

REPORT OF INVESTIGATION  
CHEVRON SS 9-7127  
GRANT LINE ROAD AND INTERSTATE 580  
TRACY, CALIFORNIA

Prepared for

Chevron U.S.A., Inc.  
San Ramon, California

Prepared by

EA Engineering, Science, and Technology, Inc.  
Lafayette, California

Barbara J. Marks 13 Nov 87  
Barbara J. Marks, P.E.S. Date  
Enviromental Scientist

Robert E. Hinchee 11/13/87  
Robert E. Hinchee, Ph.D., P.E. Date  
Civil Engineer #C 039606

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## 1. INTRODUCTION

### 1.1 SCOPE

At the request of Chevron U.S.A. Inc., EA Engineering, Science, and Technology, Inc. conducted a Soil Vapor Contaminant Assessment (SVCA) at Chevron Service Station 9-7127 in Tracy, California. This report describes the SVCA process, presents the results for the site survey, and makes recommendation for further actions based on these results.

### 1.2 SITE SETTING

Chevron Service Station 9-7127 is located near the Grant Line Road exit from Interstate 580 in Alameda County, California (Figure 1). It is located in an isolated area and is surrounded by pastures (Figure 2). There are no houses or businesses in close proximity to the site, the nearest structures being associated with a wind farm approximately 0.25 mile from the site. The site is on the top of a leveled hill, with steep sides on the east and southeast boundaries of the site. The Engineering Department of the City of Tracy did not know of any wells in the general vicinity of the site (Vincent 1987, personal communication).

### 1.3 PRINCIPLES OF SOIL VAPOR CONTAMINANT ASSESSMENT

The soil vapor survey, or SVCA, technique takes advantage of the behavior of hydrocarbon mixtures and the physicochemical properties of the individual components in the subsurface. Following a subsurface gasoline release, free product will migrate downwards towards the ground water, some of the gasoline will volatilize, and some will adsorb to the soils. In the case of a spill of sufficient volume to exceed the soil binding capacity, free

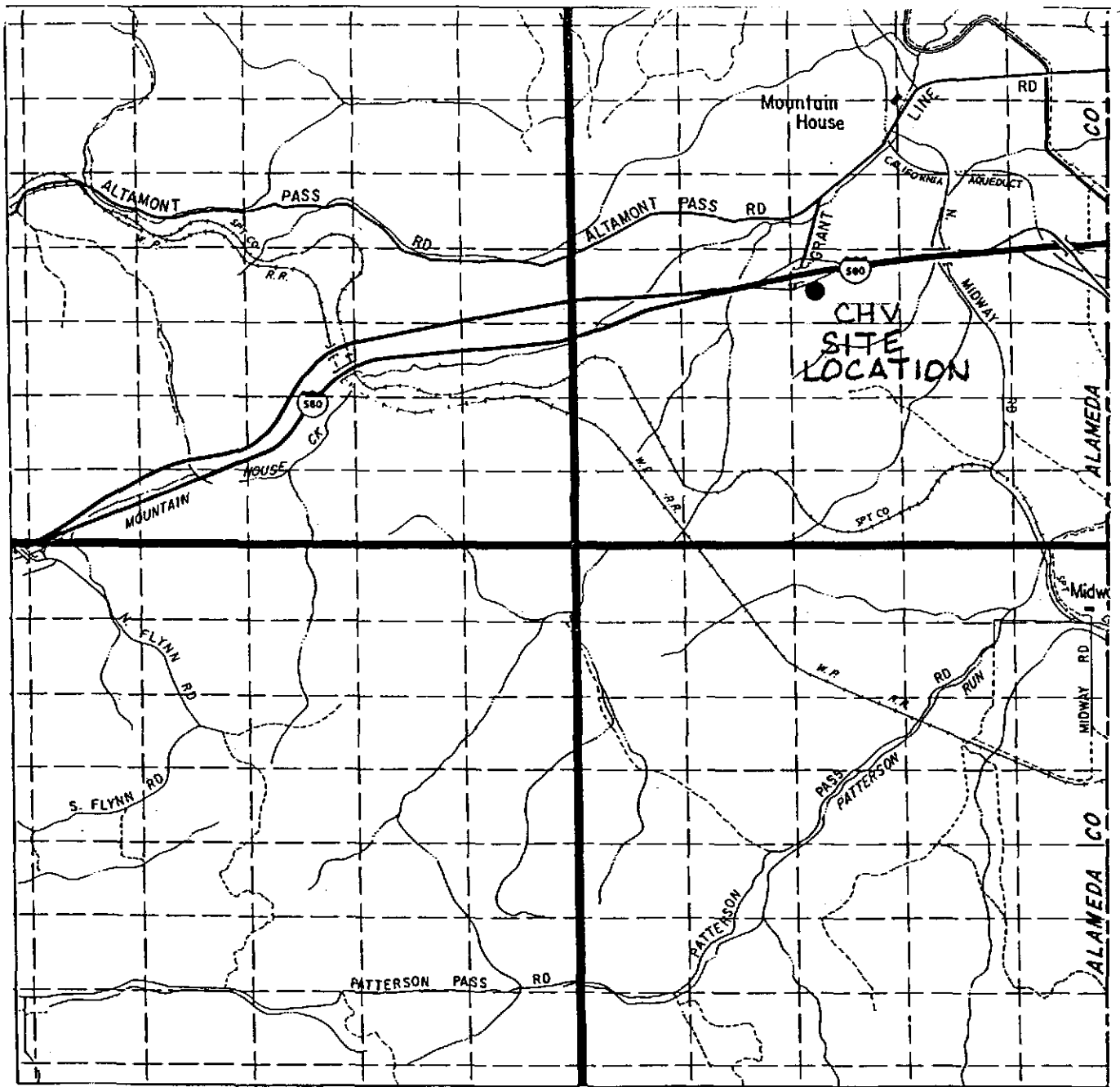


Figure 1: Location of Chevron Service Station 9-7127, Tracy, California.

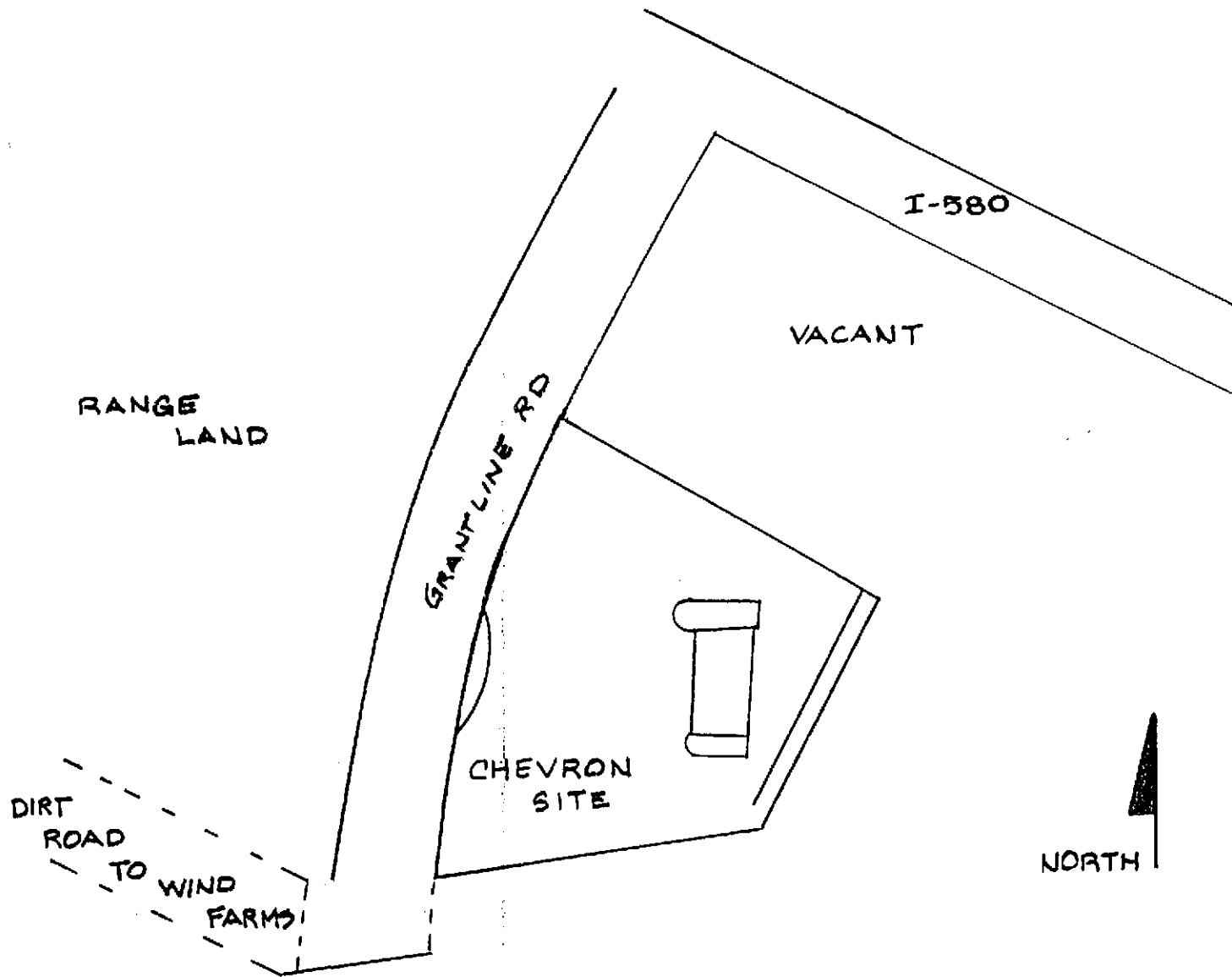


Figure 2: Land-Use in the vicinity of Chevron Service Station 9-7127, Tracy, California.

liquid will reach ground water, at which point it will float and may begin to vaporize and solubilize.

Like most hydrocarbon liquids, gasoline is a complex mixture of many compounds, each with its own physicochemical properties. The contaminants found in ground water located beneath a layer of floating hydrocarbon are generally less hydrophobic and are generally found in concentrations proportional to the hydrocarbon/water partition coefficient (i.e., the relative solubility of a given compound in the bulk hydrocarbon to its solubility in water) and to their percent composition in the gasoline. It may be noted that concentration of total benzene, toluene, and xylenes in product-saturated water may exceed 10-20 mg/L (API 1985).

Hydrocarbons will also volatilize into the air- or gas-filled soil interstices. Volatilization is largely a function of vapor pressure. The natures of the contaminant mixtures, in terms of specific component mixtures, in either the aqueous or vapor phase, are distinctly different from each other and from the gasoline. That is, the more hydrophilic hydrocarbons will be more likely to move into ground water, while the more volatile compounds are more likely to move into the vapor phase, and the compounds that are both less volatile and more hydrophobic are more likely to remain in the free product or be adsorbed to soils (Hinchee and Reisinger 1987).

Hydrocarbons not remaining in the free product will partition into either ground water or soil vapor and migrate as the result of a variety of interacting forces. In ground water, contaminants will migrate with the ground-water flow, interacting with the rock or soil geological medium. As the contaminants pass through a medium, organic constituents in the medium interact with the contaminants, and some are adsorbed or bound to particle surfaces (Bruell and Hoag 1986). The result is a net retardation in the velocity of movement of those compounds relative to that

of the ground water in which they are dissolved. The process is analogous to laboratory chromatography. The compound with the least affinity for the porous medium is least retarded and therefore moves most rapidly. This compound, then, is present at the leading edge of a contaminant plume.

The affinity of a compound for the soil porous medium is partly a function of the compound's hydrophobicity--that is, the more hydrophobic a compound the more likely it is to adsorb to the solid medium. Aqueous solubility is a good indicator of hydrophobicity: the more soluble a compound is, the less hydrophobic and more hydrophilic it is, and vice versa. Vapor pressure is a good indicator of volatility; compounds with higher vapor pressures are more volatile.

In determining the environmental fate of various hydrocarbon compounds in a hydrocarbon mixture such as gasoline, those which have a high vapor pressure are more likely to move into the vapor phase, or evaporate. Compounds with high solubility are more likely to move into ground water from the free product and, once in ground water, tend to move more rapidly. Compounds of low vapor pressure and low solubility tend to remain in the free product or be adsorbed to the solid matrix and remain relatively immobile.

Dissolved compounds will tend to volatilize from the aqueous phase. The Henry's Law constant is the equilibrium ratio of a compound's concentration in the vapor phase to its concentration in the aqueous phase. The higher a compound's Henry's Law constant, the greater its tendency to volatilize from water into air.

Figure 3 graphically illustrates the vapor pressure, aqueous solubility, and Henry's Law constants, and their relationships, for selected hydrocarbons typically found in gasoline. The

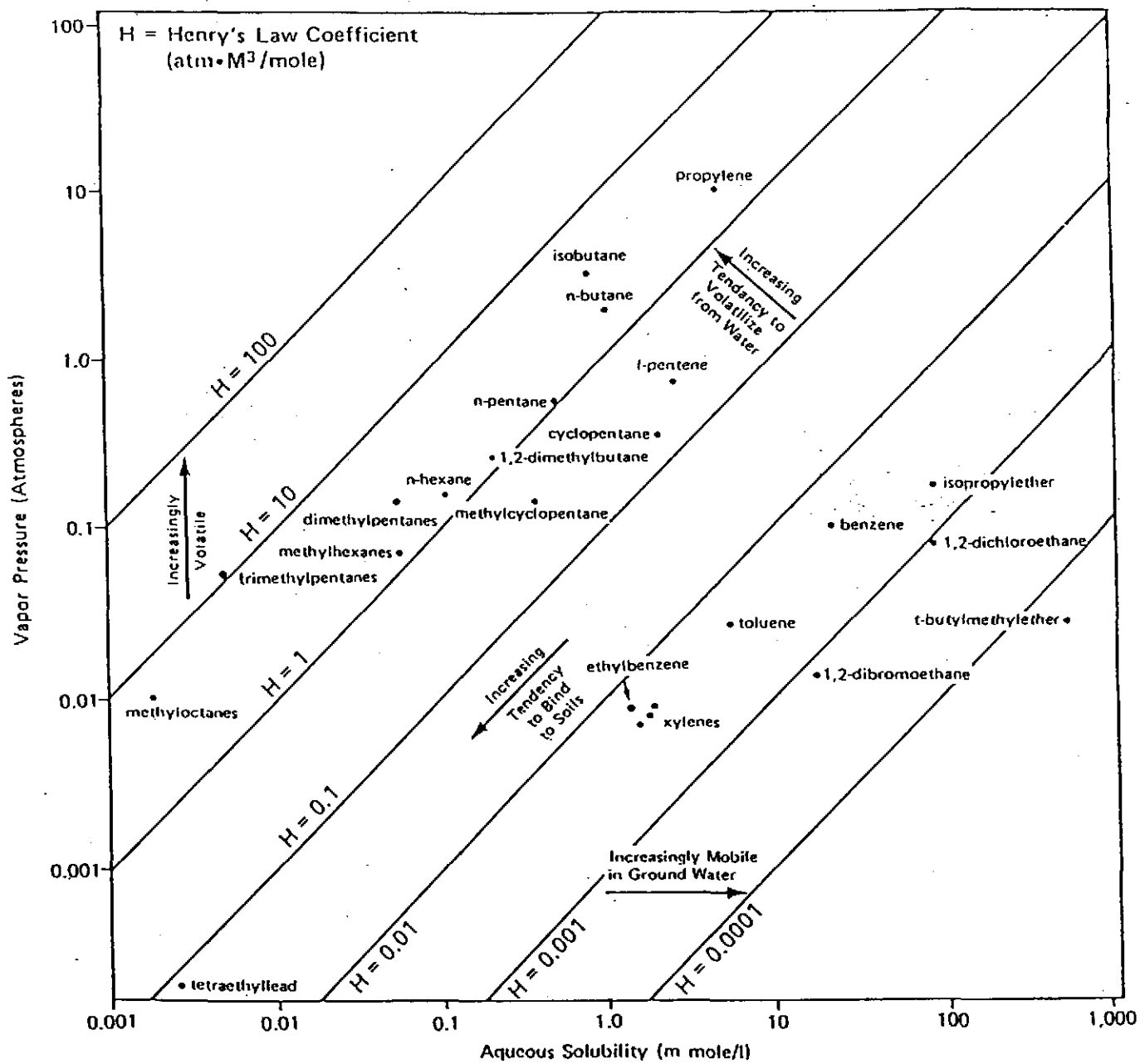


Figure 3. Vapor pressures, solubilities, and corresponding Henry's Law constants for major constituents of gasoline.



Henry's Law constant is approximated here as the ratio of vapor pressure to solubility.

The Henry's Law constant is directly related to the tendency of compounds to volatilize, as opposed to solubilizing. Compounds with Henry's Law constants greater than 0.001 (atm·m<sup>3</sup>/mole) volatilize from water into air very rapidly (Lyman et al. 1982); those with Henry's Law constants greater than 0.01 (atm·m<sup>3</sup>/mole) are generally volatilized so rapidly that they are seldom found in gasoline-contaminated ground water. It may be observed (Figure 3) that tetraethyl lead (TEL) has an extremely low solubility and a relatively low vapor pressure. As a result, this constituent would not be expected to solubilize and migrate in ground water, and although its low vapor pressure would indicate slow volatilization, its Henry's Law constant indicates that it may be more rapidly volatilized than solubilized. The fate of TEL would be expected to be long-term binding to the soil.

On the basis of these properties it can be seen that associated with any ground water, soil, or free-product contamination is vapor phase contamination. The SVCA technique takes advantage of this, and through the collection and analysis of soil vapor permits a rapid, cost-effective delineation of the extent of contamination.

## 2. FIELD INVESTIGATIONS

### 2.1 HYDROGEOLOGY

The specific soils and hydrology of the Tracy site have not been investigated. The site is in the San Joaquin Valley, where Cretaceous marine sediments dominate. The rock types are typically shales and cherts overlain by alluvial sands and gravels (DMG 1966).

### 2.2 SOIL VAPOR CONTAMINANT ASSESSMENT

On 27 October 1987, EA conducted an SVCA at the Tracy site. Soil gas samples were taken from 13 on-site locations and 2 off-site locations (Figure 4), at depths of 3 to 12 feet. At SVCA points V1 (near the tank field), V5 (at the northern end of the eastern pump island), and V8 (near the waste oil tank) vertical profiles of soil gas composition were taken. There is a well along the southeastern site boundary. Its purpose is unknown. A well headspace sample was not taken for analysis because the well could not be opened.

Before each sample was collected, a vacuum pump was used to purge previously collected vapor from the probe to ensure that soil vapor samples collected were not contaminated. The vacuum pressure reading on the purging apparatus was recorded. This vacuum pressure is related to the soil's gas permeability and is useful in data interpretation. The samples were collected through a septum with a microsyringe and injected into a Photovac 10S50 chromatograph for analysis.

The Photovac 10S50 is a portable, programmable, integrating gas chromatograph with a photoionization detector (PID). The PID is a nondestructive flow-through detector that uses high energy ultraviolet radiation as its ionization source. The high energy

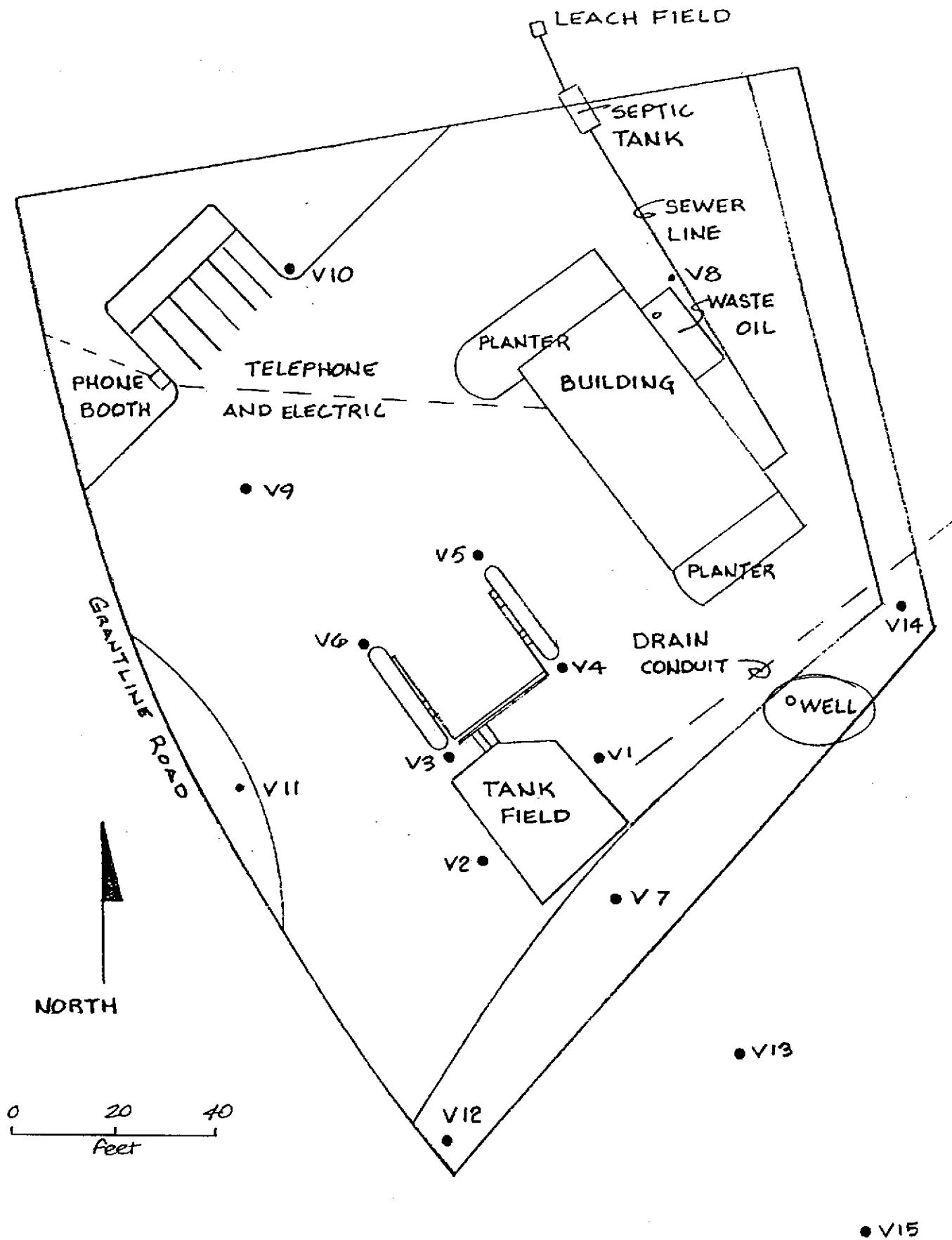


Figure 4. Site plan, with vapor sampling points, Chevron Service Station 9-7127, Tracy, California.

radiation ionizes compounds, generating an energy increase in the detector which appears as an electrical signal measured in volts; this is integrated across time by the instrument to give a value for the peak in volt-seconds (V-sec). The instrument is calibrated with standards consisting of known concentrations of hydrocarbon constituents (e.g., benzene) in air. For the reading of each standard, the instrument stores the known concentration and the V-sec response to it. The ratio for the standard, V-sec:ppm, is then used to quantify the concentrations of identifiable vapors in field samples according to their V-sec values.

The concentrations of unidentified compounds are calculated in a similar manner. Although petroleum hydrocarbons produce variable instrumental responses, the assumption may be made that all of the hydrocarbon constituents have response-to-concentration ratios approximately equivalent to that of benzene and that all quantifications may be based on the ratio for benzene. In the table of results, the column entitled "Peaks Prior to Benzene" represents the sum of the responses in V-sec for all peaks eluting prior to benzene, proportioned to the calibrated V-sec response for benzene. Similarly, the column entitled "Total Detected Petroleum Hydrocarbons" or "Total Volatile Hydrocarbons" represents the sum of all V-sec responses, proportioned to that for benzene.

The gas chromatograph is operated in backflush mode to prevent contamination of the analytical column with high concentrations of interfering compounds. Blanks are run to ensure that the system was free of contamination. As necessary, the instrument is re-calibrated by injecting standards and by running ambient air blanks approximately every two hours through the day. This re-calibration ensures that the system is operating consistently and that parametric changes caused by temperature changes through the day are accounted for. These data, along with multiple standard runs, ensure system reproducibility.

Table 1 presents the results of the SVCA. Figures 5 through 8 show isoconcentrations contours for several constituents. Moderate-to-high levels of hydrocarbon contamination of the shallow soil gas were detected. As can be seen from Figures 5 through 8, there appears to be a concentration of hydrocarbons in the vicinity of the tank field and perhaps another one near the western pump island. The soil gas hydrocarbon plumes appear to extend beyond site boundary to the southeast.

Although there are no ground-water data for contamination at this site, the SVCA results can be used to make order-of-magnitude estimates of potential dissolved benzene and toluene concentrations. A Henry's Law constant (H) is the ratio of a chemical's concentration in air to its concentration in water at equilibrium. It can be estimated by:

$$H = C_{SV}/C_w \quad \text{(Equation 1)}$$

where

H = Henry's Law constant, atm·L/mole;

$C_{SV}$  = vapor concentration, atm; and

$C_w$  = water concentration, mole/L.

For estimating ground water concentrations, equation 1 can be rearranged as:

$$C_w = C_{SV}/H \quad \text{(Equation 2)}$$

To make the units compatible, the following conversions are used:

1 ppm soil vapor =  $1 \times 10^{-6}$  atmosphere

1 mole = mole weight expressed in milligrams

The molecular weights of benzene and toluene are  $78 \times 10^3$  mg/mole and  $92 \times 10^3$  mg/mole, respectively; their Henry's Law constants are 5.6 and 6.4 atm·L/mole (EPA 1986). Using these data and Equation

TABLE 1 CONCENTRATIONS OF HYDROCARBON CONSTITUENTS IN SOIL VAPOR AT CHEVRON SS 9-7127, I-580 AND GRANT LINE ROAD, TRACY, CALIFORNIA, 27 OCTOBER 1987

Sample Location	Depth (ft)	Peaks <sup>a</sup> Prior to Benzene (ppm)	Benzene (ppm)	Toluene (ppm)	Total <sup>a</sup> Detected Hydrocarbons (ppm)
V1	3	<5	<1	<1	<5
V1/B	5	3,700	650	3,200	7,500
V1/C	8	18,000	600	2,800	20,000
V2	5	130	<5	30	160
V3	3	10	5	10	30
V3/B	5	<5	1	10	15
V4	3	20,000	3,200	5,200	28,500
V4/B	5	120	130	1,900	2,000
V5	5	1	<1	<5	<5
V5/B	7	620	40	<1	750
V6	5	1,150	540	160	7,300
V7	5	1,300	<5	<5	1,400
V8	3	<1	<1	<1	<1
V8/B	8	<1	<1	<1	<1
V9	8	1	<1	<10	10
V10	8	<1	<1	<1	<1
V11	5	<1	<1	<1	<1
V12	8	<1	<1	<1	<1
V13	12	20	<1	<1	25
V14	8	<1	<1	<1	<1
V15	12	<1	<1	<1	<1

BLANK DATA

Test Time	Peaks Prior to Benzene (ppm)	Benzene (ppm)	Toluene (ppm)
0948	<0.1	<0.1	<0.1
1256	<0.1	<0.1	<0.1

PERCENTAGE OF STANDARD RECOVERED

Test Time	Standard Benzene	Standard Toluene
1001	100	100
1306	100	100
1447	101	99

a. Quantification based on the volt-second:ppm response ratio for benzene; see text.

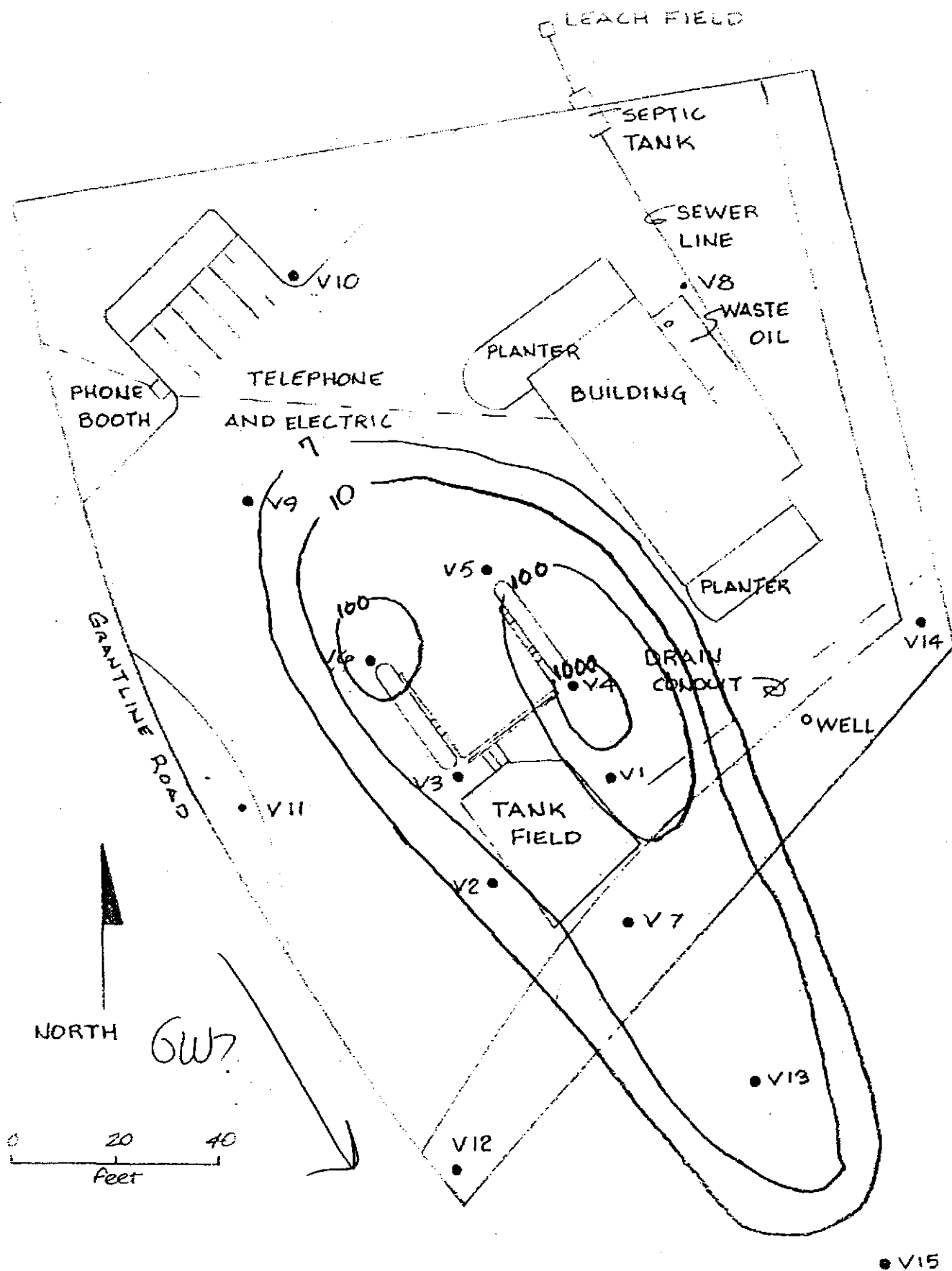


Figure 5. Isoconcentration contours of benzene (ppm) with shallow soil gas at Chevron Service Station 9-7127, Tracy, California.

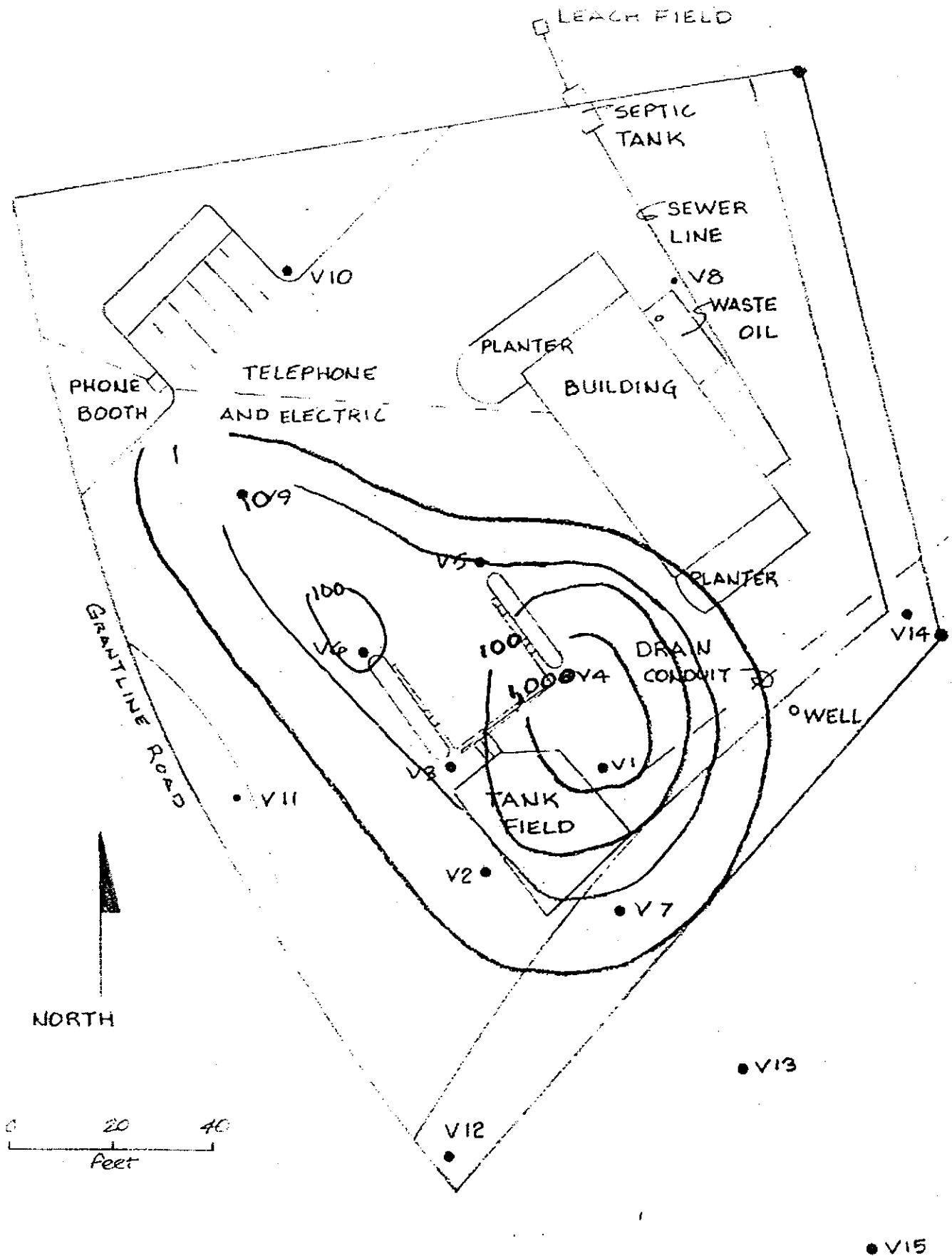


Figure 6. Isoconcentration contours of toluene (ppm) with the shallow soil gas at Chevron Service Station 9-7127, Tracy, California.



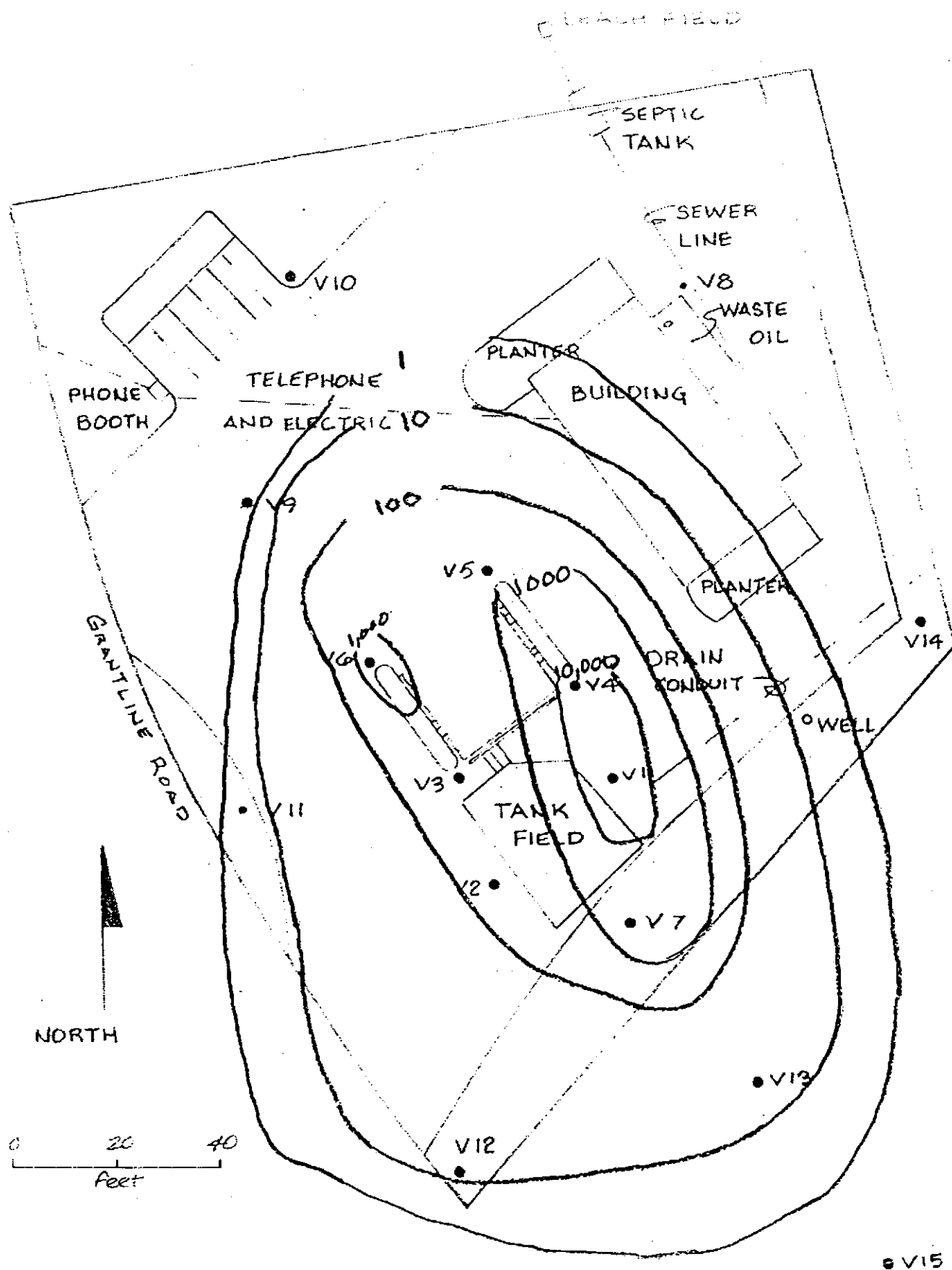


Figure 7. Isoconcentration contours of compounds which elute prior to benzene (ppm) in the shallow soil gas at Chevron Service Station 9-7127, Tracy, California.

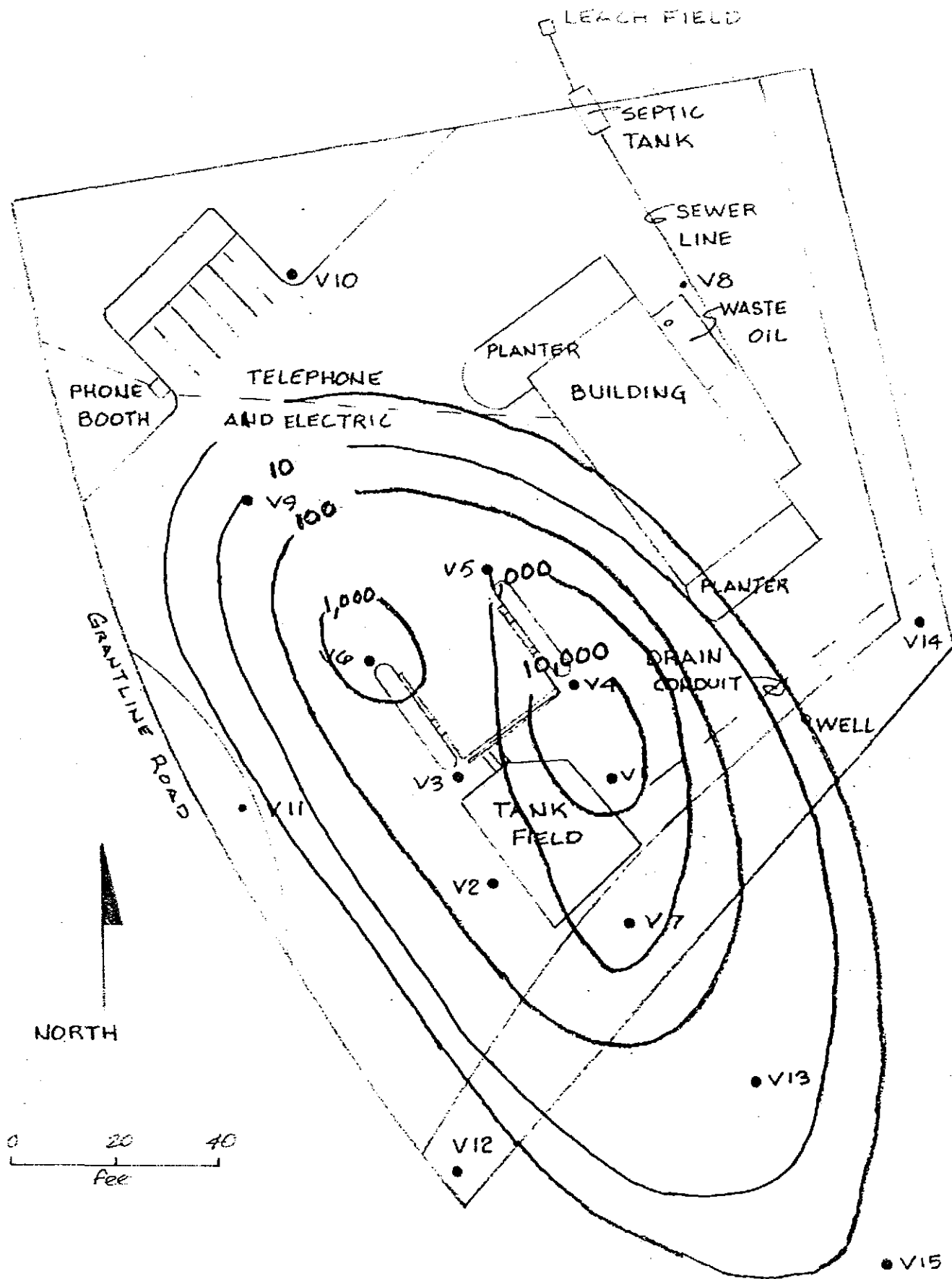


Figure 8. Isoconcentration contours of total volatile hydrocarbon (ppm) in the shallow soil gas at Chevron Service Station 9-7127, Tracy, California.

2, the expected ground-water concentration of benzene can be estimated as:

$$C_{w\text{-Benzene}} = \frac{(C_{sv}) (1 \times 10^{-6} \text{ atm/ppm}) (78 \times 10^3 \text{ mg/mole})}{(5.6 \text{ atm}\cdot\text{L/mole})}$$
$$= 0.014 C_{sv}$$

For toluene, the ground-water concentration can be estimated by:

$$C_{w\text{-toluene}} = \frac{(C_{sv}) (1 \times 10^{-6} \text{ atm/ppm}) (92 \times 10^3 \text{ mg/mole})}{(6.4 \text{ atm}\cdot\text{L/mole})}$$
$$= 0.014 C_{sv}$$

The area between the eastern pump island and the tank field (SVCA point V4) had a benzene concentration of 3,200 ppm and a toluene concentration of 5,200 ppm. Based on these soil gas concentrations, the ground water may contain 45 mg/L benzene and 70 mg/L toluene. A study sponsored by the San Francisco Bay Regional Water Quality Board (1985) found that gasoline-saturated water may contain as high as 40 mg/L of benzene and 9-76 mg/L of toluene. A similar study sponsored by the American Petroleum Institute (1985) suggested that the sum concentration of benzene, toluene, xylenes, and ethylbenzene in gasoline-saturated ground water will be at least 10-20 mg/L. Thus, the SVCA results at the Tracy site suggest there could be free product at this site.

### 3. CONCLUSIONS AND RECOMMENDATIONS

On 27 October 1987, EA conducted a SVCA survey at Chevron Service Station 9-7127 in Tracy, California. The results of the survey suggested that there could be floating free product in the area of the tank field and pump island. It is recommended that five ground-water monitoring wells be installed on the site (Figure 9). One well should be placed between SVCA points V4 and V1, to confirm the contamination in this area. The second and third wells should be along the southern site boundary, opposite the tank field, to delineate any contaminant plume. Two wells should be placed on the northern and western side boundaries to establish background concentrations. During well construction it is recommended that soil samples be taken every five feet for chemical analysis. If there is no floating product, ground-water samples should be taken. Soil and ground-water samples should be analyzed for total petroleum hydrocarbons, benzene, toluene, xylenes, and ethylbenzene.

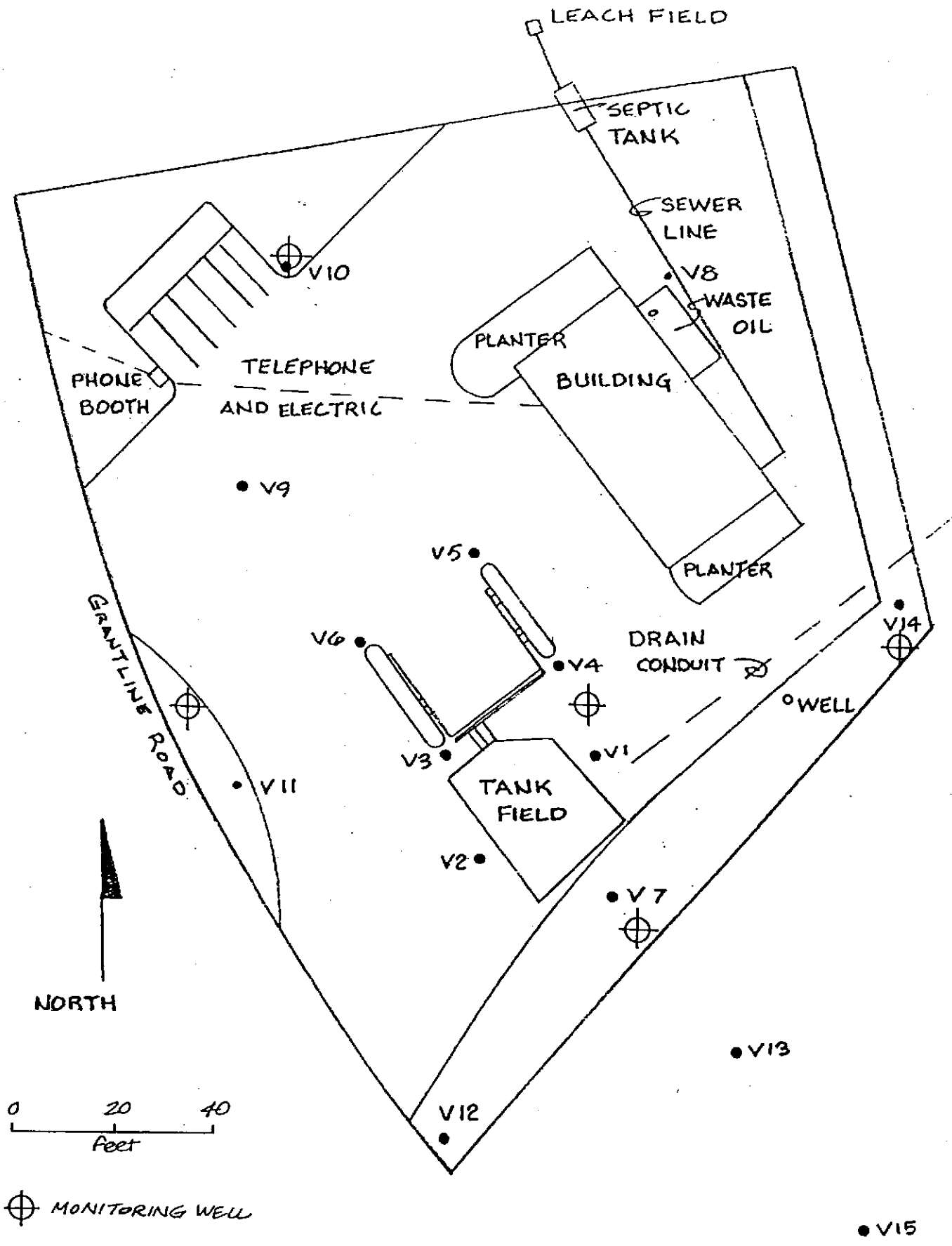


Figure 9. Proposed locations for monitoring wells at Chevron Service Station 9-7127, Tracy, California.

#### 4. REFERENCES

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EA ENGINEERING,  
SCIENCE, AND  
TECHNOLOGY, INC.

559-7127-001/F/27/10/87

SVCA DATA SHEET

Project Number: CHV

Date: 27 October 1987

Project Manager: \_\_\_\_\_

Analysts: CAP/PM/RS

Site Location: Grant Line Rd. # I-580  
Tracy CA

Pump Number: 9-7127

Grid Location	Time	Depth (ft)	OVA. (ppm)	Purge Time	Vacuum Reading	Soil Type	Comments
V1		3		10	25 <i>in Hg</i>	*	asphalt covering tank area
V3		3		10	27	*	
V1/B		5		10	3		noticeable vacuum decrease
V4		3		10	7		
V1/C		8		10	3		
V4/B		5		10	15		
V7		5		10	0		
V2		5		10	7		
V3/B		5		10	10		
V5		5		10	12	*	
V6		5		10	3		
V5/B		7		10	10		
V8		3		20	25	*	waste oil
V9		8		10	10	*	
V8/B		8		10	5		
V10		9		10	0		Soil cover

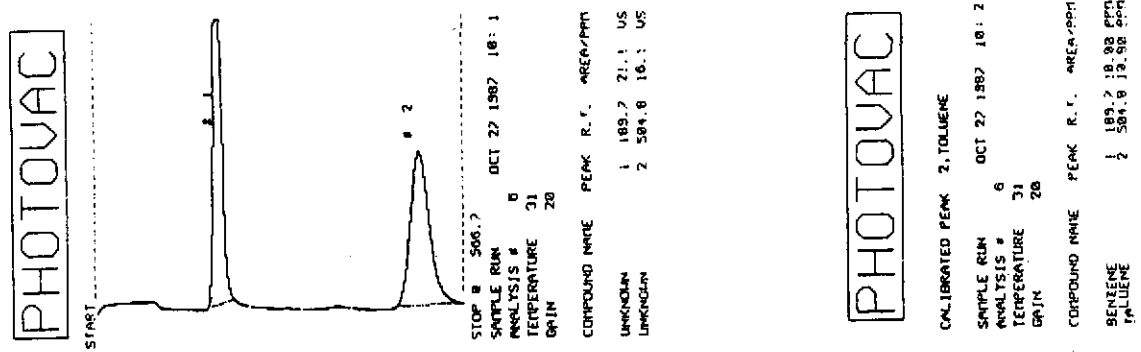




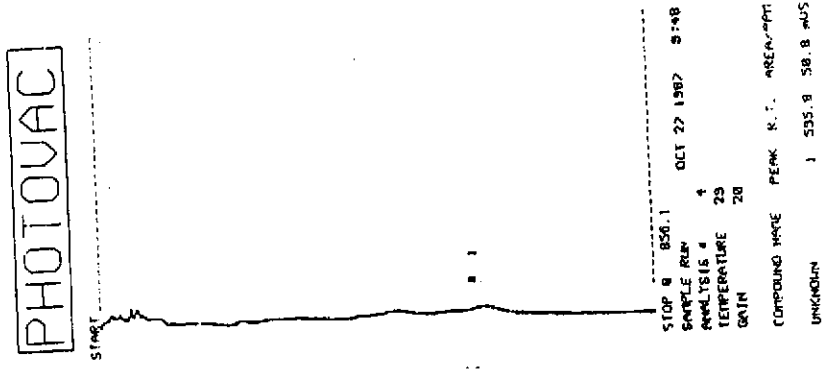
STATION NUMBER: 9-7127

PROJECT NUMBER: \_\_\_\_\_  
DATE: 27 Oct  
Chemist: CAP  
Standard Volume Injection: 100 µl

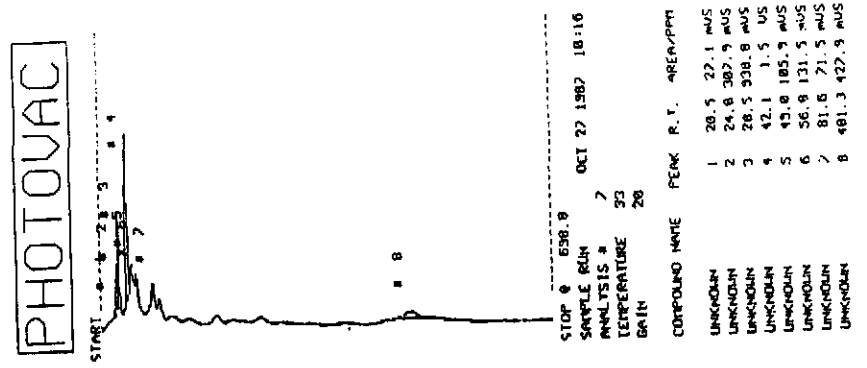
Sample: STANDARD  
Volume Injected: 100 µl



Sample: BLANK  
Volume Injected: /



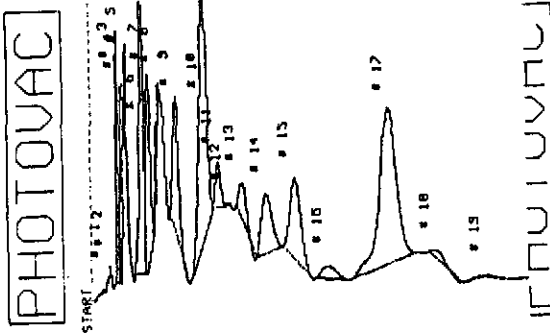
Sample: VI  
Volume Injected: 50 µl



STATION NUMBER: 9-7127

PROJECT NUMBER: CHV  
 DATE: 27 Oct 1987  
 Chemist: CAF  
 Standard Volume Injection: 100 µl

Sample: V3  
 Volume Injected: 100 µl

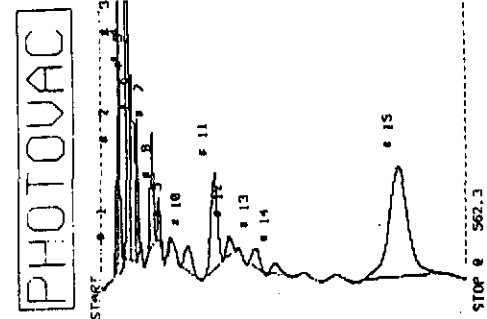


STOP @ 512.3    OCT 27 1987 18:34

ANALYSIS #	9
SAMPLE RUN	10
TEMPERATURE	33
GAIN	20

COMPOUND NAME	PEAK	R.T.	AREA/PPT
UNKNOWN	1	24.8	25.9
UNKNOWN	2	28.5	87.9
UNKNOWN	3	41.5	2.6
UNKNOWN	4	48.0	1.8
UNKNOWN	5	55.9	1.1
UNKNOWN	6	79.7	2.7
UNKNOWN	7	98.1	4.8
UNKNOWN	8	188.4	492.8
UNKNOWN	9	134.3	4.7
BENZENE	10	176.5	5.536
UNKNOWN	11	195.7	1.2
UNKNOWN	12	215.3	24.8
UNKNOWN	13	235.9	1.9
UNKNOWN	14	273.2	3.6
UNKNOWN	15	317.9	4.7
UNKNOWN	16	362.7	974.3
TOLUENE	17	403.7	5.383
UNKNOWN	18	536.3	568.6
UNKNOWN	19	611.9	118.8

Sample: V1/B  
 Volume Injected: 100 µl  
1:400 dilution



STOP @ 562.3    OCT 27 1987 18:45

ANALYSIS #	9
SAMPLE RUN	9
TEMPERATURE	34
GAIN	28

COMPOUND NAME	PEAK	R.T.	AREA/PPT
UNKNOWN	1	20.9	143.8
UNKNOWN	2	25.8	1.1
UNKNOWN	3	28.2	3.2
UNKNOWN	4	41.5	6.9
UNKNOWN	5	48.4	3.6
UNKNOWN	6	55.9	1.8
UNKNOWN	7	79.7	2.8
UNKNOWN	8	89.6	885.2
UNKNOWN	9	185.5	79.9
UNKNOWN	10	134.1	586.4
UNKNOWN	11	125.9	1.785
BENZENE	12	158.9	563.6
UNKNOWN	13	235.6	883.2
UNKNOWN	14	271.4	519.7
TOLUENE	15	483.7	8.101

Sample: V4  
 Volume Injected: 100 µl  
1:400 dilution



STOP @ 527.5    OCT 27 1987 18:57

ANALYSIS #	10
SAMPLE RUN	10
TEMPERATURE	33
GAIN	28

COMPOUND NAME	PEAK	R.T.	AREA/PPT
UNKNOWN	2	24.6	675.1
UNKNOWN	3	29.6	2.1
UNKNOWN	4	32.2	872.8
UNKNOWN	5	48.4	28.9
UNKNOWN	6	78.6	11.5
UNKNOWN	7	88.6	6.2
UNKNOWN	8	184.9	583.6
UNKNOWN	9	131.5	3.3
UNKNOWN	10	123.2	8.178
BENZENE	11	156.3	537.8
UNKNOWN	12	218.7	81.7
UNKNOWN	14	268.7	1.6
UNKNOWN	15	312.8	1.3
TOLUENE	16	458.5	17.38

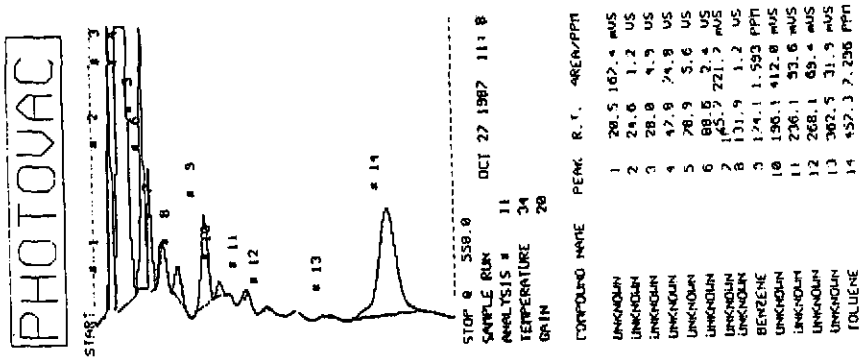
9000  
 14700V  
 100µl  
 PPT

PROJECT NUMBER: CHV  
 DATE: 27 Oct  
 Chemist: CAF  
 Standard Volume Injection: 100 µl

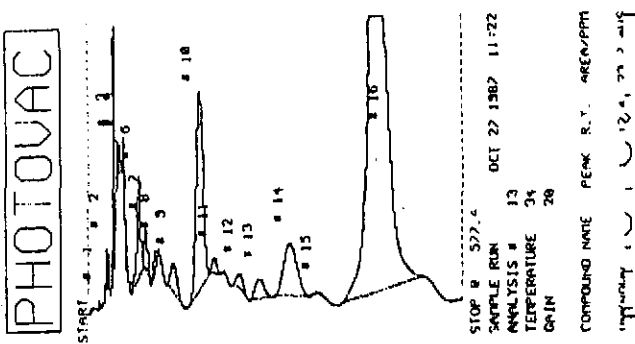
STATION NUMBER: 9-7127

TA  
104.8 VS  
90VS  
36000 41,600 v

Sample: V1/C  
 Volume Injected: 100 µl  
1:400 dilution

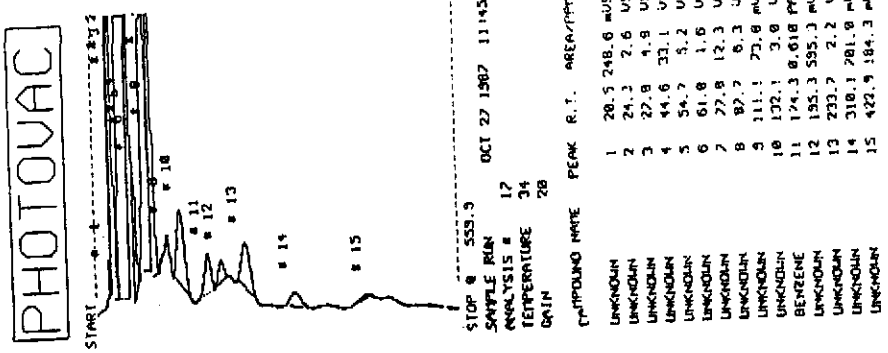


Sample: V4/B  
 Volume Injected: 100 µl  
1:40 dilution



TA  
93.1  
151.5  
356  
23  
TA  
100 VS  
95

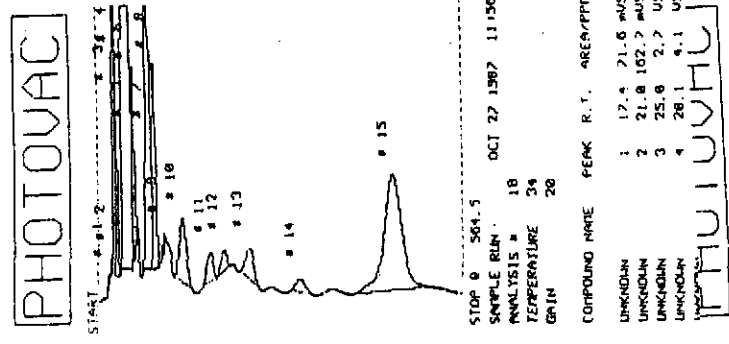
Sample: V7  
 Volume Injected: 100 µl  
1:40 dilution



STATION NUMBER: 9-7127

PROJECT NUMBER:  
 DATE: 27 Oct 1987  
 Chemist: CAF  
 Standard Volume Injection: 100 µl

Sample: V2  
 Volume Injected: 1ml  
 1:40 dilution  
 ∴ x4 dilution



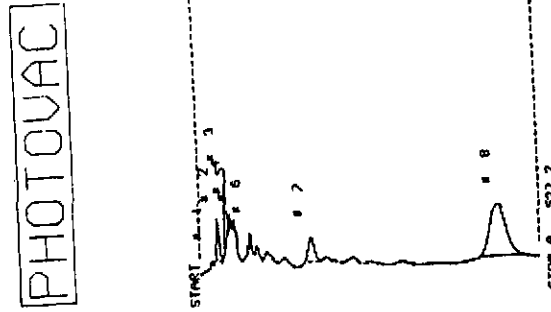
CALIBRATED PEAK 15, TOLUENE

SAMPLE RUN OCT 27 1987 11:59  
 ANALYSIS # 18  
 TEMPERATURE 34  
 GAIN 20

COMPUND NAME	PEAK	R.T.	AREA/PPT
UNKNOWN	1	17.4	21.6 µS
UNKNOWN	2	21.8	102.7 µS
UNKNOWN	3	25.8	2.7 US
UNKNOWN	4	28.1	4.1 US
UNKNOWN	5	41.6	48.4 US
UNKNOWN	6	55.6	2.4 US
UNKNOWN	7	78.5	9.1 US
UNKNOWN	8	88.6	4.8 US
UNKNOWN	9	104.8	123.4 µS
UNKNOWN	10	133.1	2.5 US
BENZENE	11	176.3	0.491 PPT
UNKNOWN	12	192.1	622.4 µS
UNKNOWN	13	236.3	1.4 US
UNKNOWN	14	314.8	672.9 µS
TOLUENE	15	468.5	7.763 PPT

101  
320  
PR  
260

Sample: V3/B  
 Volume Injected: 1ml  
 1:40 dilution  
 ∴ 1:4 dilution



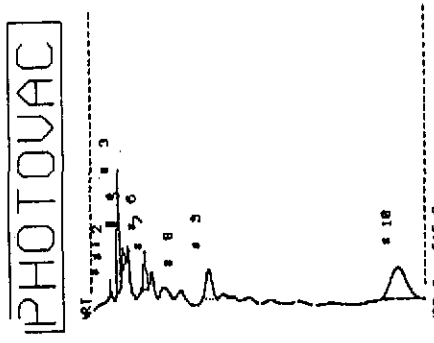
CALIBRATED PEAK 15, TOLUENE

SAMPLE RUN OCT 27 1987 12:10  
 ANALYSIS # 19  
 TEMPERATURE 34  
 GAIN 20

COMPUND NAME	PEAK	R.T.	AREA/PPT
UNKNOWN	2	28.8	623.3 µS
UNKNOWN	3	41.7	753.7 µS
UNKNOWN	4	48.6	88.5 µS
UNKNOWN	5	55.8	133.4 µS
UNKNOWN	6	79.5	84.8 µS
UNKNOWN	7	176.5	0.394 PPT
BENZENE	8	465.3	3.316 PPT

PR  
51  
300  
150  
150

Sample: V5  
 Volume Injected: 100 µl



CALIBRATED PEAK 10, TOLUENE

SAMPLE RUN OCT 27 1987 12:21  
 ANALYSIS # 20  
 TEMPERATURE 33  
 GAIN 20

COMPUND NAME	PEAK	R.T.	AREA/PPT
UNKNOWN	2	28.8	167.8 µS
UNKNOWN	3	42.3	1.8 US
UNKNOWN	4	49.2	112.2 µS
UNKNOWN	5	52.8	223.1 µS
UNKNOWN	6	81.5	586.4 µS
UNKNOWN	7	81.7	37.1 µS
UNKNOWN	8	132.1	24.6 µS
BENZENE	9	186.5	0.473 PPT
TOLUENE	10	476.1	1.861 PPT

PHOTOVAC

CALIBRATED PEAK 10, TOLUENE

SAMPLE RUN OCT 27 1987 12:21  
 ANALYSIS # 20  
 TEMPERATURE 33  
 GAIN 20

COMPUND NAME	PEAK	R.T.	AREA/PPT
UNKNOWN	2	28.8	167.8 µS
UNKNOWN	3	42.3	1.8 US
UNKNOWN	4	49.2	112.2 µS
UNKNOWN	5	52.8	223.1 µS
UNKNOWN	6	81.5	586.4 µS
UNKNOWN	7	81.7	37.1 µS
UNKNOWN	8	132.1	24.6 µS
BENZENE	9	186.5	0.473 PPT
TOLUENE	10	476.1	1.861 PPT

PR  
101

PROJECT NUMBER: CHV

DATE: 27 Oct 1987

Chemist: CAF

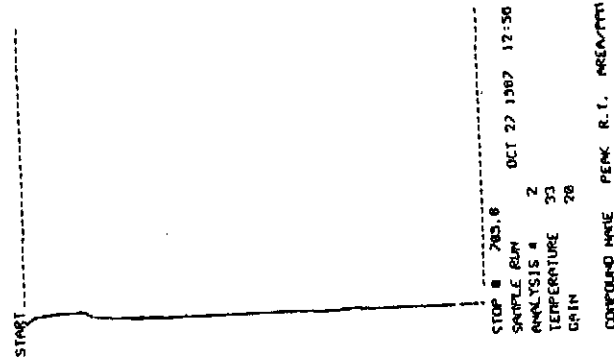
Standard Volume Injection: 100 µl

STATION NUMBER: 9-7127

Sample: BLANK

Volume Injected: 100 µl

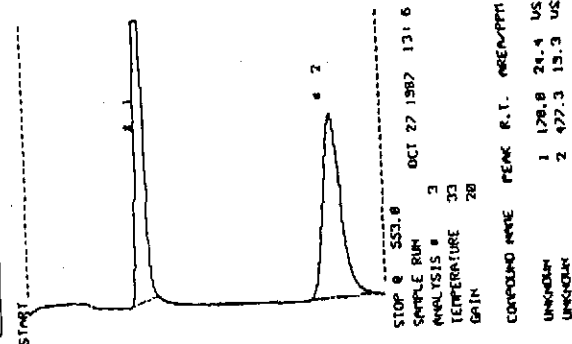
PHOTOVAC



Sample: STANDARD

Volume Injected: 100 µl

PHOTOVAC



PHOTOVAC

CALIBRATED PEAK 2, TOLUENE

SAMPLE RUN    OCT 27 1987 13:16  
 ANALYSIS # 3  
 TEMPERATURE 33  
 GAIN 28

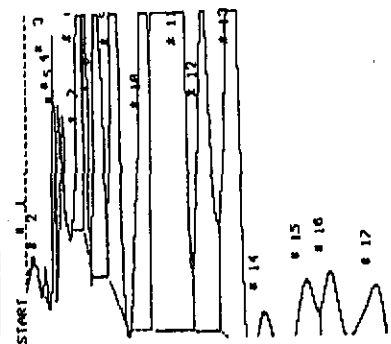
COMPOUND NAME    PEAK R.T. AREA/PTI  
 BENZENE            1 178.8 18.88 PPTI  
 TOLUENE            2 477.3 18.88 PPTI

Sample: V6

Volume Injected: 100 µl

1:400 dilution

PHOTOVAC



UNKNOWN            1 18.4 188.4 µUS  
 UNKNOWN            2 23.8 557.4 µUS  
 UNKNOWN            3 12.2 3.4 US  
 UNKNOWN            4 43.4 2.1 US  
 UNKNOWN            5 58.6 883.9 µUS  
 UNKNOWN            6 88.5 18.7 US  
 UNKNOWN            7 58.4 7.1 US  
 UNKNOWN            8 186.9 10.3 US  
 UNKNOWN            9 135.4 25.8 US  
 UNKNOWN            10 181.8 13.51 PPTI  
 UNKNOWN            11 213.2 100.7 US  
 UNKNOWN            12 274.5 26.9 US  
 UNKNOWN            13 313.4 53.8 US  
 UNKNOWN            14 378.5 5.1 US  
 UNKNOWN            15 435.3 5.8 US  
 TOLUENE            16 471.3 4.445 PPTI  
 UNKNOWN            17 541.8 18.2 US

STATION NUMBER:

9-7127

PROJECT NUMBER: CHV

DATE: 27 Oct 1987

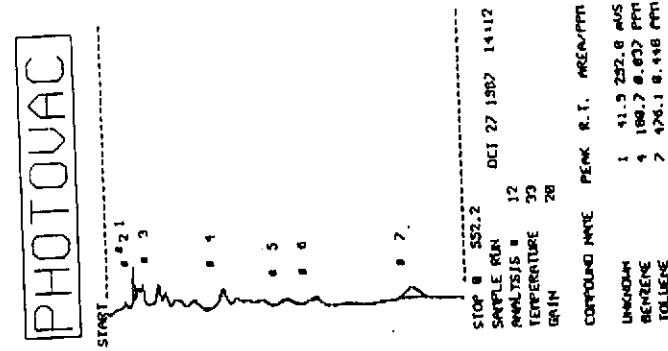
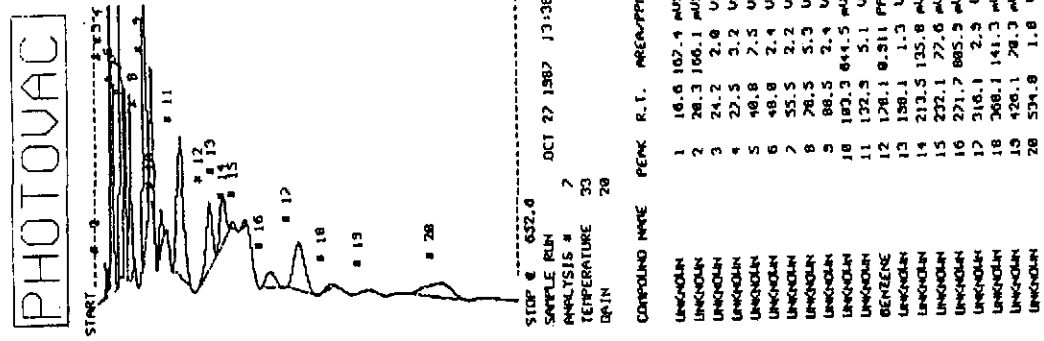
Chemist: CJP

Standard Volume Injection: 100 µl

Sample: VS/B

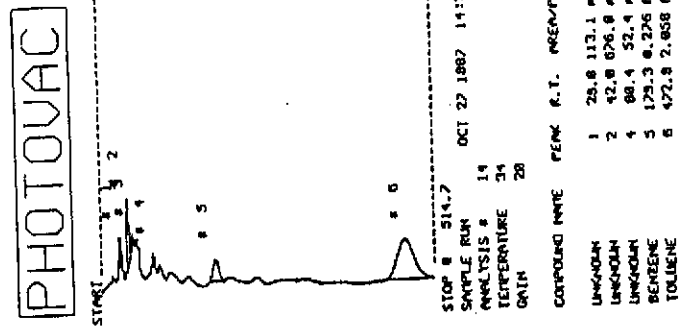
Volume Injected: 100 µl

1:40 dilution



Sample: V8

Volume Injected: 100 µl



Sample: V9

Volume Injected: 100 µl

1:40 dilution

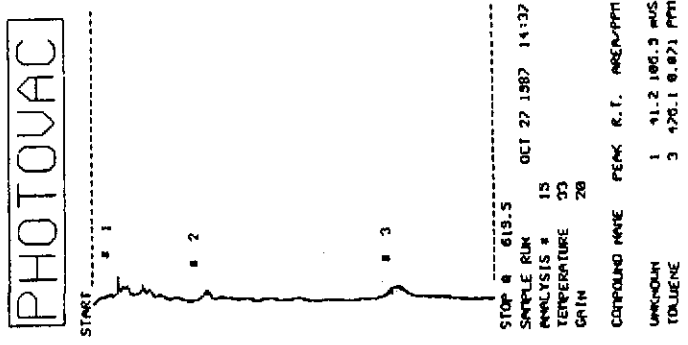
1:4 dilution

17

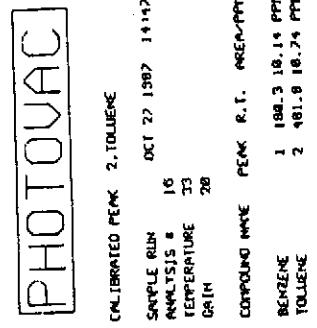
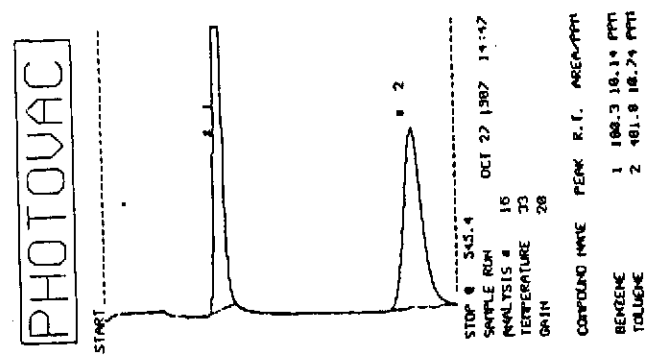
STATION NUMBER: 9-7127

PROJECT NUMBER: CAV  
DATE: 27 Oct 1987  
Chemist: CAF  
Standard Volume Injection: 100 µl

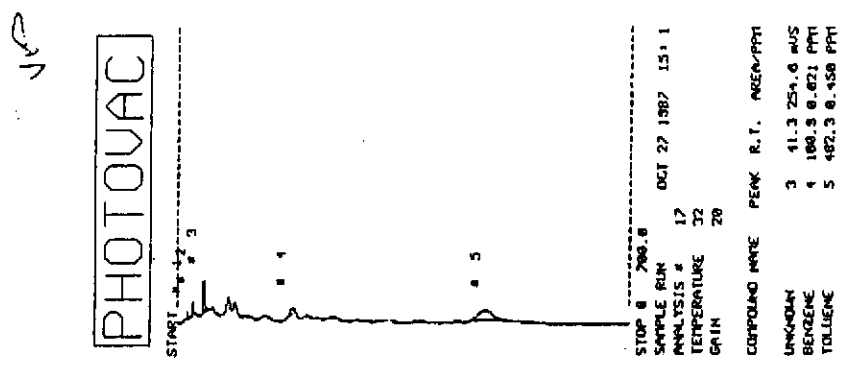
Sample: V8/B  
Volume Injected: 100 µl



Sample: STANDARD  
Volume Injected: 100 µl



Sample: V10  
Volume Injected: 100 µl

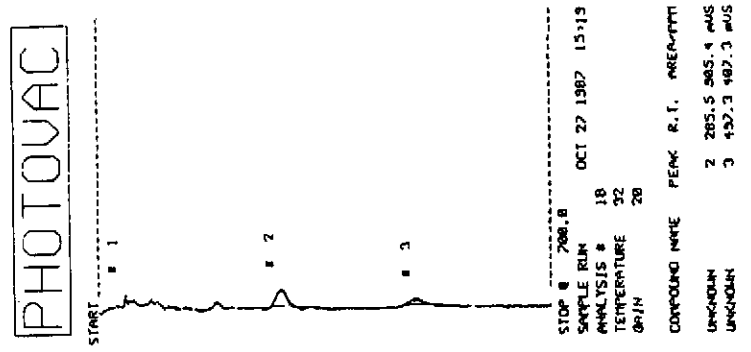


PROJECT NUMBER: CHU  
DATE: 27 Oct 1987

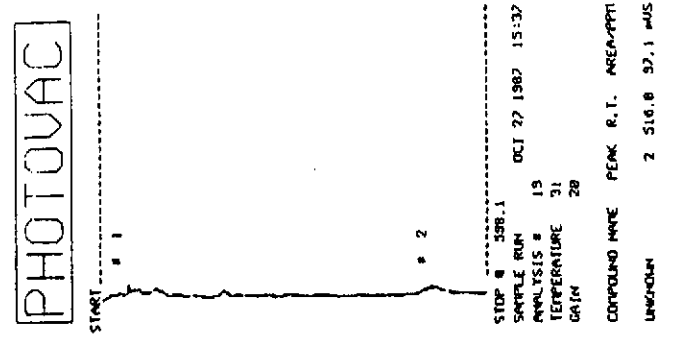
STATION NUMBER: 9-7127

Chemist: QAP  
Standard Volume Injection: 100 µl

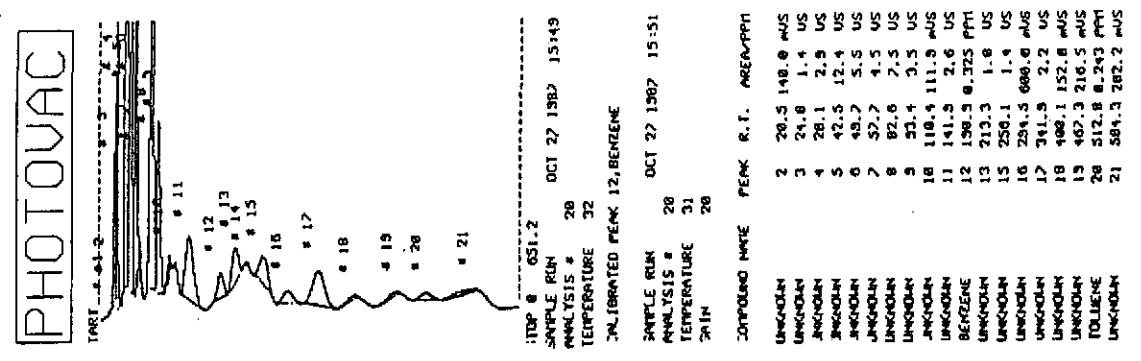
Sample: V11  
Volume Injected: 100 µl



Sample: V12  
Volume Injected: 100 µl



Sample: V13  
Volume Injected: 100 µl





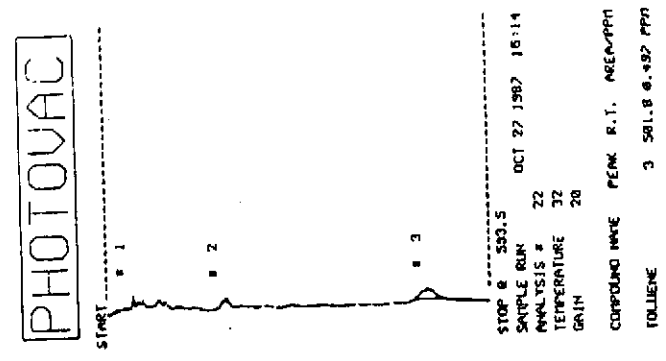
STATION NUMBER: 9-7127

PROJECT NUMBER: CHV  
DATE: 27 Oct 1957  
Chemist: CJP  
Standard Volume Injection: 100  $\mu$ l

Sample: V14  
Volume Injected: 100  $\mu$ l



Sample: V15  
Volume Injected: 100  $\mu$ l



Sample: \_\_\_\_\_  
Volume Injected: \_\_\_\_\_

To make the units compatible, the following conversions are used:

$$\begin{aligned} 1 \text{ ppm soil vapor} &= 1 \times 10^{-6} \text{ atmosphere} \\ 1 \text{ mole} &= \text{mole weight expressed in milligrams} \end{aligned}$$

The molecular weights of benzene and toluene are  $78 \times 10^3$  mg/mole and  $92 \times 10^3$  mg/mole, respectively; their Henry's Law constants are 5.6 and 6.4 atm·L/mole (EPA 1986). Using these data and Equation 2, the expected ground-water concentration of benzene can be estimated as:

$$\begin{aligned} C_{w\text{-Benzene}} &= \frac{(C_{sv}) (1 \times 10^{-6} \text{ atm/ppm}) (78 \times 10^3 \text{ mg/mole})}{(5.6 \text{ atm}\cdot\text{L/mole})} \\ &= 0.014 C_{sv} \end{aligned}$$

For toluene, the ground-water concentration can be estimated by:

$$\begin{aligned} C_{w\text{-toluene}} &= \frac{(C_{sv}) (1 \times 10^{-6} \text{ atm/ppm}) (92 \times 10^3 \text{ mg/mole})}{(6.4 \text{ atm}\cdot\text{L/mole})} \\ &= 0.014 C_{sv} \end{aligned}$$

The area between the eastern pump island and the tank field (SVCA point V4) had a benzene concentration of 3,200 ppm and a toluene concentration of 5,200 ppm. Based on these soil gas concentrations, the ground water may contain 45 mg/L benzene and 70 mg/L toluene. A study sponsored by the San Francisco Bay Regional Water Quality Board (1985) found that gasoline-saturated water may contain as high as 40 mg/L of benzene and 9-76 mg/L of toluene. A similar study sponsored by the American Petroleum Institute (1985) suggested that the sum concentration of benzene, toluene, xylenes, and ethylbenzene in gasoline-saturated ground water will be at least 10-20 mg/L. Thus, the SVCA results at the Tracy site suggest there could be free product at this site.