



Denis L. Brown

November 21, 2005

Jerry Wickham
Alameda County Health Care Services Agency
1131 Harbor Bay Parkway, Suite 250
Alameda, CA 94502-6577

Shell Oil Products US
HSE – Environmental Services
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Re: Site Conceptual Model
Former Shell Service Station
500 40th Street
Oakland, California
SAP Code 129452
Incident No. 97093400

Dear Mr. Wickham:

Attached for your review and comment is a copy of the *Site Conceptual Model* for the above referenced site. Upon information and belief, I declare, under penalty of perjury, that the information contained in the attached document is true and correct.

If you have any questions or concerns, please call me at (707) 865-0251.

Sincerely,

A handwritten signature in black ink that reads "Denis L. Brown". The signature is fluid and cursive, with a long horizontal line extending from the end of the name.

Denis L. Brown
Sr. Environmental Engineer

November 21, 2005

Mr. Jerry Wickham
Alameda County Health Care Services Agency
1131 Harbor Bay Parkway, Suite 250
Alameda, California 94502-6577

Re: **Site Conceptual Model**
Former Shell Service Station
500 40th Street
Oakland, California
Incident No. 97093400
Cambria Project No. 247-1513-007



Dear Mr. Wickham:

Cambria Environmental Technology, Inc. (Cambria) prepared this site conceptual model on behalf of Equilon Enterprises LLC dba Shell Oil Products US (Shell).

SITE BACKGROUND

Location and Current Use

The former retail gasoline station is located on the northwest corner of 40th Street and Telegraph Avenue in Oakland, California (Figure 1). The site is approximately 150 feet long by 125 feet wide. A MacArthur Bay Area Rapid Transit (BART) station parking lot is located across 40th Street from the site. Commercial businesses exist on all corners of the intersection. Surrounding neighborhood development is commercial along both roads. Single-family houses or residences are located on nearby streets. The site was an active service station prior to 1987, but is now occupied by a small retail shopping center (Figure 2).

Investigations

1982-1984 Investigation: Shell reported a fuel leak in July 1982. Between 1982 and 1984, Enviroscience IT (IT) installed 11 groundwater monitoring wells (B-1 through B-11) and 2 recovery wells (R-1 and R-2). No soil samples were analyzed for chemical analyses. Separate-phase hydrocarbons (SPH) were noted intermittently in wells B-2, B-7 and B-8, and regularly in wells B-3 and B-4. IT gauged and removed SPH by manual bailing and periodic batch extraction using a vacuum truck. In November 1983, the underground storage tanks (USTs) were removed

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from the site, and wells R-1 and R-2 were destroyed during UST removal activities. No formal UST-removal report is available. SPH presence and removal history is presented in IT 1982-1984 *Progress Reports #1-11* and 1984-1986 progress letters.

1986 Investigation: On September 23, 1986, Blaine Tech Services (Blaine) collected five soil samples for headspace analysis at 9.5 to 10 feet below grade (fbg) on the west and east ends of the USTs. The soil sample headspace concentrations ranged between 8 and 99 parts per million (ppm) gasoline. Table 1 presents historical soil analytical results. Investigation details are presented in Blaine's September 26, 1986 *Sampling Report*.



According to a July 28, 1987 Pacific Environmental Group, Inc. memorandum to Gettler-Ryan Inc., a retail commercial shopping center building was erected on the property between January and April 1986, covering wells B-2, B-6, B-7, B-9 and B-10. In addition, wells B-1, B-3, B-4, B-5 and B-8 were covered by parking lot and rear driveway pavement. Wells are not reported to have been destroyed.

1989-1990 Investigations: In 1989, Converse Environmental Consultants California (Converse) of San Francisco, California installed on-site monitoring wells MW-2, MW-3, MW-4, and MW-5; off-site monitoring wells OMW-6, OMW-8, OMW-9 and OMW-10; and off-site soil boring SB-1. In 1990, Converse installed on-site monitoring wells MW-8 and EW-1. The maximum total petroleum hydrocarbon as gasoline (TPHg) and benzene concentrations detected in soil samples collected during monitoring well and soil boring installation are 210 ppm and 0.064 ppm, respectively, in off-site monitoring well OMW-9. Monitoring well installation details are presented in Converse's September 12, 1989 *Report of Activities, August 1989* and September 28, 1990 *Report of Activities, Quarter 3, 1990*.

2004 Well Destructions: On November 18, 2004, Gregg Drilling and Testing Inc. of Martinez, California destroyed six wells (EW-1, MW-4, MW-5, OMW-10, OMW-11, and OMW-12) by pressure grouting with neat Portland Type I/II cement. Well destructions were performed in accordance with the Alameda County Public Works well destruction permit and City of Oakland Community and Economic Development encroachment permit. The results are presented in Cambria's January 21, 2005 *Well Destruction Report*.

Quarterly Monitoring: Quarterly groundwater monitoring was initiated at the site in 1990. No SPH has been detected on or off site since 1990. All site monitoring wells have shown decreasing concentration trends since monitoring began. Groundwater monitoring data is included as Attachment A.

SITE CONCEPTUAL MODEL

| | | | |
|----------------------|--|--|--|
| Site Address: | 500 40 th Street | Incident Number: | 97093400 |
| City: | Oakland | Regulator: | Alameda County Health Care Services Agency |
| Item | Evaluation Criteria | Comments/Discussion | |
| 1 | Hydrocarbon Source | | |
| 1.1 | Identify/Describe Release Source and Volume (if known) | In 1982, a leak in the piping over one of the tanks was identified. The release, which occurred sometime between 1980 and 1982, was a leaded and unleaded gasoline mixture, of which at least a portion is known to be Shell gasoline. | |
| 1.2 | Discuss Steps Taken to Stop Release | Underground storage tanks were removed in November 1983. | |
| 2 | Site Characterization | | |
| 2.1 | Current Site Use/Status | The site is a commercial shopping center located at the northeastern corner of the intersection of 40 th Street and Telegraph Avenue in Oakland, California. The shopping center was erected between January and April 1986. | |
| 2.2 | Soil Definition Status | TPHg and benzene are defined to the north, west, and east. TPHg and benzene have been detected at concentrations of up to 210 and 0.064 mg/kg, respectively, south of the site in off-site monitoring wells OMW-9 and OMW-10. | |
| 2.3 | Separate-Phase Hydrocarbon Definition Status | SPH was noted intermittently in wells B-2, B-7 and B-8, and regularly in wells B-3 and B-4. These monitoring wells were installed between 1982 and 1984 and covered in 1986 by a building and parking lot during site redevelopment. Quarterly groundwater monitoring was initiated at the site in 1990. No SPH has been detected on site or off site in groundwater monitoring wells since 1990. | |
| 2.4 | Groundwater Definition Status (BTEX) | Groundwater benzene, toluene, ethylbenzene and xylenes (BTEX) concentrations are defined to the north, west, and east. BTEX are defined to low levels to the south. | |
| 2.5 | BTEX Plume Stability and Concentration Trends | BTEX groundwater concentrations are non-detect in all on-site wells (April 2005). BTEX is present in offsite wells OMW-6 and OMW-13, located west southwest of the former UST complex, with the highest concentrations in well OMW-6 at 18 ppb benzene, 160 ppb ethylene, and 13 ppb xylenes (April 2005). As of April 2005, the BTEX concentrations in these wells have decreased an order of magnitude since 1991-1992. | |
| 2.6 | Groundwater Definition Status (MTBE) | MTBE was not detected in any on-site or off-site monitoring wells during the April 2005 quarterly sampling event. Methyl tertiary butyl ether (MTBE) was last detected in April 2004 at 1.2 ppb in OMW-9. | |



| | | | |
|----------------------|--|---|--|
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| 2.7 | MTBE Plume Stability and Concentration Trends | MTBE concentrations are non-detectable in all on-site and off-site monitoring wells. | |
| 2.8 | Groundwater Flow Direction, Depth Trends and Gradient Trends | Groundwater depth at the site has historically ranged from approximately 7.8 to 14.7 fbg. The prevailing groundwater flow direction is to the west southwest. In April 2005, the gradient was approximately 0.025 feet per foot. | |
| 2.9a | Regional Geology | The site is located in Oakland, east of the San Francisco Bay. The surficial deposits are Holocene-age alluvial fan and fluvial deposits, which are typically medium dense to dense gravely sand or sandy gravels that grade upward to sandy or silty clay. A splay of the Hayward Fault lies approximately 4,500 feet east-northeast of the site. | |
| 2.9b | Topography | The site is flat and is located approximately 80 feet above mean sea level. The topography slopes gently to the west toward San Francisco Bay. | |
| 2.9c | Stratigraphy and Hydrogeology | <p>The silty clays in the uppermost approximately 10-feet beneath the site are underlain by relatively thin sequences of sandy gravel, gravelly clay and silt to approximately 30 fbg. These units are underlain by thicker intervals of gravel and sandy gravel separated by thinner units of silty clay or sand to approximately 45 fbg. Sandy and silty clay underlies these units to a total explored depth of 54 fbg.</p> <p>The prevailing groundwater flow direction is to the west southwest. In April 2005, the gradient was approximately 0.025 feet per foot. Boring logs are included as Attachment B.</p> | |
| 2.10 | Preferential Pathways Analysis | <p>No formal utility survey has been performed. Utilities are typically buried deeper than the shallowest recorded depth to water (7.8 fbg). Therefore, it is possible that utility trenches within and near the site and impacted areas could have served as preferential pathways for chemical migration in groundwater, but there has been no indication that this is occurring.</p> <p>On-site wells installed between 1982 and 1984 were either paved over or built upon and were not properly destroyed; however, there is no known vertical gradient which would cause these wells to act as vertical conduits for chemical migration.</p> | |
| 2.11 | Other Pertinent Issues | None | |
| 3 | Remediation Status | | |
| 3.1 | Remedial Actions Taken | IT reportedly gauged and removed approximately 33.5 pints (4.19 gallons) of SPH by manual bailing and periodic batch groundwater extraction using a vacuum truck between September 1982 and July 1983. | |



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| | | Oxygen releasing compounds (ORC) socks were installed in wells MW-3, MW-5, OMW-6, and OMW-9 between April 2004 and April 2005. ORCs were removed because they had no observable appreciable effect on contaminant concentration. | |
| 3.2 | Area Remediated | SPH was removed from wells B-3 and B-4 between September 1982 and July 1983. | |
| 3.3 | Remediation Effectiveness | Manual SPH bailing and batch groundwater extraction was effective in removing some product. Free product was reported to remain following product removal cessation in July 1983, but no SPH has been detected in on site or off site groundwater monitoring wells since 1990. ORC socks had no observable appreciable effect while installed. | |
| 4 | Well and Sensitive Receptor Survey | | |
| 4.1 | Designated Beneficial Water Use | Beneficial uses of groundwater from the East Bay Plain groundwater basin is designated as an existing municipal, industrial process, industrial service, and agricultural water supply, according to the Regional Water Quality Control Board (RWQCB) Basin Plan. | |
| 4.2 | Shallow Groundwater Use | There is no known use of shallow groundwater near the site. | |
| 4.3 | Deep Groundwater Use | There is no known use of deep groundwater near the site. | |
| 4.4 | Well Survey Results | Cambria's August 2003 Well Survey did not identify any wells within a ½-mile radius of the site. Four wells of unknown use and status were identified within an area between ½-mile and 1-mile radius of the site. | |
| 4.5 | Likelihood of Impact to Wells | Due to distance of the identified wells from the site, it is unlikely that chemicals originating from the site will impact the identified wells. | |
| 4.6 | Likelihood of Impact to Surface Water | Given that the nearest surface water, Glen Echo Creek, is located approximately 3,300 feet southeast and cross gradient from the site, the likelihood of impact to surface water from chemicals originating from the site is low. | |
| 5 | Risk Assessment | | |
| 5.1 | Site Conceptual Exposure Model (current and future uses) | The site is currently a shopping center surrounded by mixed commercial and residential property. A large parking lot, an aboveground BART station, and associated tracks lie in the downgradient direction from the site. Residential lots are primarily cross gradient from the site. The land use is expected to remain commercial on site and commercial and residential | |



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| | | off site. Groundwater in the area is not used as a drinking water source. Remaining hydrocarbon impacts to groundwater are limited to TPHg and BTEX. TPHg is the only hydrocarbon detected in excess of its RWQCB environmental screening level (ESL) during the most recent sampling event. The detections of TPHg greater than the ESL were in off-site wells OMW-6 and OMW-13. OMW-6 is located in 40 th Street and OMW-13 is adjacent to the parking lot of the aboveground BART station, reducing the possibility of vapor intrusion or human exposure to impacted groundwater. A site conceptual figure is included as Figure 3. | |
| 5.2 | Exposure Pathways | Potential exposure pathways include: exposure to construction workers by dermal contact, ingestion, and particulate inhalation from subsurface soils, and inhalation of vapors from impacted soil and groundwater in indoor and outdoor air by on-site commercial and off-site residential occupants. | |
| 5.3 | Risk Assessment Status | A formal risk assessment has not been performed. | |
| 5.4 | Identified Human Exceedances | <p>A formal risk assessment has not been performed.</p> <p>Benzene, ethylbenzene, xylenes toluene, and MTBE groundwater concentration levels do not exceed RWQCB Tier 1 ESLs for groundwater that is not a current or potential source of drinking water. TPHg groundwater ESLs are exceeded in off-site monitoring wells OMW-6 and OMW-13. Benzene, ethylbenzene, toluene, xylenes, MTBE, and TPHg soil concentrations do not exceed the shallow (<3m bgs) or deep (>3m bgs) ESLs where groundwater is not a current or potential source of drinking water.</p> <p>Benzene groundwater concentrations in wells OMW-6 and OMW-13 exceed the California maximum contaminant level (MCL) for drinking water. MTBE groundwater concentrations in well OMW-10 also exceed the California MCL for drinking water. However, groundwater is not currently a drinking water source and it is not expected to be in the future.</p> | |
| 5.5 | Identified Ecological Exceedances | No ecological exceedances have been studied or identified. | |
| 6 | Additional Recommended Data or Tasks | | |
| 6.1 | Consideration of case closure is requested. | | |
| 6.2 | Destruction of remaining on- and off-site wells following closure approval | | |

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|----------------------|-----------------------------|-------------------------|--|
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Known environmental documents for site:

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| <i>Proposal for Investigations of Underground Leakage in Soils and Groundwater</i> (IT Envirosience, July 14, 1982) |
| <i>Sampling Report</i> (Converse Environmental Consultants California, September 26, 1986) |
| <i>Memorandum presenting recommendations for additional work</i> (Pacific Environmental Group, July 28, 1987) |
| <i>Draft Work Plan</i> (Converse Environmental Consultants California, February 24, 1989) |
| <i>Revised Work Plan</i> (Converse Environmental Consultants California, April 7, 1989) |
| <i>Letter report describing the impact of the October 17, 1989 earthquake on the progress of the subsurface investigations</i> (Converse Environmental Consultants California, October 23, 1989) |
| <i>Letter of Intent to Install Interim Groundwater Remediation System</i> (Converse Environmental Consultants California, October 24, 1989) |
| <i>Report of Activities, Quarter 1, 1990</i> (Converse Environmental Consultants California, March 30, 1990) |
| <i>Report of Activities, Quarter 3, 1990</i> (Converse Environmental Consultants California, September 28, 1990) |
| <i>Report of Activities, Quarter 4, 1991</i> (Converse Environmental Consultants California, December 31, 1991) |
| <i>First Quarter 1995 Activities letter</i> (Weiss Associates, April 13, 1995) |
| <i>Quarterly Groundwater Sampling Report 940218-A-1</i> (Blaine Tech Services, March 11, 1994) |
| <i>Quarterly Groundwater Sampling Report 940526-A-1</i> (Blaine Tech Services, June 16, 1994) |
| <i>Quarterly Groundwater Sampling Report 941111-Z-1</i> (Blaine Tech Services, December 8, 1994) |
| <i>Quarterly Monitoring Report – Second Quarter 1995</i> (Enviros, July 12, 1995) |
| <i>Quarterly Monitoring Report – Third Quarter 1995</i> (Enviros, October 13, 1995) |
| <i>Quarterly Monitoring Report – Fourth Quarter 1995</i> (Enviros, January 12, 1996) |
| <i>Quarterly Monitoring Report – First Quarter 1996</i> (Enviros, April 12, 1996) |
| <i>Quarterly Monitoring Report – Second Quarter 1996</i> (Enviros, July 15, 1996) |
| <i>Quarterly Monitoring Report – Third Quarter 1996</i> (Enviros, October 15, 1996) |
| <i>Quarterly Monitoring Report – Fourth Quarter 1996</i> (Enviros, January 15, 1997) |
| <i>Quarterly Monitoring Report – First Quarter 1997</i> (Enviros, April 15, 1997) |
| <i>Quarterly Monitoring Report – Second Quarter 1997</i> (Enviros, July 15, 1997) |
| <i>Quarterly Monitoring Report – Third Quarter 1997</i> (Enviros, October 15, 1997) |
| <i>Quarterly Monitoring Report – Fourth Quarter 1997</i> (Cambria Environmental, January 15, 1998) |
| <i>Quarterly Monitoring Report – First Quarter 1998</i> (Cambria Environmental, April 15, 1998) |
| <i>Quarterly Monitoring Report – Second Quarter 1998</i> (Cambria Environmental, July 15, 1998) |
| <i>Quarterly Monitoring Report – Third Quarter 1998</i> (Cambria Environmental, October 15, 1998) |
| <i>Quarterly Monitoring Report – Fourth Quarter 1998</i> (Cambria Environmental, January 15, 1999) |
| <i>Quarterly Monitoring Report – First Quarter 1999</i> (Cambria Environmental, April 15, 1999) |
| <i>Quarterly Monitoring Report – Second Quarter 1999</i> (Cambria Environmental, July 22, 1999) |
| <i>Third Quarter 1999 Monitoring Report</i> (Cambria Environmental, September 30, 1999) |
| <i>Fourth Quarter 1999 Monitoring Report</i> (Cambria Environmental, January 24, 2000) |
| <i>First Quarter 2000 Monitoring Report</i> (Cambria Environmental, August 2, 2000) |
| <i>Second Quarter 2000 Monitoring Report</i> (Cambria Environmental, August 21, 2000) |

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|---|-----------------------------|-------------------------|--|
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| <i>Third Quarter 2000 Monitoring Report (Cambria Environmental, October 9, 2000)</i> | | | |
| <i>Fourth Quarter 2000 Monitoring Report (Cambria Environmental, February 22, 2001)</i> | | | |
| <i>First Quarter 2001 Monitoring Report (Cambria Environmental, March 27, 2001)</i> | | | |
| <i>Second Quarter 2001 Monitoring Report (Cambria Environmental, June 13, 2001)</i> | | | |
| <i>Third Quarter 2001 Monitoring Report (Cambria Environmental, September 7, 2001)</i> | | | |
| <i>Fourth Quarter 2001 Monitoring Report (Cambria Environmental, January 17, 2002)</i> | | | |
| <i>First Quarter 2002 Monitoring Report (Cambria Environmental, April 22, 2002)</i> | | | |
| <i>Second Quarter 2002 Monitoring Report (Cambria Environmental, August 1, 2002)</i> | | | |
| <i>Third Quarter 2002 Monitoring Report (Cambria Environmental, September 25, 2002)</i> | | | |
| <i>Fourth Quarter 2002 Monitoring Report (Cambria Environmental, December 19, 2002)</i> | | | |
| <i>First Quarter 2003 Monitoring Report (Cambria Environmental, April 29, 2003)</i> | | | |
| <i>Second Quarter 2003 Monitoring Report (Cambria Environmental, June 23, 2003)</i> | | | |
| <i>Third Quarter 2003 Monitoring Report (Cambria Environmental, October 16, 2003)</i> | | | |
| <i>Fourth Quarter 2003 Monitoring Report (Cambria Environmental, January 28, 2004)</i> | | | |
| <i>First Quarter 2004 Monitoring Report (Cambria Environmental, April 14, 2004)</i> | | | |
| <i>Second Quarter 2004 Monitoring Report (Cambria Environmental, July 22, 2004)</i> | | | |
| <i>Fourth Quarter 2004 Monitoring Report (Cambria Environmental, February 24, 2005)</i> | | | |
| <i>Well Destruction Report (Cambria Environmental, January 21, 2005)</i> | | | |
| <i>Second Quarter 2005 Monitoring Report (Cambria Environmental, June 17, 2005)</i> | | | |



CONCLUSIONS AND RECOMMENDATIONS

All site monitoring wells have shown decreasing concentration trends in groundwater samples since groundwater monitoring began, and natural attenuation of hydrocarbon concentrations is expected to continue. MTBE has not been detected in any site wells since the second quarter 2004 monitoring event. TPHg and BTEX concentrations in all on-site wells are below their respective San Francisco RWQCB ESLs for sites at which groundwater is not a current source of drinking water.

Current TPHg concentrations in groundwater from off-site wells OMW-6 and OMW-13 exceed the ESL for sites at which groundwater is not a current source of drinking water. However, the ESL is based on an aquatic habitat criterion, which does not apply at this site. TPHg concentrations in all wells are below the ‘groundwater gross contamination ceiling level’ of 5,000 parts per billion that is based on a nuisance odor criterion and is applicable to this site. In addition, land use downgradient of the site is currently entirely commercial or mixed-use, with a

parking lot, an aboveground BART station, and rapid transit tracks and freeways extending for at least half of a mile in the downgradient direction.

Based on the lack of detectable hydrocarbon concentrations on site, decreasing concentrations that are already below the 'groundwater gross contamination ceiling level,' and the reduced risk of exposure due to the current and anticipated future land use downgradient of the site, Cambria, on behalf of Shell, requests that this site be considered for closure.



CLOSING

If you have any questions regarding the contents of this document, please call Dave Gibbs at (510) 420-3363.

Sincerely,
Cambria Environmental Technology, Inc.

David M. Gibbs P.G.
Project Geologist

Matthew W. Derby, P.E.
Senior Project Engineer

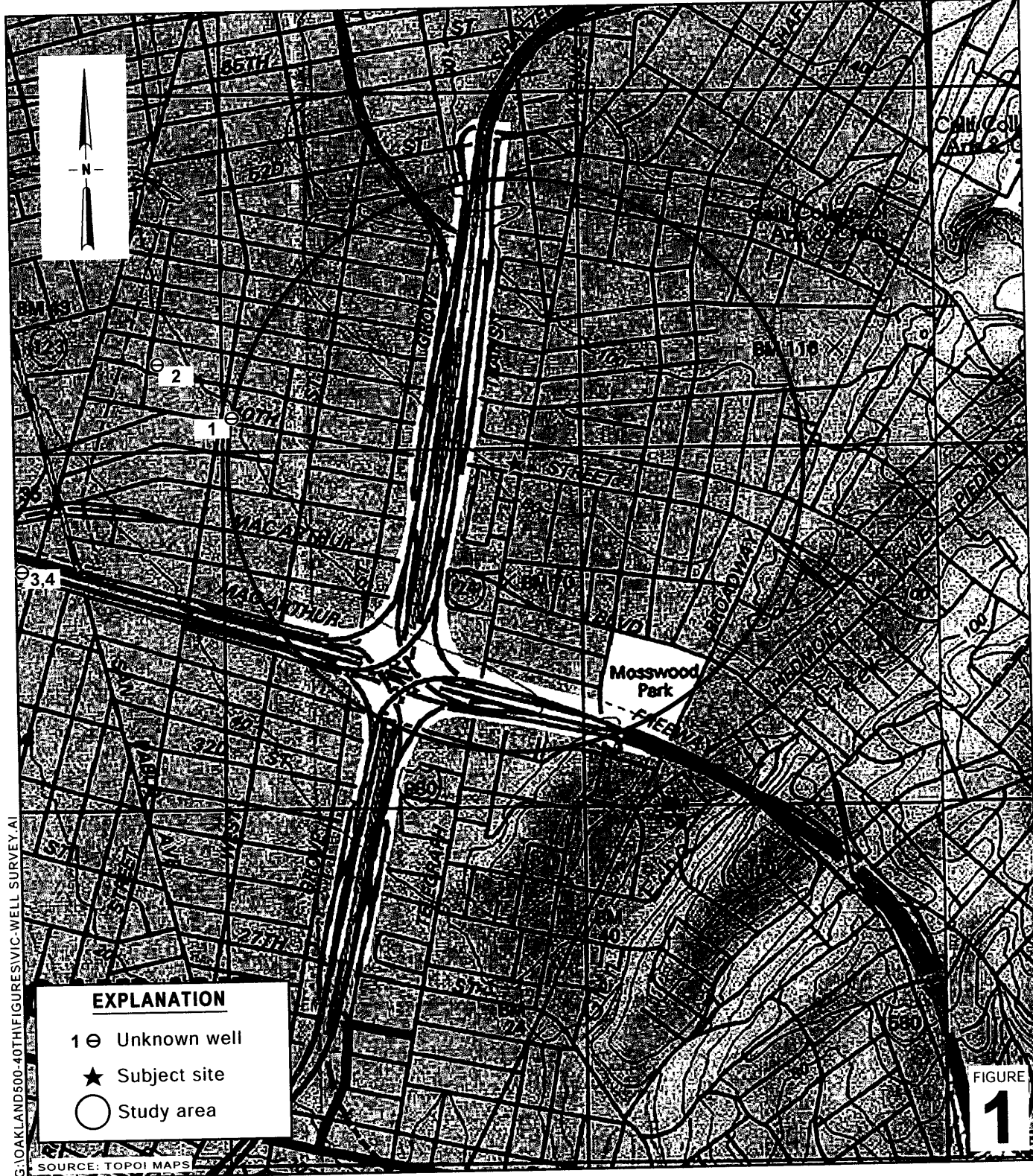


Figures: 1 - Vicinity/Area Well Survey Map
 2 - Site Plan
 3 - Site Conceptual Figure

Table: 1 - Historical Soil Analytical Results

Attachments: A - Groundwater Elevation and Analytical Data
 B - Boring Logs

cc: Denis Brown, Shell Oil Products US, 20945 S. Wilmington Ave., Carson, CA 90810
 Joseph H. Chan and Ivy T. Wong, 21213-B Hawthorne Blvd. #5146, Torrance, CA
 94609



G:\OAKLAND\500-40TH\FIGURES\VIC-WELL SURVEY.A1

EXPLANATION

- 1 ⊕ Unknown well
- ★ Subject site
- Study area

FIGURE 1

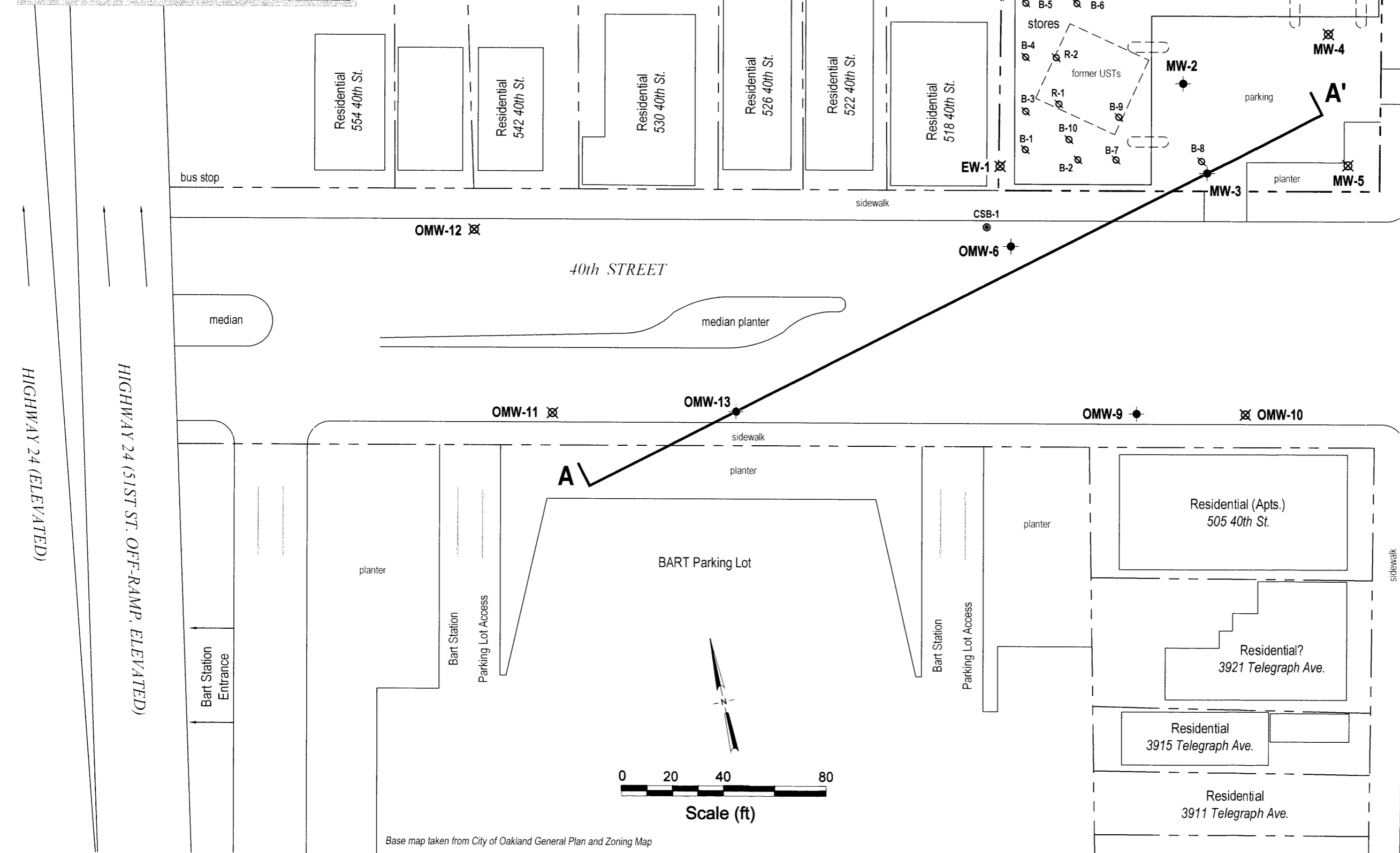
0 1/8 1/4 1/2 1
SCALE : 1" = 1/4 MILE

Former Shell Service Station
 500 40th Street
 Oakland, California
 Incident No.97093400



**Vicinity/Area Well
 Survey Map**
 (1/2-Mile Radius)

| EXPLANATION | |
|-------------|---|
| MW-2 | Monitoring well location |
| MW-4 | Destroyed monitoring well location |
| B-1 | Monitoring wells paved over or built upon |
| CSB-1 | Soil boring location |
| A | Cross section line (see Figure 3) |



Base map taken from City of Oakland General Plan and Zoning Map

TELEGRAPH AVENUE



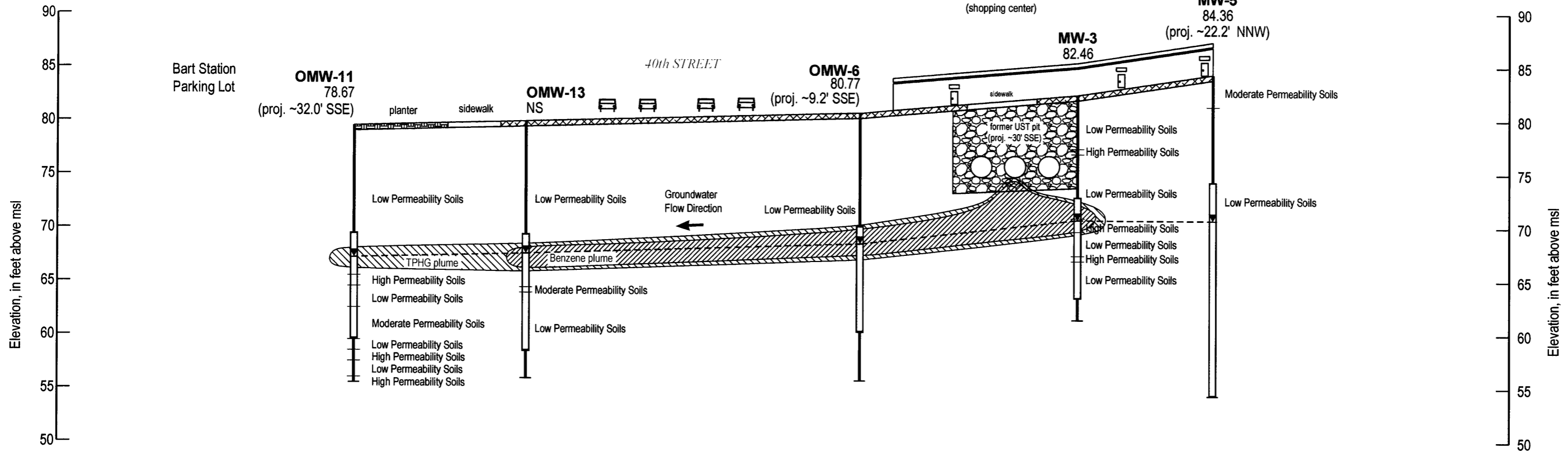
C A M B R I A

FIGURE 2

Former Shell Service Station

500 40th Street
Oakland, California
Incident No. 97093400

A West-Southwest East-Northeast A'



Elevation, in feet above msl

Elevation, in feet above msl

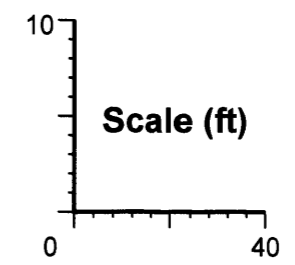
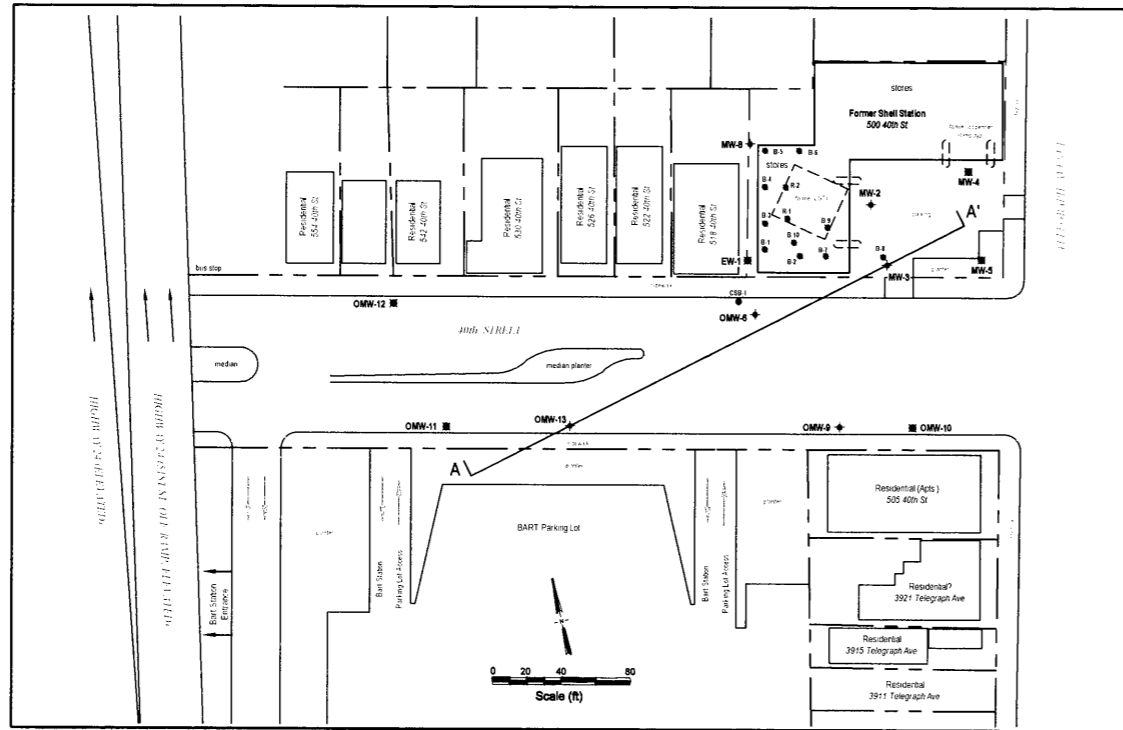


FIGURE 3

Site Conceptual Figure



C A M B R I A

Former Shell Service Station

500 40th Street
Oakland, California
Incident No. 97093400

Table 1. Historical Soil Analytical Results - Former Shell Station, Incident #97093400
500 40th St, Oakland, California

| Sample ID | Sample Depth (fbg) | Sample Date | TPHg | TPHd | (parts per million) | | | | |
|--------------|--------------------|-------------|------------|------------|----------------------|--------------|--------------|---------------|------------|
| | | | | | Benzene | Toluene | Ethylbenzene | Xylene | Total Lead |
| 1 (tank pit) | 10 | 9/25/1986 | 99 | NA | NA | NA | NA | NA | NA |
| 2 (tank pit) | 9.5 | 9/25/1986 | 8 | NA | NA | NA | NA | NA | NA |
| 3 (tank pit) | 10 | 9/25/1986 | 27 | NA | NA | NA | NA | NA | NA |
| 4 (tank pit) | 9.5 | 9/25/1986 | 74 | NA | NA | NA | NA | NA | NA |
| 5 (tank pit) | 10 | 9/25/1986 | 86 | NA | NA | NA | NA | NA | NA |
| EW-1 | 6 | 6/28/1990 | < 1.0 | < 1.0 | < 0.0025 | < 0.0025 | < 0.0025 | 0.0081 | 9.1 |
| EW-1 | 10 | 6/28/1990 | 110 | 4.4 | 0.028 | 0.380 | 0.410 | 1.600 | 3.3 |
| EW-1 | 15 | 6/28/1990 | < 1.0 | < 1.0 | < 0.0025 | 0.005 | < 0.0025 | 0.0029 | 3.0 |
| EW-1 | 20 | 6/28/1990 | < 1.0 | < 1.0 | < 0.0025 | < 0.0025 | < 0.0025 | < 0.0025 | 4.8 |
| MW-2 | 5, 10, 15 | 5/22/89 | < 10 | < 10 | < 0.025 | 0.028 | < 0.075 | < 0.075 | 0.4 |
| MW-3 | 5, 10 | 5/23/89 | < 10 | < 10 | 0.054 | 0.032 | < 0.075 | 0.099 | < 0.2 |
| MW-4 | 5, 10 | 5/23/89 | < 10 | < 10 | < 0.025 | < 0.025 | < 0.075 | < 0.075 | < 0.2 |
| MW-5 | 4 | 9/19/89 | < 10 | < 10 | < 0.025 | < 0.025 | < 0.075 | < 0.075 | 12 |
| MW-5 | 8 | 9/19/89 | < 10 | < 10 | < 0.025 | < 0.025 | < 0.075 | < 0.075 | 5.3 |
| MW-5 | 12 | 9/19/89 | < 10 | < 10 | < 0.025 | < 0.025 | < 0.075 | < 0.075 | 3.3 |
| MW-5 | 16 | 9/19/89 | < 10 | < 10 | < 0.025 | < 0.025 | < 0.075 | < 0.075 | 5.7 |
| OMW-6 | 5 | 10/16/89 | < 10 | 1.0 | < 0.025 | < 0.025 | < 0.075 | < 0.075 | 4.3 |
| OMW-6 | 10 | 10/16/89 | 18 | 17 | 0.028 | 0.040 | 0.10 | 0.45 | 3.2 |
| OMW-6 | 15 | 10/16/89 | < 10 | < 1 | < 0.025 | < 0.025 | < 0.075 | < 0.075 | 3.6 |

Table 1. Historical Soil Analytical Results - Former Shell Station, Incident #97093400
500 40th St, Oakland, California

| Sample ID | Sample Depth (fbg) | Sample Date | TPHg | TPHd | Benzene | (parts per million) | | | Total Lead |
|-----------|--------------------|-------------|------------|-----------|--------------|----------------------|---------------|--------------|------------|
| | | | | | | Toluene | Ethylbenzene | Xylene | |
| MW-8 | 6 | 6/27/90 | < 1.0 | < 1.0 | < 0.0025 | < 0.0025 | < 0.0025 | < 0.0025 | 5.4 |
| MW-8 | 10 | 6/27/90 | < 1.0 | < 1.0 | < 0.0025 | < 0.0025 | < 0.0025 | < 0.0025 | 5.4 |
| MW-8 | 15 | 6/27/90 | < 1.0 | < 1.0 | < 0.0025 | 0.0027 | < 0.0025 | < 0.0025 | 4.4 |
| MW-8 | 20 | 6/27/90 | < 1.0 | < 1.0 | < 0.0025 | < 0.0025 | < 0.0025 | < 0.0025 | 5.8 |
| CSB-1 | 5 | | < 10 | < 1 | < 0.025 | < 0.025 | < 0.075 | < 0.075 | 22 |
| CSB-1 | 10 | | < 10 | < 1 | < 0.025 | < 0.025 | < 0.075 | < 0.075 | 3.2 |
| CSB-1 | 15 | | < 10 | < 1 | < 0.025 | < 0.025 | < 0.075 | < 0.075 | 4.0 |
| CSB-1 | 20 | | < 10 | < 1 | < 0.025 | < 0.025 | < 0.075 | < 0.075 | 4.9 |
| OMW-9 | 5 | 11/13/89 | < 10 | < 1 | < 0.025 | < 0.025 | < 0.075 | < 0.075 | 3.7 |
| OMW-9 | 10 | 11/13/89 | 210 | 40 | 0.064 | 0.46 | 1.1 | 6.3 | 2.6 |
| OMW-9 | 15 | 11/13/89 | 11 | < 1 | < 0.025 | < 0.025 | < 0.075 | < 0.075 | 4.3 |
| OMW-9 | 20 | 11/13/89 | < 10 | < 1 | < 0.025 | < 0.025 | < 0.075 | < 0.075 | 3.1 |
| OMW-10 | 5 | 11/13/89 | < 1 | < 1 | < 0.0025 | < 0.0025 | < 0.0025 | < 0.0025 | 5.5 |
| OMW-10 | 10 | 11/13/89 | < 1 | < 1 | 0.020 | 0.0044 | 0.0084 | 0.024 | 4.3 |
| OMW-10 | 15 | 11/13/89 | < 1 | < 1 | < 0.0025 | < 0.0025 | < 0.0025 | < 0.0025 | 6.9 |
| OMW-11 | 5 | 11/21/91 | < 1 | < 1 | < 0.0025 | < 0.0025 | < 0.0025 | < 0.0025 | NA |
| OMW-11 | 10 | 11/21/91 | < 1 | < 1 | < 0.0025 | < 0.0025 | < 0.0025 | < 0.0025 | NA |
| OMW-11 | 14 | 11/21/91 | < 1 | < 1 | < 0.0025 | < 0.0025 | < 0.0025 | < 0.0025 | NA |
| OMW-12 | 4.5 | 11/20/91 | < 1 | < 1 | < 0.0025 | < 0.0025 | < 0.0025 | < 0.0025 | NA |
| OMW-12 | 10 | 11/20/91 | < 1 | < 1 | < 0.0025 | < 0.0025 | < 0.0025 | < 0.0025 | NA |
| OMW-12 | 15 | 11/20/91 | < 1 | < 1 | < 0.0025 | < 0.0025 | < 0.0025 | < 0.0025 | NA |
| OMW-13 | 5 | 11/21/91 | < 1 | < 1 | < 0.0025 | < 0.0025 | < 0.0025 | < 0.0025 | NA |
| OMW-13 | 9 | 11/21/91 | < 1 | < 1 | < 0.0025 | < 0.0025 | < 0.0025 | < 0.0025 | NA |
| OMW-13 | 15 | 11/21/91 | < 1 | < 1 | < 0.0025 | < 0.0025 | < 0.0025 | < 0.0025 | NA |

Table 1. Historical Soil Analytical Results - Former Shell Station, Incident #97093400
500 40th St, Oakland, California

Abbreviations and Notes:

TBA = Tert-butanol, analyzed by modified EPA Method 8260B.

MTBE = Methyl tertiary-butyl ether. Analyzed by EPA Method 8260B and 8260B C6-12. Highest concentration reported.

DIPE = Di-isopropyl ether, analyzed by modified EPA Method 8260B.

ETBE = Ethyl tert butyl ether, analyzed by modified EPA Method 8260B.

TAME = Tert-amyl methyl ether, analyzed by modified EPA Method 8260B.

Ethanol analyzed by modified EPA Method 8260B.

Methanol analyzed by analyzed by EPA Method 8015Mod.

fbg = Feet below grade.

<n = Below laboratory detection limit of n ppm.

ATTACHMENT A

Groundwater Elevation and Analytical Data

WELL CONCENTRATIONS
Former Shell Service Station
500 40th Street/Telegraph Avenue
Oakland, CA

| Well ID | Date | TPPH (ug/L) | TEPH (ug/L) | B (ug/L) | T (ug/L) | E (ug/L) | X (ug/L) | MTBE 8020 (ug/L) | MTBE 8260 (ug/L) | DIPE (ug/L) | ETBE (ug/L) | TAME (ug/L) | TBA (ug/L) | TOC (MSL) | Depth to Water (ft.) | GW Elevation (MSL) | SPH Thickness (ft.) | DO Reading (ppm) |
|----------|------------|----------------|----------------|-------------|-------------|-------------|-------------|------------------------|------------------------|----------------|----------------|----------------|---------------|--------------|----------------------------|--------------------------|---------------------------|------------------------|
| EW-1 | 08/06/1991 | 180 | <50 | 5.4 | <0.5 | 0.9 | 0.7 | NA | NA | NA | NA | NA | NA | 78.26 | NA | NA | NA | NA |
| EW-1 | 10/30/1991 | 70 | <50 | 2.6 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 78.26 | 12.72 | 65.54 | NA | NA |
| EW-1 | 02/15/1992 | <50 | NA | 2.1 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 78.26 | NA | NA | NA | NA |
| EW-1 | 03/18/1992 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 78.26 | 11.71 | 66.55 | NA | NA |
| EW-1 | 05/22/1992 | 99 | NA | 4.1 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 78.26 | 12.84 | 65.42 | NA | NA |
| EW-1 | 08/19/1992 | 140 | NA | 6.6 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 78.26 | 13.04 | 65.22 | NA | NA |
| EW-1 | 11/18/1992 | 56 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 78.26 | 12.90 | 65.36 | NA | NA |
| EW-1 | 02/11/1993 | 63 | NA | <0.5 | <0.5 | <0.5 | 0.9 | NA | NA | NA | NA | NA | NA | 78.26 | 11.28 | 66.98 | NA | NA |
| EW-1 (D) | 02/11/1993 | 63 | NA | <0.5 | <0.5 | <0.5 | 0.8 | NA | NA | NA | NA | NA | NA | 78.26 | NA | NA | NA | NA |
| EW-1 | 05/19/1993 | 60a | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 78.26 | 12.52 | 65.74 | NA | NA |
| EW-1 | 08/18/1993 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 78.26 | 12.48 | 65.78 | NA | NA |
| EW-1 | 11/17/1993 | 170 | NA | 17 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 78.26 | 12.63 | 65.63 | NA | NA |
| EW-1 (D) | 11/17/1993 | 190 | NA | 17 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 78.26 | NA | NA | NA | NA |
| EW-1 | 02/18/1994 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 78.26 | 11.38 | 66.88 | NA | NA |
| EW-1 | 05/26/1994 | <50 | NA | 3.5 | <0.5 | <0.5 | 0.51 | NA | NA | NA | NA | NA | NA | 78.26 | 12.02 | 66.24 | NA | NA |
| EW-1 | 08/29/1994 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 78.26 | 12.76 | 65.50 | NA | NA |
| EW-1 | 11/11/1994 | 200 | NA | 13 | 0.88 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 78.26 | 11.08 | 67.18 | NA | NA |
| EW-1 | 02/03/1995 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 78.26 | 10.88 | 67.38 | NA | NA |
| EW-1 | 05/07/1995 | 90 | NA | 8.6 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 78.26 | 11.32 | 66.94 | NA | NA |
| EW-1 | 08/02/1995 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 78.26 | 11.76 | 66.50 | NA | NA |
| EW-1 | 11/02/1995 | 240 | NA | 12 | 1.5 | 0.6 | 1.9 | NA | NA | NA | NA | NA | NA | 78.26 | 12.80 | 65.46 | NA | NA |
| EW-1 | 02/24/1996 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 78.26 | 10.15 | 68.11 | NA | NA |
| EW-1 | 05/04/1996 | <50 | NA | 1.4 | <0.50 | <0.50 | <0.50 | 4.1 | NA | NA | NA | NA | NA | 78.26 | 12.26 | 66.00 | NA | NA |
| EW-1 | 09/07/1996 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 78.26 | 13.43 | 64.83 | NA | NA |
| EW-1 | 11/24/1996 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 78.26 | 12.24 | 66.02 | NA | NA |
| EW-1 | 02/23/1997 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 78.26 | 12.20 | 66.06 | NA | NA |
| EW-1 | 05/01/1997 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 78.26 | 12.97 | 65.29 | NA | NA |
| EW-1 | 07/22/1997 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 78.26 | 13.43 | 64.83 | NA | NA |
| EW-1 | 11/04/1997 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <5.0 | NA | NA | NA | NA | NA | 78.26 | 13.20 | 65.06 | NA | NA |
| EW-1 | 01/21/1998 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 78.26 | 10.52 | 67.74 | NA | NA |
| EW-1 | 05/11/1998 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 78.26 | 12.35 | 65.91 | NA | NA |
| EW-1 | 08/11/1998 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 78.26 | 12.90 | 65.36 | NA | NA |

WELL CONCENTRATIONS
Former Shell Service Station
500 40th Street/Telegraph Avenue
Oakland, CA

| Well ID | Date | TPPH (ug/L) | TEPH (ug/L) | B (ug/L) | T (ug/L) | E (ug/L) | X (ug/L) | MTBE 8020 (ug/L) | MTBE 8260 (ug/L) | DIPE (ug/L) | ETBE (ug/L) | TAME (ug/L) | TBA (ug/L) | TOC (MSL) | Depth to Water (ft.) | GW Elevation (MSL) | SPH Thickness (ft.) | DO Reading (ppm) |
|---------|------------|-------------------|----------------|-------------|-------------|-------------|-------------|------------------------|------------------------|----------------|----------------|----------------|---------------|--------------|----------------------------|--------------------------|---------------------------|------------------------|
| EW-1 | 10/20/1998 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 78.26 | 13.34 | 64.92 | NA | NA |
| EW-1 | 02/08/1999 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 78.26 | 9.28 | 68.98 | NA | NA |
| EW-1 | 04/12/1999 | <50.0 | NA | <0.500 | <0.500 | <0.500 | <0.500 | <5.00 | NA | NA | NA | NA | NA | 78.26 | 10.28 | 67.98 | NA | NA |
| EW-1 | 07/27/1999 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 78.26 | 13.04 | 65.22 | NA | NA |
| EW-1 | 10/25/1999 | <50.0 | NA | 0.885 | <0.500 | <0.500 | <0.500 | <5.00 | NA | NA | NA | NA | NA | 78.26 | 13.12 | 65.14 | NA | NA |
| EW-1 | 01/24/2000 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 78.26 | 10.50 | 67.76 | NA | 2.0 |
| EW-1 | 04/24/2000 | <50.0 | NA | <0.500 | <0.500 | <0.500 | <0.500 | <2.50 | NA | NA | NA | NA | NA | 78.26 | 12.05 | 66.21 | NA | 1.8 |
| EW-1 | 07/24/2000 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 78.26 | 13.00 | 65.26 | NA | NA |
| EW-1 | 11/01/2000 | <50.0 | NA | <0.500 | <0.500 | <0.500 | <0.500 | <2.50 | NA | NA | NA | NA | NA | 78.26 | 12.15 | 66.11 | NA | 2.4 |
| EW-1 | 01/19/2001 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 78.26 | 12.24 | 66.02 | NA | 4.4 |
| EW-1 | 04/13/2001 | <50.0 | NA | <0.500 | <0.500 | <0.500 | <0.500 | <2.50 | NA | NA | NA | NA | NA | 78.26 | 12.56 | 65.70 | NA | 5.8 |
| EW-1 | 07/09/2001 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 78.26 | 12.97 | 65.29 | NA | 4.2 |
| EW-1 | 10/18/2001 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 78.26 | 13.69 | 64.57 | NA | 0.3 |
| EW-1 | 01/24/2002 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 78.26 | 11.98 | 66.28 | NA | c |
| EW-1 | 05/10/2002 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 78.26 | 12.68 | 65.58 | NA | 2.3 |
| EW-1 | 07/18/2002 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 78.26 | NA | NA | NA | NA |
| EW-1 | 10/31/2002 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 81.11 | 13.38 | 67.73 | NA | NA |
| EW-1 | 01/30/2003 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.11 | 11.43 | 69.68 | NA | NA |
| EW-1 | 04/17/2003 | <50 | NA | <0.50 | <0.50 | <0.50 | <1.0 | NA | <5.0 | NA | NA | NA | NA | 81.11 | 11.55 | 69.56 | NA | NA |
| EW-1 | 07/17/2003 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.11 | 12.84 | 68.27 | NA | NA |
| EW-1 | 10/16/2003 | <50 | NA | <0.50 | <0.50 | <0.50 | <1.0 | NA | <0.50 | NA | NA | NA | NA | 81.11 | 13.00 | 68.11 | NA | NA |
| EW-1 | 01/14/2004 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.11 | 11.15 | 69.96 | NA | NA |
| EW-1 | 04/14/2004 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.11 | 12.41 | 68.70 | NA | NA |
| EW-1 | 10/29/2004 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.11 | 12.08 | 69.03 | NA | NA |
| EW-1 | 04/14/2005 | Well destroyed | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.11 | NA | NA | NA | NA |
| MW-2 | 08/06/1991 | 1200 | 230 | 59 | 1.1 | 38 | 56 | NA | NA | NA | NA | NA | NA | 80.80 | 12.12 | 68.68 | NA | NA |
| MW-2 | 10/30/1991 | 520 | 300 | 56 | <0.5 | 56 | 100 | NA | NA | NA | NA | NA | NA | 80.80 | 11.70 | 69.10 | NA | NA |
| MW-2 | 02/15/1992 | 2300 | 2200a | 87 | <2.5 | 88 | 150 | NA | NA | NA | NA | NA | NA | 80.80 | NA | NA | NA | NA |
| MW-2 | 03/18/1992 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 80.80 | 11.10 | 69.70 | NA | NA |
| MW-2 | 05/22/1992 | 700 | NA | 24 | 1.0 | 34 | 48 | NA | NA | NA | NA | NA | NA | 80.80 | 12.12 | 68.68 | NA | NA |
| MW-2 | 08/19/1992 | 740 | NA | 21 | <2.5 | 24 | 26 | NA | NA | NA | NA | NA | NA | 80.80 | 12.18 | 68.62 | NA | NA |

WELL CONCENTRATIONS
Former Shell Service Station
500 40th Street/Telegraph Avenue
Oakland, CA

| Well ID | Date | TPPH (ug/L) | TEPH (ug/L) | B (ug/L) | T (ug/L) | E (ug/L) | X (ug/L) | MTBE 8020 (ug/L) | MTBE 8260 (ug/L) | DIPE (ug/L) | ETBE (ug/L) | TAME (ug/L) | TBA (ug/L) | TOC (MSL) | Depth to Water (ft.) | GW Elevation (MSL) | SPH Thickness (ft.) | DO Reading (ppm) |
|----------|------------|-------------------|----------------|-------------|-------------|-------------|-------------|------------------------|------------------------|----------------|----------------|----------------|---------------|--------------|----------------------------|--------------------------|---------------------------|------------------------|
| MW-2 (D) | 08/19/1992 | 840 | NA | 31 | <2.5 | 36 | 43 | NA | NA | NA | NA | NA | NA | 80.80 | NA | NA | NA | NA |
| MW-2 | 11/18/1992 | 920 | NA | 19 | <2.5 | 30 | 51 | NA | NA | NA | NA | NA | NA | 80.80 | 12.03 | 68.77 | NA | NA |
| MW-2 (D) | 11/18/1992 | 870 | NA | 25 | <2.5 | 34 | 52 | NA | NA | NA | NA | NA | NA | 80.80 | NA | NA | NA | NA |
| MW-2 | 02/11/1993 | 1000 | NA | 25 | 6.0 | 43 | 73 | NA | NA | NA | NA | NA | NA | 80.80 | 11.15 | 69.65 | NA | NA |
| MW-2 | 05/19/1993 | 570 | NA | 19 | <0.5 | 37 | 42 | NA | NA | NA | NA | NA | NA | 80.80 | 11.80 | 69.00 | NA | NA |
| MW-2 | 08/18/1993 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 80.80 | NA | NA | NA | NA |
| MW-2 | 11/17/1993 | 250 | NA | 10 | <1.0 | 26 | 20 | NA | NA | NA | NA | NA | NA | 80.80 | 12.00 | 68.80 | NA | NA |
| MW-2 | 02/18/1994 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 80.80 | NA | NA | NA | NA |
| MW-2 | 05/26/1994 | 620 | NA | 17 | 1.4 | 25 | 31 | NA | NA | NA | NA | NA | NA | 80.80 | 11.61 | 69.19 | NA | NA |
| MW-2 (D) | 05/26/1994 | 600 | NA | 16 | 1.2 | 24 | 29 | NA | NA | NA | NA | NA | NA | 80.80 | NA | NA | NA | NA |
| MW-2 | 08/29/1994 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 80.80 | 11.96 | 68.84 | NA | NA |
| MW-2 | 11/11/1994 | 1100 | NA | 28 | 3.1 | 39 | 65 | NA | NA | NA | NA | NA | NA | 80.80 | 10.74 | 70.06 | NA | NA |
| MW-2 | 02/03/1995 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 80.80 | 11.58 | 69.22 | NA | NA |
| MW-2 | 05/07/1995 | 700 | NA | 15 | <0.5 | 35 | 39 | NA | NA | NA | NA | NA | NA | 80.80 | 10.98 | 69.82 | NA | NA |
| MW-2 | 08/02/1995 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 80.80 | 11.90 | 68.90 | NA | NA |
| MW-2 | 11/02/1995 | 140 | NA | 2.3 | <0.5 | 4.4 | 3.7 | NA | NA | NA | NA | NA | NA | 80.80 | 12.12 | 68.68 | NA | NA |
| MW-2 | 02/24/1996 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 80.80 | 10.25 | 70.55 | NA | NA |
| MW-2 | 05/04/1996 | 140 | NA | 2.1 | <0.50 | 4.6 | 4.9 | 6.2 | NA | NA | NA | NA | NA | 80.80 | 11.30 | 69.50 | NA | NA |
| MW-2 | 09/07/1996 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 80.80 | 15.10 | 65.70 | NA | NA |
| MW-2 | 11/24/1996 | 620 | NA | 9.7 | <0.50 | 2.0 | 46 | <2.5 | NA | NA | NA | NA | NA | 80.80 | 12.13 | 68.67 | NA | NA |
| MW-2 | 02/23/1997 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 80.80 | 12.01 | 68.79 | NA | NA |
| MW-2 | 05/01/1997 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 80.80 | 12.94 | 67.86 | NA | NA |
| MW-2 | 07/22/1997 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 80.80 | 13.22 | 67.58 | NA | NA |
| MW-2 | 11/04/1997 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <5.0 | NA | NA | NA | NA | NA | 80.80 | 13.00 | 67.80 | NA | NA |
| MW-2 | 01/21/1998 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 80.80 | 10.47 | 70.33 | NA | NA |
| MW-2 | 05/11/1998 | 59 | NA | 0.56 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 80.80 | 12.49 | 68.31 | NA | NA |
| MW-2 | 08/11/1998 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 80.80 | 12.82 | 67.98 | NA | NA |
| MW-2 | 10/20/1998 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 80.80 | 13.13 | 67.67 | NA | NA |
| MW-2 | 02/08/1999 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 80.80 | 9.10 | 71.70 | NA | NA |
| MW-2 | 04/12/1999 | <50.0 | NA | <0.500 | <0.500 | <0.500 | <0.500 | <5.00 | NA | NA | NA | NA | NA | 80.80 | 10.06 | 70.74 | NA | NA |
| MW-2 | 07/27/1999 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 80.80 | 12.81 | 67.99 | NA | NA |
| MW-2 | 10/25/1999 | <50.0 | NA | <0.500 | <0.500 | <0.500 | <0.500 | <5.00 | NA | NA | NA | NA | NA | 80.80 | 12.89 | 67.91 | NA | NA |

WELL CONCENTRATIONS
Former Shell Service Station
500 40th Street/Telegraph Avenue
Oakland, CA

| Well ID | Date | TPPH (ug/L) | TEPH (ug/L) | B (ug/L) | T (ug/L) | E (ug/L) | X (ug/L) | MTBE 8020 (ug/L) | MTBE 8260 (ug/L) | DIPE (ug/L) | ETBE (ug/L) | TAME (ug/L) | TBA (ug/L) | TOC (MSL) | Depth to Water (ft.) | GW Elevation (MSL) | SPH Thickness (ft.) | DO Reading (ppm) |
|---------|--------------|-------------------|----------------|-------------|-------------|-------------|-------------|------------------------|------------------------|----------------|----------------|----------------|---------------|--------------|----------------------------|--------------------------|---------------------------|------------------------|
| MW-2 | 01/24/2000 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 80.80 | NA | NA | NA | NA |
| MW-2 | 04/24/2000 | <50.0 | NA | <0.500 | <0.500 | <0.500 | <0.500 | <2.50 | NA | NA | NA | NA | NA | 80.80 | 19.35 | 61.45 | NA | 1.8 |
| MW-2 | 07/24/2000 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 80.80 | 12.83 | 67.97 | NA | NA |
| MW-2 | 11/01/2000 | 53.2 | NA | <0.500 | <0.500 | <0.500 | <0.500 | <2.50 | NA | NA | NA | NA | NA | 80.80 | 11.75 | 69.05 | NA | 2.4 |
| MW-2 | 01/19/2001 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 80.80 | 12.22 | 68.58 | NA | 5.8 |
| MW-2 | 04/13/2001 | <50.0 | NA | <0.500 | <0.500 | <0.500 | <0.500 | <2.50 | NA | NA | NA | NA | NA | 80.80 | 12.40 | 68.40 | NA | 3.0 |
| MW-2 | 07/09/2001 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 80.80 | 12.98 | 67.82 | NA | 3.4 |
| MW-2 | 10/18/2001 | 71 | NA | <0.50 | <0.50 | <0.50 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 80.80 | 12.87 | 67.93 | NA | 0.7 |
| MW-2 | 01/24/2002 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 80.80 | 12.13 | 68.67 | NA | 1.4 |
| MW-2 | 05/10/2002 | 74 | NA | <0.50 | <0.50 | <0.50 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 80.80 | 12.69 | 68.11 | NA | 1.4 |
| MW-2 | 07/18/2002 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 80.80 | 12.84 | 67.96 | NA | 1.2 |
| MW-2 | 10/31/2002 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 83.66 | 13.15 | 70.51 | NA | NA |
| MW-2 | 01/30/2003 d | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 83.78 | 11.97 | 71.81 | NA | NA |
| MW-2 | 04/17/2003 | 85 | NA | <0.50 | <0.50 | <0.50 | <1.0 | NA | <5.0 | NA | NA | NA | NA | 83.78 | 12.19 | 71.59 | NA | NA |
| MW-2 | 07/17/2003 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 83.78 | 12.57 | 71.21 | NA | NA |
| MW-2 | 10/16/2003 | <50 | NA | <0.50 | <0.50 | <0.50 | <1.0 | NA | <0.50 | NA | NA | NA | NA | 83.78 | 13.13 | 70.65 | NA | NA |
| MW-2 | 01/14/2004 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 83.78 | 11.58 | 72.20 | NA | NA |
| MW-2 | 04/14/2004 | 73 | NA | <0.50 | <0.50 | <0.50 | <1.0 | NA | <0.50 | NA | NA | NA | NA | 83.78 | 12.65 | 71.13 | NA | NA |
| MW-2 | 10/29/2004 | 180 | NA | <0.50 | <0.50 | <0.50 | <1.0 | NA | <0.50 | <2.0 | <2.0 | <2.0 | <5.0 | 83.78 | 12.39 | 71.39 | NA | NA |
| MW-2 | 04/14/2005 | 150 | NA | <0.50 | <0.50 | <0.50 | <1.0 | NA | <0.50 | NA | NA | NA | NA | 83.78 | 12.14 | 71.64 | NA | NA |

| | | | | | | | | | | | | | | | | | | |
|------|------------|------|------|-----|----|-----|-----|----|----|----|----|----|----|-------|-------|-------|----|----|
| MW-3 | 08/06/1991 | 1900 | 470 | 220 | 57 | 57 | 260 | NA | NA | NA | NA | NA | NA | 79.60 | 11.12 | 68.48 | NA | NA |
| MW-3 | 10/30/1991 | 1900 | 480 | 160 | 28 | 63 | 180 | NA | NA | NA | NA | NA | NA | 79.60 | 10.93 | 68.67 | NA | NA |
| MW-3 | 02/15/1992 | 2300 | 780a | 170 | 31 | 59 | 180 | NA | NA | NA | NA | NA | NA | 79.60 | NA | NA | NA | NA |
| MW-3 | 03/18/1992 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.60 | 10.54 | 69.06 | NA | NA |
| MW-3 | 05/22/1992 | 1500 | NA | 160 | 20 | 44 | 140 | NA | NA | NA | NA | NA | NA | 79.60 | 10.79 | 68.81 | NA | NA |
| MW-3 | 08/19/1992 | 4500 | NA | 210 | 64 | 89 | 310 | NA | NA | NA | NA | NA | NA | 79.60 | 11.23 | 68.37 | NA | NA |
| MW-3 | 11/18/1992 | 2400 | NA | 81 | 14 | 39 | 140 | NA | NA | NA | NA | NA | NA | 79.60 | 11.20 | 68.40 | NA | NA |
| MW-3 | 02/11/1993 | 3000 | NA | 200 | 47 | 90 | 260 | NA | NA | NA | NA | NA | NA | 79.60 | 11.00 | 68.60 | NA | NA |
| MW-3 | 05/19/1993 | 2100 | NA | 240 | 44 | 100 | 330 | NA | NA | NA | NA | NA | NA | 79.60 | 11.16 | 68.44 | NA | NA |
| MW-3 | 08/18/1993 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.60 | 11.35 | 68.25 | NA | NA |
| MW-3 | 11/17/1993 | 1000 | NA | 110 | 13 | 60 | 150 | NA | NA | NA | NA | NA | NA | 79.60 | 11.10 | 68.50 | NA | NA |

WELL CONCENTRATIONS
Former Shell Service Station
500 40th Street/Telegraph Avenue
Oakland, CA

| Well ID | Date | TPPH (ug/L) | TEPH (ug/L) | B (ug/L) | T (ug/L) | E (ug/L) | X (ug/L) | MTBE 8020 (ug/L) | MTBE 8260 (ug/L) | DIPE (ug/L) | ETBE (ug/L) | TAME (ug/L) | TBA (ug/L) | TOC (MSL) | Depth to Water (ft.) | GW Elevation (MSL) | SPH Thickness (ft.) | DO Reading (ppm) |
|----------|------------|-------------------|----------------|-------------|-------------|-------------|-------------|------------------------|------------------------|----------------|----------------|----------------|---------------|--------------|----------------------------|--------------------------|---------------------------|------------------------|
| MW-3 | 02/18/1994 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.60 | 10.76 | 68.84 | NA | NA |
| MW-3 | 05/26/1994 | 1100 | NA | 200 | 17 | 29 | 58 | NA | NA | NA | NA | NA | NA | 79.60 | 11.85 | 67.75 | NA | NA |
| MW-3 | 08/29/1994 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.60 | 10.40 | 69.20 | NA | NA |
| MW-3 | 11/11/1994 | 870 | NA | 130 | 10 | 38 | 87 | NA | NA | NA | NA | NA | NA | 79.60 | 10.04 | 69.56 | NA | NA |
| MW-3 (D) | 11/11/1994 | 1000 | NA | 120 | 10 | 42 | 92 | NA | NA | NA | NA | NA | NA | 79.60 | NA | NA | NA | NA |
| MW-3 | 02/03/1995 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.60 | 10.06 | 69.54 | NA | NA |
| MW-3 | 05/07/1995 | 1300 | NA | 180 | 7.5 | 54 | 110 | NA | NA | NA | NA | NA | NA | 79.60 | 10.11 | 69.49 | NA | NA |
| MW-3 | 08/02/1995 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.60 | 11.02 | 68.58 | NA | NA |
| MW-3 | 11/02/1995 | 370 | NA | 36 | 1.8 | 16 | 21 | NA | NA | NA | NA | NA | NA | 79.60 | 10.97 | 68.63 | NA | NA |
| MW-3 | 02/24/1996 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.60 | 9.61 | 69.99 | NA | NA |
| MW-3 | 05/04/1996 | 460 | NA | 54 | 1.9 | 18 | 28 | 20 | NA | NA | NA | NA | NA | 79.60 | 10.40 | 69.20 | NA | NA |
| MW-3 | 09/07/1996 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.60 | 13.55 | 66.05 | NA | NA |
| MW-3 | 11/24/1996 | 2800 | NA | 290 | <10 | 29 | 39 | <50 | NA | NA | NA | NA | NA | 79.60 | 11.83 | 67.77 | NA | NA |
| MW-3 | 02/23/1997 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.60 | 11.81 | 67.79 | NA | NA |
| MW-3 | 05/01/1997 | 2000 | NA | 120 | <5.0 | 53 | 14 | 60 | NA | NA | NA | NA | NA | 79.60 | 12.34 | 67.26 | NA | NA |
| MW-3 | 07/22/1997 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.60 | 12.86 | 66.74 | NA | NA |
| MW-3 | 11/04/1997 | 470 | NA | 120 | <2.5 | <2.5 | 7.3 | <25 | NA | NA | NA | NA | NA | 79.60 | 12.62 | 66.98 | NA | NA |
| MW-3 | 01/21/1998 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.60 | 10.78 | 68.82 | NA | NA |
| MW-3 | 05/11/1998 | 4400 | NA | 260 | <10 | 220 | 36 | 170 | NA | NA | NA | NA | NA | 79.60 | 11.98 | 67.62 | NA | NA |
| MW-3 | 08/11/1998 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.60 | 12.38 | 67.22 | NA | NA |
| MW-3 | 10/20/1998 | 1700 | NA | 120 | <2.0 | 18 | 7.1 | 19 | NA | NA | NA | NA | NA | 79.60 | 12.55 | 67.05 | NA | NA |
| MW-3 (D) | 10/20/1998 | 1400 | NA | 120 | <5.0 | 18 | <5.0 | 80 | NA | NA | NA | NA | NA | 79.60 | NA | NA | NA | NA |
| MW-3 | 02/08/1999 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.60 | 8.53 | 71.07 | NA | NA |
| MW-3 | 04/12/1999 | 8040 | NA | 554 | 30 | 436 | 624 | 160 | NA | NA | NA | NA | NA | 79.60 | 10.19 | 69.41 | NA | NA |
| MW-3 | 07/27/1999 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.60 | 12.21 | 67.39 | NA | NA |
| MW-3 | 10/25/1999 | 827 | NA | 31 | 2.23 | 14.5 | 6.71 | <10.0 | NA | NA | NA | NA | NA | 79.60 | 12.35 | 67.25 | NA | NA |
| MW-3 | 01/24/2000 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.60 | NA | NA | NA | NA |
| MW-3 | 04/24/2000 | 1470 | NA | 121 | <5.00 | 63.8 | 14.1 | <25.0 | NA | NA | NA | NA | NA | 79.60 | 11.75 | 67.85 | NA | 1.0 |
| MW-3 | 07/24/2000 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.60 | 12.56 | 67.04 | NA | NA |
| MW-3 | 11/01/2000 | 1550 | NA | 143 | <1.25 | 36.4 | 35.3 | 24.4 | NA | NA | NA | NA | NA | 79.60 | 11.48 | 68.12 | NA | 2.2 |
| MW-3 | 01/19/2001 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.60 | 11.83 | 67.77 | NA | 6.6 |
| MW-3 | 04/13/2001 | 2560 | NA | 250 | <10.0 | 108 | <10.0 | 92.1 | NA | NA | NA | NA | NA | 79.60 | 12.08 | 67.52 | NA | 3.6 |

WELL CONCENTRATIONS
Former Shell Service Station
500 40th Street/Telegraph Avenue
Oakland, CA

| Well ID | Date | TPPH (ug/L) | TEPH (ug/L) | B (ug/L) | T (ug/L) | E (ug/L) | X (ug/L) | MTBE 8020 (ug/L) | MTBE 8260 (ug/L) | DIPE (ug/L) | ETBE (ug/L) | TAME (ug/L) | TBA (ug/L) | TOC (MSL) | Depth to Water (ft.) | GW Elevation (MSL) | SPH Thickness (ft.) | DO Reading (ppm) |
|---------|------------|----------------|----------------|-------------|-------------|-------------|-------------|------------------------|------------------------|----------------|----------------|----------------|---------------|--------------|----------------------------|--------------------------|---------------------------|------------------------|
| MW-3 | 07/09/2001 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.60 | 12.68 | 66.92 | NA | 2.8 |
| MW-3 | 10/18/2001 | 2300 | NA | 150 | 0.90 | 42 | 11 | NA | <5.0 | NA | NA | NA | NA | 79.60 | 13.21 | 66.39 | NA | 0.1 |
| MW-3 | 01/24/2002 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.60 | 11.83 | 67.77 | NA | 2.3 |
| MW-3 | 05/10/2002 | 3300 | NA | 77 | 0.60 | 94 | 3.1 | NA | <5.0 | NA | NA | NA | NA | 79.60 | 12.24 | 67.36 | NA | 1.5 |
| MW-3 | 07/18/2002 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.60 | 12.43 | 67.17 | NA | 2.1 |
| MW-3 | 10/31/2002 | 2100 | NA | 89 | 0.57 | 26 | 5.7 | NA | <5.0 | NA | NA | NA | NA | 82.46 | 12.60 | 69.86 | NA | 2.0 |
| MW-3 | 01/30/2003 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 82.46 | 11.76 | 70.70 | NA | 4.6 |
| MW-3 | 04/17/2003 | 2100 | NA | 55 | 0.79 | 100 | 110 | NA | <5.0 | NA | NA | NA | NA | 82.46 | 11.80 | 70.66 | NA | 1.8 |
| MW-3 | 07/17/2003 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 82.46 | 12.28 | 70.18 | NA | 4.0 |
| MW-3 | 10/16/2003 | 120 e | NA | <0.50 | <0.50 | <0.50 | <1.0 | NA | <0.50 | NA | NA | NA | NA | 82.46 | 12.35 | 70.11 | NA | 2.0 |
| MW-3 | 01/14/2004 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 82.46 | 11.35 | 71.11 | NA | 2.9 |
| MW-3 | 04/14/2004 | 130 | NA | 1.6 | <0.50 | 1.5 | <1.0 | NA | <0.50 | NA | NA | NA | NA | 82.46 | 12.12 | 70.34 | NA | 3.4 |
| MW-3 | 10/29/2004 | 490 | NA | 11 | <0.50 | 19 | 18 | NA | <0.50 | <2.0 | <2.0 | <2.0 | <5.0 | 82.46 | 11.67 | 70.79 | NA | 1.2 |
| MW-3 | 04/14/2005 | <50 | NA | <0.50 | <0.50 | <0.50 | <1.0 | NA | <0.50 | NA | NA | NA | NA | 82.46 | 11.65 | 70.81 | NA | 0.1 |

| | | | | | | | | | | | | | | | | | | |
|------|------------|-------------------|-----|------|------|------|------|----|----|----|----|----|----|-------|-------|-------|----|----|
| MW-4 | 08/06/1991 | <50 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 81.00 | 12.36 | 68.64 | NA | NA |
| MW-4 | 10/30/1991 | 50 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 81.00 | 12.02 | 68.98 | NA | NA |
| MW-4 | 02/15/1992 | 90 | NA | 0.9 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 81.00 | NA | NA | NA | NA |
| MW-4 | 03/18/1992 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.00 | 11.34 | 69.66 | NA | NA |
| MW-4 | 05/22/1992 | <50 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 81.00 | 12.35 | 68.65 | NA | NA |
| MW-4 | 08/19/1992 | 82a | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 81.00 | 12.41 | 68.59 | NA | NA |
| MW-4 | 11/18/1992 | 85a | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 81.00 | 12.28 | 68.72 | NA | NA |
| MW-4 | 02/11/1993 | 62a | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 81.00 | 11.65 | 69.35 | NA | NA |
| MW-4 | 05/19/1993 | <50 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 81.00 | 11.92 | 69.08 | NA | NA |
| MW-4 | 08/18/1993 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.00 | NA | NA | NA | NA |
| MW-4 | 11/17/1993 | <50 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 81.00 | 12.24 | 68.76 | NA | NA |
| MW-4 | 02/18/1994 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.00 | 11.69 | 69.31 | NA | NA |
| MW-4 | 05/26/1994 | <50 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 81.00 | 12.00 | 69.00 | NA | NA |
| MW-4 | 11/11/1994 | <50 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 81.00 | 11.30 | 69.70 | NA | NA |
| MW-4 | 02/03/1995 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.00 | 10.99 | 70.01 | NA | NA |
| MW-4 | 05/07/1995 | <50 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 81.00 | 11.69 | 69.31 | NA | NA |
| MW-4 | 08/02/1995 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.00 | 11.72 | 69.28 | NA | NA |

WELL CONCENTRATIONS
Former Shell Service Station
500 40th Street/Telegraph Avenue
Oakland, CA

| Well ID | Date | TPPH (ug/L) | TEPH (ug/L) | B (ug/L) | T (ug/L) | E (ug/L) | X (ug/L) | MTBE 8020 (ug/L) | MTBE 8260 (ug/L) | DIPE (ug/L) | ETBE (ug/L) | TAME (ug/L) | TBA (ug/L) | TOC (MSL) | Depth to Water (ft.) | GW Elevation (MSL) | SPH Thickness (ft.) | DO Reading (ppm) |
|---------|------------|-------------------|----------------|-------------|-------------|-------------|-------------|------------------------|------------------------|----------------|----------------|----------------|---------------|--------------|----------------------------|--------------------------|---------------------------|------------------------|
| MW-4 | 11/02/1995 | <50 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 81.00 | 12.23 | 68.77 | NA | NA |
| MW-4 | 02/24/1996 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.00 | 11.13 | 69.87 | NA | NA |
| MW-4 | 05/04/1996 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 81.00 | 11.80 | 69.20 | NA | NA |
| MW-4 | 09/07/1996 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.00 | 13.27 | 67.73 | NA | NA |
| MW-4 | 11/24/1996 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 81.00 | 12.42 | 68.58 | NA | NA |
| MW-4 | 02/23/1997 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.00 | 12.38 | 68.62 | NA | NA |
| MW-4 | 05/01/1997 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 81.00 | 13.08 | 67.92 | NA | NA |
| MW-4 | 07/22/1997 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.00 | 13.73 | 67.27 | NA | NA |
| MW-4 | 11/04/1997 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.00 | NA | NA | NA | NA |
| MW-4 | 01/21/1998 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.00 | 11.41 | 69.59 | NA | NA |
| MW-4 | 05/11/1998 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.00 | NA | NA | NA | NA |
| MW-4 | 08/11/1998 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.00 | 13.05 | 67.95 | NA | NA |
| MW-4 | 10/20/1998 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 81.00 | 13.30 | 67.70 | NA | NA |
| MW-4 | 02/08/1999 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.00 | 9.19 | 71.81 | NA | NA |
| MW-4 | 04/12/1999 | <50.0 | NA | <0.500 | <0.500 | <0.500 | <0.500 | <5.00 | NA | NA | NA | NA | NA | 81.00 | 9.26 | 71.74 | NA | NA |
| MW-4 | 07/27/1999 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.00 | 12.57 | 68.43 | NA | NA |
| MW-4 | 10/25/1999 | <50.0 | NA | <0.500 | <0.500 | <0.500 | <0.500 | <5.00 | NA | NA | NA | NA | NA | 81.00 | 13.15 | 67.85 | NA | NA |
| MW-4 | 01/24/2000 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.00 | NA | NA | NA | NA |
| MW-4 | 04/24/2000 | <50.0 | NA | <0.500 | <0.500 | <0.500 | <0.500 | 14.5 | NA | NA | NA | NA | NA | 81.00 | 12.55 | 68.45 | NA | 2.5 |
| MW-4 | 07/24/2000 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.00 | 13.31 | 67.69 | NA | NA |
| MW-4 | 11/01/2000 | <50.0 | NA | <0.500 | <0.500 | <0.500 | <0.500 | <2.50 | NA | NA | NA | NA | NA | 81.00 | 12.09 | 68.91 | NA | 2.8 |
| MW-4 | 01/19/2001 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.00 | 12.58 | 68.42 | NA | 8.4 |
| MW-4 | 04/13/2001 | <50.0 | NA | <0.500 | <0.500 | <0.500 | <0.500 | <2.50 | NA | NA | NA | NA | NA | 81.00 | 12.75 | 68.25 | NA | 2.6 |
| MW-4 | 07/09/2001 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.00 | 13.30 | 67.70 | NA | 4.2 |
| MW-4 | 10/18/2001 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 81.00 | 13.45 | 67.55 | NA | 1.4 |
| MW-4 | 01/24/2002 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.00 | 12.55 | 68.45 | NA | c |
| MW-4 | 05/10/2002 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 81.00 | 12.93 | 68.07 | NA | 1.5 |
| MW-4 | 07/18/2002 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.00 | 13.13 | 67.87 | NA | 1.4 |
| MW-4 | 10/31/2002 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 83.92 | 13.40 | 70.52 | NA | NA |
| MW-4 | 01/30/2003 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 83.92 | 12.44 | 71.48 | NA | NA |
| MW-4 | 04/17/2003 | <50 | NA | <0.50 | <0.50 | <0.50 | <1.0 | NA | <5.0 | NA | NA | NA | NA | 83.92 | 12.24 | 71.68 | NA | NA |
| MW-4 | 07/17/2003 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 83.92 | 13.02 | 70.90 | NA | NA |

WELL CONCENTRATIONS
Former Shell Service Station
500 40th Street/Telegraph Avenue
Oakland, CA

| Well ID | Date | TPPH (ug/L) | TEPH (ug/L) | B (ug/L) | T (ug/L) | E (ug/L) | X (ug/L) | MTBE 8020 (ug/L) | MTBE 8260 (ug/L) | DIPE (ug/L) | ETBE (ug/L) | TAME (ug/L) | TBA (ug/L) | TOC (MSL) | Depth to Water (ft.) | GW Elevation (MSL) | SPH Thickness (ft.) | DO Reading (ppm) |
|----------|------------|----------------|----------------|-------------|-------------|-------------|-------------|------------------------|------------------------|----------------|----------------|----------------|---------------|--------------|----------------------------|--------------------------|---------------------------|------------------------|
| MW-4 | 10/16/2003 | <50 | NA | <0.50 | <0.50 | <0.50 | <1.0 | NA | <0.50 | NA | NA | NA | NA | 83.92 | 13.15 | 70.77 | NA | NA |
| MW-4 | 01/14/2004 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 83.92 | 12.20 | 71.72 | NA | NA |
| MW-4 | 04/14/2004 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 83.92 | 12.80 | 71.12 | NA | NA |
| MW-4 | 10/29/2004 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 83.92 | 12.41 | 71.51 | NA | NA |
| MW-4 | 04/14/2005 | Well destroyed | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 83.92 | NA | NA | NA | NA |
| MW-5 | 08/06/1991 | <50 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 81.50 | 13.02 | 68.48 | NA | NA |
| MW-5 | 10/30/1991 | <50 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 81.50 | 12.73 | 68.77 | NA | NA |
| MW-5 | 02/15/1992 | <50 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 81.50 | NA | NA | NA | NA |
| MW-5 | 03/18/1992 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.50 | 12.52 | 68.98 | NA | NA |
| MW-5 | 05/22/1992 | <50 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 81.50 | 13.05 | 68.45 | NA | NA |
| MW-5 | 08/19/1992 | 55a | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 81.50 | 13.04 | 68.46 | NA | NA |
| MW-5 | 11/18/1992 | <50 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 81.50 | 12.91 | 68.59 | NA | NA |
| MW-5 | 02/11/1993 | 59a | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 81.50 | 12.44 | 69.06 | NA | NA |
| MW-5 | 05/19/1993 | <50 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 81.50 | 12.84 | 68.66 | NA | NA |
| MW-5 (D) | 05/19/1993 | <50 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 81.50 | NA | NA | NA | NA |
| MW-5 | 11/17/1993 | <50 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 81.50 | 12.89 | 68.61 | NA | NA |
| MW-5 | 02/18/1994 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.50 | 12.30 | 69.20 | NA | NA |
| MW-5 | 05/26/1994 | <50 | NA | 1.8 | 2.4 | 1.3 | 4.9 | NA | NA | NA | NA | NA | NA | 81.50 | 12.73 | 68.77 | NA | NA |
| MW-5 | 08/29/1994 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.50 | 12.88 | 68.62 | NA | NA |
| MW-5 | 11/11/1994 | <50 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 81.50 | 12.20 | 69.30 | NA | NA |
| MW-5 | 02/03/1995 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.50 | 11.78 | 69.72 | NA | NA |
| MW-5 | 05/07/1995 | <50 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 81.50 | 12.47 | 69.03 | NA | NA |
| MW-5 | 08/02/1995 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.50 | 12.83 | 68.67 | NA | NA |
| MW-5 | 11/02/1995 | <50 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 81.50 | 13.02 | 68.48 | NA | NA |
| MW-5 | 02/24/1996 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.50 | 12.11 | 69.39 | NA | NA |
| MW-5 | 05/04/1996 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 81.50 | 13.20 | 68.30 | NA | NA |
| MW-5 | 09/07/1996 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.50 | 14.24 | 67.26 | NA | NA |
| MW-5 | 11/24/1996 | <50 | NA | <0.50 | <0.5 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 81.50 | 13.58 | 67.92 | NA | NA |
| MW-5 | 02/23/1997 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.50 | 13.54 | 67.96 | NA | NA |
| MW-5 | 05/01/1997 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 81.50 | 14.17 | 67.33 | NA | NA |
| MW-5 | 07/22/1997 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.50 | 14.35 | 67.15 | NA | NA |

WELL CONCENTRATIONS
Former Shell Service Station
500 40th Street/Telegraph Avenue
Oakland, CA

| Well ID | Date | TPPH (ug/L) | TEPH (ug/L) | B (ug/L) | T (ug/L) | E (ug/L) | X (ug/L) | MTBE 8020 (ug/L) | MTBE 8260 (ug/L) | DIPE (ug/L) | ETBE (ug/L) | TAME (ug/L) | TBA (ug/L) | TOC (MSL) | Depth to Water (ft.) | GW Elevation (MSL) | SPH Thickness (ft.) | DO Reading (ppm) |
|----------|------------|----------------|----------------|-------------|-------------|-------------|-------------|------------------------|------------------------|----------------|----------------|----------------|---------------|--------------|----------------------------|--------------------------|---------------------------|------------------------|
| MW-5 | 11/04/1997 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 81.50 | 14.30 | 67.20 | NA | NA |
| MW-5 (D) | 11/04/1997 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 81.50 | NA | NA | NA | NA |
| MW-5 | 01/21/1998 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.50 | 12.86 | 68.64 | NA | NA |
| MW-5 | 05/11/1998 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 81.50 | 13.89 | 67.61 | NA | NA |
| MW-5 | 08/11/1998 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.50 | 14.20 | 67.30 | NA | NA |
| MW-5 | 10/20/1998 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 81.50 | 14.41 | 67.09 | NA | NA |
| MW-5 | 02/08/1999 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.50 | 10.31 | 71.19 | NA | NA |
| MW-5 | 04/12/1999 | <50.0 | NA | <0.500 | <0.500 | <0.500 | <0.500 | <5.00 | NA | NA | NA | NA | NA | 81.50 | 11.30 | 70.20 | NA | NA |
| MW-5 | 07/27/1999 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.50 | 12.63 | 68.87 | NA | NA |
| MW-5 | 10/25/1999 | <50.0 | NA | <0.500 | <0.500 | <0.500 | <0.500 | <5.00 | NA | NA | NA | NA | NA | 81.50 | 14.15 | 67.35 | NA | NA |
| MW-5 | 01/24/2000 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.50 | 11.65 | 69.85 | NA | 1.8 |
| MW-5 | 04/24/2000 | <50.0 | NA | <0.500 | <0.500 | <0.500 | <0.500 | <2.50 | NA | NA | NA | NA | NA | 81.50 | 13.71 | 67.79 | NA | 2.1 |
| MW-5 | 07/24/2000 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.50 | 14.48 | 67.02 | NA | NA |
| MW-5 | 11/01/2000 | <50.0 | NA | <0.500 | <0.500 | <0.500 | <0.500 | <2.50 | NA | NA | NA | NA | NA | 81.50 | 13.26 | 68.24 | NA | 3.2 |
| MW-5 | 01/19/2001 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.50 | 13.68 | 67.82 | NA | 7.8 |
| MW-5 | 04/13/2001 | <50.0 | NA | <0.500 | <0.500 | <0.500 | <0.500 | <2.50 | NA | NA | NA | NA | NA | 81.50 | 13.90 | 67.60 | NA | 3.2 |
| MW-5 | 07/09/2001 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.50 | 14.72 | 66.78 | NA | 4.8 |
| MW-5 | 10/18/2001 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 81.50 | 14.41 | 67.09 | NA | 1.1 |
| MW-5 | 01/24/2002 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.50 | 13.69 | 67.81 | NA | 1.4 |
| MW-5 | 05/10/2002 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 81.50 | 14.05 | 67.45 | NA | 2.2 |
| MW-5 | 07/18/2002 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.50 | 14.23 | 67.27 | NA | 1.2 |
| MW-5 | 10/31/2002 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 84.36 | 14.36 | 70.00 | NA | 2.8 |
| MW-5 | 01/30/2003 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 84.36 | 13.70 | 70.66 | NA | 2.4 |
| MW-5 | 04/17/2003 | <50 | NA | <0.50 | <0.50 | <0.50 | <1.0 | NA | <5.0 | NA | NA | NA | NA | 84.36 | 13.52 | 70.84 | NA | 2.6 |
| MW-5 | 07/17/2003 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 84.36 | 14.13 | 70.23 | NA | 1.6 |
| MW-5 | 10/16/2003 | <50 | NA | <0.50 | <0.50 | <0.50 | <1.0 | NA | <0.50 | NA | NA | NA | NA | 84.36 | 14.21 | 70.15 | NA | 2.1 |
| MW-5 | 01/14/2004 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 84.36 | 14.15 | 70.21 | NA | 3.1 |
| MW-5 | 04/14/2004 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 84.36 | 13.95 | 70.41 | NA | 2.5 |
| MW-5 | 10/29/2004 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 84.36 | 13.63 | 70.73 | NA | 0.8 |
| MW-5 | 04/14/2005 | Well destroyed | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 84.36 | NA | NA | NA | 0.8 |
| OMW-6 | 08/06/1991 | 26000 | 3600 | 910 | 420 | 560 | 1900 | NA | NA | NA | NA | NA | NA | 77.90 | 10.71 | 67.19 | NA | NA |

WELL CONCENTRATIONS
Former Shell Service Station
500 40th Street/Telegraph Avenue
Oakland, CA

| Well ID | Date | TPPH (ug/L) | TEPH (ug/L) | B (ug/L) | T (ug/L) | E (ug/L) | X (ug/L) | MTBE 8020 (ug/L) | MTBE 8260 (ug/L) | DIPE (ug/L) | ETBE (ug/L) | TAME (ug/L) | TBA (ug/L) | TOC (MSL) | Depth to Water (ft.) | GW Elevation (MSL) | SPH Thickness (ft.) | DO Reading (ppm) |
|-----------|------------|-------------------|----------------|-------------|-------------|-------------|-------------|------------------------|------------------------|----------------|----------------|----------------|---------------|--------------|----------------------------|--------------------------|---------------------------|------------------------|
| OMW-6 | 10/30/1991 | 20000 | 4600 | 710 | 240 | 410 | 1700 | NA | NA | NA | NA | NA | NA | 77.90 | 10.50 | 67.40 | NA | NA |
| OMW-6 | 02/15/1992 | 35000 | 27000 | 690 | 420 | 650 | 3000 | NA | NA | NA | NA | NA | NA | 77.90 | NA | NA | NA | NA |
| OMW-6 | 03/18/1992 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.90 | 9.24 | 68.66 | NA | NA |
| OMW-6 | 05/22/1992 | 15000 | NA | 460 | 110 | 300 | 1600 | NA | NA | NA | NA | NA | NA | 77.90 | 10.13 | 67.77 | NA | NA |
| OMW-6 | 08/19/1992 | 24000 | NA | 600 | 300 | 460 | 2000 | NA | NA | NA | NA | NA | NA | 77.90 | 10.16 | 67.74 | NA | NA |
| OMW-6 | 11/18/1992 | 29000 | NA | 480 | 250 | 450 | 2300 | NA | NA | NA | NA | NA | NA | 77.90 | 9.94 | 67.96 | NA | NA |
| OMW-6 | 02/11/1993 | 24000 | NA | 1300 | 250 | 630 | 2400 | NA | NA | NA | NA | NA | NA | 77.90 | 9.20 | 68.70 | NA | NA |
| OMW-6 | 05/19/1993 | 18000 | NA | 750 | 180 | 520 | 2500 | NA | NA | NA | NA | NA | NA | 77.90 | 10.64 | 67.86 | NA | NA |
| OMW-6 | 08/18/1993 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.90 | 10.04 | 67.86 | NA | NA |
| OMW-6 | 11/17/1993 | 14000 | NA | 260 | 64 | 430 | 1900 | NA | NA | NA | NA | NA | NA | 77.90 | 10.12 | 67.78 | NA | NA |
| OMW-6 | 02/18/1994 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.90 | 9.65 | 68.25 | NA | NA |
| OMW-6 | 05/26/1994 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.90 | NA | NA | NA | NA |
| OMW-6 | 08/29/1994 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.90 | NA | NA | NA | NA |
| OMW-6 | 11/11/1994 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.90 | NA | NA | NA | NA |
| OMW-6 | 02/03/1995 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.90 | 8.96 | 68.94 | NA | NA |
| OMW-6 | 05/07/1995 | 11000 | NA | 460 | 82 | 280 | 540 | NA | NA | NA | NA | NA | NA | 77.90 | 8.64 | 69.26 | NA | NA |
| OMW-6 (D) | 05/07/1995 | 14000 | NA | 480 | 61 | 230 | 370 | NA | NA | NA | NA | NA | NA | 77.90 | NA | NA | NA | NA |
| OMW-6 | 08/02/1995 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.90 | 12.09 | 65.81 | NA | NA |
| OMW-6 | 02/24/1996 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.90 | NA | NA | NA | NA |
| OMW-6 | 05/04/1996 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.90 | NA | NA | NA | NA |
| OMW-6 | 09/07/1996 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.90 | 14.45 | 63.45 | NA | NA |
| OMW-6 | 11/24/1996 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.90 | NA | NA | NA | NA |
| OMW-6 | 02/23/1997 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.90 | 13.12 | 64.78 | NA | NA |
| OMW-6 | 05/01/1997 | 17000 | NA | 630 | 52 | 610 | 1300 | 380 | NA | NA | NA | NA | NA | 77.90 | 13.19 | 64.71 | NA | NA |
| OMW-6 (D) | 05/01/1997 | 20000 | NA | 630 | 54 | 630 | 1300 | 500 | <20 | NA | NA | NA | NA | 77.90 | NA | NA | NA | NA |
| OMW-6 | 07/22/1997 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.90 | 13.52 | 64.38 | NA | NA |
| OMW-6 | 11/04/1997 | 10000 | NA | 610 | 23 | 410 | 820 | <100 | NA | NA | NA | NA | NA | 77.90 | 13.12 | 64.78 | NA | NA |
| OMW-6 | 01/21/1998 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.90 | 12.19 | 65.71 | NA | NA |
| OMW-6 | 05/11/1998 | 14000 | NA | 500 | 32 | 900 | 1000 | 110 | NA | NA | NA | NA | NA | 77.90 | 12.71 | 65.19 | NA | NA |
| OMW-6 (D) | 05/11/1998 | 14000 | NA | 490 | <25 | 900 | 980 | 370 | NA | NA | NA | NA | NA | 77.90 | NA | NA | NA | NA |
| OMW-6 | 08/11/1998 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.90 | 13.18 | 64.72 | NA | NA |
| OMW-6 | 10/20/1998 | 7500 | NA | 220 | <20 | 290 | 130 | 120 | NA | NA | NA | NA | NA | 77.90 | 13.11 | 64.79 | NA | NA |

WELL CONCENTRATIONS
Former Shell Service Station
500 40th Street/Telegraph Avenue
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| Well ID | Date | TPPH (ug/L) | TEPH (ug/L) | B (ug/L) | T (ug/L) | E (ug/L) | X (ug/L) | MTBE 8020 (ug/L) | MTBE 8260 (ug/L) | DIPE (ug/L) | ETBE (ug/L) | TAME (ug/L) | TBA (ug/L) | TOC (MSL) | Depth to Water (ft.) | GW Elevation (MSL) | SPH Thickness (ft.) | DO Reading (ppm) |
|---------|------------|-------------------|----------------|-------------|-------------|-------------|-------------|------------------------|------------------------|----------------|----------------|----------------|---------------|--------------|----------------------------|--------------------------|---------------------------|------------------------|
| OMW-6 | 02/08/1999 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.90 | 9.07 | 68.83 | NA | NA |
| OMW-6 | 04/12/1999 | 11300 | NA | 818 | 67.2 | 600 | 690 | 342 | NA | NA | NA | NA | NA | 77.90 | 10.10 | 67.80 | NA | NA |
| OMW-6 | 07/27/1999 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.90 | 12.18 | 65.72 | NA | NA |
| OMW-6 | 10/25/1999 | 11100 | NA | 559 | 21.1 | 329 | 75.7 | <100 | NA | NA | NA | NA | NA | 77.90 | 12.58 | 65.32 | NA | NA |
| OMW-6 | 01/24/2000 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.90 | NA | NA | NA | NA |
| OMW-6 | 04/24/2000 | 12700 | NA | 576 | <10.0 | 452 | 141 | 556 | NA | NA | NA | NA | NA | 77.90 | 12.35 | 65.55 | NA | 1.1 |
| OMW-6 | 07/24/2000 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.90 | 13.08 | 64.82 | NA | NA |
| OMW-6 | 11/01/2000 | 10700 | NA | 179 | 27.5 | 532 | 416 | 304 | 14.6 | NA | NA | NA | NA | 77.90 | 11.91 | 65.99 | NA | 0.6 |
| OMW-6 | 01/19/2001 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.90 | 12.08 | 65.82 | NA | 6.0 |
| OMW-6 | 04/13/2001 | 8650 | NA | 103 | 25.6 | 318 | 207 | 258 | <1.00 | NA | NA | NA | NA | 77.90 | 12.00 | 65.90 | NA | 4.2 |
| OMW-6 | 07/09/2001 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.90 | 11.86 | 66.04 | NA | 5.2 |
| OMW-6 | 10/18/2001 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.90 | NA | NA | NA | NA |
| OMW-6 | 11/01/2001 | 6600 | NA | 85 | <2.0 | 160 | 53 | NA | <20 | NA | NA | NA | NA | 77.90 | 13.23 | 64.67 | NA | 3.4 |
| OMW-6 | 01/24/2002 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.90 | 12.63 | 65.27 | NA | 4.2 |
| OMW-6 | 05/10/2002 | 7600 | NA | 230 | 2.9 | 370 | 25 | NA | <20 | NA | NA | NA | NA | 77.90 | 13.07 | 64.83 | NA | 1.2 |
| OMW-6 | 07/18/2002 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.90 | NA | NA | NA | NA |
| OMW-6 | 10/31/2002 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NS | NA | NA | NA | NA |
| OMW-6 | 11/11/2002 | 6600 | NA | 37 | <5.0 | 42 | <5.0 | NA | <50 | NA | NA | NA | NA | NS | 12.82 | NA | NA | 1.0 |
| OMW-6 | 01/30/2003 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NS | 12.78 | NA | NA | 2.8 |
| OMW-6 | 04/17/2003 | 5500 | NA | 89 | 1.4 | 61 | 20 | NA | <5.0 | NA | NA | NA | NA | NS | 13.02 | NA | NA | 1.6 |
| OMW-6 | 07/17/2003 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NS | 13.08 | NA | NA | 2.0 |
| OMW-6 | 10/16/2003 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NS | NA | NA | NA | NA |
| OMW-6 | 01/14/2004 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NS | 12.69 | NA | NA | 8.9 |
| OMW-6 | 04/14/2004 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NS | NA | NA | NA | NA |
| OMW-6 | 10/29/2004 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NS | 12.21 | NA | NA | 0.1 |
| OMW-6 | 04/14/2005 | 3600 | NA | 18 | <0.50 | 160 | 13 | NA | <0.50 | NA | NA | NA | NA | NS | 12.88 | NA | NA | 0.7 |
| MW-8 | 08/06/1991 | 90 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 79.91 | 13.08 | 66.83 | NA | NA |
| MW-8 | 10/30/1991 | <50 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 79.91 | 12.87 | 67.04 | NA | NA |
| MW-8 | 02/15/1992 | <50 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 79.91 | NA | NA | NA | NA |
| MW-8 | 03/18/1992 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.91 | 11.54 | 68.37 | NA | NA |
| MW-8 | 05/22/1992 | <50 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 79.91 | 12.32 | 67.59 | NA | NA |

WELL CONCENTRATIONS
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500 40th Street/Telegraph Avenue
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| Well ID | Date | TPPH (ug/L) | TEPH (ug/L) | B (ug/L) | T (ug/L) | E (ug/L) | X (ug/L) | MTBE 8020 (ug/L) | MTBE 8260 (ug/L) | DIPE (ug/L) | ETBE (ug/L) | TAME (ug/L) | TBA (ug/L) | TOC (MSL) | Depth to Water (ft.) | GW Elevation (MSL) | SPH Thickness (ft.) | DO Reading (ppm) |
|---------|------------|-------------------|----------------|-------------|-------------|-------------|-------------|------------------------|------------------------|----------------|----------------|----------------|---------------|--------------|----------------------------|--------------------------|---------------------------|------------------------|
| MW-8 | 08/19/1992 | 60 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 79.91 | 12.58 | 67.33 | NA | NA |
| MW-8 | 11/18/1992 | <50 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 79.91 | 12.47 | 67.44 | NA | NA |
| MW-8 | 02/11/1993 | 76a | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 79.91 | 11.02 | 68.89 | NA | NA |
| MW-8 | 05/19/1993 | <50 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 79.91 | 11.78 | 68.13 | NA | NA |
| MW-8 | 08/18/1993 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.91 | 12.22 | 67.69 | NA | NA |
| MW-8 | 11/17/1993 | <50 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 79.91 | 12.25 | 67.66 | NA | NA |
| MW-8 | 02/18/1994 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.91 | 10.56 | 69.35 | NA | NA |
| MW-8 | 05/26/1994 | <50 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 79.91 | 11.30 | 68.61 | NA | NA |
| MW-8 | 08/29/1994 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.91 | 11.90 | 68.01 | NA | NA |
| MW-8 | 11/11/1994 | <50 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 79.91 | 10.12 | 69.79 | NA | NA |
| MW-8 | 02/03/1995 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.91 | 11.64 | 68.27 | NA | NA |
| MW-8 | 05/07/1995 | <50 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 79.91 | 10.77 | 69.14 | NA | NA |
| MW-8 | 08/02/1995 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.91 | 10.92 | 68.99 | NA | NA |
| MW-8 | 11/02/1995 | <50 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 79.91 | 11.93 | 67.98 | NA | NA |
| MW-8 | 02/24/1996 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.91 | NA | NA | NA | NA |
| MW-8 | 05/04/1996 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 79.91 | 11.66 | 68.25 | NA | NA |
| MW-8 | 09/07/1996 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.91 | 9.84 | 70.07 | NA | NA |
| MW-8 | 11/24/1996 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 79.91 | 11.53 | 68.38 | NA | NA |
| MW-8 | 02/23/1997 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.91 | 11.54 | 68.37 | NA | NA |
| MW-8 | 05/01/1997 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 79.91 | 12.37 | 67.54 | NA | NA |
| MW-8 | 07/22/1997 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.91 | 12.73 | 67.18 | NA | NA |
| MW-8 | 11/04/1997 | 50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <5.0 | NA | NA | NA | NA | NA | 79.91 | 12.60 | 67.31 | NA | NA |
| MW-8 | 01/21/1998 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.91 | 9.73 | 70.18 | NA | NA |
| MW-8 | 05/11/1998 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 79.91 | 11.93 | 67.98 | NA | NA |
| MW-8 | 08/11/1998 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.91 | 12.35 | 67.56 | NA | NA |
| MW-8 | 10/20/1998 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 79.91 | 12.88 | 67.03 | NA | NA |
| MW-8 | 02/08/1999 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.91 | 8.79 | 71.12 | NA | NA |
| MW-8 | 04/12/1999 | <50.0 | NA | <0.500 | <0.500 | <0.500 | <0.500 | <5.00 | NA | NA | NA | NA | NA | 79.91 | 9.86 | 70.05 | NA | NA |
| MW-8 | 07/27/1999 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.91 | 12.35 | 67.56 | NA | NA |
| MW-8 | 10/25/1999 | <50.0 | NA | <0.500 | <0.500 | <0.500 | <0.500 | <5.00 | NA | NA | NA | NA | NA | 79.91 | 12.53 | 67.38 | NA | NA |
| MW-8 | 01/24/2000 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.91 | 8.42 | 71.49 | NA | 1.3 |
| MW-8 | 04/24/2000 | <50.0 | NA | <0.500 | <0.500 | <0.500 | <0.500 | <2.50 | NA | NA | NA | NA | NA | 79.91 | 11.49 | 68.42 | NA | 2.0 |

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| Well ID | Date | TPPH (ug/L) | TEPH (ug/L) | B (ug/L) | T (ug/L) | E (ug/L) | X (ug/L) | MTBE 8020 (ug/L) | MTBE 8260 (ug/L) | DIPE (ug/L) | ETBE (ug/L) | TAME (ug/L) | TBA (ug/L) | TOC (MSL) | Depth to Water (ft.) | GW Elevation (MSL) | SPH Thickness (ft.) | DO Reading (ppm) |
|---------|------------|-------------------|----------------|-------------|-------------|-------------|-------------|------------------------|------------------------|----------------|----------------|----------------|---------------|--------------|----------------------------|--------------------------|---------------------------|------------------------|
| MW-8 | 07/24/2000 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.91 | 12.87 | 67.04 | NA | NA |
| MW-8 | 11/01/2000 | <50.0 | NA | <0.500 | <0.500 | <0.500 | <0.500 | <2.50 | NA | NA | NA | NA | NA | 79.91 | 11.19 | 68.72 | NA | 4.0 |
| MW-8 | 01/19/2001 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.91 | 11.62 | 68.29 | NA | 7.0 |
| MW-8 | 04/13/2001 | <50.0 | NA | <0.500 | <0.500 | <0.500 | <0.500 | <2.50 | NA | NA | NA | NA | NA | 79.91 | 11.86 | 68.05 | NA | 4.6 |
| MW-8 | 07/09/2001 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.91 | 12.42 | 67.49 | NA | 6.4 |
| MW-8 | 10/18/2001 | 81 | NA | <0.50 | <0.50 | <0.50 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 79.91 | 13.24 | 66.67 | NA | 2.3 |
| MW-8 | 01/24/2002 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.91 | 11.39 | 68.52 | NA | 3.1 |
| MW-8 | 05/10/2002 | 95 | NA | <0.50 | <0.50 | <0.50 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 79.91 | 12.25 | 67.66 | NA | 2.5 |
| MW-8 | 07/18/2002 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 79.91 | 12.45 | 67.46 | NA | 2.8 |
| MW-8 | 10/31/2002 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 82.34 | NA | NA | NA | NA |
| MW-8 | 11/11/2002 | 110 | NA | <0.50 | <0.50 | <0.50 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 82.34 | 12.03 | 70.31 | NA | NA |
| MW-8 | 01/30/2003 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 82.34 | 11.85 | 70.49 | NA | NA |
| MW-8 | 04/17/2003 | <50 | NA | <0.50 | <0.50 | <0.50 | <1.0 | NA | <5.0 | NA | NA | NA | NA | 82.34 | 11.30 | 71.04 | NA | NA |
| MW-8 | 07/17/2003 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 82.34 | 12.40 | 69.94 | NA | NA |
| MW-8 | 10/16/2003 | <50 | NA | <0.50 | <0.50 | <0.50 | <1.0 | NA | <0.50 | NA | NA | NA | NA | 82.34 | 12.62 | 69.72 | NA | NA |
| MW-8 | 01/14/2004 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 82.34 | 11.85 | 70.49 | NA | NA |
| MW-8 | 04/16/2004 | <50 | NA | <0.50 | <0.50 | <0.50 | <1.0 | NA | <0.50 | NA | NA | NA | NA | 82.34 | 12.00 | 70.34 | NA | NA |
| MW-8 | 10/29/2004 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 82.34 | 11.66 | 70.68 | NA | NA |
| MW-8 | 04/14/2005 | <50 | NA | <0.50 | <0.50 | <0.50 | <1.0 | NA | <0.50 | NA | NA | NA | NA | 82.34 | 10.81 | 71.53 | NA | NA |

| | | | | | | | | | | | | | | | | | | |
|-------|------------|-------------------|-------|----|-----|-----|-----|----|----|----|----|----|----|-------|-------|-------|----|----|
| OMW-9 | 08/06/1991 | 3900 | 190 | 58 | 8.8 | 80 | 220 | NA | NA | NA | NA | NA | NA | 77.71 | 10.38 | 67.33 | NA | NA |
| OMW-9 | 10/30/1991 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.71 | NA | NA | NA | NA |
| OMW-9 | 03/18/1992 | 1800a | 210 | 84 | 11 | 49 | 60 | NA | NA | NA | NA | NA | NA | 77.71 | 8.76 | 68.95 | NA | NA |
| OMW-9 | 05/20/1992 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.71 | NA | NA | NA | NA |
| OMW-9 | 08/19/1992 | 4600 | 22a | 63 | <25 | 48 | 70 | NA | NA | NA | NA | NA | NA | 77.71 | 9.98 | 67.73 | NA | NA |
| OMW-9 | 11/18/1992 | 1800 | 130a | 30 | 9.2 | 46 | 61 | NA | NA | NA | NA | NA | NA | 77.71 | 9.81 | 67.90 | NA | NA |
| OMW-9 | 02/11/1993 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.71 | NA | NA | NA | NA |
| OMW-9 | 05/19/1993 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.71 | NA | NA | NA | NA |
| OMW-9 | 08/18/1993 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.71 | 9.75 | 67.96 | NA | NA |
| OMW-9 | 11/17/1993 | 5900 | 2400a | 86 | 14 | 150 | 46 | NA | NA | NA | NA | NA | NA | 77.71 | 9.92 | 67.79 | NA | NA |
| OMW-9 | 02/18/1994 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.71 | NA | NA | NA | NA |
| OMW-9 | 05/26/1994 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.71 | NA | NA | NA | NA |

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|---------|------------|-------------------|----------------|-------------|-------------|-------------|-------------|------------------------|------------------------|----------------|----------------|----------------|---------------|--------------|----------------------------|--------------------------|---------------------------|------------------------|
| OMW-9 | 08/29/1994 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.71 | NA | NA | NA | NA |
| OMW-9 | 11/11/1994 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.71 | NA | NA | NA | NA |
| OMW-9 | 02/03/1995 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.71 | NA | NA | NA | NA |
| OMW-9 | 05/07/1995 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.71 | NA | NA | NA | NA |
| OMW-9 | 08/02/1995 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.71 | NA | NA | NA | NA |
| OMW-9 | 02/24/1996 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.71 | NA | NA | NA | NA |
| OMW-9 | 05/04/1996 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.71 | NA | NA | NA | NA |
| OMW-9 | 09/07/1996 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.71 | NA | NA | NA | NA |
| OMW-9 | 11/24/1996 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.71 | NA | NA | NA | NA |
| OMW-9 | 02/23/1997 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.71 | NA | NA | NA | NA |
| OMW-9 | 05/01/1997 | 4700 | 1100 | 150 | 14 | 97 | 52 | 330 | NA | NA | NA | NA | NA | 77.71 | 12.10 | 65.61 | NA | NA |
| OMW-9 | 07/22/1997 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.71 | NA | NA | NA | NA |
| OMW-9 | 11/04/1997 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.71 | NA | NA | NA | NA |
| OMW-9 | 01/21/1998 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.71 | 11.32 | 66.39 | NA | NA |
| OMW-9 | 05/11/1998 | 5500.0 | 1500 | 220 | 10 | 160 | 91 | 110 | NA | NA | NA | NA | NA | 77.71 | 11.95 | 65.76 | NA | NA |
| OMW-9 | 08/11/1998 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.71 | 12.08 | 65.63 | NA | NA |
| OMW-9 | 10/20/1998 | 1200 | 780 | 18 | <5.0 | 14 | 6.0 | 48 | NA | NA | NA | NA | NA | 77.71 | 12.03 | 65.68 | NA | NA |
| OMW-9* | 11/23/1998 | 1700 | 890 | 88 | 9.0 | 42 | 22 | 170 | NA | NA | NA | NA | NA | 77.71 | 11.85 | 65.86 | NA | NA |
| OMW-9 | 02/08/1999 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.71 | 8.01 | 69.70 | NA | NA |
| OMW-9 | 04/12/1999 | 2670 | 1870 | 97 | <5.00 | 111 | 54 | 401 | NA | NA | NA | NA | NA | 77.71 | 9.55 | 68.16 | NA | NA |
| OMW-9 | 07/27/1999 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.71 | 11.87 | 65.84 | NA | NA |
| OMW-9 | 10/25/1999 | 2670 | 606 | 31.3 | <2.50 | 8.32 | <2.50 | 107 | NA | NA | NA | NA | NA | 77.71 | 11.93 | 65.78 | NA | NA |
| OMW-9 | 01/24/2000 | 1400 | 1250 | 44.5 | <1.00 | 12.6 | 8.66 | 69.8 | 23.5 | NA | NA | NA | NA | 77.71 | 10.32 | 67.39 | NA | 1.2 |
| OMW-9 | 04/24/2000 | 1440 | 644 | 53.3 | 0.605 | 4.63 | 10.2 | 80.7 | NA | NA | NA | NA | NA | 77.71 | 11.33 | 66.38 | NA | 1.8 |
| OMW-9 | 07/24/2000 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.71 | 11.82 | 65.89 | NA | NA |
| OMW-9 | 11/01/2000 | 2160 | 685 | 92.6 | 7.96 | 4.69 | 4.02 | 88.8 | NA | NA | NA | NA | NA | 77.71 | 11.45 | 66.26 | NA | 2.0 |
| OMW-9 | 01/19/2001 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.71 | 11.83 | 65.88 | NA | 4.2 |
| OMW-9 | 04/13/2001 | 3620 | 923 | 167 | 3.16 | 60.2 | 14.5 | 231 | NA | NA | NA | NA | NA | 77.71 | 12.19 | 65.52 | NA | 3.8 |
| OMW-9 | 07/09/2001 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.71 | 12.04 | 65.67 | NA | 3.8 |
| OMW-9 | 10/18/2001 | 1400 | <500 | 23 | 0.77 | 1.8 | 1.4 | NA | 10 | NA | NA | NA | NA | 77.71 | 12.90 | 64.81 | NA | 0.4 |
| OMW-9 | 01/24/2002 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.71 | 11.97 | 65.74 | NA | 4.0 |
| OMW-9 | 05/10/2002 | 3900 | 380 | 84 | 2.9 | 120 | 23 | NA | 11 | NA | NA | NA | NA | 77.71 | 12.27 | 65.44 | NA | 1.1 |

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|---------|------------|-------------------|----------------|-------------|-------------|-------------|-------------|------------------------|------------------------|----------------|----------------|----------------|---------------|--------------|----------------------------|--------------------------|---------------------------|------------------------|
| OMW-9 | 07/18/2002 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.71 | 12.42 | 65.29 | NA | 4.2 |
| OMW-9 | 10/31/2002 | 4700 | <1500 | 40 | 1.1 | 14 | 14 | NA | <5.0 | NA | NA | NA | NA | NS | 12.60 | NA | NA | 2.4 |
| OMW-9 | 01/30/2003 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NS | 12.15 | NA | NA | 4.8 |
| OMW-9 | 04/17/2003 | <50 | 120 | <0.50 | <0.50 | <0.50 | <1.0 | NA | <5.0 | NA | NA | NA | NA | NS | 11.61 | NA | NA | 1.8 |
| OMW-9 | 07/17/2003 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NS | 12.22 | NA | NA | 4.2 |
| OMW-9 | 10/16/2003 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NS | NA | NA | NA | NA |
| OMW-9 | 01/14/2004 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NS | 11.87 | NA | NA | 9.1 |
| OMW-9 | 04/14/2004 | 460 | 470 e | 6.1 | <0.50 | 21 | 1.2 | NA | 1.2 | NA | NA | NA | NA | NS | 12.44 | NA | NA | 1.0 |
| OMW-9 | 10/29/2004 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NS | 11.95 | NA | NA | 11.4 |
| OMW-9 | 04/14/2005 | <50 | 210 e | <0.50 | <0.50 | <0.50 | <1.0 | NA | <0.50 | NA | NA | NA | NA | NS | 11.82 | NA | NA | 1.9 |

| | | | | | | | | | | | | | | | | | | |
|------------|------------|-------------------|------|-----|------|-----|-----|----|----|----|----|----|----|-------|-------|-------|----|----|
| OMW-10 | 08/07/1991 | 460 | <50 | 73 | 1.0 | 18 | 8.4 | NA | NA | NA | NA | NA | NA | 77.91 | 10.00 | 67.91 | NA | NA |
| OMW-10 | 10/31/1991 | 630 | 150 | 100 | <0.5 | 33 | 26 | NA | NA | NA | NA | NA | NA | 77.91 | 10.10 | 67.81 | NA | NA |
| OMW-10 | 02/15/1992 | 810 | 570a | 85 | 2.5 | 44 | 38 | NA | NA | NA | NA | NA | NA | 77.91 | NA | NA | NA | NA |
| OMW-10 | 03/18/1992 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.91 | 9.55 | 68.36 | NA | NA |
| OMW-10 | 05/21/1992 | 280 | NA | 47 | 0.7 | 4.0 | 3.1 | NA | NA | NA | NA | NA | NA | 77.91 | 10.41 | 67.50 | NA | NA |
| OMW-10 | 08/19/1992 | 330 | NA | 35 | <1 | 6.0 | 4.1 | NA | NA | NA | NA | NA | NA | 77.91 | 10.46 | 67.45 | NA | NA |
| OMW-10 | 11/18/1993 | 300 | NA | 30 | 0.8 | 7.1 | 6.3 | NA | NA | NA | NA | NA | NA | 77.91 | 10.31 | 67.60 | NA | NA |
| OMW-10 | 02/11/1993 | 510a | NA | 49 | 3.8 | 18 | 18 | NA | NA | NA | NA | NA | NA | 77.91 | 9.68 | 68.23 | NA | NA |
| OMW-10 | 05/19/1993 | <50 | NA | 96 | <0.5 | 3.4 | 1.5 | NA | NA | NA | NA | NA | NA | 77.91 | 10.19 | 67.72 | NA | NA |
| OMW-10 | 08/18/1993 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.91 | 10.29 | 67.62 | NA | NA |
| OMW-10 | 11/17/1993 | 400 | NA | 24 | <1.0 | 2.8 | 1.9 | NA | NA | NA | NA | NA | NA | 77.91 | 10.32 | 67.59 | NA | NA |
| OMW-10 | 02/18/1994 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.91 | 9.30 | 68.61 | NA | NA |
| OMW-10 | 05/26/1994 | 330 | NA | 32 | 13 | 7.5 | 26 | NA | NA | NA | NA | NA | NA | 77.91 | 10.14 | 67.77 | NA | NA |
| OMW-10 | 08/09/1994 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.91 | 10.38 | 67.53 | NA | NA |
| OMW-10 | 11/11/1994 | 110 | NA | 7.8 | <0.5 | 2.3 | 1.5 | NA | NA | NA | NA | NA | NA | 77.91 | 9.34 | 68.57 | NA | NA |
| OMW-10 | 02/03/1995 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.91 | 10.17 | 67.74 | NA | NA |
| OMW-10 | 05/07/1995 | 1600 | NA | 110 | 3.1 | 17 | 12 | NA | NA | NA | NA | NA | NA | 77.91 | 9.63 | 68.28 | NA | NA |
| OMW-10 | 08/02/1995 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.91 | 10.07 | 67.84 | NA | NA |
| OMW-10 | 11/02/1995 | 1200 | NA | 47 | 0.8 | 1.4 | 2.4 | NA | NA | NA | NA | NA | NA | 77.91 | 9.74 | 68.17 | NA | NA |
| OMW-10 (D) | 11/02/1995 | 1300 | NA | 50 | 0.8 | 1.5 | 2.5 | NA | NA | NA | NA | NA | NA | 77.91 | NA | NA | NA | NA |
| OMW-10 | 02/24/1996 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.91 | NA | NA | NA | NA |

WELL CONCENTRATIONS
Former Shell Service Station
500 40th Street/Telegraph Avenue
Oakland, CA

| Well ID | Date | TPPH (ug/L) | TEPH (ug/L) | B (ug/L) | T (ug/L) | E (ug/L) | X (ug/L) | MTBE 8020 (ug/L) | MTBE 8260 (ug/L) | DIPE (ug/L) | ETBE (ug/L) | TAME (ug/L) | TBA (ug/L) | TOC (MSL) | Depth to Water (ft.) | GW Elevation (MSL) | SPH Thickness (ft.) | DO Reading (ppm) |
|------------|------------|----------------|----------------|-------------|-------------|-------------|-------------|------------------------|------------------------|----------------|----------------|----------------|---------------|--------------|----------------------------|--------------------------|---------------------------|------------------------|
| OMW-10 | 05/04/1996 | 1100 | NA | 76 | 16 | 7.4 | 32 | 57 | NA | NA | NA | NA | NA | 77.91 | 9.97 | 67.94 | NA | NA |
| OMW-10 (D) | 05/04/1996 | 700 | NA | 63 | 13 | 6.4 | 25 | 21 | NA | NA | NA | NA | NA | 77.91 | NA | NA | NA | NA |
| OMW-10 | 09/07/1996 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.91 | 13.00 | 64.91 | NA | NA |
| OMW-10 | 11/24/1996 | 540 | NA | 13 | 2.7 | 1.3 | 1.7 | 16 | NA | NA | NA | NA | NA | 77.91 | 12.56 | 65.35 | NA | NA |
| OMW-10 (D) | 11/24/1996 | 490 | NA | 25 | <2.0 | <2.0 | <2.0 | 66 | NA | NA | NA | NA | NA | 77.91 | NA | NA | NA | NA |
| OMW-10 | 02/23/1997 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.91 | 12.52 | 65.39 | NA | NA |
| OMW-10 | 05/01/1997 | 910 | NA | 1.3 | 10 | 4.1 | 5.9 | 4.1 | NA | NA | NA | NA | NA | 77.91 | 13.13 | 64.78 | NA | NA |
| OMW-10 | 07/22/1997 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.91 | 13.46 | 64.45 | NA | NA |
| OMW-10 | 11/04/1997 | 460 | NA | 5.0 | <0.50 | 1.3 | 2.2 | <5.0 | NA | NA | NA | NA | NA | 77.91 | 12.08 | 65.83 | NA | NA |
| OMW-10 | 01/21/1998 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.91 | 11.77 | 66.14 | NA | NA |
| OMW-10 | 05/11/1998 | 370 | NA | 4.1 | 0.7 | <0.50 | 0.88 | 5.2 | NA | NA | NA | NA | NA | 77.91 | 12.86 | 65.05 | NA | NA |
| OMW-10 | 08/11/1998 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.91 | 13.20 | 64.71 | NA | NA |
| OMW-10 | 10/20/1998 | 490 | NA | <0.50 | <0.50 | 1.6 | 2.3 | 5.9 | NA | NA | NA | NA | NA | 77.91 | 13.20 | 64.71 | NA | NA |
| OMW-10** | 11/23/1998 | 150 | 790 | 3.2 | 0.72 | <0.50 | 1.5 | 5 | NA | NA | NA | NA | NA | 77.91 | 12.85 | 65.06 | NA | NA |
| OMW-10 | 02/08/1999 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.91 | 9.18 | 68.73 | NA | NA |
| OMW-10 | 04/12/1999 | 1910 | NA | 59.8 | 65.80 | 67 | 41.6 | <100 | NA | NA | NA | NA | NA | 77.91 | 10.25 | 67.66 | NA | NA |
| OMW-10 | 07/27/1999 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.91 | 12.85 | 65.06 | NA | NA |
| OMW-10 | 10/25/1999 | 130 | NA | 1.08 | <0.500 | 0.522 | <0.500 | <5.00 | NA | NA | NA | NA | NA | 77.91 | 12.99 | 64.92 | NA | NA |
| OMW-10 | 01/24/2000 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.91 | 10.61 | 67.30 | NA | 0.6 |
| OMW-10 | 04/24/2000 | 60.7 | NA | 1.73 | <0.500 | <0.500 | <0.500 | <2.50 | NA | NA | NA | NA | NA | 77.91 | 12.35 | 65.56 | NA | 1.1 |
| OMW-10 | 07/24/2000 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.91 | 12.76 | 65.15 | NA | NA |
| OMW-10 | 11/01/2000 | <50.0 | NA | 0.664 | <0.500 | <0.500 | <0.500 | <2.50 | NA | NA | NA | NA | NA | 77.91 | 11.96 | 65.95 | NA | 2.2 |
| OMW-10 | 01/19/2001 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.91 | 12.51 | 65.40 | NA | 3.4 |
| OMW-10 | 04/13/2001 | 91.0 | NA | 1.75 | 0.720 | <0.500 | 0.718 | 6.11 | NA | NA | NA | NA | NA | 77.91 | 12.95 | 64.96 | NA | 6.2 |
| OMW-10 | 07/09/2001 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.91 | 13.11 | 64.80 | NA | 3.4 |
| OMW-10 | 10/18/2001 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 77.91 | 19.69 | 58.22 | NA | 0.2 |
| OMW-10 | 01/24/2002 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.91 | 12.83 | 65.08 | NA | 2.5 |
| OMW-10 | 05/10/2002 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 77.91 | 13.20 | 64.71 | NA | 1.1 |
| OMW-10 | 07/18/2002 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 77.91 | 13.22 | 64.69 | NA | 2.3 |
| OMW-10 | 10/31/2002 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 81.14 | 13.55 | 67.59 | NA | NA |
| OMW-10 | 01/30/2003 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.14 | 12.67 | 68.47 | NA | NA |
| OMW-10 | 04/17/2003 | <50 | NA | <0.50 | <0.50 | <0.50 | <1.0 | NA | 6.6 | NA | NA | NA | NA | 81.14 | 12.14 | 69.00 | NA | NA |

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| Well ID | Date | TPPH (ug/L) | TEPH (ug/L) | B (ug/L) | T (ug/L) | E (ug/L) | X (ug/L) | MTBE 8020 (ug/L) | MTBE 8260 (ug/L) | DIPE (ug/L) | ETBE (ug/L) | TAME (ug/L) | TBA (ug/L) | TOC (MSL) | Depth to Water (ft.) | GW Elevation (MSL) | SPH Thickness (ft.) | DO Reading (ppm) |
|---------|------------|-------------------|----------------|-------------|-------------|-------------|-------------|------------------------|------------------------|----------------|----------------|----------------|---------------|--------------|----------------------------|--------------------------|---------------------------|------------------------|
| OMW-10 | 07/17/2003 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.14 | 13.08 | 68.06 | NA | NA |
| OMW-10 | 10/16/2003 | 120 e | NA | 0.68 | <0.50 | <0.50 | <1.0 | NA | 0.99 | NA | NA | NA | NA | 81.14 | 13.27 | 67.87 | NA | NA |
| OMW-10 | 01/14/2004 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.14 | 12.55 | 68.59 | NA | NA |
| OMW-10 | 04/14/2004 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.14 | 13.04 | 68.10 | NA | NA |
| OMW-10 | 10/29/2004 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.14 | 12.61 | 68.53 | NA | NA |
| OMW-10 | 04/14/2005 | Well destroyed | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 81.14 | NA | NA | NA | NA |
| OMW-11 | 11/22/1991 | 450 | 240 | 1.1 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 75.76 | 11.90 | 63.86 | NA | NA |
| OMW-11 | 02/15/1992 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 75.76 | NA | NA | NA | NA |
| OMW-11 | 03/18/1992 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 75.76 | NA | NA | NA | NA |
| OMW-11 | 05/20/1992 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 75.76 | NA | NA | NA | NA |
| OMW-11 | 08/19/1992 | 270a | <50 | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 75.76 | 12.06 | 63.70 | NA | NA |
| OMW-11 | 11/18/1992 | 400a | 100 | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 75.76 | 12.01 | 63.75 | NA | NA |
| OMW-11 | 02/11/1993 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 75.76 | NA | NA | NA | NA |
| OMW-11 | 05/20/1993 | 200a | <0.5 | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 75.76 | 11.90 | 63.86 | NA | NA |
| OMW-11 | 08/18/1993 | 180a | <50 | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 75.76 | 11.90 | 63.86 | NA | NA |
| OMW-11 | 11/17/1993 | 150a | <50a | <0.5 | 3.6 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 75.76 | 11.94 | 63.82 | NA | NA |
| OMW-11 | 02/18/1994 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 75.76 | NA | NA | NA | NA |
| OMW-11 | 05/26/1994 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 75.76 | NA | NA | NA | NA |
| OMW-11 | 08/29/1994 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 75.76 | 11.98 | 63.78 | NA | NA |
| OMW-11 | 11/11/1994 | 160 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 75.76 | 10.88 | 64.88 | NA | NA |
| OMW-11 | 02/03/1995 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 75.76 | 10.62 | 65.14 | NA | NA |
| OMW-11 | 03/05/1995 | 220 | 100 | 0.7 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 75.76 | NA | NA | NA | NA |
| OMW-11 | 05/07/1995 | 160 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 75.76 | 11.49 | 64.27 | NA | NA |
| OMW-11 | 08/02/1995 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 75.76 | NA | NA | NA | NA |
| OMW-11 | 02/24/1996 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 75.76 | NA | NA | NA | NA |
| OMW-11 | 05/04/1996 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 75.76 | NA | NA | NA | NA |
| OMW-11 | 09/07/1996 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 75.76 | NA | NA | NA | NA |
| OMW-11 | 11/24/1996 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 75.76 | NA | NA | NA | NA |
| OMW-11 | 02/23/1997 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 75.76 | NA | NA | NA | NA |
| OMW-11 | 05/01/1997 | 130 | 71 | <0.50 | <0.50 | <0.50 | 0.61 | <2.5 | NA | NA | NA | NA | NA | 75.76 | 13.76 | 62.00 | NA | NA |
| OMW-11 | 07/22/1997 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 75.76 | NA | NA | NA | NA |

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|---------|------------|-------------------|----------------|-------------|-------------|-------------|-------------|------------------------|------------------------|----------------|----------------|----------------|---------------|--------------|----------------------------|--------------------------|---------------------------|------------------------|
| OMW-11 | 11/04/1997 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 75.76 | NA | NA | NA | NA |
| OMW-11 | 01/21/1998 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 75.76 | NA | NA | NA | NA |
| OMW-11 | 05/11/1998 | 100 | 85 | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 75.76 | 13.18 | 62.58 | NA | NA |
| OMW-11 | 08/11/1998 | 110 | <50 | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 75.76 | 13.50 | 62.26 | NA | NA |
| OMW-11 | 10/20/1998 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 75.76 | NA | NA | NA | NA |
| OMW-11 | 04/12/1999 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 75.76 | NA | NA | NA | NA |
| OMW-11 | 07/27/1999 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 75.76 | NA | NA | NA | NA |
| OMW-11 | 10/25/1999 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 75.76 | NA | NA | NA | NA |
| OMW-11 | 01/24/2000 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 75.76 | NA | NA | NA | NA |
| OMW-11 | 04/24/2000 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 75.76 | NA | NA | NA | NA |
| OMW-11 | 05/11/2000 | <50.0 | <50.0 | <0.500 | <0.500 | <0.500 | <0.500 | <2.50 | NA | NA | NA | NA | NA | 75.76 | 12.21 | 63.55 | NA | NA |
| OMW-11 | 07/24/2000 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 75.76 | NA | NA | NA | NA |
| OMW-11 | 07/29/2000 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 75.76 | NA | NA | NA | NA |
| OMW-11 | 10/26/2000 | <50.0 | b | <0.500 | <0.500 | <0.500 | <0.500 | <2.50 | NA | NA | NA | NA | NA | 75.76 | 12.47 | 63.29 | NA | 1.5 |
| OMW-11 | 11/01/2000 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 75.76 | NA | NA | NA | NA |
| OMW-11 | 01/19/2001 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 75.76 | 12.29 | 63.47 | NA | NA |
| OMW-11 | 04/13/2001 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 75.76 | NA | NA | NA | NA |
| OMW-11 | 04/26/2001 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 75.76 | NA | NA | NA | NA |
| OMW-11 | 04/27/2001 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 75.76 | NA | NA | NA | NA |
| OMW-11 | 07/09/2001 | 130 | <50 | <0.50 | <0.50 | <0.50 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 75.76 | 13.00 | 62.76 | NA | 3.6 |
| OMW-11 | 10/18/2001 | 200 | <50 | <0.50 | <0.50 | <0.50 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 75.76 | 13.35 | 62.41 | NA | 0.6 |
| OMW-11 | 01/24/2002 | <50 | 170 | <0.50 | <0.50 | <0.50 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 75.76 | 12.18 | 63.58 | NA | 1.7 |
| OMW-11 | 05/10/2002 | 180 | <50 | <0.50 | <0.50 | <0.50 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 75.76 | 12.44 | 63.32 | NA | 1.3 |
| OMW-11 | 07/18/2002 | 230 | 68 | <0.50 | <0.50 | <0.50 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 75.76 | 12.32 | 63.44 | NA | 1.9 |
| OMW-11 | 10/31/2002 | 210 | <50 | <0.50 | <0.50 | <0.50 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 78.67 | 12.70 | 65.97 | NA | NA |
| OMW-11 | 01/30/2003 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 78.67 | NA | NA | NA | NA |
| OMW-11 | 04/17/2003 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 78.67 | NA | NA | NA | NA |
| OMW-11 | 07/17/2003 | 120 e | <50 | <0.50 | <0.50 | <0.50 | <1.0 | NA | <0.50 | NA | NA | NA | NA | 78.67 | 12.56 | 66.11 | NA | NA |
| OMW-11 | 10/16/2003 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 78.67 | NA | NA | NA | NA |
| OMW-11 | 01/14/2004 | 97 e | <50 | <0.50 | 0.67 | <0.50 | <1.0 | NA | <0.50 | NA | NA | NA | NA | 78.67 | 12.17 | 66.50 | NA | 1.6 |
| OMW-11 | 04/14/2004 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 78.67 | 12.41 | 66.26 | NA | NA |
| OMW-11 | 10/29/2004 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 78.67 | 12.31 | 66.36 | NA | NA |

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| Well ID | Date | TPPH (ug/L) | TEPH (ug/L) | B (ug/L) | T (ug/L) | E (ug/L) | X (ug/L) | MTBE 8020 (ug/L) | MTBE 8260 (ug/L) | DIPE (ug/L) | ETBE (ug/L) | TAME (ug/L) | TBA (ug/L) | TOC (MSL) | Depth to Water (ft.) | GW Elevation (MSL) | SPH Thickness (ft.) | DO Reading (ppm) |
|------------|------------|----------------|----------------|-------------|-------------|-------------|-------------|------------------------|------------------------|----------------|----------------|----------------|---------------|--------------|----------------------------|--------------------------|---------------------------|------------------------|
| OMW-11 | 04/14/2005 | Well destroyed | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 78.67 | NA | NA | NA | NA |
| OMW-12 | 12/02/1991 | <1000 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 75.65 | 10.31 | 65.34 | NA | NA |
| OMW-12 | 03/18/1992 | <50 | <50 | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 75.65 | 8.93 | 66.72 | NA | NA |
| OMW-12 | 05/20/1992 | 180a | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 75.65 | 10.26 | 65.39 | NA | NA |
| OMW-12 | 08/19/1992 | 230a | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 75.65 | 10.53 | 65.12 | NA | NA |
| OMW-12 | 11/18/1992 | 220a | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 75.65 | 10.45 | 65.20 | NA | NA |
| OMW-12 | 02/11/1993 | 240 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 75.65 | 8.90 | 66.75 | NA | NA |
| OMW-12 | 05/19/1993 | 110a | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 75.65 | 10.60 | 65.05 | NA | NA |
| OMW-12 | 08/18/1993 | 140a | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 75.65 | 10.28 | 65.37 | NA | NA |
| OMW-12 | 11/17/1993 | 120a | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 75.65 | 10.24 | 65.41 | NA | NA |
| OMW-12 | 02/18/1994 | 180a | NA | 1.7 | 2.1 | 0.9 | 4.8 | NA | NA | NA | NA | NA | NA | 75.65 | 8.97 | 66.68 | NA | NA |
| OMW-12 | 05/26/1994 | 150 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 75.65 | 9.62 | 66.03 | NA | NA |
| OMW-12 | 08/29/1994 | 110 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 75.65 | 10.20 | 65.45 | NA | NA |
| OMW-12 | 11/11/1994 | 90 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 75.65 | 8.54 | 67.11 | NA | NA |
| OMW-12 | 02/03/1995 | 80 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 75.65 | 8.28 | 67.37 | NA | NA |
| OMW-12 (D) | 02/03/1995 | 100 | NA | 0.6 | <0.5 | 0.7 | 1.1 | NA | NA | NA | NA | NA | NA | 75.65 | NA | NA | NA | NA |
| OMW-12 | 05/07/1995 | 110 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 75.65 | 9.17 | 66.48 | NA | NA |
| OMW-12 | 08/02/1995 | 90 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 75.65 | 10.06 | 65.59 | NA | NA |
| OMW-12 (D) | 08/02/1995 | 120 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 75.65 | NA | NA | NA | NA |
| OMW-12 | 11/02/1995 | 130 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 75.65 | 10.09 | 65.56 | NA | NA |
| OMW-12 | 02/24/1996 | 80 | NA | <0.5 | <0.5 | <0.5 | <0.5 | NA | NA | NA | NA | NA | NA | 75.65 | 7.81 | 67.84 | NA | NA |
| OMW-12 | 05/04/1996 | 61 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 75.65 | 11.72 | 63.93 | NA | NA |
| OMW-12 | 09/07/1996 | 66 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 75.65 | 12.65 | 63.00 | NA | NA |
| OMW-12 | 11/24/1996 | 70 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 75.65 | 11.54 | 64.11 | NA | NA |
| OMW-12 | 02/23/1997 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 75.65 | 11.53 | 64.12 | NA | NA |
| OMW-12 | 05/01/1997 | 79 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 75.65 | 12.17 | 63.48 | NA | NA |
| OMW-12 | 07/22/1997 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 75.65 | 12.48 | 63.17 | NA | NA |
| OMW-12 (D) | 07/22/1997 | 51 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 75.65 | NA | NA | NA | NA |
| OMW-12 | 11/04/1997 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <5.0 | NA | NA | NA | NA | NA | 75.65 | 12.54 | 63.11 | NA | NA |
| OMW-12 | 01/21/1998 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 75.65 | 9.82 | 65.83 | NA | NA |
| OMW-12 | 05/11/1998 | 53 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 75.65 | 11.63 | 64.02 | NA | NA |

WELL CONCENTRATIONS
Former Shell Service Station
500 40th Street/Telegraph Avenue
Oakland, CA

| Well ID | Date | TPPH (ug/L) | TEPH (ug/L) | B (ug/L) | T (ug/L) | E (ug/L) | X (ug/L) | MTBE 8020 (ug/L) | MTBE 8260 (ug/L) | DIPE (ug/L) | ETBE (ug/L) | TAME (ug/L) | TBA (ug/L) | TOC (MSL) | Depth to Water (ft.) | GW Elevation (MSL) | SPH Thickness (ft.) | DO Reading (ppm) |
|---------|------------|-------------------|----------------|-------------|-------------|-------------|-------------|------------------------|------------------------|----------------|----------------|----------------|---------------|--------------|----------------------------|--------------------------|---------------------------|------------------------|
| OMW-12 | 08/11/1998 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 75.65 | 12.05 | 63.60 | NA | NA |
| OMW-12 | 10/20/1998 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 75.65 | 12.31 | 63.34 | NA | NA |
| OMW-12 | 02/08/1999 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | <2.5 | NA | NA | NA | NA | NA | 75.65 | 8.25 | 67.40 | NA | NA |
| OMW-12 | 04/12/1999 | Well Inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 75.65 | NA | NA | NA | NA |
| OMW-12 | 07/27/1999 | <50.0 | NA | <0.500 | <0.500 | <0.500 | <0.500 | <2.50 | NA | NA | NA | NA | NA | 75.65 | 10.88 | 64.77 | NA | NA |
| OMW-12 | 10/25/1999 | <50.0 | NA | <0.500 | <0.500 | <0.500 | <0.500 | <5.00 | NA | NA | NA | NA | NA | 75.65 | 11.00 | 64.65 | NA | NA |
| OMW-12 | 01/24/2000 | Well Inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 75.65 | NA | NA | NA | NA |
| OMW-12 | 04/24/2000 | <50.0 | NA | <0.500 | <0.500 | <0.500 | <0.500 | <2.50 | NA | NA | NA | NA | NA | 75.65 | 10.53 | 65.12 | NA | 2.0 |
| OMW-12 | 07/24/2000 | <50.0 | NA | <0.500 | <0.500 | <0.500 | <0.500 | <2.50 | NA | NA | NA | NA | NA | 75.65 | 11.55 | 64.10 | NA | NA |
| OMW-12 | 11/01/2000 | <50.0 | NA | <0.500 | <0.500 | <0.500 | <0.500 | <2.50 | NA | NA | NA | NA | NA | 75.65 | 10.34 | 65.31 | NA | 2.6 |
| OMW-12 | 01/19/2001 | <50.0 | NA | <0.500 | <0.500 | <0.500 | <0.500 | <2.50 | NA | NA | NA | NA | NA | 75.65 | 10.60 | 65.05 | NA | 7.6 |
| OMW-12 | 04/13/2001 | <50.0 | NA | <0.500 | <0.500 | <0.500 | <0.500 | <2.50 | NA | NA | NA | NA | NA | 75.65 | 10.75 | 64.90 | NA | 2.8 |
| OMW-12 | 07/09/2001 | 69 | NA | <0.50 | <0.50 | <0.50 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 75.65 | 11.64 | 64.01 | NA | 4.8 |
| OMW-12 | 10/18/2001 | 81 | NA | <0.50 | <0.50 | <0.50 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 75.65 | 11.95 | 63.70 | NA | 1.3 |
| OMW-12 | 01/24/2002 | <50 | NA | <0.50 | <0.50 | <0.50 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 75.65 | 10.27 | 65.38 | NA | 3.4 |
| OMW-12 | 05/10/2002 | 73 | NA | <0.50 | <0.50 | <0.50 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 75.65 | 10.86 | 64.79 | NA | 1.6 |
| OMW-12 | 07/18/2002 | 71 | NA | <0.50 | <0.50 | <0.50 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 75.65 | 10.66 | 64.99 | NA | 1.7 |
| OMW-12 | 10/31/2002 | 76 | NA | <0.50 | <0.50 | <0.50 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 78.58 | 11.20 | 67.38 | NA | NA |
| OMW-12 | 01/30/2003 | 58 | NA | <0.50 | <0.50 | <0.50 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 78.58 | 10.30 | 68.28 | NA | NA |
| OMW-12 | 04/17/2003 | <50 | NA | <0.50 | <0.50 | <0.50 | <1.0 | NA | <5.0 | NA | NA | NA | NA | 78.58 | 10.17 | 68.41 | NA | NA |
| OMW-12 | 07/17/2003 | <50 | NA | <0.50 | <0.50 | <0.50 | <1.0 | NA | <0.50 | NA | NA | NA | NA | 78.58 | 11.05 | 67.53 | NA | NA |
| OMW-12 | 10/16/2003 | <50 | NA | <0.50 | <0.50 | <0.50 | <1.0 | NA | <0.50 | NA | NA | NA | NA | 78.58 | 11.33 | 67.25 | NA | NA |
| OMW-12 | 01/14/2004 | 67 e | NA | <0.50 | 0.87 | <0.50 | <1.0 | NA | <0.50 | NA | NA | NA | NA | 78.58 | 10.50 | 68.08 | NA | 2.8 |
| OMW-12 | 04/14/2004 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 78.58 | 10.85 | 67.73 | NA | NA |
| OMW-12 | 10/29/2004 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 78.58 | 10.72 | 67.86 | NA | NA |
| OMW-12 | 04/14/2005 | Well destroyed | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 78.58 | NA | NA | NA | NA |
| OMW-13 | 11/22/1991 | 900 | 1000 | 37 | 9.5 | 74 | 130 | NA | NA | NA | NA | NA | NA | 76.36 | 11.96 | 64.40 | NA | NA |
| OMW-13 | 03/18/1992 | 900a | 590a | 24 | 28 | 320 | 320 | NA | NA | NA | NA | NA | NA | 76.36 | 10.84 | 65.52 | NA | NA |
| OMW-13 | 05/20/1992 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | NA | NA | NA | NA |
| OMW-13 | 08/19/1992 | 7000 | 470a | 180 | 36 | 150 | 150 | NA | NA | NA | NA | NA | NA | 76.36 | 12.12 | 64.24 | NA | NA |
| OMW-13 | 11/18/1992 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | 12.00 | 64.36 | NA | NA |

WELL CONCENTRATIONS
Former Shell Service Station
500 40th Street/Telegraph Avenue
Oakland, CA

| Well ID | Date | TPPH (ug/L) | TEPH (ug/L) | B (ug/L) | T (ug/L) | E (ug/L) | X (ug/L) | MTBE 8020 (ug/L) | MTBE 8260 (ug/L) | DIPE (ug/L) | ETBE (ug/L) | TAME (ug/L) | TBA (ug/L) | TOC (MSL) | Depth to Water (ft.) | GW Elevation (MSL) | SPH Thickness (ft.) | DO Reading (ppm) |
|---------|------------|-------------------|----------------|-------------|-------------|-------------|-------------|------------------------|------------------------|----------------|----------------|----------------|---------------|--------------|----------------------------|--------------------------|---------------------------|------------------------|
| OMW-13 | 02/11/1993 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | NA | NA | NA | NA |
| OMW-13 | 05/20/1993 | 9200 | NA | 320 | 83 | 490 | 950 | NA | NA | NA | NA | NA | NA | 76.36 | 12.26 | 64.10 | NA | NA |
| OMW-13 | 08/18/1993 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | 11.75 | 64.61 | NA | NA |
| OMW-13 | 11/17/1993 | 38000 | 3800 | 210 | <130 | 1000 | 2500 | NA | NA | NA | NA | NA | NA | 76.36 | 11.78 | 64.58 | NA | NA |
| OMW-13 | 02/18/1994 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | NA | NA | NA | NA |
| OMW-13 | 05/26/1994 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | NA | NA | NA | NA |
| OMW-13 | 08/29/1994 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | NA | NA | NA | NA |
| OMW-13 | 11/11/1994 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | 10.28 | 66.08 | NA | NA |
| OMW-13 | 02/03/1995 | 1.0 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | 10.01 | 66.35 | NA | NA |
| OMW-13 | 03/05/1995 | 9100 | 3900 | 200 | 9.7 | 200 | 130 | NA | NA | NA | NA | NA | NA | 76.36 | NA | NA | NA | NA |
| OMW-13 | 05/07/1995 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | NA | NA | NA | NA |
| OMW-13 | 08/02/1995 | 8000 | 2900 | 180 | 6.6 | 190 | 55 | NA | NA | NA | NA | NA | NA | 76.36 | 11.80 | 64.56 | NA | NA |
| OMW-13 | 02/24/1996 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | NA | NA | NA | NA |
| OMW-13 | 05/04/1996 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | NA | NA | NA | NA |
| OMW-13 | 09/07/1996 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | NA | NA | NA | NA |
| OMW-13 | 11/24/1996 | 15000 | 7700 | 50 | <20 | 74 | 60 | <100 | NA | NA | NA | NA | NA | 76.36 | 12.35 | 64.01 | NA | NA |
| OMW-13 | 02/23/1997 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | NA | NA | NA | NA |
| OMW-13 | 05/01/1997 | 2600 | 290 | 33 | 10 | 30 | 14 | 88 | NA | NA | NA | NA | NA | 76.36 | 13.83 | 62.53 | NA | NA |
| OMW-13 | 07/22/1997 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | NA | NA | NA | NA |
| OMW-13 | 11/04/1997 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | NA | NA | NA | NA |
| OMW-13 | 01/21/1998 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | NA | NA | NA | NA |
| OMW-13 | 05/11/1998 | 10000 | 1400 | 60 | 17 | 120 | 23 | <50 | NA | NA | NA | NA | NA | 76.36 | 13.21 | 63.15 | NA | NA |
| OMW-13 | 08/11/1998 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | NA | NA | NA | NA |
| OMW-13 | 10/20/1998 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | NA | NA | NA | NA |
| OMW-13 | 02/08/1999 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | NA | NA | NA | NA |
| OMW-13 | 04/12/1999 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | NA | NA | NA | NA |
| OMW-13 | 07/27/1999 | 6270 | 2230 | 32.0 | 26.0 | 53.0 | <5.00 | 33.0 | NA | NA | NA | NA | NA | 76.36 | 11.87 | 64.49 | NA | NA |
| OMW-13 | 10/25/1999 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | NA | NA | NA | NA |
| OMW-13 | 01/24/2000 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | NA | NA | NA | NA |
| OMW-13 | 04/24/2000 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | NA | NA | NA | NA |
| OMW-13 | 05/11/2000 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | NA | NA | NA | NA |
| OMW-13 | 07/24/2000 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | NA | NA | NA | NA |

WELL CONCENTRATIONS
Former Shell Service Station
500 40th Street/Telegraph Avenue
Oakland, CA

| Well ID | Date | TPPH (ug/L) | TEPH (ug/L) | B (ug/L) | T (ug/L) | E (ug/L) | X (ug/L) | MTBE 8020 (ug/L) | MTBE 8260 (ug/L) | DIPE (ug/L) | ETBE (ug/L) | TAME (ug/L) | TBA (ug/L) | TOC (MSL) | Depth to Water (ft.) | GW Elevation (MSL) | SPH Thickness (ft.) | DO Reading (ppm) |
|---------|------------|-------------------|----------------|-------------|-------------|-------------|-------------|------------------------|------------------------|----------------|----------------|----------------|---------------|--------------|----------------------------|--------------------------|---------------------------|------------------------|
| OMW-13 | 07/29/2000 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | NA | NA | NA | NA |
| OMW-13 | 11/01/2000 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | NA | NA | NA | NA |
| OMW-13 | 11/15/2000 | 2990 | 1200 | 34.8 | 37.3 | <10.0 | <10.0 | <50.0 | NA | NA | NA | NA | NA | 76.36 | 12.35 | 64.01 | NA | 1.4 |
| OMW-13 | 01/19/2001 | 4830 | 2390 | 34.8 | <5.00 | 93.1 | <5.00 | <25.0 | NA | NA | NA | NA | NA | 76.36 | 12.17 | 64.19 | NA | 7.0 |
| OMW-13 | 04/13/2001 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | NA | NA | NA | NA |
| OMW-13 | 04/26/2001 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | NA | NA | NA | NA |
| OMW-13 | 04/27/2001 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | NA | NA | NA | NA |
| OMW-13 | 07/09/2001 | 1300 | <600 | 0.74 | <0.50 | <0.50 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 76.36 | 13.20 | 63.16 | NA | 6.4 |
| OMW-13 | 10/18/2001 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | NA | NA | NA | NA |
| OMW-13 | 11/01/2001 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | 76.36 | NA | NA | NA | NA |
| OMW-13 | 11/09/2001 | 910 | <300 | <0.50 | <0.50 | 1.1 | <0.50 | NA | <5.0 | NA | NA | NA | NA | 76.36 | 13.53 | 62.83 | NA | 5.8 |
| OMW-13 | 01/24/2002 | 6300 | <1500 | 6.6 | 1.0 | 28 | 2.1 | NA | <10 | NA | NA | NA | NA | 76.36 | 12.23 | 64.13 | NA | 2.9 |
| OMW-13 | 05/10/2002 | 2800 | <400 | 3.5 | <0.50 | 15 | 1.2 | NA | <5.0 | NA | NA | NA | NA | 76.36 | 12.59 | 63.77 | NA | 1.0 |
| OMW-13 | 07/18/2002 | 3300 | <1000 | 4.3 | 0.70 | 29 | 1.8 | NA | <5.0 | NA | NA | NA | NA | 76.36 | 12.44 | 63.92 | NA | 2.1 |
| OMW-13 | 10/31/2002 | 1900 | <1000 | 0.96 | <0.50 | 7.5 | <0.50 | NA | <5.0 | NA | NA | NA | NA | NS | 12.86 | NA | NA | NA |
| OMW-13 | 01/30/2003 | Well inaccessible | | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NS | 12.86 | NA | NA | NA |
| OMW-13 | 04/17/2003 | 5800 | 1800 | 11 | 1.3 | 34 | 2.9 | NA | <10 | NA | NA | NA | NA | NS | 11.87 | NA | NA | NA |
| OMW-13 | 07/17/2003 | 5100 e | 930 e | 3.1 | <2.5 | 10 | <5.0 | NA | <2.5 | NA | NA | NA | NA | NS | 12.70 | NA | NA | NA |
| OMW-13 | 10/16/2003 | 3100 e | 740 e | <2.5 | <2.5 | <2.5 | <5.0 | NA | <2.5 | NA | NA | NA | NA | NS | 12.93 | NA | NA | NA |
| OMW-13 | 01/14/2004 | 7800 | 2100 e | 6.3 | <2.5 | 11 | 9.8 | NA | <2.5 | NA | NA | NA | NA | NS | 12.57 | NA | NA | 1.2 |
| OMW-13 | 04/14/2004 | 4400 | 1100 e | 3.3 | <2.5 | 7.6 | <5.0 | NA | <2.5 | NA | NA | NA | NA | NS | 12.50 | NA | NA | NA |
| OMW-13 | 10/29/2004 | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NA | NS | 12.35 | NA | NA | NA |
| OMW-13 | 04/14/2005 | 4900 | 2000 f | 5.0 | <2.5 | 6.7 | <5.0 | NA | <2.5 | NA | NA | NA | NA | NS | 12.01 | NA | NA | NA |

WELL CONCENTRATIONS
Former Shell Service Station
500 40th Street/Telegraph Avenue
Oakland, CA

| Well ID | Date | TPPH (ug/L) | TEPH (ug/L) | B (ug/L) | T (ug/L) | E (ug/L) | X (ug/L) | MTBE 8020 (ug/L) | MTBE 8260 (ug/L) | DIPE (ug/L) | ETBE (ug/L) | TAME (ug/L) | TBA (ug/L) | TOC (MSL) | Depth to Water (ft.) | GW Elevation (MSL) | SPH Thickness (ft.) | DO Reading (ppm) |
|---------|------|----------------|----------------|-------------|-------------|-------------|-------------|------------------------|------------------------|----------------|----------------|----------------|---------------|--------------|----------------------------|--------------------------|---------------------------|------------------------|
|---------|------|----------------|----------------|-------------|-------------|-------------|-------------|------------------------|------------------------|----------------|----------------|----------------|---------------|--------------|----------------------------|--------------------------|---------------------------|------------------------|

TPPH = Total petroleum hydrocarbons as gasoline by EPA Method 8260B; prior to July 9, 2001 analyzed by EPA Method 8015.

TEPH = Total petroleum hydrocarbons as diesel by modified EPA Method 8015.

BTEX = Benzene, toluene, ethylbenzene, xylenes by EPA Method 8260B; prior July 9, 2001 analyzed by EPA Method 8020.

MTBE = Methyl tertiary butyl ether

DIPE = Di-isopropyl ether, analyzed by EPA Method 8260B

ETBE = Ethyl tertiary butyl ether, analyzed by EPA Method 8260B

TAME = Tertiary amyl methyl ether, analyzed by EPA Method 8260B

TBA = Tertiary butyl alcohol, analyzed by EPA Method 8260B

TOC = Top of Casing Elevation

SPH = Separate-Phase Hydrocarbons

GW = Groundwater

DO = Dissolved Oxygen

ug/L = Parts per billion

ppm = Parts per million

MSL = Mean sea level

ft. = Feet

<n = Below detection limit

(D) = Duplicate sample

NA = Not applicable

NS = Not surveyed

Notes:

a = Chromatogram indicated an unidentified hydrocarbon.

b = The TEPH analysis was not performed because the sample containers were broken in the laboratory.

c = Well was inaccessible, able to gauge but not able to take DO reading.

d = Top of casing elevation altered during wellhead maintenance.

e = Hydrocarbon does not match pattern of laboratory's standard.

f = Hydrocarbon reported is in the early Diesel range, and does not match our Diesel standard.

* Field technician mistakenly sampled this well instead of OMW -11.

** Field technician mistakenly sampled this well instead of OMW-13.

DO readings are taken post-purge when wells are sampled and pre-purge in wells not sampled.

All wells except OMW-6, OMW-9, and OMW-13 surveyed March 18, 2002 by Virgil Chavez Land Surveying of Vallejo, CA.

ATTACHMENT B

Boring Logs

UNIFIED SOIL CLASSIFICATION SYSTEM

| MAJOR DIVISIONS | | LTR | DESCRIPTION | MAJOR DIVISIONS | | LTR | DESCRIPTION |
|----------------------------|------------------------------------|--|---|--------------------------|--------------------------------|--|---|
| COARSE GRAINED SOILS | GRAVEL AND GRAVELLY SOILS | GW | Well-graded gravels or gravel sand mixtures, little or no fines. | FINE GRAINED SOILS | SILTS AND CLAYS LL<50 | ML | Inorganic silts and very fine sands, rock flour, silty or clayey fine sands or clayey silts with slight plasticity. |
| | | GP | Poorly-graded gravels or gravel sand mixture, little or no fines. | | | CL | Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays. |
| | | GM | Silty gravels, gravel-sand-clay mixtures. | | | OL | Organic silts and organic silt-clays of low plasticity. |
| | GC | Clayey gravels, gravel-sand-clay mixtures. | MH | | | Inorganic silts, micaceous or diatomaceous fine sandy or silty soils, elastic silts. | |
| | SAND AND SANDY SOILS | SW | Well-graded sands or gravelly sands, little or no fines. | | SILTS AND CLAYS LL>50 | CH | Inorganic clays of high plasticity, fat clays. |
| | | SP | Poorly-graded sands or gravelly sands, little or no fines. | | | OH | Organic clays of medium to high plasticity. |
| | | SM | Silty sands, sand-silt mixtures. | | | PL | Peat and other highly organic soils. |
| | | SC | Clayey sands, sand-clay mixtures. | | | HIGHLY ORGANIC SOILS | |



Standard penetration split spoon sample



Modified California sampler



Shelby tube sample




Water level observed in boring

* No recovery

NFWE No free water encountered

NOTE: The lines separating strata on the logs represent approximate boundaries only. The actual transition may be gradual. No warranty is provided as to the continuity of soil strata between borings. Logs represent the soil section observed at the boring location on the date of drilling only.

J.H. KLEINFELDER & ASSOCIATES 
 GEOTECHNICAL CONSULTANTS • MATERIALS TESTING

IT/SHELL OIL COMPANY
 OAKLAND, CALIFORNIA

PLATE

BORING LOG LEGEND

PREPARED BY: BK DATE: 7/20/82

CHECKED BY: MLS DATE: 7/20/82

PROJECT NO. B-1232-1

| DEPTH IN FEET | DRY DENSITY lb/ft ³ | MOISTURE CONTENT % DRY WEIGHT | BLOW COUNT | SAMPLE | USES | DESCRIPTION | WELL CONST. |
|---------------|-----------------------------------|-------------------------------------|---------------|--------|------|---|----------------|
| | 0 | | | | | | Asphalt |
| | | | | | Fill | Subbase | |
| 2 | | | | | GC | Gravelly clay - black, moist, plastic, moderately stiff. | |
| 4 | | | 12 | 1-1 | | Temescal Formation. Gravelly clay - blue gray mottled brown, moist, moderately stiff to stiff, contains silt and sand. Gravel content grades in and out with some % zones. Gravels decrease, becoming stiff, slightly plastic. Grayish brown color becoming dominant. Drilling becomes harder. Gravels increase. Grading into sand/gravel/clay mixture, mottled, slight gas smell. | |
| 6 | | | | | | | |
| 8 | | | 30 | 1-2 | | | |
| 10 | | | | | | | |
| 12 | | | 15 | 1-3 | | | |
| 14 | | | | | | | |
| 16 | | | | | | | |
| 18 | | | 19 | 1-4 | | | |
| 20 | | | | | | | |
| 22 | | | | | | | |
| 24 | | | 22 | 1-5 | | | |
| 26 | | | | | | | |
| 28 | | | 18 | 1-6 | | | |
| 30 | | | | | | Bottom of boring at 30 ft. | |
| 32 | | | | | | | |

J.H. KLEINFELDER & ASSOCIATES 
 GEOTECHNICAL CONSULTANTS • MATERIALS TESTING

IT/SHELL OIL COMPANY
 OAKLAND, CALIFORNIA

LOG OF BORING NO. 1

PLATE


2

PREPARED BY: BK DATE: 7/20/82

CHECKED BY: MLS DATE: 7/20/82

PROJECT NO. B-1232-1

| DEPTH IN FEET | DRY DENSITY lb/ft ³ | MOISTURE CONTENT & DRY WEIGHT | BLOW COUNT | SAMPLE | USCS | DESCRIPTION | WELL CONST. |
|---------------|-----------------------------------|-------------------------------------|---------------|--------|------|---|----------------|
| 0 | | | | | | Asphalt | |
| | | | | | Fill | Subbase | |
| 2 | | | | | GC | Gravelly clay-black, moist, soft, plastic, some sand & silt. | |
| 4 | | | 15 | 2-1 | GC | Temescal Formation. Gravelly clay, blue gray, grayish brown, mottled, moist, stiff, plastic, gas odor | |
| 6 | | | | | | | |
| 8 | | | | | | | |
| 10 | | | 23 | 2-2 | | Increase in gravels, strong gas odor. | |
| 12 | | | | | | | |
| 14 | | | | | | Decrease in gravels. | |
| 16 | | | 22 | 2-3 | CL | Silty clay with few gravels, brown, mottled, moist, stiff, plastic | |
| 18 | | | | | | | |
| 20 | | | | | | | |
| 22 | | | 24 | 2-4 | | | |
| 24 | | | | | GC | Gravelly clay - brown, red brown, mottled, stiff to moderately stiff, some sand and silt with some high % gravel zones. | |
| 26 | | | 4 | 2-5 | | | |
| 28 | | | | | | | |
| 30 | | | | | | Bottom of boring at 30 ft. | |
| 32 | | | | | | | |

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 GEOTECHNICAL CONSULTANTS • MATERIALS TESTING

IT/SHELL OIL COMPANY
 OAKLAND, CALIFORNIA

PLATE


LOG OF BORING NO. 2


3

PREPARED BY: BK DATE: 7/20/82

CHECKED BY: MLS DATE: 7/20/82

PROJECT NO. B-1232-1

| DEPTH IN FEET | DRY DENSITY lb/ft ³ | MOISTURE CONTENT % DRY WEIGHT | BLOW COUNT | SAMPLE | USCS | DESCRIPTION | WELL CONST. |
|---------------|-----------------------------------|---|---------------|--------|------|---|----------------|
| | 0 | | | | | | Asphalt |
| | | | | | Fill | Subbase | |
| 2 | | | | | GC | Gravelly clay - black, moist, moderately stiff. | |
| 4 | | | 22 | 3-1 | CL | Temescal Formation. Silty clay - blue gray, brown mottled, moist, stiff, slightly plastic, some sand and gravels. | |
| 6 | | | | | | | |
| 8 | | | | | | | |
| 10 | | | | | | | |
| 12 | |  | | | | Brown color becomes dominant. Gravels increase. | |
| 14 | | | 22 | 3-2 | | Becoming gravelly clay, stiff to very stiff. | |
| 16 | | | | | | | |
| 18 | | | | | | | |
| 20 | | | | | | Decrease in gravels, siltier. | |
| 22 | | | | | | | |
| 24 | | | 13 | 3-3 | | Little gravels, moderately stiff, slight gas odor. | |
| 26 | | | | | | | |
| 28 | | | | | | Increase in sand. | |
| 30 | | | | | | Bottom of boring at 30 ft. | |
| 32 | | | | | | | |

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IT/SHELL OIL COMPANY
 OAKLAND, CALIFORNIA

LOG OF BORING NO. 3

PLATE


4

PREPARED BY: BK DATE: 7/20/82

CHECKED BY: MLS DATE: 7/20/82

PROJECT NO. B-1232-1

DEPTH IN FEET

| DEPTH IN FEET | DRY DENSITY lb/ft ³ | MOISTURE CONTENT & DRY WEIGHT | BLOW COUNT | SAMPLE | USCS | DESCRIPTION | WELL CONST. |
|---------------|-----------------------------------|---|---------------|--------|------|---|----------------|
| 0 | | | | | | Asphalt | |
| 2 | | | | | Fill | Subbase | |
| 4 | | | | | GC | Gravelly clay, black, moist, moderately stiff, some sand. | |
| 6 | | | | | GC | Temescal Formation, sand, gravel, clay mixture, brown, mottled, moderately stiff to stiff, slightly plastic, silty. | |
| 8 | | | | | | | |
| 10 | | | | | | | |
| 12 | |  | 22 | 4-1 | | | |
| 14 | | | | | | Increase in silt content. | |
| 16 | | | | | | | |
| 18 | | | | | | | |
| 20 | | | | | | | |
| 22 | | | 16 | 4-2 | | Becoming stiff. | |
| 24 | | | | | | | |
| 26 | | | | | | | |
| 28 | | | | | | Coarse material increase some sand lenses, more gravel. | |
| 30 | | | | | | | |
| 32 | | | 35 | 4-3 | | | |
| | | | | | | Bottom of boring at 31.5 ft. | |

J.H. KLEINFELDER & ASSOCIATES 
 GEOTECHNICAL CONSULTANTS • MATERIALS TESTING

IT/SHELL OIL COMPANY
 OAKLAND, CALIFORNIA

PLATE

5

LOG OF BORING NO. 4

PREPARED BY: BK DATE: 7/20/82

CHECKED BY: MLS DATE: 7/20/82

PROJECT NO. B-1232-1

| DEPTH IN FEET | DRY DENSITY lb/ft ³ | MOISTURE CONTENT % DRY WEIGHT | BLOW COUNT | SAMPLE | USCS | DESCRIPTION | WELL CONST. |
|---------------|-----------------------------------|-------------------------------------|---------------|--------|------|--|----------------|
| 0 | | | | | | Asphalt | |
| | | | | | Fill | Sub base | |
| 2 | | | | | CL | Silty clay - black, moist, moderately stiff. | |
| 4 | | | 19 | 5-1 | CL | Temescal Formation silty clay with gravel, brown, blue gray mottled moist, stiff, plastic | |
| 6 | | | | | | | |
| 8 | | | | | | | |
| 10 | | | | | | grading into | |
| 12 | | | | | GC | Gravelly clay - brown, mottled, stiff, non- plastic, some sand and silt | |
| 14 | | | 27 | 5-2 | | | |
| 16 | | | | | | gravels increase | |
| 18 | | | | | | | |
| 20 | | | | | | | |
| 22 | | | | | | Gravel/sand/clay mixture dense | |
| 24 | | | 17 | 5-3 | | | |
| 26 | | | | | | gravels up to 2 inches | |
| 28 | | | | | | | |
| 30 | | | | | | Bottom of boring 30 feet | |
| 32 | | | | | | | |

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 GEOTECHNICAL CONSULTANTS • MATERIALS TESTING

IT/SHELL OIL COMPANY
 OAKLAND, CALIFORNIA

PLATE

LOG OF BORING NO. 5

6

PREPARED BY: BK DATE: 7/20/82

CHECKED BY: MLS DATE: 7/20/82

PROJECT NO. B-1232-1

| DEPTH IN FEET | DRY DENSITY lb/ft ³ | MOISTURE CONTENT % DRY WEIGHT | BLOW COUNT | SAMPLE | USES | DESCRIPTION | MILL CONST. |
|---------------|-----------------------------------|-------------------------------------|---------------|--------|------|---|----------------|
| 0 | | | | | | Asphalt | |
| | | | | | Fill | Sub base | |
| 2 | | | 15 | 6-1 | GC | Gravelly clay - black, moist stiff, some sand and silt | |
| 4 | | | | | | | |
| 6 | | | | | GC | Temescal Formation Gravelly clay/clayey gravel brown, mottled, dense well graded | |
| 8 | | | | | | | |
| 10 | | | | | | | |
| 12 | | | 27 | 6-2 | | | |
| 14 | | | | | | | |
| 16 | | | | | | | |
| 18 | | | | | | | |
| 20 | | | | | | | |
| 22 | | | | | | Increase in silt with a decrease in gravels less dense | |
| 24 | | | 14 | 6-3 | | | |
| 26 | | | | | | | |
| 28 | | | | | | | |
| 30 | | | | | | Bottom of boring 30 feet | |
| 32 | | | | | | | |

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 GEOTECHNICAL CONSULTANTS • MATERIALS TESTING

IT/SHELL OIL COMPANY
 OAKLAND, CALIFORNIA

LOG OF BORING NO. 6

PLATE

7


PREPARED BY: BK DATE: 7/20/82


CHECKED BY: MLS DATE: 7/20/82


PROJECT NO. B-1232-1

| DEPTH IN FEET | DRY DENSITY lb/ft ³ | MOISTURE CONTENT & DRY WEIGHT | BLDW COUNT | SAMPLE | USES | DESCRIPTION | WELL CONST. |
|---------------|-----------------------------------|-------------------------------------|---------------|--------|------|--|----------------|
| 0 | | | | | | Asphalt | |
| | | | | | Fill | Sub base | |
| 2 | | | | | GC | Gravelly clay - black, soft moist, some sand | |
| 4 | | | | | CL | Temescal Formation silty clay with gravels brown, mottled, some blue gray, moderate stiff, plastic, gas odor | |
| 6 | | | | | | | |
| 8 | | | | | | | |
| 10 | | | | | | | |
| 12 | | ▽ | | | | | |
| 14 | | | | | | | |
| 16 | | | | | | Few gravels | |
| 18 | | | | | | | |
| 20 | | | | 7-1 | * | | |
| 22 | | | | | | | |
| 24 | | | | | | | |
| 26 | | | | | | | |
| 28 | | | | 7-2 | * | | |
| 30 | | | | | | Bottom of boring 30 feet | |
| 32 | | | | | | Note: due to height restrictions no drive samples taken | |

* - grab sample

| | | |
|---|---|-------------------|
| J.H. KLEINFELDER & ASSOCIATES GEOTECHNICAL CONSULTANTS • MATERIALS TESTING  | IT/SHELL OIL COMPANY OAKLAND, CALIFORNIA | PLATE 8 |
| | LOG OF BORING NO. 7 | |
| PREPARED BY: BK DATE: 7/20/82 | PROJECT NO. B-1232-1 | |
| CHECKED BY: MLS DATE: 7/20/82 | | |

| DEPTH IN FEET | DRY DENSITY lb/ft ³ | MOISTURE CONTENT & DRY WEIGHT | BLOW COUNT | SAMPLE | USCS | DESCRIPTION | WELL LOGS. |
|---------------|-----------------------------------|---|---------------|--------|------|---|---------------|
| 0 | | | | | | Asphalt | |
| | | | | | Fill | Sub base | |
| 2 | | | | | GC | Gravelly clay, black moist, moderately stiff | |
| 4 | | | | | CL | Temescal-Formation Gravelly clay - blue gray, brown, mottled, moist, moderately stiff to stiff, slightly plastic, some silt and sand, gas odor | |
| 6 | | | | | | | |
| 8 | | | | | | | |
| 10 | | | 16 | 8-1 | | | |
| 12 | |  | | | | becoming brown | |
| 14 | | | | | | | |
| 16 | | | | | | | |
| 18 | | | | | | grading into silty clay with gravel, grayish brown, very stiff, plastic, some sand. | |
| 20 | | | 33 | 8-2 | | | |
| 22 | | | | | | | |
| 24 | | | | | | | |
| 26 | | | | | | decrease in sand and gravel | |
| 28 | | | | | | | |
| 30 | | | 16 | 8-3 | | | |
| 32 | | | | | | Bottom of boring 31.5 feet | |

J.H. KLEINFELDER & ASSOCIATES 
 GEOTECHNICAL CONSULTANTS • MATERIALS TESTING

IT/SHELL OIL COMPANY
 OAKLAND, CALIFORNIA

PLATE

LOG OF BORING NO. 8

9

PREPARED BY: BK DATE: 7/20/82

CHECKED BY: MLS DATE: 7/20/82

PROJECT NO. B-1232-1

UNIFIED SOIL CLASSIFICATION SYSTEM

| MAJOR DIVISIONS | | LTR | DESCRIPTION | MAJOR DIVISIONS | | LTR | DESCRIPTION | | |
|----------------------------|------------------------------------|-----|---|--------------------------|--------------------------------|----------------------------|---|--|--|
| COARSE GRAINED SOILS | GRAVEL AND GRAVELLY SOILS | GW | Well-graded gravels or gravel sand mixtures, little or no fines. | FINE GRAINED SOILS | SILTS AND CLAYS LL<50 | ML | Inorganic silts and very fine sands, rock flour, silty or clayey fine sands or clayey silts with slight plasticity. | | |
| | | GP | Poorly-graded gravels or gravel sand mixture, little or no fines. | | | CL | Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays. | | |
| | | GM | Silty gravels, gravel-sand-clay mixtures. | | | OL | Organic silts and organic silt-clays of low plasticity | | |
| | | GC | Clayey gravels, gravel-sand-clay mixtures. | | | MH | Inorganic silts, micaceous or diatomaceous fine sandy or silty soils, elastic silts | | |
| | SAND AND SANDY SOILS | SU | Well-graded sands or gravelly sands, little or no fines. | | SILTS AND CLAYS LL>50 | CH | Inorganic clays of high plasticity, fat clays. | | |
| | | SP | Poorly-graded sands or gravelly sands, little or no fines. | | | OH | Organic clays of medium to high plasticity. | | |
| | | SM | Silty sands, sand-silt mixtures. | | | Pt | Peat and other highly organic soils. | | |
| | | SC | Clayey sands, sand-clay mixtures. | | | | | | |
| | | | | | | HIGHLY ORGANIC SOILS | | | |

| U.S. STANDARD SERIES SIEVE | | | | CLEAR SQUARE SIEVE OPENINGS | | | |
|----------------------------|------|--------|--------|-----------------------------|--------|---------|----------|
| 200 | 40 | 10 | 4 | 3/4" | 3" | 12" | |
| SILTS AND CLAYS | SAND | | | GRAVEL | | COBBLES | BOULDERS |
| | FINE | MEDIUM | COARSE | FINE | COARSE | | |

GRAIN SIZES

▼ Water level observed in boring

* No recovery

NFWE No free water encountered

NOTE: The lines separating strata on the logs represent approximate boundaries only. The actual transition may be gradual. No warranty is provided as to the continuity of soil strata between borings. Logs represent the soil section observed at the boring location on the date of drilling only.



DESIGNED BY :

DRAWN BY :

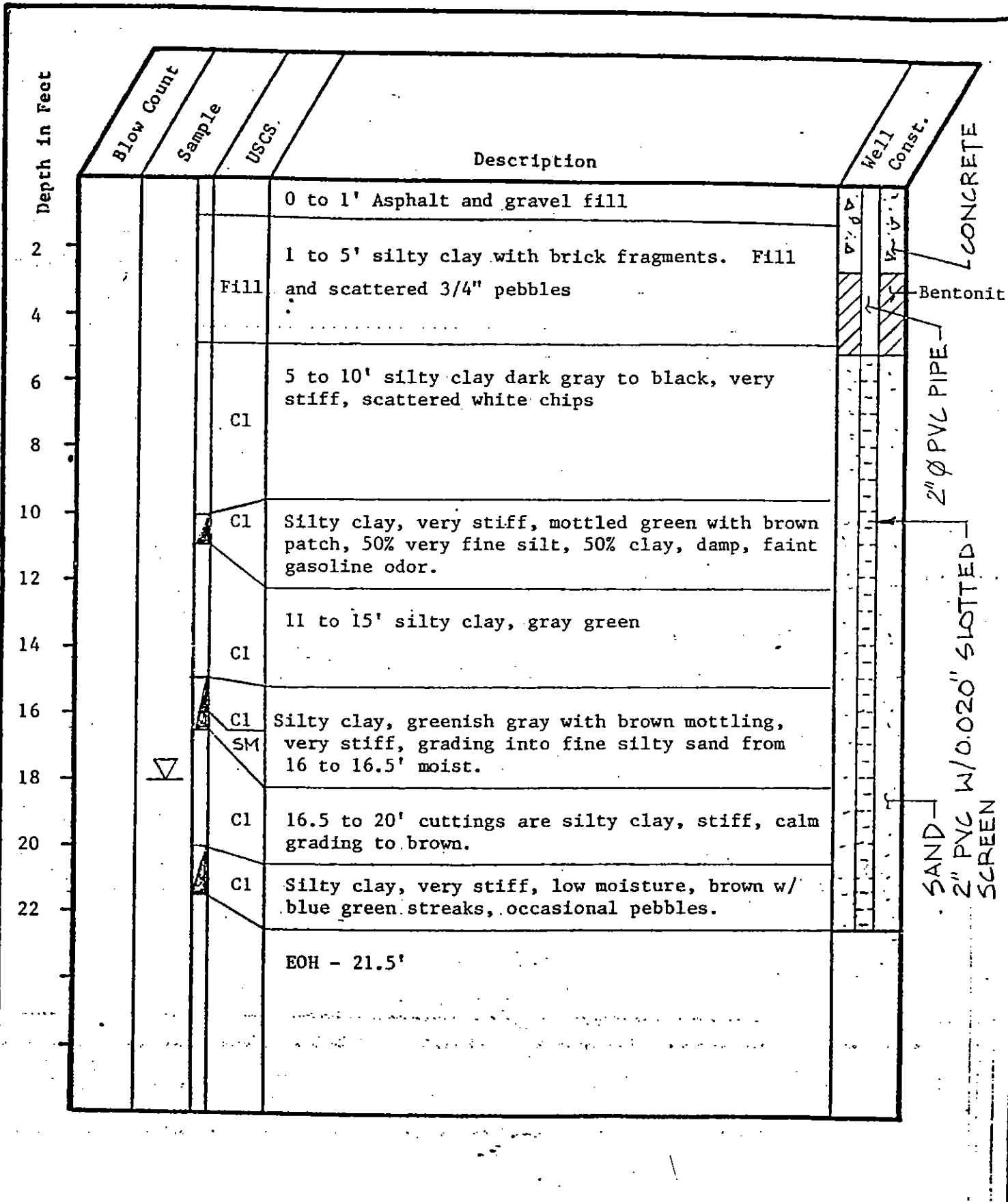
PROJECT NO :

SCALE :

DATE :

PLATE

1



IT Enviroscience
 1815 Arnold Drive • Martinez, CA 94553
 Telephone (415) 228-8400

PREPARED BY: RMG
 CHECKED BY:

SHELL OIL COMPANY
 500 40th Street
 Oakland, California

LOG OF BORING NO. E-9
 PROJECT NO. 1-3522

PLATE
 2

| Depth in Feet | Blow Count | Sample | USCS | Description | Well Const. |
|---------------|------------|--------|------|--|---|
| 0 - 2 | | | | 0 - 1' Asphalt and gravel fill | |
| 2 - 10 | | | Cl | 1 - 10' silty clay, very stiff, gray green | BENTONITE 2" Ø PVC PIPE |
| 10 - 10.5 | | | SW | 10 - 10.5 gravel 1/8 to 1/4", loose with strong gasoline odor. | |
| 10.5 - 11.5 | | | Cl | 10.5 - 11.5 silty clay, gray green, stiff, scattered pebbled throughout, faint gasoline odor. | |
| 11.5 - 15 | | | Cl | 11.5 - 15 cuttings are very stiff, blue green clay, 10% silt, little moisture. | |
| 15 - 16.5 | | | Cl | Silty clay, very stiff, crumbly, low moisture, blue green w/mottled brown patches, 40% silt, 59% clay, 1% pebbles. | |
| 16.5 - 20 | | | Cl | 16.5 to 20' gradational change to brown, plastic silty clay, 10% silt, little moisture. | |
| 20 - 21.5 | | | Cl | Silty clay, very stiff, crumbly, low moisture, 30% silt, 70% clay. Dark brown with pale blue green color along vertical fractures. | SAND 2" PVC W/0.020" SLOTTED SCREEN |
| 21.5 - 22 | | | Cl | EOH 21.5' | |
| 22 - 23 | | | | Well dry at 12:00 - 7/21/83 | |
| 23 - 24 | | | | | |
| 24 - 25 | | | | | |
| 25 - 26 | | | | | |
| 26 - 27 | | | | | |
| 27 - 28 | | | | | |
| 28 - 29 | | | | | |
| 29 - 30 | | | | | |
| 30 - 31 | | | | | |
| 31 - 32 | | | | | |
| 32 - 33 | | | | | |
| 33 - 34 | | | | | |
| 34 - 35 | | | | | |
| 35 - 36 | | | | | |
| 36 - 37 | | | | | |
| 37 - 38 | | | | | |
| 38 - 39 | | | | | |
| 39 - 40 | | | | | |
| 40 - 41 | | | | | |
| 41 - 42 | | | | | |
| 42 - 43 | | | | | |
| 43 - 44 | | | | | |
| 44 - 45 | | | | | |
| 45 - 46 | | | | | |
| 46 - 47 | | | | | |
| 47 - 48 | | | | | |
| 48 - 49 | | | | | |
| 49 - 50 | | | | | |

IT Enviroscience

1315 Arnold Drive • Martinez, CA 94553
Telephone (415) 228-8400

SHELL OIL COMPANY
500 40th Street
Oakland, California

PLATE

3

PREPARED BY: RMG

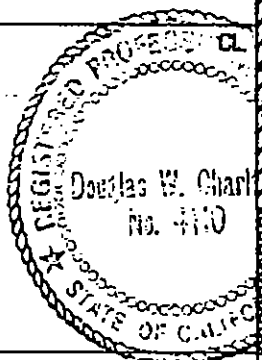
LOG OF BORING NO. B-10

CHECKED BY:

PROJECT NO.: 1-3532

LOG OF BORING NO. MW-2

| DATE DRILLED: 5/22/89 | | ELEVATION: | | WL TAKEN: 05-22-89 | | EQUIPMENT: 8"x 3-3/4" & 12"x 8" | | | | | |
|-----------------------|--------|-------------|--------|--------------------|-----------------|---------------------------------|---|-------------------|-----------|----------------|-------|
| DEPTH (ft) | SAMPLE | WATER LEVEL | SYMBOL | MOISTURE | PLASTICITY | COLOR | DESCRIPTION | WELL CONSTRUCTION | BLOWS/FT. | T.P.H Hg/Kg | TESTS |
| 5 | D | | | moist | loose | brown | SANDY GRAVEL (Fill) SP-GP | | 11 | | |
| | | | | | soft | black | GRAVELLY CLAY Glass and brick fragments and asphalt fragments | | | | |
| 10 | D | | | moist | stiff | | SILTY CLAY | | 33 | | |
| | | | | | moist | stiff | tan mottled gray rust | | | | |
| 15 | D | | | | | brown | | | 48 | | |
| | | | | | | black | SILTY CLAY Some fine sand | | | | |
| 20 | D | | | | dense | gray | SANDY GRAVEL Trace silt | | 73 | | |
| | | | | | stiff | mottled tan rust | SILTY CLAY | | | | |
| 25 | D | | | | medium dense | | Fine SANDY GRAVEL (angular) | | 36 | | |
| | | | | | medium dense | gray mottled rust | SILTY CLAY Lenses sand | | | | |
| 30 | D | | | wet | loose | tan | GRAVELLY SAND | | 13 | | |
| | | | | | very moist | loose | gray | | | | |
| 35 | | | | | | | | | 31 | | |
| 40 | | | | | | | | | 23 | | |
| 45 | | | | | | | | | 10 | | |



SHELL OIL COMPANY
500 40th street
Oakland, California

Project No.
88-44-361-01

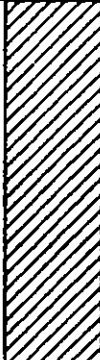



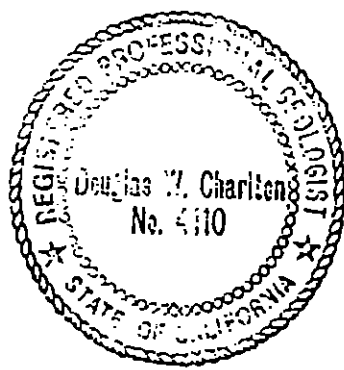
Converse Environmental Consultants California

Drawing No.
A-1

LOG OF BORING NO.MW-2

continued - page 2

| DEPTH (ft) | SAMPLE | WATER LEVEL | SYMBOL | MOISTURE | PLASTICITY | COLOR | DESCRIPTION | WELL CONSTRUCTION | BLOCKS/FT. | T.P.H Hg/Kg | TESTS |
|------------|--------|-------------|---|------------|------------|------------------|-----------------------------|---|------------|----------------|-------|
| 25 | | |  | very moist | medium | tan mottled rust | SILTY CLAY and fine SAND CL |  | 14 | | |
| | | | | | | brown | SILTY CLAY Lenses sand | | 53 | | |
| 30 | | | | | | | Bottom of Hole at 25 ft. | | | | |
| 35 | | | | | | | | | | | |
| 40 | | | | | | | | | | | |



SHELL OIL COMPANY
500 40th Street
Oakland, California

Project No.
88-44-361-01

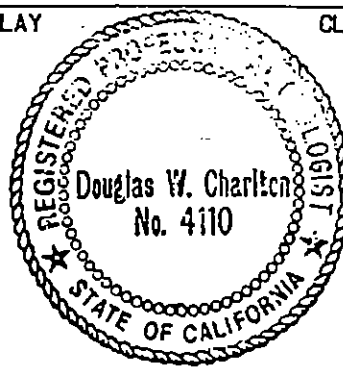


Converse Environmental Consultants California

Drawing No.
A-2

LOG OF BORING NO. MW-3

| DATE DRILLED: 5/23/89 | | ELEVATION: | | WL TAKEN: 5/23/89 | | EQUIPMENT: 8"x 3-3/4" & 12"x 8" | | | | | |
|-----------------------|--------|-------------|--------|-------------------|--------------|---------------------------------|--|-------------------|-----------|--------------|-------|
| DEPTH (ft) | SAMPLE | WATER LEVEL | SYMBOL | MOISTURE | PLASTICITY | COLOR | DESCRIPTION | WELL CONSTRUCTION | BLOWS/FT. | T.P.H. Mg/Kg | TESTS |
| 5 | D | | | moist | loose | brown | SANDY GRAVEL (Fill) GP | | 13 | | |
| | | | | moist | stiff | black mottled tan | SILTY CLAY CL | | | | |
| 10 | D | | | | medium dense | tan mottled rust | GRAVEL LENS GP | | 38 | | |
| | | | | | stiff | | SILTY CLAY Trace gravel CL | | | | |
| 15 | D | | | | medium dense | gray mottled tan | | | 32 | | |
| | | | | | stiff | | | | | | |
| 20 | D | | | | medium dense | tan | Fine SAND with angular GRAVEL some silt GM | | 49 | | |
| | | | | | stiff | tan mottled gray | SILTY CLAY Trace gravel CL | | | | |
| 25 | D | | | very moist | | | Some fine sand | | 13 | | |
| | | | | wet | | tan mottled rust | LENS SANDY CLAY GC | | | | |
| 30 | D | | | very moist | | | SILTY CLAY CL | | 28 | | |
| | | | | | | | | | | | |
| 35 | D | | | | very stiff | | | | 27 | | |
| | | | | | | | | | | | |
| 40 | D | | | moist | very stiff | tan | SILTY CLAY CL | | 17 | | |
| 45 | | | | | | | Bottom of Hole at 21 ft. | | 45 | | |



SHELL OIL COMPANY
500 40th Street
Oakland, California

Project No.
88-44-361-01



Converse Environmental Consultants California

Drawing No.
A-3

LOG OF BORING NO. MW-5

| DATE DRILLED: 9-19-89 | | ELEVATION: | | WL TAKEN: 9-19-89 | | EQUIPMENT: 8"x 12" Hollow Stem Auger | | | | | |
|-----------------------|----------------------|----------------------------------|----------------|-------------------|-----------------------------------|--|-----------------------------|-----------|--------------|--------------|----|
| DEPTH (ft) | SAMPLE WATER LEVEL | SYMBOL | MOISTURE | CONSISTENCY | COLOR | DESCRIPTION | WELL CONSTRUCTION | BLOMS/FT. | O.V.H. (ppm) | T.P.H. (ppm) | |
| 1 | [Water Level Symbol] | [Symbol: Gravelly Sand and Silt] | slightly moist | medium dense | dark brown | Gravelly SAND and SILT some rubble (Fill) | [Well Construction Diagram] | 9 | 0 | | |
| | | [Symbol: Sandy Silt] | | medium | | Sandy SILT increasing Clay | | | | | ML |
| | | [Symbol: Silty Clay] | | | brown | Silty CLAY trace Sand, trace Gravel | | | | | CL |
| | | [Symbol: Silty Clay] | | | brown mottled gray | Silty CLAY and fine SAND black tubelets | | | | | CL |
| 5 | | | | | | | | | | | |
| 2 | | | | | | | | | | | |
| 10 | | | | | | | | | | | |
| 3 | | | moist | medium | light brown mottled rust and gray | Sandy CLAY som Silt | CL | 14 | 0 | | |
| 15 | | | moist | medium | | Fine Sandy CLAY and SILT | CL | 15 | | | |
| | | | very moist | | | | | | | | |
| | | | wet | | | | | | | | |
| 20 | | | | | | Total Depth of Boring: 20 ft. Below Ground Surface | | | | | |

SHELL OIL COMPANY
500 40th Street
Oakland, California

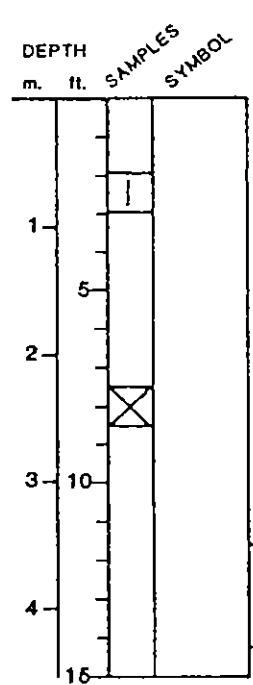
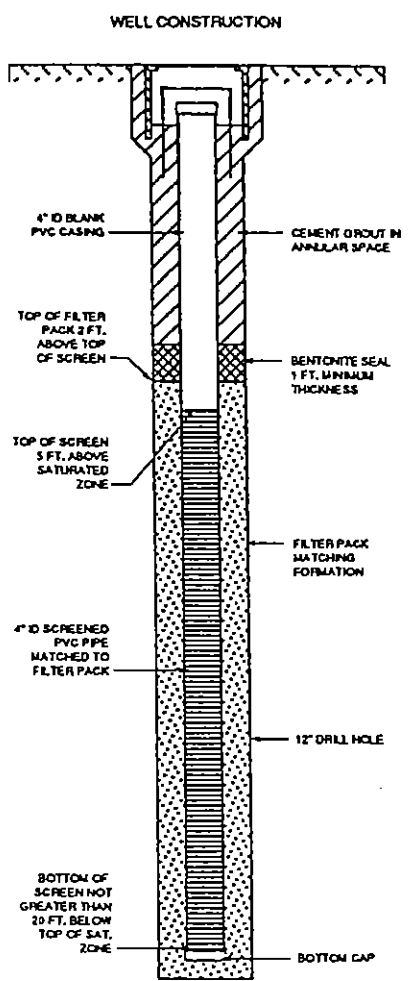
Project No.
88-44-361-01



Converse Environmental Consultants California

Drawing No.
A-2

| MAJOR DIVISIONS | | SYMBOLS | TYPICAL NAMES |
|---|--|--|--|
| COARSE GRAINED SOILS More than half is larger than No. 200 sieve | GRAVELS More than half coarse fraction is larger than No. 4 sieve | Clean gravels with little or no fines | GW Well graded gravels, gravel-sand mixtures |
| | | | GP Poorly graded gravels, gravel-sand mixtures |
| | | Gravels with over 12% fines | GM Silty gravels, poorly graded gravel-sand-silt mixtures |
| | | | GC Clayey gravels, poorly graded gravel-sand-clay mixtures |
| | SANDS More than half coarse fraction is smaller than No. 4 sieve | Clean sands with little or no fines | SW Well graded sands, gravelly sands |
| | | | SP Poorly graded sands, gravelly sands |
| | | Sands with over 12% fines | SM Silty sands, poorly graded sand-silt mixtures - |
| | | | SC Clayey sands, poorly graded sand-clay mixtures |
| FINE GRAINED SOILS > half is smaller than No. 200 sieve | SILTS AND CLAYS Liquid limit less than 50 | ML Inorganic silts and very fine sands, rock flour, silty or clayey fine sands, or clayey silts with slight plasticity | |
| | | CL Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays | |
| | | OL Organic clays and organic silty clays of low plasticity | |
| | SILTS AND CLAYS Liquid limit greater than 50 | MH Inorganic silts, micaceous or diatomaceous fine, sandy or silty soils, elastic silts | |
| | | CH Inorganic clays of high plasticity, fat clays | |
| | | OH Organic clays of medium to high plasticity, organic silts | |
| HIGHLY ORGANIC SOILS | Pt Peat and other highly organic soils | | |



SAMPLE TYPE

DRIVE SAMPLE, 2.5" ID Sampler, driven with 140 lb. weight, 30" drop

NO RECOVERY

Water level at time of drilling

Stabilized water level on date noted

Note:

Soil conditions indicated by boring logs apply only at the location of the particular boring and at the time of drilling. Subsurface conditions may differ at other locations and may change at the boring location with the passage of time. Data presented in the logs represent a simplification of the actual conditions encountered.

UNIFIED SOIL CLASSIFICATION AND BORING LOG SYMBOLS

Scale _____ Project No. _____

Prepared by _____ Date _____

Checked by _____ Drawing No. _____

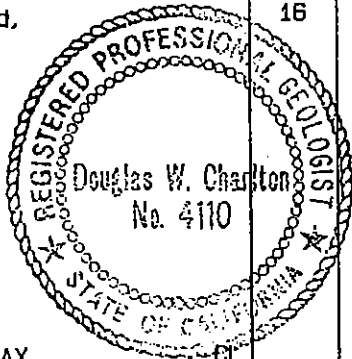
Approved by _____ A 1



Converse Environmental
Consultants California

LOG OF BORING NO. CSB-1

| DATE DRILLED: 10-17-89 | | ELEVATION: | | WL TAKEN: n/a | | EQUIPMENT: 3 3/4" x 8" Hollow-Stem Auger | | | | |
|------------------------|--------|------------|------------|---------------|--------------------------|---|-----------|--------------|--------------------------------|-------|
| DEPTH (ft) | SAMPLE | SYMBOL | MOISTURE | CONSISTENCY | COLOR | DESCRIPTION | BLOWS/FT. | O.V.M. (ppm) | DRY DENSITY lb/ft ³ | TESTS |
| 5 | 1 | A A A A | moist | loose | dark brown | Gravelly SAND and SILT, some Rubble, some Asphalt. (Fill) | SW | | | |
| | | A A A A | | | dark gray | | | | | |
| | | A A A A | moist | medium | dark brown | Silty CLAY, trace Gravel, trace Sand. | CL | | | |
| | | A A A A | very moist | medium | | Decreasing Gravel and Sand, bits of brick in cuttings. | 8 | | | |
| 10 | 2 | A A A A | moist | medium | light gray | Silty CLAY, some Sand and Gravel. No odor. | 18 | 0 | | |
| | | A A A A | moist | medium | light brown | | CL | | | |
| 15 | 3 | A A A A | moist | medium | light brown mottled gray | Silty CLAY, some fine Sand, trace Gravel. | 16 | 0 | | |
| | | A A A A | moist | stiff | light brown | Fine Sandy CLAY. No odor. | CL | 17 | 0 | |
| 20 | 4 | A A A A | moist | stiff | light brown | Fine Sandy CLAY. No odor. | CL | 17 | 0 | |



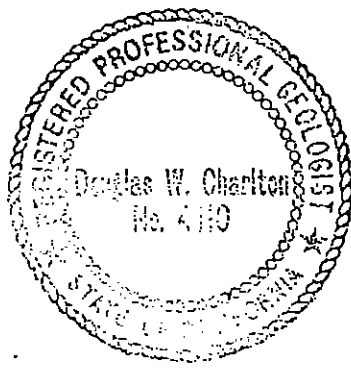
SHELL OIL COMPANY
 500 40th Street
 Oakland, California

Project No.
 88-44-361-0

LOG OF BORING NO. CSB-1

continued - page 2

| DEPTH (ft) | SAMPLE WATER LEVEL | SYMBOL | MOISTURE | CONSISTENCY | COLOR | DESCRIPTION | BLMS/FT. | D.V.M. (ppm) | DRY DENSITY lb/ft ³ | TESTS |
|------------|--------------------|--------|----------|-------------|-------------|---|----------|--------------|--------------------------------|-------|
| | | | moist | stiff | light brown | Fine Sandy CLAY. No odor. CL | | | | |
| 5 | | | | medium | light brown | Silty CLAY, water bearing lenses. No odor. CL | 13 | 0 | | |
| 25 | | | | | | Total Depth of Boring: 25 ft. Below Ground Surface. | | | | |
| 30 | | | | | | | | | | |
| 35 | | | | | | | | | | |
| 40 | | | | | | | | | | |

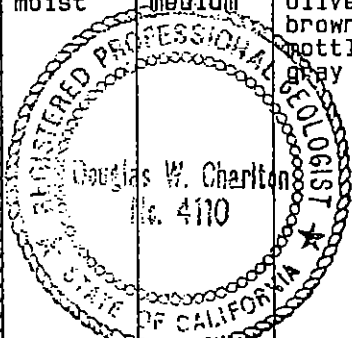


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Project No.
 88-44-361-0

LOG OF BORING NO. OMW-6

| DATE DRILLED: 10-16-89 | | ELEVATION: | | WL TAKEN: n/a | | EQUIPMENT: 3 3/4" x 8" Hollow-Stem Auger | | | | |
|------------------------|--------|------------|----------|---------------|--------------------------|--|-------------------|-----------|--------------|-------------|
| DEPTH (ft) | SAMPLE | SYMBOL | MOISTURE | CONSISTENCY | COLOR | DESCRIPTION | WELL CONSTRUCTION | BLOWS/FT. | O.V.M. (ppm) | T.P.H. (mm) |
| | | A A A | moist | loose | light brown | Gravelly SAND (Fill). | SW | | | |
| | | / / / | moist | medium | dark black | Silty CLAY, trace Gravel. Slight petroleum odor. | CL | | 2.6 | |
| 1 | | / / / | moist | medium | olive mottled black | Silty CLAY, decreasing Gravel. Slight petroleum odor. | CL | 14 | 0 | |
| 5 | | / / / | moist | medium | olive brown mottled gray | Sandy CLAY, some Silt. Trace shell fragments. Strong petroleum odor. | CL | 10 | 82 | |
| 10 | | / / / | moist | medium | | Black tubelets. | CL | 10 | 0 | |
| 15 | | / / / | | | tan brown | | | | | |
| 20 | | / / / | wet | stiff | | Silty CLAY, trace Sand. | CL | 20 | 0 | |

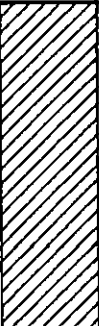
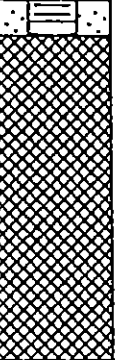




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Project No.
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LOG OF BORING NO.OMW-6

continued - page 2

| DEPTH (FT) | SAMPLE | WATER LEVEL | SYMBOL | MOISTURE | CONSISTENCY | COLOR | DESCRIPTION | WELL CONSTRUCTION | BLOWS/FT. | D.V.M. (ppm) | T.P.H. (ppm) |
|------------|--------|-------------|---|----------|-------------|-----------|---|---|-----------|--------------|--------------|
| | | |  | wet | stiff | tan brown | Silty CLAY, trace Sand. CL |  | | 0 | |
| 25 | | |  | moist | stiff | lt brown | Silty CLAY. Sandy CLAY lens. No odor. CL |  | 8 | 0 | |
| 30 | | | | | | | Total Depth of Boring: 25 ft Below Ground Surface. | | | | |
| 35 | | | | | | | | | | | |
| 40 | | | | | | | | | | | |



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





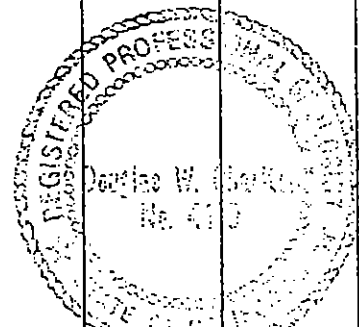
Converse Environmental West

Drawing No.
A-5

LOG OF BORING NO. OMW-9

DATE DRILLED: 10-17-89 ELEVATION: WL TAKEN: n/a EQUIPMENT: 3 3/4" x 8" Hollow-Stem Auger

| DEPTH (ft) | SAMPLE | WATER LEVEL | SYMBOL | MOISTURE | CONSISTENCY | COLOR | DESCRIPTION | WELL CONSTRUCTION | BLOCKS/FT. | O.V.H. (ppm) | T.P.H. (ppm) |
|------------|--------|-------------|---|----------------|-------------|-------------|---|---|------------|--------------|--------------|
| | | |  | moist | loose | light brown | Silty SAND and GRAVEL. SM/GM (Fill) | | | | |
| | | |  | moist | medium | black | Silty CLAY, trace fine Sand. CL |  | | | |
| 1 | | |  | moist | medium | dark olive | Fine Sandy CLAY, trace Gravel. Petroleum odor. CL |  | 15 | 0 | |
| 5 | | |  | slightly moist | stiff | light olive | Fine Sandy CLAY, some angular Gravel. Strong Petroleum odor. CL |  | 11 | 126 | |
| 10 | | |  | slightly moist | stiff | tan brown | Fine Sandy CLAY, trace Gravel, mottled gray. CL |  | 13 | 0 | |
| 15 | | |  | wet | loose | lt. brwn | F. SAND and GRAVEL lens. SP/GP |  | 25 | 0 | |
| 20 | | |  | moist | medium | black | Silty CLAY, some decaying shells. No odor. CL |  | | | |






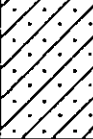


SHELL OIL COMPANY
500 40th Street
Oakland, California

Project No.
88-44-361-0

Drawing No.
A-6

LOG OF BORING NO.OMW-9

continued - page 2

| DEPTH (ft) | SAMPLE | WATER LEVEL | SYMBOL | MOISTURE | CONSISTENCY | COLOR | DESCRIPTION | WELL CONSTRUCTION | BLOWS/FT. | O.V.H. (ppm) | T.P.H. |
|------------|--------|-------------|---|------------|-------------|-----------------|--|--|-----------|--------------|--------|
| | | |  | moist | medium | black | Silty CLAY, some decaying shells. No odor. CL |  | | | |
| 5 | | |  | very moist | medium | light tan brown | Very fine Sandy CLAY, gray mottles. CL | | 18 | 0 | |
| 25 | | |  | wet | medium | light tan brown | Clayey fine SAND, thin lenses of Sandy Clay. SC |  | 16 | | |
| | | |  | | | | | | 12 | | |
| | | | | | | | | | 14 | | |
| | | | | very moist | | light brown | Silty fine SAND, rust mottles. SC | | 7 | | |
| 30 | | | | | | | | | 10 | | |
| | | | | | | | Total Depth of Boring: 30 ft Below Ground Surface. | | | | |
| 35 | | | | | | | | | | | |
| 40 | | | | | | | | | | | |



SHELL OIL COMPANY
500 40th Street
Oakland, California

Project No.
88-44-361-C

LOG OF BORING NO. OMW-10

| DATE DRILLED: 11-13-89 | | ELEVATION: | | WL TAKEN: n/a | | EQUIPMENT: 3 3/4" x 8" Hollow-Stem Auger. | | | | |
|------------------------|--------------------|------------|----------------|---------------|-------------|---|-------------------|-----------|--------------|-------------|
| DEPTH (ft) | SAMPLE WATER LEVEL | SYMBOL | MOISTURE | CONSISTENCY | COLOR | DESCRIPTION | WELL CONSTRUCTION | BLOWS/FT. | O.V.M. (ppm) | T.P.H. (mm) |
| | | | | | light brown | Silty SAND and GRAVEL baserock. | SM/GM | | | |
| | | | moist | medium | black | Silty CLAY, trace fine Sand, stained olive. | CL | | 0 | |
| | | | | | | Increasing staining. | | | | |
| 1 | | | slightly moist | medium | dark gray | Fine Sandy CLAY, trace Gravel, stained olive. No odor. | CL | 18 | 0 | |
| 5 | | | | | | Increasing SAND and GRAVEL. | | | | |
| 2 | | | slightly moist | medium | dark gray | Fine to medium Sandy CLAY, little Gravel. Mottled olive and rust stains. | CL | 14 | 0 | |
| 10 | | | | | | | | | | |
| 3 | | | moist | stiff | light brown | Silty CLAY, trace fine Sand | | 16 | 0 | |
| 15 | | | | | | | | | | |
| | | | wet | | lt. brwn. | F to m Sand, GRYL, tr Cly. | GW | 23 | 0 | |
| 20 | | | v. moist | medium | | F. Sandy CLAY, tr Gravel. | CL | | | |



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Project No.
88-44-361-0


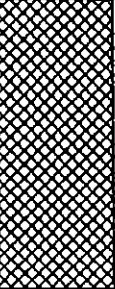



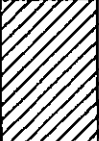
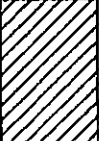


Converse Environmental West

Drawing No.
A-8

LOG OF BORING NO.OMW-10

continued - page 2

| DEPTH (ft) | SAMPLE | WATER LEVEL | SYMBOL | MOISTURE | CONSISTENCY | COLOR | DESCRIPTION | WELL CONSTRUCTION | BLDGS/FT. | D.V.M. (ppm) | T.P.H. (cont) |
|------------|--------|-------------|---|----------|-------------|------------|--|---|-----------|--------------|---------------|
| P | | |  | v. moist | | lt. brwn. | F. Sandy CLAY, tr. Gravel. CL |  | 22 | 0 | |
| | | |  | moist | | | Clayey f. SAND, lt. Grvl. SC | | | | |
| | | |  | moist | medium | | F. Sandy CLAY, lt. Gravel. CL | | | | |
| | | |  | v. moist | m. dense | lt. brwn. | Fine Sandy GRAVEL. GP | | | | |
| | | |  | | | | Fine Sandy CLAY. CL | | | | |
| | P | |  | moist | medium | gray brown | Fine Sandy CLAY, rust stains. CL | 7 | 10 | 0 | |
| 25 | | | | | | | Total Depth of Boring: 24 ft Below Ground Surface. | | | | |
| 30 | | | | | | | | | | | |
| 35 | | | | | | | | | | | |
| 40 | | | | | | | | | | | |



SHELL OIL COMPANY
500 40th Street
Oakland, California

Project No.
88-44-361-0

Drawing No.
A-9

LOG OF BORING NO. EW-1

DATE DRILLED: 6/28/90 EL: n/a WL TAKEN: n/a EQUIPMENT: 3.75"x 8" / 7.25"x 12" H.S.A

| DEPTH (ft) | SAMPLE | WATER LEVEL | SYMBOL | MOISTURE | CONSISTENCY | COLOR | DESCRIPTION | WELL CONSTRUCTION | BLOWS/FT. | O.V.N. (ppm) | T.P.H. (ppm) |
|------------|--------|-------------|--------|----------------|--------------|---------------|--------------------------------------|-------------------|-----------|--------------|--------------|
| | | | | moist | loose | light brown | 0.2' CONCRETE. Pea GRAVEL. (F111) | | | | |
| | | | | moist | medium | black | Silty CLAY, trace Gravel. | CL | | | |
| 5 | 1 | | | | | dark gray | Gravelly CLAY. | CL | 5 | | |
| | | | | moist | medium dense | tan | Fine SAND. | SP | 6 | | |
| | | | | | loose | tan | Fine SAND. | SP | 2 | | |
| | | | | slightly moist | stiff | dark gray | Silty CLAY. | CL | 8 | | |
| | | | | slightly moist | stiff | dark gray | Silty CLAY. | CL | 5 | | |
| | | | | slightly moist | stiff | dark gray | Silty CLAY, some fine Sand. | CL | 9 | | |
| 10 | 2 | | | moist | dense | | Clayey GRAVEL. | GC | 17 | | |
| | | | | | medium dense | dark gray | Clayey GRAVEL. | GC | 15 | | |
| | | | | | dense | dark gray | Clayey GRAVEL. | GC | 12 | | |
| | | | | slightly moist | very stiff | tan | Silty CLAY. | CL | 14 | | |
| | | | | slightly moist | very stiff | tan | Silty CLAY. | CL | 16 | | |
| | | | | slightly moist | very stiff | tan | Silty CLAY, trace Gravel. | CL | 7 | | |
| | | | | slightly moist | very stiff | tan | Silty CLAY, trace Gravel. | CL | 18 | | |
| | | | | slightly moist | very stiff | tan | Silty CLAY, trace Gravel. | CL | 15 | | |
| 15 | 3 | | | slightly moist | very stiff | grayish brown | Silty CLAY. | CL | 14 | | |
| | | | | slightly moist | very stiff | tan | Silty CLAY, trace Gravel. | CL | 15 | | |
| | | | | slightly moist | very stiff | tan | Silty CLAY, trace Gravel. | CL | 11 | | |
| | | | | slightly moist | very stiff | tan | Silty CLAY, trace Gravel. | CL | 10 | | |
| | | | | slightly moist | very stiff | tan | Silty CLAY, trace Gravel. | CL | 14 | | |
| | | | | slightly moist | very stiff | tan | Silty CLAY, trace Gravel. | CL | 18 | | |
| | | | | slightly moist | very stiff | tan | Silty CLAY, trace Gravel. | CL | 20 | | |
| | | | | slightly moist | very stiff | tan | Silty CLAY, trace Gravel. | CL | 10 | | |
| | | | | slightly moist | very stiff | tan | Silty CLAY, trace Gravel. | CL | 15 | | |
| | | | | slightly moist | very stiff | tan | Silty CLAY, trace Gravel. | CL | 19 | | |
| | | | | slightly moist | very stiff | tan | Silty CLAY, trace Gravel. | CL | 21 | | |
| | | | | slightly moist | very stiff | tan | Silty CLAY, trace Gravel. | CL | 7 | | |
| 20 | 4 | | | slightly moist | very stiff | light brown | Silty Clay, tr fine Sand. | CL | 18 | | |
| | | | | slightly moist | very stiff | light brown | Silty CLAY. | CL | 7 | | |
| | | | | slightly moist | very stiff | light brown | Silty CLAY. | CL | 18 | | |

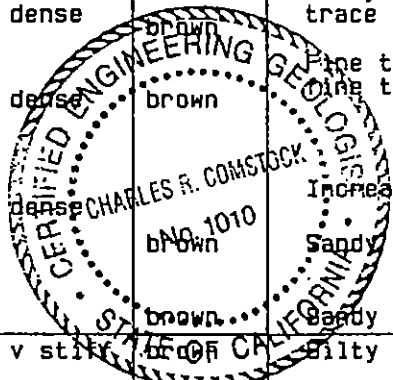
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500 40th Street
Oakland, California

Project No.
88-44-361-2

LOG OF BORING NO. EW-1

continued - page 2

| DEPTH (ft) | SAMPLE | WATER LEVEL | SYMBOL | MOISTURE | CONSISTENCY | COLOR | DESCRIPTION | MELL CONSTRUCTION | BLOWS/BLK. | D.V.M. (ppm) | T.P.H. (ppm) |
|------------|--------|-------------|--------|----------------|--------------|---------------|--|-------------------|------------|--------------|--------------|
| | S | | | slightly moist | | | Silty CLAY. CL | | 7 | | |
| | S | | | moist | hard | reddish brown | Silty CLAY, trace Gravel. CL Last 2" Clayey Sandy Gravel. | | 19 | | |
| | S | | | | | | Sandy GRAVEL, some Silt, trace Clay. GM | | 20 | | |
| | S | | | | | | 0.2' Sandy CLAY. GM | | 22 | | |
| | S | | | very moist | dense | reddish brown | Sandy GRAVEL, some Silt. GM | | 17 | | |
| | S | | | wet | medium dense | brown | Gravelly CLAY. GC | | 20 | | |
| 25 | S | | | | | | Sandy GRAVEL, some Clay, some Silt. GM | | 11 | | |
| | S | | | | | | Gravelly SAND, some Silt. GC | | 12 | | |
| | S | | | wet | dense | brown | Increasing Gravel. GM | | 15 | | |
| | S | | | | | | Sandy GRAVEL, some Silt. GM | | 17 | | |
| | S | | | | | | | | 12 | | |
| | S | | | wet | medium dense | | Silty SAND, some Gravel, SC/GC trace Clay. GM | | 18 | | |
| | S | | | wet | | | Fine to coarse Sandy Clay to coarse GRAVEL. GM | | 12 | | |
| 30 | S | | | | | | | | 20 | | |
| | S | | | | | | | | 22 | | |
| | S | | | | | | | | 15 | | |
| | S | | | | | | | | 23 | | |
| | S | | | | | | | | 15 | | |
| | S | | | wet | | | Increasing Gravel. GM | | 16 | | |
| | S | | | | | | Sandy GRAVEL. GP | | 19 | | |
| | S | | | | | | | | 24 | | |
| | S | | | | | | | | 17 | | |
| | S | | | | | | | | 18 | | |
| | S | | | | | | | | 50/5" | | |
| | S | | | | | | | | 20 | | |
| | S | | | | | | | | 23 | | |
| | S | | | wet | | | Sandy GRAVEL. GP | | 17 | | |
| 35 | S | | | wet | | | Fine to medium GRAVEL, some Sand, some Clay. GP | | 22 | | |
| | S | | | | | | | | 22 | | |
| | S | | | wet | | brown | | | 20 | | |
| | S | | | | | | | | 14 | | |
| | S | | | | | | | | 17 | | |
| | S | | | | | | | | 16 | | |
| | S | | | | | rd brn | Silty fine SAND. SM | | 22 | | |
| | S | | | moist | | | Fine SAND and GRAVEL, some Silt. GP | | 50/5" | | |
| | S | | | | very dense | | | | 16 | | |
| 40 | S | | | moist | very dense | brown | Silty Sandy GRAVEL. GM | | 24 | | |



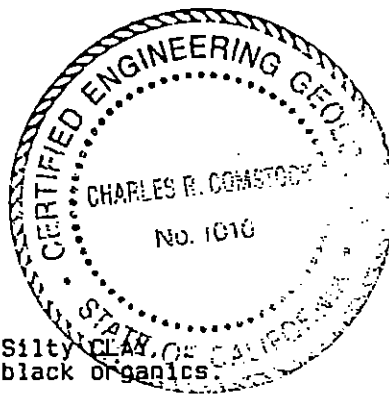
SHELL OIL COMPANY
500 40th Street
Oakland, California

Project No.
88-44-361-20

LOG OF BORING NO. EW-1

continued - page 3

| DEPTH (ft) | SAMPLE | WATER LEVEL | SYMBOL | MOISTURE | CONSISTENCY | COLOR | DESCRIPTION | WELL CONSTRUCTION | BLOWS/GIN. | D.V.M. (ppm) | T.P.H. (ppm) | | | | |
|------------|--------|-------------|--------|----------------|-------------|---------------|--|-------------------|------------|--------------|--------------------------------|----|----|--|--|
| 45 | S | | | moist | hard | brown | Sandy CLAY, some GRAVEL. CL | | 12 | | | | | | |
| | S | | | | | | | | | | | 13 | | | |
| 50 | S | | | moist | very dense | brown | Sandy CLAY, some GRAVEL. CL | | 27 | | | | | | |
| | S | | | | | | | | | | | 29 | | | |
| | S | | | | | | | | | | | 6 | | | |
| | S | | | | | | | | | | | 23 | | | |
| 55 | S | | | slightly moist | very stiff | tan | Gravelly SAND, some Clay. SC | | 33 | | | | | | |
| | S | | | | | | | | | | | 60 | | | |
| | S | | | | | | | | | | | | 6 | | |
| | S | | | | | | | | | | Silty CLAY, black organics. CL | | 14 | | |
| | S | | | | | | | | | | Silty CLAY. CL | | 12 | | |
| | S | | | | | | | | | | Silty CLAY. CL | | 16 | | |
| 60 | S | | | slightly moist | hard | reddish brown | Silty CLAY. CL | | 19 | | | | | | |
| | S | | | | | | | | | | | 10 | | | |
| | | | | | | | <p>Total Depth of Boring: 44 ft. Below Ground Surface.</p> <p>Casing: blank 4" ID schedule 40 PVC pipe.</p> <p>Screen: slotted 4" ID schedule 40 PVC pipe. (0.020" slot)</p> <p>Filter Pack: 12/20 Sand.</p> | | | | | | | | |



SHELL OIL COMPANY
500 40th Street
Oakland, California

Project No.

88-44-361-20



Converse Environmental West

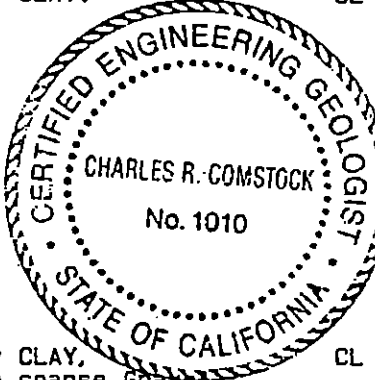
Drawing No.

A-7

LOG OF BORING NO. MW-8

DATE DRILLED: 6/27/90 EL: n/a WL TAKEN: n/a EQUIPMENT: 3.75"x 8" / 7.25"x 12" H.S.

| DEPTH (ft) | SAMPLE | WATER LEVEL | SYMBOL | MOISTURE | CONSISTENCY | COLOR | DESCRIPTION | SW | CL | WELL CONSTRUCTION | BLOWS/6IN. | O.V.H. (ppm) | T.P.H. (cns) |
|------------|--------|-------------|--------|----------------|-------------|---------------|----------------------------------|----|----|-------------------|------------|--------------|--------------|
| | | | ▲▲▲ | moist | loose | light brown | Gravelly SAND. (Fill) | SW | | | | | |
| | | | ▨▨▨ | moist | medium | black | Silty CLAY, trace Gravel. | | CL | | | | |
| 5 | 1 | | ▨▨▨ | slightly moist | very stiff | brownish gray | Silty CLAY. | | CL | | 7 10 | | |
| 10 | 2 | | ▨▨▨ | slightly moist | very stiff | light gray | Silty CLAY. | | CL | | 6 11 | | |
| 15 | 3 | | ▨▨▨ | moist | very stiff | grayish brown | Silty CLAY, trace coarse Gravel. | | CL | | 5 12 | | |
| 20 | 4 | | ▨▨▨ | very moist | very stiff | reddish brown | Silty CLAY. | | CL | | 12 11 | | |



SHELL OIL COMPANY
500 40th Street
Oakland, California

Project No.
88-44-361-20

LOG OF BORING NO. MW-8

continued - page 2

| DEPTH (ft) | SAMPLE | WATER LEVEL | SYMBOL | MOISTURE | CONSISTENCY | COLOR | DESCRIPTION | WELL CONSTRUCTION | BLONS/5IN. | O.V.M. (ppm) | T.P.H. (ppm) | | |
|------------|--------|-------------|--------|----------|-------------|-------------|---|---|--------------|--------------------------------|---|--|----|
| 25 | S | 11K | | wet | | | | | 10 | | | | |
| | | | | wet | very stiff | light brown | Silty CLAY, trace fine Sand. CL | | 10 | | | | |
| | | | | | | | | | | 20 | | | |
| | | | | | | | | | | 21 | | | |
| | | | | | | | | | | 10 | | | |
| | S | | | | | wet | m dense | | | SAND and CLAY, some Gravel. SC | 11 | | |
| | | | | | | | | | | Sandy GRAVEL, some CLAY. GC | 13 | | |
| | | | | | | | | | | | 14 | | |
| | | | | | | | | | | | 10 | | |
| | | | | | | | | | | | 15 | | |
| | | | | | | | | | | | 12 | | |
| | 30 | | | S | | | wet | | medium dense | tan | Sandy fine to coarse GRAVEL, some Clay, some Silt. GC | | 15 |
| | | | | | | | | 18 | | | | | |
| | | | | | | | | 18 | | | | | |
| | | | | | | | | 4 | | | | | |
| | | | | | | | | 8 | | | | | |
| | | | | | | | | 10 | | | | | |
| | | | | | | | | 12 | | | | | |
| | | | | | | | | 30 | | | | | |
| | | | | | | | | 27 | | | | | |
| | | | | | | | | 8 | | | | | |
| | | | | | | | | 17 | | | | | |
| 35 | | S | | | wet | dense | tan | Sandy GRAVEL, some Silt, trace Clay. GM | | 25 | | | |
| | | | | | | | | 27 | | | | | |
| | | | | | | | | 5 | | | | | |
| | | | | | | | | 4 | | | | | |
| | | | | | | | | 3 | | | | | |
| | | | | | | | | 18 | | | | | |
| | | | | | | | | 10 | | | | | |
| | | | | | | | | 16 | | | | | |
| | | | | | | | | 15 | | | | | |
| | | | | | | | | 25 | | | | | |
| | | | | | | | | 13 | | | | | |
| | 40 | S | | | moist | | tan | Fine SAND and Silt, some Clay. SM | | | 14 | | |
| | | | | | | | | 8 | | | | | |
| | | | | | | | | 8 | | | | | |
| | | | | | | | | 7 | | | | | |
| | | | | | | | | 14 | | | | | |
| | | | | | | | | 35 | | | | | |
| | | | | moist | stiff | tan | Silty CLAY, tr fine Sand. CL | | 32 | | | | |
| | | | | | | | | | 35 | | | | |
| | | | | moist | hard | brn gry | Silty CLAY, trace Gravel, trace fine Sand. CL | | | | | | |

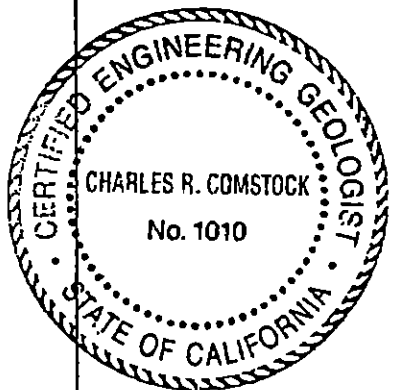
SHELL OIL COMPANY
500 40th Street
Oakland, California

Project No.
88-44-361-2C

LOG OF BORING NO. MW-8

continued - page 3

| DEPTH (ft) | SAMPLE | WATER LEVEL | SYMBOL | MOISTURE | CONSISTENCY | COLOR | DESCRIPTION | WELL CONSTRUCTION | BLOWS/BLN. | D.V.M. (ppm) | T.P.H. (ppm) |
|------------|--------|----------------|------------------|----------------|-------------|-----------------------------------|---|------------------------|------------|--------------|--------------|
| | S | | [Hatched Symbol] | slightly moist | | | Silty CLAY. CL | [Cross-hatched Symbol] | 12 | | |
| | | slightly moist | | hard | tan | Silty CLAY, trace fine Gravel. CL | 14 | | | | |
| | S | | | slightly moist | very stiff | tan | Silty CLAY, some Sand. CL | | 18 | | |
| | | | | | | | | | 21 | | |
| | | | | | | | | | 8 | | |
| | | | | | | | | | 10 | | |
| | | | | | | | | | 15 | | |
| | | | | | | | | | 17 | | |
| 45 | | | | | | | Total Depth of Boring: 44 ft Below Ground Surface. Casing: blank 4" ID blank schedule 40 PVC Pipe. Screen: slotted 4" ID schedule 40 PVC Pipe. (0.020" slot) Filter Pack: 2/12 Sand. | | | | |
| 50 | | | | | | | | | | | |
| 55 | | | | | | | | | | | |
| 60 | | | | | | | | | | | |

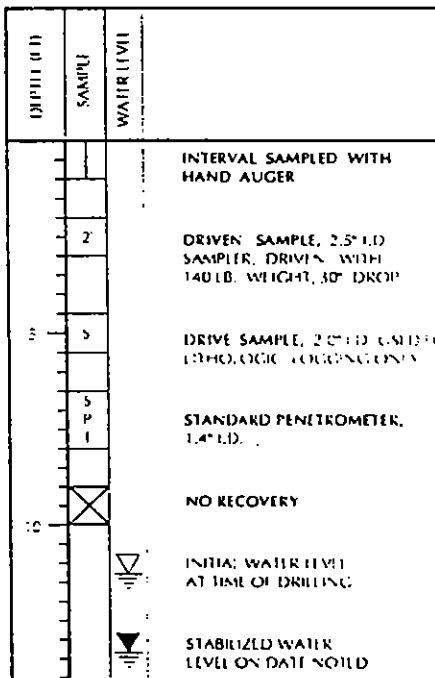


SHELL OIL COMPANY
 500 40th Street
 Oakland, California

Project No.
 88-44-361-20

| MAJOR DIVISIONS | | | SYMBOLS | TYPICAL NAMES |
|---|--|---------------------------------------|---|---|
| COARSE GRAINED SOILS MORE THAN HALF IS LARGER THAN NO. 200 SIEVE | GRAVELS MORE THAN HALF COARSE FRACTION IS LARGER THAN NO. 4 SIEVE | CLEAN GRAVELS WITH LITTLE OR NO FINES | GW | WELL GRADED GRAVELS, GRAVEL-SAND MIXTURES |
| | | | GP | POORLY GRADED GRAVELS, GRAVEL-SAND MIXTURES |
| | | GRAVELS WITH OVER 12% FINES | GM | SILTY GRAVELS, POORLY GRADED GRAVEL-SAND-SILT MIXTURES |
| | | | GC | CLAYEY GRAVELS, POORLY GRADED GRAVEL-SAND-CLAY MIXTURES |
| | SANDS MORE THAN HALF COARSE FRACTION IS SMALLER THAN NO. 4 SIEVE | CLEAN SANDS WITH LITTLE OR NO FINES | SW | WELL GRADED SANDS, GRAVELLY SANDS |
| | | | SP | POORLY GRADED SANDS, GRAVELLY SANDS |
| | | SANDS WITH OVER 12% FINES | SM | SILTY SANDS, POORLY GRADED SAND-SILT MIXTURES |
| | | | SC | CLAYEY SANDS, POORLY GRADED SAND-CLAY MIXTURES |
| FINE GRAINED SOILS MORE THAN HALF IS SMALLER THAN NO. 200 SIEVE | SILTS AND CLAYS LIQUID LIMIT LESS THAN 50 | ML | INORGANIC SILTS AND VERY FINE SANDS, ROCK FLOUR, SILTY OR CLAYEY FINE SANDS, OR CLAYEY SILTS WITH SLIGHT PLASTICITY | |
| | | CL | INORGANIC CLAYS OF LOW TO MEDIUM PLASTICITY, GRAVELLY CLAYS, SANDY CLAYS, SILTY CLAYS, LEAN CLAY | |
| | | OL | ORGANIC CLAYS AND ORGANIC SILTY CLAYS OF LOW PLASTICITY | |
| | SILTS AND CLAYS LIQUID LIMIT GREATER THAN 50 | MH | INORGANIC SILTS, AMYCTACEOUS OR DIATOMACEOUS FINE, SANDY OR SILTY SILTS, ELASTIC SILTS | |
| | | CH | INORGANIC CLAYS OF HIGH PLASTICITY, FAT CLAYS | |
| | | OH | ORGANIC CLAYS OF MEDIUM TO HIGH PLASTICITY, ORGANIC SILTS | |
| HIGHLY ORGANIC SOILS | | PT | PEAT AND OTHER HIGHLY ORGANIC SOILS | |

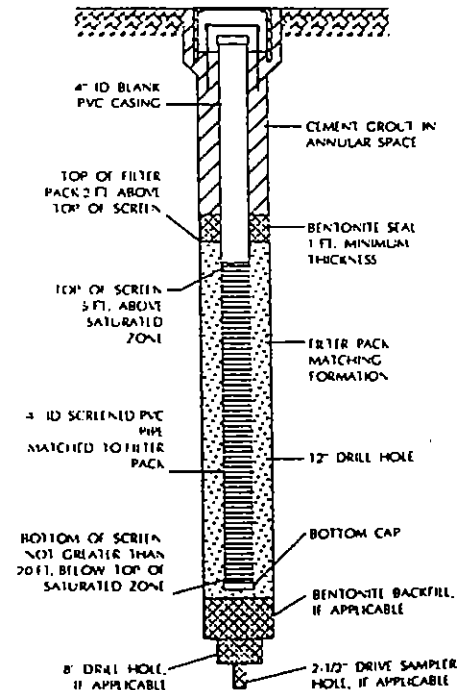
SAMPLE TYPE



NOTE:

SOIL CONDITIONS INDICATED BY BORING LOGS APPLY ONLY AT THE LOCATION OF THE PARTICULAR BORING AND AT THE TIME OF DRILLING. SUBSURFACE CONDITIONS MAY DIFFER AT OTHER LOCATIONS AND MAY CHANGE AT THE BORING LOCATION WITH THE PASSAGE OF TIME. DATA PRESENTED IN THE LOGS REPRESENTS SIMPLIFICATION OF THE ACTUAL CONDITIONS ENCOUNTERED. SEE CONDITIONS INDICATED BETWEEN SAMPLES FOR DETAILS.

WELL CONSTRUCTION



UNIFIED SOIL CLASSIFICATION, BORING LOG, AND WELL CONSTRUCTION SYMBOLS

SHELL OIL COMPANY
500 40th Street
Oakland, California

Project No.

88-44-361-20

LOG OF BORING NO. OMW-11

| | | |
|--|---|---|
| Start: 11/21/91 Completion: 11/21/91 Water Measure: 11/22/91 | Geologist: C. Brown Assistant Geol.: N/A Drilling Co.: A.T.D. | Driller/Helper: N/A Drilling Method: Hollow Stem Auger Auger/Bit Dia.: 3.75" x 8" - 7.25" x 13" |
|--|---|---|

| DEPTH (FT) | SAMPLE | WATER LEVEL | SYMBOL | WELL CONSTRUCT. | DESCRIPTION | MOISTURE | SOIL CONSISTENCY OR ROCK HARDNESS | COLOR | BLOWS / 6" | PERCENT RECOVERY |
|------------|--------|-------------|--------|-----------------|---|---------------------|-----------------------------------|----------------|------------|------------------|
| | | | | | 8" Concrete, 7" Base | | | gray brown | | |
| | | | | | Silty Clay CL | moist | dense | black | | |
| | S | | | | | | | | 4 | |
| 5 | 1 | | | | | moist | stiff | brown | 9 | |
| | | | | | | | | | | |
| | S | | | | | | | | | |
| 10 | 2 | | | | Clayey Sand, little fine Gravel SC | moist | medium dense | gray with rust | 5 | |
| | S | | | | | | | | 13 | |
| | S | | | | | | | | 10 | |
| | S | | | | | | | | 16 | |
| | S | | | | | | | | 18 | |
| | S | | | | | moist to very moist | | | 9 | |
| | S | | | | | | | | 11 | |
| | S | | | | | | | | 14 | |
| | S | | | | | | | | 18 | |
| | S | | | | Slightly Clayey, coarse Sand, trace to little fine Gravel SP/SC | wet | loose | | 5 | |
| 15 | 3 | | | | | | | | 5 | |
| | S | | | | Fine Sandy Clay CL | very moist | stiff | gray with rust | 4 | |
| | S | | | | | | | | 5 | |
| | S | | | | | | | | 5 | |
| | S | | | | | | | | 7 | |
| | S | | | | Clayey fine Sand SC | | medium dense | | 4 | |
| | S | | | | | | | | 5 | |
| | S | | | | | | | | 6 | |
| | S | | | | Silty fine Sand SP/SM | | | brown | 6 | |
| | S | | | | | | | | 6 | |
| 20 | 2 | | | | Coarse Sand and fine Gravel, trace Clay GP/GC | wet | | | 9 | |
| | S | | | | | | | | 20 | |



SHELL OIL COMPANY
 500 40th Street
 Oakland, California

Project No.
 88-44-361-20

LOG OF BORING NO. OMW-11

Continued - Page 2

| DEPTH (FT) | SAMPLE | WATER LEVEL | SYMBOL | WELL CONSTRUCT. | DESCRIPTION | MOISTURE | SOIL CONSISTENCY OR ROCK HARDNESS | COLOR | BLOWS / 6" | PERCENT RECOVERY |
|-------------------------|--------|-------------|--------|-----------------|---|----------|-----------------------------------|-------|----------------|------------------|
| 5 25 | S | | | | Clayey coarse Sand and fine Gravel SC/GC | wet | dense | brown | 11 | |
| | S | | | | Fine Gravelly coarse Sand, trace Clay SP | | | | 19 | |
| | S | | | | Very Sandy Clay/Clayey Sand CL/SC | | | | 21 | |
| | P | | | | Fine Gravelly fine to medium Sand SP | | | | 16 | |
| | T | | | | | | | | rust with gray | |
| 3 | | | | | | gray | 5 | 10 | | |
| | | | | | Total Depth of Boring: 24 ft. Casing: Blank 4" ID Sch. 40 PVC Screen: Slotted 4" ID Sch. 40 PVC, 0.020" slots Filter Pack: 2/12 sand | | | | | |
| 30 | | | | | | | | | | |
| 35 | | | | | | | | | | |
| 40 | | | | | | | | | | |

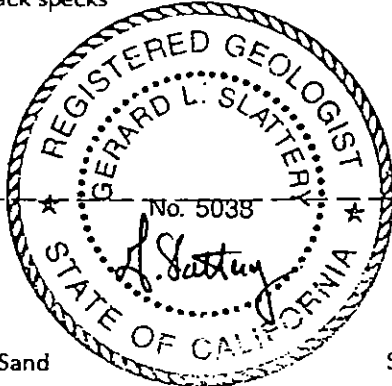
SHELL OIL COMPANY
500 40th Street
Oakland, California

Project No.
88-44-361-20

LOG OF BORING NO. OMW-12

| | | |
|---|---|---|
| Start: 11/20/91 Completion: 11/20/91 Water Measure: 12/2/91 | Geologist: C. Brown Assistant Geol.: N/A Drilling Co.: A.T.D. | Driller/Helper: N/A Drilling Method: Hollow Stem Auger Auger/Bit Dia.: 3.75" x 8" - 7.25" x 13" |
|---|---|---|

| DEPTH (FT) | SAMPLE | WATER LEVEL | SYMBOL | WELL CONSTRUCT. | DESCRIPTION | MOISTURE | SOIL CONSISTENCY OR ROCK HARDNESS | COLOR | BLOWS / 6" | PERCENT RECOVERY |
|------------|--------|-------------|--------|-----------------|---------------------------------|----------|-----------------------------------|--------------|----------------|------------------|
| | | | | | ≈8" Concrete, 8" Base, 6" Fill | | | | | |
| | | | | | 6" layer Gravel | | | | | |
| | | | | | Silty Clay | CL | moist | stiff | black | |
| | | | | | trace black specks | | | | brown | 10 |
| | S | | | | | | | | | 10 |
| 5 | 1 | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | S | | | | Clayey Sand | SC | moist | medium dense | gray with rust | 6 |
| | 2 | | | | | | | | | 18 |
| 10 | | | | | | | | | | 16 |
| | S | | | | Fine Sandy Silt | ML | | | | 11 |
| | | | | | | | | | | 11 |
| | S | | | | Clayey Sand, little fine Gravel | SC | very moist to wet | | red brown | 16 |
| | | | | | wet Sand lens | | | | | 9 |
| | SPT | | | | wet Sand lens | | | | | 12 |
| | 1 | | | | wet Sand lens | | | | | 12 |
| | | | | | | | | | | 18 |
| | S | | | | Coarse Sand, pea Gravel | SC/GC | wet | | | 8 |
| | | | | | | | | | | |
| 15 | 3 | | | | Fine Sandy Clay | CL | very moist | stiff | gray | 10 |
| | S | | | | | | | | | 5 |
| | | | | | | | | | | 8 |
| | S | | | | wet lens | | wet | | rust with gray | 11 |
| | | | | | | | very moist | | | 12 |
| | SPT | | | | | | | | | 4 |
| | 2 | | | | Silty Clay | CL | | | | 5 |
| | | | | | | | wet | | | 12 |
| | | | | | | | | | | 15 |
| | S | | | | Clayey Sand and fine Gravel | SC/GC | very moist | stiff | | 4 |
| 20 | | | | | Silty Clay | CL | moist | | | 7 |



SHELL OIL COMPANY
 500 40th Street
 Oakland, California

Project No.

88-44-361-20




Converse Environmental West

Drawing No.

A-4

LOG OF BORING NO. OMW-12

Continued - Page 2

| DEPTH (FT) | SAMPLE | WATER LEVEL | SYMBOL | WELL CONSTRUCT. | DESCRIPTION | MOISTURE | SOIL CONSISTENCY OR ROCK HARDNESS | COLOR | BLOWS / 6" | PERCENT RECOVERY |
|------------|--------|-------------|--------|-----------------|---|----------|-----------------------------------|----------------|------------|------------------|
| | S | | | | Silty Clay | CL | moist | rust with gray | 5 | |
| | S | | | | | | | | 8 | |
| | S | | | | | | | | 6 | |
| | S | | | | | | | | 7 | |
| | S | | | | | | | | 4 | |
| | P | | | | | | | | 5 | |
| | T | | | | | | | | 6 | |
| | 3 | | | | Becoming Sandy | | | | 8 | |
| 25 | | | | | Total Depth of Boring: 24 ft. Casing: Blank 4" ID Sch. 40 PVC Screen: Slotted 4" ID Sch. 40 PVC, 0.020" slots Filter Pack: 2/12 sand | | | | | |
| 30 | | | | |  | | | | | |
| 35 | | | | | | | | | | |
| 40 | | | | | | | | | | |

SHELL OIL COMPANY
500 40th Street
Oakland, California

Project No.

88-44-361-20



Converse Environmental West

Drawing No.

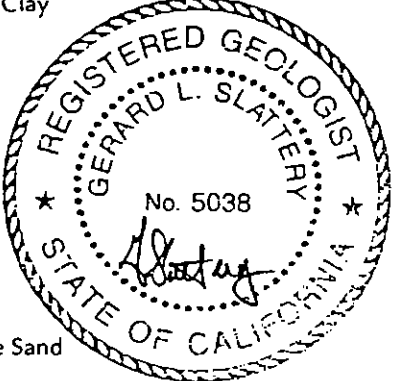
A-5

LOG OF BORING NO. OMW-13

Start: 11/21/91
 Completion: 11/21/91
 Water Measure: 11/22/91

Geologist: C. Brown
 Assistant Geol.: N/A
 Drilling Co.: A.T.D.

Driller/Helper: N/A
 Drilling Method: Hollow Stem Auger
 Auger/Bit Dia.: 3.75" x 8" - 7.25" x 13"

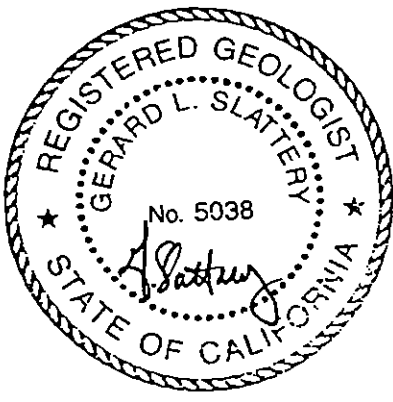
| DEPTH (FT) | SAMPLE | WATER LEVEL | SYMBOL | WELL CONSTRUCT. | DESCRIPTION | MOISTURE | SOIL CONSISTENCY OR ROCK HARDNESS | COLOR | BLOWS / 6" | PERCENT RECOVERY |
|------------|--------|-------------|--------|-----------------|---|----------|-----------------------------------|----------------------|------------|------------------|
| | | | | | 8" Concrete, 8" Base | | | | | |
| | | | | | Silty Clay | moist | stiff | dark gray black | | |
| | S | | | |  | | | mottled gray brown | 4 | |
| 5 | 1 | | | | | | | | 8 | |
| | S | | | | | | | | 5 | |
| | S | | | | | | | | 9 | |
| | S | | | | trace Sand | | | gray | 12 | |
| | | | | | Grading into fine Sandy Clay | | | | 14 | |
| | S | | | | Fine Sandy Clay/Clayey Sand | | | | 5 | |
| 10 | 2 | | | | | | | | 7 | |
| | S | | | | Silty Clay | | stiff | light gray with rust | 6 | |
| | S | | | | Clayey Sand and Gravel | | dense | | 24 | |
| | | | | | | | | | 25 | |
| | S | | | | | | | | 9 | |
| | S | | | | | | | | 15 | |
| | S | | | | | | | | 16 | |
| | S | | | | | wet | | | 20 | |
| 15 | 3 | | | | | | medium dense | | 8 | |
| | S | | | | | | | | 9 | |
| | S | | | | Sandy Silt | | stiff | rust | 10 | |
| | | | | | Clayey Sand and Gravel | | | brown | 7 | |
| | S | | | | | | | | 12 | |
| | | | | | | | | | 16 | |
| | S | | | | | | | | 12 | |
| | S | | | | | | | | 19 | |
| | S | | | | | | | | 23 | |
| | S | | | | | | | | 34 | |
| 20 | | | | | | wet | medium dense | | 10 | |
| | | | | | | | | | 15 | |

SHELL OIL COMPANY
 500 40th Street
 Oakland, California

Project No.
 88-44-361-20

LOG OF BORING NO. OMW-13

Continued - Page 2

| DEPTH (FT) | SAMPLE | WATER LEVEL | SYMBOL | WELL CONSTRUCT. | DESCRIPTION | MOISTURE | SOIL CONSISTENCY OR ROCK HARDNESS | COLOR | BLOWS / 6" | PERCENT RECOVERY | | |
|------------|--------|-------------|--------|-----------------|---|----------|-----------------------------------|----------------|------------|------------------|--|--|
| | S | | | | Silty Clay | CL | very moist | stiff | gray brown | 5 | | |
| | S | | | | | | moist | | | 8 | | |
| | S | | | | | | | | | 6 | | |
| | S | | | | | | | | | 7 | | |
| | SPT | | | | Sandy Clay with occasional Clayey Sand lens | | very moist | gray with rust | | 4 | | |
| | 3 | | | | | | | | | 5 | | |
| | | | | | | | | | | 6 | | |
| | | | | | | | | | | 8 | | |
| 25 | | | | | Total Depth of Boring: 24 ft. Casing: Blank 4" ID Sch. 40 PVC Screen: Slotted 4" ID Sch. 40 PVC, 0.020" slots Filter Pack: 2/12 sand | | | | | | | |
| 30 | | | | |  | | | | | | | |
| 35 | | | | | | | | | | | | |
| 40 | | | | | | | | | | | | |

SHELL OIL COMPANY
500 40th Street
Oakland, California

Project No.

88-44-361-20



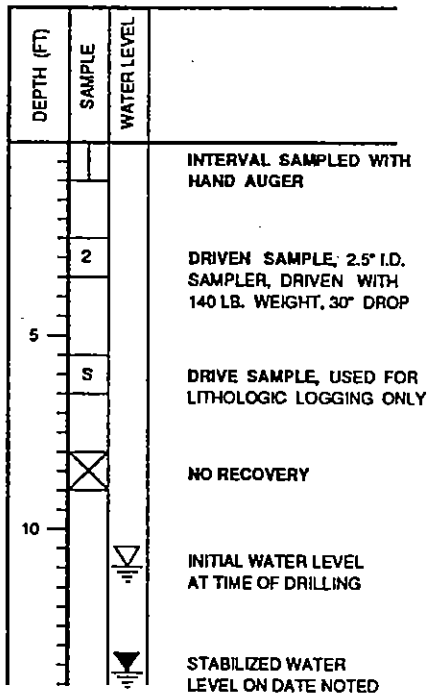
Converse Environmental West

Drawing No.

A-7

| MAJOR DIVISIONS | | | SYMBOLS | TYPICAL NAMES |
|--|---|---|-------------------------------------|---|
| COARSE GRAINED SOILS MORE THAN HALF IS LARGER THAN NO. 200 SIEVE | GRAVELS MORE THAN HALF COARSE FRACTION IS LARGER THAN NO. 4 SIEVE | CLEAN GRAVELS WITH LITTLE OR NO FINES | GW | WELL GRADED GRAVELS, GRAVEL-SAND MIXTURES |
| | | | GP | POORLY GRADED GRAVELS, GRAVEL-SAND MIXTURES |
| | | GRAVELS WITH OVER 12% FINES | GM | SILTY GRAVELS, POORLY GRADED GRAVEL-SAND-SILT MIXTURES |
| | | | GC | CLAYEY GRAVELS, POORLY GRADED GRAVEL-SAND-CLAY MIXTURES |
| | SANDS MORE THAN HALF COARSE FRACTION IS SMALLER THAN NO. 4 SIEVE | CLEAN SANDS WITH LITTLE OR NO FINES | SW | WELL GRADED SANDS, GRAVELLY SANDS |
| | | | SP | POORLY GRADED SANDS, GRAVELLY SANDS |
| | | SANDS WITH OVER 12% FINES | SM | SILTY SANDS, POORLY GRADED SAND-SILT MIXTURES |
| | | | SC | CLAYEY SANDS, POORLY GRADED SAND-CLAY MIXTURES |
| FINE GRAINED SOILS MORE THAN HALF IS SMALLER THAN NO. 200 SIEVE | SILTS AND CLAYS LIQUID LIMIT LESS THAN 50 | | ML | INORGANIC SILTS AND VERY FINE SANDS, ROCK FLOUR, SILTY OR CLAYEY FINE SANDS, OR CLAYEY SILTS WITH SLIGHT PLASTICITY |
| | | | CL | INORGANIC CLAYS OF LOW TO MEDIUM PLASTICITY, GRAVELLY CLAYS, SANDY CLAYS, SILTY CLAYS, LEAN CLAY |
| | | | OL | ORGANIC CLAYS AND ORGANIC SILTY CLAYS OF LOW PLASTICITY |
| | SILTS AND CLAYS LIQUID LIMIT GREATER THAN 50 | | MH | INORGANIC SILTS, MICACEOUS OR DIATOMACEOUS FINE, SANDY OR SILTY SOILS, ELASTIC SILTS |
| | | | CH | INORGANIC CLAYS OF HIGH PLASTICITY, FAT CLAYS |
| | | | OH | ORGANIC CLAYS OF MEDIUM TO HIGH PLASTICITY, ORGANIC SILTS |
| HIGHLY ORGANIC SOILS | | Pt | PEAT AND OTHER HIGHLY ORGANIC SOILS | |

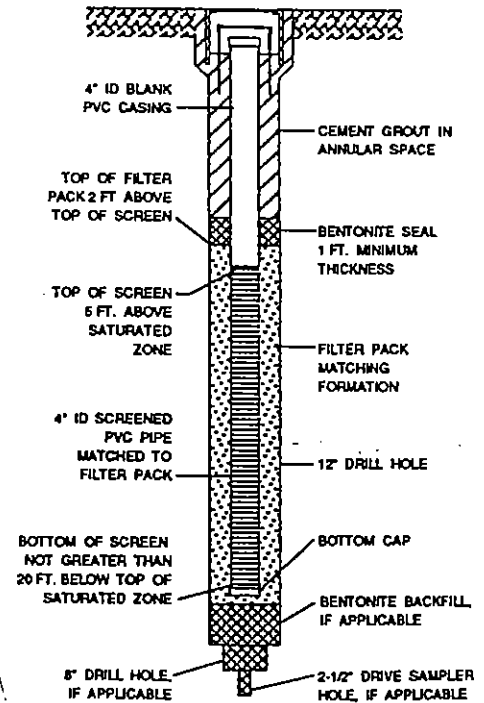
SAMPLE TYPE



NOTE:

SOIL CONDITIONS INDICATED BY BORING LOGS APPLY ONLY AT THE LOCATION OF THE PARTICULAR BORING AND AT THE TIME OF DRILLING. SUBSURFACE CONDITIONS MAY DIFFER AT OTHER LOCATIONS AND MAY CHANGE AT THE BORING LOCATION WITH THE PASSAGE OF TIME. DATA PRESENTED IN THE LOGS REPRESENT A SIMPLIFICATION OF THE ACTUAL CONDITIONS ENCOUNTERED.

WELL CONSTRUCTION



UNIFIED SOIL CLASSIFICATION, BORING LOG, AND WELL CONSTRUCTION SYMBOLS

SHELL OIL COMPANY
500 40th Street
Oakland, California

Project No.

88-44-361-20



Converse Environmental West

Drawing No.

A-1