 9/15/2004 | 13.39 | 6.63 | 6.76 |
| | 12/16/2004 | 13.39 | 4.69 | 8.70 |
| | 3/22/2005 | 13.39 | 4.86 | 8.53 |
| | 6/24/2005 | 13.39 | 5.13 | 8.26 |
| | 9/12/2005 | 13.39 | 6.33 | 7.06 |
| | 12/2/2005 | 13.39 | 5.25 | 8.14 |
| | 3/2/2006 | 13.39 | 4.33 | 9.06 |
| | 6/15/2006 | 13.39 | 5.44 | 7.95 |
| | 9/14/2006 | 13.39 | 6.03 | 7.36 |
| | 1/11/2007 | 13.39 | 5.41 | 7.98 |
| | 4/9/2007 | 13.39 | 5.71 | 7.68 |
| | 9/17/2007 | 13.39 | 6.65 | 6.74 |
| | 12/19/2007 | 13.39 | 5.37 | 8.02 |
| | 3/11/2008 | 13.39 | 5.32 | 8.07 |
| | 6/10/2008 | 13.39 | 6.40 | 6.99 |
| | 9/9/2008 | 13.39 | 7.03 | 6.36 |
| | 12/2/2008 | 13.39 | 6.73 | 6.66 |

Notes:

- 1. Top of casing elevations are referenced to mean sea level (msl) and surveyed with reference to the benchmark located at Peterson Street and East 7th Street.
- 2. NM refers to Not Measured.
- 3. ft, msl refers to feet above mean sea level.



APPENDIX C HISTORICAL GROUNDWATER ANALYTICAL DATA





| | | | | | | Total | | 1,2- | cis-1,2- | trans-1,2- | |
|----------|------------|-------------|---------|------------|--------------|---------|------------|----------|------------|------------|------------|
| Well | Date | TPH-g | Benzene | Toluene | Ethylbenzene | Xylenes | TCE | DCA | DCE | DCE | VC |
| Location | Sampled | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) |
| MW-1 | 2/8/1999 | 48,000 | 3,900 | 6,300 | 970 | 4,300 | NA | <30 | NA | NA | NA |
| 10100-1 | 6/15/2000 | 29,000 | 3,900 | <100 | 1,900 | 4,200 | <5.0 | <5.0 | < 5.0 | <5.0 | <5.0 |
| | 9/22/2000 | 25,000 | 3,100 | 1,800 | 470 | 3,600 | NA | NA | NA | NA | NA |
| | 12/19/2000 | 25,000 | 3,200 | 1,900 | 480 | 3,300 | <2.5 | <2.5 | <2.5 | <2.5 | <2.5 |
| | 3/21/2000 | 21,000 | 3,200 | 1,700 | 290 | 2,600 | <2.5 | <2.5 | <2.5 | <2.5 | <2.5 |
| | 6/21/2001 | 12,000 | 2,000 | 880 | 180 | 1,180 | <0.5 | 3.0 | <0.5 | <0.5 | <0.5 |
| | 9/26/2001 | 16,000 | 1,100 | 130 | < 10 | 320 | < 2.5 | < 2.5 | < 2.5 | < 2.5 | < 2.5 |
| | 12/3/2001 | 15,000 | 2,800 | 1,200 | 310 | 1,660 | <3.1 | <3.1 | <3.1 | <3.1 | <3.1 |
| | 3/25/2002 | 11,000 | 3,200 | 1,200 | 73 | 1,860 | <5 | <5 | <5 | <5 | <5 |
| | 6/28/2002 | 26,000 | 3,200 | 1,800 | 640 | 2,900 | <3.1 | <3.1 | <3.1 | <3.1 | <3.1 |
| | 9/11/2002 | 27,000 | 3,200 | 1,900 | 720 | 3,500 | <4.2 | <4.2 | <4.2 | <4.2 | <4.2 |
| | 12/16/2002 | 20,000 | 2,800 | 490 | 500 | 2,300 | <4.2 | <4.2 | <4.2 | <4.2 | <4.2 |
| | 3/28/2003 | 20,000 | 2,700 | 1,500 | 650 | 2,300 | <3.6 | <3.6 | <3.6 | <3.6 | <3.6 |
| | 6/24/2003 | 14,000 | 2,400 | 1,400 | 500 | 2,100 | <4.2 | <4.2 | <4.2 | <4.2 | <4.2 |
| | 9/26/2003 | 11,000 | 1,200 | 960 | 370 | 1,600 | <1.0 | <1.0 | <1.0 | <1.0 | <1.0 |
| | 12/16/2003 | Not Sampled | | 000 | 0.0 | 1,000 | 11.0 | 11.0 | 11.0 | 11.0 | 11.0 |
| | 4/6/2004 | 18,000 | 2,400 | 1,300 | 550 | 1,730 | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 |
| | 6/23/2004 | 25,000 | 2,700 | 1,700 | 680 | 2,300 | <2.5 | <2.5 | <2.5 | <2.5 | <2.5 |
| | 9/15/2004 | Not Sampled | • | .,. 00 | 000 | 2,000 | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 |
| | 12/16/2004 | 1,800 | 260 | 89 | 32 | 119 | <2.5 | <2.5 | <2.5 | <2.5 | <2.5 |
| | 3/22/2005 | 19,000 | 2,400 | 960 | 530 | 1,330 | <3.6 | <3.6 | <3.6 | <3.6 | <3.6 |
| | 6/24/2005 | 12,000 | 2,400 | 450 | 470 | 940 | <3.6 | <3.6 | <3.6 | <3.6 | <3.6 |
| | 9/13/2005 | 17,000 | 2,700 | 1,000 | 740 | 1,760 | <1.0 | <1.0 | <1.0 | <1.0 | <1.0 |
| | 12/2/2005 | 9,300 | 1,500 | 500 | 420 | 1,060 | <3.6 | <3.6 | <3.6 | <3.6 | <3.6 |
| | 3/2/2006 | 6,200 | 1,400 | 200 | 180 | 370 | <3.6 | <3.6 | <3.6 | <3.6 | <3.6 |
| | 6/15/2006 | 10,000 | 2,500 | 200 | 440 | 570 | <4.2 | <4.2 | <4.2 | <4.2 | <4.2 |
| | 9/14/2006 | 13,000 | 2,300 | 320 | 450 | 870 | <4.2 | <4.2 | <4.2 | <4.2 | <4.2 |
| | 1/11/2007 | 14,000 | 1,200 | 270 | 450 | 850 | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 |
| | 4/9/2007 | 12,000 | 1,800 | 270 | 520 | 750 | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 |
| | 9/17/2007 | 9,000 | 1,200 | 230 | 450 | 471 | <2.0 | <2.0 | <2.0 | <2.0 | <2.0 |
| | 12/19/2007 | 12,000 | 1,400 | 290 | 670 | 746 | <2.5 | <2.5 | <2.5 | <2.5 | <2.5 |
| | 3/11/2008 | 10,000 | 1,900 | 290 280 | 550 | 650 | <2.5 | <2.5 | <2.5 | <2.5 | <2.5 |
| | 6/10/2008 | 8,700 | 1,700 | 170 | 430 | 373 | <2.5 | <2.5 | <2.5 | <2.5 | <2.5 |
| | 9/9/2008 | 7,600 | 830 | | 230 540 | 350 | <1.7 | <1.7 | <1.7 | <1.7 | <1.7 |
| | 12/2/2008 | 5,700 | 940 | 220 | 430 | 299 | <1.3 | <1.3 | <1.3 | <1.3 | <1.3 |
| | 0/0/4000 | 44.000 | 44.000 | 4.000 | 050 | 4 =00 | | | | | |
| MW-2 | 2/8/1999 | 41,000 | 11,000 | 4,900 | 650 | 1,720 | NA .F.O | 60 25 | NA .F.O | NA .F.O | NA .F.O |
| | 6/29/2000 | 31,000 | 11,000 | 930 | 4,400 | 250 | <5.0 | 25 | <5.0 | <5.0 | <5.0 |
| | 9/22/2000 | 24,000 | 10,000 | 2,700 | 370 | 1,200 | NA | NA | NA | NA | NA |
| | 12/19/2000 | 43,000 | 9,800 | 4,000 | 810 | 2,430 | <13 | 21 | <13 | <13 | <13 |
| | 3/23/2001 | 34,000 | 10,000 | 3,200 | 410 | 1,220 | <13 | 14 | <13 | <13 | <13 |
| | 6/21/2001 | 30,000 | 8,600 | 2,600 | 440 | 1,230 | <0.5 | 5.6 | <0.5 | <0.5 | <0.5 |
| | 9/26/2001 | 26,000 | 12,000 | 3,900 | 590 | 1,960 | < 10 | 11 | < 10 | < 10 | < 10 |
| | 12/3/2001 | 45,000 | 13,000 | 5,100 | 950 | 2,930 | <7.1 | 14 | <7.1 | <7.1 | <7.1 |
| | 3/25/2002 | 21,000 | 11,000 | 3,700 | 1,000 | 2,790 | <17 | <17 | <17 | <17 | <17 |
| | 6/28/2002 | 8,400 | 2,200 | 680 | 21 | 220 | <3.1 | 8.8 | <3.1 | <3.1 | <3.1 |
| | 9/11/2002 | 23,000 | 6,600 | 1,000 | 600 | 1,320 | <6.3 | 10 | <6.3 | <6.3 | <6.3 |
| | 12/16/2002 | 6,000 | 1,600 | 410 | 150 | 402 | 4.5 | 2.7 | 69 | 6.9 | <2.5 |
| | 3/28/2003 | 30,000 | 9,300 | 920 | 930 | 2,000 | <13 | 14 | <13 | <13 | <13 |
| | 6/24/2003 | 19,000 | 10,000 | 1,700 | 1,100 | 2,530 | <13 | <13 | <13 | <13 | <13 |
| | 9/26/2003 | 20,000 | 10,000 | 2,100 | 960 | 2,520 | <17 | <17 | <17 | <17 | <17 |
| | 12/16/2003 | 22,000 | 10,000 | 2,700 | 1,200 | 2,920 | <25 | <25 | <25 | <25 | <25 |
| | 4/6/2004 | 27,000 | 7,600 | 1,700 | 630 | 1,420 | <10 | <10 | <10 | <10 | <10 |
| | 6/23/2004 | 33,000 | 8,200 | 1,800 | 870 | 1,930 | <17 | <17 | <17 | <17 | <17 |
| | 9/15/2004 | 46,000 | 13,000 | 1,300 | 1,400 | 2,710 | <17 | <17 | <17 | <17 | <17 |
| | 12/16/2004 | Not Sampled | | 4 000 | 4 000 | 0.500 | .47 | .47 | .47 | .4.7 | .47 |
| | 3/22/2005 | 42,000 | 9,900 | 1,200 | 1,200 | 2,530 | <17 | <17 | <17 | <17 | <17 |





| | | | | | | Total | | 1,2- | cis-1,2- | trans-1,2- | |
|----------|--------------|---------------------------|------------------|----------------|--------------|----------------|----------------|-------------|----------------|-------------|----------------|
| Well | Date | TPH-g | Benzene | Toluene | Ethylbenzene | Xylenes | TCE | DCA | DCE | DCE | VC |
| Location | Sampled | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) |
| MIN O | 6/24/2005 | 31,000 | 40.000 | 4 000 | 810 | 4 200 | .00 | <20 | <20 | <20 | <20 |
| MW-2 | 9/13/2005 | 35,000 | 12,000 13,000 | 1,200 1,100 | 1,300 | 1,380 2,260 | <20 <7.1 | <20 <7.1 | <20 <7.1 | <20 <7.1 | <20 <7.1 |
| | | | | 1,100 | 1,300 | 2,200 | <1.1 | <7.1 | <1.1 | <1.1 | <7.1 |
| | 12/2/2005 | Not Sample | | 620 | 740 | 4 260 | -7.4 | -7.4 | -7.4 | .7.4 | -7.4 |
| | 3/2/2006 | 25,000 | 7,900 | 620 | | 1,260 | <7.1 | <7.1 | <7.1 | <7.1 | <7.1 |
| | 6/15/2006 | 47,000 | 11,000 | 800 | 1,200 | 2,230 | <20 | <20 | <20 | <20 | <20 |
| | 9/14/2006 | 50,000 | 11,000 | 470 | 1,200 | 2,330 C | <10 | <10 | <10 | <10 | <10 |
| | 1/11/2007 | 29,000 | 10,000 | 240 | 1,100 | 1,340 | <13 | <13 | <13 | <13 | <13 |
| | 4/9/2007 | 33,000 | 9,200 | 1,000 | 1,200 | 1,510 | <13 | <13 | <13 | <13 | <13 |
| | 9/17/2007 | 11,000 | 9,200 | 410 | 1,100 | 1,300 | <13 | <13 | <13 | <13 | <13 |
| | 12/19/2007 | 32,000 | 9,900 | 240 | 1,100 | 770 | <17 | <17 | <17 | <17 | <17 |
| | 3/11/2008 | 40,000 | 12,000 | 270 | 1,500 | 1,290 | <13 | <13 | <13 | <13 | <13 |
| | 6/10/2008 | 26,000 | 9,700 | 160 | 990 | 890 | <13 | <13 | <13 | <13 | <13 |
| | 9/9/2008 | 34,000 | 12,000 | 130 | 1,600 | 790 | <13 | <13 | <13 | <13 | <13 |
| | 12/2/2008 | 20,000 | 8,400 | 110 | 1,000 | 610 | <20 | <20 | <20 | <20 | <20 |
| MW-3 | 2/8/1999 | 35,000 | 1,200 | 3,400 | 1,400 | 4,900 | NA | <30 | NA | NA | NA |
| | 6/29/2000 | 39,000 | 7,800 | 630 | 8,000 | 3,400 | <5.0 | 600 | < 5.0 | < 5.0 | <5.0 |
| | 9/22/2000 | 83,000 | 16,000 | 20,000 | 1,300 | 7,000 | NA | NA | NA | NA | NA |
| | 12/19/2000 | 50,000 | 1,200 | 1,600 | 510 | 1,810 | <8.3 | 350 | <8.3 | <8.3 | <8.3 |
| | 3/22/2001 | 1,300 | 98 | 67 | 51 | 104 | <0.5 | 2.3 | < 0.5 | <0.5 | < 0.5 |
| | 6/21/2001 | 34,000 | 5,900 | 6,200 | 340 | 1,550 | 2.4 | 120 | 0.8 | < 0.5 | < 0.5 |
| | 9/26/2001 | 59,000 | 12,000 | 13,000 | 780 | 3,680 | < 8.3 | 990 | < 8.3 | < 8.3 | < 8.3 |
| | Removed fron | | | | | ,,,,,,, | | | | | |
| MW-4 | 2/8/1999 | 15,000 | 670 | 90 | 780 | 940 | NA | <30 | NA | NA | NA |
| 10100-4 | 6/15/2000 | 2,300 | 230 | < 5 | 10 | 94 | <0.5 | 0.88 | 2.1 | <0.5 | <0.5 |
| | 9/22/2000 | 12,000 | 2,800 | 82 | 1,100 | 1,300 | NA | NA | NA | NA | NA |
| | | | 2,800 | | | • | | | | | |
| | 12/19/2000 | 2,200 | | 2.9 | 100 | 81.4 | <0.5 | <0.5 | <0.5 | < 0.5 | <0.5 |
| | 3/22/2001 | 5,600 | 1,100 | 13 | 310 | 303 | <0.5 | <0.5 | 1.6 | <0.5 | <0.5 |
| | 6/21/2001 | 11,000 | 2,300 | 26 | 570 | 641 | <0.5 | 1.4 | 3.3 | <0.5 | <0.5 |
| | 9/26/2001 | 17,000 | 7,900 | < 50 | 440 | 581 | < 0.5 | 1.9 | 8.1 | < 0.5 | < 0.5 |
| | Removed fron | n sampling pi I | rogram in Oct | ober 2001 | | | | | | | |
| MW-5 | 2/8/1999 | 4,900 | 780 | 440 | 230 | 370 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 |
| | 6/29/2000 | 3,900 | 1,500 | 28 | 330 | 260 | < 0.5 | 36 | < 0.5 | < 0.5 | < 0.5 |
| | 9/27/2000 | 16,000 | 4,300 | 3,100 | 420 | 1,600 | NA | NA | NA | NA | NA |
| | 12/19/2000 | 21,000 | 3,200 | 1,100 | 1,100 | 1,300 | <4.2 | 15 | <4.2 | <4.2 | <4.2 |
| | 3/22/2001 | 6,200 | 1,500 | 360 | 310 | 288 | < 0.5 | 3.3 | < 0.5 | < 0.5 | < 0.5 |
| | 6/21/2001 | 18,000 | 3,400 | 2,300 | 350 | 1,020 | < 0.5 | 21 | < 0.5 | < 0.5 | < 0.5 |
| | 9/26/2001 | 5,100 | 2,400 | 1,200 | < 10 | 460 | < 3.6 | 22 | < 3.6 | < 3.6 | < 3.6 |
| | Removed from | n sampling p | rogram in Oct | ober 2001 | | | | | | | |
| MW-6 | 6/15/2000 | 1,100 | 3.8 | 2.2 | 2.1 | 4.8 | < 0.5 | 0.78 | < 0.5 | < 0.5 | < 0.5 |
| | 9/22/2000 | 71 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | NA | NA | NA | NA | NA |
| | 12/19/2000 | 320 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 3/21/2001 | 820 | < 0.5 | < 0.5 | 1.4 | 0.52 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 6/21/2001 | 420 | < 0.5 | < 0.5 | 0.59 | 1 | < 0.5 | 0.9 | < 0.5 | < 0.5 | < 0.5 |
| | 9/25/2001 | 760 | < 0.5 | < 0.5 | < 0.5 | 2.9 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 12/3/2001 | 72 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | 1.6 | < 0.5 | < 0.5 | < 0.5 |
| | 3/25/2001 | 1,200 | 22 | 8.0 | 5.7 | 13.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 6/28/2002 | 1,200 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 < 0.5 | 0.6 | < 0.5 < 0.5 | < 0.5 | < 0.5 < 0.5 |
| | | | | | | | | | | | |
| | 9/11/2002 | 120 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 12/16/2002 | 62 | < 0.5 | 0.54 | 3.0 | 8.39 | 0.7 | 1 | < 0.5 | < 0.5 | < 0.5 |
| | | Not Sample | | . 0. 5 | . 0.5 | . 0. 5 | | | | | . 6. 5 |
| | 6/24/2003 | 130 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 9/26/2003 | <50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | 0.7 | < 0.5 | < 0.5 | < 0.5 |
| | 12/16/2003 | <50 | < 0.5 | < 0.5 | < 0.5 | 0.88 | 1.7 | < 0.5 | 0.6 | <0.5 | <0.5 |





| | | T | | | | Total | | 1,2- | cis-1,2- | trans-1,2- | |
|----------|------------------------|-------------|----------------|----------------|--------------------|--------------------|----------------|----------------|----------------|----------------|----------------|
| Well | Date | TPH-g | Benzene | Toluene | Ethylbenzene | Xylenes | TCE | DCA | DCE | DCE | VC |
| Location | Sampled | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) |
| MW-6 | 4/6/2004 | 260 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | <0.5 | < 0.5 | <0.5 | <0.5 | <0.5 |
| 11111-0 | 6/23/2004 | 63 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | <0.5 | 0.8 | <0.5 | <0.5 | <0.5 |
| | 9/15/2004 | <50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | <0.5 | < 0.5 | <0.5 | <0.5 | <0.5 |
| | 12/16/2004 | 240 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 3/22/2005 | 420 | < 0.5 | < 0.5 | < 0.5 | 0.95 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 6/24/2005 | 91 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 9/13/2005 | <50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 12/2/2005 | <50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | 0.7 | < 0.5 | < 0.5 | < 0.5 |
| | 3/2/2006 | 120 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 6/15/2006 | 51 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 9/14/2006 | 57 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 1/11/2007 | <50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 4/9/2007 | <50 | <0.5 | <0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 9/17/2007 | <50 | < 0.5 | <0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 12/19/2007 | <50 | < 0.5 | 0.51 | < 0.5 | 0.96 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 3/11/2008 | 64 Y | <0.5 | <0.5 | <0.5 | <0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 6/10/2008 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 9/9/2008 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 12/2/2008 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | 0.6 | <0.5 | <0.5 | <0.5 |
| MW-7 | 6/15/2000 | 1,000 | 250 | < 10 | <10 | 16 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 9/22/2000 | <50 | 2 | < 0.5 | < 0.5 | < 0.5 | NA | NA | NA | NA | NA |
| | 12/19/2000 | <50 | 1.6 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 3/21/2001 | 160 | 59 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 6/21/2001 | <50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 9/25/2001 | < 50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 12/3/2001 | 82 | 24 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 3/25/2002 | <50 | 0.56 | 0.75 | < 0.5 | 0.69 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 6/28/2002 | <50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 9/11/2002 | <50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 12/16/2002 | <50 | < 0.5 | < 0.5 | 1.6 | 3.7 | 0.5 | <0.5 | <0.5 | <0.5 | <0.5 |
| | 3/28/2003 | <50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 6/24/2003 | <50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 9/26/2003 | <50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 12/16/2003 | <50 | < 0.5 | < 0.5 | < 0.5 | 0.75 | 1.8 | < 0.5 | 0.6 | < 0.5 | < 0.5 |
| | 4/6/2004 | <50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 6/23/2004 | <50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 9/15/2004 | <50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 12/16/2004 | <50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 3/22/2005 | Not Sampled | | | | | | | | | |
| | 6/24/2005 9/12/2005 | Not Sampled | - O E | - O F | - O F | - O F | - O E | - O F | - O F | ∠O.F | , O.F. |
| | 9/12/2005 | <50 <50 | < 0.5 < 0.5 | < 0.5 < 0.5 | < 0.5 < 0.5 | < 0.5 < 0.5 | < 0.5 < 0.5 | < 0.5 < 0.5 | < 0.5 < 0.5 | < 0.5 < 0.5 | < 0.5 < 0.5 |
| | 3/2/2005 | <50 <50 | < 0.5 < 0.5 | < 0.5 < 0.5 | < 0.5 < 0.5 | < 0.5 < 0.5 | < 0.5 < 0.5 | < 0.5 < 0.5 | < 0.5 < 0.5 | < 0.5 < 0.5 | < 0.5 < 0.5 |
| | 6/15/2006 | <50 <50 | < 0.5 | < 0.5 | < 0.5 < 0.5 | 0.62 | < 0.5 | < 0.5 | < 0.5 < 0.5 | < 0.5 | < 0.5 |
| | 9/14/2006 | <50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 1/11/2007 | <50 <50 | < 0.5 | < 0.5 | < 0.5 | <0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 4/9/2007 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 9/17/2007 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 12/19/2007 | <50 <50 | 0.93 | <0.5 | <0.5 | <0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 3/11/2008 | <50 | 2.6 | <0.5 | <0.5 | <0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 6/10/2008 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 9/9/2008 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 12/2/2008 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 |
| MW-8 | 6/15/2000 | 5,400 | 150 | <5 | 8.9 | 8.7 | 210 | <13 | 1,100 | 73 | 25 |
| INI NA-O | 9/22/2000 | 1,800 | 340 | <5 <2.5 | 8.9 <2.5 | 8.7 <2.5 | NA NA | <13 NA | 1,100 NA | 73 NA | 25 NA |
| | JIZZIZ000 | 1,500 | J-U | ~2.0 | \2. 0 | ~2.0 | 11/7 | 14/7 | 14/7 | INA | INA |





| | | | | | | Total | | 1,2- | cis-1,2- | trans-1,2- | |
|----------|------------|------------------|---------|----------------|--------------|----------------|---------------|---------------|---------------|-------------|-------------|
| Well | Date | TPH-g | Benzene | Toluene | Ethylbenzene | Xylenes | TCE | DCA | DCE | DCE | VC |
| Location | Sampled | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) |
| | | | | | | | | | | | |
| MW-8 | 12/19/2000 | 2,700 | 410 | <2.5 | 4.8 | <2.5 | 130 | 9.1 | 1,000 | 67 | 48 |
| | 3/21/2001 | 3,500 | 530 | <2.5 | 21 | <2.5 | 32 | <3.6 | 760 | 39 | 58 |
| | 6/21/2001 | 2,400 | 490 | <2.5 | 29 | <2.5 | 28 | 4.9 | 910 | 48 | 75 |
| | 9/25/2001 | 1,500 | 170 | 4.3 | 1.6 | 2.7 | 36 | 5.0 | 820 | 59 | 53 |
| | 12/3/2001 | 1,200 | 190 | 14 | 2.7 | 11.3 | 100 | <2.5 | 650 | 44 | 31 |
| | 3/25/2002 | 990 | 280 | 7.2 | 1.4 | 6.8 | 10 | 3.6 | 790 | 33 | 49 |
| | 6/28/2002 | 2,200 | 410 | <1.0 | 40 | <1.0 | 18 | 4.9 | 900 | 54 | 80 |
| | 9/11/2002 | 2,000 | 390 | 1.6 | 39 | <1.0 | 17 | <3.6 | 1,000 | 60 | 91 |
| | 12/16/2002 | 95 | 26 | <0.5 | 1 | <0.5 | 17 | 2.2 | 330 | 36 | 4.7 |
| | 3/28/2003 | 1,500 | 400 | <0.5 | 50 | 0.62 | 3.5 | <2.5 | 700 | 39 | 41 |
| | 6/24/2003 | 3,300 | 520 | <0.5 | 58 | 0.63 | 6.4 | 3.7 | 1,000 | 49 | 61 |
| | 9/26/2003 | 1,300 | 280 | 3.9 | 38 | 0.85 | 20 | <3.6 | 890 | 49 | 47 |
| | 12/16/2003 | 1,100 | 310 | <2.5 | 14 | <2.5 | 12 | 4.3 | 1,200 | 53 | 110 |
| | 4/6/2004 | 3,800 | 420 | <0.5 | 53 | 1.2 | 4.4 | 3.7 | 1,100 | 39 | 58 |
| | 6/23/2004 | 4,600 | 570 | 2.9 | 100 | 1.5 | <8.3 | <8.3 | 1,300 | 50 | 80 |
| | 9/15/2004 | 4,900 | 710 | <1.0 | 100 | <1.0 | <7.1 | <7.1 | 1,200 | 49 | 100 |
| | 12/16/2004 | 3,800 | 450 | <0.5 | 75 | 6.5 | <8.3 | <8.3 | 1,500 | 60 | 86 |
| | 3/22/2005 | 1,700 | 120 | <1.0 | 9.8 | <1.0 | <3.6 | <3.6 | 620 | 27 | 38 |
| | 6/24/2005 | 1,400 | 100 | <1.0 | 37 | <1.0 | <5.0 | <5.0 | 770 | 29 | 51 |
| | 9/13/2005 | 2,700 | 250 | <1.0 | 110 | <1.0 | <7.1 | <7.1 | 1,000 | 35 | 60 |
| | 12/2/2005 | 1,500 | 160 | <1.0 | 33 | <1.0 | 13 | <5.0 | 930 | 46 | 80 |
| | 3/2/2006 | 2,000 L | 210 | <0.5 | 36 | <0.5 | <6.3 | <6.3 | 890 | 34 | 50 |
| | 6/15/2006 | 1,400 | 78 | <0.5 | 21 | <0.5 | 6.9 | <5.0 | 700 | 28 | 41 |
| | 9/14/2006 | 1,600 | 120 | <0.5 | 42 | <0.5 | 7.6 | <6.3 | 800 | 37 | 43 |
| | 1/11/2007 | 1,100 Y | 130 | <0.5 | 49 | 1.1 C | <6.3 | <6.3 | 820 | 32 | 58 |
| | 4/9/2007 | 2,200 L | 160 | <0.5 | 65 | 1.1 | <6.3 | <6.3 | 820 | 24 | 55 |
| | 9/17/2007 | 3,300 L Y | 230 | <0.5 | 140 | <0.5 | <6.3 | <6.3 | 900 | 28 | 91 |
| | 12/19/2007 | 3,300 | 280 | <0.5 | 120 | <0.5 | <10 | <10 | 1,200 | 36 | 150 |
| | 3/11/2008 | 1,700 | 180 | 2.1 C | 110 | 3.5 | 1.0 | <0.5 | 890 | 28 | 67 |
| | 6/10/2008 | 4,000 | 300 | 5.0 C | 220 | 3.3 C | <6.3 | <6.3 | 940 | 27 | 70 |
| | 9/9/2008 | 4,100 | 300 | <0.5 | 230 | <0.5 | <6.3 | <6.3 | 1,200 | 36 | 190 |
| | 12/2/2008 | 2,200 | 210 | 1.5 | 91 | 2.8 | <6.3 | <6.3 | 830 | 43 | 200 |
| MW-9 | 12/3/2001 | 90,000 | 15,000 | 15,000 | 2,200 | 9,100 | <10 | <10 | <10 | <10 | <10 |
| 14144-3 | 3/25/2001 | 71,000 | 15,000 | 17,000 | 1,900 | 8,000 | <31 | <31 | <31 | <31 | <31 |
| | 6/28/2002 | 60,000 | 5,800 | 7,400 | 1,100 | 5,400 | <13 | <13 | <13 | <13 | <13 |
| | 9/11/2002 | 57,000 | 8,300 | 6,100 | 340 | 4,700 | <10 | 18 | <10 | <10 | <10 |
| | 12/16/2002 | 29,000 | 5,500 | 3,900 | 300 | 1,860 | <5 | 8.9 | <5 | <5 | <5 |
| | 3/28/2003 | 61,000 | 13,000 | 8,600 | 860 | 4,800 | <20 | <20 | <20 | <20 | <20 |
| | 6/24/2003 | 45,000 | 15,000 | 9,600 | 1,100 | 5,200 | <5 | 10 | <5 | <5 | <5 |
| | 9/26/2003 | 34,000 | 12,000 | 5,600 | 880 | 4,700 | <17 | <17 | <17 | <17 | <17 |
| | 12/16/2003 | 34,000 | 14,000 | 4,900 | 940 | 4,700 | <42 | <42 | <42 | <42 | <42 |
| | 4/6/2004 | 60,000 | 14,000 | 3,100 | 1,300 | 5,500 | <17 | <17 | <17 | <17 | <17 |
| | 6/23/2004 | 53,000 | 12,000 | 2,600 | 1,100 | 4,800 | <20 | <20 | <20 | <20 | <20 |
| | 9/15/2004 | 76,000 | 17,000 | 2,200 | 1,500 | 6,600 | <20 | <20 | <20 | <20 | <20 |
| | 12/16/2004 | 63,000 | 15,000 | 1,700 | 1,300 | 5,900 | <20 | <20 | <20 | <20 | <20 |
| | 3/22/2005 | 66,000 | 13,000 | 2,000 | 1,200 | 5,800 | <17 | <17 | <17 | <17 | <17 |
| | 6/24/2005 | 54,000 | 16,000 | 780 | 1,300 | 5,200 | <20 | <20 | <20 | <20 | <20 |
| | 9/13/2005 | 48,000 | 11,000 | 4,800 | 470 | 4,110 | <17 | <17 | <17 | <17 | <17 |
| | 12/2/2005 | 39,000 | 12,000 | 3,800 | 650 | 3,470 C | <20 | <20 | <20 | <20 | <20 |
| | 3/2/2006 | 51,000 | 12,000 | 3,500 3,500 | 750 | 4,170 C | <20 <20 | <20 <20 | <20 <20 | <20 | <20 <20 |
| | 6/15/2006 | 67,000 | 16,000 | 5,000 | 1,900 | 5,790 | <20 <36 | <20 <36 | <20 <36 | <20 <36 | <20 <36 |
| | 9/14/2006 | 49,000 | 13,000 | 620 | 1,000 | 3,680 | <13 | <13 | <30 <13 | <30 <13 | <13 |
| | 1/11/2007 | 45,000 45,000 | 13,000 | 460 | 1,100 | 3,050 | <13 <17 | <13 <17 | <13 <17 | <13 <17 | <13 <17 |
| | 4/9/2007 | 49,000 | 13,000 | 580 | 1,100 | 3,020 | <17 <17 | <17 <17 | <17 <17 | <17 <17 | <17 |
| | 9/17/2007 | 19,000 | 9,600 | 250 | 1,000 | 3,020 2,540 | <17 <17 | <17 <17 | <17 <17 | <17 | <17 |
| | 12/19/2007 | 44,000 | 9,500 | 170 | 800 | 2,540 1,880 | <20 | <20 | <20 | <20 | <20 |
| | 12/13/2007 | 1 -4,000 | 3,300 | 170 | 000 | 1,000 | <20 | <20 | <20 | ~ ∠U | ~ ∠U |





| | | | | | | Total | | 1,2- | cis-1,2- | trans-1,2- | |
|----------|------------|-------------|--------------|--------------|--------------|--------------|-------------|--------------|--------------|--------------|--------------|
| Well | Date | TPH-g | Benzene | Toluene | Ethylbenzene | Xylenes | TCE | DCA | DCE | DCE | VC |
| Location | Sampled | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) |
| | | | | | | | | | | | |
| MW-9 | 3/11/2008 | 17,000 | 12,000 | 300 | 1,100 | 2,350 | <42 | <42 | <42 | <42 | <42 |
| | 6/10/2008 | 9,500 | 2,500 | 54 | 400 | 494 | <5.0 | <5.0 | <5.0 | <5.0 | <5.0 |
| | 9/9/2008 | 45,000 | 14,000 | 91 | 1,700 | 1,940 | <10 | <10 | <10 | <10 | <10 |
| | 12/2/2008 | 9,000 | 3,200 | 15 | 290 | 417 | <5.0 | <5.0 | 12 | <5.0 | <5.0 |
| MW-10 | 12/3/2001 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 |
| | 3/25/2002 | 51 | 2.5 | 3.6 | 0.53 | 2.27 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 |
| | 6/28/2002 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 |
| | 9/11/2002 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 |
| | 12/16/2002 | <50 | <0.5 | 0.65 | 3.0 | 7.53 | 0.8 | <0.5 | <0.5 | <0.5 | <0.5 |
| | 3/28/2003 | <50 <50 | <0.5 <0.5 | < 0.5 | <0.5 | <0.5 | <0.5 | <0.5 <0.5 | <0.5 | <0.5 <0.5 | <0.5 |
| | | | | | | | | | | | |
| | 6/24/2003 | <50 | <0.5 | < 0.5 | <0.5 | < 0.5 | <0.5 | < 0.5 | < 0.5 | <0.5 | <0.5 |
| | 9/26/2003 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | < 0.5 | <0.5 | <0.5 |
| | 12/16/2003 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | 0.6 | <0.5 | <0.5 | <0.5 | <0.5 |
| | 4/6/2004 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | < 0.5 | <0.5 | <0.5 |
| | 6/23/2004 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | < 0.5 | <0.5 | <0.5 |
| | 9/15/2004 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | < 0.5 | < 0.5 | < 0.5 | <0.5 | <0.5 |
| | 12/16/2004 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | < 0.5 |
| | 3/22/2005 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | < 0.5 |
| | 6/24/2005 | <50 | <0.5 | < 0.5 | < 0.5 | <0.5 | <0.5 | <0.5 | < 0.5 | <0.5 | < 0.5 |
| | 9/12/2005 | <50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 12/2/2005 | <50 | <0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 3/2/2006 | <50 | 0.74 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | <0.5 | < 0.5 |
| | 6/15/2006 | <50 | < 0.5 | < 0.5 | <0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 9/14/2006 | <50 | <0.5 | < 0.5 | <0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 1/11/2007 | <50 | < 0.5 | <0.5 | <0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 4/9/2007 | <50 | < 0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | < 0.5 | < 0.5 | <0.5 |
| | 9/17/2007 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | < 0.5 | <0.5 | <0.5 |
| | 12/19/2007 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 |
| | 3/11/2008 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 |
| | 6/10/2008 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 |
| | 9/9/2008 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 |
| | 12/2/2008 | <50 | 0.56 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 |
| | | | | | | | | | | | |
| MW-11 | 12/3/2001 | 1,600 | 470 | <0.5 | 3.7 | <0.5 | < 0.5 | < 0.5 | < 0.5 | <0.5 | <0.5 |
| | 3/25/2002 | 130 | 11 | 20 | 3.3 | 14.5 | <0.5 | <0.5 | < 0.5 | <0.5 | <0.5 |
| | 6/28/2002 | <50 | 7.7 | <0.5 | <0.5 | <0.5 | 0.6 | <0.5 | < 0.5 | <0.5 | < 0.5 |
| | 9/11/2002 | 120 | 66 | <0.5 | 0.74 | <0.5 | <0.5 | <0.5 | 0.6 | <0.5 | < 0.5 |
| | 12/16/2002 | 160 | 42 | 0.89 | 4.8 | 11.1 | 3.6 | <0.5 | 1.1 | <0.5 | < 0.5 |
| | 3/28/2003 | <50 | <0.5 | < 0.5 | < 0.5 | <0.5 | <0.5 | <0.5 | < 0.5 | <0.5 | <0.5 |
| | 6/24/2003 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | < 0.5 | < 0.5 | < 0.5 | <0.5 | <0.5 |
| | 9/26/2003 | <50 | 1.2 | 0.69 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 12/16/2003 | 91 | 4.7 | < 0.5 | < 0.5 | 0.51 | 2.9 | < 0.5 | 0.9 | 0.6 | < 0.5 |
| | 4/6/2004 | <50 | <0.5 | < 0.5 | < 0.5 | <0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 6/23/2004 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 9/15/2004 | <50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 |
| | 12/16/2004 | <50 | 1.3 | <0.5 | <0.5 | 0.59 | <0.5 | <0.5 | < 0.5 | < 0.5 | <0.5 |
| | 3/22/2005 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | < 0.5 | <0.5 | <0.5 |
| | 6/24/2005 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 |
| | 9/13/2005 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 |
| | 12/2/2005 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 |
| | 3/2/2006 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 |
| | 6/15/2006 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 |
| | 9/14/2006 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 |
| | 1/11/2007 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 |
| | 4/9/2007 | <50 <50 | <0.5 <0.5 | <0.5 <0.5 | <0.5 <0.5 | <0.5 <0.5 | <0.5 | <0.5 <0.5 | <0.5 <0.5 | <0.5 <0.5 | <0.5 <0.5 |
| | | Not Sampled | | \0. 0 | \0. 0 | ~ 0.0 | \0.0 | ~ 0.0 | \0. 0 | ~0.0 | ~ 0.0 |
| | 3/11/2001 | Inor Sample | 4 | | | | | | | | |





| | | | | | | Total | | 1,2- | cis-1,2- | trans-1,2- | |
|----------|-------------------------|-----------|---------------------|--------------|--------------|--------------|------------|--------------|----------|------------|--------------|
| Well | Date | TPH-g | Benzene | Toluene | Ethylbenzene | Xylenes | TCE | DCA | DCE | DCE | VC |
| Location | Sampled | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) | (ug/L) |
| MW-11 | 12/19/2007 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 |
| | 3/11/2008 | 52 Y | <0.5 | <0.5 | <0.5 | <0.5 | < 0.5 | <0.5 | <0.5 | <0.5 | <0.5 |
| | 6/10/2008 | <50 | <0.5 | <0.5 | <0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | <0.5 |
| | 9/9/2008 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | < 0.5 | <0.5 | <0.5 |
| | 12/2/2008 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 |
| MW-12 | 6/28/2002 | 71 | <0.5 | <0.5 | <0.5 | <0.5 | 170 | <0.5 | 42 | 47 | 0.9 |
| 14144-12 | 9/11/2002 | 89 | <0.5 | <0.5 | <0.5 | <0.5 | 180 | <0.5 | 46 | 51 | 0.9 |
| | 12/16/2002 | 130 | <0.5 | 0.9 | 4.2 | 9.9 | 200 | <0.5 <0.5 | 57 | 60 | 0.9 |
| | 3/28/2003 | 110 | <0.5 | <0.5 | < 0.5 | <0.5 | 190 | <0.7 | 53 | 53 | 0.9 |
| | 6/24/2003 | 140 | <0.5 <0.5 | <0.5 | <0.5 <0.5 | <0.5 <0.5 | 220 | <0.7 <1.0 | 58 | 66 | <1.0 |
| | 9/26/2003 | 230 | 2.9 | 1.1 | 3.8 | 6.71 | 210 | <0.7 | 60 | 63 | <0.7 |
| | 12/16/2003 | 120 | <0.5 | <0.5 | <0.5 | 0.65 | 140 | <0.7 | 44 | 44 | <0.7 |
| | 4/6/2004 | 76 | <0.5 | <0.5 | <0.5 | < 0.5 | 160 | <0.5 | 49 | 54 | <0.5 |
| | | | | | | | | | | | |
| | 6/23/2004 9/15/2004 | 99 130 | <0.5 <0.5 | <0.5 <0.5 | <0.5 <0.5 | <0.5 <0.5 | 200 290 | <0.5 <1.7 | 65 73 | 74 83 | <0.5 <1.7 |
| | 9/15/2004 12/16/2004 | 110 | <0.5 0.94 | <0.5 <0.5 | <0.5 <0.5 | <0.5 <0.5 | 290 240 | <1.7 <2.0 | 73 80 | 83 77 | <1.7 <2.0 |
| | 3/22/2005 | | | | | | | | | | |
| | | 61 | <0.5 | <0.5 | <0.5 | <0.5 | 95 | <0.5 | 26 | 42 | <0.5 |
| | 6/24/2005 | 59 | < 0.5 | < 0.5 | <0.5 | < 0.5 | 120 | <1.0 | 31 | 39 | <1.0 |
| | 9/12/2005 | 64 | <0.5 | <0.5 | <0.5 | <0.5 | 130 | <0.7 | 34 | 42 | <0.7 |
| | 12/2/2005 | 80 Y,Z | <0.5 | <0.5 | <0.5 | <0.5 | 170 | <1.0 | 43 | 49 | <1.0 |
| | 3/2/2006 | 54 Y Z | <0.5 | <0.5 | <0.5 | <0.5 | 84 | <0.8 | 27 | 31 | <0.8 |
| | 6/15/2006 | 58 Y,Z | <0.5 | <0.5 | <0.5 | <0.5 | 99 | <0.5 | 30 | 38 | <0.5 |
| | 9/14/2006 | 81 Y Z | <0.5 | <0.5 | <0.5 | <0.5 | 110 | <1.0 | 41 | 47 | <1.0 |
| | 1/11/2007 | 76 Y Z | <0.5 | <0.5 | <0.5 | <0.5 | 140 | <1.0 | 47 | 53 | <1.0 |
| | 4/9/2007 | 70 Y Z | 1.4 | <0.5 | <0.5 | <0.5 | 130 | <1.0 | 43 | 48 | <1.0 |
| | 9/17/2007 | 84 L Y | <0.5 | <0.5 | <0.5 | <0.5 | 160 | <1.0 | 61 | 63 | <1.0 |
| | 12/19/2007 | 68 Y | < 0.5 | <0.5 | <0.5 | <0.5 | 140 | <0.7 | 55 | 57 | <0.7 |
| | 3/11/2008 | 72 Y | <0.5 | <0.5 | <0.5 | <0.5 | 90 | <0.7 | 29 | 32 | <0.7 |
| | 6/10/2008 | 63 Y | <0.5 | <0.5 | <0.5 | <0.5 | 110 | <0.7 | 44 | 44 | <0.7 |
| | 9/9/2008 | 89 Y Z | 1.2 | <0.5 | <0.5 | <0.5 | 140 | <0.7 | 60 | 59 | <0.7 |
| | 12/2/2008 | 65 Y | 0.53 | <0.5 | <0.5 | <0.5 | 98 | <0.5 | 54 | 58 | <0.5 |
| MW-13 | 6/28/2002 | 5,600 | 120 | 55 | 130 | 9.5 | 61 | <0.5 | 430 | 14 | 4.4 |
| | 9/11/2002 | 4,500 | 58 | 7.5 | 150 | 14 | 63 | <0.5 | 410 | 13 | <1.3 |
| | 12/16/2002 | 4,800 | 90 | <0.5 | 85 | 24 | 76 | <0.5 | 250 | 9.4 | 1.8 |
| | 3/28/2003 | 4,400 | 55 | <0.5 | 51 | 14.3 | 85 | < 0.5 | 150 | 13 | 1.8 |
| | 6/24/2003 | 8,300 | 100 | <0.5 | 94 | 12 | 68 | <1.0 | 250 | 19 | 4.2 |
| | 9/26/2003 | 7,200 | 150 | <1.0 | 89 | 57 | 51 | <1.0 | 270 | 23 | 5.1 |
| | 12/16/2003 | 8,100 | 120 | 36 | 72 | 26.6 | 66 | < 0.7 | 240 | 23 | 10 |
| | 4/6/2004 | 3,300 | 22 | <1.0 | 37 | 9.0 | 90 | < 0.5 | 190 | 23 | 8 |
| | 6/23/2004 | 7,000 | 140 | 25 | 88 | 21 | 53 | <2.0 | 350 | 31 | 25 |
| | 9/15/2004 | 6,700 | 84 | <1.0 | 78 | 7.2 | 37 | <1.7 | 300 | 40 | 31 |
| | 12/16/2004 | 4,300 | 61 | < 0.5 | 44 | 11.5 | 69 | <2.0 | 240 | 32 | 15 |
| | 3/22/2005 | 3,000 | 24 | < 0.5 | 20 | 7.6 | 72 | < 0.5 | 120 | 23 | 6.6 |
| | 6/24/2005 | 2,600 | 63 | < 0.5 | 25 | 4.3 | 42 | <1.0 | 150 | 36 | 16 |
| | 9/12/2005 | 2,500 | 20 C | < 0.5 | 33 | 6.7 c | 25 | <1.3 | 170 | 38 | 22 |
| | 12/2/2005 | 4,200 Y | 70 C | < 0.5 | 21 C | 15.5 C | 17 | <1.3 | 140 | 40 | 24 |
| | 3/2/2006 | 3,200 L Y | 67 C | < 0.5 | 27 | 5.19 C | 43 | <0.8 | 110 | 32 | 16 |
| | 6/15/2006 | 3,400 | 92 C | <0.5 | 26 | 3.4 C | 43 | <0.8 | 120 | 39 | 18 |
| | 9/14/2006 | 2,000 | <0.5 | <0.5 | 64 C | 38 C | 15 | <0.8 | 93 | 45 | 17 |
| | 1/11/2007 | 25,000 Y | 44 | <5.0 | 160 | 69 C | 24 | <0.8 | 87 | 45 | 11 |
| | 4/9/2007 | 5,800 Y | 42 C | <5.0 | 41 | 21.2 C | 34 | <0.8 | 82 | 43 | 14 |
| | 9/17/2007 | 3,800 L | 52 C | 4.0 | 25 | 8.2 C | 11 | <0.8 | 56 | 65 | 11 |
| | 12/19/2007 | 8,400 | <0.5 | <0.5 | 41 | 23.2 C | 21 | <0.5 | 77 | 61 | 10 |
| | 3/11/2008 | 6,300 Y | <0.5 | <0.5 | 59 | 8.8 C | 22 | <1.0 | 49 | 41 | 7.4 |
| | 6/10/2008 | 7,000 | 87 C | <0.5 | 37 | 9.0 C | 9.5 | <1.0 | 31 | 51 | 4.7 |

APPENDIX C



HISTORICAL GROUNDWATER ANALYTICAL RESULTS FORMER LEMOINE SAUSAGE FACTORY 630 29TH AVENUE OAKLAND, CALIFORNIA

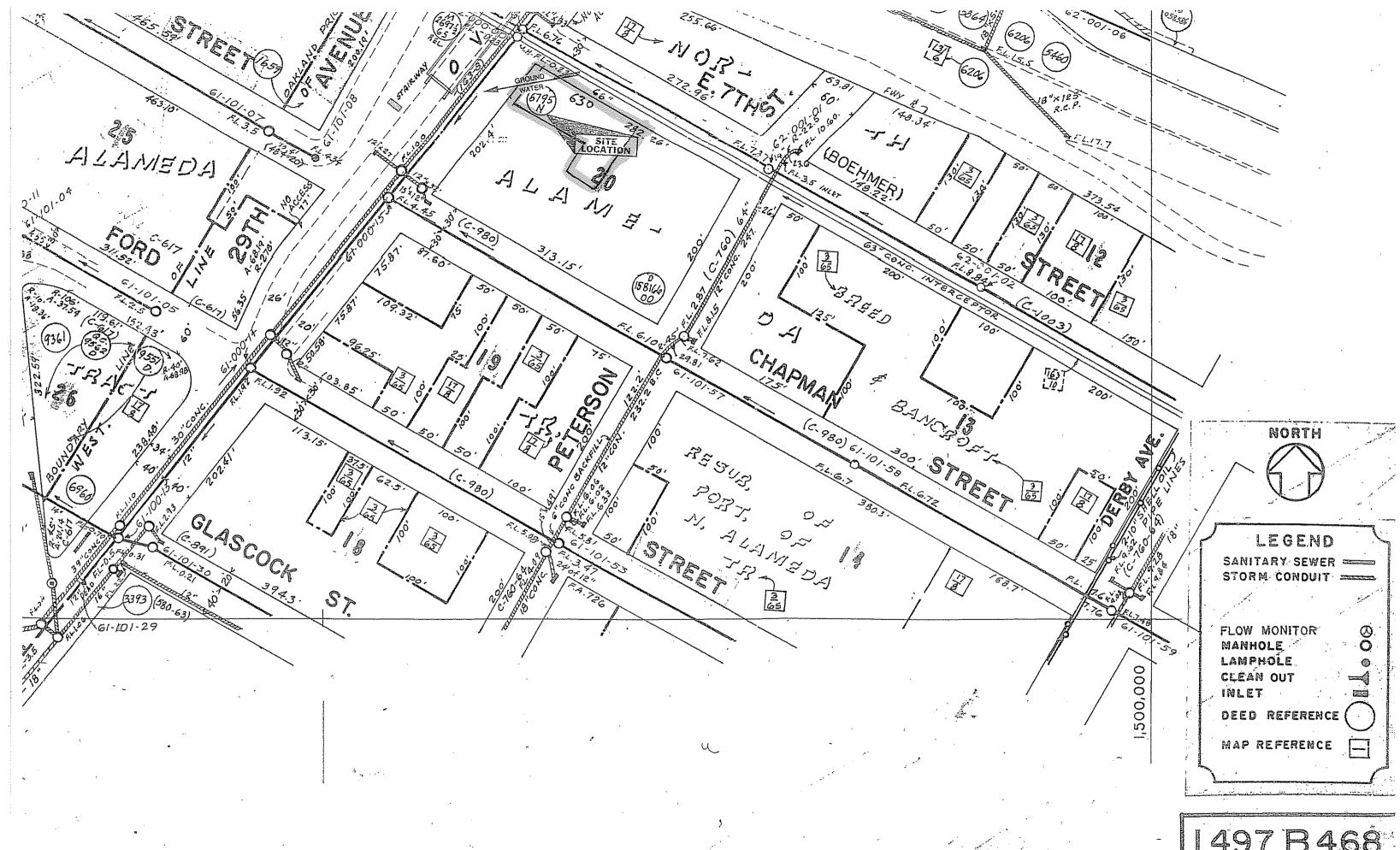
| Well Location | Date Sampled | TPH-g (ug/L) | Benzene (ug/L) | Toluene (ug/L) | Ethylbenzene (ug/L) | Total Xylenes (ug/L) | TCE (ug/L) | 1,2- DCA (ug/L) | cis-1,2- DCE (ug/L) | trans-1,2- DCE (ug/L) | VC (ug/L) |
|------------------|-----------------------|-----------------|-------------------|-------------------|------------------------|----------------------------|---------------|-----------------------|---------------------------|-----------------------------|--------------|
| MW-13 | 9/9/2008 12/2/2008 | 4,300 3,200 | 29 C 55 C | <0.5 <0.5 | 41 27 | 9.5 C 13.2 | 17 16 | <0.5 <0.5 | 52 51 | <0.5 63 | 6.5 5.8 |
| | CDPH MCL | - | 1 | 150 | 300 | 1,750 | 5 | 0.5 | 6 | 10 | 0.5 |

Notes:

- 1. Results are reported in micrograms per liter (μg/L).
- 2. NA refers to Not Analyzed.
- 3. TPH-g refers to Total Petroleum Hydrocarbons as Gasoline.
- 4. TCE refers to Trichloroethene.
- 5. trans-1,2-DCE refers to trans-1,2-dichlororethene.
- 6. cis-1,2-DCE refers to cis-1,2-dichlororethene.
- 7. VC refers to vinyl chloride.
- 8. 1,2-DCA refers to 1,2-dichloroethane.
- 9. Y = Sample exhibits chromatographic pattern which does not resemble standard.
- 10. Z = Sample exhibits unknown single peak or peaks.
- 11. C = Presence confirmed, but RPD between columns exceed 40%.
- 12. L = Lighter hydrocarbons contributed to the quantitation.
- 13. CDPH MCL refers to California Department of Public Health Maximum Contaminant Level.



APPENDIX D UNDERGROUND UTILITY LOCATIONS



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