

B R O W N   A N D  
C A L D W E L L

March 27, 1996

Ms. Madhulla Logan  
Department of Environmental Health  
Environmental Protection Division  
1131 Harbor Bay Parkway, #250  
Alameda, CA 94502-6577

ENVIRONMENTAL  
PROTECTION  
96 MAR 28 PM 2:50

Subject:        Calculation of Cancer Risk from Inhalation of Indoor Air (Source Groundwater)  
                  Modelled with Equations Presented in "*Standard Guide for Risk-Based Corrective  
                  Action Applied at Petroleum Release Sites*"  
                  Former E-Z Serve Station #100877 Located at 525 West A Street Hayward, CA

Dear Ms. Logan:

This letter responds to your verbal request that the cancer risk for the indoor air pathway (source groundwater) for the Former E-Z Serve Hayward Site be calculated with equations presented in "*Standard Guide for Risk-Based Corrective Action Applied at Petroleum Release Sites*" (RBCA).

The following parameters were changed to site-specific values prior to running the model:

Depth to groundwater	488 cm from a default value of 300 cm
Thickness of capillary fringe	61 cm from a default value of 5 cm
Thickness of vadose zone	427 cm from a default value of 295 cm
Enclosed space air exchange rate	0.000183 s <sup>-1</sup> from a default value of 0.00014 s <sup>-1</sup>

Average air exchange rate for a house in the western United States from *Exposure Factors Handbook*, USEPA/600/P-95/0002A, June 1995.

The cancer risk associated with indoor air using the USEPA toxicity factor of 0.1 (mg/kg/day)<sup>-1</sup> was calculated to be 1x10<sup>-5</sup> (Appendix A). The cancer risk associated with indoor air using the California toxicity factor of 0.029 (mg/kg/day)<sup>-1</sup> was calculated to be 4x10<sup>-5</sup> (Appendix A). Risk results using either toxicity factor are within the acceptable risk range of 1x10<sup>-4</sup> to 1x10<sup>-6</sup>.

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Environmental Engineering And Consulting • Analytical Services

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3480 BUSKIRK AVENUE, PLEASANT HILL, CA 94523-4342  
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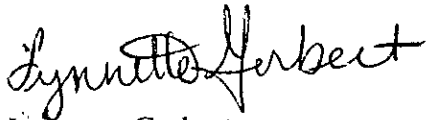
Ms. Madhulla Logan  
March 27, 1996  
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It is our understanding that the equations presented in RBCA are based on a conservative model developed by Johnson and Ettinger. It is important to note that there are several other models available which are routinely used to calculate risks from the indoor air pathway. We initially used the Karimi model in our risk assessment and calculated a risk of  $2 \times 10^{-6}$  (refer to Brown and Caldwell's letter dated September 12, 1995 which responded to your written comments of our risk assessment). In our experience, the Farmers model gives similar results to the Karimi model. The Thibodeaux-Hwang and Jury models are also available though less conservative than Karimi or Farmers.

If you have any questions please call me at (510) 210-2290.

Sincerely,

BROWN AND CALDWELL



Lynnette Gerbert  
Staff Toxicologist

Enclosures  
TD:lkg

cc: Mr. Brian Cobb, E-Z Serve Petroleum Marketing Company of California  
Mr. John Reeves, Attorney at Law

**APPENDIX A**  
**RISK CALCULATIONS USING EQUATIONS PRESENTED IN RBCA**

**Calculation of Risk Due to Inhalation of Indoor Air**  
**Source: Groundwater**  
**Chemical: Benzene**  
**Toxicity Factor: USEPA**  
**Former E-Z Serve Station #100877**  
**525 West A Street, Hayward, California**

$$\text{Risk} = (\text{SF}_i \times \text{IR}_{\text{air}} \times \text{ET} \times \text{EF} \times \text{ED} \times \text{VF}_{\text{wesp}} \times \text{C}) / (\text{BW} \times \text{AT} \times 365 \text{ days/year})$$

Concentration, mg/L	1 879 Chemical-Specific
VF <sub>wesp</sub> = See Below	0.002 See Below
BW = Body Weight, Kg	70 Default
ATc = Averaging time for carcinogens, years	70 Default
SF <sub>i</sub> = Inhalation slope factor, (mg/kg-day) <sup>-1</sup>	0.029 Chemical-Specific
IR <sub>air</sub> = Inhalation rate, m <sup>3</sup> /hr	0.83 Default
ET = Exposure Time, hours/day	24 Default
EF = Exposure Frequency, days/year	350 Default
ED = Exposure Duration, years	30 Default

Risk 1E-05

$$\text{VF}_{\text{wesp}} = (\text{H} \times (\text{Deff}_{\text{fws}} / \text{L}_{\text{gw}}) / (\text{ER} \times \text{L}_{\text{b}})) / (1 + ((\text{Deff}_{\text{fws}} / \text{L}_{\text{gw}}) / (\text{ER} \times \text{L}_{\text{b}})) + ((\text{Deff}_{\text{fws}} / \text{L}_{\text{gw}}) / (\text{Deff}_{\text{crack}} / \text{L}_{\text{crack}}) \times \text{n})) \times 1 \text{E} + 3$$

H = Henry's Law Constant, cm <sup>3</sup> -H <sub>2</sub> O/cm <sup>3</sup> -air	0.22 Chemical-Specific
Deff <sub>fws</sub> = See below	0.0002 See Below
L <sub>gw</sub> = Depth to groundwater, cm	488 Site-Specific
ER = Enclosed space air exchange rate, L/s	0.000183 Default
L <sub>b</sub> = Enclosed space volume/infiltration area ratio, cm	200 Default
Deff <sub>crack</sub> = See below	0.007 See Below
L <sub>crack</sub> = Enclosed space foundation/wall thickness, cm	15 Default
n = Areal fraction of cracks in foundations/walls	0.01 Default
VF <sub>wesp</sub>	0.002

$$\text{Deff}_{\text{fws}} = (\text{h}_{\text{cap}} + \text{h}_{\text{v}}) \times ((\text{h}_{\text{cap}} / \text{Deff}_{\text{cap}}) + (\text{h}_{\text{v}} / \text{Deff}_{\text{s}}))^{-1}$$

h <sub>cap</sub> = Thickness of capillary fringe, cm	61 Default
h <sub>v</sub> = Thickness of vadose zone, cm	427 Default
Deff <sub>cap</sub> = See below	2.17E-05 See Below
Deff <sub>s</sub> = See below	0.007 See Below
Deff <sub>fws</sub>	0.0002

$$\text{Deff}_{\text{cap}} = ((\text{D}_{\text{air}} \times \text{O}^{3.33}_{\text{acap}}) / \text{O}^2 \text{T}) + ((\text{D}_{\text{wat}} \times \text{O}^{3.33}_{\text{wcap}}) / (\text{H} \times \text{O}^2 \text{T}))$$

D <sub>air</sub> = Diffusion coefficient in air, cm <sup>2</sup> /s	0.093 Chemical-Specific
O <sub>acap</sub> = Volumetric air content in capillary fringe soils, cm <sup>3</sup> -air/cm <sup>3</sup> -soil	0.038 Default
OT = Total soil porosity, cm <sup>3</sup> /cm <sup>3</sup> -soil	0.38 Default
D <sub>wat</sub> = Diffusion coefficient in water, cm <sup>2</sup> /s	1.10E-05 Chemical-Specific
O <sub>wcap</sub> = Volumetric water content in capillary fringe soils, cm <sup>3</sup> -h <sub>2</sub> O/cm <sup>3</sup> -soil	0.342 Default
H = Henry's Law Constant (cm <sup>3</sup> -H <sub>2</sub> O/cm <sup>3</sup> -air)	0.22 Chemical-Specific
Deff <sub>cap</sub>	2.17E-05

$$\text{Deff}_{\text{s}} = ((\text{D}_{\text{air}} \times \text{O}^{3.33}_{\text{ss}}) / \text{O}^2 \text{T}) + ((\text{D}_{\text{wat}} \times \text{O}^{3.33}_{\text{ws}}) / (\text{H} \times \text{O}^2 \text{T}))$$

D <sub>air</sub> = Diffusion coefficient in air, cm <sup>2</sup> /s	0.093 Chemical-Specific
O <sub>ss</sub> = Volumetric air content in vadose zone soils, cm <sup>3</sup> -air/cm <sup>3</sup> -soil	0.26 Default
OT = Total soil porosity, cm <sup>3</sup> /cm <sup>3</sup> -soil	0.38 Default
D <sub>wat</sub> = Diffusion coefficient in water, cm <sup>2</sup> /s	1.10E-05 Chemical-Specific
O <sub>ws</sub> = Volumetric water content in vadose zone soils, cm <sup>3</sup> -h <sub>2</sub> O/cm <sup>3</sup> -soil	0.12 Default
H = Henry's Law Constant (cm <sup>3</sup> -H <sub>2</sub> O/cm <sup>3</sup> -air)	0.22 Chemical-Specific
Deff <sub>s</sub>	0.007

$$\text{Deff}_{\text{crack}} = ((\text{D}_{\text{air}} \times \text{O}^{3.33}_{\text{acrack}}) / \text{O}^2 \text{T}) + ((\text{D}_{\text{wat}} \times \text{O}^{3.33}_{\text{wcrack}}) / (\text{H} \times \text{O}^2 \text{T}))$$

D <sub>air</sub> = Diffusion coefficient in air, cm <sup>2</sup> /s	0.093 Chemical-Specific
O <sub>acrack</sub> = Volumetric air content in foundation/wall cracks, cm <sup>3</sup> -air/cm <sup>3</sup> -total volume	0.26 Default
OT = Total soil porosity, cm <sup>3</sup> /cm <sup>3</sup> -soil	0.38 Default
D <sub>wat</sub> = Diffusion coefficient in water, cm <sup>2</sup> /s	1.10E-05 Chemical-Specific
O <sub>wcrack</sub> = Volumetric water content in foundation/wall cracks, cm <sup>3</sup> -h <sub>2</sub> O/cm <sup>3</sup> -total volume	0.12 Default
H = Henry's Law Constant (cm <sup>3</sup> -H <sub>2</sub> O/cm <sup>3</sup> -air)	0.22 Chemical-Specific
Deff <sub>crack</sub>	0.007

**Calculation of Risk Due to Inhalation of Indoor Air**  
**Source: Groundwater**  
**Chemical: Benzene**  
**Toxicity Factor: California**  
**Former E-Z Serve Station #100877**  
**525 West A Street, Hayward, California**

$$\text{Risk} = (\text{SF}_i \times \text{IR}_{\text{air}} \times \text{ET} \times \text{EF} \times \text{ED} \times \text{VF}_{\text{wesp}} \times \text{C}) / (\text{BW} \times \text{ATc} \times 365 \text{ days/year})$$

Concentration, mg/L	1.879 Chemical-Specific
VF <sub>wesp</sub> = See Below	0.002 See Below
BW = Body Weight, Kg	70 Default
ATc = Averaging time for carcinogens, years	70 Default
SF <sub>i</sub> = Inhalation slope factor, (mg/kg-day) <sup>-1</sup>	0.1 Chemical-Specific
IR <sub>air</sub> = Inhalation rate, m <sup>3</sup> /hr	0.83 Default
ET = Exposure Time, hours/day	24 Default
EF = Exposure Frequency, days/year	350 Default
ED = Exposure Duration, years	30 Default
<b>Risk</b>	<b>4E-05</b>

$$\text{VF}_{\text{wesp}} = (\text{H} \times (\text{Deff}_{\text{fws}} / \text{L}_{\text{gw}}) / (\text{ER} \times \text{L}_b)) / (1 + ((\text{Deff}_{\text{fws}} / \text{L}_{\text{gw}}) / (\text{ER} \times \text{L}_b)) + ((\text{Deff}_{\text{fws}} / \text{L}_{\text{gw}}) / (\text{Deff}_{\text{crack}} / \text{L}_{\text{crack}}))^n) \times 1 \text{E} + 3$$

H = Henry's Law Constant, cm <sup>3</sup> -H <sub>2</sub> O/cm <sup>3</sup> -air	0.22 Chemical-Specific
Deff <sub>fws</sub> = See below	0.0002 See Below
L <sub>gw</sub> = Depth to groundwater, cm	488 Site-Specific
ER = Enclosed space air exchange rate, L/s	0.000183 Default
L <sub>b</sub> = Enclosed space volume/infiltration area ratio, cm	200 Default
Deff <sub>crack</sub> = See below	0.007 See Below
L <sub>crack</sub> = Enclosed space foundation/wall thickness, cm	15 Default
n = Areal fraction of cracks in foundations/walls	0.01 Default
<b>VF<sub>wesp</sub></b>	<b>0.002</b>

$$\text{Deff}_{\text{fws}} = (\text{h}_{\text{cap}} + \text{h}_v) \times ((\text{h}_{\text{cap}} / \text{Deff}_{\text{cap}}) + (\text{h}_v / \text{Deff}_{\text{fs}}))^{-1}$$

h <sub>cap</sub> = Thickness of capillary fringe, cm	61 Default
h <sub>v</sub> = Thickness of vadose zone, cm	427 Default
Deff <sub>cap</sub> = See below	2.17E-05 See Below
Deff <sub>fs</sub> = See below	0.007 See Below
<b>Deff<sub>fws</sub></b>	<b>0.0002</b>

$$\text{Deff}_{\text{cap}} = ((\text{D}_{\text{air}} \times \text{O}^{3.33}_{\text{acap}}) / \text{O}^2 \text{T}) + ((\text{D}_{\text{wat}} \times \text{O}^{3.33}_{\text{wcap}}) / (\text{H} \times \text{O}^2 \text{T}))$$

D <sub>air</sub> = Diffusion coefficient in air, cm <sup>2</sup> /s	0.093 Chemical-Specific
O <sub>acap</sub> = Volumetric air content in capillary fringe soils, cm <sup>3</sup> -air/cm <sup>3</sup> -soil	0.038 Default
OT = Total soil porosity, cm <sup>3</sup> /cm <sup>3</sup> -soil	0.38 Default
D <sub>wat</sub> = Diffusion coefficient in water, cm <sup>2</sup> /s	1.10E-05 Chemical-Specific
O <sub>wcap</sub> = Volumetric water content in capillary fringe soils, cm <sup>3</sup> -h <sub>2</sub> O/cm <sup>3</sup> -soil	0.342 Default
H = Henry's Law Constant (cm <sup>3</sup> -H <sub>2</sub> O/cm <sup>3</sup> -air)	0.22 Chemical-Specific
<b>Deff<sub>cap</sub></b>	<b>2.17E-05</b>

$$\text{Deff}_{\text{fs}} = ((\text{D}_{\text{air}} \times \text{O}^{3.33}_{\text{ss}}) / \text{O}^2 \text{T}) + ((\text{D}_{\text{wat}} \times \text{O}^{3.33}_{\text{ws}}) / (\text{H} \times \text{O}^2 \text{T}))$$

D <sub>air</sub> = Diffusion coefficient in air, cm <sup>2</sup> /s	0.093 Chemical-Specific
O <sub>ss</sub> = Volumetric air content in vadose zone soils, cm <sup>3</sup> -air/cm <sup>3</sup> -soil	0.26 Default
OT = Total soil porosity, cm <sup>3</sup> /cm <sup>3</sup> -soil	0.38 Default
D <sub>wat</sub> = Diffusion coefficient in water, cm <sup>2</sup> /s	1.10E-05 Chemical-Specific
O <sub>ws</sub> = Volumetric water content in vadose zone soils, cm <sup>3</sup> -h <sub>2</sub> O/cm <sup>3</sup> -soil	0.12 Default
H = Henry's Law Constant (cm <sup>3</sup> -H <sub>2</sub> O/cm <sup>3</sup> -air)	0.22 Chemical-Specific
<b>Deff<sub>fs</sub></b>	<b>0.007</b>

$$\text{Deff}_{\text{crack}} = ((\text{D}_{\text{air}} \times \text{O}^{3.33}_{\text{acrack}}) / \text{O}^2 \text{T}) + ((\text{D}_{\text{wat}} \times \text{O}^{3.33}_{\text{werack}}) / (\text{H} \times \text{O}^2 \text{T}))$$

D <sub>air</sub> = Diffusion coefficient in air, cm <sup>2</sup> /s	0.093 Chemical-Specific
O <sub>acrack</sub> = Volumetric air content in foundation/wall cracks, cm <sup>3</sup> -air/cm <sup>3</sup> -total volume	0.26 Default
OT = Total soil porosity, cm <sup>3</sup> /cm <sup>3</sup> -soil	0.38 Default
D <sub>wat</sub> = Diffusion coefficient in water, cm <sup>2</sup> /s	1.10E-05 Chemical-Specific
O <sub>werack</sub> = Volumetric water content in foundation/wall cracks, cm <sup>3</sup> -h <sub>2</sub> O/cm <sup>3</sup> -total volume	0.12 Default
H = Henry's Law Constant (cm <sup>3</sup> -H <sub>2</sub> O/cm <sup>3</sup> -air)	0.22 Chemical-Specific
<b>Deff<sub>crack</sub></b>	<b>0.007</b>

CHAIN OF CUSTODY RECORD

G97-04-221

2/2

BCA Log Number \_\_\_\_\_

Client name Brown & Caldwell Project or PO# 5172-10  
 Address 3480 Buskirk Avenue Phone # (510) 937-9010  
 City, State, Zip Pleasant Hill, CA 94523 Report attention Todd Miller

Analyses required									
TPA, BTEX, MPSE	Hazardous sample Special handling required	[Grid for analyses with 10 columns and 4 rows]							
		[Grid for analyses with 10 columns and 4 rows]							
		[Grid for analyses with 10 columns and 4 rows]							
		[Grid for analyses with 10 columns and 4 rows]							
Remarks: <u>G97-04-221</u>									

Lab Sample number	Date sampled	Time sampled	Type* See key below	Sampled by	Number of containers	Analyses required													
				Sample description		TPA, BTEX, MPSE	Hazardous sample Special handling required	[Grid for analyses with 10 columns and 4 rows]											
	<u>4/9/97</u>	<u>10:20</u>	<u>GW</u>	<u>J. LaPlante</u>	<u>100877-MW-4</u>			<u>2</u>	<u>X</u>										
	<u> </u>	<u>11:03</u>	<u> </u>		<u>100877-MW-2</u>			<u>2</u>	<u>X</u>										
	<u> </u>	<u>11:03</u>	<u> </u>		<u>100877-MW-2-D</u>			<u>2</u>	<u>X</u>										
	<u>4/9/97</u>	<u>11:03</u>	<u>GW</u>		<u>100877-MW-2-FB</u>	<u>2</u>	<u>X</u>												

Signature	Print Name	Company	Date	Time
<u>J. LaPlante</u>	<u>J. LaPlante</u>	<u>Brown &amp; Caldwell</u>	<u>4/9/97</u>	<u>13:30</u>
<u>Donna Mather</u>	<u>Donna Mather</u>	<u>VOC</u>	<u>4/9/97</u>	<u>1330</u>