

The Flood Building 870 Market Street, Suite 712 San Francisco, CA 94102 (415) 986-3336 Fax (415) 986-3370 jck@javaherlanconsulting.com

August 22, 2000

MEMORANDUM

To:	Doug Oram, Ph.D.						
	ETIC Engineering, Inc.						

From: Mehrdad M. Javaherian, Ph.D., P.Hg., P.E., DABT Javaherian Consulting, Inc.

Re: Risk-Based Corrective Action Analysis Nestle USA, Inc. Facility 1310 14th Street, Oakland, CA

1.0 INTRODUCTION

14

15

This memorandum documents a risk-based corrective action (RBCA) analysis and associated conceptual site model (CSM) for the above referenced site (see Figure 1), focusing on protection of human health at and in the vicinity of the site. This analysis was based on RBCA guidelines outlined by the American Society for Testing and Materials (ASTM, 1995 and 1998), the US Environmental Protection Agency ([USEPA], 1991), and the California Environmental Protection Agency Department of Toxic Substance Control ([DTSC], 1999).

This RBCA analysis focuses on continued commercial/industrial land use at the site, with the purpose of determining potential health risks to future site occupants in the absence of continued remediation. The RBCA analysis is supplemented by proposed continued monitoring of groundwater quality focusing on determining the effectiveness of past remediation efforts and natural attenuation in the future (ETIC Engineering, Inc. ([ETIC], 2000a), together with an upcoming risk management plan (RMP) outlining measures for protection of construction workers, land use restrictions, and/or institutional controls for future use of the site.

Past investigations and associated site characterization data serving as the basis for this RBCA analysis have been compiled and summarized ETIC Engineering, Inc. ([ETIC], 2000b). This RBCA analysis makes direct references to results of past investigations documented by ETIC, (2000b), with tabular summaries of specific data used for risk calculations included herein.

2.0 CONCEPTUAL SITE MODEL

As the initial step in evaluation of health risks resulting from potential exposure to contaminants at the site, a conceptual site model (CSM) of chemical occurrence, fate, transport, and potential exposure was developed. Specifically, the CSM documents sources of chemicals, affected media and transport mechanisms, and potential exposure pathways and

Risk Assessment & Toxicology • Environmental Modeling Water Resource Development & Management www.javaherianconsulting.com



receptors at the site. Development of the CSM was based on available information characterizing land use and hydrogeologic conditions, together with soil gas, soil matrix, and groundwater quality data summarized by ETIC (2000b). Figure 2 is a graphical representation of the CSM, which is comprised of the components summarized below.

2.1 Sources of Chemicals

Historical site investigations have identified the subsurface presence of chemicals consistent with those used at the site (see Appendix I). Occurrence of chemicals in soil and groundwater underlying the site is likely due to historical spills and releases associated with former underground storage tanks (USTs) and dust control operations, which utilized used oil. No primary sources in the form of on-going leaks and/or spills are known to exist at the site, with USTs and associated piping and dispensers removed in 1988 and 1989 (ETIC, 2000b). The presence of residual non-aqueous phase liquids (NAPLs) and impacted soils and groundwater serve as potential secondary sources of chemicals. To address secondary sources, remedial efforts at the site have included soil excavation, NAPL skimming, soil vapor extraction, and multi-phase extraction activities. Details of remedial actions are summarized by ETIC (2000b).

2.2 Affected Media and Transport Mechanisms

Review of historical investigation results indicates the presence of petroleum hydrocarbons and volatile organic compounds (VOCs) in surface soils (<4 ft below ground surface [bgs]), subsurface soils (>4 ft bgs), and groundwater (see Figures 10 through 21 of ETIC, 2000b). Impacted groundwater is a result of historical dissolution and leaching of chemicals through soils and NAPL migration to the water table. Due to the volatile nature of various chemicals released at the site, soil vapor underlying the site has also been impacted (see Appendix I). Offsite migration of chemicals in groundwater appears limited to the immediate vicinity of the site (see Figures 16 through 18 of ETIC, 2000b). This is due in part to the limited groundwater velocity (0.1 to 1 ft/day) estimated at the site (Harding Lawson Associates [HLA], 1991).

2.3 Land and Groundwater Use

14

11

.....

1.7

1

-

,

ŝ.

7

٤

养

i

STITLE OF

Historical land use at the site has been limited to industrial use. Plans for future property development involve continued industrial/commercial land use (ETIC, 2000b). While much of the area surrounding the site is characterized by industrial land use, a residential building is located approximately 100 feet hydraulically downgradient of the site.

Review of available data indicates that no water supply wells are present at or within a one-mile radius of the site. This finding is based in part on results of two door-to-door well surveys performed in March 1999 and March 2000 (ETIC, 1999 and 2000c). Given the low permeability fine-grained sediments, combined with the limited saturated thickness of the waterbearing formation underlying the site, development of potable water supplies at and in the vicinity of the site is highly unlikely. Furthermore, potential water supply development would likely be limited to deeper water-bearing units, as opposed to the shallow unit impacted by past site operations.

2.4 Potential Exposure Pathways and Receptors

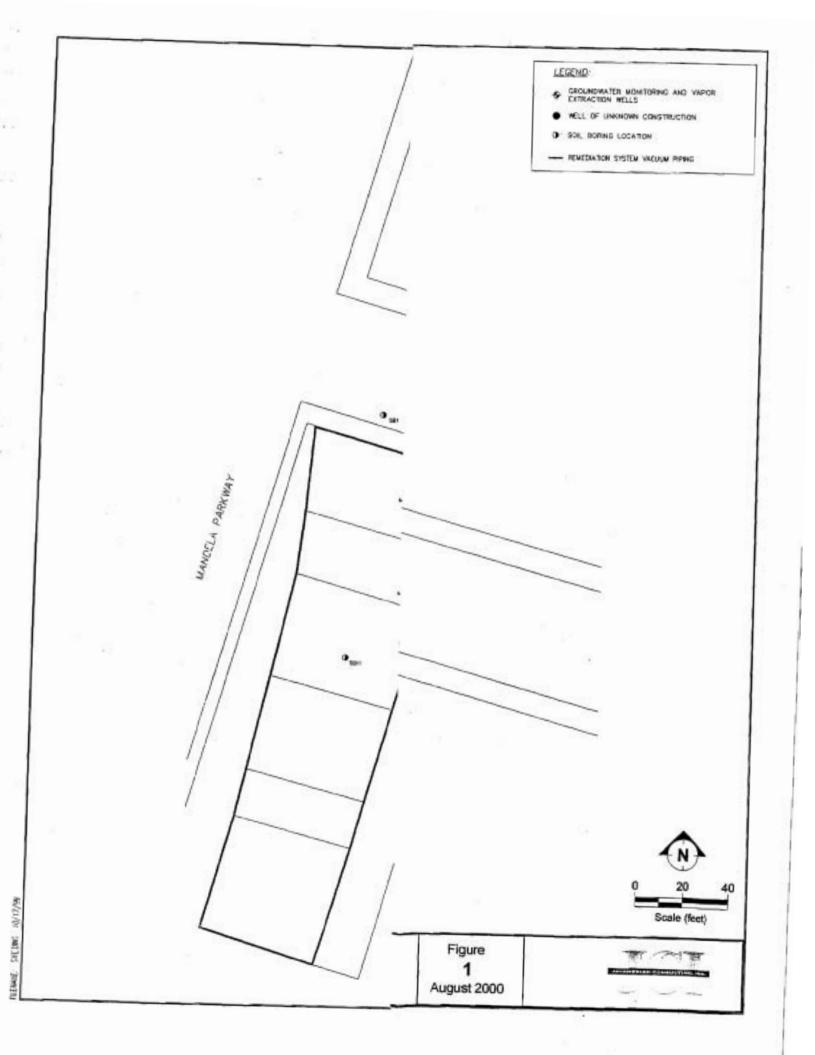
Potential exposure pathways and receptors (exposure scenarios) were evaluated based on the previously defined sources of chemicals, affected media, transport mechanisms, and land use at and in the vicinity of the site. This analysis accounted for the four principal elements of an exposure pathway:

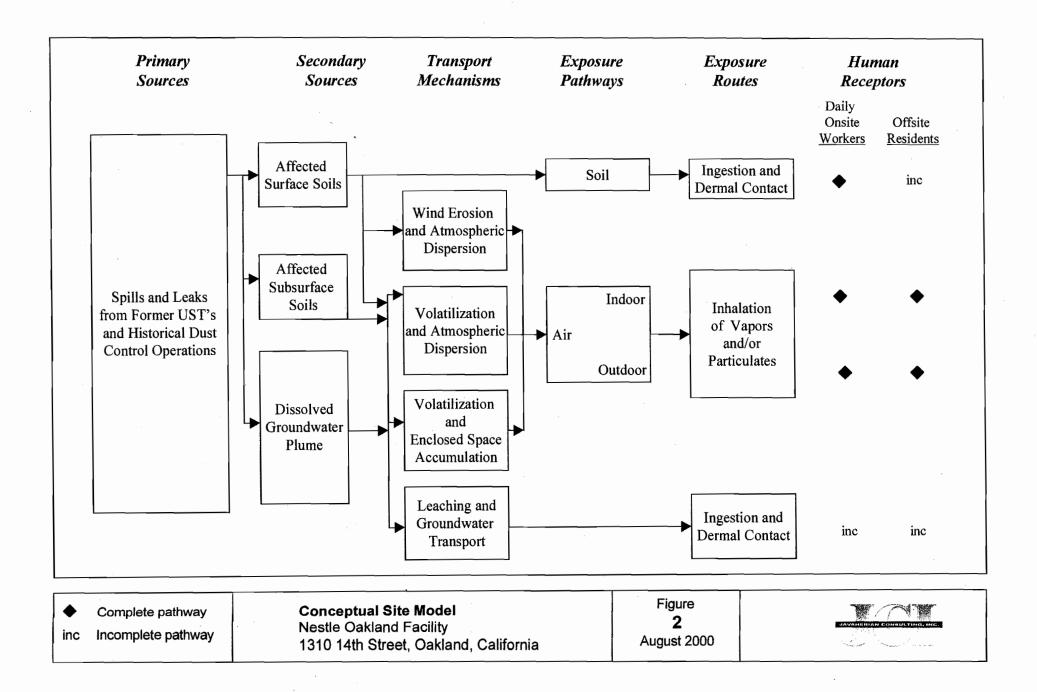
1) a source and mechanism of chemical release;

2) one or more retention or transport media (e.g., soil, groundwater, and/or air);

3) a point of potential contact with the contaminated medium (referred to as the exposure point); and

4) an exposure route at the point of contact (e.g., inhalation, ingestion, or dermal contact).







Analysis of exposure pathways links sources, locations, and types of environmental releases with population locations and activity patterns, in order to establish significant and complete exposure pathways. Based on available data, analysis of exposure pathways for human receptors at and in the vicinity of the site is summarized below.

Because of the current presence of a paved surface throughout the site, direct exposure of site occupants to surface soils (<4 ft bgs) and associated contaminants is not likely. Future site development plans (industrial/commercial use) indicate the presence of a paved surface throughout much of the site, with some unpaved areas (ETIC, 2000b). Accordingly, future site occupants may potentially be exposed to chemicals in surface soils within unpaved areas. Direct exposure to soils may occur via ingestion, inhalation, and dermal contact.

Based on the presence of volatile chemicals in soil and groundwater underlying the site, daily onsite industrial/commercial workers may be subject to inhalation of contaminated vapor emissions to outdoor and/or indoor air. Exposure of offsite downwind receptors to vapor emissions from the site is assumed negligible, since the magnitude of risk-based screening levels associated with the inhalation route of exposure will be governed by the larger intake associated with onsite receptors.

Based on the depth to the water table of the shallow aquifer (approximately 5 to 7 feet below ground surface) and absence of potential drinking water sources at and in the vicinity of the site, direct exposure to groundwater at on- and offsite locations is assumed incomplete. Chemical concentrations in groundwater have historically remained at low levels in downgradient monitoring wells immediately adjacent to the site (ETIC, 2000b). As a result, indirect exposure (inhalation of volatiles from groundwater) of nearby residents to chemicals in offsite groundwater is considered insignificant. Nevertheless, this pathway was assumed complete and conservatively evaluated based on potential volatilization of chemicals (to outdoor and indoor air) detected in groundwater at offsite locations.

Review of soil quality data (Appendix I) indicates sporadic detection of chemicals at low levels in unsaturated soils. The higher soil detections are limited to saturated or capillary fringe soils near the water table (approximately 5 ft bgs), where residual NAPLs may be present. The absence of measurable soil contamination above the water table is consistent with historical date of releases and remediation activities, suggesting that soil leaching to groundwater in the future is not a significant release mechanism. This is further corroborated by the stability of chemical concentrations in groundwater (wells MW-28 and MW-29) at offsite locations. Hence, potential (on- and offsite) indirect exposure to chemicals subject to leaching to groundwater in the future was considered negligible. As mentioned above, potential indirect exposure of offsite receptors to chemicals emanating from the site was accounted for through evaluation of exposure to chemicals currently (and historically) detected in groundwater at offsite locations.

Future construction work at the site may also result in exposure of construction workers to chemicals in soil and groundwater. Consistent with RWQCB practice, this risk will be addressed through the RMP for the site, outlining risk management practices and appropriate health and safety measures necessary prior to initiation of construction at the site.

To summarize, the following exposure scenarios corresponding to relevant human receptors were assumed complete in this RBCA analysis:

- Ingestion, inhalation, and dermal contact with surface soils (on-site industrial/commercial worker);
- inhalation of volatile emissions from subsurface soils and groundwater to indoor air (on-site industrial/commercial worker);
- inhalation of volatile emissions from subsurface soils and groundwater to outdoor air (on-site industrial/commercial worker);
- inhalation of volatile emissions from groundwater to indoor air (off-site residents); and
- inhalation of volatile emissions from groundwater to outdoor air (off-site residents).

1.2

¥ B

с. 1 ш

1

222

3.0 RISK-BASED CORRECTIVE ACTION ANALYSIS

Making use of available site characterization data, a RBCA analysis based on ASTM (1995 and 1998) USEPA (1991), and DTSC (1999) guidelines was performed. The RBCA process is the integration of site assessment, remedial action selection, and monitoring with USEPA-recommended risk and exposure assessment practices. This creates a process by which corrective action decisions are made in a consistent manner that is protective of human health and the environment.

3.1 Tier I RBCA Input Data

State of

Consistent with the tiered approach adopted by the ASTM RBCA guidelines, the initial attempt at evaluating the risk associated with potential exposure to chemicals emanating from the site was based on a Tier I evaluation. As outlined in ASTM (1995 and 1998), the Tier I evaluation involves comparison of the site-specific chemical source concentrations to highly conservative, generic Risk-Based Screening Levels (RBSLs) based on simplified chemical transport and exposure equations. These algorithms are supplemented by generalized site conditions conservatively represented by default data adopted by ASTM (1995 and 1998). All Tier I input data are included as Appendix II. Chemical-specific toxicity data and chemical-physical properties are included as Appendix III.

For each exposure scenario, chemicals of potential concern (COPCs) and media-specific source concentrations were identified based on available soil matrix, soil vapor, and groundwater quality data. Hydrocarbon fuel mixtures (i.e. total petroleum hydrocarbons [TPH] as gasoline [TPH-g] and as diesel [TPH-d]) were included as COPCs, with risks quantified based on the approach outlined by the Massachusetts Department of Environmental Protection ([MDEP] 1994), The rationale behind selection of COPCs and associated source concentrations for each exposure scenario is summarized below.

3.1.1 Inhalation, Ingestion, and Dermal Contact with Soils-Onsite Commercial/Industrial Receptor: For evaluation of direct exposure to chemicals in onsite soils, all chemicals detected in surface soils (<4 ft bgs) were included as COPCs (see Appendix I). As a conservative measure, selection of COPC soil source concentrations focused on historical maximum chemical levels detected in surface soil (see Table 1). Specifically, maximum chemical concentrations in soil samples collected from <4 feet bgs were used to represent soil quality in surface soils. Sample locations are depicted on Figure 1.

COPC	Sample ID	COPC Source Concentration* (mg/kg)
1,2-Dichloroethane (1,2-DCA)	SB13	2.50E-03
Ethylbenzene	SB13	2.70E-03
Toluene	SB13	2.00E-03
Xylenes	SB13	2.70E-03
TPH-g	SB13	6.30E-01
TPH-d	SB13	3.90E+02

Table 1. Chemicals of Potential Concern and Source Concentrations Direct Exposure to Surface Soils Onsite Commercial/Industrial Receptor

* Concentrations represent historical maximum values in shallow (<4 ft bgs) soil samples

3.1.2 Outdoor and Indoor Air Inhalation of Volatiles from Soils and Groundwater-Onsite Commercial/Industrial Receptor: For evaluation of indirect exposure to chemicals in soils and groundwater, shallow (3 ft bgs) soil vapor quality data within the footprint of contaminated soils and groundwater plumes (see Figure 26 of ETIC, 2000b) were used as representative of COPC source concentrations (Appendix I). Soil vapor concentrations at 3 feet bgs correspond to vapor contribution from all potential subsurface sources, including residual NAPLs, soils, and groundwater. Hence, risk estimates using soil vapor quality data represent total pathway risks to indoor and outdoor receptors from combined soil and groundwater sources. Use of soil vapor data in risk assessments is acknowledged by the USEPA (1989), DTSC (1994, 1999), GSI (1995 and 1997), and the California Regional Water Quality Control Board San Francisco Bay Region



(RWQCB, 1999). The method and rationale behind collection of soil gas samples at the site are summarized by ETIC (2000a and 2000b).

As a result of using soil vapor quality data, chemicals detected in shallow soil vapor samples were included as COPCs, with their maximum detected concentrations used as representative of source levels in vapor phase (see Table 2).

Table 2. Chemicals of Potential Concern and Source Concentrations Volatilization to Outdoor and Indoor Air Pathways Onsite Commercial/Industrial Receptor

COPC	Sample ID	COPC Source Concentration* (ppbv)
Benzene	SB3	9,900
Toluene	SB3 (dup)	240
Ethylbenzene	SB3	68
Total Xylenes	SB12	610
Methyl t-butyl ether	SB14	2.9
TPH-g	SB12	750,000
Acetone	SB2	260
1,3-Butadiene	SB5	61
2-Butanone	SB2	24
Carbon Disulfide	SB5	18
Chloroform	SB2	. 3.9
Chloromethane	SB11	3.7
1,2-Dichlorobenzene	SB12	480
1,4-Dichlorobenzene	SB12	76
1,4-Dioxane	SB11	22
Hexane	SB12	18,000
4-Methyl-2-pentanone	SB4	15
Methylene chloride	SB4	340
Styrene	SB2	3
Tetrachloroethene	SB4	160
Tetrahydrofuran	SB13	58
1,1,1-Trichloroethane	SB4	21
1,3,5-Trimethylbenzene	SB12	740
1,2,4-Trimethylbenzene	SB12	580

* Concentrations represent historical maximum values in shallow (3 ft bgs) soil vapor samples

dup = Concentration detected in duplicate sample

k

This list of COPCs represents a larger number of chemicals than those encountered in soil matrix and groundwater beneath the site. Due to the absence of data characterizing chemical toxicity and physical/chemical properties, eight chemicals (Cyclohexane, Ethanol, 4-Ethyltoluene, Freon 11, Freon 12, Freon 113, Heptane, and 2-Propanol) detected in soil vapor samples were excluded as COPCs; however, detection of most of these chemicals was limited in frequency and magnitude (see Appendix I). The limited presence of these chemicals is corroborated by their absence at above detection limits in soil matrix and groundwater samples across the site.

3.1.3 Outdoor and Indoor Air Inhalation of Volatiles from Groundwater-Offsite Residential Receptor: For evaluation of potential indirect exposure to chemicals in groundwater at the nearest (100 ft downgradient) residential property, chemicals detected over the past two years in offsite monitoring wells MW-28 and MW-29 (see Figure 1) located approximately 50 ft downgradient of the site were included as COPCs (see Appendix I). As a conservative measure, historical maximum concentrations of these COPCs (Table 3) were used as representative of source concentrations.



COPC	Sample ID	COPC Source Concentration* (mg/l)
Benzene	MW-28	1.80E-02
1,1 DCA	MW-29	8.70E-02
1,2 DCA	MW-28	1.70E-01
cis-1,2 DCE	MW-29	2.30E-03
Ethylbenzene	MW-28	2.20E-03
MTBE	MW-28	5.60E-02
Toluene		2.00E-02
TCE	MW-29	1.90E-03
Xylenes	MW-28	1.30E-02

Table 3. Chemicals of Potential Concern and Source ConcentrationsVolatilization to Outdoor and Indoor Air Pathways Offsite Residential Receptor

* Concentrations represent historical maximum values in groundwater at offsite monitoring wells MW-28 and MW-29

The basis for using data from these wells as a conservative representation of potential future COPC concentrations at offsite locations include:

- 1. stability of the groundwater plume with respect to offsite migration;
- 2. consistent presence of COPCs at residual levels (i.e. at or below detection levels) in wells MW-28 and MW-29 over the (7-year) period of record (see Appendix I);
- 3. conservative omission of additional attenuation between the offsite wells and the nearest residential building.

Quarterly monitoring of groundwater quality at MW-28 and MW-29 has been conducted for over 7 years, yielding COPC levels at or around detection limits throughout the monitoring period (see Appendix I). Accordingly, data from these wells and farther downgradient wells CC-1 and CC-2 (see Figure 1) have been used to represent the downgradient extent of COPC plumes in groundwater underlying the site. Comparatively, historical operations at the site date back to 1929 through 1991, with groundwater contamination initially encountered in 1989. Based on estimated groundwater seepage velocities of 0.1 to 1 ft per day (HLA, 1991) and the absence of hydraulic control at the site, quarterly data collected over the past 7 years at MW-28 and MW-29 reflect the stability of the groundwater plume with respect to offsite migration. Hence, use of these data as representative of the offsite presence of chemicals is considered conservative in that it ignores further attenuation in groundwater between monitored locations and potential offsite receptors located 100 to 200 feet downgradient of the site. The occurrence of this attenuation is corroborated by the absence of COPC detections in further downgradient monitoring well CC-1 and sporadic detections at residual levels in monitoring well CC-2.

3.2 Tier I RBCA Results

教授

繄

ţ.

4 10

i.

ġ.

TANK.

Country of

COPCs, media-specific concentrations, and ASTM (1995) default input data were incorporated into the highly conservative ASTM (1995) exposure algorithms, yielding Tier I RBSLs corresponding to target risk and hazard levels of 1×10^6 and 1.0, respectively. Tier I output data, including sample calculations using soil vapor data, are included as Appendix IV and are summarized below. Calculation of RBSLs for TPH is summarized in Appendix V. Table 4 depicts a comparison of highly conservative Tier I RBSLs with COPC source concentrations for direct exposure of daily site occupants to chemicals in surface (<4 ft bgs) soils. As indicated in Table 4, source concentrations for all COPCs are protective of the highly conservative Tier I RBSLs for direct exposure to surface soils.



Table 4.	Tier I Results for Direct Exposure to Surface Soils
	Onsite Commercial/Industrial Receptor

COPC	COPC Source Concentration (mg/kg)	Tier I RBSLs * (mg/kg)
1,2 DCA	2.50E-03	1
Ethylbenzene	2.70E-03	3,400**
Toluene	2.00E-03	6,400**
Xylenes	2.70E-03	66,000**
TPH-g	6.30E-01	1,400
TPH-d	3.90E+02	1,600

*: RBSL corresponds to lower endpoint of target risk and hazard levels of 1 x 10⁻⁶ and 1.0, respectively

**: RBSL is greater than constituent residual saturation in soil

17

÷.

2 ŝ

> 2 1

È

Contraction of the

10.66

Tables 5 depicts a comparison of the highly conservative Tier I RBSLs with COPC source concentrations for indirect exposure of daily onsite receptors to vapor emissions to outdoor air.

COPC	COPC Source Concentration (ppby)	Tier I RBSLs* (ppby)	Carcinogenic Risk	Non-Carcinogenic Hazard	
Benzene	9.9E+03	1.7E+04	5.90E-07	9.80E-03	
Toluene	240	6.2E+07		3.90E-06	
Ethylbenzene	68	1.5E+08	-	4.40E-07	
Total Xylenes	610	1.1E+08	-	5.50E-06	
Methyl t-butyl ether	2.9	1.1E+07	2.50E-13	5.20E-09	
COPCConcentration (ppbv)(ppbv)Benzene9.9E+031.7E+04Toluene2406.2E+07Ethylbenzene681.5E+08Total Xylenes6101.1E+08Methyl t-butyl ether2.91.1E+07TPH-g7.5E+051.5E+06Acetone2605.8E+07		1.5E+06	-	5.0E-01	
	260	5.8E+07	-	4.50E-06	
1,3-Butadiene	61	7.1E+03	8.60E-09	-	
2-Butanone	24	2.0E+08		1.20E-07	
Carbon Disulfide	18	1.1E+08		1.60E-07	
Chloroform	3.9	1.2E+04	3.20E-10	1.30E-04	
Chloromethane	3.7	2.3E+04	1.60E-10	6.50E-08	
1,2-Dichlorobenzene	480	2.4E+07	-	2.00E-05	
1,4-Dichlorobenzene	76	3.0E+04	2.50E-09	5.90E-06	
1,4-Dioxane	22	2.5E+06	8.70E-12	-	
Hexane	1.8E+04	1.4E+07	_	1.30E-03	
4-Methyl-2-pentanone	15	1.4E+07	-	1.10E-06	
Methylene chloride	340	4.1E+05	8.40E-10	7.80E-07	
Styrene	3 🔩	1.7E+08	-	1.80E-08	
Tetrachloroethene	160	4.8E+04	3.30E-09	4.00E-06	
Tetrahydrofuran	58	2.5E+05	2.30E-10	1.10E-06	
International381,1,1-Trichloroethane21		1.2E+08	-	1.80E-07	
1,3,5-Trimethylbenzene	740	2.5E+08	-	3.00E-06	
1,2,4-Trimethylbenzene	580	1.4E+09		4.10E-07	
Tot	al Pathway Risk/Hazard:		6.06E-07	5.11E-01	

Table 5. Tier I Results Volatilization-to-Outdoor Air Pathway **Onsite Commercial/Industrial Receptor**

*: RBSL corresponds to lower endpoint of target risk and hazard levels of 1 x 10⁻⁶ and 1.0, respectively

9

As previously indicated, this analysis made use of maximum detected soil vapor concentrations as representative of vapor contribution from all potential subsurface sources (i.e. residual NAPL, soil, and groundwater). Hence, RBSLs represent soil vapor concentrations at 3 ft bgs (see Appendix IV), corresponding to target risk/hazard levels of 1×10^{-6} and 1.0, respectively.

Due to the quantity of COPCs detected in soil vapor, individual and total pathway risks/hazards were also quantified (see Table 5) to represent potential cumulative impacts. As indicated in Table 5, soil vapor concentrations for all COPCs are protective of the highly conservative Tier I RBSLs. In addition, total pathway (i.e. cumulative) risk/hazard estimates remain protective of the target risk/hazard of 1×10^{-6} and 1.0, respectively.

Table 6 provides a comparison between the highly conservative Tier I RBSLs and COPC source concentrations for indoor air inhalation of vapors associated with daily onsite receptors.

COPC	COPC Source Concentration* (ppbv)	Tier I RBSLs* (ppbv)	Carcinogenic Risk	Non-Carcinogenic Hazard			
Benzene	9,900	660	1.50E-05	2.40E-01			
Toluene	240	2.4E+06	-	9.80E-05			
Ethylbenzene	68	6.2E+06	-	1.10E-05			
Total Xylenes	610	4.4E+06	. –	1.40E-04			
Methyl t-butyl ether	2.9	4.6E+05	6.30E-12	1.30E-07			
TPH-g	7.5E+05	6.5E+04	-	1.15E+01			
Acetone	260	2.4E+06	-	1.10E-04			
1,3-Butadiene	61	2.9E+02	2.10E-07	- ,			
2-Butanone	24	8.3E+06	-	2.90E-06			
Carbon Disulfide	18	4.4E+06	-	4.10E-06			
Chloroform	3.9	4.9E+02	7.90E-09	3.20E-03			
Chloromethane	3.7	1.2E+04	3.10E-10	1.60E-06			
1,2-Dichlorobenzene	480	9.4E+05	-	5.10E-04			
1,4-Dichlorobenzene	76	1.2E+03	6.30E-08	1.50E-04			
1,4-Dioxane	22	1.0E+05	2.20E-10				
Hexane	1.8E+04	5.6E+05	-	3.20E-02			
4-Methyl-2-pentanone	15	5.4E+05	-	2.80E-05			
Methylene chloride	340	1.6E+04	2.10E-08	1.90E-05			
Styrene	3	6.7E+06		4.50E-07			
Fetrachloroethene	160	1.9E+03	. 8.30E-09	1.00E-04			
Fetrahydrofuran	58	1.0E+04	5.70E-09	2.70E-05			
1,1,1-Trichloroethane	21	4.6E+06	-	4.60E-06			
,3,5-Trimethylbenzene	740	1.0E+07	-	7.40E-05			
1,2,4-Trimethylbenzene	580	5.8E+07		1.00E-05			
Total Path	way Risk/Hazard:	-	1.54E-05	1,17E+01			

Table 6. Tier I Results Volatilization-to-Indoor Air Pathway Onsite Commercial/Industrial Receptor

*: RBSL corresponds to lower endpoint of target risk and hazard levels of 1 x 10⁻⁶ and 1.0, respectively Bolded parameters indicate exceedance of RBSLs.



As indicated in Table 6, with the exception of the benzene and TPH-g, shallow soil vapor concentrations for all COPCs are protective of the highly conservative Tier I RBSLs for indoor air exposure. For the more stringent indoor air pathway, the carcinogenic risk and noncarcinogenic hazard for benzene approximate 1.5×10^{-5} and 0.24, respectively. The carcinogenic risk associated with benzene represents 98 percent of the total pathway risk. The noncarcinogenic hazard for TPH-g represents 98 percent of the total pathway hazard and results in exceedance of the target hazard level of 1.0. Accordingly, benzene and TPH-g volatilization to onsite indoor air was further evaluated in the Tier II analysis.

Table 7 depicts a comparison between highly conservative Tier I RBSLs and COPC concentrations for the groundwater volatilization-to-indoor air and outdoor air pathways for offsite residential receptors. As indicated, with the exception of benzene and 1,2-DCA volatilization-to-indoor air, all COPCs are protective of the highly conservative RBSLs for both indoor and outdoor air exposure pathways.

COPC	COPC Source Concentration (mg/l)	Tier I RBSLs* (mg/l) Groundwater Volatilization to Indoor Air	Tier I RBSLs* (mg/l) Groundwater Volatilization to Outdoor Air
Benzene	1.80E-02	7E-03	3.2
1,1 DCA	8.70E-02	21	11,000**
1,2 DCA	1.70E-01	2.20E-02	7.5
cis-1,2 DCE	2.30E-03	0.780	410**
Ethylbenzene	2.20E-03	77	37,000**
MTBE	5.60E-02	24	3,600
Toluene	2.00E-02	33	16,000**
TCE	1.90E-03	2.80E-02	8
Xylenes	1.30E-02	610**	290,000**

Table 7. Tier I Results Volatilization to Indoor and Outdoor Air Offsite Residential Receptor

*: RBSL corresponds to target risk and hazard levels of 1 x 10⁻⁶ and 1.0, respectively

**: RBSL is greater than constituent solubility in water

Bolded parameters indicate exceedance of RBSLs.

Based on the Tier I results, the following exposure scenarios were further evaluated in the Tier II analysis:

Benzene volatilization to indoor air from subsurface sources (Onsite commercial/industrial receptor);

TPH-g volatilization to indoor air from subsurface sources (Onsite commercial/industrial receptor); and

• Benzene and 1,2-DCA volatilization to indoor air from groundwater (Offsite residential receptor).

3.3 Tier II RBCA Input Data

Consistent with the ASTM guidelines, a Tier II analysis was performed on exposure scenarios and COPCs exceeding the highly conservative Tier I RBSLs. Specifically, site-specific target levels (SSTLs) were calculated accounting for site-specific conditions, chemical attenuation between source and receptor locations, and relevant target risk levels.

As part of the Tier II analysis, the highly conservative vapor transport and exposure algorithms used in the Tier I analysis were maintained. The sole deviation from the Tier I analysis involved changes to select input data characterizing site conditions. These data, as summarized in Table 8, correspond to values adopted for the Oakland Urban Land Redevelopment Program Tier I Risk-Based Screening Levels (Spence and Gomez, 1997 and 1999), and accordingly maintain significant conservatism. All other input data were maintained from the Tier I analysis (see Appendix II).

Parameter	Value	Reference
Depth to groundwater	7 ft	Site specific value
Capillary fringe thickness	2 ft	Default value for mixed sediments (Spence and Gomez, 1997 and 1999)
Vadose zone thickness	5 ft	Back-calculated from capillary fringe thickness and depth to groundwater
Soil porosity	0.4	Default value for mixed sediments (Spence and Gomez, 1997 and 1999)
Vadose zone water content	0.25	Default value for mixed sediments (Spence and Gomez, 1997 and 1999)
Vadose zone air content	0.15	Default value for mixed sediments (Spence and Gomez, 1997 and 1999)
Capillary fringe water content	0.38	Default value for mixed sediments (Spence and Gomez, 1997 and 1999)
Capillary fringe air content	0.02	Default value for mixed sediments (Spence and Gomez, 1997 and 1999)
Building air exchange rate	0.00056/s	Default value for Oakland (Spence and Gomez, 1999)
Foundation crack fraction	0.001	Default value (Spence and Gomez, 1997 and 1999)

Table 8. Tier II Input Data

3.4 Tier II RBCA Results

く名崩

Tier II output data are included as Appendix VI, including sample calculation for Tier II SSTLs using soil gas data. SSTL development for TPH-g is summarized in Appendix V. Results of the Tier II analysis are summarized in Table 9. As indicated in Table 9, Tier II COPC source concentrations are protective of SSTLs for both on- and offsite receptors.

Exposure Scenario	COPC	COPC Source Concentration	Tier II SSTL
Volatilization to Indoor Air-Onsite			
Commercial/Industrial Receptor	Benzene	9,900 ppbv	43,800 ppbv
Volatilization to Indoor Air-Onsite			
Commercial/Industrial Receptor	TPH-g	750,000 ppbv	4,000,000 ppbv
Volatilization to Indoor Air-Offsite		***************************************	
Residential Receptor	Benzene	0.018 mg/l	1.10 mg/l
Volatilization to Indoor Air-Offsite			
Residential Receptor	1,2 - DCA	0.170 mg/l	3.90 mg/l

Table 9. Tier II RBCA Results

3.5 Uncertainty Analysis

The assumptions, procedures, and parameters used in this RBCA analysis are subject to various degrees of uncertainty. To this end, conservative assumptions are incorporated into the RBCA process to ensure protection of human health, as documented herein. Specifically, uncertainty and conservatism associated with sample collection and analysis, fate and transport calculations, representation of site conditions, standard exposure factors, toxicological endpoints, and interpretation of target risk levels are documented below.

12



3.5.1 Sample Collection and Analysis: Environmental sampling and analysis error can stem from improper sample collection and handling procedures, inadequate sample numbers, laboratory analysis errors, and the heterogeneity of the subsurface environment. The use of standard techniques such as the collection of duplicates, and the use of trip and method blanks can be used to reduce the likelihood of errors. Errors in data analyses can occur from the simplest tabulation and typographical errors to complex interpretational errors. Matrix interference due to the presence of high concentrations often raise the detection limits of other chemicals in the analytical procedure and introduce uncertainty in the method of data analyses.

The sampling effort implemented at the Nestle site was specifically designed to identify areas that were suspected to have elevated chemical concentrations. This sampling bias resulted in a data base that focused on the worst-case areas of the site. This focused approach resulted in assumptions related to representation of COPC concentrations that make this RBCA analysis conservative in nature. These conditions will result in a significant overestimation of risk and excessively low RBSLs and SSTLs.

3.5.2 ASTM RBCA Fate and Transport Algorithms: The ASTM guidelines and the GSI RBCA Spreadsheet System used in this analysis employ a series of simplified fate and transport models for predicting COPC concentrations at points of exposure. The simplified analytic nature of these models, particularly those used to simulate volatilization and transport of vapor emissions to outdoor and indoor air, often result in grossly over-estimated COPC exposure point concentrations (Sanders and Stern, 1994; GSI, 1995 and 1997; AEHS, 1997; Javaherian, 1994 and 1997); in turn, these result in over-estimation of health risks and lower RBSLs and SSTLs. In fact, GSI (1995 and 1997) warns against delineation of cleanup levels based on the use of its formulation for vapor intrusion to indoor air. Examples of physical and chemical processes ignored by the simplified GSI vapor transport models include:

- loss mechanisms- absence of loss mechanisms such as biodegradation and adsorption results in over-estimation of vapor and contaminant flux to outdoor and indoor air;
- depleting contaminant source- use of a non-depleting, constant source results in an unlimited supply of contaminated vapor and an over-estimation of vapor and contaminant flux to outdoor and indoor air over time; and
- water movement- absence of water movement through subsurface soils results in an over-estimation of air-filled porosity and vapor and contaminant flux to outdoor and indoor air.

3.5.3 Representation of Site Conditions: As part of the Tier I analysis, the ASTM RBCA process promotes the use of conservative default values for various parameters representing site conditions. This RBCA analysis consistently incorporated conservative assumptions for selection of input parameters, while attempting to maintain a reasonable, site-specific evaluation. Examples of conservative assumptions used to formulate input parameters include:

- On- and offsite buildings will directly overlie locations of historical maximum soil matrix, soil vapor, and groundwater concentrations;
- Cracks may exist in foundations of both onsite and offsite buildings;

÷ ù

17

1.5

i and

No.

, Å

ž

- The paved surface at the site has a negligible impact on vapor emissions to outdoor air;
- Historical maximum chemical concentrations in surface soil, soil vapor, and groundwater are representative of current and future source concentrations; and
- No chemical attenuation occurs in groundwater between the site and the location of the nearest offsite residential facility.

Use of these conservative assumptions results in an over-estimation of health risks and lower RBSLs and SSTLs.



3.5.4 Standard Exposure Factors: Standard exposure scenarios evaluated in this RBCA analysis incorporate the most likely site-specific exposure pathways and represent the greatest potential for exposure to contaminants at the site. Conservative assumptions consistent with state and federal guidelines were used to conceptualize the exposure scenarios. These methods and procedures contribute to an overall overestimation of potential exposure.

Numerous conservative exposure assumptions serve as the basis for exposure parameters adopted by ASTM (1995). Duration, frequency, and other input parameters were selected to represent the maximally exposed individual and are not an accurate portrayal of time spent at a place of business or residence. The quantitative effect of these uncertainties may be significant in overestimating overall potential health risk.

The exposure parameters used to develop the onsite indoor worker exposure scenarios at the site are conservative estimates of the true exposures. Although indoor workers are present at the site, the assumed duration of exposure is likely to be much greater than the true duration. For instance, an indoor onsite worker is assumed to be indoors 8-hours per day, 250-days per year, for 25 years. In reality, based on Department of Labor statistics regarding average job tenure nationwide, this type of worker would be expected to remain in his/her job less than 10 years.

Further, the hypothetical worker is assumed to be exposed to chemical emissions that were conservatively estimated from maximum reported soil and groundwater concentrations (e.g. Tier I analysis). Therefore, assuming exposure to air concentrations of COPCs based on maximum concentrations and using the conservative exposure parameters provided, the onsite indoor worker scenario significantly overestimates the true risk/hazard associated with site-related COPC emissions; this results in underestimation (i.e. lower) of RBSLs.

Likewise, the onsite outdoor worker is assumed to have the same exposure frequency and duration as the indoor worker. In reality, based on weather conditions alone, a worker will not be outdoors 250-days per year. For the same reasons documented above, a worker would not be expected to remain in his/her job for a 25-year duration. Consequently, the outdoor worker scenario also overestimates the true risk/hazard, while underestimating action levels associated with site-related COPC emissions.

à

3.5.5 Toxicological Endpoints: Several aspects of the toxicological data employed in the ASTM RBCA process contain a high degree of uncertainty that affect estimation of risk and delineation of SSTLs. These uncertainties arise in two primary areas: first, slope factors used in this assessment correspond to the 95% upper confidence limit (UCL) on the low-dose portion of the chemical's dose-response curve, as extrapolated from high-dose human or animal response data using the EPA linearized multistage model (LMS). This assumption means actual risks are likely to be lower than the risk estimates calculated in this assessment.

Second, results of animal studies are often used to predict the potential human health effects of a chemical. Extrapolation of toxicological data from animal tests is one of the largest sources of uncertainty in the human health risk evaluation process. There may be important, but unidentified differences in uptake, metabolism, distribution, and elimination of chemicals between a test species and humans. Animal studies are usually conducted under high-dose conditions, whereas humans are rarely exposed to such high doses. The dose level itself may be responsible for the observed carcinogenic effects. Also, animal lifetimes tend to be less than two years, while assumed human life expectancy is 70 years.

3.5.6 Interpretation of Target Risk Levels: The excess lifetime cancer risk used to evaluate carcinogenic compounds is often misunderstood. For example, a risk level of one-in-one million (1×10^{-6}) associated with exposure to a particular chemical is often misconstrued as an expectation that one out of one million people exposed to the chemical will be stricken with cancer. In actuality the carcinogenic risk is not an actual risk, but rather a mathematical risk based on conservative scientific assumptions used in the risk assessment process. The Food and Drug Administration (FDA) uses this conservative estimate to ensure that the risk is not understated.



Uncertainties from the various sources discussed above are additive; hence, the overall effect of using conservative assumptions in each step of the risk assessment process results in significant overestimation of potential risks/hazards, and an underestimation of action levels. Accordingly, comparison of COPC concentrations with applicable RBSLs must be viewed with an understanding of the uncertainty and conservatism involved, and how these effect risk estimations. Because of the high degree of conservatism associated with the RBCA process, findings of insignificant risk (high RBSLs) may reflect conditions close to reality; however, findings of measurable risk (low RBSLs) may reflect conditions that result from the conservative nature of the evaluation.

4.0 CONCLUSIONS

Based on the historical levels of chemicals in soil matrix, soil vapor, and groundwater at on- and offsite locations, together with results of this RBCA analysis, the following conclusions are formulated for the site:

- Risks/hazards associated with direct exposure of daily site (commercial/industrial) occupants to observed levels of chemicals in surface soils are protective of USEPA-defined target risk/hazard levels;
- Risks/hazards associated with onsite (commercial/industrial) indoor and outdoor air inhalation of volatiles detected in shallow soil vapor samples are protective of USEPA-defined target risk/hazard levels;
- Risks/hazards associated with offsite (residential) indoor and outdoor air inhalation of volatiles detected in groundwater at offsite locations are protective of USEPA-defined target risk/hazard levels;
- A risk management plan outlining appropriate risk management practices, health and safety measures, and deed restrictions should be developed prior to initiation of construction activities and redevelopment at the site.

5.0 REFERENCES

ι.

1 3

10 - A

1

. 19

.

Â.

Anon, 1994. Interim Final Petroleum Report: Development of Health-Based Alternative to the Total Petroleum Hydrocarbon Parameter. Prepared for the Bureau of Waste Site Cleanup, Massachusetts Department of Environmental Protection. August.

Agency for Toxic Substances and Disease Registry (ATSDR), 1993. Toxicological Profile for Polycyclic Aromatic Hydrocarbons (PAHs). Update. US Department of Health and Human Services.

ATSDR, 1994. Toxicological Profile for naphthalene. Draft Update. US Department of Health and Human Services.

Association for the Environmental Health of Soils (AEHS), 1997, Exposure Pathway Modeling for RBCA, 7th Annual West Coast Conference on Contaminated Soils and Groundwater. March.

American Petroleum Institute (API), 1993. APIDSS: Exposure/Risk Assessment Decision Framework for the Management of Subsurface Contaminants.

American Society for Testing and Materials (ASTM), 1995.Standard Guide for Risk-Based Corrective Action Applied at Petroleum Release Sites, E 1739-95.

ASTM, 1998. Standard Provisional Guide for Risk-Based Corrective Action, PS 104-98.

Bruya, J., and A. Friedman, 1992. Petroleum Hydrocarbons, What Are They? Friedman and Bruya, Inc., Seattle Washington.

California Department of Toxic Substance Control (DTSC), 1994. California Cancer Potency Factors: Update. Office of Environmental Health Hazard Assessment. State of California Environmental Protection Agency (Cal-EPA). November 1, 1994.

EMCON, 1995. Fractionation Approach for Assessing Risk from Petroleum Hydrocarbons (From Appendix B of the Ecological Risk Assessment for King Salmon Airport).

ETIC Engineering, Inc., 1999. Door-to-Door Wells Survey, Nestle USA Facility, 1310 14th Street, Oakland, CA, March 3.

ETIC, 2000a. Response to Comments from ACHA and RWQCB on Draft Risk Assessment for Nestle USA, Inc. Site, 1340 14th Street, Oakland, California, June 27th.

ETIC, 2000b. Comprehensive Site Characterization Report, Support for the Site as a Low-Risk Soil and Groundwater Case, Nestle USA Facility, 1310 14th Street, Oakland CA, October.

ETIC, 2000c. Door-to-Door Well Survey, Nestle USA Facility, 1310 14th Street, Oakland CA, March 22.

Gruse, W.A., and D.R. Stevens, 1960. The Chemical Technology of Petroleum.

Groundwater Services, Inc. (GSI), 1995. Tier I and Tier II RBCA Spreadsheet System, Version 1.0.

GSI, 1997. Tier I and Tier II RBCA Spreadsheet System, Version 1.01.

.

5 7

8

1

ş

, È

- 1929-S

÷.

.

- Javaherian, M.M., 1994. Evaluation of Unsaturated/Vadose Zone Models for Superfund Sites, Research and Development, USEPA Center for Subsurface Modeling Support.
- Javaherian, M.M., 1997. A Finite-Difference Model for Simulation of Contaminant Fate and Transport and Exposure Pathways Through the Vadose Zone, *Water Resources Research*.
- Massachusetts Department of Environmental Protection (MDEP), 1994. Interim Final Petroleum Report: Development of Health-Based Alternative to the Total Petroleum Hydrocarbon Parameter, August.

Millner, G.C., R.C. James, and A.C. Nye, 1992. Human Health-Based Soil Cleanup Guidelines for Diesel Fuel No. 2. Journ. of Soil Cont. 1(2).

Montgomery Watson, 1996. Fuel Action Level Development, US Army Corps of Engineers, The Presidio, San Francisco, CA.

Office of Environmental Health Hazard Assessment (OEHHA), 2000, Toxicity Criteria Database, California Environmental Protection Agency, on-line @ www.oehha.org/risk.html

Purdy, G.A., 1957. Petroleum: Prehistoric to Petrochemicals.

Regional Water Quality Control Board (RWQCB) San Francisco Bay Region, 1999. Personal communication with Dr. Ravi Arulanantham, November 2nd.

Sanders, P.F., and A.L. Stern, 1994, Calculation of Soil Cleanup Criteria for Carcinogenic Volatile Organic Compounds as Controlled by the Soil-to-Indoor Air Exposure Pathway, *Environ. Tox. and Chem.*, 12(8): 745-758.

Speight, J.G., 1980. The Chemistry and Technology of Petroleum.

Speight, J.G., 1991. The Chemistry and Technology of Petroleum, 2nd Edition.

Spence, L.R., and M. Gomez, 1997. Draft Tier I: Risk-Based Screening Levels, Oakland Urban Land Redevelopment Program, City of Oakland Environmental Services Division, Oakland, CA.

Spence, L.R., and M. Gomez, 1999. Tier I: Risk-Based Screening Levels, Oakland Urban Land Redevelopment Program, City of Oakland Environmental Services Division, Oakland, CA.

USEPA, 1989. Risk Assessment Guidance for Superfund (RAGS). Volume 1, Human Health Evaluation Manual (PartA). Office of Emergency and Remedial Response, Washington, D.C. EPA/540/1-89/002.

USEPA, 1990a. Guidance for Data Usability in Risk Assessment, Interim Final. EPA/540/G-90/008, Directive 9285.7-05. October.

USEPA, 1990b. Hazardous Waste Management System Toxicity Characteristics, Revisions 55 FR 11798-11863, Washington, D.C.

USEPA, 1991, Risk Assessment Guidance for Superfund, Volume I, Part C. Risk Evaluation of Remedial Alternatives, Interim, December.

USEPA, 1997, Health Effects Assessment Summary Tables (HEAST).

х.

5.4

5 B

1.

USEPA, 1999, Region 9 Preliminary Remediation Goals Chemical Toxicity Database, on-line @ www.epa.gov/region09/waste/sfund/prg/

USEPA, 2000, Integrated Risk Information System (IRIS), on-line database.

Appendix I

Soil Matrix, Soil Vapor, and Groundwater Quality Data

	í —	1	(ka)			A			NE	STLE US	<u>A FACILI</u>	TY, OAK	LAND, C.	A									
	<u> </u>	(µg	(KR)		(mg	/kg)									(µg/kg)		_						
Sample	1		Ethyi-	Total			Chloro-	C U = 1	~	1,2-Di-	1,3-Di-	1,4-Di-	1,1-Di-	1,2-Di-	1,1-Di-	cis-1,2-				Methyl	Tetra-	1,1,1-Tri-	Tri-
ID	Benzene	Tolucne	benzene	Xylenes	TPH-g	TPH-d		Chloro-	Chloro-	chloro-	chloro-	chioro-	chloro-	chloro-	chloro-	Dichloro-	Freen	Freon	Methylene	t-butyi	chloro-	chloro-	chloro-
SB1, 3.5-4.0	<1.3	<1.3	<1.3	<1.3	<0.13	1,200	<1.1	form	methane	benzene	benzene	benzene	ethane	ethane	ethene	ethene	11	12	Chloride	ether	ethene	ethane	ethene
SB1, 6.5-7.0	<1.0	<1.0	<1.0	<1.0	<0.10	<5.9	<0.8	<1.1 <0.8	<1.1	<1.1	<1.1	<1.1	<1.1	<1.1	<1.1	<1.1	<1.1	<1.1	<1.1	<1.3	<1.1	<1.1	<1.1
					0.10	-2.2	~0.0	~0, a	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8	<1.0	< 0.8	<0.8	<0.8
SB2, 3.5-4.0	<0.9	<0.9	<0.9	<0.9	<0.09	<5.6	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	-1.0	.1.0							
SB2, 6.5-7.0	<1.0	<1.0	<1.0	<1.0	<0.10	<5.9	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	1.0	<1.0 <1.0	<1.0	<1.0	<1.0	<1.0	<0.9	<1.0	<1.0	<1.0
SB3, 3.5-4.0	<1.0	<1.0	~1.0	-1.0	-0.10							110	-1.0	1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0
SB3, 6.5-7.0	11,000	190,080	<1.0 100.000	<i.0 460,000</i.0 	<0.10	<5.6	<0.7	<0.7	<0.7	<0.7	<0.7	<0.7	<0.7	0.7	<0.7	<0.7	<0.7	<0.7	<0.7	<1.0	<0.7	<0.7	<0.7
	11,000	190,080	100,000	400,000	6,160	<5.7	<0.7	<0.7	<0.7	<0.7	<0.7	<0.7	<0.7	1.8	<0.7	<0.7	<0.7	<0.7	<0.7	73	<0.7	<0.7	<0.7
SB4, 3.5-4.0	<1.0	<1.0	<1.0	<1.0	<0.10	<5.5	<0.7	<0.7	-0.7	-0 -								-0,1	-0.7	/5	-0.7	-0.7	~0.7
SB4, 6.5-7.0	82	8.5	7.3	13	0.55	94	<0.7	<0.7	<0.7 <0.8	<0.7	<0.7	<0.7	<0.7	<0.7	<0.7	<0.7	<0.7	<0.7	<0.7	<1.0	<0.7	<0.7	<0.7
					0.05	~	50.0	-0.0	<0.8	<0.8	<0.8	<0.8	<0.8	1.0	<0.8	<0.8	<0.8	<0.8	<0.8	<[.]	<0.8	< 0.8	<0.8
SB5, 3.5-4.0	<0.9	<0.9	<0.9	<0.9	<0.09	<5.5	<0.6	<0.6	<0.6	<0.6	<0.6	<0.6	<0.6	0.6	-0.6	~ ~ ~							
SB5, 6.5-7.0	<0.8	<0.8	<0,8	<0.8	<0.08	<5.9	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8	0.0	<0.6 <0.8	<0.6 <0.8	<0.6	<0.6	<0.6	<0.9	<0.6	<0.6	<0.6
SB6, 3.5-4.0	-10	-10											-0.0	0.7	<0.0	NU.8	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8
SB6, 6.5-7.0	<1.0 76,000	<1.0 490,000	<1.0	<1.0	<0.10	<5.5	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8	<1.0	<0.8	<0.8	<0.8
300, 0.2-7.0	70,000	490,000	170,000	990,000	10,100	1,100	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	430	<1.0	<1.0	<1.0	<1.0	<1.0	32	<0.8	<0.8	<0.8
SB7, 3.5-4.0	<1.0	<1.0	<1.0	<1.0	<0.10	<5.4	-0.0	-0.0										-110		52	-1.0	~1.0	-1.0
SB7, 6.5-7.0	<1.1	<1.1	<1.1	<1.1	<0.10	<5.8	<0.8 <0.9	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8	<1.0	<0.8	<0.8	<0.8
			-1.1	-1.1	50.11	. ~	CO.9	<0.9	<0.9	<0.9	<0.9	<0.9	<0.9	<0.9	<0.9	<0.9	<0.9	<0.9	<0.9	<1.1	<0.9	<0.9	<0.9
SB8, 3.5-4.0	<1.0	<1.0	<1.0	<1.0	<0.10	<5.6	<0.7	<0.7	<0.7	<0.7	<0.7	<0.7	-07	-0.7	-0.7								
SB8, 6.5-7,0	430	360	120	830	13	<5.8	<0.9	<0.9	<0.9	<0.9	<0.9	<0.9	<0.7 <0.9	<0.7 1.2	<0.7 <0.9	<0.7	<0.7	<0.7	<0.7	<1.0	<0.7	<0.7	<0.7
SB9, 3.5-4.0										-0.9	-0.2	50.5	~0.9	1.4	<0.9	<0.9	<0.9	<0.9	<0.9	22	<0.9	<0.9	<0.9
SB9, 6.5-7.0	<0.9 24	<0.9	<0.9	<0.9	<0.09	<5.6	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<0.9	<1.0	<1.0	<1.0
0.07, 0.3-7.9	24	<6.1	<6.1	<6.1	<0.61	<5.8	<1.1	<1.1	<1.1	<1.1	<1.1	<1.1	<1.1	<1.1	<1.1	<1.1	<1.1	<1.1	<1.1	<6.1	<1.1	<1.1	<1.1
SB10, 3.5-4.0	<0.9	<0.9	<0.9	<0.9	<0.09	<5.6	<0.8	<0.8	-0.8	-0.0	-0.0	-0.5									51.1	51.1	51.1
SB10, 6.5-7.0	<1.3	<1.3	<1.3	<1.3	<0.13	<6.4	<1.0	<1.0	<0.8 <1.0	<0.8 <1.0	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8	<0.9	<0.8	<0.8	<0.8
						-0.4	-1.0	~1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.3	<1.0	<1.0	<1.0
SB11, 3.5-4.0	<2.0	<2.0	<2.0	<2.0	<0.20	<5.5	<1.1	<1.1	<1.1	<1.1	<1.1	<1.1	<1.1	<1.1	<1.1	<1.1	<1.1						
SB11, 6.5-7.0	<1.1	<1.1	<i.i< td=""><td><1.i</td><td><0.11</td><td><5.7</td><td><1.0</td><td><1.0</td><td><1.0</td><td><1.0</td><td><1.0</td><td><1.0</td><td><1.0</td><td><1.0</td><td><1.0</td><td><1.0</td><td><1.1</td><td><1.1 <1.0</td><td><1.1</td><td><2.0</td><td><1.1</td><td><1.1</td><td><1.1</td></i.i<>	<1.i	<0.11	<5.7	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.1	<1.1 <1.0	<1.1	<2.0	<1.1	<1.1	<1.1
SB12, 3.5-4.0	<1.0	<1.0	~ 1 0												41.0	51.0	~1.0	~1.0	<1.0	<1.1	<1.0	<1.0	<1.0
SB12, 4.5-5.0	70	<1.0 32	<1.0	<1.0	<0.10	<5.5	<0.6	<0.6	<0.6	<0.6	<0.6	<0.6	<0.6	<0.6	<0.6	<0.6	<0.6	<0.6	<0.6	<1.0	<0.6	<0.6	<0.6
SB12, 6.5-7.0	<1.0	<).0	4,000 23	6,700 9.8	496	2,900	1.7	<0.9	<0.9	3,100	38	330	<0.9	<0.9	<0.9	<0.9	<0.9	<0.9	<0.9	14	<0.9	<0.9	<0.9
0.012, 0.0 7.0	-1.0	-1.0	23	9.0	2.25	60	<1.1	<1.1	<1.1	<1.1	<1.1	<1.1	<1.1	<1.1	<i.1< td=""><td><1.1</td><td><1.1</td><td><1.1</td><td><1.1</td><td>0.6</td><td><1.1</td><td><1.1</td><td><1.1</td></i.1<>	<1.1	<1.1	<1.1	<1.1	0.6	<1.1	<1.1	<1.1
SB13, 3.5-4.0	<1.2	2.0	2.7	2.7	0.63	390	<0.9	<0.9	<0.9	<0.9	<0.9	<0.9	-0.0										
SB13, 6.5-7.0	250	48	150	490	12	65	<1.4	<1.4	<1.4	<1.4	<1.4	<1.4	< 0.9	2.5	<0.9	<0.9	<0.9	<0.9	<0.9	<1.2	<0.9	<0.9	<0.9
0014 25 45									-1.7	21.4	1.4	-1.4	<1.4	1.4	<1.4	<1.4	<1.4	<1.4	<1.4	<5.5	<1.4	<1.4	<1.4
SB14, 3.5-4.0	<0.8	<0.8	<0.8	<0.8	<0.08	<5.5	<0.8	<0.8	<0.8	< 0.8	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8	<0.8	~0.8	<0.9	-0.9	-0.8
SB14, 6.5-7.0	560	290	330	1,700	28.5	450	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	<1.0	9.7	<1.0	<1.0	<1.0	<1.0	<0.8	<0.8 84	<0.8 <1.0	<0.8 <1.0	8.0> 0.1>
SB15, 3,5-4.0	<5,4	<5,4	<5.4	<5.4	<0.51	140		~	~ .								-1.0	-1.0	51.0	0.4	-1.0	×1.0	~1.0
SB15, 6.5-7.0	<6.1	12	<6.1	< 5.4 8.5	<0.5} <0.57	140 81	<9.1 <9.8	<9.1 <9.8	<9.1	<9.1	<9.1	<9.1	<9.1	<9.1	<9.1	<9.1	<9.1	<9.1	<9.1	<5.4	<9.1	<9.1	<9.1
, , , , , , , , , , , , , , , , , , , ,	J.1		-0.1	0.3	NC.37	60	-9.8	< 9,8	<9.8	<9.8	<9.8	<9.8	<9.8	<9.8	<9.8	<9.8	<9,8	<9.8	<9.8	<6.1	<9.8	<9.8	<9.8

À.

Table I.1. Concentrations of Volatile Organic Compounds in Soil Samples, 12-13 AUGUST 1999

Notes:

µg/kg mg/kg NA TPH-g TPH-d

Micrograms per kilogram. Milligrams per kilogram. Not analyzed. Total Petroleum Hydrocarbons as gasoline. Total Petroleum Hydrocarbons as dicsel.

Table I.2. Concentrations of Volatile Organic Comopunds in Soil Vapor Samples, 12-13 AUG	UST 1999
NESTLE USE FACILITY, OAKLAND, CA	

5\$\$ THE

10,40

Sample			Ethyl-	Total			1,3-Bu-	2-Bu-	Carbon	Chloro-	Chloro-	Chloro-	Cyclo-	1,2-Di- chloro-	1,3-Di- chloro-	1,4-Di- chloro-	1,1-Di- chloro-	1,2-Di- chloro-	1,1-Di- chloro-	cis-1,2- Dichloro-
ID	Benzene	Toluene	benzene	Xylenes	TPH-g	Acetone	tadiene	tanone	Disulfide	benzene	form	methane	hexane	benzene	benzene	benzene	ethane	ethane	ethene	ethene
SB1, 3'	4.3	3.1	<0.65	2.74	800	77 a	2.8	13	6.2	<0.65	<0.65	<0.65	<2.6	<0.65	<0.65	0.77	<0.65	<0.65	<0.65	<0.65
SB2, 3'	7.5	12	3.6	17.6	1190	260 a	<2.7	24	9.0	<0.67	3.9	<0.67	12	<0.67	<0.67	1.8	<0.67	<0.67	<0.67	<0.67
SB3, 3'	9,900	230	68	67	36000	<190	<190	<190	<190	<48	<48	<48	<190	<48	<48	<48	<48	<48	<48	<48
SB3, 3' dup	9,500	240	<140	<140	40000	<580	<580	<580	<580	<140	<140	<140	<580	<140	<140	<140	<140	< 1 40	<140	<140
SB4, 3'	1,200	76	8.1	18.7	4600	200 a	19	<14	<14	<3.5	<3.5	<3.5	32	<3.5	<3.5	<3.5	<3.5	<3.5	<3.5	<3.5
SB5, 3'	7.6	5.6	0.80	1.9	1900	45 a	61	12	18	<0.71	<0.71	0.77	8.2	<0.71	<0.71	<0.71	<0.71	<0.71	<0.71	<0.71
SB6, 3'	3.0	4.2	<0.68	2.52	560	11 a	<2.7	4.0	<2.7	<0.68	<0.68	<0.68	<2.7	<0.68	<0.68	<0.68	<0.68	<0.68	<0.68	<0.68
SB7, 3'	5.9	6.2	0.87	4.3	780	43 a	3.4	7.9	3.3	<0.73	<0.73	<0.73	5.1	<0.73	<0.73	2.0	<0.73	<0.73	<0.73	<0.73
SB8, 3'	10	12	3.8	15.7	1300	42 a	<11	<11	<11	<2.8	<2.8	<2.8	<11	<2.8	<2.8	<2.8	<2.8	<2.8	<2.8	<2.8
SB9, 3'	12	18	1.7	9.9	690	19 a	<2.7	6.0	<2.7	<0.68	1.1	<0.68	4.9	<0.68	<0.68	<0.68	<0.68	<0.68	<0.68	<0.68
SB10, 3'	3.5	2.8	<0.80	1.7	610	39 a	<3.2	9.7	<3.2	<0.80	1.6	<0.80	<3.2	<0.80	<0.80	<0.80	<0.80	<0.80	<0.80	<0.80
SB11, 3'	2.7	1.9	<0.82	0.91	520	38 a	<3.3	9.9	<3.3	<0.82	<0.82	3.7	<3.3	<0.82	<0.82	<0.82	<0.82	<0.82	<0.82	<0.82
SB12, 3'	250	<70	<70	610	750000	<280	<280	<280	<280	<70	<70	<70	<280	480	<70	76	<70	<70	<70	<70
SB13, 3'	0.91	8.5	<0.67	1.3	550	49 a	<2.7	5.5	6.4	<0.67	<0 .6 7	<0.67	<2.7	<0.67	<0.67	<0.67	<0.67	<0.67	<0.67	<0.67
SB14, 3'	2.7	5.3	0.87	4.7	620	10 a	<2.8	3.5	<2.8	<0.70	<0.70	<0.70	<2.8	<0.70	<0.70	1.6	<0.70	<0.70	<0.70	<0.70
SB15, 3'	42	12	1.6	6.7	2100	51 a	13	13	<5.8	<1.4	<1.4	<1.4	<5.8	<1.4	<1.4	<1.4	<1.4	<1.4	<1.4	<1.4

Notes:

All Concentrations in ppbv

Parts per billion volumetric. ppbv

Compound present in laboratory blank greater than reporting limit (background subtraction not performed). Exceeds instrument calibration range. а

b

NA Not analyzed.

Total Petroleum Hydrocarbons as gasoline. Total Petroleum Hydrocarbons as diesel. TPH-g

TPH-d

Fabl	le I	.2 (Con	tinu	ed)

1.14

- ·

					· · · ·				4-Methyl-		Methyi			Tetra-	Tetra-	1,1,1-Tri-	Tri-	1,2,4-Tri-	1,3,5-Tri-
Sample	1,4-Di-		4-Ethyl-	Freon	Freon	Freon	Hep-	Hex-	2-penta-	Methylene	t-butyl	2-Pro-	Sty-	chloro-	hydro-	chloro-	chloro-	methyl-	methyl-
ID OD1 21	oxane	Ethanol	toluene	11	12	113	tane	ane	none	Chloride	ether	panol	rene	ethene	furan	ethane	ethene	benzene	benzene
SB1, 3'	<2.6	63	<2.6	0.74	0.93	27	<2.6	4.4	3.8	3.7	<2.6	5.6	<0.65	1.2	<2.6	<0.65	<0.65	1.1	<0.65
SB2, 3'	<2.7	110	<2.7	1.2	200	<0.67	3.3	5.3	8.1	2.2	<2.7	<2.7	3.0	<0.67	<2.7	<0.67	<0.67	2.0	0. 77
SB3, 3'	<190	<190	<190	<48	180	<48	<190	590	<190	<48	<190	<190	<48	<48	<190	<48	<48	<48	<48
SB3, 3' dup	<580	<580	<580	<140	160	<140	<580	580	<580	<140	<580	<580	<140	<140	<580	<140	<140	<140	<140
SB4, 3'	<14	1,400	<14	<3.5	100	<3.5	<14	19	15	340	<]4	22	<3.5	160	<14	21	<3.5	<3.5	<3.5
SB5, 3'	3.3	55	<2.8	4.4	1.2	3.4	<2.8	<2.8	<2.8	<0.71	<2.8	<2.8	<0.71	<0.71	<2.8	<0.71	<0.71	<0.71	<0.71
SB6, 3'	<2.7	35	<2.7	<0.68	<0.68	<0.68	<2.7	<2.7	<2.7	<0.68	<2.7	<2.7	<0.68	<0.68	<2.7	<0.68	<0.68	1.1	<0.68
SB7, 3'	8.2	94	<2.9	0.74	1.1	<0.73	<2.9	6.8	4.4	<0.73	<2.9	3.8	1.0	2.0	<2.9	<0.73	<0.73	1.8	<0.73
SB8, 3'	<11	62	<11	6.5	630	<2.8	<11	<11	<11	<2.8	<11	<11	<2.8	<2.8	<11	<2.8	<2.8	5.3	<2.8
SB9, 3'	<2.7	47	<2.7	1.5	20	<0.68	<2.7	4.3	<2.7	<0.68	<2.7	<2.7	<0.68	<0.68	<2.7	<0.68	<0.68	2.3	0.77
SB10, 3'	<3.2	40	<3.2	<0.80	1.4	<0.80	<3.2	3.9	<3.2	<0.80	<3.2	<3.2	<0.80	<0.80	<3.2	<0.80	<0.80	1.2	<0.80
SB11, 3'	22	23	<3.3	4.6	<0.82	<0.82	<3.3	<3.3	<3.3	. 1.2	<3.3	<3.3	<0.82	<0.82	<3.3	<0.82	<0.82	0.85	<0.82
SB12, 3'	<280	<280	760	<70	<70	<70	<280	18,000	<280	<70	<280	<280	<70	<70	<280	<70	<70	580	740
SB13, 3'	4.3	410 b	<2.7	<0.67	<0.67	<0.67	3.4	<2.7	<2.7	5.6	<2.7	26	<0.67	<0.67	58	<0.67	<0.67	1.1	<0.67
SB14, 3'	<2.8	67	<2.8	<0.70	<0.70	<0.70	<2.8	<2.8	2.8	1.3	2.9	<2.8	0.82	<0.70	<2.8	<0.70	<0.70	2.0	0.81
SB15, 3'	<5.8	190	<5.8	<1.4	46	<1.4	<5.8	50	<5.8	4.8	<5.8	<5.8	<1.4	2.1	<5.8	<1.4	<1.4	1.8	<1.4

Notes: All Concentrations in ppbv pnbv Parts per billion volumetric.

Compound present in laboratory blank greater than reporting limit (background subtraction not performed). Exceeds instrument calibration range. а

b

NA

Not analyzed. Total Petroleum Hydrocarbons as gasoline. Total Petroleum Hydrocarbons as diesel. TPH-g

TPH-d

					. (Concentration	n (μg/L)						
Well	Date			Ethyl-									
No.	Sampled	Benzene	Toluene	benzene	Xylenes	TPH-g	TPH-d	1,1-DCA	1,2-DCA 1	,1,1-TCA	TCE	MTBE	Notes
					/								
MW-2	03/23/93	ND	ND	ND	ND	ND	ND						
	07/27/93	ND	ND	ND	ND	ND	ND		·	`			
	11/05/93	·											
	02/25/94	<1	<1	<1	<1	<100	<1,000						
	06/03/94	<0.5	< 0.5	< 0.5	<0.5	<50	<20,000	·					
	08/31/94	< 0.3	< 0.3	< 0.3	<0.6	<500	<500						
	12/22/94	<0,5	< 0.5	<0.5	<0.5	<50	<50						а
	03/13/95	0.8	< 0.5	< 0.5	< 0.5	<50	<400						
	06/09/95	< 0.5	< 0.5	< 0.5	< 0.5	<100	<50		•				
	09/21/95	0.7	< 0.5	<0.5	< 0.5	<50	<50						
	12/12/95	<0.5	< 0.5	<0.5	<1.0	<100	<50		·				
	03/12/96	<0.5	< 0.5	< 0.5	< 0.5	<100	<50						
	06/21/96												
	08/29/96	<0.5	< 0.5	< 0.5	<0.5	<50	<150						
	01/16/97	<0.5	< 0.5	< 0.5	<0.5	<50	<150		< 0.5	<0.5	<0.5		
	07/07/97	< 0.5	< 0.5	< 0.5	< 0.5	<50	<150					< 0.5	
	01/27/98	<0.5	< 0.5	< 0.5	< 0.5	100	<150					<0.5	
	07/22/98	< 0.5	< 0.5	< 0.5	<0.5	<50						<0.5	
	07/22/99	<0.5	< 0.5	< 0.5	<0.5	<50	<200	< 0.5	< 0.5	<0.5	<0.5	<0.5	
MW-3	03/23/93	35	2.9	2	3.2	300	ND				<u>.</u>		
	07/27/93	97	1	4	1.1	220	ND						
	11/05/93	4.9	ND	ND	1.2	170	ND						
	02/25/94	42	<1	<1	<1	100	<1,000				<u> -</u>		
	06/03/94	120	8.2	8.4	4.5	320	<20,000						
	08/31/94	83	1.1	5.3	2.9	<500	<500						
	12/22/94	1,460	18	100	50	3,800	270						
	03/13/95	3,600	260	270	280	14,000	1,700						
	06/09/95	4,700	58	140	71	3,700	120						
	09/21/95	9,800	58	600	95	14,000	300						
	12/12/95	330	2.1	47	5.3	700	<50						
	03/12/96	350	4.6	23	8.7	600	<50						
	06/21/96	940	76	98 44	57	1,900 900	<50						
	08/29/96	420	29	44	28		<150 700			<0.5			
	01/16/97	1,600	270	120	194	3,600	/00	<0.5	9.2	<0.5	<0.5		

- 10

Page 1 of 11

			•			Concentratio	m (ug/L)						
Well	Date			Ethyl-			(µ6/2)					<u> </u>	
No.	Sampled	Benzene	Toluene	benzene	Xylenes	TPH-g	TPH-d	1.1-DCA	1.2-DCA	1,1,1-TCA	TCE	MTBE	Notes
					•			.,	-,- 2 0,1	1,1,1 1011	100	WIDE	INOLES
MW-3	04/15/97	1,300	300	180	160	4,300	800	< 0.5	16	< 0.5	1.1	6.9	
	07/07/97	100	84	100	67	1,900	350					3.8	
	10/27/97	1,030	60	54	40	2,200		< 0.5	2.4	< 0.5	<0.5	3.1	
	01/27/98	1,070	98	73	69	3,200						3.9	
	04/22/98	610	56	49	54	1,800		< 0.5	3.0	< 0.5	< 0.5	1.1	
	07/22/98	1,800	230	160	180	3,600	370				-0.5	5.0	
	10/21/98	78	1.0	3.8	0.6	110	<250	< 0.5	0.6	< 0.5	< 0.5	< 0.5	
	07/23/99	1,500	140	76.0	260	4,000	790	< 0.5	1.0	< 0.5	< 0.5	5.60	
	10/28/99	1,100	43	58	102	3,000	600	< 0.5	0.9	-0.5	< 0.5	. 5.00	
	02/10/00	690	22	36	49	1,400	520	<0.5	<0.5	<0.5	<0.5	2.20	
	04/27/00	1,100	140	73	163	2,400	250	<0.5	0.6	<0.5	<0.5	<0.5	
MW-5	02/05/99	<0.5	<0.5	<0.5	<0.5	<50	<150	<0.5	<0.5	<0.5	<0.5	<0.5	
MW-6	03/23/93	ND											
11111-0	07/27/93	ND	ND	ND	ND	ND	ND						
	11/05/93	ND	ND	ND	ND	ND	ND						
	02/25/94	ND	ND	ND	ND	ND	ND						
	06/03/94	<1	<1	<1	3.5	<100	<1,000						
	08/31/94	2.7	<0.5	< 0.5	< 0.5	69	<20,000						
		< 0.3	8.7	1.6	3.5	<500	<500						
	12/22/94	< 0.5	<0.5	< 0.5	<0.5	<50	<50						а
	03/13/95	1.2	<0.5	< 0.5	< 0.5	<50	<400						
	06/09/95	0.6	<0.5	< 0.5	< 0.5	<100	<50						
	09/21/95	<0.5	<0.5	<0.5	< 0.5	<50	<50						
	12/12/95	<0.5	<0.5	< 0.5	<1.0	<100	<50						
	03/12/96	<0.5	<0.5	<0.5	<0.5	<100	<50	~					
	06/21/96				'								
	08/29/96	< 0.5	<0.5	<0.5	<0.5	<50	<150						
	01/16/97	5.5	16	2.9	16	140	220	< 0.5	6.3	< 0.5	< 0.5		
	07/07/97	<0.5	< 0.5	<0.5	<0.5	<50	<150					< 0.5	
	07/22/98	<0.5	<0.5	<0.5	<0.5	<50	<250		~~			<0.5	
MW-11	02/05/99	<0.5	<0.5	<0.5	<0.5	<50	<150	•		·		<0.5	
MW-12	02/05/99	<0.5	<0.5	<0.5	<0.5	<50	<150					<0.5	

Page 2 of 11

						Concentratio	m (ug/L) .						
Well	Date			Ethyl-			(<u>-8,-)</u>						
<u>No</u> .	Sampled	Benzene	Toluene	benzene	Xylenes	TPH-g	TPH-d		12 004	1,1,1-TCA	TOP		
					119101100	1111-5	1111-0	1,1-DCA	1,2-DCA	1,1,1-1CA	TCE	MTBE	Notes
MW-13	02/05/99	<0.5	< 0.5	< 0.5	< 0.5	<50	<150					< 0.5	
												~0.5	
MW-15	02/05/99	<0.5	< 0.5	<0.5	< 0.5	<50	430	< 0.5	<0.5	< 0.5	< 0.5	<0.5	
	07/22/99	<0.5	< 0.5	<0.5	< 0.5	<50	<200	< 0.5	< 0.5	<0.5	< 0.5	<0.5 <0.5	
								010	-0.5	~0. 5	~0. J	<0.5	
MW-25	03/23/93	ND	ND	ND	ND	ND	ND						•
	07/27/93	ND	ND	ND	ND	ND	ND						
	11/05/93	4.2	4.4	2.5	20	170	ND	·					
	02/25/94	2.1	<1	<1	<1	<100	<1,000						
	06/03/94	2.4	14	<0.5	3.4	97	<20,000						
	08/31/94	0.5	< 0.3	< 0.3	<0.6	<500	<500					 	
	12/22/94	0.5	< 0.5	<0.5	<0.5	<50	<50						
	03/13/95	0.58	< 0.5	< 0.5	< 0.5	150	950						а
	06/09/95	0.8	< 0.5	< 0.5	< 0.5	<100	60						
	09/21/95	<0.5	< 0.5	<0.5	<0.5	50	<50						
	12/12/95	< 0.5	< 0.5	< 0.5	<1.0	<100	<50						
	03/12/96	< 0.5	< 0.5	<0.5	< 0.5	120	<50						
	06/21/96												
	08/29/96	<0.5	<0.5	< 0.5	<0.5	90	<150						
	01/16/97	0.6	< 0.5	<0.5	< 0.5	80	<150	25	41	< 0.5	< 0.5		
	07/07/97	< 0.5	< 0.5	<0.5	< 0.5	140	<150			-0.5	-0.5	11	
	01/27/98	<0.5	< 0.5	<0.5	< 0.5	<100						10	
	07/22/98	< 0.5	< 0.5	<0.5	< 0.5	<50	<250					24	
	02/05/99	<0.5	< 0.5	<0.5	< 0.5	<50	340	28	59	< 0.5	< 0.5	28	h
	04/07/99	< 0.5	< 0.5	<0.5	< 0.5	<50	<250	27	72	< 0.5	< 0.5	20	i
	07/23/99	1.80	< 0.5	<0.5	< 0.5	<50	<200	30	58	< 0.5	< 0.5	23.0	1
	10/27/99	<0.5	1.4	< 0.5	1.0	<100	<200	35	47		< 0.5	20.0	
	02/08/00	<0.5	<0.5	<0.5	<0.5	100	<250	39	41	<0.5	<0.5	29.0	q
	04/26/00	<0.5	<0.5	<0.5	<0.5	<100	<250	51	38	<0.5	<0.5	18	t t
													-
MW-26	03/23/93	180	190	55	330	7,000	1,300	ND	ND	ND	ND		
	07/27/93 11/05/93	470	96	30	80	1,800	ND	ND	140	ND	ND		
	02/25/94	4,700	1,300	9	1,400	19,000	ND	ND	120	ND	ND		
	02/23/94	4,800	570	200	860	14,000	<1,000	<1	28	<1	<1		

Nagase ----

30

Page 3 of 11

						Concentratio	n (μg/L)						
Well	Date			Ethyl-									
No.	Sampled	Benzene	Toluene	benzene	Xylenes	TPH-g	TPH-d	1,1-DCA	1,2-DCA	1,1,1 - TCA	TCE	MTBE	Notes
MW-26	06/02/04		• • •										
IVI W-20	06/03/94	4,100	300	120	230	12,000	<20,000	1.7	140	<0.5	< 0.5		с
	08/31/94	4,100	360	170	450	93,000	1,400	<4.0	<4.0	<4.0	<4.0	· 	
	12/22/94	1,030	170	85	290	5,000	560	<2.0	<2.0	<2.0	<2.0		đ
	03/13/95	320	19	23	66	3,000	810	53	5.8	< 0.5	< 0.5		-
	06/09/95	14,000	64	31	230	10,800	310	240	3.1	1	< 0.5		
	09/21/95	1,900	160	160	330	8,000	200	1.3	120	< 0.5	<0.5		
	12/12/95	13,000	38	36	120	25,000	0.6	1.4	180	< 0.5	<0.5		b
	03/12/96	9,000	33	30	65	4,400	<50	< 0.5	180	< 0.5	< 0.5		U
	06/21/96	14,000	27	16	66	5,400	<50	3.2	170	< 0.5	< 0.5		
	08/29/96	8,500	26	28	74	19,000	<150	< 0.5	160	< 0.5	< 0.5		
	01/16/97	6,500	21	31	47	4,600		4.3	>50	< 0.5	< 0.5	26	
	04/15/97	16,000	33	40	160	26,000	2,200	3.5	97	<0.5	2.4	20 40	_
	07/07/97	22,000	44	170	200	28,000	1,100	<5.0	<5.0	<5.0	<5.0	40 95	e
	10/27/97	16,000	26	100	37	30,000		3.6	92	< 0.5	< 0.5	38	
	01/27/98	23,600	<5.0	<5.0	<5.0	26,000	420	8.3	100	<0.5	< 0.5	100	
	04/22/98	5,000	4.3	9.2	16	14,000		13	130	< 0.5	< 0.5	27	
	07/22/98	3,800	5.7	6.9	11	5,200	750	10	110		<0.5	33	
	10/21/98	420	< 0.5	2.1	2.7	820	<250	24	82	< 0.5	<0.5	33	
	02/05/99	20	< 0.5	0.60	0.80	230	230	10	51	<0.5 <0.5	<0.5	29	
	04/07/99	<0.5	< 0.5	< 0.5	< 0.5	80	<250	15	54	<0.5 <0.5	<0.5	29	
	07/23/99	7.10	< 0.5	< 0.5	0.80	180	<200	13	32	<0.5 <0.5	<0.5 <0.5	12.0	
	10/27/99	14	1.4	2.9	7.8	400	<200	12	30	-0.5	<0.5		
	02/08/00	<0.5	<0.5	<0.5	<0.5	80	<250	13	32	<0.5	<0.5		
	04/26/00	0.7	<0.5	0.6	<0.5	200	340	13 7.5	32 39	<0.5 <0.5	<0.5 <0.5	28.0 22	
MW-27	06/21/96	<0.5	< 0.5	< 0.5	<0.5	<50	<50	< 0.5	6.8	< 0.5	< 0.5		
	08/29/96												
	01/16/97	12	5.0	<0.5	2.6	70	<150	< 0.5	5.7	< 0.5	< 0.5		
	07/22/98	<0.5	< 0.5	< 0.5	<0.5	<50	<250	<1.0	1.4		<1.0	<0.5	
	02/05/99	<0.5	<0.5	< 0.5	<0.5	<50	<150	<0.5	0.7	< 0.5	< 0.5	< 0.5	
	07/23/99	<0.5	<0.5	< 0.5	<0.5	<50	<200	< 0.5	0.7	< 0.5	<0.5	<0.5	
	10/27/99	<0.5	<0.5	<0.5	<0.5	<100	<200	<0.5	<0.5		< 0.5		
	02/08/00 04/27/00	<0.5	<0.5	<0.5	<0.5	<50	<250	<0.5	<0.5	<0.5	<0.5	<0.5	
	04/27/00	<0.5	<0.5	<0.5	<0.5	<100	250	<0.5	<0.5	<0.5	<0.5	<0.5	

						Concentratio	on (µg/L)						
Well	Date			Ethyl-									
No.	Sampled	Benzene	Toluene	benzene	Xylenes	TPH-g	TPH-d	1,1-DCA	1.2-DCA	1,1,1-TCA	TCE	MTBE	Notes
										1,1,1 10/1	TCL	MIDE	THOLES
MW-28	03/23/93	ND	ND	ND	ND	110	ND						
	07/27/93	ND	ND	ND	ND	ND	ND						
	11/05/93	ND	ND	ND	2.1	ND	ND						
	02/25/94	<1	<1	<1	<1	<100	<1						
	06/03/94	3.1	< 0.5	< 0.5	< 0.5	<50	<20,000						
	08/31/94	1.4	< 0.3	< 0.3	<0.6	<500	<500						
	12/22/94	<0.5	< 0.5	< 0.5	< 0.5	<50	<50						· a
	03/13/95	0.91	< 0.5	< 0.5	< 0.5	<50	<400						·a
	06/09/95	<0.5	< 0.5	<0.5	< 0.5	<100	<50	· 					
	09/21/95	<0.5	<0.5	<0.5	< 0.5	<50	<50						
	12/12/95	< 0.5	< 0.5	< 0.5	<1.0	<100	<50						
	03/12/96	< 0.5	< 0.5	< 0.5	< 0.5	<100	<50						
	06/21/96	<0.5	<0.5	< 0.5	< 0.5	<100	<50						
	08/29/96	< 0.5	< 0.5	< 0.5	< 0.5	<50	<150						
	01/16/97	18	20	2.2	13	220	<150	5.1	85	< 0.5	<0.5	8.2	
	04/15/97	< 0.5	< 0.5	< 0.5	<0.5	120	<150	1.1	150	< 0.5	<0.5	7.1	
	07/07/97	< 0.5	< 0.5	< 0.5	< 0.5	110	<150	<5.0	170	<5.0	<5.0	7.1	
	10/27/97	3.6	< 0.5	< 0.5	< 0.5	300		6.2	120	<0.5	<0.5	36	
	01/27/98	7.6	< 0.5	< 0.5	<0.5	500	<150			-0.5	-0.5	56	
	04/22/98	< 0.5	<0.5	< 0.5	< 0.5	<50		1.0	89	< 0.5	< 0.5	8.6	
	07/22/98	< 0.5	< 0.5	< 0.5	< 0.5	<50	·	<1.0	85	-0.5	<1.0	8.0 18	
	10/21/98	< 0.5	< 0.5	< 0.5	<0.5	<50	<250	0.5	80	< 0.5	<0.5	12	
	02/05/99	< 0.5	< 0.5	< 0.5	<0.5	<50	<150	32	29	<0.5	< 0.5	5.0	L.
	04/07/99	< 0.5	< 0.5	< 0.5	< 0.5	<50	<250	< 0.5	62	<0.5	<0.5	4.5	h
	07/23/99	< 0.5	< 0.5	< 0.5	<0.5	<50	<200	< 0.5	50	< 0.5	<0.5	1.80	
	10/27/99						<200			-0.5			
	11/02/99	0.7	< 0.5	<0.5	< 0.5	<100	-200	< 0.5	32		 <0,5		
	02/08/00	<0.5	<0.5	<0.5	<0.5	<50	<250	<0.5	32 39	<0.5	<0.3 <0.5		
	04/26/00	<0.5	<0.5	<0.5	<0.5	<100	<250	<0.5	50	<0.5 <0.5	<0.5 <0.5	4.30 1.5	
												212	
MW-29	03/23/93	ND	ND	ND	ND	ND	ND						
	07/27/93	ND	ND	ND	ND	ND	ND			·			
	11/05/93	ND	ND	2.1	11	ND	ND						
	02/25/94	<1	<1	<1	<1	<100	<1,000						
	06/03/94	<0.5	<0.5	<0.5	<0.5	<50	<20,000						

114.5

						Concentratio	n (µg/L)						
Well	Date			Ethyl-									
No.	Sampled	Benzene	Toluene	benzene	Xylenes	TPH-g	TPH-d	1,1-DCA	1,2-DCA	1,1,1-TCA	TCE	MTBE	Notes
									/				riotes
MW-29	08/31/94	<0.3	< 0.3	<0.3	<0.6	<500	<500						
	12/22/94	<0.5	< 0.5	< 0.5	< 0.5	<50	<50						а
	03/13/95	0.59	<0.5	<0.5	< 0.5	<50	<400						a
	06/09/95	< 0.5	< 0.5	<0.5	<0.5	<100	<50						
	09/21/95	<0.5	<0.5	< 0.5	<0.5	<50	<50						
	12/12/95	< 0.5	<0.5	< 0.5	<1.0	<100	<50						
	03/12/96	< 0.5	< 0.5	< 0.5	<1.0	<100	<50						
	06/21/96												
	08/29/96	< 0.5	< 0.5	< 0.5	< 0.5	<50	<150						
	01/16/97	6.6	8.9	0.6	9.3	120	<150	47	24	<0.5	<0.5		
	07/07/97	< 0.5	< 0.5	< 0.5	< 0.5	<50	<150	52	24	<0.3 <5.0	<0.5 <5.0	1.8	
	01/27/98	<0.5	< 0.5	< 0.5	< 0.5	100	<150					1.2	
	07/22/98	< 0.5	< 0.5	< 0.5	<0.5	<50	<250	12	29			8.0	
	02/05/99	<0.5	< 0.5	< 0.5	<0.5	<50	<150	< 0.5	68	< 0.5	<1.0	7.8	
	04/07/99	<0.5	< 0.5	< 0.5	<0.5	<50	<250	<0.5 30	38		<0.5	8.5	
	07/23/99	<0.5	< 0.5	< 0.5	<0.5	<50	<200	30 44	33	<0.5	< 0.5	4.9	j
	10/27/99	<0.5	< 0.5	< 0.5	<0.5	<100	<200	36	23	<0.5	1.9	4.70	k, 1
	02/08/00	<0.5	<0.5	<0.5	<0.5	<50	<200 <250	30 87	23 25		< 0.5		
	04/26/00	<0.5	< 0.5	<0.5	<0.5	<100	<250	61	25 38	<0.5	<0.5	18.0	S
			-0.0		-0.5	<100	~230	01	38	<0.5	<0.5	12	u
MW-30	03/23/93	ND	ND	ND	ND	ND	ND						
	07/27/93	ND	ND	ND	ND	ND	ND			-			
	11/05/93	ND	ND	ND	2.8	ND	ND						
	02/25/94	1.3	<1	<1	<1	<100	<1,000						
	06/03/94	1.1	< 0.5	< 0.5	<0.5	<50	<20,000			~~			
	08/31/94	0.8	< 0.3	< 0.3	<0.6	<500	<500				·		
	12/22/94	0.6	< 0.5	<0.5	< 0.5	<50	<50						
	03/13/95	0.98	< 0.5	< 0.5	<0.5	<50	<400						а
	06/09/95	<0.5	< 0.5	< 0.5	< 0.5	<100	<50						
	09/21/95	< 0.5	< 0.5	< 0.5	<0.5	<50	<50						
	12/12/95	<0.5	< 0.5	<0.5	<1.0	<100	<50						
	03/12/96	<0.5	< 0.5	< 0.5	< 0.5	<100	<50						
	06/21/96												
	08/29/96	<0.5	<0.5	< 0.5	<0.5	<50	<150						
	01/16/97	<0.5	< 0.5	<0.5	0.6	80	<150	< 0.5	< 0.5	< 0.5	0.9		

 Table I.3. Concentrations (µg/L) Of Organic Compounds In Groundwater Samples

 NESTLE USA FACILITY, OAKLAND

tr a

्रम्

• 218

kannan a

						Concentratio	n (ug/L)						
Well	Date			Ethyl-			(1-0 /						
No	Sampled	Benzene	Toluene	benzene	Xylenes	TPH-g	TPH-d	1,1-DCA	1,2-DCA	1,1,1-TCA	TCE	MTBE	Notes
									/	-,,,,- 1011		MIDL/	Rotes
MW-30	07/07/97	<0.5	<0.5	<0.5	<0.5	<50	<150				~-	<0.5	
	01/27/98	5.4	<0.5	<0.5	<0.5	100				·		<0.5	
	07/22/98	<0.5	<0.5	<0.5	<0.5	<50						< 0.5	
	04/07/99	<0.5	<0.5	<0.5	< 0.5	<50	<250	·				< 0.5	
	07/22/99	<0.5	<0.5	<0.5	<0.5	<50		<0.5	< 0.5	<0.5	< 0.5	<0.5	
	10/28/99	<0.5	<0.5	<0.5	<0.5	<100	<200	< 0.5	< 0.5		< 0.5		
	02/08/00	<0.5	<0.5	<0.5	<0.5	<50	<250	<0.5	<0.5	<0.5	<0.5	<0.5	
	04/27/00	<0.5	<0.5	<0.5	<0.5	<100	250	<0.5	<0.5	<0.5	<0.5	<0.5	
MW-32	03/23/93	391	6.2	3.1	9	440	ND	ND	60	ND	ND		
	07/27/93	ND	ND	ND	ND	ND	ND	ND	14	ND	ND		
	11/05/93	20	ND	1.8	2.1	170	ND	ND	7.9	ND	ND		
	02/25/94	5.6	<1	<1	<1	<100	<1,000	<1	<1	<1	<1		
	06/03/94	120	1.3	< 0.5	1.4	350	<20,000	< 0.5	11	<0.5	< 0.5		
	08/31/94	39	0.5	2.2	1.2	<500	<500	<4.0	10	<0.5 <4.0	<4.0		
	12/22/94	4.8	<0.5	< 0.5	<0.5	<50	<50	<2.0	4.6	<2.0	<2.0		
	03/13/95	220	3.6	6.5	5.8	1,100	<400	< 0.5	16	<0.5	<0.5		а
	06/09/95	1,500	7.9	43	14	2,200	180	0.7	< 0.5	0.5	< 0.5		
	09/21/95	1,200	2.4	72	4.5	2,300	60	< 0.5	6.7	< 0.5	<0.5 1.4		
	12/12/95	230	< 0.5	8.9	<1.0	500	<50	< 0.5	28	<0.5	<0.5		
	03/12/96	40	<0.5	1.7	< 0.5	110	<50	< 0.5	6.8	<0.5	< 0.5		
	06/21/96									-0.5	-0.5		
	08/29/96	150	< 0.5	49	< 0.5	700	<150	< 0.5	. 27	< 0.5	< 0.5		
	01/16/97	14	< 0.5	1.9	<0.5	150	<150	< 0.5	10	<0.5	~0.3 0.7		c
	07/07/97	370	11	110	21	1,600	190			-0.5	0.7	11	f
	01/27/98	13	<0.5	1.0	< 0.5	300		< 0.5	7.5	< 0.5	< 0.5	2.5	g
	07/22/98	700	55	88	66	2,300				-0.5	-0.5	2.5 14	
	07/22/99	59.0	0.80	1.80	<0.5	900	220	<0.5	5.9	< 0.5	<0.5	8.70	
	10/28/99	95	2.5	2.1	1.6	500	<200	< 0.5	12	-0.5	< 0.5	0.70 	
	02/10/00	7.0	<0.5	<0.5	<0.5	120	<250	<0.5	4.3	< 0.5	<0.5	1.10	
	04/27/00	240	7.0	12	18.8	800	250	<0.5	9.8	<0.5	<0.5	<0.5	
MW-33	04/07/99	0.60	<0.5	0.90	<0.5	<50	<250					<0.5	
	07/22/99	8.90	< 0.5	1.00	<0.5	<50	<200	0.6	0.7	< 0.5	< 0.5	<0.5	
	10/28/99	40	0.9	21	3.8	200	<200	0.8	1.3		<0.5	-0.5	

25

2003120: 15

						Concentratio	on (ug/L)						
Well	Date			Ethyl-			(1.6/~)			······································			
No	Sampled	Benzene	Toluene	benzene	Xylenes	TPH-g	h-HqT	1.1-DCA	12-DCA	1,1,1-TCA	TCE	MTDT	Mart
						DD		1,1 DOM	1,2-DCA	1,1,1-1CA	ICE	MTBE	Notes
MW-33	02/10/00	20	0.7	12	10.0	380	<250	0.9	0.6	<0.5	<0.5	1.30	
	04/27/00	6.9	<0.5	6.4	<0.5	<100	250	4.3	0.9	<0.5	<0.5	<0.5	
										-015	-0.5	~0.5	
MW-?	02/05/99	<0.5	<0.5	< 0.5	< 0.5	<50	430					<0.5	
												-0.5	
PR-26	07/26/99	20,000	15,000	1,100	7,250	82,500	11,000				_ ~ ¹	33.0	
	10/26/99	28,000	25,000	2,300	8,400	110,000	60,000	< 0.5	24		< 0.5		
PR-45	07/26/99	13,200	8,200	2,600	15,600	82,500	39,000					35.0	
	10/28/99	12,000	8,200	1,700	8,500	45,000	25,000	< 0.5	< 0.5		< 0.5		
	02/09/00	24,000	25,000	10,000	53,000	360,000	82,000	<0.5	4.0	<0.5	<0.5	1,000	
	04/27/00	17,000	9,500	16,000	92,000	1,300,000	20,300	<5.0	· <5.0	<5.0	<5.0	<5.0	
PR-52	07/26/00	10 000	1										
FR-32	07/26/99 10/28/99	12,000	1,720	750	12,400	172,000	40,000	<0.5	1.8	< 0.5	< 0.5	217	m
	02/09/00	19,000	530	1,800	5,800	40,000	450,000	<0.5	<0.5		< 0.5		
	02/09/00 04/28/00	22,000	.1,600	4,100	15,800	200,000	140,000	<0.5	1.3	<0.5	<0.5	430	
	04/20/00	20,000	2,200	4,700	18,600	270,000	88,000	<1.0	<1.0	<1.0	<1.0	<5.0	
PR-53	07/26/99	31,000	12,000	1,900	8,800	110.000		-0.5					
	10/27/99	17,000	3,900	890	3,320	110,000 54,000	98,000	<0.5	43	<0.5	<0.5	43.0	n
	02/09/00	21,000	5,000	1,200	5,320. 5,300	65,000	16,000 9,400	<0.5	18		<0.5		
	04/28/00	34,000	30,000	9,300	51,000	730,000	9,400 104,000	0.6	20	<0.5	<0.5	67.0	r
		0 1,000	50,000	2,500	51,000	750,000	104,000	<1.0	<1.0	<1.0	<1.0	340	
PR-54	07/26/99	32,000	22,000	1,500	21,800	170,000	28,000	<0.5	3.0	<0.5	<0.5	56.0	-
	10/26/99	27,000	10,000	3,700	19,500	190,000	350,000	< 0.5	<0.5	-0.5	< 0.5	50.0	0
	02/09/00	27,000	23,000	9,900	50,000	960,000	110,000	<0.5	3.9	<0.5	<0.5 <0.5	1,000	
	04/28/00	24,000	14,000	1,200	9,000	76,000	80,000	<1.0	1.6	<1.0	<1.0	300	
						-				10	-1.0	500	
PR-64	07/26/99	22,000	18,000	1,700	10,300	110,000		< 0.5	130	< 0.5	<0.5	35.0	р
	10/27/99	11,000	7,400	1,200	3,900	66,000	50,000	< 0.5	110		< 0.5		Р
	02/09/00	22,000	20,000	6,000	17,000	120,000	40,000	<0.5	>50	<0.5	<0.5	110	
	04/28/00	19,000	16,000	1,800	13,900	130,000	78,000	<1.0	67	<1.0	<1.0	300	
PR-65	07/26/99	12,000	1,400	1,300	13,000	69 000	16 500	-0 -					
	10/26/99	12,000	2,300	1,300	13,000	68,000	16,500	< 0.5	2.6	<0.5	<0.5	20.0	
	_ = = = = = = = = = = = = = = = = = = =	14,000	2,500	1,000	11,000	65,000	50,000	<0.5	<0.5		<0.5		

1,30

						Concentration	1 (μg/L)						
Well	Date			Ethyl-								,	
No.	Sampled	Benzene	Toluene	benzene	Xylenes	TPH-g	TPH-d	1,1-DCA	1.2-DCA	1,1,1-TCA	TCE	MTBE	Notes
						¥				.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		MIDL	Indies
	07/07/00												
PR-68	07/26/99	1,900	24.0	27.0	62.0	4,900	11,000	<0.5	1.2	< 0.5	< 0.5	4.40	
	10/26/99	2,800	36	86	62	8,000	2,800	< 0.5	<0.5		<0.5		
PR-76	04/07/99	< 0.5	<0.5	<0.5	<0.5	<50	<250					-0.5	
						50	-250		-			<0.5	
V-24	04/07/99	<0.5	<0.5	<0.5	<0.5	120	<250			·		0.5	
V-31	07/26/99	7,000	600	550	1,370	17,500	5,350					19.0	
	10/26/99	7,000	120	850	950	18,000	3,000	< 0.5	<0.5		<0.5	19.0	
							-,	-10	-0.5		-0.5		
V-46	02/05/99	<0.5	<0.5	< 0.5	<0.5	<50	270	<0.5	<0.5	<0.5	<0.5	< 0.5	
V-55	07/22/00	8.000	10.0	540									
V-35	07/22/99	8,000	480	740	2,880	30,000	2,100	<0.5	<0.5	< 0.5	<0.5	13.0	
	10/28/99	11,000	59	1,200	317	28,000	38,000	< 0.5	< 0.5		<0.5		
	02/09/00	2,200	59	760	350	7,900	10,000	<0.5	<0.5	<0.5	<0.5	9.70	
	04/28/00	2,900	510	440	2,340	14,000	26,500	<5.0	<5.0	<5.0	<5.0	<5.0	
V-72	07/26/99	13,500	6.80	1.10	3.90	3,900	12,900	<0.5	11	<0.5	<0.5	<0.5	
	10/28/99	2,900	58	21	47.7	6,000	48,000	< 0.5	3.4		< 0.5	-0.5	
	02/09/00	670	8.2	<0.5	17.8	890	6,100	<0.5	3.0	< 0.5	<0.5 <0.5	<0.5	
	04/28/00	130	<0.5	<0.5	<0.5	200	5,950	<0.5	0.7	<0.3 <0.5	<0.5 <0.5		
							5,500	-015	0.7	~0.5	<0.5	<0.5	
V-84	07/26/99	2,400	440	80.0	340	8,700	2,350	<0.5	2.4	< 0.5	<0.5	6.40	
	10/26/99	1,100	130	46	108	4,000	700	< 0.5	< 0.5	·	< 0.5		
	02/09/00	300	30	8.9	53	2,300	1,100	<0.5	1.2	<0.5	<0.5	<0.5	
	04/28/00	30	1.9	<0.5	<0.5	100	550	<5.0	<5.0	<5.0	<5.0	<0.5	
29 (CC-1)	07/23/99	<0.5	<0.5	<0.5	-0.5	~50	<200	-0.5	-0.5				
27 (00-1)	10/28/99	<0.5 <0.5	<0.5 <0.5	<0.5	<0.5 <0.5	<50	<200	< 0.5	<0.5	<0.5	<0.5	< 0.5	
	02/08/00	<0.5 <0.5	<0.5 < 0.5	<0.5 < 0.5	<0.5 < 0.5	<100 < 50	<200 < 250	<0.5	<0.5		< 0.5		
	04/26/00	<0.5 <0.5	<0.5 <0.5	<0.5 <0.5	<0.5 <0.5	<50 <100		<0.5	<0.5	<0.5	<0.5	<0.5	
		~0.5	~0.5	~0.5	<0.5	~100	<250	<0.5	<0.5	<0.5	<0.5	<0.5	
30 (CC-2)	07/22/99	0.90	< 0.5	< 0.5	< 0.5	<50	<200	<0.5	<0.5	< 0.5	<0.5	<0.5	
	10/28/99	<0.5	<0.5	<0.5	<0.5	<100	<200	< 0.5	< 0.5		<0.5	-0.5	1

Page 9 of 11

						Concentration	n (μg/L)						
Well	Date			Ethyl-									
No.	Sampled	Benzene	Toluene	benzene	Xylenes	TPH-g	TPH-d 1	,1-DCA	1,2-DCA	1,1,1 - TCA	TCE	MTBE	Notes
30 (CC-2)	02/08/00	<0.5	-0.5	-0 =									
50 (00-2)	04/26/00	· · · · ·	<0.5	<0.5	<0.5	<50	<250	<0.5	<0.5	<0.5	<0.5	<0.5	
	04/20/00	<0.5	<0.5	<0.5	<0.5	<100	<250	<0.5	0.7	<0.5	<0.5	<0.5	
81	02/05/99	< 0.5	< 0.5	< 0.5	<0.5	<50	<150	<0.5	<0.5	<0.5	<0.5	-0.5	
× .	07/22/99	0.70	< 0.5	< 0.5	<0.5	<50	<200	< 0.5	< 0.5			<0.5	
						-50	~200	~0.5	~0.3	<0.5	<0.5	<0.5	
94	02/05/99	<0.5	< 0.5	< 0.5	< 0.5	<50	170					<0.5	
	07/22/99	<0.5	< 0.5	< 0.5	< 0.5	<50	<200	< 0.5	< 0.5	< 0.5	< 0.5	<0.5	
										0.0	.0.0	-0.5	
210	02/05/99	< 0.5	< 0.5	< 0.5	<0.5	<50	960					< 0.5	
222	10/20/00												
223	10/26/99	<0.5	<0.5	< 0.5	< 0.5	<100	<200	< 0.5	< 0.5		< 0.5		
	02/10/00	<0.5	<0.5	<0.5	<0.5	<50	640	<0.5	<0.5	<0.5	<0.5	<0.5	
	04/27/00	<0.5	<0.5	<0.5	<0.5	<100	250	<0.5	<0.5	<0.5	<0.5	<0.5	
224	07/26/99	-0.5	-0.5	-0.5	-0.5								
224	0//20/99	<0.5	<0.5	<0.5	<0.5	<50	640	<0.5	<0.5	<0.5	< 0.5	<0.5	
239	07/26/99	55,000	85.0	1,500	190	30,000		<0.5	<0.5	-0.5	-0.5	5 20	
	10/26/99	23,000	53	1,500	103.2	28,000	10,000	<0.5	<0.5	<0.5	< 0.5	5.30	
	02/10/00	40,000	48	1,900	52	44,000	21,000	<0.3 <0.5	<0.5 1.0		< 0.5		
	04/28/00	25,000	540	2,000	710	36,000				<0.5	<0.5	14.0	
	0.120,00	25,000	540	2,000	/10	30,000	12,500	<5.0	<5.0	<5.0	<5.0	<5.0	
241	04/07/99	<0.5	<0.5	<0.5	<0.5	<50	<250	. 				< 0.5	
249	07/22/99	<0.5	<0.5	<0.5	<0.5	<50	<200	<0.5	<0.5	<0.5	<0.5	< 0.5	
277	01122133	<0.5	<0.5	<0.5	<0.5	<20	<200	<0.5	<0.5	<0.5	<0.5	<0.5	

io anto

Notes:

a. Non-diesel peak reported.

b. No diesel pattern detected; result due to high gasoline concentration.

c. Bromodichloromethane detected, 0.84 μ g/L.

d. 8 other volatiles detected by 8260.

e. cis-1,2-DCE detected, 0.7 µg/L.

f. cis-1,2-DCE detected, 0.8 µg/L.

g. Values for benzene and ethylbenzene are estimated.

h. 1,1-DCE detected, 0.9 µg/L.

ŝ.

						Concentration	n (μg/L)				
Well	Date			Ethyl-							
No.	Sampled	Benzene	Toluene	benzene	Xylenes	TPH-g	TPH-d 1,1-DCA 1,2	-DCA 1,1,1-TCA	TCE	MTBE	Notes
	,	tected, 1.6 µg/L									
		tected, 1.4 μg/L roethene detecte									
		loroethene dete									
	,	chloride detect		-							
		chloride detecte	• =								
	•	chloride detecte									
	-	chloride detecte									
	· ·	roethene detecte									
	r. Methylene	chloride detecte	ed at 0.8 µg/L	J.							
	,	roethene detecte									
	,	oethene detecte									
	u. 1,1-Dichlo	roethene detect	ed at 5.2 μg/J	L.							
ND	Not detected.										
		or not sampled.									
μg/L	Micrograms p	er liter.									
TPH-g	Total Datrala	um Hydrocarbo	ne as gasolin	e							
TPH-g TPH-d		um Hydrocarbo		0.							
1,1-DCA	1,1-Dichloroe	•	no up dieben								
1,2-DCA	1,2-Dichloro										
1,1-DCE	1,1-Dichloro										
1,1,1-TCA	1,1,1-Trichlo										
c 1,2-DCE	cis 1,2-Dichl	•									
TCE	Trichloroethe	ene.									
MTBE	Methyl t-but	yl ether.									

Appendix II

Tier I Input Data

といい

.

RBCA TIER 1 Input Data

Site Name: Nestle USA, Inc., Facility

Software: GSI RBCA Spreadsheet

2

		Nestle USA, Inc.,	Facility				Software	: GSI RBCA Spreadsheet			
	Site Location: 0	Jakiano, CA		Completed By:							
NOTE: values	correspond to ASTM (1995) Tier 1 default values	5	(completed by:	JCI						
Exposure			Residential		Commerci	al/Industrial	Surface				
Parameter	Definition (Units)	Adult	(1-6yrs)	(1-16 yrs)	Chronic	Constrctn	Parameters	Definition (Units)	Residential	Constrctn	
ATc	Averaging time for carcinogens (yr)	70					A	Contaminated soil area (cm^2)	2.2E+06	1.0E+06	
ATn	Averaging time for non-carcinogens (yr)	30	6	16	25	1	w	Length of affect, soil parallel to wind (cm)	1.5E+03	1.0E+03	
BW	Body Weight (kg)	70	15	35	70		W.gw	Length of affect, soil parallel to groundwater (cm)	1.5E+03	1.02+03	
ED	Exposure Duration (yr)	30	6	16	25	1	Uair	Ambient air velocity in mixing zone (cm/s)	2.3E+02		
t	Averaging time for vapor flux (yr)	30			25	1	delta	Air mixing zone height (cm)	2.0E+02		1
EF	Exposure Frequency (days/yr)	350			250	180	Lss	Thickness of affected surface soils (cm)	1.0E+02		
EF.Derm	Exposure Frequency for dermal exposure	350			250		Pe	Particulate areal emission rate (g/cm ² /s)	6.9E-14		
IRġw	Ingestion Rate of Water (L/day)	2			1			(3.6.1. 2.6)	0.02-14		
IRs	Ingestion Rate of Soil (mg/day)	100	200		50	100					
IRadj	Adjusted soil ing. rate (mg-yr/kg-d)	1.1E+02			9.4E+01		Groundwate	r Definition (Units)	Value		
IRa.in	Inhalation rate indoor (m^3/day)	15			20		delta.gw	Groundwater mixing zone depth (cm)	2.0E+02		
iRa.out	Inhalation rate outdoor (m ³ /day)	20			20	10	1	Groundwater infiltration rate (cm/yr)	3.0E+01		
SA	Skin surface area (dermal) (cm^2)	5.8E+03		2.0E+03	5.8E+03	5.8E+03	Ugw	Groundwater Darcy velocity (cm/yr)	2.5E+03		
SAadj	Adjusted dermal area (cm ² -yr/kg)	2.1E+03			1.7E+03		Ugw.tr	Groundwater seepage velocity (cm/yr)	6.6E+03		
м	Soil to Skin adherence factor	1					Ks	Saturated hydraulic conductivity(cm/s)	0.02.00		
AAFs	Age adjustment on soil ingestion	FALSE			FALSE		grad	Groundwater gradient (cm/cm)			
AAFd	Age adjustment on skin surface area	FALSE			FALSE		Sw	Width of groundwater source zone (cm)			
tox	Use EPA tox data for air (or PEL based)?	TRUE					Sd	Depth of groundwater source zone (cm)			
gwMCL?	Use MCL as exposure limit in groundwater?	FALSE					phi.eff	Effective porosity in water-bearing unit	3.8E-01		
							foc.sat	Fraction organic carbon in water-bearing unit	1.0E-03		
							BIO?	Is bioattenuation considered?	FALSE		
							BC	Biodegradation Capacity (mg/L)			
	osed Persons to	Residential				al/Industrial					
	osure Pathways				Chronic	Constrctn	Soil	Definition (Units)	Value		
Outdoor Air I							hc	Capillary zone thickness (cm)	5.0E+00	•	
SS.v	Volatiles and Particulates from Surface Soils	FALSE			TRUE	FALSE	hv	Vadose zone thickness (cm)	3.0E+02		-
S.v	Volatilization from Subsurface Soils	FALSE			FALSE		rho	Soil density (g/cm^3)	1.7		
GW.v	Volatilization from Groundwater	FALSE			FALSE		foc	Fraction of organic carbon in vadose zone	0.01		
Indoor Air Pa							phi	Soil porosity in vadose zone	0.38		
S.b	Vapors from Subsurface Soils	FALSE			FALSE		Lgw	Depth to groundwater (cm)	3.0E+02		
GW.b	Vapors from Groundwater	FALSE			FALSE		Ls	Depth to top of affected subsurface soil (cm)	1.0E+02		
Soil Pathway					70/15	E	Lsubs	Thickness of affected subsurface soils (cm)	2.0E+02		
SS.d	Direct Ingestion and Dermal Contact	FALSE			TRUE	FALSE	pН	Soil/groundwater pH	6.5		
Groundwater		FAL 05			EAL OF				capillary	vadose	foundation
GW.i	Groundwater Ingestion	FALSE			FALSE		phi.w	Volumetric water content	0.342	0.12	0.12
S.I	Leaching to Groundwater from all Soils	FALSE			FALSE		phi.a	Volumetric air content	0.038	0.26	0.26
							B. 31 H				
							Building	Definition (Units)	Residential	Commercial	
	Distance -	Dest			C	a l/local scatter and	Lb	Building volume/area ratio (cm)	2.0E+02	3.0E+02	
	ceptor Distance	Distance	dential On-Site		Distance	ial/Industrial	ER	Building air exchange rate (s^-1)	1.4E-04	2.3E-04	
	On- or Off-Site	Distance			Distance	On-Site	Lcrk	Foundation crack thickness (cm)	1.5E+01		
GW S	Groundwater receptor (cm)		TRUE			TRUE	eta	Foundation crack fraction	0.01		
3	Inhalation receptor (cm)		TRUE			TRUE					
							Transport				
Matrix of					•		Transport	Definition (Linite)			
Target Risks		Individual	Cumulative				Groundwate	Definition (Units)	Residential	Commercial	
TRab	Target Risk (class A&B carcinogens)	1.0E-06	Gumulauve	-			ax				
TRc	Target Risk (class A&B carcinogens) Target Risk (class C carcinogens)	1.0E-05					ay	Longitudinal dispersivity (cm)			
THQ	Target Risk (class C carcinogens) Target Hazard Quotient	1.0E-05					az	Transverse dispersivity (cm) Vertical dispersivity (cm)			
Opt	Calculation Option (1, 2, or 3)	1					Vapor	ventual dispersivity (cm)			
Tier	RBCA Tier	1					dcy	Transverse dispersion coefficient (cm)			
							dcz	Vertical dispersion coefficient (cm)			1

Table II.2. RBCA Tier I Input/Output Data Outdoor Air Inhalation of Benzene from Soil Vapor-Onsite Commercial/Industrial Receptor

	Soil Specific Pa	arameters	
ASTM Default	ρa	1.7	Soil Bulk Density (g/cm [^]) of (kg/L)
ASTM Default	θ_{as}	0.26	Air Content of Soil (v/v)
ASTM Default	θ_{ws}	0.12	Water Content of Soil (v/v)
ASTM Default	· θ _t	0.38	Total Soil Porosity (v/v)
Site-Specific	d	91	Depth to location of vapor sample (cm) – 3 ft depth
	Diffusivity Para	meters	
ASTM Default	н	0.22	Henry's Constant (dimensionless)
ASTM Default	D ^{air}	9.30E-02	Air Diffusion Coefficient (cm^/s)
ASTM Default	D ^{wat}	1.10E-05	Water Diffusion Coefficient (cm [^] /s)
Calculated	D ^{eff} s	0.0073	Effective Diffusion Coefficient through Soil (cm^/s)
	Prediction of F	lux from Soil	Vapor Concentration
Site Specific	· C,	9,900	Maximum Benzene Concentration in Soil Vapor (ppbv)
Unit Conv	C,	32	Maximum Benzene Concentration in Soil Vapor (µg/L)
Calculated	F	2.6E-06	Maximum Diffusive Vapor Flux Predicted from Benzene Concentration in Soil Vapor (μg/cm ² -sec)
	Outdoor Air Co	oncentration	
ASTM Default	s	200	Outdoor Mixing Height (cm)
ASTM Default	U _{air} outdoor	225	Outdoor Wind Velocity (cm/sec)
ASTM Default	W	1500	Width of Outdoor Source Area Parallel to Wind Direction (cm)
Calculated	Coutdoor	8.5E-08	Outdoor Air Concentration (µg/cm ³)
	Dose		
ASTM Default	IR airOutdoor	20	Daily Outdoor Inhalation Rate (m ³ /day)
ASTM Defauit	EF	250	Exposure Frequency (days/year)
ASTM Default	ED	25	Exposure Duration (years)
Calculated	Dose	11	Dose (mg)
	Risk		
CAL EPA	SF,	0.1	California Cancer Slope Factor for Benzene(kg-day/mg)
ASTM Default	BW	70	Body Weight (kg)
ASTM Default	AT _c	70	Averaging Time for Carcinogens (years)
Calculated	Risk	5.9E-07	Risk (positive/population)
Calculated	RBSL	17,000	Tier 1 Risk-Based Screening Level (ppbv) for TRL = 1E-06

Notes:

ASTM = American Standard for Testing and Materials, 1995. Standard Guide for Risk Based Corrective Action Applied at Petroleum Release Sites, E 1739-95.

Calculations: Effective diffusivity, diffusive vapor flux, enclosed space air concentrations, dose, and risk calculations from ASTM 95 guidance formulas presented above. level.

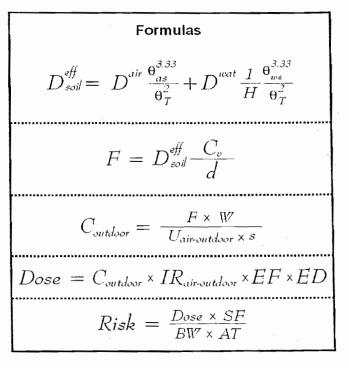


Table II.3. RBCA Tier I Input/Output Data Indoor Air Inhalation of Benzene from Soil Vapor-Onsite Commercial/Industrial Receptor

	Soil/Building P	arameters	
ASTM Default	. ρ _a	1.7	Soil Bulk Density (g/cm^3) of (kg/L)
ASTM Default	θ_{as}	0.26	Air Content of Soil (v/v)
ASTM Default	θ_{ws}	0.12	Water Content of Soil (v/v)
ASTM Default	θ_{ac}	0.26	Air Content of Crack (v/v)
ASTM Default	θ_{wc}	0.12	Water Content of Crack (v/v)
ASTM Default	θι	0.38	Total Porosity-Soil and Crack (v/v)
Site-specific	Lsoil	91	Depth to Location of Vapor Sample (cm) – 3.0 ft depth
ASTM Default	Lcrack	15	Foundation Crack Thickness (cm)
ASTM Default	η	0.01	Foundation Crack Fraction (dimensionless)
	Diffusivity Para	ameters	
ASTM Default	Н	0.22	Henry's Constant (dimensionless)
ASTM Default	\mathbf{D}^{air}	9.30E-02	Air Diffusion Coefficient (cm^2/s)
ASTM Default	D ^{wat}	1.10E-05	Water Diffusion Coefficient (cm^2/s)
Calculated	D ^{eff} soil	0.0073	Effective Diffusion Coefficient through Soil (cm^2/s)
Calculated		0.0073	Effective Diffusion Coefficient through Foundation Cracks (cm^2/s)
	Prediction of F	lux from Soi	Vapor Concentration
Site Specific	C _{source} = C _v	9,900	Maximum Benzene Concentration in Soil Vapor (ppbv)
Unit Conv	$C_{source} = C_v$	32	Maximum Benzene Concentration in Soil Vapor (µg/L)
Calculated	F	1.5E-07	Diffusive Vapor Flux Predicted from Benzene Concentration in Soil
Guiodiatou			Vapor (µg/cm ² -sec)
	Indoor Air Con		Fundament Cross Malume (influention Area Patio (am)
ASTM Default	Lb	300	Enclosed Space Volume/Infiltration Area Ratio (cm)
ASTM Default	ER _{air} indoor	0.00023	Enclosed Space Air Exchange Rate (sec ⁻¹)
Calculated	Cindoor	2.1E-06	Enclosed Space Air Concentration (µg/cm³)
	Dose	20	Daily Indoor Inhalation Rate (m ³ /day)
ASTM Default	IR _{air} indoor	20	Exposure Frequency-Adult (days/year)
ASTM Default	EF	250	• • • • • •
ASTM Default	ED	25	Exposure Duration (years)
Calculated	Dose	260	Dose (mg)
DTOO	Risk	0.4	Inhalation California Cancer Slope Factor for Benzene (kg-day/mg)
DTSC	SF	0.1	
ASTM Default	BW	70	Body Weight (kg) Averaging Time for Carcinogens (years)
ASTM Default	AT Diata E	70	
Calculated	Risk	1.5E-05	Risk (positive/population)
Calculated	RBSL	660.0	Tier I Risk-Based Screening Level (ppbv) for TRL = 1E-06

Notes:

ASTM = American Standard for Testing and Materials, 1995. Standard Guide for Risk Based Corrective Action Applied at Petroleum Release Sites, E 1739-95.

Calculations: Effective diffusivity, diffusive vapor flux, enclosed space air concentrations, dose, and risk calculations from ASTM 95 guidance formulas presented above.

Formulas

$$D_{soil}^{eff} = D^{air} \frac{\theta_{as}^{3.33}}{\theta_T^2} + D^{wat} \frac{1}{H} \frac{\theta_{ws}^{3.33}}{\theta_T^2}$$

$$D_{crack}^{eff} = D^{air} \frac{\theta_{ac}^{3.33}}{\theta_T^2} + D^{wat} \frac{1}{H} \frac{\theta_{wc}^{3.33}}{\theta_T^2}$$

$$D_{crack}^{eff} = \frac{L_{soil} + L_{crack}}{D_{crack}^{eff} \eta} \frac{L_{soil}}{D_{soil}^{eff}}$$

$$F = D_v^{eff} \frac{\Delta C_v}{\Delta \chi}$$

$$= \frac{C_{source}}{L_{soil}} \frac{D_{soil}^{eff}}{L_{soil}}$$

$$C_{indoor} = \frac{F}{ER_{aivindoor} \times L_b}$$

$$Dose = C_{indoor} \times IR_{air-indoor} \times EF \times ED$$

$$Risk = \frac{Dose \times SF}{BW \times AT}$$

Appendix III

Chemical-Specific Data

(🕉

100 - 1122

	INHA	LATION	ORAL		
COPC	RfD	CSF	RfD	CSF	
Benzene	1.70E-03	1.00E-01	NA	NA	
Toluene	1.10E-01	NA	2.00E-01	NA	
Ethylbenzene	2.90E-01	NA	1.00E-01	NA	
Total Xylenes	2.00E-01	NA	2.00E+00	NA	
Methyl t-butyl ether	8.57E-01	1.60E-04	NA	NA	
Acetone	1.00E-01	NA	NA	NA	
1,3-Butadine	NA	1.80E+00	NA	NA	
2-Butanone	2.86E-01	NA	NA	NA	
Carbon Disulfide	2.00E-01	NA	NA	NA	
Chloroform	NA	8.10E-02	NA	NA	
Chloromethane	8.60E-05	6.30E-03	NA	NA	
Cis-1,2-Dichloroethene	1.00E-02	NA	NA	NA	
1,1-Dichloroethane	1.43E-01	NA	NA	NA	
1,2-Dichloroethane	NA	NA	3.00E-02	9.10E-02	
1,2-Dichlorobenzene	5.70E-02	NA	NA	NA	
1,4-Dichlorobenzene	3.00E-02	4.00E-02	NA	NA	
1,4-Dioxane	NA	2.70E-01	NA	NA	
n-Hexane	5.71E-02	NA	NA	NA	
4-Methyl-2-pentanone	2.29E-02	NA	NA	NA	
Methylene chloride	8.57E-01	3.50E-03	NA	NA	
Naphthalene	8.60E-04	NA	2.00E-02	NA	
n-Nonane	6.00E-01	NA	6.00E-01	NA	
Styrene	2.86E-01	NA	NA	NA	
Tetrachloroethene	1.10E-01	2.10E-02	NA	NA	
Tetrahydrofuran	8.60E-02	6.80E-03	NA	NA	
Trichloroethene	NA	1.00E-02	NA	NA	
1,1,1-Trichloroethane	2.86E-01	NA	NA	NA	
1,3,5-Trimethylbenzene	1.70E-03	NA	NA	NA	
1,2,4-Trimethylbenzene	1.70E-03	NA	NA	NA	

Table III.1 Chemical Toxicity Data

NA = Not applicable for evaluation of complete exposure pathways

COPC = Chemical of Potential Concern

RfD = Reference Dose (mg/kg-day)

100

÷

ŝ

<u>لة</u>

CSF = Cancer Slope Factor 1/(mg/kg-day)

Source: IRIS (USEPA 2000), HEAST (USEPA, 1997), DTSC (1994). Region IX PRGs (USEPA, 1999), OEHHA (2000)

Table III.2
Chemical and Physical Properties for COPCs

	Henry's Law Constant	Diffusion Coefficient in air	Diffusion Coefficient in water	Lon Kee
COPC .	(dim)	(cm2/sec)	(cm2/sec)	Log Koc (log l/kg)
Benzene	2.20E-01	9.30E-02	1.10E-05	NA NA
Toluene	2.60E-01	8.50E-02	9.40E-06	2.13E+00
Ethylbenzene	3.20E-01	7.60E-02	8.50E-06	1.98E+00
Total Xylenes	2.90E-01	7.20E-02	8.50E-06	2.38E+00
Methyl t-butyl ether	2.40E-02	7.90E-02	9.41E-05	NA
Acetone	1.04E-03	1,24E-01	1.14E-05	<u>NA</u>
1,3-Butadine	7.00E+00	1.70E-02	1.00E-05	NA
2-Butanone	1.81E-03	8.08E-02	9.80E-06	NA NA
Carbon Disulfide	6.99E-01	1.04E-01	1,00E-05	NA
Chloroform	1.41E-01	1.00E-01	1.00E-05	NA
Chloromethane	3.67E-01	1.30E-01	1.68E-04	NA
Cis-1,2-Dichloroethylene	2.00E-01	7.00E-02	1.00E-05	NA
1,1-Dichloroethane	2.00E-01	7.00E-02	1.00E-05	NA
1,2-Dichloroethane	4.00E-02	1.00E-01	1.00E-05	1.76E+00
1,2-Dichlorobenzene	8.07E-02	6.90E-02	7.90E-06	NA
1,4-Dichlorobenzene	6.65E-02	6.90E-02	7.90E-06	NA
1,4-Dioxane	4.00E-04	1.00E-04	1.00E-05	NA
n-Hexane	5.07E+00	2.00E-01	7.77E-06	2.94E+00
4-Methyl-2-pentanone	1.73E-02	7.35E-02	8.68E-05	NA
Methylene chloride	1.33E-01	1.00E-01	1.17E-05	NA
Naphthalene	4.90E-02	7.20E-02	9.40E-06	3.11E+00
n-Nonane	5.00E+00	2.00E-01	7.00E-06	2.90E+00
Styrene	1.09E-01	7.10E-02	8.00E-06	NA
Tetrachloroethene	1.21E+00	7.20E-02	8.20E-06	NA
Tetrahydrofuran	2.20E-01	1.00E-01	1.00E-05	NA
richloroethene	4.00E-01	8.00E-02	9.00E-06	NA
1,1,1-Trichloroethane	7.15E-01	7.80E-02	8.80E-06	NA
,3,5-Trimethylbenzene	3.00E-01	2.40E-04	7.10E-06	NA
,2,4-Trimethylbenzene	2.00E-01	4.10E-05	7.10E-06	NA

NA = Not applicable for evaluation of complete exposure pathways dim = dimensionless COPC = Chemical of Potential Concern Koc = Organic-carbon partition coefficient Source: Region IX PRGs (USEPA, 1999); ASTM (1995, 1998)

2

ಕ ಖ

1 5-66

y y - Allerander

> : 7 1.0

7 8

1

1 5 M

Appendix IV

Tier I Output Data

10000

1.1.1

Sec. And

Same and

acility SOIL RBSL VALI 4 Ft BGS)		Target	k (Class A & B) Risk (Class C) lazard Quotient	1.0E-5 1.0E+0	0 PI	EL expo	osure limit? osure limit?			culation Option:	1	1 OF 1					
		Target	Risk (Class C) azard Quotient	1.0E-5 1.0E+0	0 PI	EL expo	osure limit?			culation Option:	1	1 OF 1					
		Target	Risk (Class C) azard Quotient	1.0E-5 1.0E+0	0 PI	EL expo	osure limit?			culation Option:	1						
		-	azard Quolient	1.0E+0													
4 Ft BGS)	Representative	Target H			posure	e Pathwa					<u> </u>						
	Representative		RBSL Result	s For Complete Ex	posure	e Pathwa	avs ("x" if Com	alata									
	Representative							netej	RBSL Results For Complete Exposure Pathways ("x" if Complete)								
	Concentration					Innostic			Construction	Annibashia	RBSL	-					
RN	concentration	So	il Leaching to	Groundwater					Worker	RBSL	Exceeded ?	Required CRF					
	(mg/kg)	Residential: (on-site)	Commercial: (on-site)	Regulatory(MCL): (on-site)			Commercial: (on-site)	Ċ	Commercial: (on-site)	(mg/kg)	"■" If yes	Only if "yes" let					
ne, 1,2-	2.5E-3	NA	NA	NA	N	NA	1.0E+0		NA	1.0E+0		<1					
e	2.7E-3	NA	NA	NA	N	NA	3.4E+3		NA	3.4E+3		<1					
	2.0E-3	NA	NA	NA	N	NA	6.4E+3		NA	6.4E+3		<1					
ed isomers)	2.7E-3	NA	NA	NA	N	NA	6.6E+4		NA	6.6E+4		<1					
•	ne, 1,2- e	(mg/kg) ne, 1,2- e 2.7E-3 2.7E-3 2.0E-3	So So (mg/kg) Residential: (on-site) ne, 1,2- 2.5E-3 NA e 2.7E-3 NA 2.0E-3 NA	Soil Leaching to former cial: Commercial: (mg/kg) Residential: Commercial: (ne, 1,2- 2.5E-3 NA NA a 2.7E-3 NA NA 2.0E-3 NA NA	Soil Leaching to Groundwater (mg/kg) Residential: (on-site) Commercial: (on-site) Regulatory(MCL): (on-site) ne, 1,2- 2.5E-3 NA NA NA a 2.7E-3 NA NA NA 2.0E-3 NA NA NA	RN Soil Leaching to Groundwater X (mg/kg) Residential: (on-site) Commercial: (on-site) Regulatory(MCL): (on-site) Residential: (on-site) ne, 1,2- 2.5E-3 NA NA NA 2.7E-3 NA NA NA NA 2.0E-3 NA NA NA NA	RN Soil Leaching to Groundwater X and Definitiant (mg/kg) Residential: (on-site) Commercial: (on-site) Regulatory(MCL): (on-site) Residential: (on-site) Residential: (on	Soil Leaching to Groundwater X and Dermal Contact (mg/kg) Residential: (on-site) Commercial: (on-site) Regulatory(MCL): (on-site) Residential: (on-site) Commercial: (on-site) ne, 1,2- 2.5E-3 NA NA NA NA 2.7E-3 NA NA NA NA 3.4E+3 2.0E-3 NA NA NA NA A	RN Soil Leaching to Groundwater X and Dermal Contact (mg/kg) Residential: (on-site) Commercial: (on-site) Regulatory(MCL): (on-site) Residential: (on-site) Commercial: (on-site) Commercial: (on-site)	RN Soil Leaching to Groundwater X and Dermal Contact Worker (mg/kg) Residential: (on-site) Commercial: (on-site) Regulatory(MCL): (on-site) Residential: (on-site) Commercial: (on-site) Commer	RN Soil Leaching to Groundwater X and Dermai Contact Worker RBSL (mg/kg) Residential: (on-site) Commercial: (on-site) Regulatory(MCL): (on-site) Residential: (on-site) Commercial: (on-site) Commercial: (on-site) </td <td>RN Soil Leaching to Groundwater X and Dermal Contact Worker Residentiat: Commercial: Main of the second second</td>	RN Soil Leaching to Groundwater X and Dermal Contact Worker Residentiat: Commercial: Main of the second					

>Res indicates risk-based target concentration greater than constituent residual saturation value

© Groundwater Services, Inc. (GSI), 1995-1997. All Rights Reserved.

Software: GSI RBCA Spreadsheet Version: 1.0.1 Serial: G-273-IBX-894

	RBCA TI	ER I OUTPUT DAT	A-OFFSIT	E RESIDEN	ITIAL RECEPT	ORS				Table	e IV.2	
Site Name: NE	STLE OAKLAND FACILITY		Completed By	/: JCI								1 OF 1
GROUNDWATER RBSL VALUES			Target Risk (Class A & B) 1.0E-6 Image: MCL exposure limit? Target Risk (Class C) 1.0E-5 Image: PEL exposure limit? Target Hazard Quotient 1.0E+0 Image: PEL exposure limit?			Calculation Option: 1						
				RBSI	Results For Com	plete Exposure	Pathways ("x" if	Complete)				
CONSTITUEN	TS OF CONCERN	Representative Concentration		Groundwater	Ingestion		iter Volatilization ndoor Air	-	ter Volatilization utdoor Air	Applicable RBSL	RBSL Exceeded ?	Required CRF
CAS No.	Name	(mg/L)	Residential: (on-site)	Commercial: (on-site)	Regulatory(MCL): (on-site)	Residential: (off-site)	Commercial: (on-site)	Residential (off-site)	Commercial: (on-site)	(mg/L	" II " If yes	Only if "yes" le
71-43-2	Benzene	1.8E-2	NA	NA	NA	7.0E-3	NÄ	3.2E+0	NA	7.0E-3	1	-
156-59-2	Dichloroethene, cis-1,2-	2.3E-3	NA	NA	NA	7.8E-1	NA	4.1E+2	NA	7.8E-1		-
75-34-3	Dichloroethane, 1,1-	8.7E-2	NA	NA	NA	2.1E+1	NA	1.1E+4	NA	2.1E+1		-
107-06-2	Dichloroethane, 1,2-	1.7E-1	NA	NA	NA	2.2E-2	NA	7.5E+0	NA	2.2E-2		-
100-41-4	Ethylbenzene	2.2E-3	NA	NA	NA	7.7E+1	NA	3.7E+4	NA	7.7E+1		-
1634-04-4	Methyl t-Butyl Ether	5.6E-2	NA	NA	NA	2.4E+1	NA	3.6E+3	NA	2.4E+1		-
79-01-6	Trichloroethene	1.9E-3	NA	NA	NA	2.8E-2	NA	8.0E+0	NA	2.8E-2		
108-88-3	Toluene	2.0E-2	NA	NA	NA	3.3E+1	NA	1.6E+4	NA	3.3E+1		-
1330-20-7	Xylene (mixed isomers)	1.3E-2	NA	NA	NA	6.1E+2	NA	2.9E+5	NA	6.1E+2		-

>Sol indicates risk-based target concentration greater than constituent solubility

© Groundwater Services, Inc. (GSI), 1995-1997. All Rights Reserved.

Ľ

Software: GSI RBCA Spreadsheet Version: 1.0.1 Serial: G-273-IBX-894

Table IV.3. RBCA Tier I Output Data Tier I Risk and RBSL Sample Calculation Outdoor Air Inhalation of Benzene from Soil Vapor-Onsite Commercial/Industrial Receptor

	Soil Specific P	ramotora							
ASTM Default		1.7	Sail Pulk Density (alom [*]) of (1-11)						
ASTM Default	ρ _a θ _{as}	0.26	Soil Bulk Density (g/cm [°]) of (kg/L)						
ASTM Default			Air Content of Soil (v/v)						
ASTM Default	θ _{ws}	0.12	Water Content of Soil (v/v)						
	θι	0.38	Total Soil Porosity (v/v)						
Site-Specific	d	91	Depth to location of vapor sample (cm) ~ 3 ft depth						
	Diffusivity Para								
ASTM Default	H	0.22	Henry's Constant (dimensionless)						
ASTM Default	D ^{air}	9.30E-02	Air Diffusion Coefficient (cm ² /s)						
ASTM Default	D ^{wat}	1.10E-05	Water Diffusion Coefficient (cm [^] /s)						
Calculated	D ^{eff} s	0.0073	Effective Diffusion Coefficient through Soil (cm ⁴ /s)						
Prediction of Flux from Soil Vapor Concentration									
Site Specific	C,	9,900	Maximum Benzene Concentration in Soil Vapor (ppbv)						
Unit Conv	C _v	32	Maximum Benzene Concentration in Soil Vapor (µg/L)						
Calculated	F	2.6E-06	Maximum Diffusive Vapor Flux Predicted from Benzene						
			Concentration in Soil Vapor (µg/cm ² -sec)						
	Outdoor Air Co								
ASTM Default	S	200	Outdoor Mixing Height (cm)						
ASTM Default	U _{air} outdoor	225	Outdoor Wind Velocity (cm/sec)						
ASTM Default	W	1500	Width of Outdoor Source Area Parallel to Wind Direction (cm)						
Calculated	Coutdoor	8.5E-08	Outdoor Air Concentration (µg/cm ³)						
	Dose								
ASTM Default	IR _{air} Outdoo r	20	Daily Outdoor Inhalation Rate (m ³ /day)						
ASTM Default	EF	250	Exposure Frequency (days/year)						
ASTM Default	ED	25	Exposure Duration (years)						
Calculated	Dose	11	Dose (mg)						
	Risk								
CAL EPA	SF	0.1	California Cancer Slope Factor for Benzene(kg-day/mg)						
ASTM Default	BW	70	Body Weight (kg)						
ASTM Default	ATc	70	Averaging Time for Carcinogens (years)						
Calculated	Risk	5.9E-07	Risk (positive/population)						
Calculated	RBSL	17,000	Tier 1 Risk-Based Screening Level (ppbv) for TRL = 1E-06						

Formulas $D_{\text{soil}}^{\text{eff}} = D_{\text{or}}^{\text{air}} \frac{\theta_{\text{as}}^{3.33}}{\theta_{\tau}^2} + D_{\text{wat}}^{\text{wat}} \frac{1}{H} \frac{\theta_{\text{ws}}^{3.33}}{\theta_{\tau}^2}$ $F = D_{\text{soil}}^{\text{eff}} - \frac{C_v}{J}$ $C_{outdoor} = \frac{F \times W}{U_{air-outdoor} \times s}$ $Dose = C_{outdoor} \times IR_{air-outdoor} \times EF \times ED$ $Risk = \frac{Dose \times SF}{BW \times AT}$

Notes:

ASTM = American Standard for Testing and Materials, 1995. Standard Guide for Risk Based Corrective Action Applied at Petroleum Release Sites, E 1739-95.

Calculations: Effective diffusivity, diffusive vapor flux, enclosed space air concentrations, dose, and risk calculations from ASTM 95 guidance formulas presented above. level.

	Indo	or Air li	Table IV.4. RBCA Tier I Out Tier I Risk and RBSL Sample Ca nhalation of Benzene from Soil Vapor-Onsi	alculation	ercial/Industrial Receptor
	Soil/Building Par	ameters	· · · · · · · · · · · · · · · · · · ·	r	
ASTM Default	ρa	1.7	Soil Bulk Density (g/cm^3) of (kg/L)		Formulas
ASTM Default	θ_{as}	0.26	Air Content of Soil (v/v)		
ASTM Default	θ_{ws}	0.12	Water Content of Soil (v/v)		peff pair 0 ^{3.33} pwat
ASTM Default	Θ_{ac}	0.26	Air Content of Crack (v/v)		$D_{soil}^{\text{eff}} = D^{air} \frac{\theta^{3.33}}{\theta^2} + D^{wat}$
ASTM Default	θως	0.12	Water Content of Crack (v/v)		Θ_T
ASTM Default	Θ_t	0.38	Total Porosity-Soil and Crack (v/v)		
Site-specific	Lsoil	91	Depth to Location of Vapor Sample (cm) – 3.0 ft depth		$D^{\text{eff}}_{\text{mark}} = D^{air} \frac{\theta^{3.33}}{ac} + D^{wat}$
ACTM Default	1	15			

, 1058 G. 200 A.

	ASTM Default	θ _{wc}	0.12	Water Content of Crack (v/v)
	ASTM Default	Θ_t	0.38	Total Porosity-Soil and Crack (v/v)
	Site-specific	Lsoil	91	Depth to Location of Vapor Sample (cm) - 3.0 ft depth
	ASTM Default	Lcrack	15	Foundation Crack Thickness (cm)
1	ASTM Default	η	0.01	Foundation Crack Fraction (dimensionless)
		Diffusivity Pa	rameters	
	ASTM Default	Н	0.22	Henry's Constant (dimensionless)
	ASTM Default	D ^{air}	9.30E-02	Air Diffusion Coefficient (cm^2/s)
	ASTM Default	D ^{wat}	1.10E-05	Water Diffusion Coefficient (cm ² /s)
	Calculated	D ^{eff} soil	0.0073	Effective Diffusion Coefficient through Soil (cm^2/s)
	Calculated	D ^{eff} crack	0.0073	Effective Diffusion Coefficient through Foundation Cracks (cm^2/s)
		Prediction of	Flux from Soil	Vapor Concentration
	Site Specific	C _{source} = C _v	9,900	Maximum Benzene Concentration in Soil Vapor (ppbv)
	Unit Conv	$C_{source} = C_v$	32	Maximum Benzene Concentration in Soil Vapor (µg/L)
	Calculated	F	1.5E-07	Diffusive Vapor Flux Predicted from Benzene Concentration in Soil Vapor (μ g/cm ² -sec)
		Indoor Air Co	ncentration	•
	ASTM Default	Lb	300	Enclosed Space Volume/Infiltration Area Ratio (cm)
	ASTM Default	ERaicindoor	0.00023	Enclosed Space Air Exchange Rate (sec ⁻¹)
1	Calculated	Cindoor	2.1E-06	Enclosed Space Air Concentration (µg/cm ³)
		Dose	•	
	ASTM Default	IR airindoor	20	Daily Indoor Inhalation Rate (m ³ /day)
	ASTM Default	EF	250	Exposure Frequency-Adult (days/year)
	ASTM Default	ED	25	Exposure Duration (years)
	Calculated	Dose	260	Dose (mg)
		Risk		
	DTSC	SFI	0.1	Inhalation California Cancer Slope Factor for Benzene (kg-day/mg)
	ASTM Default	BW	70	Body Weight (kg)
	ASTM Default	AT	70	Averaging Time for Carcinogens (years)
	Calculated	Risk	1.5E-05	Risk (positive/population)
	Calculated	RBSL	660.0	Tier I Risk-Based Screening Level (ppbv) for TRL = 1E-06

 Θ_{ws} $D_{crack}^{u} = D^{air} \frac{\theta_{ac}}{\theta_{T}^{2}} + D^{wat} \frac{1}{H} \frac{\theta_{wc}^{3,33}}{\theta_{T}^{2}}$ $D_{c}^{eff} = \frac{\underline{L_{soil} + L_{crack}}}{\underbrace{\frac{L_{crack}}{D_{crack}^{eff}} + \underbrace{\frac{L_{soil}}{D_{soil}^{eff}}}}$ $F = D_v^{\text{eff}} \, \frac{\Delta C_v}{\Delta \chi}$ $=\frac{C_{\text{source}} \frac{D_{\text{soil}}^{\text{eff}}}{L_{\text{soil}}}}{1 + \frac{D_{\text{soil}}^{\text{eff}}}{L_{\text{soil}} \frac{L_{\text{crack}}}{D_{\text{crack}}^{\text{eff}} \eta}}$ $C_{indoor} = \frac{F}{ER_{air-indoor} \times L_b}$ $Dose = C_{indoor} \star IR_{air-indoor} \star EF \star ED$ $Risk = \frac{Dose \times SF}{BW \times AT}$

Notes:

ASTM = American Standard for Testing and Materials, 1995. Standard Guide for Risk Based Corrective Action Applied at Petroleum Release Sites, E 1739-95.

Calculations: Effective diffusivity, diffusive vapor flux, enclosed space air concentrations, dose, and nsk calculations from ASTM 95 guidance formulas presented above.

Appendix V

TPH RBSL and SSTL Calculations

ENG:

APPENDIX V TPH RBSL and SSTL Analysis

There are two common ways of assessing potential risks from hydrocarbon mixtures. One method involves selection of indicator constituents (e.g. BTEX) and assessing risks to only these chemicals. The assumption inherent in this approach is that the indicator constituents represent the majority of the risk, and the constituents in the mixture that are not assessed contribute a negligible amount to the total risk.

A second method for assessing the potential risks from constituent mixtures involves separating the mixture into constituent fractions and selecting surrogate compounds to represent the toxicity and mobility of each fraction. It is not necessary for the surrogate compound to be present in the fraction, as long as there is reasonable certainty that the surrogate compound has similar or greater toxicity and similar or greater mobility than compounds that are known to exist in the fraction.

The surrogate compound approach generally yields lower, more conservative screening levels for TPH (MDEP, 1994; Montgomery Watson, 1996); hence, this approach was used to develop RBSLs for TPH at the Nestle site. It should be noted that potential risks associated with indicator chemicals is already addressed through development of RBSLs for individual hydrocarbon compounds detected at the site. Making use of the surrogate chemical approach, RBSLs were developed for TPH-g and TPH-d, where applicable.

V-1 TPH CHARACTERISTICS

Toxicity values are available for a limited number of petroleum hydrocarbons; thus, the approach taken evaluated select surrogate constituents that represent gasoline-range and diesel-range compounds. The variability in constituent composition of the commercial products refined from crude oil is exacerbated by the inability to obtain a constituent-specific breakdown of hydrocarbon mixtures, as the high cost of constituent analyses outweighs usefulness of the data.

General criteria for selecting indicator or surrogate compounds include:

- Percent contribution of constituent in a given petroleum product;
- Mobility and persistence in the environmental media; and
- Availability of human toxicity criteria.

V-1.1 Gasoline

ŧ

ŗ,¥

1 2

1448

and the second

.

Gasoline is a hydrocarbon mixture produced for use in internal combustion engines. The composition of gasoline mixtures has varied over time among different refineries and among different sources of the crude oil feedstock. Commercial gasoline is generally reported in the literature as having a boiling point range of approximately 40 degrees C to 200-210 degrees C, encompassing carbon numbers from C_4/C_5 to C_{11}/C_{12} . The composition of gasoline typically is as follows:

- 49 to 62 percent alkanes (15 to 17 percent straight chain and 28 to 36 percent branched chain);
- 3 to 5 percent cyclolkanes;
- 1 to 11 percent alkenes;
- 20 to 49 percent alkylated benzenes (including benzene); and
- less than 1 percent naphthalenes.

The branched-chain alkanes and aromatic constituents increase the octane rating of the gasoline, and the presence of these constituents has slightly increased as alkyl leads have been phased out.

The ASTM Standard Specification for Automotive Spark-Ignition Engine Fuel, D 4814, indicates that the average percentages of aliphatic and aromatic fractions in gasoline are 60 percent and 40 percent respectively. A USEPA reference dose is available for only one alkane, n-hexane, which is present in gasoline at an average of 6.65 percent by weight (EMCON, 1995). BTEX comprises the largest fraction of the monocyclic aromatic constituents and specific screening levels for each of these compounds are presented in this report. Based on the boiling point range, polycyclic aromatic hydrocarbons (PAHs) are not expected to be prevalent in gasoline with naphthalene reported at an average weight percent of 0.79 percent (EMCON, 1995). Benzo(a)pyrene has been reported at 0.19 to 2.8 ppm. These low PAH concentrations are corroborated by Cline et al. (1991), who cite data that 0.2 to 0.5 percent by volume naphthalene, 3.9 ppm benzo(b)flouranthene, and 1.8 ppm anthracene were present in a gasoline sample.

Commercial gasoline also contains a variety of additives to improve fuel performance, or to act as antioxidants, metal scavenging agents, or as deicing agents. From the 1920's until approximately 1981, alkyl leads were added to gasoline as anti-knock agents. To scavenge the lead as volatile lead halide salts, 1,2-dibromomethane and 1,2-dichloroethane were also added. With the phase-out of alkyl leads, additives such as t-butyl alcohol, methanol, ethanol, and MTBE are used as anti-knock agents. Alcohols also serve as deicing agents and to inhibit water separation.

V-1.2 Diesel Fuels

5

Į P

. *

THE PARTY

15.00

100

3

100

Diesel fuels are products prepared for use in diesel engines for a variety of vehicles (e.g. automobiles, trucks, diesel locomotives, and boats) as well as other small engines. Diesel products are from the middle distillate range, and are characterized by boiling points ranging from 150 to 400 degrees C, with the carbon range C_9 to C_{22} . As a further definition, kerosene is a light fraction within this diesel range, with a boiling point range of 180 to 230 degrees C, and a carbon range of C_{11} to C_{12} . Diesel has been reported to contain the following classes of constituents:

- 64 percent aliphatic hydrocarbons;
- 1 to 2 percent alkenes; and
- 35 percent aromatic hydrocarbons and 2-to 3-ring PAHs.

However, it is expected that these amounts will vary with the specific type of diesel and the sources.

Given the boiling point range, very low concentrations of benzene are expected in diesel fuels. Millner et al. (Millner, 1992) state that diesel typically has less than 0.02 percent benzene. Additionally, the boiling point range of diesel is below the boiling points of most of the 3-ring and larger PAHs, so the PAHs in diesel are largely of the naphthalene class. n-alkanes have also been reported in diesel, with constituents from n-undecane to nonadecane composing 10 to 63 weight percent of samples analyzed.

V-2 SELECTION OF SURROGATE COMPOUNDS

Surrogate compounds were selected based on the above analysis and a review of available literature (Purdy, 1957; Gruse and Stevens, 1960; Speight, 1980 and 1991; Bruya and Friedman, 1992; Millner, 1992; and Anon, 1994). Specifically, n-Hexane and n-nonane were selected as surrogate compounds for the aliphatic fraction of gasoline and diesel, respectively. Naphthalene was used as the surrogate compound for the aromatic fraction of gasoline and diesel.

Use of these compounds is consistent with documented composition of the target hydrocarbons and with the conservative nature of this analysis, as the selected compounds are considered the most mobile and/or toxic within hydrocarbon mixtures. For example, n-nonae is more mobile in the environment than larger alkanes, with higher neurotoxic effects than larger chain length compounds. Also, the relative ability of n-nonae to produce toxic effects is similar whether the exposure occurs via inhalation or oral exposure route. Naphthalene has a short half-life in the

environment because of its tendency to volatilize and biodegrade; however, its exposure to humans has manifested in hemolytic anemia (ATSDR, 1994). Selection of these constituents as surrogates is also consistent with approaches implemented at other sites in the San Francisco Bay Area (e.g. Montgomery Watson, 1996) and with MDEP (1994) guidance.

V-3 CALCULATION OF TPH RBSLs and SSTLs

5 B

۲Ŗ

Tables V-1 and V-2 document RBSLs for TPH-g and TPH-d in soil, respectively, accounting for direct exposure of daily site occupants to surface soils. The TPH RBSLs are based on the weight percent distribution of each of the surrogate compounds, also presented on Tables V-1 and V-2.

Table V-1.TPH-g Surface Soil RBSL Calculation
Onsite Commercial/Industrial Receptor

ALC: NOT OF	Surrogate Chemical	Chemical-Specific RBSL (mg/kg)	Percent Distribution (by weight)	TPH-g RBSL (mg/kg)
	Aliphatic (n-Hexane			
	as surrogate)	2,000	60 %	3,333
	Aromatic			
	Naphthalene as	560	40 %	1,400
	surrogate)			

Under the surrogate compound approach, the TPH RBSL is calculated by dividing the constituent-specific screening level for the surrogate compound in soil by the weight percent of the fraction the surrogate compound represents. Constituent-specific screening levels were calculated based on the previously referenced ASTM (1995 and 1998) algorithms.

As indicated in Table V-1, the TPH-g soil RBSL based on the surrogate approach approximates 1,400 mg/kg. This RBSL corresponds to the more conservative value derived from the aromatic fraction.

Table V-2. TPH-d Surface Soil RBSL Calculation Onsite Commercial/Industrial Receptor

Surrogate Chemical	Chemical-Specific RBSL (mg/kg)	Percent Distribution (by weight)	TPH-d RBSL (mg/kg)
Aliphatic (n-nonane as			
surrogate)	. 10,000	65 %	15,384
Aromatic (Naphthalene as			
surrogate)	560	35 %	1,600

As indicated in Table V-2, the TPH-d soil RBSL based on the surrogate approach (aromatic fraction) approximates 1,600 mg/kg.

Table V-3 depicts use of the surrogate approach for development of shallow soil vapor RBSLs for TPH-g. As indicated, conservative TPH-g RBSLs of 1,500,000 ppbv and 65,000 ppbv are derived using the surrogate (aromatic fraction) approach for the volatilization to outdoor air and indoor air pathways, respectively.

Table V-3. TPH-g Soil Vapor RBSL Calculation Onsite Commercial/Industrial Receptor

Exposure Pathway	Surrogate Chemical	Chemical- Specific RBSL (ppbv)	Percent Distribution (by weight)	TPH-g RBSL (ppbv)
Volatilization to	Aliphatic (n-Hexane			
Outdoor Air	as surrogate)	14,000,000	60 %	2.33E+07
Volatilization to	Aromatic			
Outdoor Air	(Naphthalene as surrogate)	610,000	40 %	1,500,000
Volatilization to	Aliphatic (n-Hexane			
Indoor Air	as surrogate)	560,000	60 %	933,000
Volatilization to	Aromatic			
Indoor Air	(Naphthalene as . surrogate)	26,000	40 %	65,000

Because the Tier I TPH-g RBSL for indoor air (65,000 ppbv) is exceeded by the site maximum TPH-g shallow soil vapor concentration (750,000 ppbv), a Tier II SSTL was developed using the same approach. The chemical-specific SSTLs, as documented in Table V-4, were based on Tier II input data documented in Section 3.3 of this Memorandum. Based on the Tier II TPH-g SSTL for indoor air inhalation approximates 4,000,000 ppbv. This SSTL is protective of the maximum TPH-g concentration (750,000 ppbv) detected in shallow soil vapor samples underlying the site.

-

1

18

STATES AND A STATES

Table V-4. TPH-g Soil Vapor SSTL Calculation Onsite Commercial/Industrial Receptor

Exposure Pathway	Surrogate Chemical	Chemical- Specific SSTL (ppbv)	Percent Distribution (by weight)	TPH-g SSTL (ppby)
Volatilization to	Aliphatic (n-Hexane			
Indoor Air	as surrogate)	37,000,000	60 %	62,000,000
Volatilization to Indoor Air	Aromatic (Naphthalene as surrogate)	1,600,000	40 %	4,000,000

Appendix VI

Tier II Output Data

Table VI.1. RBCA Tier II Input/Output DataTier 2 Risk and SSTL CalculationIndoor Air Inhalation of Benzene from Soil Vapor-Onsite Commercial/Industrial Receptor

Soli//Building ParametersASTM Default ρ_a 1.7Soli Builk Density (g/cm^3) of (kg/L)Oakland ULR θ_{as} 0.15Air Content of Soli (v/v)Oakland ULR θ_{as} 0.15Air Content of Soli (v/v)Oakland ULR θ_{ac} 0.15Air Content of Crack (v/v)Oakland ULR θ_{ac} 0.25Water Content of Crack (v/v)Oakland ULR θ_{ac} 0.25Water Content of Crack (v/v)Oakland ULR θ_{ac} 0.25Water Content of Crack (v/v)Site-specificLsoil91Depth to Location of Vapor Sample (cm) – 3.0 ft depthASTM DefaultLcrack15Foundation Crack Traction (dimensionless)Diffusivity ParametersASTM DefaultH0.22Henry's Constant (dimensionless)ASTM DefaultD ^{mat} 1.10E-05Water Diffusion Coefficient (cm^2/s)CalculatedD ^{eff} _{sol} 0.0011Effective Diffusion Coefficient through Soil Vapor (pp/v)Unit ConvC _{source} = Cv9.900Maximum Benzene Concentration in Soil Vapor (pp/l)Unit ConvC _{source} = Cv3.2Maximum Benzene Concentration in Soil Vapor (µg/L)Diffusive Vapor Flux Predicted from Benzene Concentration in Soil Vapor (µg/cm ² -sec)				
Oakland ULR θ_{ss} 0.15Air Content of Soil (V/v)Oakland ULR θ_{ss} 0.25Water Content of Soil (V/v)Oakland ULR θ_{ss} 0.25Water Content of Soil (V/v)Oakland ULR θ_{ss} 0.25Water Content of Crack (V/v)Site-specificLsoil91Depth to Location of Vapor Sample (cm) – 3.0 ft depthASTM DefaultLcrack15Foundation Crack Traction (dimensionless)Diffusivity ParametersASTM DefaultH0.22Henry's Constant (dimensionless)ASTM DefaultD ^{ast} 9.30E-02Air Diffusion Coefficient (cm^2/s)CalculatedD ^{eff} and0.0011Effective Diffusion Coefficient through Soil (cm^2/s)CalculatedD ^{eff} and0.0011Effective Diffusion Coefficient through Foundation Cracks (cm*2/s)Prediction of Flux from Soil Vapor ConcentrationSoil Vapor (ppv)Unit ConvC _{source} = C _v 32Maximum Benzene Concentration in Soil Vapor (ppv)Unit ConvC _{source} = C _v 32Maximum Benzene Concentration in Soil Vapor (ppv)Unit ConvC _{source} = C _v 32Maximum Benzene Concentration in Soil Vapor (µg/cm ²)CalculatedF2.2E-09Diffusive Vapor Flux Predicted from Benzene Concentration in SoilASTM DefaultLb300Enclose		Soil/Building	Parameters	
Oakland ULR θ_{ws} 0.25Water Content of Soli (V/V)Oakland ULR θ_{ws} 0.25Water Content of Soli (V/V)Oakland ULR θ_{ws} 0.25Water Content of Crack (V/V)Oakland ULR θ_{ws} 0.25Water Content of Crack (V/V)Oakland ULR θ_{ws} 0.25Water Content of Crack (V/V)Oakland ULR θ_{v} 0.40Total Porosity-Soil and Crack (V/V)Site-specificLsoil91Depth to Location of Vapor Sample (cm) – 3.0 ft depthASTM DefaultLcrack15Foundation Crack Thickness (cm)Oakland ULR η 0.001Foundation Crack Fraction (dimensionless)Diffusivity ParametersASTM DefaultD ^{air} 9.30E-02Air Diffusion Coefficient (cm^2/s)ASTM DefaultD ^{wist} 1.10E-05Water Diffusion Coefficient through Soil (cm^2/s)CalculatedD ^{eff} _{soil} 0.0011Effective Diffusion Coefficient through Soil (cm^2/s)CalculatedD ^{eff} _{soil} 0.0011Effective Diffusion Coefficient through Foundation Cracks (cm^2/s)Prediction of Flux from Soil Vapor ConcentrationSoil Vapor (ppbv)Unit ConvCalculatedF2.2E-09Diffusive Vapor Flux Predicted from Benzene Concentration in Soil Vapor (µg/ch ² -sec)Indoor Air ConcentrationSole Air ConcentrationArea Ratio (cm)ASTM DefaultLb300Enclosed Space Air Exchange Rate (sec ⁻¹)CalculatedC _{rador} 3.2E-08Enclosed Space Air Concentration (µg/cm ³)DoseDose		ρ _a	1.7	Soil Bulk Density (g/cm^3) of (kg/L)
Oakland ULR θ_{ac} 0.15Air Content of Crack (v/v)Oakland ULR θ_{ac} 0.15Air Content of Crack (v/v)Oakland ULR θ_{ac} 0.25Water Content of Crack (v/v)Oakland ULR θ_{t} 0.40Total Porosity-Soil and Crack (v/v)Oakland ULR θ_{t} 0.40Total Porosity-Soil and Crack (v/v)Site-specificLsoil91Depth to Location of Vapor Sample (cm) – 3.0 ft depthASTM DefaultLcrack15Foundation Crack Thickness (cm)Oakland ULR η 0.001Foundation Crack Fraction (dimensionless)Diffusivity ParametersDiffusivity ParametersASTM DefaultD ^{air} 9.30E-02Air Diffusion Coefficient (cm^2/s)ASTM DefaultD ^{air} 9.30E-02Air Diffusion Coefficient (cm^2/s)CalculatedD ^{eff} _{sol} 0.0011Effective Diffusion Coefficient through Soil (cm^2/s)CalculatedD ^{eff} _{sol} 0.0011Effective Diffusion Coefficient through Foundation Cracks (cm^2/s)CalculatedD ^{eff} _{sol} 0.0011Effective Diffusion Coefficient through Foundation Cracks (cm^2/s)Verefiction of Flux from Soil Vapor ConcentrationSoil Vapor (ppbv)Unit ConvC _{source} = Cv9.900Maximum Benzene Concentration in Soil Vapor (ug/L)Diffusive Vapor Flux Predicted from Benzene Concentration in Soil Vapor (ug/Cl)CalculatedF2.2E-09Indoor Air ConcentrationEnclosed Space Volume/Infiltration Area Ratio (cm)ASTM DefaultLb300Enclosed Space Air Exchange		θ_{as}	0.15	
Oakland ULR θ_{wc} 0.25 Water Content of Crack (v/v)Oakland ULR θ_{wc} 0.25 Water Content of Crack (v/v)Oakland ULR θ_{i} 0.40 Total Porosity-Soil and Crack (v/v)Site-specificLsoil91Depth to Location of Vapor Sample (cm) – 3.0 ft depthASTM DefaultLcrack15Foundation Crack Thickness (cm)Oakland ULR η 0.001 Foundation Crack Traction (dimensionless)Diffusivity ParametersASTM DefaultH 0.22 Henry's Constant (dimensionless)ASTM DefaultD ^{air} $9.30E-02$ Air Diffusion Coefficient (cm^2/s)ASTM DefaultD ^{air} $9.30E-02$ Air Diffusion Coefficient (cm^2/s)CalculatedD ^{eff} sol 0.0011 Effective Diffusion Coefficient through Soil (cm^2/s)CalculatedD ^{eff} sol 0.0011 Effective Diffusion Coefficient through Foundation Cracks (cm^2/s)CalculatedD ^{eff} sol 0.0011 Effective Diffusion Coefficient through Foundation Cracks (cm^2/s)CalculatedD ^{eff} sol 0.0011 Effective Diffusion Coefficient through Foundation Cracks (cm^2/s)Verdiction of Flux from Soil Vapor ConcentrationSoil Vapor (ppbv)Maximum Benzene Concentration in Soil Vapor (ppbv)Unit ConvC_sourceC, $3.2E-09$ Maximum Benzene Concentration in Soil Vapor (ug/L)CalculatedF $2.2e-09$ Unifusive Vapor Flux Predicted from Benzene Concentration in Soil Vapor (ug/cm ² -sec)Indoor Air ConcentrationEnclosed Space Air Exchange Rate (sec ⁻¹)C		θ_{ws}	0.25	Water Content of Soil (v/v)
Oakland ULRθt0.40Total Porosity-Soil and Crack (w/v)Site-specificLsoil91Depth to Location of Vapor Sample (cm) – 3.0 ft depthASTM DefaultLcrack15Foundation Crack Thickness (cm)Oakland ULRη0.001Foundation Crack Thickness (cm)Oakland ULRη0.001Foundation Crack Traction (dimensionless)Diffusivity ParametersFoundation Crack Fraction (dimensionless)ASTM DefaultH0.22ASTM DefaultD ^{air} 9.30E-02ASTM DefaultD ^{watt} 1.10E-05Vater Diffusion Coefficient (cm^2/s)CalculatedD ^{eff} ottoD ^{eff} otto0.0011Effective Diffusion Coefficient through Soil (cm^2/s)CalculatedD ^{eff} ottoD ^{eff} otto0.0011Effective Diffusion Coefficient through Soil (cm^2/s)CalculatedD ^{eff} ottoD ^{eff} otto0.0011Effective Diffusion Coefficient through Soil (cm^2/s)Prediction of Flux from Soil Vapor ConcentrationSite SpecificC source = CvQuarter of the source = Cv9,900Maximum Benzene Concentration in Soil Vapor (µg/L)Unit ConvC source = CvSource = Cv9,900Maximum Benzene Concentration in Soil Vapor (µg/L)CalculatedF2.2E-09Diffusive Vapor Flux Predicted from Benzene Concentration in SoilVapor (µg/cm ² -sec)Indoor Air ConcentrationASTM DefaultLb300ASTM DefaultER _{ab} indoor <t< td=""><td></td><td>θ_{ac}</td><td>0.15</td><td>Air Content of Crack (v/v)</td></t<>		θ_{ac}	0.15	Air Content of Crack (v/v)
Site-specificLsoil91Depth to Location of Vapor Sample (cm) - 3.0 ft depthASTM DefaultLcrack15Foundation Crack Thickness (cm)Oakland ULR η 0.001Foundation Crack Traction (dimensionless)Diffusivity ParametersASTM DefaultH0.22Henry's Constant (dimensionless)ASTM DefaultD ^{air} 9.30E-02Air Diffusion Coefficient (cm^2/s)ASTM DefaultD ^{air} 9.30E-02Air Diffusion Coefficient (cm^2/s)ASTM DefaultD ^{evat} 1.10E-05Water Diffusion Coefficient (cm^2/s)CalculatedD ^{eff} _{solt} 0.0011Effective Diffusion Coefficient through Soil (cm^2/s)CalculatedD ^{eff} _{solt} 0.0011Effective Diffusion Coefficient through Foundation Cracks (cm^2/s)Prediction of Flux from Soil Vapor ConcentrationSoil Vapor (ppbv)Unit ConvC _{source} = Cv9,900Vunit ConvC _{source} = Cv32Maximum Benzene Concentration in Soil Vapor (µg/L)Diffusive Vapor Flux Predicted from Benzene Concentration in Soil Vapor (µg/cm ² -sec)Indoor Air ConcentrationEnclosed Space Volume/Infiltration Area Ratio (cm) Vapor (µg/cm ² -sec)ASTM DefaultER _{su} Indoor0.00023ASTM DefaultER2.2E-08CalculatedC _{indoor} 3.2E-08Enclosed Space Air Exchange Rate (sec ⁻¹)CalculatedC _{indoor} ASTM DefaultEF250Exposure Frequency-Adult (days/year)ASTM DefaultEF250Exposure Frequency-Adult (days		θ_{wc}	0.25	Water Content of Crack (v/v)
ASTM DefaultLcrack15Foundation Crack Thickness (cm)0.01 to the phileOakland ULR η 0.001Foundation Crack Thickness (cm)Diffusivity ParametersASTM DefaultH0.22Henry's Constant (dimensionless)ASTM DefaultD ^{air} 9.30E-02Air Diffusion Coefficient (cm^2/s)ASTM DefaultD ^{air} 9.30E-02Air Diffusion Coefficient (cm^2/s)ASTM DefaultD ^{eff} 0.0011Effective Diffusion Coefficient through Soil (cm^2/s)CalculatedD ^{eff} 0.0011Effective Diffusion Coefficient through Foundation Cracks (cm^2/s)CalculatedD ^{eff} 0.0011Effective Diffusion Coefficient through Foundation Cracks (cm^2/s)Vapor CharterC.9.900Maximum Benzene ConcentrationSite SpecificC.Source = C.v32Vunit ConvC.Source = C.v32CalculatedF2.2E-09Diffusive Vapor Flux Predicted from Benzene Concentration in Soil Vapor (µg/L)Diffusive Vapor (µg/cm ² -sec)Indoor Air ConcentrationASTM DefaultLb300Enclosed Space Volume/Infiltration Area Ratio (cm)ASTM DefaultER _{air} indoor0.0023Enclosed Space Air Exchange Rate (sec ⁻¹)CalculatedC _{indoor} 3.2E-08Enclosed Space Air Concentration (µg/cm ³)DoseDoseAstm DefaultIR _{ai} indoor20ASTM DefaultEF250Exposure Frequency-Adult (days/year)ASTM DefaultEF250Exposure Frequency-Adult (days/year) <td></td> <td>θ_t</td> <td>0.40</td> <td>Total Porosity-Soil and Crack (v/v)</td>		θ_t	0.40	Total Porosity-Soil and Crack (v/v)
Oakland ULR η 0.001Foundation Grack Minkness (uni)Oakland ULR η 0.001Foundation Grack Fraction (dimensionless)Diffusivity ParametersASTM Default D^{air} 9.30E-02Air Diffusion Coefficient (cm^2/s)ASTM Default D^{air} 9.30E-02Air Diffusion Coefficient (cm^2/s)ASTM Default D^{wat} 1.10E-05Water Diffusion Coefficient (cm^2/s)Calculated D^{eff}_{soit} 0.0011Effective Diffusion Coefficient through Soil (cm^2/s)Calculated D^{eff}_{crack} 0.0011Effective Diffusion Coefficient through Foundation Cracks (cm^2/s)Prediction of Flux from Soil Vapor ConcentrationSolid Vapor (ppbv)Unit Conv $C_{source} = C_v$ 9.900Maximum Benzene Concentration in Soil Vapor (µg/L)Diffusive Vapor Flux Predicted from Benzene Concentration in Soil Vapor (µg/L)CalculatedF2.2E-09Diffusive Vapor Flux Predicted from Benzene Concentration in SoilASTM DefaultLb300Enclosed Space Volume/Infiltration Area Ratio (cm)ASTM DefaultLb300Enclosed Space Air Exchange Rate (sec ⁻¹)CalculatedC _{indoor} 3.2E-08Enclosed Space Air Concentration (µg/cm ³)DoseDoseASTM DefaultEF250ASTM DefaultEF250Exposure Frequency-Adult (days/year)ASTM DefaultEF250Exposure Duration (years)		Lsoil	91	Depth to Location of Vapor Sample (cm) – 3.0 ft depth
Diffusivity ParametersASTM DefaultH0.22Henry's Constant (dimensionless)ASTM DefaultDair9.30E-02Air Diffusion Coefficient (cm^2/s)ASTM DefaultD ^{eff} 9.30E-05Water Diffusion Coefficient (cm^2/s)CalculatedD ^{eff} 0.0011Effective Diffusion Coefficient through Soil (cm^2/s)CalculatedD ^{eff} 0.0011Effective Diffusion Coefficient through Foundation Cracks (cm^2/s)CalculatedD ^{eff} 0.0011Effective Diffusion Coefficient through Foundation Cracks (cm^2/s)Prediction of Flux from Soil Vapor ConcentrationSource = Cv9,900Site SpecificCsource = Cv9,900Maximum Benzene Concentration in Soil Vapor (ppbv)Unit ConvCsource = Cv32Maximum Benzene Concentration in Soil Vapor (µg/L)CalculatedF2.2E-09Diffusive Vapor Flux Predicted from Benzene Concentration in SoilASTM DefaultLb300Enclosed Space Volume/Infiltration Area Ratio (cm)ASTM DefaultER _{at} indoor0.00023Enclosed Space Air Exchange Rate (sec ⁻¹)CalculatedC _{indoor} 3.2E-08Enclosed Space Air Concentration (µg/cm ³)DoseASTM DefaultEF250Exposure Frequency-Adult (days/year)ASTM DefaultEF250Exposure Frequency-Adult (days/year)ASTM DefaultED25Exposure Duration (years)		Lcrack	15	Foundation Crack Thickness (cm)
ASTM DefaultH0.22Henry's Constant (dimensionless)ASTM DefaultDair9.30E-02Air Diffusion Coefficient (cm^2/s)ASTM DefaultD ^{wat} 1.10E-05Water Diffusion Coefficient (cm^2/s)CalculatedD ^{eff} soil0.0011Effective Diffusion Coefficient through Soil (cm^2/s)CalculatedD ^{eff} crack0.0011Effective Diffusion Coefficient through Foundation Cracks (cm^2/s)Prediction of Flux from Soil Vapor ConcentrationSite SpecificC_source = Cv9,900Maximum Benzene Concentration in Soil Vapor (ppbv)Unit ConvC_source = Cv32Maximum Benzene Concentration in Soil Vapor (µg/L)CalculatedF2.2E-09Diffusive Vapor Flux Predicted from Benzene Concentration in SoilASTM DefaultLb300Enclosed Space Volume/Infiltration Area Ratio (cm)ASTM DefaultER _{air} indoor0.00023Enclosed Space Air Exchange Rate (sec ⁻¹)CalculatedC _{indoor} 3.2E-08Enclosed Space Air Concentration (µg/cm ³)DoseASTM DefaultEF250Exposure Frequency-Adult (days/year)ASTM DefaultEF250Exposure Frequency-Adult (days/year)ASTM DefaultEF250Exposure Frequency-Adult (days/year)ASTM DefaultED25Exposure Duration (years)	Oakland ULR	η	0.001	Foundation Crack Fraction (dimensionless)
ASTM DefaultDate9:30E-02Air Diffusion Coefficient (cm^2/s)ASTM DefaultD ^{reft} 1.10E-05Water Diffusion Coefficient (cm^2/s)CalculatedD ^{eff} 0.0011Effective Diffusion Coefficient through Soil (cm^2/s)CalculatedD ^{eff} 0.0011Effective Diffusion Coefficient through Foundation Cracks (cm^2/s)CalculatedD ^{eff} 0.0011Effective Diffusion Coefficient through Foundation Cracks (cm^2/s)Prediction of Flux from Soil Vapor ConcentrationSite Specific $C_{source} = C_v$ 9,900Unit Conv $C_{source} = C_v$ 32Maximum Benzene Concentration in Soil Vapor (µg/L)CalculatedF2.2E-09Indoor Air ConcentrationASTM DefaultLb300Enclosed Space Volume/Infiltration Area Ratio (cm)ASTM DefaultERairIndoorASTM DefaultCindoorASTM DefaultERairIndoorASTM DefaultERairIndoorCalculatedCindoorCalculatedCindoorCalculatedCindoorASTM DefaultEF250Exposure Frequency-Adult (days/year)ASTM DefaultEF250Exposure Frequency-Adult (days/year)ASTM DefaultEF250Exposure Duration (years)		Diffusivity Pa	rameters	
ASTM Default D^{wat} 1.10E-05Water Diffusion Coefficient (cm^2/s)Calculated D^{eff}_{soll} 0.0011Effective Diffusion Coefficient through Soil (cm^2/s)Calculated D^{eff}_{orack} 0.0011Effective Diffusion Coefficient through Foundation Cracks (cm^2/s)Prediction of Flux from Soil Vapor ConcentrationSite Specific $C_{source} = C_v$ 9,900Unit Conv $C_{source} = C_v$ 32Maximum Benzene Concentration in Soil Vapor (µg/L)CalculatedF2.2E-09Indoor Air ConcentrationASTM DefaultLb300ASTM DefaultER _{air} indoor0.00023Calculated C_{indoor} 3.2E-08Enclosed Space Air Exchange Rate (sec ⁻¹)CalculatedCindoorASTM DefaultIR _{air} indoor20Daily Indoor Inhalation Rate (m³/day)ASTM DefaultEF250Exposure Frequency-Adult (days/year)ASTM DefaultEF250Exposure Frequency-Adult (days/year)ASTM DefaultEF250Exposure Duration (years)			0.22	Henry's Constant (dimensionless)
Calculated D^{eff}_{soil} 0.0011Effective Diffusion Coefficient through Soil (cm^2/s)Calculated D^{eff}_{crack} 0.0011Effective Diffusion Coefficient through Foundation Cracks (cm^2/s)Prediction of Flux from Soil Vapor ConcentrationSite Specific $C_{source} = C_v$ 9,900Maximum Benzene Concentration in Soil Vapor (µg/L)Unit Conv $C_{source} = C_v$ 32Maximum Benzene Concentration in Soil Vapor (µg/L)CalculatedF2.2E-09Diffusive Vapor Flux Predicted from Benzene Concentration in SoilASTM DefaultLb300Enclosed Space Volume/Infiltration Area Ratio (cm)ASTM DefaultER _{air} indoor0.00023Enclosed Space Air Exchange Rate (sec ⁻¹)CalculatedC _{indoor} 3.2E-08Enclosed Space Air Concentration (µg/cm ³)DoseASTM DefaultIR _{air} indoor20Daily Indoor Inhalation Rate (m ³ /day)ASTM DefaultEF250Exposure Frequency-Adult (days/year)ASTM DefaultED25Exposure Duration (years)			9.30E-02	Air Diffusion Coefficient (cm^2/s)
CalculatedDeficrack0.0011Effective Diffusion Coefficient through Foundation Cracks (cm^2/s)Prediction of Flux from Soil Vapor ConcentrationSite Specific $C_{source} = C_v$ 9,900Maximum Benzene Concentration in Soil Vapor (ppbv)Unit Conv $C_{source} = C_v$ 32Maximum Benzene Concentration in Soil Vapor (µg/L)CalculatedF2.2E-09Diffusive Vapor Flux Predicted from Benzene Concentration in SoilASTM DefaultLb300Enclosed Space Volume/Infiltration Area Ratio (cm)ASTM DefaultCindoor0.0023Enclosed Space Air Exchange Rate (sec ⁻¹)CalculatedCindoor3.2E-08Enclosed Space Air Concentration (µg/cm ³)DoseASTM DefaultIR _{air} indoor20ASTM DefaultEF250Exposure Frequency-Adult (days/year)ASTM DefaultEF250Exposure Duration (years)		D ^{wat}	1.10E-05	Water Diffusion Coefficient (cm ² /s)
Prediction of Flux from Soil Vapor ConcentrationSite Specific $C_{source} = C_v$ 9,900Maximum Benzene Concentration in Soil Vapor (ppbv)Unit Conv $C_{source} = C_v$ 32Maximum Benzene Concentration in Soil Vapor (µg/L)CalculatedF2.2E-09Diffusive Vapor Flux Predicted from Benzene Concentration in SoilASTM DefaultLb300Enclosed Space Volume/Infiltration Area Ratio (cm)ASTM DefaultER _{air} indoor0.00023Enclosed Space Air Exchange Rate (sec ⁻¹)CalculatedC _{indoor} 3.2E-08Enclosed Space Air Concentration (µg/cm ³)DoseDoseDaily Indoor Inhalation Rate (m³/day)ASTM DefaultEF250Exposure Frequency-Adult (days/year)ASTM DefaultED25Exposure Duration (years)		D ^{eff} soit	0.0011	Effective Diffusion Coefficient through Soil (cm^2/s)
Site Specific Unit Conv $C_{source} = C_v$ $9,900$ Maximum Benzene Concentration in Soil Vapor (ppbv)Unit Conv $C_{source} = C_v$ 32Maximum Benzene Concentration in Soil Vapor (µg/L)CalculatedF $2.2E-09$ Diffusive Vapor Flux Predicted from Benzene Concentration in Soil Vapor (µg/cm²-sec)Indoor Air ConcentrationEnclosed Space Volume/Infiltration Area Ratio (cm)ASTM DefaultLb300ASTM DefaultER _{air} indoor0.00023Enclosed Space Air Exchange Rate (sec-1)CalculatedC _{indoor} 3.2E-08Enclosed Space Air Concentration (µg/cm³)DoseDoseASTM DefaultIR _{air} indoorASTM DefaultEF250Exposure Frequency-Adult (days/year)ASTM DefaultED25Exposure Duration (years)	Calculated			
Unit Conv $C_{source} = C_v$ 32Maximum Benzene Concentration in Soil Vapor (µg/L)CalculatedF2.2E-09Diffusive Vapor Flux Predicted from Benzene Concentration in SoilASTM DefaultLb300Enclosed Space Volume/Infiltration Area Ratio (cm)ASTM DefaultER _{atr} indoor0.00023Enclosed Space Air Exchange Rate (sec ⁻¹)CalculatedC _{indoor} 3.2E-08Enclosed Space Air Concentration (µg/cm ³)DoseDoseDaily Indoor Inhalation Rate (m³/day)ASTM DefaultEF250Exposure Frequency-Adult (days/year)ASTM DefaultED25Exposure Duration (years)		Prediction of	Flux from Soil	Vapor Concentration
Calculated F 2.2E-09 Diffusive Vapor Flux Predicted from Benzene Concentration in Soil Vapor (µg/cm ² -sec) ASTM Default Lb 300 Enclosed Space Volume/Infiltration Area Ratio (cm) ASTM Default ER _{atr} indoor 0.00023 Enclosed Space Air Exchange Rate (sec ⁻¹) Calculated C _{indoor} 3.2E-08 Enclosed Space Air Concentration (µg/cm ³) Dose Dose Daily Indoor Inhalation Rate (m ³ /day) ASTM Default EF 250 Exposure Frequency-Adult (days/year) ASTM Default ED 25 Exposure Duration (years)	Site Specific	$C_{source} = C_v$	9,900	Maximum Benzene Concentration in Soil Vapor (ppbv)
Calculated F 2.22-09 Vapor (μg/cm²-sec) Indoor Air Concentration Vapor (μg/cm²-sec) ASTM Default Lb 300 Enclosed Space Volume/Infiltration Area Ratio (cm) ASTM Default ER _{air} indoor 0.00023 Enclosed Space Air Exchange Rate (sec ⁻¹) Calculated C _{indoor} 3.2E-08 Enclosed Space Air Concentration (μg/cm³) Dose Dose Vapor (μg/cm²-sec) ASTM Default IR _{air} indoor 20 Daily Indoor Inhalation Rate (m³/day) ASTM Default EF ASTM Default EF 250 Exposure Frequency-Adult (days/year) ASTM Default ED 25 Exposure Duration (years)	Unit Conv	$C_{source} \simeq C_v$	32	Maximum Benzene Concentration in Soil Vapor (µg/L)
Indoor Air Concentration ASTM Default Lb 300 Enclosed Space Volume/Infiltration Area Ratio (cm) ASTM Default ER _{air} indoor 0.00023 Enclosed Space Air Exchange Rate (sec ⁻¹) Calculated C _{indoor} 3.2E-08 Enclosed Space Air Concentration (µg/cm³) Dose ASTM Default IR _{air} indoor 20 Daily Indoor Inhalation Rate (m³/day) ASTM Default EF ASTM Default EF 250 Exposure Frequency-Adult (days/year) ASTM Default ED 25 Exposure Duration (years)	Calculated	F	2.2E-09	
ASTM Default ERairindoor 0.00023 Enclosed Opace Volume/minitude/rited relate (ser. ¹) Calculated C _{indoor} 3.2E-08 Enclosed Space Air Exchange Rate (ser. ¹) Dose Dose ASTM Default IR _{air} indoor 20 ASTM Default IR _{air} indoor 20 Daily Indoor Inhalation Rate (m³/day) ASTM Default EF 250 Exposure Frequency-Adult (days/year) ASTM Default ED 25 Exposure Duration (years)		Indoor Air Co	ncentration	
ASTM Default ER _{air} indoor 0.00023 Enclosed Space Air Exchange Rate (sec ⁻¹) Calculated C _{indoor} 3.2E-08 Enclosed Space Air Concentration (µg/cm³) Dose Dose Daily Indoor Inhalation Rate (m³/day) ASTM Default EF 250 Exposure Frequency-Adult (days/year) ASTM Default ED 25 Exposure Duration (years)	ASTM Default	Lb	300	Enclosed Space Volume/Infiltration Area Ratio (cm)
Calculated C _{indoor} 3.2E-08 Enclosed Space Air Concentration (μg/cm ³) Dose Dose ASTM Default IR _{air} indoor 20 Daily Indoor Inhalation Rate (m ³ /day) ASTM Default EF 250 Exposure Frequency-Adult (days/year) ASTM Default ED 25 Exposure Duration (years)	ASTM Default	ERairindoor	0.00023	
DoseASTM DefaultIR _{air} indoor20Daily Indoor Inhalation Rate (m³/day)ASTM DefaultEF250Exposure Frequency-Adult (days/year)ASTM DefaultED25Exposure Duration (years)	Calculated	Cindoor	3.2E-08	
ASTM Default EF 250 Exposure Frequency-Adult (days/year) ASTM Default ED 25 Exposure Duration (years)				
ASTM Default ED 25 Exposure Duration (years)	ASTM Default	IR _{air} indoor	20	Daily Indoor Inhalation Rate (m ³ /day)
	ASTM Default	EF	250	Exposure Frequency-Adult (days/year)
	ASTM Default	ED	25	Exposure Duration (years)
Carculated Dose 260 Dose (mg)	Calculated	Dose	260	Dose (mg)
Risk		Risk		
DTSC SF ₁ 0.1 Inhalation California Cancer Slope Factor for Benzene (kg-day/mg)	DTSC	SF	0.1	
ASTM Default BW 70 Body Weight (kg) '	ASTM Default	BW	70	Body Weight (kg) '
ASTM Default AT70 Averaging Time for Carcinogens (years)	ASTM Default	AT	70	Averaging Time for Carcinogens (years)
Calculated Risk 2.3E-07 Risk (positive/population)		Risk	2.3E-07	
Calculated SSTL 43,800 Tier II Site-Specific Target Level (ppbv) for TRL = 1E-06	Calculated	SSTL	43,800	Tier II Site-Specific Target Level (ppbv) for TRL = 1E-06

Seturant wight

ς.

Notes:

ASTM = American Standard for Testing and Materials, 1995. Standard Guide for Risk Based Corrective Action Applied at Petroleum Release Sites, E 1739-95.

ULR = Tier I Risk-Based Screening Levels, Oakland Urban Land Redevelopment Program (Spence and Gomez, 1997 and 1999).

Calculations: Effective diffusivity, diffusive vapor flux, enclosed space air concentrations, dose, and risk calculations from ASTM 95 guidance formulas presented above.

Formulas
$D_{soil}^{\text{eff}} = D^{air} \frac{\theta_{as}^{5.55}}{\theta_T^2} + D^{wat} \frac{1}{H} \frac{\theta_{ws}^{5.55}}{\theta_T^2}$
$D_{crack}^{eff} = D_{crack}^{air} \frac{\theta_{ac}^{3.33}}{\theta_{T}^{2}} + D_{H}^{wat} \frac{1}{H} \frac{\theta_{wc}^{5.33}}{\theta_{T}^{2}}$
$D_{v}^{eff} = \frac{L_{soil} + L_{crack}}{\frac{L_{crack}}{D_{crack}^{eff} \eta} + \frac{L_{soil}}{D_{soil}^{eff}}}$
$F = D_v^{\text{eff}} \frac{\Delta C_v}{\Delta \chi}$
$= \frac{C_{\text{source}} \frac{D_{\text{soil}}^{\text{eff}}}{L_{\text{soil}}}}{L_{\text{soil}}}$
$=\frac{\frac{C_{\text{source }}\frac{D_{\text{soil}}^{\text{eff}}}{L_{\text{soil}}}}{1+\frac{D_{\text{soil}}^{\text{eff}}}{L_{\text{soil}}}\frac{L_{\text{crack}}}{D_{\text{crack}}^{\text{eff}}\eta}}$
$C_{indoor} = \frac{F}{ER_{air-indoor} \times L_b}$
$Dose = C_{indoor} \star IR_{air-indoor} \star EF \star ED$
$Risk = \frac{Dose \times SF}{BW \times AT}$

		TIER II OUTPUT D	ATA-OFFSI	TE RESIDE	NTIAL RECEP	PTOF	R					Table	• VI.2	
Site Name: Ne Site Location:	estle USA Inc., Facility		Completed B	y: JCI										
One Location.			r											<u>1 OF 1</u>
GROUNDWATER SSTL VALUES		Target Risk (Class A & B) 1.0E-6 D MCL exposure limit?					Calculation Option: 2							
		Target Risk (Class C) 1.0E-5		PEL exposure limit?										
·			Target Hazard Quotient 1.0E+0											
				SSTL	Results For Com	plete	e Exposure	Pathways ("x" if	Com	plete)				
CONSTITUEN	ONSTITUENTS OF CONCERN		Groundwater Ingestion			Groundwater Volatilization			Groundwater Volatilization to Outdoor Air			Applicable SSTL	SSTL Exceeded ?	Required CR
CAS No.	Name	(mg/L)	Residential: (on-site)	Commercial: (on-site)	Regulatory(MCL): (on-site)		esidential: (off-site)	Commercial: (on-site)		esidential (on-site)	Commercial: (on-site)	(mg/L	" If yes	Only if "yes" is
71-43-2	2 Benzene	1.8E-2	NA	NA	NA	1.1E+0		NA	NA		NA NA	1.1E+0	<u> </u>	<1
	2 Dichloroethane, 1,2-	1.7E-1												

10002582 1108

22 200**2**

>Sol indicates risk-based target concentration greater than constituent solubility

© Groundwater Services, Inc. (GSI), 1995-1997. All Rights Reserved.

Software: GSI RBCA Spreadsheet Serial: G-273-IBX-894 Version: 1.0.1

