

PACIFIC ENVIRONMENTAL GROUP, INC.

June 27, 1997 Project 325-004.1E

Mr. Phil Briggs Chevron Products Company P.O. Box 5004 San Ramon, California 94583-0804

Re: Risk-Based Corrective Action - Tier 2 Former Chevron Service Station 9-7127 Grant Line Road at Interstate 580 , Tracy, California

FIRST INPDATE

Dear Mr. Briggs:

On behalf of Chevron Products Company, Pacific Environmental Group, Inc. (PACIFIC) has completed a Tier 2 Risk-Based Corrective Action (RBCA) evaluation for the site referenced above. The RBCA is based upon the framework presented in the American Society for Testing and Materials (ASTM), *Standard Guide for Risk-Based Corrective Action Applied at Petroleum Release Sites, Designation: E 1739-95.* Since the site background was presented in the previous RBCA Tier 1 report (PACIFIC, June 28, 1996), for brevity, it will not be presented again.

In PACIFIC's Tier 1 RBCA evaluation, the impacted groundwater and subsurface soil representative concentrations were compared to Permissible Exposure Limits (PELs) for inhalation of benzene, ethylbenzene, toluene, and xylenes (BTEX compounds). The resulting comparison of the PELs to the representative concentrations was favorable. However in order to be as conservative as possible, a Tier 2 evaluation of the site was conducted. This letter presents those results.

METHODOLOGY

Sampling

In order to conduct the Tier 2 evaluation, site-specific data was collected in order to replace the overly conservative default values inherent in a Tier 1 evaluation. This data was collected by obtaining an outcrop sample of the Neroly Formation Sandstone from the roadcut exposure adjacent to the southwest boundary of the site. Groundwater occurs at approximately 28 feet below ground surface (bgs) in Well MW-1, and the outcrop sample is similar in lithologic character to the sandstone logged in Well MW-1

and to sandstone evident in many of the soil borings drilled on site. Therefore, the physical characteristics of the outcrop sample are reasonably representative of site conditions.

The outcrop sample was collected on November 28, 1996, and was submitted to Cooper Testing Lab, Inc., for falling head permeability, fraction of organic carbon, pH, and specific gravity testing (Attachment A). Table 1 presents the site-specific data used to calculate the Site-Specific Target Levels (SSTLs). The data obtained from the falling head permeability test (ASTM D5085) included permeability, volume of solids, volume of voids, percent porosity, and percent saturation. The initial values obtained during the test were used to calculate the Tier 2 SSTLs. The "initial" values more accurately represent actual site conditions; this is due to the fact that the initial data is collected at the start of the test when moisture content more closely resembles actual field conditions. After the initial data is obtained, the sample is saturated with water in order to determine its permeability and then the parameters are recorded again producing the "final" column.

The volumetric water and air contents of the sample were determined in cubic centimeters (cc) in the following manner for the vadose zone: -0.20,

Volume of Voids x % Saturation = cc Water $V_{010} = \frac{1000}{700} = \frac{42.64}{70292} = Porestry = 4670$

42.64 cc x 0.5488 = 23.4 cc watertherefore, 42.64 cc - 23.4 cc = 19.24 cc air 23.4/42.64 = 55/0 23.4 cc water / 92.92 total cc = 25% water content 19 24/42.69= 45/00

4610

Rieb For check

and 19.24 cc air / 92.92 total cc = 20% air content

For the capillary fringe zone, the water and air contents were estimated to be 29% and 17%, respectively. When compared with ASTM's Tier 1 porosity value of 38%, the capillary fringe water and air contents comprise 90% and 10%, respectively. In order to be more conservative, the Tier 2 water content of the capillary zone was estimated to be 29% (approximately 63% of the porosity) while the air content of the capillary zone was estimated to be 17% (approximately 37% of the porosity). These are conservative estimates when compared with American Society for Testing and Material's (ASTM) default Tier 1 values of 0.342 water content and 0.038 air content.

The volumetric water and air contents of the possible future foundation crack were estimated to be 16% and 30%. These values, which must add up to meet the porosity, were obtained by subtracting the difference between the Tier 2 porosity value of 0.46 and the Tier 1 default of 0.38. This difference, equal to 0.08, was divided by two resulting in 0.04. The result (0.04) was then added to each of the Tier 1 default values for foundation crack water and air content values. Therefore, the Tier 1 foundation crack water content of 0.12 + 0.04 = 0.16 and the Tier 1 foundation crack air content of 0.26+0.04 = 0.30.

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These data replace the default values generally used to calculate the Risk-Based Screening Levels for Tier I RBCA evaluations. The site-specific data were derived from the analytical results of the physical testing. However, some of the site-specific data, such as vadose zone depth, depth to uppermost affected soil, and gradient were obtained from soil boring logs and quarterly groundwater monitoring reports. The laboratory soil test data for the physical tests are presented as Attachment A.

Calculation of Representative Concentrations

The representative concentrations of the site were recalculated for the Tier 2 evaluation in order to include more recent data and to present a more realistic interpretation of the site. The following summaries describe the methods used to calculate the Tier 2 representative concentrations of BTEX compounds.

- Groundwater: The means of the BTEX compounds for the last four quarters of data (November 1995, February, May, and August 1996) were calculated. However, non-detectable concentrations were not included in the calculation in order to provide a conservative risk assessment. Table 2 presents the groundwater data used to calculate the representative concentrations for the BTEX compounds. Since the data were not normally distributed (except for ethylbenzene), they were logtransformed. The Coefficient of Variance test was performed on the data in order to determine if the data were normally distributed prior to being logtransformed. The Coefficient of Variance test is le burd stout unte about lognormal. drem state simply dividing the arithmetic standard deviation of the data set by the arithmetic average. If the resulting outcome is greater than 1, then the data are not normally distributed and must be logtransformed. However if the outcome is less than or equal to 1, then the data are normally distributed and the arithmetic mean is to be used (EPA, 1992). All of the groundwater data (except ethylbenzene concentrations) were found not to be normally distributed and, therefore, were logtransformed. The groundwater data used to calculate the representative concentrations for Tier 2 are included in Attachment B and include historical groundwater analytical concentrations.
- Subsurface Soil: In order to obtain a representative concentration for each BTEX compound at the site, the most recent and relevant soil data were gathered from the former area of petroleum hydrocarbon impact. The data found to be the most appropriate for use in this evaluation consisted of the soil boring data collected in December 1987 (B-2, B-3, B-4, B-5, and B-7), sidewall and interface samples collected during the removal of the underground storage tanks (USTs) in 1991 (Af, Aop, Bf, Bop, Cf, Cop), and the soil data collected during the installation of Soil Boring B-1 and Monitoring Well MW-1 in

1992. Soil data from Monitoring Wells MW-5, MW-6, MW-7, and MW-8, installed in 1993, were also considered however, since all BTEX compounds were found to be below detectable concentrations, these data were not included in the calculation of the representative concentrations. The soil samples collected during the installation of Monitoring Wells MW-2 and MW-3 were not analyzed, therefore this data was unavailable. As with the groundwater data, all concentrations below detectable concentrations were excluded from the calculation of the mean. Table 3 presents the soil data used to calculate the representative concentrations. Again, the Coefficient of Variance test was performed on the data in order to determine if the data were normally distributed. It was determined that all BTEX compound data from the subsurface soil were not normally distributed; therefore the mean representative concentrations presented here are generated through the lognormal transformation procedure. The soil data used to generate the representative concentrations are presented as Attachment C.

HUMAN HEALTH RISK EVALUATION RESULTS

Groundwater Services, Inc. (GSI) software was used to evaluate the potential risk to human health and safety from the site. Since subsurface soil and groundwater are known to be impacted with BTEX compounds, these media were evaluated as potential pathways. Therefore, inhalation of groundwater and subsurface soil vapors indoors and inhalation of groundwater and subsurface soil vapors outdoors were four of the potential pathways evaluated. The last two pathways evaluated were subsurface soil leaching to groundwater and groundwater ingestion. All pathways were evaluated for on site exposures, not off site. All Tier 2 RBCA evaluations were completed using GSI's computer modeling software.

The models used to evaluate the pathways for benzene's carcinogenic risk utilize a slope factor, also called a cancer potency factor. The slope factor is used to estimate the upper-bound probability of an individual's risk of developing cancer as a result of a lifetime exposure to a particular level of a potential carcinogen. In order to comply with the State of California's stricter cancer slope factor values, a separate SSTL was calculated for benzene using a slope factor of 0.1 (mg/kg-day)⁻¹ (California Environmental Protection Agency, Office of Environmental Health Hazard Assessment, April 10, 1995). The Federal slope factor is 0.029 (mg/kg-day)⁻¹. The California slope factor results in a more conservative calculation than does the Federal slope factor.

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GROUNDWATER

Inhalation

Inhalation on site was evaluated by modeling the risk from groundwater volatilization to enclosed spaces and to ambient air. The excess lifetime risk of cancer, or target level, is the theoretical risk that one extra individual will develop cancer above the normal "background" of people who develop cancer. In general, risk assessments of residential areas use excess lifetime cancer risks of $1:1,000,000 (10^{-6})$; this number correlates to one extra individual developing cancer above the normal cancer rate for 1,000,000 people. Commercial and industrial settings usually have excess lifetime cancer risks of 10^{-6} to 10^{-4} . A excess lifetime risk for cancer of $1:100,000 (10^{-6})$ was used for benzene because the site is planned to become a commercial business in the near future. All other non-cancerous petroleum hydrocarbon compounds (ETX) were evaluated using a hazard quotient of 1. All exposure parameters were assumed to be commercial. The representative concentrations were then compared to the SSTLs generated by the GSI software.

| Constituent of Concern | Measured Mean Concentration (mg/L) | Modeled Volatilization to Ambient Air (mg/L) | Modeled Volatilization to Indoor Air (mg/L) | Minimum SSTL Exceeded (Yes/No) |
|---------------------------|--|---|--|--------------------------------------|
| Benzene | 0.32 | 290 | 0.96 | No , |
| Benzene - CA | 0.32 | 84 | 0.28 | Yes |
| Ethvlbenzene | 0.58 | >Sol | >Sol · | No |
| Toluene | 0.59 | >Sol | 110 | No |
| Xylenes | 0.15 | >Sol | >Sol | No |

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Groundwater - Inhalation

>Sol = Selected risk level is not exceeded for all possible dissolved levels (\leq pure component solubility).

All representative concentrations were below the applicable SSTLs at the specified risk levels except for benzene-CA for the modeled volatilization of groundwater to indoor air.

Ingestion

Ingestion was evaluated by modeling the risk for human ingestion of groundwater on site. An excess lifetime cancer risk of $1:100,000 (10^{-5})$ was used for benzene because the site is to become a commercial business in the near future. All other non-cancerous petroleum hydrocarbon compounds (ETX) were evaluated using a hazard quotient of 1. All exposure parameters were assumed to be commercial. The representative concentrations were then compared to the SSTLs generated by the GSI software.

| Constituent of Concern | Measured Mean Concentration (mg/L) | Modeled Ingestion (mg/L) | Minimum SSTL Exceeded (Ycs/No) |
|---------------------------|--|--------------------------------|--------------------------------------|
| Benzene | 0.32 | 0,099 | Yes |
| Benzene - CA | 0.32 | 0.029 | Yes |
| Ethylbenzene | 0.58 | 10 | No |
| Toluene | 0.59 | 20 | No |
| Xylenes | 0,15 | >Sol | No |
| Sol = Selected | ns per liter risk level is not exceede omponent solubility). | d for all possible | dissolved levels |

Groundwater - Ingestion

All representative concentrations were below the applicable SSTLs at the specified risk levels except for benzene.

SUBSURFACE SOIL

Inhalation

Inhalation was evaluated by modeling the risk from subsurface soil volatilization to enclosed spaces and to ambient air on site. An excess lifetime cancer risk of 1:100,000 (10^{-5}) was used for benzene because the site is planned to become a commercial business in the near future. All other non-cancerous petroleum hydrocarbon compounds (ETX) were evaluated using a hazard quotient of 1. All exposure parameters were assumed to be commercial. The representative concentrations were then compared to the SSTLs generated by the GSI software.

| Constituent of Concern | Measured Mean Concentration (mg/kg) | Modeled Volatilization to Ambient Air (mg/kg) | Modeled Volatilization to Indoor Air (mg/kg) | Minimum SSTL Exceeded (Yes/No) |
|------------------------|---|--|---|--------------------------------------|
| Benzene | 0.18 | 220 | 0.53 | No |
| Benzene - CA | 0.18 | 63 | 0.15 | Yes - |
| Ethylbenzene | 0.48 | >Res | >Res | No |
| Toluene | 0.38 | >Res | 160 | No |
| Xvlenes | 0.73 | >Res | >Res | No |

Subsurface Soil - Inhalation

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All representative concentrations were below the applicable SSTLs at the specified risk levels except for benzene-CA for the modeled volatilization of subsurface soil to indoor air.

Soil Leaching to Groundwater

Although soil leaching to groundwater is not an exposure pathway, it could provide a source for possible groundwater ingestion. Therefore, this pathway was evaluated for the Tier 2 RBCA. Again, an excess lifetime risk for cancer of 1:100,000 (10⁻⁵) was used for benzene because the site is planned to become a commercial business in the near future. All other non-cancerous petroleum hydrocarbon compounds (ETX) were evaluated using a hazard quotient of 1. All exposure parameters were assumed to be commercial. The representative concentrations were then compared to the SSTLs generated by the GSI software.

| Constituent of Concern | Measured Mean Concentration (mg/kg) | Leaching to Groundwater (mg/kg) | Minimum SSTL Exceeded (Yes/No) |
|---------------------------|---|---------------------------------------|--------------------------------------|
| Benzene | 0.18 | 0.13 | Yes |
| Benzene - CA | 0.18 | 0.037 | Yes |
| Ethylbenzene | 0:48 | 27 | No |
| Toluene | 0.38 | 73 | No |
| Xvienes | 0.73 | >Res | No |
| >Res = Selecte | rams per kilogram ed risk level is not exc stration | eeded for pure comp | ound present at any |

Subsurface Soil - Leaching to Groundwater

All representative concentrations were below the applicable SSTLs at the specified risk levels except for benzene for the modeled leaching of subsurface soil to groundwater.

RECOMMENDATIONS

Since the benzene concentrations at the site have been shown to present a slight risk to commercial workers for indoor inhalation and for groundwater ingestion with an excess lifetime cancer risk of $1:100,000 (10^{-5})$, the Tier 2 was rerun using an excess lifetime cancer risk of $1:10,000 (10^{-4})$. All of the benzene concentrations are below the SSTLs for the pathways evaluated above when the excess lifetime risk for cancer is decreased to $1:10,000 (10^{-4})$, except for on-site groundwater ingestion. However, if the $1:100,000 (10^{-5})$ excess lifetime risk for cancer is used, action needs to be taken in order to reduce or eliminate the possible exposure of future employees or customers at the site.

There are several corrective actions which could be undertaken in order to reduce the exposure to benzene; however, the most logical and cost-effective of these actions would

be to implement a risk management program for the site and any future development. Since the site is currently ranch land, there should be no risk to human health (Environmental Health Consultants, May 14, 1993) at the present time. However, PACIFIC recommends that, when the site is redeveloped commercially, a risk management plan be implemented.

The risk management plan should contain at least two provisions. The first is that in order to mitigate the risk for benzene inhalation indoors, the new building when constructed should have a vapor barrier within or beneath the floor that prevents vapors from traveling up from the soil or groundwater. This precaution should eliminate the risk from benzene for indoor air. The Tier 2 RBCA evaluation has already shown that inhaling outdoor air does not pose a risk from any BTEX compounds in the groundwater or soil.

Secondly, the existing water-supply well should be properly abandoned if it is not needed, since ingestion of benzene from groundwater has been shown to be a risk at 10⁻⁵ target level. Note that originally, the water-supply well was not installed as a drinking water source, but rather to operate the restrooms at the former service station. The water-supply well was recently sampled on February 19, 1997 (Attachment B), and general mineral, physical, and inorganic analyses were performed on the water obtained from the supply well. The results indicate that nitrate, specific conductance, and total dissolved solids are above drinking water standards and therefore the water is not suitable for human consumption. However, if site use depicts that non-potable water is necessary, the well may still be used, however a carbon adsorption vessel is recommended to be attached prior to resuming the use of the water-supply well. This would eliminate any potential risk from benzene for anyone ingesting the groundwater on the site, even though it is non-potable water. And hum often will carbon adsorption vessel be furdaced?

CONCLUSION

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> PACIFIC believes that the risk at the site can be reduced and managed by limiting exposure. Abandonment of the existing extraction well, or installation of a carbon adsorption vessel to treat water from the well prior to non-potable use and a vapor barrier beneath proposed buildings should prevent or limit potential risk from the site while also allowing natural attenuation to biodegrade BTEX compounds present in soil and groundwater at the site.

This is acceptable if enrent property onner will againe with recommandations.

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If you have any questions or comments on the contents of this letter, please call.

Sincerely,

Pacific Environmental Group, Inc.

Michelle Gracia

Michelle Gracia Senior Staff Scientist

Ross W.N. Tinline Senior Geologist RG 5860

REFERENCES

- American Society for Testing and Materials. Standard Guide for Risk-Based Corrective Action Applied at Petroleum Release Sites, Designation: E 1739-95. November 1995.
- California Environmental Protection Agency, Office of Environmental Health Hazard Assessment, April 10, 1995
- Chevron Products Company. Second and Third Quarter Groundwater Monitoring Reports for 1996, Former Chevron Service Station #9-7127 Interstate 580 and Grantline Road near Tracy, California. November 4, 1996.

Environmental Health Consultants. Human Risk Evaluation. May 14, 1993.

- Environmental Protection Agency. Statistical Analysis of Ground-Water Monitoring Data at RCRA Facilities, Addendum to Interim Final Guidance. July 1992.
- Groundwater Services, Inc. Tier 1 and Tier 2 RBCA Spreadsheet System. October 1995.

Pacific Environmental Group, Inc. Risk-Based Corrective Action Site Evaluation Results. June 28, 1996.

 Attachments: Table 1 - RBCA Default/Site-Specific Data Table 2 - Groundwater Data Used to Calculate the Representative Concentrations
 Table 3 - Soil Data Used to Calculate the Representative Concentrations
 Figure 1 - Site Location Map Figure 2 - Extended Site Map Attachment A - Laboratory Soil Test Data Attachment B - Historical Groundwater Data Attachment C - Historical Soil Certified Analytical Reports

Table 1 RBCA Default/Site-Specific Data

Risk-Based Corrective Action - Tier 2 Former Chevron Service Station 9-7127 Grant Line Road at Interstate 580 Tracy, California

| | Default | Site-Specific |
|--|----------|---------------|
| Characteristics | Values | Values |
| Vadose Zone | | |
| Vadose zone thickness (ft) | 9.68 | 28.5 |
| Capillary zone thickness (ft) | 0.164 | 0.5 |
| Depth to Groundwater (ft) | 9.844 | 29 |
| Affected Soils | | |
| Surficial soil depth (ft) | 3.28 | 12 |
| Depth to uppermost affected soil (ft) | 3.28 | 15 |
| Depth to base of affected soil (ft) | 9.844 | 30 |
| Contaminated soil area (sq. ft) | 2.420 | 2,420 |
| Length of affected soil parallel | 2,420 | 51750 |
| to assumed wind direction (ft) | 49.2 | 49.2 |
| Length of affected soil zone parallel | 49.2 | 40.2 |
| to groundwater flow direction (ft) | 49.2 | 49.2 |
| | | |
| Soil density (g/cu.cm) | 1.7 | 1.17 |
| Soil/Groundwater pH | 6.5 | 7 |
| Soil Parameters | | |
| Foc in vadose zone | 0.01 | 0.015 |
| Soil porosity | 0.38 | 0.46 |
| Volumetric Water Content | | |
| Capillary fringe | 0.342 | 0.29 |
| Vadose zone | 0.12 | 0.25 |
| Foundation crack | 0.12 | 0.16 |
| | 0.12 | 0.10 |
| Volumetric Air Content | . | |
| Capillary fringe | 0.038 | 0.17 |
| Vadose zone | 0.26 | 0.20 |
| Foundation crack | 0.26 | 0.3 |
| Groundwater | | |
| Gradient | | 0.004 NE |
| Saturated hydraulic conductivity | | 0.0007 cm/sec |
| Longitudinal dispersivity (ft) | | |
| Transverse dispersivity (ft) | | |
| Vertical dispersivity (ft) | | |
| Groundwater mixing zone depth (ft) | 6.56 | 12 |
| Water Infiltration rate (ft/yr) | 0.984 | 0.984 |
| GW Darcy velocity (ft/yr) | 82 | |
| GW transport velocity (ft/yr) | 216 | |
| Foc in water zone | 0.001 | 0.001 |
| Building Parameters | | |
| Building volume/area ratio (cm) | 300 | 300 |
| Building air exchange rate (1/s) | 0.00023 | 0.00023 |
| Foundation crack thickness (cm) | | - |
| Foundation crack inickness (cm) | 15 | 15 |
| ft = feet | 0.01 | 0.01 🗙 |
| | | |
| sq.ft = square feet | | |
| g/cu.cm = grams per cubic centimeter NE = northeast | | |
| cm/sec = centimeters per second | | |
| - | | |
| ft/yr = feet per year | | |

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Table 2 Groundwater Data Used to Calculate the Representative Concentrations

Risk-Based Corrective Action - Tier 2 Former Chevron Service Station 9-7127 Grant Line Road at Interstate 580 Tracy, California

| Monitoring | Sample | Benzene | Ethylbenzene | Toluene | Xylenes | |
|---------------|-----------------------|---------|--------------|---------|---------|--|
| Well | Date | (mg/L) | (mg/L) | (mg/L) | (mg/L) | |
| MW-1 | 11/15/95 | 15 | 1.1 | 9.6 | 5. | |
| | 02/27/96 | 0.048 | ND | 0.071 | 0.02 | |
| | 05/30/96 | 15 | 1.1 | 11 | 4. | |
| | 08/27/96 | 11 | 0.79 | 9.5 | 3. | |
| MW-3 | 11/15/95 | 8 | 0.43 | 2.9 | 1. | |
| | 02/27/96 | · 5 | 0.22 | 0,5 | 0.1 | |
| | 05/30/96 | 13 | 0.87 | 7.2 | 2. | |
| | 08/27/96 | 9.5 | 0.74 | 6.9 | 2 | |
| MW-4 | 11/15/95 | 0.094 | 0.00077 | 0.0094 | 0.004 | |
| | 02/27/96 | 0.1 | ND | 0.015 | 0.00 | |
| | 05/30/96 | 0.24 | 0.0006 | 0.004 | 0.003 | |
| | 08/27/96 | 0.011 | ND | ND | N | |
| MW-6 | 08/27/96 | 0.0016 | ND | ND | N | |
| | 05/30/96 | 0.0013 | ND | ND | 0.000 | |
| | 02/27/96 | 0.0011 | ND | ND | N | |
| ogtransformed | Mean = | 0.32 | 0.58* | 0.59 | 0.1 | |
| | ns per liter ected | | 0.58* | | | |

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Table 3 Soil Data Used to Calculate the Representative Concentrations

Risk-Based Corrective Action - Tier 2 Former Chevron Service Station 9-7127 Grant Line Road at Interstate 580 Tracy, California

| Sample | Sample | Sample Depth | Benzene | Ethylbenzene | Toluene | Xylenes |
|------------------|----------|--------------|---------|--------------|---------|---------|
| ID | Date | (feet, bgs) | (mg/kg) | (mg/kg) | (mg/kg) | (mg/kg) |
| B-2 | 12/01/87 | 20 | 0.001 | ND | ND | |
| B-3 | 12/01/87 | 14 | 1.2 | 0.8 | 0.68 | |
| B-4 | 12/01/87 | 15 | 19 | 28 | 85 | 14 |
| B-5 | 12/01/87 | 5 | 0.076 | 0.002 | 0.007 | 0.0 |
| B-7 | 12/01/87 | 5 | 0.022 | 0.024 | 0.003 | 0.04 |
| Af" | 04/04/91 | 14 | ND | 66 | 41 | 1 |
| Aop* | 04/04/91 | 14 | 0.007 | 0.005 | ND | 0.0 |
| Bf | 04/04/91 | 14 | 20 | 110 | 220 | 56 |
| Bop [*] | 04/04/91 | 14 | 0.007 | 0.012 | 0.016 | 0.0 |
| Cf | 04/04/91 | 13 | 0.018 | 0.014 | 0.013 | 0.04 |
| Copª | 04/04/91 | 15 | 30 | 60 | 180 | 35 |
| #5 ^b | 04/16/91 | 13 | ND | 1.7 | 0.8 | 1 |
| #8 [⊳] | 04/16/91 | 14 | 0.085 | 0.27 | 0.24 | 1 |
| #13 [⊳] | 04/16/91 | 15 | ND | 0.044 | 0.047 | 0.3 |
| #14 [⊳] | 04/16/91 | 13 | 0.005 | 0.03 | 0.006 | 0,1 |
| MW-1 | 12/08/92 | 19 | ND | ND | 0.0056 | 0.007 |
| | | 24 | ND | 30 | 79 | 20 |
| | | 29 | 21 | 150 | 560 | 84 |
| | | 38.5 | ND | ND | 0.013 | 0.02 |
| B-1 | 12/09/92 | 18 | ND | ND | 0.014 | 0.0 |
| | | 22 | ND | ND . | 0.013 | 0.01 |
| gtransforme | d Mean = | | 0.18 | 0.48 | 0.38 | 0. |

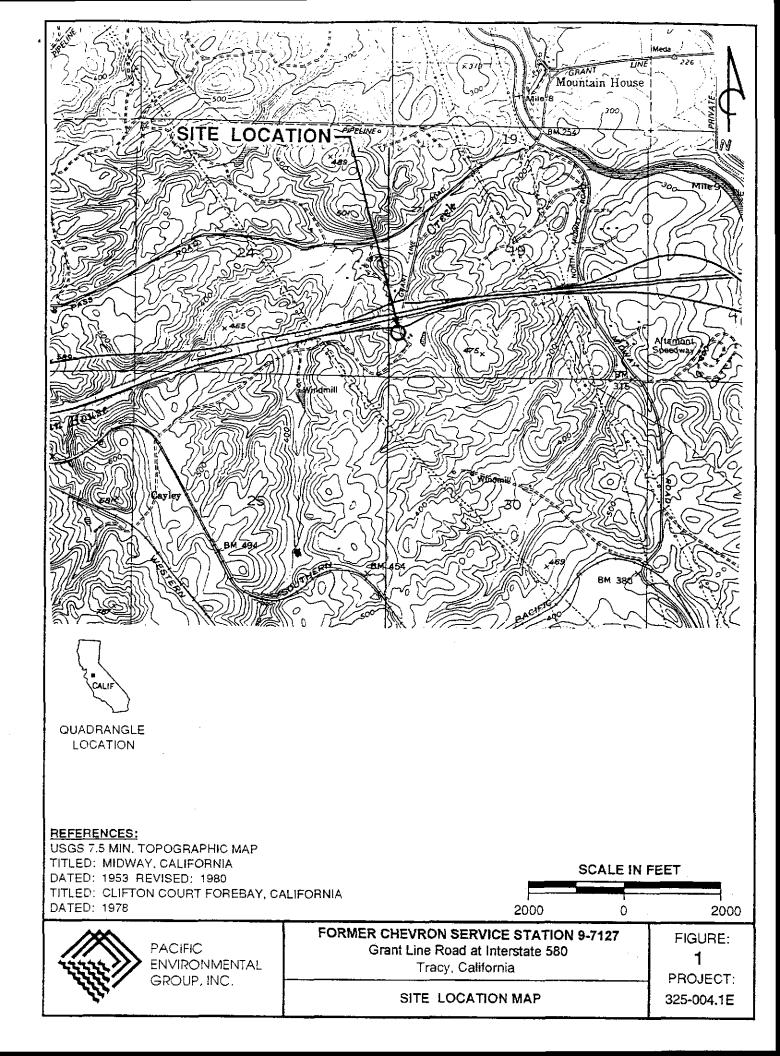
mg/kg = Milligram per kilogram

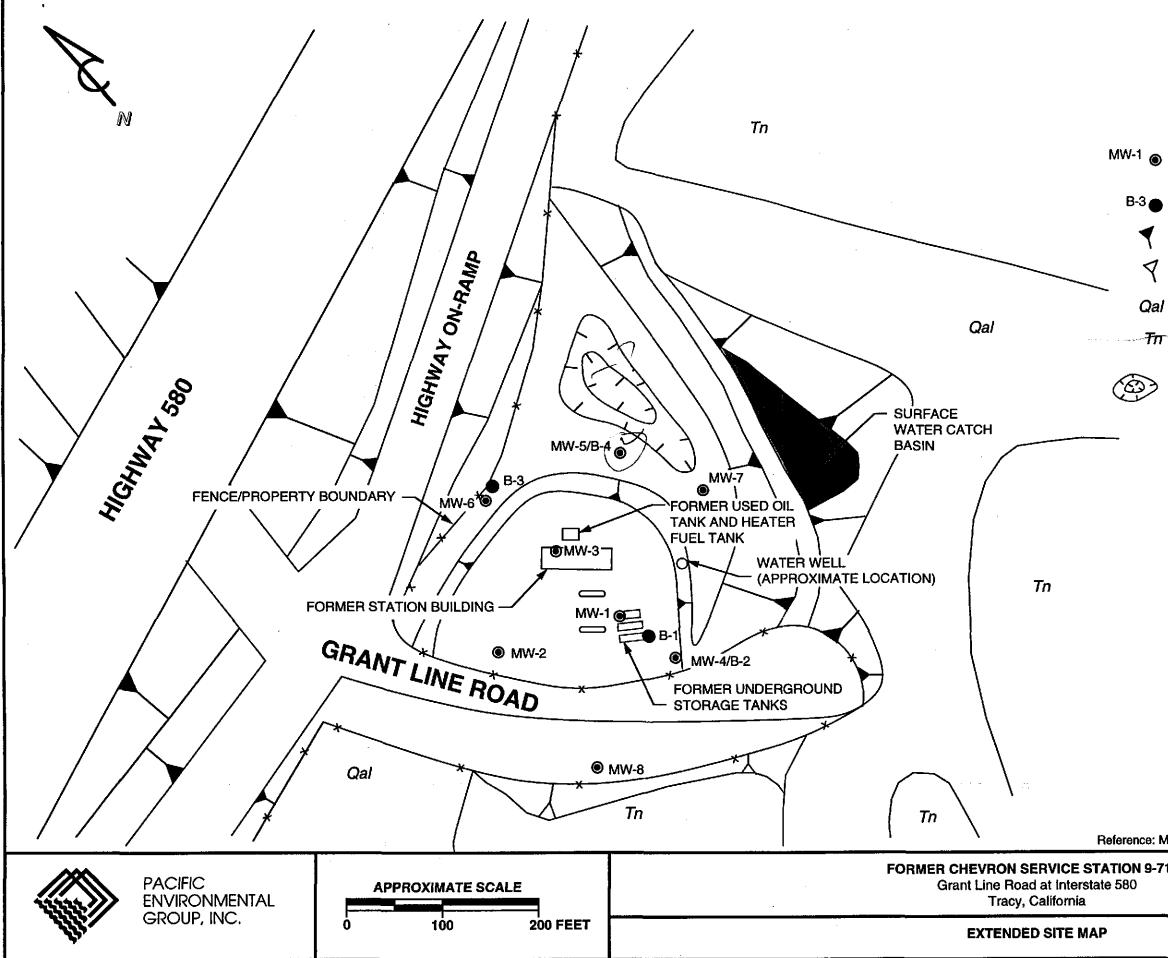
ND = Not detected

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a. Sidewall and interface samples were collected during the tank removal

b. Confirmation soil samples collected during the overexcavation of the tank removal.





LEGEND

MW-1
 GROUNDWATER MONITORING WELL LOCATION AND DESIGNATION

B-3 SOIL BORING LOCATION AND DESIGNATION

FILL SLOPE

CUT SLOPE

Qal ALLUVIUM INCLUDING SURFICIAL FILL

DEPRESSION

Reference: Map prepared from aerial photograph dated 1981 and well survey data.

| /127 | |
|------|------------|
| | FIGURE: |
| | 2 |
| | PROJECT: |
| | 325-004.1E |

ATTACHMENT A

LABORATORY SOIL TEST DATA

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COOPER TESTING LABORATORY

01012101298

1951 Colony, Unit X Mountain View, California 94043 Tel: 415 968-9472 FAX: 415 968-4228

LETTER OF TRANSMITTAL

TO:

Pacific Environmental Group 2025 Gateway Place, #440 San Jose, CA 95110 Attn: Ross Tinline

DATE: December 17, 1996

PROJECT: 325004.1E

CTL#: 226-010

ENCLOSED: Laboratory soil test data.

REMARKS:

Carl RC

COOPER TESTING LAB

Organic Content ASTM D2974

Cooper Testing Lab

| JOB NO.: 226-010 | | <u> </u> | | | |
|-------------------------------|--------|----------|-------|---------------------------------------|-----|
| CLIENT: Pacific Environmental | 1 | | DATE: | 12/10/96 | |
| PROJECT 325004.1E | | | BY: | DC | |
| BORING: | OC-1 | | | | |
| SAMPLE: | | | | | |
| DEPTH, ft.: | | | | | |
| SOIL CLASSIFICATION: | gray | | | | |
| (visual) | brown | | | | |
| | SAND- | | 1 | | |
| | STONE | | | [| |
| | | | | | |
| | | | | | |
| | | | | | |
| SOIL, ORGANICS & DISH, gm: | 182.29 | | | · · · · · · · · · · · · · · · · · · · | |
| SOIL & DISH, gm: | 180.78 | | | | |
| DISH, gm: | 78.95 | | | | |
| SOIL, gm: | 101.83 | · 0 | 0 | 0 | 0 |
| SOIL & ORGANICS, gm: | 103.34 | 0 | 0 | 0 | 0 |
| % ORGANICS: | 1.5 | ERR | ERR | ERR | ERR |

| | | | esting Lab | | ī | |
|---|---------------------------------|-----|--------------|----------------|-----|-----|
| Job#: 226-010 Client: Pacific E Project: 325004.1 | nvironmenta E | al | Date: By: | 12/11/96 DC | | |
| Boring: Sample: Depth, ft.: | OC-1 | | | | | |
| Soil Classification: (visual) | gray brown SAND- STONE | | | | | |
| Wt. of Pycnometer Soil & Water, gm: | 352.72 | | | | | |
| Temp. centigrade: | 17 | | | | | |
| Wt. of Pycnometer & Water, gm: | 316.31 | | | | | |
| Wt. Dry Soil, gm: | 56.84 | | | | | |
| Temp. Correction Factor: | 1 | | | | | |
| Specific Gravity: | 2.78 | ERR | EAR | ERA | ERR | ERA |

Remarks: The temperature correction factor is shown as 1 if the weight of the pycnometer is taken from the lab temperature correction curve.

Specific Gravity ASTM D-854

Falling Head Permeability ASTM D 5084 Cooper Testing Lab, Inc.

:

| Job No: | 226-010a | | Boring: | | | Date: | 12/11/96 | |
|--------------|-----------|------------|-------------|-------------------------|-------------|------------|-------------------------|--|
| Client: | Pacific E | | Sample: | OC-1 | | By: | DC | |
| Project: | 325004.1 | | Depth: | | | | | |
| Soil: | gray brov | vn SANDST | ONE | | | | | |
| Sample P | | _ | | | | Max. Hyd | raulic | |
| Cell: | 70 psi | _Bot. Cap: | 65 psi | Top Cap: | 65 psi | Gradient: | 6 | |
| Elapsed T | ime (min) | | Head, (cm |) 1) | Permeabil | itv cm/sec | | |
| 0 | | | 28.0 | · · · · · · · · · · · · | Start of Te | | ··· ··· ··· ··· ··· ··· | |
| 1 | | | 20.4 | | 6.8 x 10E- | - | | |
| 3 | | | 9.1 | | 8.1 x 10E-4 | | | |
| 5 | | | 5.0 | | 7.4 x 10E-4 | | | |
| 0 | | | 28.0 | | | • | | |
| 2 | | | 13.0 | | 8.3 x 10E-4 | 1 · | | |
| 8 | | | 2.8 | | 6.2 x 10E-4 | | | |
| 0 | | | 28.0 | | | • | | |
| 4 | | | 8.1 | | 6.7 x 10E-4 | ţ | | |
| | | Average Pe | ermeability | : | 7 x 10E-4 | | cm/sec | |
| Sample Da | | | Initial | | | Final | | |
| Height, in.: | | | 2.00 | | | 1.95 | | |
| Diameter, i | n.: . | 5 | 1.90 | | | 1.86 | | |
| Area, in2: | | | 2.84 | | | 2.72 | | |
| Volume, in: | | | 5.67 | | | 5.30 | | |
| Total Volun | | | 92.92 | | | 86.83 | | |
| /ol of Solic | | | 50.29 | | | 50.29 | - | |
| /ol. of Voic | | | 42.64 | \sim | | 36.54 | | |
| /oid Ratio: | 1 | | 0.85 | (0)) | | 0.73 | | |
| Porosity, % | | | 45.88 | 160) | | 42.08 | | |
| Saturation, | | | 54.88 | $\sum /$ | | 95.24 | | |
| p. Gravity | | | 2.78 | \sim | | 2.78 | | |
| Vet Weight | | | 163.2 | | | 174.6 | · · · | |
| y Weight, | gm: | | 139.8 | | - | 139.8 | | |
| are, gm: | | | 0.00 | • | | 0.00 | | |
| loisture, % | | | 16.7 | | | 24.9. | | |
| ry Density | . pcf: | | 93.9 | j | | 100.5 | | |

ATTACHMENT B

HISTORICAL GROUNDWATER DATA



FET 14 MDZ

February 12, 1997

Ms. Eva Chu Alameda County Health Care Services Department of Environmental Health 1131 Harbor Bay Parkway, Suite 250 Alameda, CA 94502-6577

Re: Former Chevron Service Station #9-7127 Interstate 580 and Grantline Road near Tracy, California

Dear Ms. Chu:

Enclosed is the Fourth Quarter Groundwater Monitoring report for 1996, prepared by our consultant Gettler-Ryan Inc. for the above noted facility. Ground water samples were analyzed for TPH-g, BTEX and MtBE constituents.

Constituents detected in the wells were similar as in previous sampling events. Samples were not taken from monitoring wells MW-2, MW-5, MW-7 and MW-8 to comply with the new sampling program. These wells will be sampled annually starting in May 1997. The remaining wells will be sampled semi-annually starting in November 1996. The water well (supply well) will be sampled annually starting in November 1996.

Groundwater depth varied from 11.61 to 28.98 feet below grade with a direction of flow to the northeast. Groundwater levels were taken each month and the gradient and direction of flow was similar as to the quarterly sampling events. The existing water well (supply well) was sampled this quarter and all constituents were below method detection limits.

Chevron will continue to sample the wells based on the sampling program noted above. If you have any questions or comments call me at (510) 842-9136.

Sincerely, CHEVRON PRODUCTS COMPANY

Philip R. Briggs

Site Assessment and Remediation Project Manager

Enclosure

Chevron Products Company 6001 Bollinger Canyon Road Building L San Ramon, CA 94583 P.D. Box 6004 San Ramon, CA 94583-0904

Marketing – Sales West Phone 510 842-9500 Ms. Eva Chu Former Chevron Service Station # 9-7127 February 12, 1997 Page 2

cc. Ms. Bette Owen, Chevron

Mr. John Moody RWQCB-Central Valley Region 3443 Routier Road Sacramento, CA 95827-3098

Mr. Ardavan Onsori 29310 Union City Blvd. Union City, CA 94587

Mr. & Mrs. Joe Jess Jess Ranch Route 5, Box 704-A Tracy, CA 95376

Mr. Ross Tinline Pacific Environmental Group 2025 Gateway Place, Suite 440 San Jose, CA 95110 (less analytical data)



December 16, 1996

Job #5251.80

Mr. Phil Briggs Chevron Products Company P.O. Box 5004 San Ramon, CA 94583

Re: Fourth Quarter Groundwater Monitoring & Sampling Report Former Chevron Service Station #9-7127 Interstate 580 and Grant Line Road Tracy, California

Dear Mr. Briggs:

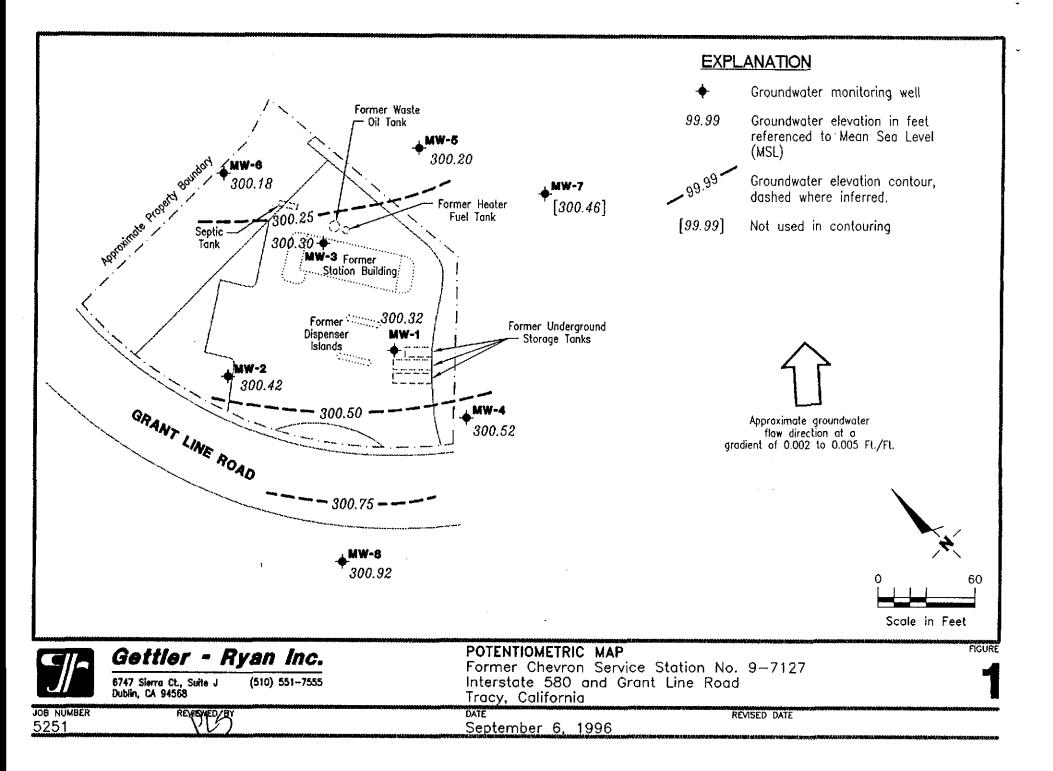
This report documents the monthly monitoring and quarterly groundwater sampling event performed by Gettler-Ryan Inc. (G-R). On November 11, 1996, field personnel were on-site to monitor eight wells (MW-1 through MW-8) and sample four wells (MW-1, MW-3, MW-4, and MW-6) and a supply well, at the Former Chevron Service Station #9-7127 located at Interstate 580 and Grant Line Road in Tracy, California.

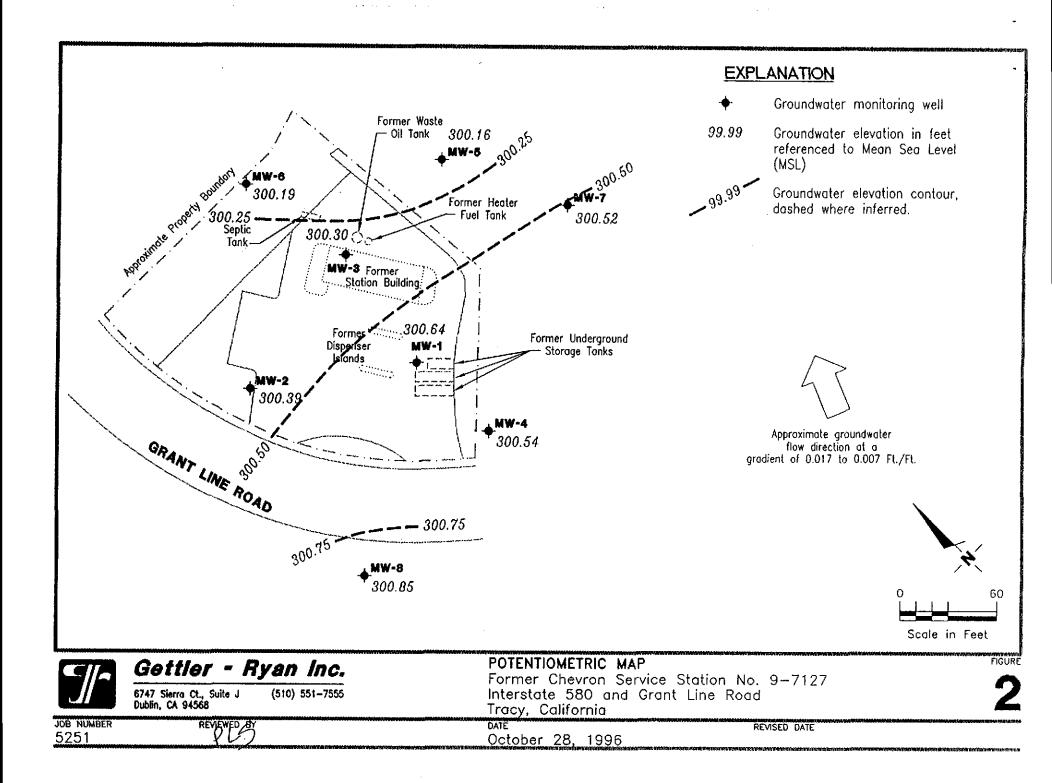
Static groundwater levels were measured on September 6, October 28, and November 11, 1996. All wells were checked for the presence of separate-phase hydrocarbons. Separate-phase hydrocarbons were not present in any of the wells. Static water level data and groundwater elevations are presented in Table 1. Potentiometric maps are included as Figures 1, 2 and 3.

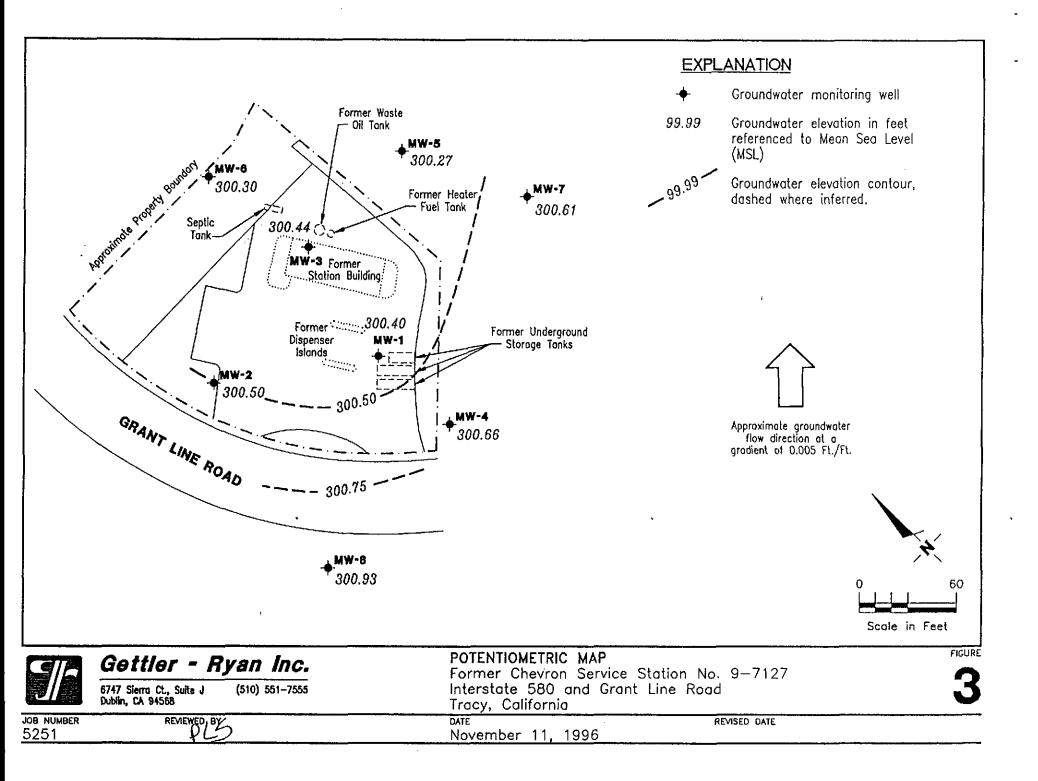
Groundwater samples were collected from the monitoring wells as specified by G-R Standard Operating Procedure -Groundwater Sampling (attached). The field data sheets are also attached. The samples were analyzed by NEI/GTEL Environmental Laboratories, Inc. Analytical results are presented in Table 1. The chain of custody document and laboratory analytical reports are attached.

Thank you for allowing Gettler-Ryan Inc. to provide environmental services to Chevron. Please call if you have any questions or comments regarding this report.

Sincerely, OED GEO Deanna L. Harding Project Coordinator Penny L. Silzer lo. 5523 'ennv Geologist, R.G. No. 5523 Senior DLH/PLS/dlh 5251.QML Figure 1: Potentiometric Map - September 6, 1996 Figure 2: Potentiometric Map - October 28, 1996 Figure 3: Potentiometric Map - November 11, 1996 Table 1: Water Level Data and Groundwater Analytical Results Attachments: Standard Operating Procedure - Groundwater Sampling Field Data Sheets Chain of Custody Document and Laboratory Analytical Reports 6747 Sierra Court, Suite J Dublin, California 94568 (510) 551-7555









| Well ID/ | | DTW | OWE | Product | | - | | _ | | |
|----------|----------|-------------|---------------------|-------------------|--|-----------|--------|---------|---|--------|
| TOC (ft) | Date | (ft) | GWE (msl) | Thickness (ft) | TPH(G) < | В | Т | E | x | MTBE |
| | | (19 | (11131) | (1) | | | | ppb | | > |
| MW-1/ | | | | | | | | а. С | | |
| 329.17 | 2/15/94 | 29.77 | 299,40 | 0 | 99,000 | 20,000 | 24,000 | 2,000 | 9,800 | |
| | 4/21/94 | 29.85 | 299.32 | 0 | <u> </u> | | | | ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | |
| | 6/1/94 | 29.92 | 299.25 | 0 | 56,000 | 12,000 | 15,000 | 1,100 | 5,800 | |
| | 6/28/94 | 30.15 | 299.02 | 0 | | | | | | |
| | 7/19/94 | 20.30 | 308.87 | õ | | | | | | |
| | 9/2/94 | 30.61 | 298.96 ¹ | 0.5 | | | | | | |
| | 9/12/94 | 31.66 | 298.04 | 0.66 | <u> </u> | | | | | |
| | 10/12/94 | 31.70 | 298.70 ¹ | 1.54 | | | | | | |
| | 11/30/94 | 29.95 | 299.84 ¹ | 0.77 | <u>. </u> | _ | | | | |
| | 3/9/95 | 29.54 | 299.88 | 0.31 | | <u></u> | | *** | | |
| | 4/18/95 | 29.01 | 300.16 | 0 | | | | | | |
| | 5/17/95 | 29.09 | 300.08 | 0 | 130,000 | 22,000 | 30,000 | 2,000 | 10,000 | |
| | 6/7/95 | 29.24 | 299.93 | ŏ | | | | 2,000 | | |
| | 7/21/95 | 29.66 | 299.51 | Ō | | | | | | |
| | 8/15/95 | 29.87 | 299.30 | ŏ | 41,000 | 9,400 | 12,000 | 1,400 | 7,700 | |
| | 9/7/95 | 29.85 | 299.32 | ŏ | | | | | 7,700 | |
| | 10/9/95 | 30.01 | 299.16 | Ō | _ | | | | | |
| | 11/15/95 | 29.88 | 299.29 | Ō | 68,000 | 15,000 | 9,600 | 1,100 | 5,500 | <2,000 |
| | 12/30/95 | 29.99 | 299.18 | Ō | | | | | 5,500 | ~2,000 |
| | 1/29/96 | 29.32 | 299.85 | Sheen | | | | | | |
| | 2/27/96 | 28.51 | 300.66 | 0 | 520 | 48 | 71 | <0,5 | 27 | 28 |
| | 3/5/96 | 28.44 | 300.73 | Ō | | | | | | 20 |
| | 4/23/96 | 28.20 | 300.97 | Ō | B | A-7* | | | | |
| | 5/30/96 | 28.47 | 300.70 | 0 | 57,000 | 15,000 | 11,000 | 1,100 | 4,900 | <250 |
| | 6/19/96 | 28.43 | 300.74 | ō | | | | | 4,500 | ~250 |
| | 7/15/96 | 28.66 | 300,51 | Sheen | | | | | | |
| | 8/27/96 | 28.73 | 300.44 | 0 | 74,000 | 11,000 | 9,500 | 790 | 3,600 | <120 |
| | 9/9/96 | 28.85 | 300.32 | 0 | | | | | 3,000 | ~120 |
| | 10/28/96 | 28.53 | 300.64 | Sheen | | <u> </u> | *** | | | |
| | 11/11/96 | 28.77 | 300.40 | 0 | 69,000 | 13,000 | 9,100 | 810 | 3,200 | <250 |
| | | | | v | 07,000 | 101000 | 7,100 | 010 | J 20 0 | ×230 |
| /W-2/ | | | | | | | | | | |
| 27.22 | 2/15/94 | 27.09 | 300.13 | 0 | 83 | 21 | 6 | 1 | 3 | |
| | 4/21/94 | 27.81 | 299.41 | Õ | | <u>21</u> | | 1 | | |
| | 6/1/94 | 27.98 | 299.24 | 0 | <50 | 1.3 | 0.5 | ~~~ | | |
| | 6/28/94 | 28.17 | 299.05 | ŏ | | | | <0.5 | <0.5 | |
| | 7/19/94 | 28.35 | 299.05 | 0 | | | | | | |
| | 9/2/94 | 28.52 | 298.70 | 0 | 82 | 13 | | 26 | 1.4 | |
| | | A179 1.5 A1 | 270.10 | v | 04 | 15 | 16 | 3.6 | 14 | |

1

| Well ID/ | | Th/201 27 | | Product | | | | | | |
|----------|----------|-----------|--------|----------------|------------|-----------|---------|-------------|-------|----------|
| TOC (ft) | Date | DTW | GWE | Thickness | TPH(G) | В | т | E | x | MTBE |
| 100 (11) | Late | (ft) | (msl) | (ft) | <> | | | ppb | | > |
| MW-2 | 9/12/94 | 28.56 | 298.66 | 0 | | | | | | |
| (cont) | 10/12/94 | 28.62 | 298.60 | 0 | | | | | | |
| . , | 11/30/94 | 28,38 | 298.84 | 0 | <50 | | | | | |
| | 3/9/95 | 27.41 | 299.81 | 0 | | 3.6 | 4,5 | 1.0 | 4.5 | |
| | 4/18/95 | 26.79 | 300.43 | 0 | | | | | | |
| | 5/17/95 | 26.95 | 300.27 | 0 | <50 | < 0.5 | | | | |
| | 6/7/95 | 27.06 | 300.16 | õ | <u> </u> | < 0.5 | < 0.5 | <0.5 | <0.5 | |
| | 7/21/95 | 27.47 | 299.75 | õ | | | | | | |
| | 8/15/95 | 27.57 | 299.65 | õ | <50 | < 0.5 | | | | |
| | 9/7/95 | 28.69 | 298.53 | ŏ | | | <0.5 | < 0.5 | < 0.5 | |
| | 10/9/95 | 27.85 | 299.37 | ŏ | | - | | | | |
| | 11/15/95 | 27.91 | 299.31 | ŏ | <50 | < 0.50 | < 0.50 | ~~ <0.50 | | |
| | 12/30/95 | 27.60 | 299.62 | õ | ~~~ | <0.50 | | < 0.50 | <0.50 | <5.0 |
| | 1/29/96 | 27.16 | 300.06 | ŏ | | | | - | | |
| | 2/27/96 | 26.25 | 300.97 | õ | < 50 | < 0.5 | <0,5 | < 0.5 | <0.5 | |
| | 3/5/96 | 26.70 | 300.52 | ō | _ | | ~0,5 | | | <5.0 |
| | 4/23/96 | 25.82 | 301.40 | ō | | | | | | |
| | 5/30/96 | 26.16 | 301.05 | õ | <50 | < 0.5 | < 0.5 | < 0.5 | | |
| | 6/19/96 | 26.27 | 300.95 | ō | | | | | <0.5 | < 5.0 |
| | 7/15/96 | 26.46 | 300.76 | õ | | | | | | |
| | 8/27/96 | 26.72 | 300.50 | õ | <50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | <5.0 |
| | 9/6/96 | 26.80 | 300.42 | Ŏ | | | | | | |
| | 10/28/96 | 26.83 | 300.39 | õ | | | | | | |
| | 11/11/96 | 26.72 | 300.50 | ŏ | 8 to | | | | | |
| | | | | | | | | | | |
| MW-3/ | | | | | | | | | | |
| 329.28 | 2/15/94 | 29.87 | 299.41 | 0 [°] | 23,000 | 11.000 | | e 10 | | |
| | 4/21/94 | 29.96 | 299.32 | ŏ | | 11,000 | 1,700 | 540 | 1,000 | |
| | 6/1/94 | 30.11 | 299.17 | ŏ | 27 000 | 12 000 | | | | |
| | 6/28/94 | 30.31 | 298.97 | õ | 27,000 | 12,000 | 2,600 | 600 | 2,200 | |
| | 7/19/94 | 30.50 | 298.78 | 0 | *== | | | | | |
| | 9/2/94 | 30.61 | 298.67 | 0 | 34,000 | 16 000 | 4 100 | | | |
| | 9/12/94 | 30.65 | 298,63 | ŏ | - | 16,000 | 4,100 | 770 | 3,000 | |
| | 10/12/94 | 1 30.74 | 298.54 | ő | · | | | | | |
| | 11/30/94 | 30.44 | 298.84 | 0 | 33,000 | 16,000 | 1 000 | | 2 400 | |
| | 3/9/95 | 29.53 | 299.75 | 0 | | | 3,000 | 740 | 2,400 | |
| | 4/18/95 | 28.97 | 300.31 | 0 | | **** | | | | |
| | 5/17/95 | 29.19 | 300.09 | 0 | 27,000 - | 10,000 | 760 | | | |
| | 6/7/95 | 29.24 | 300.04 | 0 | 27,000 | | | 490 | 1,000 | |
| | | | 500.01 | v | | | | | | |

 Table 1.
 Water Level Data and Groundwater Analytical Results - Former Chevron Service Station #9-7127, Interstate 580 at Grant Line Road, Tracy, California (continued)



| WALL 1157 | | | | Product | | | | | | |
|----------------------|----------|-------|--------|-----------|---------------------|--------|--|-------|-------|------------|
| Well ID/ TOC (ft) | Date | DTW | GWE | Thickness | TPH(G) | В | Т | E | x | MTBE |
| 100 (ll) | Date | (ft) | (msl) | (ft) | < | | ······································ | ppb | | > |
| MW-3 | 7/21/95 | 29.70 | 299.58 | 0 | | | | | | |
| (cont) | 8/15/95 | 29.78 | 299.50 | ŏ | 39,000 ³ | 13,000 | 2,900 | 700 | 1,700 | |
| | 9/7/95 | 29.86 | 299.42 | ŏ | | | | | | |
| | 10/9/95 | 30.02 | 299.26 | ŏ | | | | | | _ |
| | 11/15/95 | 30.06 | 299.22 | ŏ | 21,000 | 8,000 | 2,900 | 430 | 1,500 | <1,000 |
| | 12/30/95 | 29.75 | 299.53 | ŏ | | | 2,700 | | 1,500 | |
| | 1/29/96 | 29.22 | 300.06 | ŏ | | | | | | |
| | 2/27/96 | 28.43 | 300.85 | ŏ | <2,500 | 5,000 | 500 | 220 | 130 | 710 |
| | 3/5/96 | 28.35 | 300.93 | ŏ | | | 500 | | | |
| | 4/23/96 | 28.10 | 301.18 | ŏ | | _ | | _ | | |
| | 5/30/96 | 28.42 | 300.86 | ŏ | 37,000 | 13,000 | 7,200 | 870 | 2,900 | <120 |
| | 6/19/96 | 28.51 | 300.77 | õ | | | | _ | 2,500 | |
| | 7/15/96 | 28.63 | 300.65 | õ | | | | | | |
| | 8/27/96 | 28.90 | 300.38 | Ō | 50,000 | 9,500 | 6,900 | 740 | 2,900 | <120 |
| | 9/6/96 | 28.98 | 300.30 | Ö | | | | | | |
| | 10/28/96 | 28.98 | 300.30 | Ó | | | | | *** | |
| | 11/11/96 | 28.84 | 300.44 | 0 | 52,000 | 11,000 | 5,500 | 780 | 3,000 | <250 |
| | | | | | | | , | | , | |
| MW-4/ | 5/21/93 | | | | <50 | 12 | 2 | < 0.5 | 1 | |
| | 11/5/93 | | | | 300 | 56 | 10 | 0.8 | 3 | |
| 329.44 | 2/15/94 | 29.90 | 299.54 | 0 | 260 | 47 | 12 | 2 | 4 | |
| | 4/21/94 | 29.99 | 299.45 | õ | | | | | | |
| | 6/1/94 | 30.14 | 299.30 | ō | 860 | 200 | 23 | 2.8 | 9.6 | |
| | 6/28/94 | 30.32 | 299.12 | ò | | | | | | |
| | 7/19/94 | 30.50 | 298.94 | 0 | | | | | | |
| | 9/2/94 | 30.62 | 298.82 | 0 | 1,700 | 250 | 27 | 6.4 | 15 | |
| | 9/12/94 | 30.69 | 298.75 | 0 | *** | | | | | |
| | 10/12/94 | 30.75 | 298.69 | 0 | | | | | | |
| | 11/30/94 | 30.51 | 298.93 | 0 | 830 | 350 | 29 | 8.1 | 22 | |
| | 3/9/95 | 29.61 | 299.83 | 0 | | | | | | |
| | 4/18/95 | 29.08 | 300.36 | 0 | | | | | | |
| | 5/17/95 | 29.22 | 300.22 | 0 | 470 | 200 | 2.2 | 0.9 | 2.1 | |
| | 6/7/95 | 29.27 | 300.17 | 0 | | | | *** | | |
| | 7/21/95 | 29.72 | 299.72 | 0 | | | | | | |
| | 8/15/95 | 29.77 | 299.67 | 0 | 100 | 4.2 | 0.8 | < 0.5 | < 0.5 | |
| | 9/7/95 | 29.85 | 299.59 | 0 | | | | | | |
| | 10/9/95 | 30.02 | 299.42 | 0 | | | | | | |
| | 11/15/95 | 30.05 | 299.39 | 0 | 270 | 94 | 9.4 | 0.77 | 4.3 | 27 |
| | 12/30/95 | 29.79 | 299.65 | 0 | | | | | | |



| Well ID/ | | DTW | GWE | Product | A 11111 (| - | | | | |
|----------|----------|---------|--------|-------------------|------------------|--------------------|-----------|--------|--------------------|----------|
| TOC (ft) | Date | (ft) | (msi) | Thickness (ft) | TPH(G) < | В | r | E | x | MTBE |
| | | | (1131) | (11) | | | | -ppb | | > |
| MW-4 | 1/29/96 | 29.31 | 300.13 | 0 | | | | | | |
| (cont) | 2/27/96 | 28.58 | 300.86 | 0 | 690 | | | | <u></u> | |
| | 3/5/96 | 28.55 | 300.89 | õ | | 100 | 15 | <0.5 | 2.0 | 79 |
| | 4/23/96 | 28.15 | 301.29 | ŏ | | | - | | | _ |
| | 5/30/96 | 28.40 | 301.04 | 0 0 | | | | | *** | — |
| | 6/19/96 | 28.47 | 300.97 | 0 | 700 | 240 | 4.0 | 0.6 | 3.9 | <5.0 |
| | 7/15/96 | 28.62 | 300.82 | ů | | — | | | | P |
| | 8/27/96 | 28.85 | 300.59 | Ö | | | | | | |
| | 9/6/96 | 28.92 | 300.52 | Ő | <50 | 11 | < 0.5 | < 0.5 | < 0.5 | <5.0 |
| | 10/28/96 | 28.90 | 300.54 | 0 | | | | | | |
| | 11/11/96 | 28.78 | 300.66 | 0 | | | | | | — |
| | | 20170 | 500.00 | V . | 240 | 57 | 1,4 | 0.7 | 1.8 | <5.0 |
| MW-5 | 5/25/93 | | | | | | | | | |
| | 11/5/93 | | | | <50 | < 0.5 | < 0.5 | < 0.5 | 0.9 | |
| 312.88 | 2/15/94 | | | | <50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | |
| 12.00 | | 25.10 | 287.78 | 0 | <50 | < 0.5 | 1 | < 0.5 | 1 | |
| | 4/21/94 | 13.21 | 299.67 | 0 | | | -+- | | | |
| | 6/1/94 | 13.39 | 299.49 | 0 | <50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | _ |
| | 6/28/94 | 13.73 | 299.15 | 0 | | - | | | | |
| | 7/19/94 | 13.80 | 299.08 | 0 | | | | | *** | _ |
| | 9/2/94 | 14.02 | 298.86 | 0 | <50 | 3.2 | 1.8 | < 0.5 | 2.1 | |
| | 9/12/94 | 14.03 | 298.85 | 0 | | | | | | |
| | 10/12/94 | 14.15 | 298.73 | 0 | | <u> </u> | | | | _ |
| | 11/30/94 | 13.91 | 298.97 | 0 | <50² | < 0.5 ² | < 0.52 | <0.5² | < 0.5 ² | |
| | 3/9/95 | 12.97 | 299.91 | 0 | | | | | | _ |
| | 4/18/95 | 12.48 | 300.40 | 0 | | _ | | | | _ |
| | 5/17/95 | 12.71 | 300.17 | 0 | 150 | 1.0 | < 0.5 | < 0.5 | < 0.5 | _ |
| | 6/7/95 | 12.85 | 300.03 | 0 | | | | | ~~ | _ |
| | 7/21/95 | 13.30 | 299.58 | 0 | | | | | _ | |
| | 8/15/95 | 13,41 | 299.47 | 0 | <50 | < 0.5 | < 0.5 | <0.5 | < 0.5 | |
| | 9/7/95 | 13.42 | 299.46 | 0 | | | | | ~0.5 | |
| | 10/9/95 | 13.61 | 299.27 | 0 | | | | | | |
| | 11/15/95 | 13.63 | 299.25 | 0 | <50 | < 0.50 | < 0.50 | < 0.50 | < 0.50 | <5.0 |
| | 12/30/95 | 13.30 | 299.58 | 0 | | | | ~0.50 | | |
| | 1/29/96 | 12.75 | 300.13 | 0 | | | | | | |
| | 2/27/96 | 12.02 | 300.86 | Ō | < 50 | < 0.5 | < 0.5 | < 0.5 | | |
| | 3/5/96 | , 11.96 | 300.92 | Ö | | | <0.5 — | | <0.5 | < 5.0 |
| | 4/23/96 | 11.77 | 301.11 | Ō | | | | _ | | |
| | 5/30/96 | 12.17 | 300.71 | Ō | <50 | < 0.5 | < 0.5 | < 0.5 | <0.5 | |
| | 6/19/96 | 12.25 | 300.63 | ō | | ~0.5 | < 0.5 | < 0.5 | <0.3 | <5.0 |

4



| Well ID/ | | TYPE I | | Product | | | | | | |
|----------|--|--------|--------|-----------|--------|-------|-------|-------|-------|-------|
| TOC (ft) | Date | DTW | GWE | Thickness | TPH(G) | В | Т | E | x | MTBE |
| | Date (ft) (msl) (ft) <ppb< th=""><th>ррь</th><th></th><th>></th></ppb<> | | | | | | | ррь | | > |
| MW-5 | 7/15/96 | 12.39 | 300.49 | 0 | | | | | | |
| (cont) | 8/27/96 | 12.65 | 300.23 | ŏ | <50 | < 0.5 | < 0.5 | <0.5 | | |
| | 9/6/96 | 12.68 | 300.20 | Ő | | | | <0.5 | <0.5 | <5.0 |
| | 10/28/96 | 12.72 | 300.16 | õ | | | | | | |
| | 11/11/96 | 12.61 | 300.27 | Ő | | | | | | |
| | 11/11/70 | 19.01 | 300.#/ | v | | | | | | |
| MW-6 | | | | | | | | | | |
| 312.20 | 12/30/95 | 13.65 | 298.55 | 0 | *** | | | | | |
| | 1/29/96 | 12.18 | 300.02 | 0 | | | | | | |
| | 2/27/96 | 11.45 | 300.75 | 0 | 70 | 1.1 | < 0.5 | < 0.5 | < 0.5 | < 5.0 |
| | 3/5/96 | 11.32 | 300.88 | 0 | | | - | | | |
| | 4/23/96 | 11.12 | 301.08 | 0 | | | _ | | _ | |
| | 5/30/96 | 11.45 | 300.75 | Ō | 60 | 1.3 | < 0.5 | <0.5 | 0.9 | < 5.0 |
| | 6/19/96 | 11.54 | 300.66 | 0 | | | | | | |
| | 7/15/96 | 11.76 | 300.44 | 0 | · | | | | | |
| | 8/27/96 | 11.95 | 300.25 | 0 | 90 | 1.6 | < 0.5 | < 0.5 | < 0.5 | < 5.0 |
| | 9/6/96 | 12.02 | 300.18 | 0 | | | | | | |
| | 10/28/96 | 12.01 | 300.19 | 0 | | | | | | |
| | 11/11/96 | 11.90 | 300.30 | 0 | 1104 | <0.5 | < 0.5 | <0.5 | < 0.5 | <5.0 |
| MW-7 | | | | | | | | | | |
| 313.36 | 12/30/95 | 12.38 | 300.98 | 0 | | | | | | |
| | 1/29/96 | 13.14 | 300.22 | õ | | | | | *** | |
| | 2/27/96 | 12.34 | 301.02 | ŏ | <50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | <5.0 |
| | 3/5/96 | 12.35 | 301.01 | ŏ | ~~~ | | ~0.5 | | ~0.5 | |
| | 4/23/96 | 12.13 | 301.23 | ŏ | | | | | | |
| | 5/30/96 | 12.42 | 300.94 | õ | <50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 5.0 |
| | 6/19/96 | 12.57 | 300.79 | ŏ | | | | ~~ | | |
| | 7/15/96 | 12.70 | 300.66 | Ő | | | | | | |
| | 8/27/96 | 12.85 | 300.51 | ŏ | < 50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | <5.0 |
| | 9/6/96 | 12.90 | 300.46 | Õ | | | | | | |
| | 10/28/96 | 12.84 | 300.52 | ŏ | | | | | | |
| | 11/11/96 | 12.75 | 300.61 | ŏ | | | | | | |



| Well ID/ | | DTW | GWE | Product | TRUAN | | _ | | | |
|--------------|----------|-------|----------|-------------------|-------------|--------|--------|-------------|--------|-----------|
| TOC (ft) | Date | (ft) | (mai) | Thickness (ft) | TPH(G) < | В | Т | E | x | MTBE |
| | | | ((((a))) | (11) | | | | ppb | | > |
| MW-8 | | | | | | | | | | |
| 329.91 | 12/30/95 | 30.30 | 299.61 | 0 | | | | | | |
| | 1/29/96 | 29.56 | 300.35 | 0 | *== | | | _ | | |
| | 2/27/96 | 28.68 | 301.23 | 0 | <50 | < 0.5 | < 0.5 | < 0.5 | <5.0 | <5.0 |
| | 3/5/96 | 28.75 | 301.16 | 0 | | | | | | < <u></u> |
| | 4/23/96 | 28.25 | 301.66 | Ō | | | | | | |
| | 5/30/96 | 28.44 | 301.47 | Ó | < 50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 5.0 |
| | 6/19/96 | 28.51 | 301.40 | 0 | | | | | | |
| | 7/15/96 | 28.67 | 301.24 | 0 | | | | | | |
| | 8/27/96 | 28.92 | 300.99 | 0 | <50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 5.0 |
| | 9/6/96 | 28.99 | 300.92 | 0 | | | | | | ~ |
| | 10/28/96 | 29.06 | 300.85 | 0 | | | | <u>+</u> | | |
| | 11/11/96 | 28.98 | 300.93 | 0 | | | | | | |
| | | | | | | | | | | |
| Supply Well | 11/15/95 | | | | ~ 60 | -0.50 | | -0.50 | | |
| | 11/11/96 | | | *** | < 50 | < 0.50 | < 0.50 | < 0.50 | < 0.50 | < 5.0 |
| | 11/11/30 | | | | <50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | <5.0 |
| frip Blank | | | | | | | | | | |
| TB-LB | 2/15/94 | | | | ~ 80 | 10 F | 10.5 | | | |
| | 6/1/94 | | | | < 50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | |
| | 9/2/94 | | | <u> </u> | <50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | |
| | 11/30/94 | | | | < 50 | < 0.5 | < 0.5 | < 0.5 | <0.5 | |
| | 5/17/95 | | | - | < 50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | |
| | 8/15/95 | | | | <50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | |
| | 11/15/95 | | | | <50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | |
| | 2/27/96 | | * | | <50 | < 0.50 | < 0.50 | < 0.50 | < 0.50 | < 5.0 |
| | 5/30/96 | | | | < 50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | <5.0 |
| | | | | | < 50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | < 5.0 |
| | 8/27/96 | | | | < 50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | <5.0 |
| | 11/11/96 | | | | <50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | <5.0 |
| Bailer Blank | | | | | | | | | | |
| BB | 2/15/94 | | | | < 50 | < 0.5 | < 0.5 | < 0.5 | < 0.5 | |



EXPLANATION:

TOC = Top of casing elevation (ft) = feet DTW = Depth to water GWE = Groundwater elevation mal = Measurements referenced relative to mean sea level TPH(G) = Total Purgeable Petroleum Hydrocarbons as Gasoline B = Benzene T = Toluene E = Ethylbenzene X = Xylenes MTBE = Methyl-tertiary-butyl ether ppb = Parts per billion --- = Not analyzed/Not applicable

ANALYTICAL METHODS:

TPH(G) = EPA Method 8015/5030BTEX = EPA Method 8020 MTBE = EPA Method 8020

5251.tqm

NOTES:

All top of casing elevations were surveyed by Tronoff Land Surveying, Davis, California on November 2, 1993.

Water level elevation data and laboratory analytical results prior to May 17, 1995, were compiled from Quarterly Monitoring Reports prepared for Chevron by Sierra Environmental Services.

- GWE corrected for the presence of free-phase hydrocarbons using: GWE = [(TOC-DTW) + (0.8)(Product Thickness)]. 0.8 is the assumed specific gravity of free-phase hydrocarbons.
 Fetimated concentration. TET summate measured dependent of assumed assumed specific.
 - Estimated concentration. TFT surrogate recovery demonstrated sample specific matrix effect. Benzene and Toluene are estimated values due to low recovery of (TFT) surrogate. The (BFB) surrogate had acceptable recovery. Low surrogate recovery can be attributed to sample effervescence (GTEL).
- Laboratory reported data obtained from multiple dilutions. Dilution factor noted represents the dilution used for majority of results.
 - Laboratory report indicates hydrocarbons in the gasoline range do not match the gasoline standard pattern.



March 17, 1997

Job #5251.80

Mr. Phil Briggs Chevron Products Company P.O. Box 5004 San Ramon, CA 94583

Re: Former Chevron Service Station #9-7127 Interstate 580 and Grant Line Road Tracy, California

Dear Mr. Briggs:

The letter documents the site visit performed by Gettler-Ryan Inc. On February 19, 1997, field personnel were on site to obtain a grab sample from the "supply well" at the above referenced site. The grab sample was analyzed for California Drinking Water Standards by Sequoia Analytical and reported in Table 1. The laboratory analytical results are attached.

Thank you for allowing Gettler-Ryan Inc. to provide environmental services to Chevron. Please call if you have any questions or comments regarding this report.

Sincerely, erdin **Project Coordinator**

5251dws.ltr

Table 1:Supply Well Analytical ResultsAttachments:Chain of Custody Document and Laboratory Analytical Reports



Table 1 Former Chevron Service Station #9-7127 Interstate 580 & Grant Line Road Tracy, California

SUPPLY WELL GENERAL MINERAL, PHYSICAL & INORGANIC CHEMICAL ANALYSES (Drinking Water Standards) Sampled February 19, 1997

| Constituent | (Actual) Result | Maximum Contaminant Level (MCL) | Detection Limit for Reporting |
|---|--------------------|---------------------------------------|-------------------------------------|
| Chloride (CI) | 150 mg/L | 250 mg/L+ | 2.0 mg/L |
| Nitrate | 46 mg/L | 45 mg/L | 2.0 mg/L |
| Specific Conductance (E.C.) | 1000 µmho/cm | 900µmho/cm+ | 1.0 μ mho/cm |
| Total Filterable Residue @ 180 C (TDS) | 670 mg/L | 500 mg/L+ | 1.0 mg/L |
| Iron (Fe) | 0.47 μg/L | 300 µg/L | 100 µg/L |
| Manganese (MN) | 0.11 µg/L | 50 μg/L | 30 µg/L |
| Total Coliform | Absent | | |

+ = Indicates Secondary Drinking Water Standards

mg/L = miligram per liter/parts per million $\mu g/L = micrgram$ per liter/parts per billion $\mu mho/cm = Micromhos/per centimeter$



680 Chesapeake Drive 404 N. Wiget Lane

| Date of Report: Mar 4, 1997 Lab Name: Sequoia Analytical | Sampler Name: Employed by: | F. Cline Gettler-Ry | | Date/Time Sample Collected: ategies | 2/19/97 | 1130 |
|---|-------------------------------|------------------------|---------|--|---------|--------------|
| | _ | | Date/Ti | me Sample Received @ Lab: | 2/20/97 | 1238 |
| | Sample ID No.: | 9702A15 | 01 | Date Completed: | Feb 26, | 1997 |
| | | | | | | 8111119 1 |

GENERAL MINERAL, PHYSICAL, & INORGANIC CHEMICAL ANALYSES (4/95)

| System Name: <u>Gettler-Ryan/Geostrategies</u> Name/No. of Sample Source: <u>Supply Well</u> | System Number: |
|---|----------------|
| User ID: $ _H_ _E_ _N_ $ Station Number: $ _ _ _ _ $ | |
| Date Analyses Complete Submitted by: Phone # | Y Y M M D D |

| MCL/Reporting Units | Constituent | Entry # | Analyses Results | DLR |
|---|---|--|---------------------|------|
| | | | | |
| mg/L | Total Hardness (as CaC03) | 00900 | | |
| mg/L | Calcium (Ca) | 00916 | | |
| mg/L | Magnesium (Mg) | 00927 | | |
| mg/L | Sodium (Na) | 00929 | · | |
| mg/L | Potassium (K) | 00937 | <u> </u> | |
| Total Cations | meg/L Value: | | | |
| Total Cations | meq/L value. | | | |
| Total Cations | meq/L Value. | | | |
| mg/L | Total Alkalinity (as CaC03) | | | |
| mg/L mg/L | Total Alkalinity (as CaC03) Hydroxide (OH) | | | |
| mg/L mg/L mg/L | Total Alkalinity (as CaC03) Hydroxide (OH) Carbonate (CO3) | 00410 | | |
| mg/L mg/L | Total Alkalinity (as CaC03) Hydroxide (OH) Carbonate (CO3) Bicarbonate (HC03) | 00410 71830 00445 | | |
| mg/L mg/L mg/L mg/L * mg/L + | Total Alkalinity (as CaC03) Hydroxide (OH) Carbonate (CO3) Bicarbonate (HC03) Sulfate (S04) | 00410 | | |
| mg/L mg/L mg/L mg/L * mg/L + * mg/L + | Total Alkalinity (as CaC03) Hydroxide (OH) Carbonate (CO3) Bicarbonate (HC03) Sulfate (S04) Chloride (Cl) | 00410 71830 00445 00440 00945 | | 0.50 |
| mg/L mg/L mg/L * mg/L * mg/L + * mg/L + 45 mg/L | Total Alkalinity (as CaC03) Hydroxide (OH) Carbonate (CO3) Bicarbonate (HC03) Sulfate (S04) Chloride (Cl) Nitrate (NO3) | 00410 71830 00445 00440 00945 00940 | | 0.50 |
| mg/L mg/L mg/L mg/L * mg/L + * mg/L + | Total Alkalinity (as CaC03) Hydroxide (OH) Carbonate (CO3) Bicarbonate (HC03) Sulfate (S04) Chloride (Cl) | 00410 71830 00445 00440 00945 | | 0.50 |

| Sta Units | pri (Laboratory) | 00403 | | |
|------------|---|-------|------|-----|
| ** µmho/cm | + Specific Conductance (E.C.) | 00095 | 1000 | 1.0 |
| *** mg/L - | Total Filterable Residue at 180 C (TDS) | 70300 | 670 | 1.0 |
| 15 UNITS | Apparent Color (Untiltered) | 00081 | | |
| 3.0 TON | Odor Threshold at 60 C | 00086 | | |
| 5.0 NTU | Lab Turbidity | 82079 | | |
| 0.50 mg/L | MBAS | 38260 | | |

* 250-500-600

** 900-1600-2200 *** 500-1000-1500

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680 Chesapeake DriveRedwood City, CA 94063404 N. Wiget LaneWalnut Creek, CA 94598819 Striker Avenue, Suite 8Sacramento, CA 95834

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FAX (415) 364-9233 FAX (510) 988-9673 FAX (916) 921-0100

INORGANIC CHEMICALS

| MCL/Reporting Units | | Constituent | Entry | Analyses | DLR |
|------------------------|-------------|---------------------|-------|--------------|-----|
| | | | # | Results | |
| 1000 | | | | · ···· ··· · | |
| 1000 | μg/L | Aluminum (Al) | 01105 | | 50 |
| 6.0 | µg/L | Antimony | 01097 | | 6.0 |
| 50 | µg/L | Arsenic (As) | 01002 | | 2.0 |
| 1000 | µg/L | Barium (Ba) | 01007 | | 100 |
| 4.0 | µg/L | Beryllium | 01012 | | 1.0 |
| 5.0 | µg/L | Cadmium (Cd) | 01027 | | 1.0 |
| 50 | μg/L + | Chromium (Total Cr) | 01034 | | 10 |
| 1000 | $\mu g/L +$ | Copper (Cu) | 01042 | | 50 |
| 300 | μg/L | Iron (Fe) | 01045 | 0.47 | 100 |
| | μg/L | Lead (Pb) | 01051 | | 5.0 |
| 50 | μg/L | Manganese (Mn) | 01055 | 0.11 | 30 |
| 2.0 | μg/L | Mercury (Hg) | 71900 | | 1.0 |
| 100 | μg/L | Nickel | 01067 | | 10 |
| 50 | µg/L | Selenium (Se) | 01147 | | 5.0 |
| 100 | µg/L | Silver (Ag) | 01077 | | 10 |
| 2.0 | µg/L | Thallium | 01059 | - | 1.0 |
| 5000 | µg/L | Zinc (Zn) | 01092 | | 50 |

ADDITIONAL ANALYSES

| NTU | Field Turbidity | 82078 | |
|--------------|------------------------------|-------|----------|
| С | Source Temperature | 00010 | |
| | Langelier Index Source Temp. | 71814 | |
| | Langelier Index at 60 C | 71813 | |
| Std. Units | Field pH | 00400 | |
| | Aggressiveness Index | 82383 | |
| mg/L | Silica | 00955 | |
| mg/L | Phosphate | 00650 | |
| mg/L | lodide | 71865 | |
| | Sodium Absorption Ratio | 00931 | |
| 7 MFL | Asbestos (*) | 81855 | 0.20 |
| | Boron | 01020 | |
| 1,000 μg/L | Nitrate as N (Nitrogen) | 00618 | 400 |
| _10,000 μg/L | Nitrate + Nitrite as N | A-029 | 400 |
| 1,000 μg/L | Nitrite as N (Nitrogen) | 00620 | 400 |
| 200 μg/L | Cyanide | 01291 | 100 |
| mg/L | Ammonia | 00612 | |
| μg/L | Lithium | 01132 | |
| mg/L | Bromide | 82298 | |
| mg/L | Bromate | A-027 | |
| <u>·· </u> | 1 | | |

SEQUOIA ANALYTICAL

Mike Gregory Project Manager

- + indicates Secondary Drinking Water Standards
- * Detection Limit for Reporting Purposes



680 Chesapeake Drive 404 N. Wiget Lane

Redwood City, CA 94063 (415) 364-9600 Walnut Creek, CA 94598 819 Striker Avenue, Suite 8 Sacramento, CA 95834

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FAX (415) 364-9233 FAX (510) 988-9673 FAX (916) 921-0100

| Gettler Ryan/Geostrategies 6747 Sierra Court Suite G | Client Proj. ID: Chevron #9-7127 | Sampled: 02/19/97 Received: 02/20/97 | | |
|---|----------------------------------|---|--|--|
| Dublin, CA 94568 | Lab Proj. ID: 9702E76 | Analyzed: see below | | |
| Attention: Deanna Harding | | Reported: 02/28/97 | | |

LABORATORY ANALYSIS

| Analyte | Units | Date Analyzed | Detection Limit | Sample Results |
|--|-------|------------------|--------------------|-------------------|
| Lab No: 9702E76-01 Sample Desc : LIQUID,Supply Well | | | | |
| Total Coliform | P/A | 02/20/97 | N/A | Absent |

alytes reported as N.D. were not present above the stated limit of detection.

EQUOIA ANALYTICAL - ELAP #1210

ike Gregory oject Manager

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FAX (415) 364-9233 FAX (510) 988-9673 FAX (916) 921-0100

| Gettler Ryan/Geostrategies 6747 Sierra Court, Ste J Dublin, CA 94568 | Client Project ID: Matrix: | Chevron 9-1 Liquid | 7127 | | | | |
|--|-------------------------------|-----------------------|------|-----------|-------|------|-----|
| Attention: Deanna Harding | Work Order #: | 9702A15 | 01 | Reported: | Mar 4 | 4, 1 | 997 |

QUALITY CONTROL DATA REPORT

| Analyte: | Beryllium | Cadmium | Chromium | Nickel | |
|-------------------|-----------------|-----------------|-----------------|-----------------|--|
| | ME0224976010MDC | ME0224976010MDC | ME0224976010MDC | ME0224976010MDC | |
| Analy. Method: | | EPA 6010 | EPA 6010 | EPA 6010 | |
| Prep. Method: | EPA 3010 | EPA 3010 | EPA 3010 | EPA 3010 | |
| Analyst: | | C. Medefesser | C. Medefesser | C. Medefesser | |
| MS/MSD #: | | 970268406 | 970268406 | 970268406 | |
| Sample Conc.: | | N.D. | N.D. | N.D. | |
| Prepared Date: | | 2/24/97 | 2/24/97 | 2/24/97 | |
| Analyzed Date: | 2/26/97 | 2/26/97 | 2/26/97 | 2/26/97 | |
| instrument I.D.#: | MTJA2 | MTJA2 | MTJA2 | MTJA2 | |
| Conc. Spiked: | 1.0 mg/L | 1.0 mg/L | 1.0 mg/L | 1.0 mg/L | |
| Result: | 1.0 | 1.0 | 1.0 | 1.0 | |
| MS % Recovery: | 100 | 100 | 100 | 100 | |
| Dup. Result: | 1.0 | 1.0 | 1.0 | 1.0 | |
| MSD % Recov.: | 100 | 100 | 100 | 100 | |
| RPD: | 0.0 | 0.0 | 0.0 | 0.0 | |
| RPD Limit; | 0-20 | 0-20 | 0-20 | 0-20 | |

| LCS #: | BLK022497BS | BLK022497BS | BLK022497BS | BLK022497BS | |
|---------------------------------|-------------|-------------|-------------|-------------|--|
| Prepared Date: | 2/24/97 | 2/24/97 | 2/24/97 | 2/24/97 | |
| Analyzed Date: | 2/26/97 | 2/26/97 | 2/26/97 | 2/26/97 | |
| Instrument I.D.#: | MTJA2 | MTJA2 | MTJA2 | MTJA2 | |
| Conc. Spiked: | 1.0 mg/L | 1.0 mg/L | 1.0 mg/L | 1.0 mg/L | |
| LCS Result: | 1.0 | 1.0 | 1.0 | 1.1 | |
| LCS % Recov.: | 100 | 100 | 100 | 110 | |
| MS/MSD LCS Control Limits | 80-120 | 80-120 | 80-120 | 80-120 | |

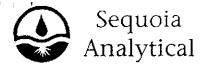
SEQUOIA ANALYTICAL



Please Note:

The LCS is a control sample of known, interferent-free matrix that is analyzed using the same reagents, preparation, and analytical methods employed for the samples. The matrix spike is an aliquot of sample fortified with known quantities of specific compounds and subjected to the entire analytical procedure. If the recovery of analytes from the matrix spike does not fall within specified control limits due to matrix interference, the LCS recovery is to be used to validate the batch.

** MS = Matrix Spike, MSD = MS Duplicate, RPD = Relative % Difference



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 FAX (510)
 988-9673

 (916)
 921-9600
 FAX (916)
 921-0100

| Gettler Ryan/Geostrategies 6747 Sierra Court, Ste J Dublin, CA 94568 | Client Project ID: Matrix: | Chevron 9 Liquid | -7127 | | 9460805138 | | |
|--|-------------------------------|---------------------|-------|-----------|------------|------|----|
| Attention: Deanna Harding | Work Order #: | 9702A15 | 01 | Reported: | Mar 4 | , 19 | 97 |

QUALITY CONTROL DATA REPORT

| Analyte: | Conductivity | Total Dissolved | Chloride | Nitrate |
|-------------------|------------------------|-----------------|-----------------|-----------------|
| | conductivity | Solids | Chionde | INITIALE |
| QC Batch#: | N022097120100A | IN022597160100A | IN0220973000ACB | IN0220973000ACB |
| Analy. Method: | EPA 120.1 | EPA 160.1 | EPA 300.0 | EPA 300.0 |
| Prep. Method: | N.A. | N.A. | N.A. | N.A. |
| | | | Hart. | 10.A. |
| Analyst: | J. Saadeh | N. Le | S. Fong | S. Fong |
| MS/MSD #: | 9702A1201 | 9702A1501 | 9702A1501 | 9702A1501 |
| Sample Conc.: | 460 | 340 | 150 | 46 |
| Prepared Date: | 2/20/97 | 2/25/97 | 2/20/97 | 2/20/97 |
| Analyzed Date: | 2/20/97 | 2/25/97 | 2/21/97 | 2/21/97 |
| Instrument I.D.#: | MANUAL | MANUAL | INIC2 | INIC2 |
| Conc. Spiked: | 1 400 µmho s/cn | 250 mg/L | 10 mg/L | 10 mg/L |
| Result: | 1900 | 570 | 160 | 56 |
| MS % Recovery: | 97 | 92 | 100 | 100 |
| Dup. Result: | 1800 | 580 | 160 | 56 |
| MSD % Recov.: | 96 | 96 | 100 | 100 |
| RPD: | 5.4 | 1.7 | 0.0 | 0.0 |
| RPD Limit: | 0-20 | 0-20 | 0-20 | 0-20 |
| | • -• | 0.00 | 0.20 | 0-20 |
| | | | | |
| LCS #: | LCS022097 | LCS022597 | LCS022097 | LCS022097 |
| Prepared Date: | 2/20/97 | 2/25/97 | 2/20/97 | 2/20/97 |
| Analyzed Date: | 2/20/97 | 2/25/97 | 2/21/97 | 2/21/97 |
| Instrument I.D.#: | MANUAL | MANUAL | INIC2 | INIC2 |
| Conc. Spiked: | 710 µmhos/cm | 500 mg/L | 10 mg/L | 10 mg/L |
| LCS Result: | 680 | 480 | 9.5 | 9.6 |
| LCS % Recov.: | 96 | 96 | 9.5 | 96 |
| | ······ | | | |
| M\$/MSD | 75-125 | 75-125 | 75-125 | 75-125 |
| LCS | 80-120 | 80-120 | 80-120 | 80-120 |
| Control Limits | | | | |

SEQUOIA ANALYTICAL

Mike Gregory Project Manager

** MS=Matrix Spike, MSD=MS Duplicate, RPD=Relative % Difference

The LCS is a control sample of known, interferent-free matrix that is analyzed using the same reagents,

preparation, and analytical methods employed for the samples. The matrix spike is an aliquot of sample fortified with known quantities of specific compounds and subjected to the entire analytical procedure. If the recovery of analytes from the matrix spike does not fall within specified control limits due to matrix

interference, the LCS recovery is to be used to validate the batch.

Piease Note:

| | IUX U | 1 01 | Lui | л кө | port | and | CUC to | Ch | evro | n C | C' 1 | ct: i | | 0 | | | (| Cha | in- | of- | Cue | tc y-Reco | <u>n kr</u> | |
|-----------|---------------------|--|---------------------|--|--|--------|---------------------------------------|-------------------|-----------------|----------------------|--------------------------|----------|-------------|--|--------------------------------|---|---|--|-----------|--------------------------|--------------------|-----------------|-------------|--|
| | | | Che | Newron Facility Number | | | | | | | | | | | | l (Hami | •) <u>PH</u> | IL BR | IGGS | | <u>UU</u> | | <u></u> | |
| | Chevron U. | | Con | uuliant F | ing Addri Protect Ni | 5 | 251 | | | | | · | | Chevron Conlact (Hame) PHIL BRIGGS (Phone) (510) 842-9136 | | | | | | | | | | |
| | P.O. BOX | | | | ultant Project Number 5251 ultant Nome Gettler-Ryan | | | | | | | | | | | Laboratory Name SEQUOIA Service Code: 2202790 Laboratory Service Order # 9050840 | | | | | | | | |
| | San Ramon, | | 1 | Addrese | drass 6747 Sierra Ct, Ste J, Dublin 94568 | | | | | | | | | | rySer | vice | Orde | <u>r / </u> | 00000 | 40 | 0 | | ······ | |
| | FAX (415)8 | 42-9591 | | Project Contact (Name) Deanna Harding | | | | | | | | | | Samples Collected by (Name) Frank Cline | | | | | | | | | | |
| | | | | Project (| ionlact [| Hame) | 51-7555 | arum | <u>5</u> | | 71. 70 | 0.0 | | Collection | n Dole. | 2/19 | 197 | | · | | | | | |
| | | ······································ | , I | | () | Phone) | 51-7555 | (Fa) | (Numbe | ir) | 51-70 | 00 | _ | Signature | · | | Ľ | <u>(e</u> | <u> </u> | н | ਾਹੇ ਾਹੇ | | | |
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| | • | X | L E | Matrix S I Sol A M W I Water C I Charo | 6 = Crub 6 = Composite 0 = Discrete | | E E | [| | | | 1 2 | 3 | | | | H. S | \$ 17. | नु युँ – | | | DO NOT BILL | | |
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| | THE I | , K | | ≺∪ ⊾ | 305 | | | 8 | لم ^ع | , ' | | l st | Ę | ĝ | Б. | 150 | | | CO P | Ц. Ц | s. – | 14 cm 12 ; | 39 | |
| | ~ ~ . | Lab Sample Number | Number of Container | Sol Vate | 000 | | Sumple Preservation | (cad (Year or No) | 1 | TPH Diesed (8015) | All and Groave (5520) | 1 | - <u>4</u> | Puryeable Organica (8240) | Extroctable Organics (8270) | 5 X | | | | [] [] | Dissolved 160.1 | | | |
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| | | | <u></u> | 205 | 1 ⁴⁷ | ㅋ | N N | · <u>0</u> . | E S | <u>P</u> ~ | 5 | 1 2° | 23 | 4 | 19.55 | Metais Cd.Cr.Pb.Zn.Ni (ICAP or At) | | Nitrate chlorid 200.1/Iron magginere | D e d | lotal Coliform e-coli | D C T A | Mike Sveep | 14 | |
| f | Supply Wel | 1 | 5 | W | 6 | 1130 | #N/45 M/a. | Y | 1 | | 1 | | ۰. | 1 | | | 8 | | | н Х | <u>20</u> | Per the | | |
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ATTACHMENT C

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HISTORICAL SOIL CERTIFIED ANALYTICAL REPORTS

TANK REMOVAL SAMPLING

April 4, 1991 / 910404-G-1

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SCOPE OF REQUESTED SERVICES

In accordance with your request, our office was asked to provide field personnel who would be sent to the site for the specific purpose of obtaining environmental samples following the removal of three gasoline tanks, one waste oil tank and one fuel oil tank.

Our personnel would collect the samples, arrange for the requested analyses of the samples and maintain adequate documentation for the issuance of a formal Sampling Report. The collection of environmental samples was to be performed in accordance with the requirements of the State Water Resources Control Board, Regional Water Quality Control Board, and the specific directions of the Local Implementing Agency (LIA) inspector.

The subject site is located within the overall jurisdiction of the Regional Water Quality Control Board -- Central Valley Region (Region 5). Initial inspection and evaluation of sites in this area is customarily conducted by the local implementing agency (LIA): the Alameda County Health Agency.

EXECUTION OF THE WORK PERFORMED ON APRIL 4, 1991

Personnel were dispatched from our office and arrived at the subject site on Thursday, April 4, 1991.

Chevron USA, Inc. was represented by Mr. Gordon Johnson and Ms. Nancy Vukelich.

The local implementing agency, Alameda County Health Agency, was represented by Mr. Gil Wistar, who was present to observe the tank removal and sampling.

In accordance with the local regulations and the field judgment of the LIA representative, a detailed inspection of each tank was conducted following their removal from the open excavation. The tanks were visually inspected and likely failure points were probed with small pointed metal examination tools. No holes were observed in any of the tanks.

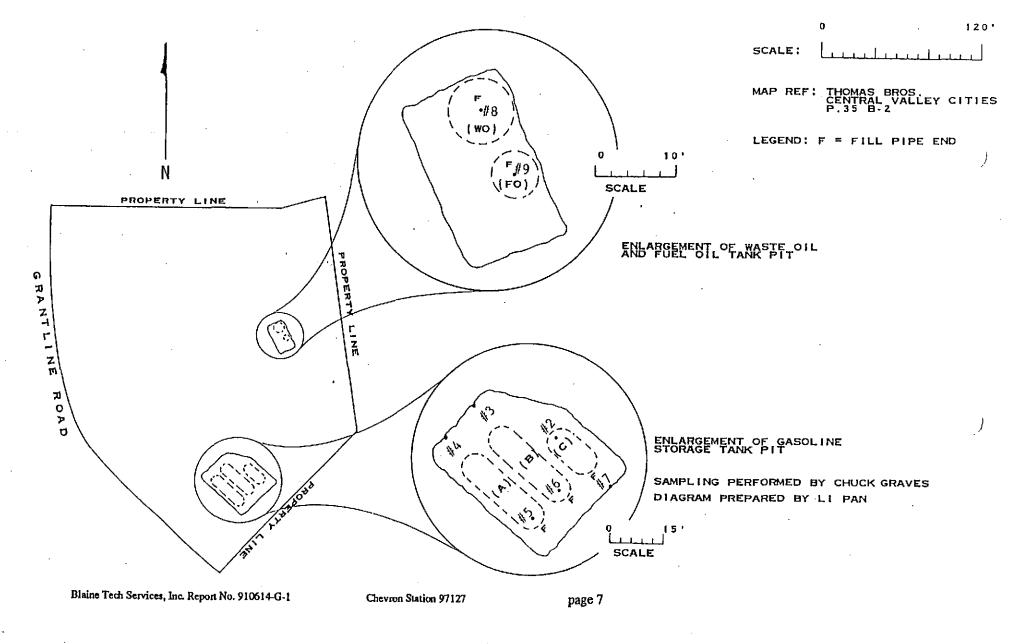
| TANK I.D. | SIZE IN GALLONS | tank Content | MATERIAL OF CONSTRUCTION | INSPECTION FOUND |
|--------------|--------------------|-----------------|-----------------------------|---------------------|
| | | | | |
| A | 10,000 | GASOLINE | FIRERGLASS | NO HOLES |
| в | 10,000 | GASOLINE | FIBERGLASS | NO HOLES |
| С | 6,000 | GASOLINE | FIBERGLASS | NO HOLES |
| WO | 1,000 | WASTE OIL | FIBERGLASS/ | NO BOLES |
| | | | SPHERICAL | |
| FO | 750 | FUEL OIL | FIBERGLASS/ | NO HOLES |
| | | | SPHERICAL | |

Blaine Tech Services, Inc. Report No. 910614-G-1

TANK REMOVAL DIAGRAM

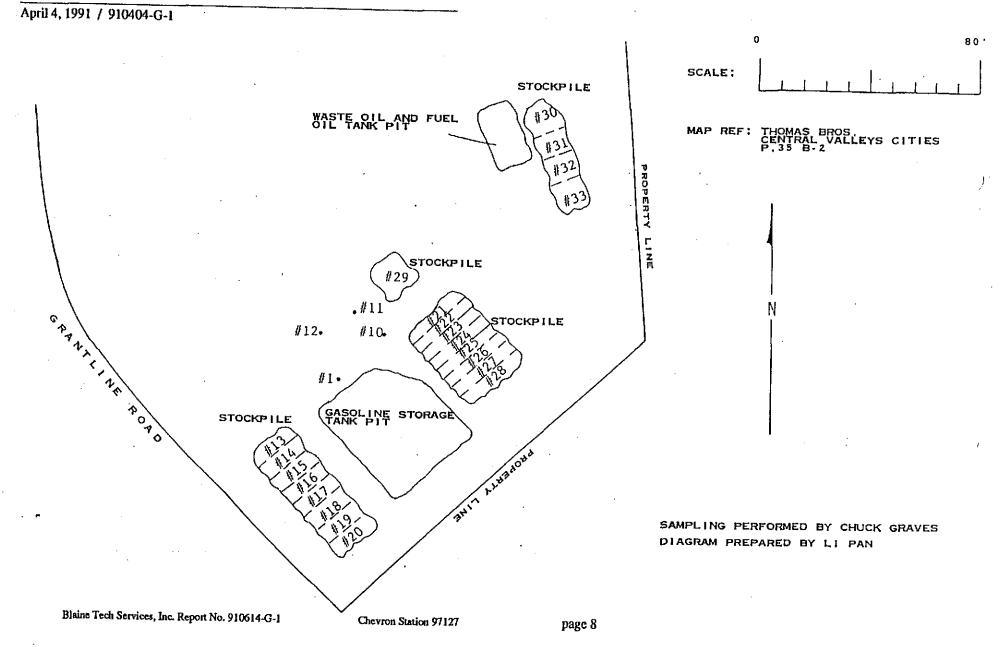
DIAGRAM ONE

April 4, 1991 / 910404-G-1



TANK REMOVAL DIAGRAM

DIAGRAM TWO



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ADDITIONAL EXCAVATION DIAGRAM

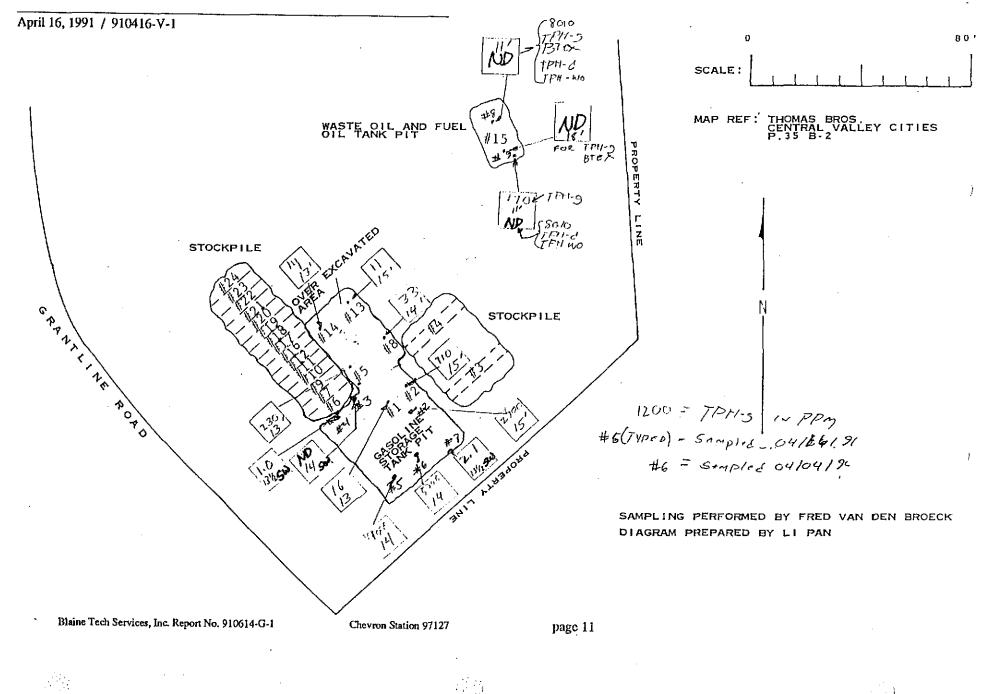


TABLE OF SAMPLING LOCATIONS AND ANALYTICAL RESULTS

| I.D. | SAMPLE | | TYPE 5 | | | | | | NOT | | tical resu Per Milli | on or Par | reported ts Per B | ln llion | |
|---------------------------------|-----------------------------------|--|--|------------------------------|---|--|------------------------|--|--|--------------------------|-----------------------------|---------------------------------|-------------------------------|----------------------------------|---------------------------------|
| GIVEN This Sample Area | DEPTH IN FT. BELOW GRADE | SAMPLING LOCATION DICTATED BY | METHOD FOR THE SAMPLE OBTAINED | SAMPLE MATRIX | DATE SAMPLED | BIS CHAIN OF CUSTODY I.D. | BTS Sample I.D. | NAME OF Dohs HMTL Laboratory | LABORATORY SAMPLE I.D. | трн Ля Сля | BEN- Lenz | TOL- | { Ethyl Ben- | х т - | TOTAL |
| AF | 14.0 | STANDARD | INTRFACE | SOIL | 04/04/91 | 910404-G-1 | 15 | SEQUOIA | 104-0738 | 4000 | ND | UENE 41 | ZENE 66 | LENES | LEAD |
| λορ | 13.5 | LIA | SIDEWALL | SOIL | 04/04/91 | 910404-G-1 | Få | SEQUOIA | 104-0737 | 1.0 | 0.0070 | ND | 0.0050 | 310 0.030 | 13 9.1 |
| BF | 14.0 | STANDARD | INTRFACE | SOIL | 04/04/91 | 910404-G-1 | 16 | SEQUOIA | 104-0739 | 5700 | 20 | | ····· | | |
| Вор | 14.0 | LIA | SIDEWALL | SOIL | 04/04/91 | 910404-G-1 | 13 | SEQUOIA | 104-0736 | ND | 0.0070 | 220 0,016 | 10 0.012 | 560. 0.030 | 80 7.7 |
| CF | 12.5 | LIN | SIDEWALL | SOIL | 04/04/91 | 910404-G-1 | #7 | SEQUOIA | 104-0740 | 2.1 | 0.018 | 0.013 | 0.014 | 0.046 | |
| Сор | 15.0 | STANDARD | INTRFACE | SOIL | 04/04/91 | 910404-G-1 | 12 | SEQUOIN | 104-0735 | 2900 | 30 | 180 | 60 | 350 | 6.9 14 |
| | 13.0 | ELECTIVE | CONFIRM | 501L 501L | 04/16/91 04/16/91 | 910416-V-1 910416-V-1 | 11 · 12 | SEQUOIA SEQUOIA | 104-2649 104-2650 | 16 710 | 0.0090 | 0.014 | 0.021 | 0.17 0.41 | 3.6 8.1 |
| PRODUCT | LINE/DI | SPENSER PUN | IP ISLAND | | · | | ····· | | | | ······ | | | | |
| 11 10 11 12 | 2,5 4,0 4,0 4,0 | LIA LIA LIA LIA | INTRFACE INTRFACE INTRFACE INTRFACE | SOIL SOIL SOIL SOIL | 04/04/91 04/04/91 04/04/91 .04/04/91 | 910404-G-1 910404-G-1 910404-G-1 910404-G-1 | 1 10 11 12 | SEQUOIA SEQUOIA SEQUOIA SEQUOIA | 104-0734 104-0743 104-0744 104-0745 | 1200 3.3 750 15 | 3.3 D.20 12 0.23 | 17 0.043 33 0.19 | 17 0.060 19 0,26 | 86 0.16 110 1.3 | 17 7.7 9.5 |
| 15 10 113 114 | 13.0 14.0 15.0 13.0 | ELECTIVE ELECTIVE ELECTIVE ELECTIVE | CONFIRM CONFIRM CONFIRM CONFIRM | SOIL SOIL SOIL SOIL | 04/16/91 04/16/91 04/16/91 04/16/91 | 910416-V-1 910416-V-1 910416-V-1 910416-V-1 910416-V-1 | 15 98 913 914 | SEQUOIA SEQUOIA SEQUOIA SEQUOIA | 104-2653 104-2656 104-2661 104-2662 | 220 33 11 9.2 | ND 0.065 ND 0.0050 | 0.80 0.24 0.047 0.0060 | 1.7 0.27 0.044 0.030 | 1.3 10 1.5 0.31 0.13 | 6.9 2.6 6.1 5.1 3.6 |

Standard - The location conformed to established (professional or regulatory) definitions for the type of sample being collected. Example: a standard RWQCB interface sample.

LIA

- The local implementing agency inspector chose a sampling location that was different from a standard (pre-defined) location.

Elective - Elective samples are not taken to comply with regulatory requirements, but to obtain information. Sampling locations may be chosen by the property owner, the contractor, a consultant, etc. The samples may or may not be analyzed.

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Chevron Station 97127

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TABLE OF SAMPLING LOCATIONS AND ANALYTICAL RESULTS

NOTE: Analytical results are reported in Parts Per Hillon or Parts Per Billon

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| I.D. GIVEN | SAMPLE Depth | SAMPLING | TYPE 4 Method | | | BTS | | | | • | | P | PH | | | | | |
|------------------------|----------------------------------|----------------------------------|--|------------------------------|--|--|--------------------------|--|--|----------------------|----------------------|----------------|-----------------------|----------------|--------------------------|--|--|--|
| TRIS SAMPLE AREA | IN FT. BELOH GRADE | LOCATION DICTATED BY | FOR THE SAMPLE OBTAINED | SAMPLE MATRIX | DATE SAMPLED | CHAIN OF CUSTODY I.D. | BTS SAMPLE I.D. | NAME OF DOHS HMTL LABORATORY | LABORATORY SAMPLE I.D. | трн Аз Саз | Ben- Zene | TOL- UENE | ETHYL BEN- ZENE | XY – Lenes | TOTAL LEAD | | | |
| Won | 11.0 | STANDARD | INTRFACE | SOIL | 04/04/91 | 910404-G-1 | 18 | SEQUOIA | 104-0741 | ND | ND | ND | ND | ND | 3.3 | | | |
| Fol | 11.0 | STANDARD | INTRFACE | SOIL | 04/04/91 | 910404-G-1 | 19 | SEQUOIA | 104-0742 | 170 | ND | ND | ND | 2.7 | 1.7 | | | |
| #15 | 18.0 | ELECTIVE | CONFIRM | SOIL | 04/16/91 | 910416-V-1 | #15 | SEQUOIA | 104-2663 | ND | ND | ND | ND | ND | 6.1 | | | |
| STOCK | 6-12" 6-12" 6-12" 6-12" | RWQCB RWQCB RWQCB RWQCB | DISCRETE DISCRETE DISCRETE DISCRETE | SOIL SOIL SOIL SOIL | 04/04/91 04/04/91 04/04/91 04/04/91 | 910404-G-1 910404-G-1 910404-G-1 910404-G-1 910404-G-1 | 130 131 132 133 | SEQUOIA SEQUOIA SEQUOIA SEQUOIA | 104-0763 104-0764 104-0765 104-0765 | ND ND ND ND | ND ND ND ND | ND ND ND | nd Nd Nd Nd | ND ND ND | 2,6 4.1 5.9 2.5 | | | |

I.D. SAMPLE TYPE 6 GIVEN SAMPLING DEPTH METHOD BT S IN TT. CHAIN OF ---PPB---THIS LOCATION FOR THE BTS NAME OF -PPM------BLLOW DICTATED EPA 8010 SANPLE SAMPLE SAMPLE DATE CUSTODY SAMPLE DOHS HMTL LABORATORY TPH-HBF TOTAL OIL OBTAINED AREA GRADE BY MATRIX SAMPLED I.D. LABORATORY SAMPLE I.D. DIESEL GREASE COMPOUNDS I.D. WoM 11.0 STANDARD ND INTRFACE SOIL 04/04/91 910404-G-1 18 104-0741 ND ND SEQUOIA FoM 11.0 STANDARD INTRFACE SOIL 04/04/91 19. 104-0742 ND ND 910404-G-1 SEQUOIA ND 104-0763 104-0764 104-0765 104-0765 ND ND ND 6-12" 6-12" 6-12" 6-12" RWQCB RWQCB RWQCB RWQCB DISCRETE DISCRETE DISCRETE SOIL SOIL SOIL 04/04/91 04/04/91 04/04/91 SEQUOIA SEQUOIA SEQUOIA ND ND ND STOCK 910404-G-1 130 ND ND 910404-G-1 910404-G-1 131 132 2.6 DISCRETE SOL 04/04/91 910404-G-1 133 SEQUOIA ND ND

| I.D. GIVEN THIS SAMPLE AREA | SAMPLE DEPTH IN FT. BELOW GRADE | SAMPLING LOCATION DICTATED BY | TYPE L METHOD FOR THE SAMPLE OBTAINED | SAMP LE MATRIX | DATE SAMP LED | BTS CHAIN OF CUSTODY I.D. | bts Sample I.D. | NAME OF DOHS HMTL LABORATORY | LABORATORY SAMPLE_I.D | CADMIUN | CHROMIDH | PM | 21NC | NICKEL |
|---|---|--|---|------------------------------|--|--|--------------------------|--|--|--------------------------|-------------------------|--------------------------|----------------------|-----------------------|
| WoH | 11.0 | STANDARD | INTRFACE | SOIL | 04/04/91 | 910404-G-1 | 18 | SEQUOIN | 104-0741 | 4.8 | 7.9 | 3.3 | 23 | 10 |
| FoM | 11.0 | STANDARD | INTRFACE | SOIL | 04/04/91 | 910404-G-1 | 19 | SEQUOIA | 104-0742 | 2.2 | 4.4 | 1.7 | 13 | 8.5 |
| STOCK | 6-12" 6-12" 6-12" 6-12" | RWQCB RWQCB RWQCB RWQCB | DI SCRETE DI SCRETE DI SCRETE DI SCRETE | SOIL SOIL SOIL SOIL | 04/04/91 04/04/91 04/04/91 04/04/91 | 910404-G-1 910404-G-1 910404-G-1 910404-G-1 910404-G-1 | +30 31 32 33 | SEQUOIA SEQUOIA SEQUOIA SEQUOIA | 104-0763 104-0764 104-0765 104-0766 | 3.4 2.8 5.2 2.7 | 8.4 7.9 18 5.9 | 2.6 4.1 5.9 2.5 | 22 25 42 21 | 9.7 15 16 11 |

Standard - The location conformed to established (professional or regulatory) definitions for the type of sample being collected. Example: a standard RWQCB interface sample.

LIA - The local implementing agency inspector chose a sampling location that was different from a standard (pre-defined) location.

Elective - Elective samples are not taken to comply with regulatory requirements, but to obtain information. Sampling locations may be chosen by the property owner, the contractor, a consultant, etc. The samples may or may not be analyzed.

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Chevron Station 97127

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Table 2 Soil Analytical Data Total Petroleum Hydrocarbons (TPH as Gasoline and BTEX Compounds)

Former Chevron U.S.A. Service Station 9-7127 Highway I-580 at Grant Line Road Tracy, California

| Boring Number | Sample Date | Sample Depth (feet) | TPH as Gasoline (ppm) | Benzene (ppm) | Toluene (ppm) | Ethylbenzene (ppm) | Xylenes (ppm) |
|------------------|--|---|---|---|---|---|---|
| B-1 MW-1 | 12/09/92 12/08/92 | 7 12.5 17.5 21.5 19 24 29 30.5 38.5 | ND 4.0 ND ND 2,600 8,100 ND ND | ND ND ND ND <5.0* 21 ND ND | ND ND 0.014 0.013 0.0056 79 560 ND | ND ND ND ND 30 150 ND | ND 0.015 0.025 0.018 0.0079 200 840 ND |
| Detection L | imits: | | 1.0 | 0.005 | 0.013 | ND 0.005 | 0.024 |
| ND = Not | s per million detected method reportir | a limit. | · | · | | _ <u></u> t | |