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Atlantic Richfield Company (a BP affiliated company)

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21 July 2008

 Re: Site Conceptual Model with Feasibility Study Report Former BP Station # 11132 3201 35<sup>th</sup> Avenue Oakland, California ACEH Case #RO0000014

"I declare, that to the best of my knowledge at the present time, that the information and/or recommendations contained in the attached document are true and correct."

Submitted by:

Tail Suppl

Paul Supple Environmental Business Manger



#### **Prepared for:**

Mr. Paul Supple Environmental Business Manager Atlantic Richfield Company P.O. Box 1257 San Ramon, California 94583

# Prepared by:

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21 July 2008

Project No. 06-08-655

#### SITE CONCEPTUAL MODEL WITH FEASIBILITY STUDY REPORT Former BP Station #11132

3201 35<sup>th</sup> Avenue Oakland, California

BROADBENT & ASSOCIATES, INC. ENGINEERING, WATER RESOURCES & ENVIRONMENTAL

21 July 2008

Project No. 06-08-655

Atlantic Richfield Company P.O. Box 1257 San Ramon, CA 94583 Submitted via ENFOS

Attn.: Mr. Paul Supple

Re: Site Conceptual Model with Feasibility Study Report, Former BP Station #11132 3201 35<sup>th</sup> Avenue, Oakland, California; ACEH Case #RO0000014

Dear Mr. Supple:

Broadbent & Associates, Inc. (BAI) is pleased to submit this *Site Conceptual Model with Feasibility Study Report* for Former BP Station #11132 (herein referred to as Station #11132) located at 3201 35<sup>th</sup> Avenue, Oakland, California (Site). This report was prepared in response to a directive letter from Mr. Paresh Khatri of Alameda County Environmental Health (ACEH) dated 22 May 2008.

Should you have questions or require additional information, please do not hesitate to contact us at (530) 566-1400.

Sincerely, BROADBENT & ASSOCIATES, INC.

Thomas A. Venus, P.E. Senior Engineer

the but 71

Robert H. Miller, P.G., C.HG. Principal Hydrogeologist

Attachment



cc: Mr. Paresh Khatri, Alameda County Environmental Health (Submitted via ACEH ftp site) Ms. Shelby Lathrop, ConocoPhillips, 76 Broadway, Sacramento, California 95818 Electronic copy uploaded to GeoTracker

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#### 1.0 INTRODUCTION

On behalf of the Atlantic Richfield Company, RM - a BP affiliated company, Broadbent & Associates, Inc. (BAI) has prepared this Site Conceptual Model with Feasibility Study Report for the Former BP Service Station No. 11132, located at 3201 35<sup>th</sup> Avenue, Oakland, Alameda County, California (Site). This report was prepared in response to the request within the 22 May 2008 directive letter from Mr. Paresh Khatri of the Alameda County Environmental Health (ACEH). This report includes discussions on the site background and previous environmental activities, regional and Site geology and hydrogeology, definition of contamination within soil and ground water, discussion of preferential pathways, status of Site remediation, sensitive receptors, preliminary risk assessment, feasibility study of remediation alternatives, discussion of data gaps, conclusions and recommendations. Tables, figures, and appendices referenced within this report are provided following the conclusion of the document's text.

#### 2.0 BACKGROUND INFORMATION

#### 2.1 Site Background

The Site is currently a 76-branded gasoline service station located on the northeast corner of 35<sup>th</sup> Avenue and Sutter Street, southwest of Interstate 580, in a mixed commercial and residential area of Oakland. The Site has operated as a gasoline service station since at least the early 1970's. It was acquired in 1989 from Mobil by BP and operated under the BP brand. BP sold the station in 1994 to Tosco, which was acquired by ConocoPhillips who now operates the 76-branded station. The original underground storage tank (UST) release was reported on 15 April 1986, following a failed UST integrity test on 5 March 1986 (Mobil, 1986; PetroTite, 1986). The ACEH-assigned Fuel Leak Case number is RO0000014 / GeoTracker Global ID No. T0600100213.

A Quik Stop convenience store/gasoline station is located at 3130  $35^{th}$  Avenue across the street approximately 150 feet to the southwest of the Site. Two former gasoline service stations are located slightly further west of the Site along  $35^{th}$  Avenue: A former Texaco-branded gasoline station on the northeast corner of  $35^{th}$  Avenue and School Street, now operated as Tito's Car Washing & Detail Shop at 3101  $35^{th}$  Avenue; and a former Exxon-branded gasoline station on the northwest corner of  $35^{th}$  Avenue and School Street but presently a vacant lot. The former Exxon station is an active leaking UST case, ACEH Fuel Leak Case No.RO0000271 / GeoTracker Global ID No. T0600100538.

#### 2.2 Previous Environmental Activities

Mobil reported that three former USTs at the Site failed a tank integrity test on 5 March 1986 (Mobile, 1986; PetroTite, 1986). Former USTs at the Site included one 12,000-gallon, one 8,000-gallon, and one 5,000-gallon steel UST. These USTs had been installed in 1972. Lee filed a closure plan with Alameda County on 20 March 1986 (Lee, 1986). Kaprealian Engineering,

Inc. (KEI) subsequently conducted a UST inspection and soil sampling during the removal of the three USTs in April 1986 (KEI, 1986). KEI reported ground water on the bottom of the excavation during UST removal and soil sampling, but did not report on the condition of the USTs or the excavated soil. Four soil samples were obtained beneath two USTs at two feet below the tanks within the native soil, and three samples were collected from beneath one UST. The samples were analyzed for Total Petroleum Hydrocarbons in the Gasoline Range (TPH-G). Concentrations of TPH-G (up to 210 mg/kg) were detected in five of the seven samples. The Bay Area Air Quality Management District (BAAQMD) issued a permit to aerate 150 cubic yards of soil onsite before disposal at a Class III landfill (BAAQMD, 1986). However, no evidence of excavation or soil analysis was found. Sample collection location maps and analytical results are provided within Appendix A.

KEI installed three monitoring wells (MW-1 through MW-3) on 30 July 1986 (KEI, 1986). MW-1 was drilled to 45 feet below ground surface (ft bgs), and MW-2 and MW-3 were drilled to 35 ft bgs. The boring logs indicated that silty clay with rock fragments and gravel were encountered during drilling. Copies of boring logs are provided within Appendix B. Ground water was encountered during drilling between 24 and 33 ft bgs. A faint gasoline odor was reported in the soil cuttings encountered between five and seven ft bgs. One soil sample from each boring, collected between 16 and 26 ft bgs, was analyzed for TPH-G. Concentrations of TPH-G (up to 12.0 mg/kg) were detected in the soil samples. Ground-water samples were also collected from each monitoring well and analyzed for TPH-G and Benzene, Toluene, Ethylbenzene, and Total Xylenes (BTEX). Concentrations of TPH-G (up to 26,000  $\mu$ g/L) and BTEX (up to 3,800  $\mu$ g/L Benzene, 1,000  $\mu$ g/L Toluene, and 1,700  $\mu$ g/L Total Xylenes) were detected in ground-water samples collected from wells MW-1 and MW-2.

It appears that KEI performed monthly monitoring and quarterly sampling of the three monitoring wells from October 1986 to February 1989. Available reports indicated that ground water from well MW-1 had odors that increased from "moderate" to "strong," while MW-2 had odors that increased from "slight" to "moderate." Sheen was reported in well MW-1 on 23 December 1986. On 21 December 1988, KEI reported three inches of Separate-Phase Hydrocarbons (SPH or Free Product, FP) in well MW-1. FP was also reported in well MW-2 and sheen reported in well MW-3 on 15 February 1989. In a 28 September 1987 report, KEI stated that "the presence of a small amount of floating product in MW-1, undocumented until the present quarter, implies the possibility that a pocket of free product is being leached from the soil into the groundwater" (KEI, 1987). A figure attached to the KEI 16 March 1989 monitoring and sampling report indicated the direction of ground-water flow was to the south. Quarterly ground-water samples were collected and analyzed for TPH-G and BTEX. Concentrations of TPH-G (up to 210,000  $\mu$ g/L), Benzene (up to 28,000  $\mu$ g/L), Toluene (up to 30,000  $\mu$ g/L), Ethylbenzene (up to 8.5  $\mu$ g/L), and Total Xylenes (up to 12,000  $\mu$ g/L) were detected in the three early wells. At the time, the highest concentrations of both TPH-G and BTEX were detected in ground-water samples collected from well MW-1, near the southeast corner of the UST complex.

Alton Geoscience, Inc. (Alton) drilled ten soil borings to various depths ranging from 25 to 35 ft bgs in January and February 1990 (Alton, 1990). The borings were advanced three to four feet beyond the depth at which first ground water was encountered. The report contained no information about Site geology or hydrogeology, other than a ground-water elevation contours figure showing that the direction of ground-water flow beneath the Site was toward the

southwest at the time of the investigation. The borings were converted into temporary wells (TW-1 through TW-10) and ground-water samples collected. Samples from MW-1 and TW-2 were not analyzed due to the presence of FP. Concentrations of TPH-G (up to 240,000  $\mu$ g/L) were detected in samples collected from wells MW-2 and MW-3, and from temporary wells TW-1, TW-3, TW-5, TW-6, TW-9, and TW-10. Concentrations of BTEX (up to 2,400  $\mu$ g/L Benzene, 7,300  $\mu$ g/L Toluene, 5,600  $\mu$ g/L Ethylbenzene, and 28,000  $\mu$ g/L Total Xylenes) were detected in the analyzed samples. The highest concentrations of TPH-G and BTEX were detected in temporary wells TW-5 (located off-site to the southwest within 35<sup>th</sup> Avenue), and TW-10 (located near the northwest corner of the UST complex) (Alton, 1990).

Alton drilled two onsite soil borings based on the results of these activities. The borings were converted into one ground-water monitoring well (MW-4) and one recovery well (RW-1). Alton drilled three off-site soil borings that were converted into monitoring wells MW-5 through MW-7 (Alton, 1990). The borings were drilled to approximately 35 ft bgs. During drilling, soil samples were collected from borings at five-foot intervals until the first ground water was encountered, at about 26 ft bgs in MW-5 and 28 ft bgs in MW-6 and MW-7. Silty clay was the predominant soil type encountered in each boring. At the time of the investigation, ground-water elevation data indicated a southerly ground-water flow direction, with an average gradient of approximately 0.01 ft/ft. Alton reported no known or reported ground-water production wells in use as domestic or municipal water supply sources within the immediate vicinity or within a <sup>1</sup>/<sub>2</sub>-mile radius of the Site (Alton, 1990).

Eighteen samples collected from the five well borings were analyzed for TPH-G and BTEX. Concentrations of TPH-G (up to 770 mg/kg), and BTEX (up to 4.8 mg/kg Benzene), 44 mg/kg Toluene, 13 mg/kg Ethylbenzene, and 94 mg/kg Total Xylenes) were detected in soil samples from RW-1, near the southwest corner of the UST complex, and MW-5, off-site towards the southwest.

Ground-water samples were collected from wells MW-3 through MW-7. Wells MW-1 and MW-2 were not sampled because FP was present in each well at measured thicknesses of 1.25 ft and 0.10 ft, respectively. Concentrations of TPH-G (up to 280  $\mu$ g/L) and BTEX (up to 200  $\mu$ g/L Benzene, 210  $\mu$ g/L Toluene, 46  $\mu$ g/L Ethylbenzene, and 290  $\mu$ g/L Total Xylenes) were detected in the ground-water samples collected from wells MW-3 and MW-5. The sample from off-site well MW-5, the most down-gradient off-site monitoring well, had the highest concentrations of TPH-G and BTEX in both soil and ground-water samples. Alton noted that well MW-5 is located approximately ten feet from the Quik Stop's USTs (Alton 1990).

In August 1990, KEI conducted soil sampling during routine dispenser modifications and upgrades (KEI, 1990). Three soil samples (D1 through D3) were collected from beneath product dispensers at depths ranging from approximately three to seven ft bgs. Four soil samples (PT-1 through PT-4) were also collected from product pipe trenches at depths of approximately three ft bgs. The samples were analyzed for TPH-G, BTEX, and organic lead. Concentrations of TPH-G (21 mg/kg), Benzene (9.9  $\mu$ g/kg), Toluene (62  $\mu$ g/kg), Ethylbenzene (60  $\mu$ g/kg), and Total Xylenes (38 mg/kg) were detected in soil sample PT-3, from the pipeline trench that supplied the northern dispenser island. Approximately 150 cubic yards of soil was disposed of at an approved Class III disposal facility (KEI, 1990).

Alton drilled three off-site soil borings (SB-8 through SB-10) in February 1991. The borings were converted into ground-water monitoring wells MW-8 through MW-10 (Alton, 1991). The borings were drilled to approximately 35 or 40 ft bgs. Soil samples were collected from the borings at five-foot intervals and at significant lithologic changes, until the first ground water was encountered, at approximately 25 ft bgs in each well. Silty clay was the predominant soil type encountered throughout each boring. Depth to ground water, as measured from the top of casing on 15 April 1991, ranged from 12 to 18 ft. The depth to water was not measured in RW-1 because an "oily substance" was present on the water surface. According to Alton, these data indicated a southeasterly ground-water flow direction with an average hydraulic gradient of approximately 0.003 ft/ft at the time of the investigation. A pumping test was also conducted to estimate aquifer parameters. Based on the pumping test data, the average hydraulic conductivity beneath the Site was determined to be 0.016 ft/min (Alton, 1991).

Nine soil samples, collected from 10.5 to 26.0 ft bgs, were analyzed for TPH-G and BTEX. Concentrations of TPH-G (up to 390,000  $\mu$ g/L) and BTEX (up to 1,800  $\mu$ g/L Benzene, 16,000  $\mu$ g/L Toluene, 6,700  $\mu$ g/L Ethylbenzene, and 37,000  $\mu$ g/L Total Xylenes) were detected in samples taken from the borings. The highest concentrations were detected at 20.5 to 21.0 ft bgs in boring SB-8 (MW-8).

Alton conducted a sensitive receptors survey as part of their supplemental site investigation study. The report, dated 20 February 1991, stated that the nearest residence was 50 feet, the nearest hospital was 11,000 feet, and the nearest school was 1,000 feet from the Site. According to Alton, the aquifer was a Class III: Not a Potential Source of Drinking Water (Alton, 1991).

Hydro-Environmental Technologies, Inc. (HETI) prepared an Interim Remedial Action Plan on 20 March 1992. In this plan, HETI stated that FP was routinely removed by hand bailing from monitoring wells MW-1 and MW-2 and recovery well RW-1 during the quarterly sampling rounds. HETI estimated that 5 gallons of product were removed each quarter. HETI proposed an interim ground-water and product recovery system to facilitate removal of free- and dissolved-phase hydrocarbons from the ground water at the Site. HETI also stated that "while this system will not be designed to address the off-site portion of the hydrocarbon plume, it will provide data necessary to plan the most cost-effective long-term remedial solution" (HETI, 1992). Ground-water monitoring and sampling data since 1990 is summarized within Table 1 and Table 2.

The East Bay Municipal Utility District (EBMUD) issued a Wastewater Discharge Permit to BP on 10 November 1992. The remediation system was activated on 25 November 1992, and operated intermittently until September 1995. The ground-water extraction and treatment system removed 935,229 gallons at approximately one gallon per minute from recover well RW-1. The last discharge report submitted by BP to EBMUD was in October 1995.

EMCON conducted supplemental assessment activities at the Site on 11 November 1994. One exploratory soil boring (THP-1) was advanced using Cone-Penetrometer Testing (CPT) equipment, and soil samples were collected from the boring. The boring was advanced approximately 23 ft bgs near the northern side of the station building. Soil types logged from drilling included sandy gravel and silty sand underlain by clay to approximately 23 ft bgs. The CPT equipment met with refusal at the extent explored (23 ft bgs). The soil sample from boring

THP-1 was collected from 4.0-4.5 ft bgs and submitted for TPH-G, BTEX, Total Petroleum Hydrocarbons in the Diesel Range (TPH-D), Total Petroleum Hydrocarbons in the Oil Range (TPH-O) and Polychlorinated Biphenyls (PCBs). TPH-O, at a concentration of 120 mg/kg, was the only analyte reported (EMCON, 1994).

In April 2004, URS observed Gregg Drilling advance six on-site soil borings utilizing a truckmounted Geoprobe direct push technologies (DPT) rig. The borings were advanced to an approximate depth between 26 and 42 ft bgs (UB-7 through UB-12). A site map depicting the soil boring locations is provided in Appendix C. Soil samples were collected for analysis at approximate ten foot intervals. Concentrations of Gasoline-Range Organics (GRO) were detected above laboratory reporting limits in six samples collected from four of the five on-site borings at concentrations up to 820 mg/kg in sample UB-10-25, where 25 represents the sample depth in feet bgs. Benzene was detected above the laboratory reporting limit in two samples from two on-site borings at concentrations of 0.0093 mg/kg in UB-7-41 and 0.17 mg/kg in UB-9-35. Toluene was detected above the laboratory reporting limit in sample UB-9-35 at a concentration of 0.014 mg/kg. Ethylbenzene was detected in four samples from four on-site borings at concentrations up to 5.7 mg/kg in UB-10-25. Total xylenes were detected above the laboratory reporting limit in 13 samples from each of the five on-site borings at concentrations up to 37 mg/kg in UB-10-35. MTBE was detected in 13 samples from four of the on-site borings at concentrations up to 0.20 mg/kg in UB-7-41. TBA was detected above the laboratory reporting limit in five samples from three on-site borings at concentrations up to 0.85 mg/kg in UB-10-35.

In July 2004, URS observed Gregg Drilling advance six off-site soil borings utilizing a vanmounted Cone Penetrometer Testing (CPT) rig to an approximate depth of 50 feet bgs (UB-1 through UB-6) (Appendix C). Selected soil samples were submitted for laboratory analysis based on field observations and ground-water elevations. MTBE was detected above the laboratory reporting limits in one sample from the four off-site borings at concentrations of 0.0056 mg/kg in UB-4-30 and 0.018 mg/kg in UB-4-30.5. No other analytes were detected above the laboratory reporting limits from the off-site samples. Historical soil analytical data are provided within Appendix A. Lithologic boring logs and well construction details are provided within Appendix B.

Stratus Environmental, Inc. performed the field activities associated with a mobile Dual-Phase Extraction (DPE) event conducted during 26-28 November 2007 (BAI, 2008). Existing onsite wells MW-1, MW-2, and RW-1 were used as individual extraction wells for the mobile DPE events. Selection of these wells for extraction was based on construction, quarterly ground-water monitoring levels, laboratory analytical results, and locations on the Site. The remaining onsite and offsite wells, with the exception of distant wells MW-5 and MW-6, were used as observation points to monitor for observable influence. The extraction events on each of the three wells lasted 11 to 12 hours. During the mobile DPE events, the average soil vapor extraction rate was approximately 48.3 scfm and the average applied system vacuum was approximately 25.0-inches Mercury. Laboratory analytical results reported relatively high GRO in soil vapor extracted from well MW-2 (maximum of 1,500 ppmv GRO). Initial concentrations of hydrocarbons in the extracted ground water during the event were relatively high for the samples collected from wells MW-1 and RW-1 (maximum of 3,000  $\mu$ g/L GRO). The concentrations in soil vapor decreased over time during extraction from wells MW-1 and RW-1, while concentrations increased over

time during extraction from well MW-2. The concentration of hydrocarbons in ground water decreased over time during extraction from wells MW-1 and RW-1, while concentrations of GRO and MTBE increased over time during extraction from well MW-2. Approximately 2,090 gallons of ground water was extracted as a result of this mobile DPE event. Approximately 0.0091 lbs of GRO and 0.0003 lbs of Benzene in ground water and 14.0 lbs of GRO and 0.029 lbs of Benzene in soil vapor were removed from the subsurface during extraction activities. It is believed that contaminant recovery efficiency was limited due to the relatively tight soil permeability in the vadose zone and beneath the ground-water table.

### 3.0 HYDROCARBON SOURCE

### 3.1 Release Source and Volume

The exact release source and volume released is unknown. However, based on historical reports and the observed contaminant concentrations, the source area is believed to be the UST complex located in the southwestern portion of the Site. The predominant depth of first detected contamination in soils in the vicinity of the UST complex leads one to presume that the release occurred beneath the invert of the USTs. An unknown amount of petroleum hydrocarbon contamination is presently bound within the soil matrix in this area, and dissolved within groundwater under and downgradient of the Site. A fluctuating ground-water table has likely "smeared" contaminants in soils up to the high water mark downgradient of the Site, contributing to a secondary source of contamination after the suspect USTs were removed and replaced.

#### 3.2 Release Intervention

The removal and replacement of underground petroleum storage and dispensing infrastructure was conducted as a measure to stop the release.

# 4.0 SITE CHARACTERIZATION

### 4.1 Current Site Use

The Site is currently an operational 76-branded service station located on the northeast corner of 35<sup>th</sup> Avenue and Sutter Street, southwest of Interstate 580, in a mixed commercial and residential area of Oakland. Improvements to the property include the two service station buildings sharing a common roof, one inactive pump island on the north side of the station building(s) and two active pump islands south of the building(s) each with two double-sided dispensers under one large canopy. An aboveground propane storage tank surrounded by bollard posts is located in the southeastern corner of the lot. A fenced remediation compound (inactive) is located in the northwestern portion of the Site. Concrete covers ground surfaces around the pump islands and over the UST complex, located in the southwestern portion of the Site. Asphalt covers the majority of the rest of the Site, with the exception of thin planters along the borders where driveways are absent. Existing USTs consist of one 12,000-gallon and two 10,000-gallon double-wall fiberglass USTs, installed in 1986. According to the station manager, these USTs contain regular unleaded, plus unleaded, and super unleaded gasoline and are equipped with an

electronic leak detection system. In addition, the station personnel inventory the contents of the USTs by manually gauging the tanks.

#### 4.2 Soil Definition Status

Soils underlying the Site have been consistently characterized as silty clay or sandy clay, although clayey silt and sandy silt have also been described. These soils of low to very low permeability have complicated plans and available technologies for remediation at this Site. Copies of available lithologic soil boring logs and well construction details are provided within Appendix B. Constructed geologic cross-sections are provided within Appendix C.

#### 4.3 Ground-Water Definition Status

#### 4.3.1 Ground-Water Flow Direction, Depth, and Gradient

Ground-water depth varies across the Site and through time from approximately 11 to 24 ft bgs. Historically, the ground-water gradient has ranged from 0.003 ft/ft to 0.01 ft/ft. Based on ground-water elevation data, the ground-water flow direction has varied between southeast and southwest. Historic ground-water flow directions and gradients are provided in Table 3.

#### 4.3.2 Separate-Phase Hydrocarbons

Separate-phase hydrocarbons (SPH) or free product were first detected in on-site well MW-1 during quarterly monitoring and sampling activities conducted on 21 December 1988 by KEI. Three inches of SPH were reported in MW-1 during this visit. On 15 February 1989, SPH were detected in well MW-2 and sheen was observed in well MW-3. On 25 and 26 February 1991, SPH were observed within well RW-1 during quarterly monitoring and sampling activities. Free product has also been observed in wells MW-8, MW-9, and MW-10 since monitoring began. Consistent free product measurement and removal began in 1990 for MW-1, 1993 for wells MW-8, MW-9, and MW-10, and 2001 for RW-1. Historical free product measurements and removal amounts are provided in Table 4.

The free product currently observed at the Site consists of a black, heavily-degraded, almost grease-like material. Through observation the product can be classified as very aged and viscous. Operation of the ground-water extraction remediation system from 1992 to 1995 appeared to have had little effect on the free product thickness in wells associated with the Site. Since free product removal was initiated, measurable SPH have steadily decreased in wells MW-1, MW-8, MW-9, MW-10, and RW-1. Free product measurements during the recent Second Quarter 2008 monitoring event ranged from non-detect to 0.04 feet.

#### 4.3.3 Gasoline-Range Organics

Concentrations of TPH-G/GRO have been detected above laboratory reporting limits in each well associated with the Site (MW-1 through MW-10 and RW-1). However, concentrations in wells MW-3, MW-4, MW-6, and MW-7 have been intermittently detected at relatively low levels since monitoring first began. The highest on-site concentration of TPH-G/GRO was reported in well MW-1 (1,700,000  $\mu$ g/L), which is located approximately ten feet directly north

of the UST complex and west of the dispenser islands. The highest off-site concentration of TPH-G/GRO was reported in MW-9 (1,500,000  $\mu$ g/L), which is located approximately 35 feet east-southeast of the USTs. Results of ground-water sampling and laboratory analysis are summarized in Table 1 and Appendix A. Second Quarter 2008 GRO concentrations are included in the map of ground-water elevation contours provided as Drawing 3. Drawing 4 depicts the TPH-G/GRO iso-concentration contours map of the Site for First Quarter 2007 (from the most recent monitoring event that sampled the greatest number of Site wells).

## 4.3.4 Benzene, Toluene, Ethylbenzene, and Xylenes

Concentrations o BTEX have been detected above laboratory reporting limits in each well associated with the Site (MW-1 through MW-10 and RW-1). However, concentrations in wells MW-3, MW-4, MW-6, and MW-7 have been intermittently detected at relatively low levels since monitoring first began. The highest on-site concentrations of Benzene and Toluene were reported in well MW-2, which is located approximately 40 feet south of the UST complex, at 15,000 µg/L and 21,000 µg/L, respectively. The highest on-site concentrations of Ethylbenzene and Total Xylenes were reported in well MW-1 at 24,000 µg/L and 120,000 µg/L, respectively. The highest off-site concentrations of Benzene and Ethylbenzene were reported in well MW-8, which is located approximately 130 feet south-southeast of the UST complex, at 19,000 µg/L and 20,000  $\mu$ g/L, respectively. The highest off-site concentration of Toluene was reported in MW-10, located approximately 100 feet south of the USTs, at 38,000 µg/L. The highest concentration of Total Xylenes was detected in MW-9 at 120,000 µg/L. Results of ground-water sampling and laboratory analysis are summarized in Table 1 and Appendix A. Second Quarter 2008 Benzene concentrations are included in the map of ground-water elevation contours provided as Drawing 3. Drawing 5 depicts the benzene iso-concentration contours map of the Site for First Quarter 2007 (from the most recent monitoring event that sampled the greatest number of Site wells).

### 4.3.5 <u>Methyl-Tertiary Butyl Ether</u>

Methyl-Tertiary Butyl Ether (MTBE) has been detected above laboratory reporting limits in each well associated with the Site (MW-1 through MW-10 and RW-1). However, concentrations in wells MW-3, MW-4, MW-6, and MW-7 have been intermittently detected at relatively low levels since monitoring first began. The highest on-site concentration of MTBE was reported in well RW-1, which is located approximately ten feet south of the UST complex, at 78,000  $\mu$ g/L. The highest off-site concentration of MTBE was detected in MW-8 at 5,700  $\mu$ g/L. Results of ground-water sampling and laboratory analysis are summarized in Table 1 and Appendix A. Second Quarter 2008 MTBE concentrations are included in the map of ground-water elevation contours provided as Drawing 3. Drawing 6 depicts the MTBE iso-concentration contours map of the Site for First Quarter 2007 (from the most recent monitoring event that sampled the greatest number of Site wells).

### 4.4 Regional Geology

According to the *East Bay Plain Groundwater Basin Beneficial Use Evaluation Report* (California Regional Water Quality Control Board – San Francisco Bay Region/SFRWQCB, June 1999), the Site is located within the Oakland Sub-Area of the East Bay Plain of the San Francisco Basin. The Oakland Sub-Area contains a sequence of alluvial fans. The alluvial fill thickness ranges from 300 to 700 feet deep. There are no well-defined aquitards such as estuarine muds. The largest and deepest wells in this sub-area historically pumped one to two million gallons per day at depths greater than 200 feet. Overall, sustainable yields are low due in part to low recharge potential. The Merritt sand in West Oakland was an important part of the early water supply for the City of Oakland. It is shallow (up to 60 feet), but before the turn of the last century, septic systems contaminated the water supply wells.

Throughout most of the Alameda County portion of the East Bay Plain, from Hayward north to Albany, water level contours show that the general direction of ground-water flow is from east to west or from the Hayward Fault to the San Francisco Bay. Ground-water flow direction generally correlates to topography. Flow direction and velocity are also influenced by buried stream channels that typically are oriented in an east to west direction. In the southern end of the study area however, near the San Lorenzo Sub-Area, the direction of flow may not be this simple. According to information presented in *East Bay Plain Groundwater Basin Beneficial Use Evaluation Report*, the small set of water level measurements available seemed to show that the ground water in the upper aquifers may be flowing south, with the deeper aquifers, the Alameda Formation, moving north. The nearest natural drainage is Peralta Creek, located approximately 500 feet north of the Site. Peralta Creek flows generally east to west near the Site vicinity.

### 4.5 Topography

The Site is situated at an approximate elevation of 175 feet above mean sea level. The Site is relatively flat, but slopes slightly to the southwest, consistent with the local topography.

### 4.6 Stratigraphy

Sediments encountered at the Site consist primarily of silty clays or clayey silts with varying amounts of sand and gravel, extending from the ground surface to the total depth investigated, approximately 45 ft bgs. Boring logs are provided in Appendix B. Geologic cross-sections encompassing both on-site and off-site lithology are provided in Appendix C.

### 4.7 Preferential Pathway Analysis

Although some underground utilities within the public right-of-way were included in maps produced by URS (Appendix C), BAI has no record of a formal utility survey of the Site and surrounding area. Therefore, it is unknown whether utility trenches within and near the Site and current plume area could be serving as preferential pathways for contaminant migration above or below the ground-water table. However, due to the significantly greater depth to water than that of common underground utilities, it is unlikely that pathways created by underground conduits on or near the Site would act as preferential pathways for contaminant migration. This is especially true if the presumed mode of contaminant release was from the invert of the older USTs removed from the Site in 1986.

### 5.0 **REMEDIATION STATUS**

#### 5.1 Remedial Actions Taken

As mentioned previously, each of the USTs were removed from the Site and replaced, along with the additional facilities associated with an active service station (dispenser islands, product lines, etc.). Numerous soil borings and monitor wells have also been installed to delineate and monitor the extent of contamination and migration as discussed in previous sections. A ground-water extraction remediation system was installed on-site and operated between November 1992 and September 1995. On-site well RW-1, located approximately ten feet south of the UST complex, was utilized as the sole extraction well during system operation. Approximately 935,229 gallons of water was extracted at approximately one gallon per minute from RW-1 between 1992 and 1995. In addition to the ground-water extraction system, free product measurement and removal has been conducted in wells MW-1, MW-2, MW-8, MW-9, MW-10, and RW-1. Since September 2007, absorbent socks have been suspended across the ground-water table within wells MW-1, MW-2, MW-8, MW-9, MW-10, and RO-1. Since September 2007, absorbent socks have been suspended across the ground-water table within wells MW-1, MW-2, MW-8, MW-9, MW-10, and RO-1. A three-day mobile DPE event was conducted in late November 2007. Approximately 0.0091 lbs of GRO and 0.0003 lbs of Benzene in 2,090 gallons of ground water, and 14.0 lbs of GRO and 0.029 lbs of Benzene in soil vapor were removed from the subsurface during extraction activities.

#### 5.2 Areas Remediated

Remedial action has taken place in the immediate vicinity of the USTs and dispenser islands. Monitor wells and investigative borings have been installed on-site to the east, west and south. Monitor wells and investigative borings have also been installed off-site to the west, southwest, south, and southeast of the property. Free product removal has been conducted primarily on the southern portion of the Site, off-site to the south (downgradient), and immediately north of the UST complex. The remediation system extracted ground water from well RW-1, which is located adjacent and just south (downgradient) of the USTs.

#### 5.3 Remediation Effectiveness

Replacement of the facility infrastructure has substantially removed the primary onsite contaminant sources. Free product thickness and presence has dramatically decreased since measurement and removal was first initiated. The effectiveness of the ground-water extraction system appears to have had some effect. Contaminant concentrations within the ground water on-site and off-site were not noticeably decreased during or after the operation of the remediation system. No remedial action has been taken to address the onsite soil contamination.

### 6.0 WELL AND SENSITIVE RECEPTOR SURVEY

### 6.1 Designated Beneficial Shallow and Deep Ground-Water Use

According to the *East Bay Plain Groundwater Basin Beneficial Use Evaluation Report*, the City of Oakland does not have "any plans to develop local ground-water resources for drinking water purposes, because of existing or potential saltwater intrusion, contamination, or poor or limited

quantity." However, the California Regional Water Quality Control Board – San Francisco Bay Region's Basin Plan denotes existing beneficial uses of municipal and domestic supply (MUN), industrial process supply (PROC), industrial service supply (IND), and agricultural supply (AGR) for the East Bay Plain ground-water basin.

### 6.2 Well Survey Results

A sensitive receptors survey was conducted by Alton Geoscience on 20 February 1991. This survey concluded that no public water supply wells are located within 2,500 feet of the Site and no private water supply wells are located within 1,000 feet of the Site. The nearest residence was stated to be within approximately 50 feet of the Site. Allandale School is located approximately 1,000 feet from the Site and the nearest hospital is approximately 11,000 feet away. Peralta Creek is the nearest surface body of water at approximately 500 feet north of the Site. The local water supply was described as public and supplied by the East Bay Municipal Water District. The supplier's water source was said to be provided by Sierra snow melt and the Pardee Dam. The aquifer was classified as a Class III aquifer, which is not a potential source of drinking water. A copy of the Sensitive Receptors Survey/Site Survey and Literature Search conducted by Alton is provided within Appendix D.

#### 6.3 Likelihood of Impact to Wells

Based on the results of the well survey, it is unlikely that the ground-water contamination associated with the Site poses a potential threat to wells. No private wells were identified within 1,000 feet of the Site and no public wells were identified within 2,500 feet of the Site.

#### 6.4 Likelihood of Impact to Surface Water

Based on the results of the well survey, Peralta Creek is the closest surface water to the Site (approximately 500 feet north). Ground-water contamination associated with the Site is unlikely to impact Peralta Creek due to the observed ground-water flow direction, which is generally between southwest and southeast.

### 7.0 RISK ASSESSMENT

#### 7.1 Site Conceptual Exposure Model

The Site is currently an operational 76-brand service station owned by ConocoPhillips. The Site is open to the public and by authorized environmental professionals performing sampling or other relevant activities. Review of historical investigation data indicates that the majority of soil and ground-water contamination associated with the Site is present at depths generally greater than 15 ft beneath and downgradient of the UST complex area. Public and general occupational exposure to these secondary sources of contamination is believed to be remote and/or of short duration.

### 7.2 Exposure Pathways

Potential exposure pathways associated with this Site include human inhalation, ingestion, and absorption risks by environmental professionals. A remote but unknown potential exposure pathway might be human inhalation by tradesmen in the underground utility installation and maintenance occupation. The likelihood of vapor migration has not been verified by a soil-gas investigation. However, the soil concentrations present would seem unlikely to present a viable exposure pathway of concern. It is also noted that the majority of soil and ground-water contamination associated with this Site is located in the southern portion of the Site near Sutter Street and 35<sup>th</sup> Avenue, away from the station building, where employees are present for extended periods of time. Soil and ground-water contamination also appears to be present offsite to the south and southwest within roadways, which are rarely frequented by people not traveling in a vehicle. In addition, customers are not present for extended periods while utilizing the station, and would be congregating in open-air areas.

#### 7.3 Risk Assessment Status

A formal Risk Assessment has not been performed for this Site. Based on the geologic/ hydrogeologic characteristics and limited viable exposure pathways, consideration should be given to development of risk-based cleanup levels in lieu of strict adherence to Maximum Contaminant Levels for drinking water, Environmental Screening Levels or California Human Health Screening Levels.

#### 7.4 Identified Human Exceedances

Human exceedances are unknown at this time but unlikely due to the geologic/hydrogeologic characteristics and location of the contaminants.

#### 7.5 Identified Ecological Exceedances

Ecological exceedances are unknown at this time but unlikely due to the geologic/hydrogeologic characteristics and location of the contaminants.

### 8.0 FEASIBILITY STUDY

#### 8.1 Screening of Remediation Technologies

Several potential full-scale remediation technologies described within the Remediation Technologies Screening Matrix and Reference Guide, 4<sup>th</sup> Edition (Federal Remediation Technologies Roundtable, 2002) were evaluated to identify feasible remediation alternatives for the complex conditions and contamination at the Site. The Federal Remediation Technologies Roundtable is a working group including the Federal Environmental Protection Agency, Department of Defense, Department of Energy, Department of the Air Force, Department of the Interior, Department of the Army, Department of the Navy, and National Aeronautics and Space Administration. Of the approximately 60 remediation technologies described, 11 remediation technologies (and two methods of recovery enhancement) were screened for viability in this section. In addition to the technologies listed, a No-

Action option was evaluated. The No-Action option is typically included in feasibility studies to represent the baseline do-nothing action for comparison purposes. The technologies assessed in this initial screening are listed in the matrix below. Also presented is the media each technology would address.

	Μ	edia
Remediation Technology	Soil	Water
No Action		
Excavation	Х	
Bioventing	Х	
Soil Vapor Extraction	Х	
Dual-Phase Extraction and Treatment	Х	Х
Chemical Oxidation	Х	Х
Enhanced Bioremediation	Х	Х
Air Sparging	(X)	Х
In-Well Air Stripping	(X)	Х
Bioslurping		Х
Ground Water Extraction and Treatment		Х
Monitored Natural Attenuation		Х
Recovery Enhancements		
Thermal Treatment	X	X
Fracturing/Hydrofracturing	X	X

## Summary of Remediation Technologies Evaluated

### 8.1.1 <u>No Action</u>

Based on the hydrocarbon concentration trends in ground water, the no action option is not expected to be acceptable to ACEH. The no-action option is retained as a baseline for comparison.

#### 8.1.2 Excavation

With excavation, contaminated material is physically removed and transported to permitted off-site treatment and/or disposal facilities. Factors that limit the applicability and effectiveness of the general process include:

- Generation of fugitive emissions may be a problem during operations.
- The distance from the contaminated site to the nearest disposal facility with the required permit(s) will affect cost.
- Depth and composition of the media requiring excavation must be considered.
- Transportation of the soil through populated areas may affect community acceptability.

At this time, deeper soil impacts are known to exist at the Site, potentially beyond the reach of conventional excavating equipment. Excavation would not address the significant concentrations of hydrocarbons in ground water at the Site. Furthermore and most importantly, the presumed majority of the secondary source area is beneath the existing USTs at the Site. These USTs are owned and operated by ConocoPhillips and therefore generally not able to be disturbed or their operations hindered. Excavation is therefore screened from consideration at this time. Excavation may be

reassessed at a future date, however, if the work could be performed to coincide with an action such as UST replacement where excavation would not disrupt ConocoPhillips operation of the station.

## 8.1.3 <u>Bioventing</u>

Bioventing is an in-situ biological treatment that stimulates the natural in-situ biodegradation of aerobically degradable compounds in soil by providing oxygen to existing soil microorganisms. It does not directly address contamination in ground water. In contrast to soil vacuum vapor extraction (SVE), bioventing uses low air flow rates to provide just enough oxygen to sustain aerobic microbial activity. Oxygen is most commonly supplied through direct air injection into residual contamination in soil. In addition to degradation of adsorbed fuel residuals, volatile compounds are biodegraded as vapors move slowly through biologically active soil. Regulatory acceptance of this technology has been obtained in 30 states and in all 10 EPA regions. Bioventing is a medium to long-term technology. Cleanup ranges from a few months to several years. However, a critical factor that limits the applicability and effectiveness of this process is the presence of low permeability soils. Therefore, bioventing alone will not be retained for further consideration and evaluation due to the extensive presence of clays and silty clays at the Site which would severely reduce bioventing performance, and its inability to directly address ground-water contamination.

## 8.1.4 Soil Vapor Extraction

Soil Vapor Extraction (SVE) is an in situ unsaturated (vadose) zone soil remediation technology in which a vacuum is applied to the soil to induce the controlled flow of air and remove volatile contaminants from the soil. The gas leaving the soil may be treated to recover or destroy the contaminants, depending on local and state air discharge regulations. Vertical extraction vents are typically used at depths of five feet or greater and have been successfully applied as deep as 300 feet. Horizontal extraction vents (installed in trenches or horizontal borings) can be used as warranted by contaminant zone geometry, drill rig access, or other site-specific factors. For the soil surface, geomembrane covers are often placed over the soil surface to prevent short circuiting and to increase the radius of influence of the wells. Ground-water depression pumps may be used to reduce ground water upwelling induced by the vacuum or to increase the depth of the vadose zone. Air injection is effective for facilitating extraction of deep contamination, contamination in low permeability soils, and contamination in the saturated zone. The duration of operation and maintenance for in situ SVE is typically medium- to long-term.

Factors that may limit the applicability and effectiveness of the process include:

- Soil that has a high percentage of fines and a high degree of saturation will require higher vacuums (increasing costs) and/or hindering the operation of the in situ SVE system.
- Large screened intervals are required in extraction wells for soil with highly variable permeabilities or stratification, which otherwise may result in uneven delivery of gas flow from the contaminated regions.
- Soil that has high organic content or is extremely dry has a high sorption capacity for VOCs, which results in reduced removal rates.
- Exhaust air from in situ SVE system may require treatment to eliminate possible harm to the public and the environment.
- As a result of off-gas treatment, residual liquids may require treatment/disposal. Spent activated carbon will require regeneration or disposal.

• SVE is not effective in the saturated zone. However, lowering the water table can expose more media to SVE (this may address concerns regarding LNAPLs).

The critical factor that limits the applicability and effectiveness of this process at the Site is the presence of very low permeability soils. Therefore, SVE alone will not be retained for further consideration and evaluation due to the extensive presence of clays and silty clays at the Site which would severely reduce SVE performance, and its inability to directly address ground-water contamination.

### 8.1.5 <u>Dual-Phase Extraction and Treatment</u>

Dual-Phase Extraction (DPE), also known as multi-phase extraction and vacuum enhanced extraction, is a technology that uses a high vacuum system to remove various combinations of contaminated ground water, separate-phase petroleum hydrocarbons, and hydrocarbon vapor from the subsurface. Extracted liquids and vapors are treated and collected for disposal, or re-injected to the subsurface (where permissible under applicable state laws). In DPE systems for liquid/vapor treatment, a high vacuum system is used to remove liquid and gas from low permeability or heterogeneous formations. The vacuum extraction well includes a screened section in the zone of contaminated soils and ground water. It removes contaminants from above and below the water table. The system lowers the water table around the well, exposing more of the formation. Contaminants in the newly exposed vadose zone are then accessible to vapor extraction. Once above ground, the extracted vapors or liquid-phase organics and ground water are separated and treated.

Factors that may limit the applicability and effectiveness of the process include:

- Site geology and contaminant characteristics/distribution.
- Combination with complementary technologies (e.g., pump-and-treat) may be required to recover ground water from high yielding aquifers.
- DPE requires both water treatment and vapor treatment.
- Soil type determines permeability, which is the primary cost driver. DPE works best for permeable sand-silt mixtures. Impermeable (clayey) or excessively permeable (gravel/sand) soils are more recalcitrant.

The critical factor that limits the applicability and effectiveness of this process at the Site is the presence of very low permeability soils. A Mobile DPE Event was conducted at the Site during three days in late November 2007 as an Interim Response Measure. Approximately 0.0091 lbs of GRO and 0.0003 lbs of Benzene in 2,090 gallons of ground water and 14.0 lbs of GRO and 0.029 lbs of Benzene in soil vapor were removed from the subsurface during extraction activities. It is believed that contaminant recovery efficiency was limited due to the relatively tight soil permeability in the vadose zone and beneath the ground-water table. Although not optimum due to the extensive presence of clays and silty clays at the Site, DPE will be retained for further consideration and evaluation.

### 8.1.6 In-Situ Oxidation

In-situ oxidation encompasses a wide range of technologies, including liquid chemical oxidant injection (e.g., hydrogen peroxide) and injection of air or ozone into the subsurface. The objective is to increase the oxygen content of ground water and enhance the rate of aerobic degradation of

organic contaminants by naturally occurring microbes. For best results, factors that must be considered include redox conditions, saturation rates, presence of nutrient trace elements, pH, temperature, and permeability of the subsurface materials. In-Situ Oxidation is a full-scale technology.

The following general factors may limit the applicability and effectiveness of the process:

- A ground-water circulation system may need to be created so that contaminants do not escape from zones of active biodegradation.
- Where the subsurface is heterogeneous, it is difficult to circulate the oxygenated solution throughout every portion of the contaminated zone. Higher permeability zones are cleaned up much faster because ground water flow rates are greater.
- High iron content in subsurface materials can rapidly reduce concentrations of oxygenated solutions.
- Amended hydrogen peroxide can be consumed very rapidly near the injection well, which can create two significant problems: biological growth can be limited to the region near the injection well, limiting adequate contamination/micro-organism contact throughout the contaminated zone; and biofouling of wells can retard the input of nutrients.
- A surface treatment system, such as air stripping or carbon adsorption, may be required to treat extracted ground water prior to re-injection or disposal.

In-situ oxidation is a potentially effective treatment technology for the Site and will be retained for further evaluation and comparison of viable treatment alternatives.

### 8.1.7 Enhanced Bioremediation

Enhanced bioremediation is a process in which indigenous or inoculated micro-organisms (e.g., fungi, bacteria, and other microbes) degrade (metabolize) organic contaminants found in soil and/or ground water, converting them to innocuous end products. Nutrients, oxygen, or other amendments may be used to enhance bioremediation and contaminant desorption from subsurface materials. In the presence of sufficient oxygen (aerobic conditions), and other nutrient elements, microorganisms will ultimately convert many organic contaminants to carbon dioxide, water, and microbial cell mass.

Enhanced bioremediation typically involves the percolation or injection of ground water or uncontaminated water mixed with nutrients and saturated with dissolved oxygen. Sometimes acclimated microorganisms (bioaugmentation) and/or another oxygen source such as hydrogen peroxide is also added. An infiltration gallery is typically used for shallow contaminated soils, and injection wells are used for deeper contaminated soils and ground water.

In the absence of oxygen (anaerobic conditions), the organic contaminants will be ultimately metabolized to methane, limited amounts of carbon dioxide, and trace amounts of hydrogen gas. Under sulfate-reduction conditions, sulfate is converted to sulfide or elemental sulfur. Under nitrate-reduction conditions, dinitrogen gas is ultimately produced.

Enhanced bioremediation may be classified as a long-term technology which may take several years for cleanup of a plume. However, factors that may limit the applicability and effectiveness of the process include:

- Cleanup goals may not be attained if the soil matrix prohibits contaminant-microorganism contact.
- The circulation of water-based solutions through the soil may increase contaminant mobility and increase contaminant mobility and concentrations of the underlying ground water.
- Preferential colonization by microbes may occur causing clogging of nutrient and water injection wells.
- Preferential flow paths may severely decrease contaminant contact between injected fluids and contaminants through the contaminated zones. System is not optimal for clay, highly layered, or heterogeneous subsurface environments because of oxygen (or other electron acceptor) transfer limitations.
- Concentrations of hydrogen peroxide greater than 100-200 ppm in ground water inhibit the activity of microorganisms.

Enhanced Bioremediation is a potentially effective treatment technology for the Site and will be retained for further evaluation and comparison of viable treatment alternatives.

# 8.1.8 <u>Air Sparging</u>

Air sparging is an in situ technology in which air is injected through a contaminated aquifer. Injected air traverses horizontally and vertically in channels through the soil column, creating an underground stripper that removes contaminants by volatilization. This injected air helps flush (bubble) the contaminants up into the unsaturated zone where a vapor extraction system is usually implemented in conjunction with air sparging to remove the generated vapor phase contamination. This technology is designed to operated at high flow rates to maintain increased contact between ground water and soil and strip more ground water by sparging. Oxygen added to contaminated ground water and vadose zone soils can also enhance biodegradation of contaminants below and above the water table. Air sparging has a medium to long duration which may last, generally, up to a few years.

Factors that may limit the applicability and effectiveness of the process include:

- Air flow through the saturated zone may not be uniform, which implies that there can be uncontrolled movement of potentially dangerous vapors.
- Depth of contaminants and specific site geology must be considered.
- Air injection wells must be designed for site-specific conditions.
- Soil heterogeneity may cause some zones to be relatively unaffected.

The predominant clay layer from the surface to below ground water at the Site is thought to reduce the likely effectiveness of air sparging at the Site. Therefore, air sparging will not be retained for further evaluation.

# 8.1.9 In-Well Air Stripping

With in-well air stripping technology air is injected into a vertical well that has been screened at two depths. The lower screen is set in the saturated zone, and the upper screen is in the unsaturated

(vadose) zone. Pressurized air is injected into the well below the water table, aerating the water. The aerated water rises in the well and flows out of the system at the upper screen. Contaminated ground water is drawn into the system at the lower screen. The VOCs vaporize within the well at the top of the water table, as the air bubbles out of the water. The vapors are drawn off by a soil vapor extraction (SVE) system. The partially treated ground water is never brought to the surface; it is forced into the unsaturated zone, and the process is repeated as water follows a hydraulic circulation pattern or cell that allows continuous cycling of ground water. As ground water circulates through the treatment system in situ, contaminant concentrations are gradually reduced. Modification to the basic in-well stripping process may involve additives injected into the stripping well to enhance biodegradation (e.g., nutrients, electron acceptors, etc.). The duration of in-well air stripping is short- to long-term, depending upon contaminant concentrations, Henry's law constants of the contaminants, the radius of influence, and site hydrogeology.

Circulating wells provide a technique for subsurface remediation by creating a three-dimensional circulation pattern of the ground water. Ground water is drawn into a well through one screened section and is pumped through the well to a second screened section where it is reintroduced to the aquifer. The flow direction through the well can be specified as either upward or downward to accommodate site-specific conditions. Because ground water is not pumped above ground, pumping costs and permitting issues are reduced and eliminated, respectively. Also, the problems associated with storage and discharge are removed. In addition to ground water treatment, circulating well systems can provide simultaneous vadose zone treatment in the form of bioventing or soil vapor extraction.

Circulating well systems can provide treatment inside the well, in the aquifer, or a combination of both. For effective in-well treatment, the contaminants must be adequately soluble and mobile so they can be transported by the circulating ground water. Because circulating well systems provide a wide range of treatment options, they provide some degree of flexibility to a remediation effort.

The following factors may limit the applicability and effectiveness of the process:

- In general, in-well air strippers are more effective at sites containing high concentrations of dissolved contaminants with high Henry's law constants.
- Fouling of the system may occur by infiltrating precipitation containing oxidized constituents.
- Shallow aquifers may limit process effectiveness.
- Effective circulating well installations require a well-defined contaminant plume to prevent the spreading or smearing of contamination. They should not be applied to sites containing non-aqueous phase liquids to prevent the possibility of smearing the contaminants.
- Circulating wells are limited to sites with horizontal conductivities greater than 10<sup>-5</sup> cm/sec and a ratio of horizontal to vertical conductivities between three and ten. A ratio of less than three indicates short circulation times and a small radius of influence. If the ratio is greater than ten, the circulation time may be unacceptably long.
- Circulating wells should not be utilized at sites that have lenses of low-conductivity deposits.
- In well stripping may not be efficient in sites with strong natural flow patterns.

The low hydraulic conductivities measured in the clays at the Site is thought to limit the effectiveness of circulating wells at the Site. Therefore, in-well air stripping will not be retained for further evaluation.

## 8.1.10 <u>Bioslurping</u>

Bioslurping is the adaptation and application of vacuum enhanced dewatering technologies to remediate hydrocarbon-contaminated sites. Bioslurping utilizes elements of both, bioventing and free-product recovery, to address two separate contaminant media. Bioslurping combines elements of both technologies to simultaneously recover free product and bioremediate vadose zone soils. Bioslurping can improve free-product recovery efficiency without extracting large quantities of ground water. In bioslurping, vacuum-enhanced pumping allows light, non-aqueous phase liquids to be lifted off the water table and release from the capillary fringe. This minimizes changes to the water table elevation which minimizes the creation of a smear zone. Bioventing of vadose zone soils is achieved by drawing air into the soil due to withdrawing soil gas via the recovery well. The system is designed to minimize environmental discharge of ground water and soil gas. When free-product removal activities are completed, the bioslurping system is easily converted to a conventional bioventing system to complete the remediation. Operation and maintenance duration for bioslurping varies from a few months to years, depending on specific site conditions.

Factors that may limit the applicability and effectiveness of the bioslurping process include:

- Bioslurping is less effective in tight (low-permeability) soils.
- Low soil moisture content may limit biodegradation and the effectiveness of bioventing which tends to dry out soils.
- Low temperatures slow remediation.
- Frequently, the off-gas from the bioslurper system requires treatment before discharge. However, the treatment of off-gas may only be required shortly after the startup of the system as fuel rates decrease.
- At some sites, bioslurper systems can extract large volumes of water that may need to be treated prior to discharge depending upon the concentration of contaminants in the process water.
- Since the fuel, water and air are removed from the subsurface in one stream, mixing of the phases occurs. These mixtures may require special oil/water separators or treatment before the process water can be discharged.

The critical factor that limits the applicability and effectiveness of this process at the Site is the presence of very low permeability soils. In addition, the nature of the separate-phase hydrocarbons at the Site is that of a viscous, black grease, not very amenable at flowing through the contaminated formation without some additional method of enhancing formation recovery. Therefore, bioslurping alone will not be retained for further consideration and evaluation.

#### 8.1.11 Ground-Water Extraction and Treatment

In Ground Water Extraction and Treatment (GWET), ground water is pumped through a series of canisters containing activated carbon to which dissolved organic contaminants adsorb. This technology requires periodic replacement or regeneration of saturated carbon. Costs are typically high if used as the primary treatment on waste streams with high contaminant concentration levels. A GWET system operated at the Site from November 1992 through September 1995 removing 935,229 gallons at approximately one gallon per minute from recovery well RW-1. GWET will not

be retained for further evaluation based on poor cost-effectiveness when compared to other technologies.

#### 8.1.12 Monitored Natural Attenuation

Monitored Natural Attenuation (MNA) is sometimes referred to as Intrinsic Remediation, Bioattenuation, or Intrinsic Bioremediation. Natural subsurface processes such as dilution, volatilization, biodegradation, adsorption, and chemical reactions with subsurface materials are allowed to reduce contaminant concentrations to acceptable levels. MNA is not a "technology" per se, and there is significant debate among technical experts about its use at contaminated sites. Consideration of this option usually requires modeling and evaluation of contaminant degradation rates and pathways and predicting contaminant concentration at down-gradient receptor points. The primary objective of site modeling is to demonstrate that natural processes of contaminant degradation will reduce concentrations below regulatory standards or risk-based levels before potential exposure pathways are completed. In addition, long-term monitoring must be conducted throughout the process to confirm that degradation is proceeding at rates consistent with meeting cleanup objectives.

Monitored natural attenuation is not the same as "no action," although it is often perceived as such. CERCLA requires the evaluation of a "no action" alternative but does not require evaluation of natural attenuation. MNA is considered on a case-by-case basis, and guidance on its use is still evolving.

Compared with other remediation technologies, natural attenuation has the following advantages:

- Less generation or transfer of remediation wastes;
- Less intrusive as few surface structures are required;
- May be applied to all or part of a given site, depending on site conditions and cleanup objectives;
- MNA may be used in conjunction with, or as a follow-up to, other (active) remedial measures;
- Overall cost will likely be lower than active remediation.

Factors that may limit applicability and effectiveness include:

- Data used as input parameters for modeling need to be collected;
- MNA is not appropriate where imminent site risks are present;
- Contaminants may migrate before they are degraded;
- Institutional controls may be required, and the site may not be available for reuse until contaminant levels are reduced;
- If free product exists, it may have to be removed;
- Long-term monitoring and associated costs;
- Longer time frames may be required to achieve remediation objectives, compared to active remediation;
- The hydrologic and geochemical conditions amenable to MNA are likely to change over time and could result in renewed mobility of previously stabilized contaminants and may adversely impact remedial effectiveness; and

• More extensive outreach efforts may be required in order to gain public acceptance of MNA.

Based on the hydrocarbon concentration trends in ground water at the Site, a remediation strategy that employs monitored natural attenuation (MNA) would not be expected to be acceptable to ACEH unless implemented in conjunction with an active form of remediation or unless MNA-specific monitoring indicates that natural attenuation processes are occurring at the Site. MNA is retained for possible combination with other active technologies.

### 8.1.13 Hydrofracturing

Hydrofracturing is not a remediation treatment technology per se, but a method of enhancing conductivity into a contaminated formation. Hydrofracturing is a pilot-scale technology in which pressurized water is injected to increase the permeability of consolidated material or relatively impermeable unconsolidated material. Fissures created in the process are filled with a porous medium that can facilitate bioremediation and/or improve extraction efficiency. Fractures promote more uniform delivery of treatment fluids and accelerated extraction of mobilized contaminants. Typical applications are linked with soil vapor extraction, insitu bioremediation, and pump-and-treat systems.

The fracturing process begins with the injection of water into a sealed borehole until the pressure of the water exceeds the overburden pressure and a fracture is created. A slurry composed of a coarsegrained sand and guar gum gel or a similar substitute is then injected as the fracture grows away from the well. After pumping, the sand grains hold the fracture open while an enzyme additive breaks down the viscous fluid. The thinned fluid is pumped from the fracture, forming a permeable subsurface channel suitable for delivery or recovery of a vapor or liquid.

The hydraulic fracturing process can be used in conjunction with soil vapor extraction technology to enhance recovery. Hydraulically-induced fractures are used to deliver fluids, substrates, and nutrients for insitu bioremediation applications. The technology has widespread use in the petroleum and water-well construction industries but is an innovative method for use at remediating hazardous waste sites.

Factors that may limit the applicability and effectiveness of this process include:

- The technology should not be used in bedrock susceptible to seismic activity.
- Investigation of possible underground utilities, structures, or trapped free product is required.
- The potential exists to open new pathways leading to the unwanted spread of contaminants.
- Pockets of low permeability may still remain after using this technology.
- There is an inability to control the final location or size of the fractures that are created.
- Fractures are anticipated to collapse due to overburden pressure.

Additionally, a number of factors affect the estimated costs of creating hydraulic fractures at a site. These factors include physical site conditions such as site accessibility and degree of soil consolidation, degree of soil saturation, and geographical location which affects availability of services and supplies. The first two factors also affect the effectiveness of hydraulic fracturing. However, a further complication is the issue of potential impacts to and liability for damage to operating USTs and underground infrastructure owned by others. Hydrofracturing is therefore screened from consideration at this time. Hydrofracturing may be reassessed at a future date, however, if the work could be performed to coincide with an action such as UST and product line replacement, where hydrofracturing would not disrupt ConocoPhillips operation of the station.

### 8.1.14 <u>Thermal Treatment</u>

Thermal treatment is not a remediation treatment technology per se, but a method of enhancing volatility and or mobility of contaminants within a geologic formation. Thermal treatment is an emerging full-scale technology that uses electrical resistance/electromagnetic/fiber optic/radio frequency heating or hot-air/steam injection to increase the volatility of contaminants and facilitate extraction. The process is typically linked with soil vapor extraction, insitu bioremediation, and pump-and-treat systems. However, a complication is the issue of potential impacts to and liability for damage to operating USTs and underground infrastructure owned by others. Thermal treatment is therefore screened from consideration at this time. Thermal treatment may be reassessed at a future date, however, if the work could be performed to coincide with an action such as UST and product line removal, where thermal treatment would not disrupt ConocoPhillips operation of the station.

### 8.2 Alternative Evaluation

Based on the initial technology screening above, the following technologies have been retained to assemble the alternatives that will be evaluated:

- Alternative 1: No Action
- Alternative 2: Dual-Phase Extraction and Treatment
- Alternative 3: Chemical Oxidation
- Alternative 4: Enhanced Bioremediation
- Alternative 5: Monitored Natural Attenuation

Using the *Remediation Technologies Screening Matrix and Reference Guide*, each of the alternatives were evaluated against the following screening factors:

- **Relative Costs?** Design, construction, and operation and maintenance (O&M) costs of the core process that defines each technology, exclusive of mobilization, demobilization, and pre- and post-treatment costs. Above average means a low degree of genral costs relative to other options. Average means an average degree of general costs relative to other options. Below average means a high degree of general costs relative to the other options.
- **Capital Intensive?** Is the technology capital-intensive, with significant costs for design and construction? Above average means low degree of capital investment. Average means average degree of capital investment. Below average means high degree of capital investment.
- **O&M Intensive?** Is the technology O&M-intensive, with significant costs for labor, operation, maintenance, and repair? Above average means low degree of O&M intensity. Average means average degree of O&M intensity. Below average means high degree of O&M intensity.

- **System Reliability/Maintainability?** The expected range of demonstrated reliability and maintenance relative to other effective technologies. Above average means high reliability and low maintenance. Average means average reliability and average maintenance. Below average means low reliability and high maintenance.
- **Time?** Time required to clean up a "standard" site using the technology. Above average means less than one year for in situ soils and less than three years for ground water. Average means one to three years for in situ soils and three to ten years for ground water. Below average means more than three years for in situ soil and more than ten years for ground water.

The following table presents relative ratings per screening factor for the three alternatives retained from the screening process above. The relative ratings are from the previously referenced *Remediation Technologies Screening Matrix and Reference Guide*.

				System	
	Relative	Capital	<b>O&amp;M</b>	<b>Reliability</b> /	
Technology	Cost	Intensive	Intensive	Maintainability	Time
No Action	Above	Below	Above	Above Average	Below
	Average	Average	Average		Average
DPE	Average	Below	Below	Average	Average
		Average	Average		
Chemical Oxidation	Average	Average	Below	Average	Above
			Average		Average
Enhanced Bioremediation	Above	Average	Below	Average	Unknown
	Average		Average		
Monitored Natural Attenuation	Above	Average	Below	Average	Unknown
	Average		Average		

It must be understood that the purpose of this feasibility study was not to identify the single-best remediation technology and recommend it for full-scale implementation. The purpose was to narrow the field of potentially viable remediation technologies worthy of further investigation and potential pilot testing. This objective has been met.

### 8.3 Data Gaps

To further evaluate the applicability of the potentially viable remediation technologies identified above, additional data must be gathered. The following data gaps have been identified:

- The mobile DPE event in November 2007 was conducted as an interim remedial measure. An 11 or 12 hour DPE event was conducted on just wells MW-1, MW-2 and RW-1. Although useful data was collected, its first objective was whether any contamination would be removed from the subsurface. It is presently unknown the effect of longer-duration tests on those wells, or whether yields from wells MW-8, MW-9, or MW-10 would justify extraction from these off-site wells.
- Aside from dissolved oxygen and ph, no data has been gathered yet on bio-parameters which would indicate aerobic/anaerobic or oxidizing/reducing conditions are present at

the Site. Additional data that would be useful includes: Oxidation-Reduction Potential, Alkalinity, Methane, Carbon Dioxide, Nitrate, Sulfate, Dissolved Sulfide, Ferrous Iron, and Manganese. Availability of this data is critical to determining the viability of Chemical Oxidation, Enhanced Bioremediation, or even Monitored Natural Attenuation as remediation technologies for the Site.

• Very limited information has been obtained to date regarding the presence and type of underground infrastructure both on and off the Site. As mentioned previously, the potential for preferential pathway migration through underground infrastructure trenches is remote given the depth of the release. However, knowledge of onsite and offsite underground utility locations is important for planning future remediation activities, especially with respect to giving any further thought to the potential recovery enhancement technologies described above.

#### 9.0 CONCLUSIONS AND RECOMMENDATIONS

#### 9.1 Conclusions

The findings and conclusions of this Site Conceptual Model with Feasibility Study Report are summarized below:

- Three steel USTs, originally installed in 1972, were removed from the southwestern portion of the Site in 1986 following a tank integrity test failure.
- In 1989 Mobil Oil Corporation sold the station to BP. In 1994, BP sold the station to Tosco, which was acquired by ConocoPhillips who now operates the 76-brand gasoline service station at the Site.
- Based on observations recorded on soil boring and monitoring well construction logs, soil types at the Site generally consist of low permeability silty clays.
- The average depth to ground water at the Site is approximately 20 ft bgs, but has fluctuated between 15 ft bgs to 25 ft bgs due to seasonal/annual precipitation and ground-water recharge.
- Ground-water flow direction beneath the Site is generally towards the southwest with the hydraulic gradient ranging between 0.003 ft/ft to 0.01 ft/ft.
- A ground-water extraction and treatment system operated for almost two years drawing approximately one gallon per minute from recovery well RW-1. The thickness of separate-phase hydrocarbons was reduced from a maximum of 1.8 ft in 1994 to the current 0.05-0.01 ft.
- The separate-phase hydrocarbons have degraded significantly and now resemble a black, viscous grease-like material.
- Due to the historically fluctuating ground-water table, it is believed that a thick smear zone has developed in the plume area.
- The fact that the existing USTs were placed back within the same area as the older USTs that had failed their integrity test, and the fact that the station is currently operated by

ConocoPhillips somewhat limits the ability of BP to actively pursue some of the more aggressive remediation technologies available at the present time.

#### 9.2 **Recommendations**

Based on the findings presented within this Site Conceptual Model and Feasibility Study Report, BAI proposes the following recommendations:

- Begin collection of bio-parameters during the regularly-scheduled quarterly monitoring/ sampling events. In addition to pH and Dissolved Oxygen currently collected, also collect Oxidation-Reduction Potential, Alkalinity, Methane, Carbon Dioxide, Nitrate, Sulfate, Dissolved Sulfide, Ferrous Iron, and Manganese. Samples should be collected by micro-purging in accordance with the Standard Operating Procedure contained within Appendix A to American Petroleum Institute Publication No.4658 – Methods for Measuring Indicators of Intrinsic Bioremediation: Guidance Manual.
- Perform a utility survey to identify public and private underground infrastructure both onsite and offsite in the area of impacted soil and ground water.
- Prepare a work plan for a DPE pilot test, this time of longer duration at wells MW-1, MW-2, and RW-1, as well as investigating offsite wells MW-8, MW-9, and MW-10 if equipment and traffic control logistics can be overcome.

### 10.0 CLOSURE

The findings presented in this document are based upon: observations of field personnel from previous consultants, the points investigated, and results of analytical tests performed by various laboratories. Our services were performed in accordance with the generally accepted standard of practice at the time this document was written. No other warranty, expressed or implied was made. This report has been prepared for the exclusive use of BP. It is possible that variations in soil or ground-water conditions could exist beyond points explored in this investigation. Also changes in site conditions could occur in the future due to variations in rainfall, temperature, regional water usage, or other factors.

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		TOC	Depth to	Product	Water Level			Concentra	ntions in (µ	g/L)					
Well and	DAD	Elevation	Water	Thickness	Elevation	GRO/	D	<b>T</b> .1	Ethyl-	Total	MTDE	DO	<b>T</b> . 1		0
Sample Date	P/NP	(feet msl)	(feet bgs)	(feet)	(feet msl)	TPHg	Benzene	1 oluene	Benzene	Aylenes	MIBE	(mg/L)	Lab	рн	Comments
<b>MW-1</b>															
7/9/1990		169.75		0.22											
12/21/1990		169.75		0.58											
3/7/1991		169.75	20.59	0	149.16										
4/1/1991		169.75	16.51	0.15	153.09										
6/27/1991		169.75		0.18											
9/27/1991		169.75		0.27											
12/18/1991		169.75		0.28											
7/3/1992		169.75	22.30	0.27	147.18										
10/5/1992		169.75	23.98	0.24	145.53										
1/13/1993		169.75	17.03	0.24	152.48										
4/23/1993		169.75	18.10	0.42	151.23										
7/12/1993		169.75	22.02	0.49	147.24										
10/21/1993		169.75	25.12	1.09	143.54										
1/21/1994		169.75	23.02	0.76	145.97										
4/20/1994		169.75	24.54	1.8	143.41										
8/1/1994		169.75	24.11	0.35	145.29										
12/23/1994		169.75	18.19		151.56										
1/26/1995		169.75	16.25	1.1	152.40										
6/8/95-6/28/95		169.75		1.25	145.63										
6/8/1995		169.75	22.92		146.83										
8/22/1995		169.75	24.45	0.85	144.45										
10/27/1995		169.75	25.41		143.65										
10/30/95-12/23/95		169.75		0.69											
1/25/1996		169.75	18.20		151.55										
1/25/96-2/16/96		169.75		1.40	150.15										
4/19/1996		169.75	19.06	1.22	149.47										
7/23/1996		169.75	22.98	0.89	145.88										
11/11/1996		169.75	23.99	0.89	144.78										
1/21/1997		169.75	16.80	0.9	152.05										
4/29/1997		169.75	21.90	0.85	147.00										
4/30/1997		169.75				92,000	3,500	8,100	4,400	23,800	6,900				с

		тос	Depth to	Product	Water Level			Concentra	ations in (µ	g/L)					
Well and Sample Date	P/NP	Elevation (feet msl)	Water (feet bgs)	Thickness (feet)	Elevation (feet msl)	GRO/ TPH9	Benzene	Toluene	Ethyl- Benzene	Total Xylenes	MTRE	DO (mg/L)	Lah	nH	Comments
MW 1 Cant	1/111	(recembr)	(leet bgb)	(ieee)	(reet mist)		Denzene	Tonucile	Denizene	ing tenes	mibe	(ing/11)	Lub	P11	Comments
MW-1 Cont.															
4/30/1997		169.75				100,000	3,600	8,000	4,000	21,300	7,700	5.2			
8/21/1997		169.75				120,000	3,200	8,100	3,800	19,600	5,200				с
8/21/1997		169.75	23.40		146.35	140,000	3,000	8,500	3,900	22,100	5,700	5.3			
11/2/97-12/9/97		169.75		0.87											
11/5/1997		169.75				88,000	7,300	4,800	3,600	16,900	8,200				с
11/5/1997		169.75	23.70		145.51	68,000	6,200	4,400	3,300	14,300	8,000	4.7			
2/3/1998		169.75	13.63	0.32	155.80										
2/4/1998		169.75				160,000	2,300	8,400	5,000	29,400	<10000				с
2/4/1998		169.75				190,000	2,200	10,000	5,600	32,000	<10000	5.3			
5/28/1998		169.75	18.03	0.17	151.55	87,000	980	3,900	3,600	19,000	2,900	3.8			
12/30/1998		169.75	19.50	0.08	150.17	70,000	530	3,200	2,900	16,000	3,600				
2/2/1999		169.75	18.93	0.03	150.79	79,000	480	3,100	3,500	21,000	3,500				
5/10/1999		169.75	18.28	0.03	151.44	110,000	160	1,900	3,700	24,000	3,000				
8/24/1999		169.75	20.13	0.06	149.56	110,000	850	1,300	1,900	19,000	<50				
11/3/1999		169.75	22.27	0.36	147.12	65,000	6,300	1,100	3,300	9,500	8,900				
3/1/2000		169.75	14.79	0.23	154.73										h
4/21/2000		169.75	18.10	0.33	151.32	61,000	330	780	2,700	17,000	1,300				
7/31/2000		169.75	21.60	0.53	147.62	1,500,000	340	2,100	24,000	120,000	2,700				
11/20/2000		169.75	21.69	0.37	147.69	1,700,000	1,800	2,300	19,000	93,000	3,900				
2/18/2001		169.75	16.70	0.13	152.92										
2/26/2001		169.75	14.38	0.15	155.22	100,000	658	466	4,210	15,000	1,890				
6/7/2001		169.75	20.78	0	148.97	70,000	705	440	3,870	12,200	2,720				
9/5/2001		169.75	23.36	0.35	146.04										j
11/30/2001		169.75	20.85	0.41	148.49										k
12/6/2001		169.75	18.72	0.27	150.76	39,000	3,500	237	2,150	4,500	5,400				
2/20/2002		169.75	17.43	0.15	152.17	52,000	465	271	1,600	11,400	106				
6/20/2002		169.75	21.18	0.34	148.23										j
9/11/2002		169.75	22.86	0.4	146.49										j
11/12/2002		169.75	22.65	0.37	146.73										j
1/29/2003		169.75	18.15	0.3	151.30										j,n
5/22/2003		169.75	18.49	0.2	151.06										j

		тос	Depth to	Product	Water Level		1	Concentra	ations in (µ	g/L)	r				
Well and Sample Date	P/NP	Elevation (feet msl)	Water (feet bos)	Thickness (feet)	Elevation (feet msl)	GRO/ TPHø	Benzene	Toluene	Ethyl- Benzene	Total Xylenes	MTRE	DO (mg/L.)	Lah	nH	Comments
MW 1 C	1/11	(reet hist)	(1000 053)	(itet)	(reet mst)	11115	Denzene	Tolucile	Deližene	Ayrenes	MIDL	(III <u>g</u> /L)	Luo	рп	Comments
MW-1 Cont.															
6/24/2003		169.75	21.44	0.35	147.96										0
7/28/2003		169.75	22.72	0.35	146.68										j
8/12/2003		169.75	22.64	0.23	146.88										0
9/12/2003		169.75	20.70	0.24	148.81										0
10/3/2003		169.75		0.23											
11/18/2003	NP	169.75	21.70	0.25	148.25										
12/31/2003		169.75		0.15											
2/2/2004		169.75		0.15											
02/23/2004	NP	169.75	16.34	0.09	153.48										
3/18/2004		169.75		0.09											
4/13/2004		169.75		0.24											
05/04/2004	NP	169.75	21.28	0.16	148.60										
6/2/2004		169.75		0.08											
7/2/2004		169.75		0.28											
08/04/2004		169.75	22.54	0.10	147.29										
09/22/2004	NP	169.75	22.76	0.20	147.15										
10/26/2004		169.75		0.12											
11/10/2004		169.75	20.19	0.14	149.67										
12/27/2004		169.75		0.08											
01/13/2005		169.75	14.58	0.03	155.19										
02/15/2005		169.75	16.13	0.04	153.65										
03/07/2005		169.75	13.31	0.01	156.45										
4/29/2005		169.75		0.01											
05/16/2005		169.75	15.74	0.02	154.03										j
6/21/2005		169.75		0.01											
7/7/2005		169.75		0.18											
08/17/2005		169.75	21.15	0.08	148.66										j
9/6/2005		169.75		0.02											
10/4/2005		169.75		0.12											
11/18/2005		169.75	20.15		149.60										j
12/30/2005		169.75		0.03											

		тос	Depth to	Product	Water Level			Concentra	ations in (µ	g/L)					
Well and	D/ND	Elevation	Water	Thickness	Elevation	GRO/	D	<b>T</b> -1	Ethyl-	Total V-1	MTDE	DO	Tah	11	Gammanta
Sample Date	P/NP	(leet msi)	(leet bgs)	(leet)	(leet msi)	IPHg	вепzепе	1 oluene	Benzene	Aylenes	MIBE	(mg/L)	Lab	рн	Comments
MW-1 Cont.															
1/24/2006		169.75		0.00											
02/07/2006		169.75	15.19	0.01	154.57										j
3/30/2006		169.75		0.00											
5/19/2006	Р	169.75	17.42		152.33	44,000	73	510	3,300	5,300	86		SEQM	6.9	u, t
8/23/2006		169.75	22.01	0.14	147.74										b, j
11/15/2006		169.75	21.98	0.18	147.91										b, j
2/14/2007		169.75	17.12	0.17	152.76										b, j
5/22/2007		169.75	19.49	0.01	150.26										b, j
8/15/2007		169.75	22.24	0.01	147.52										b, j
11/8/2007		169.75	21.84	0.01	147.92										b, j
2/20/2008		169.75	16.52	0.02	153.25										b, j
5/7/2008		169.75	20.91	0.02	148.86										b, j
MW-2															
7/9/1990		168.14													
12/21/1990		168.14													
3/7/1991		168.14	19.18		148.96										
4/1/1991		168.14	15.21		152.93										
6/27/1991		168.14													
9/27/1991		168.14													
12/18/1991		168.14													
7/3/1992		168.14	20.93		147.21										
10/5/1992		168.14	22.74		145.40										
1/13/1993		168.14	15.55		152.59										
4/23/1993		168.14	16.54		151.60										
7/12/1993		168.14	20.46		147.68										
10/21/1993		168.14	24.91		143.23										
1/21/1994		168.14	21.20		146.94										
4/20/1994		168.14	22.44		145.70	1,800	140	370	54	290	24	1.7			i
8/1/1994		168.14	22.24		145.90										
12/23/1994		168.14	16.25		151.89										

		тос	Depth to	Product	Water Level			Concentra	tions in (µ	g/L)		_			
Well and Sample Date	P/NP	Elevation (feet msl)	Water (feet bgs)	Thickness (feet)	Elevation (feet msl)	GRO/ TPHa	Ronzono	Toluene	Ethyl- Benzene	Total Xylenes	MTRF	DO (mg/L)	Lah	nH	Comments
	1/111	(reet hist)	(Itel bgs)	(ieet)	(rect msr)	mng	Denzene	Toluciic	Delizene	Ауннез	MIDE	(Ing/L)	Lab	рп	comments
MW-2 Cont.															
1/26/1995		168.14	14.55		153.59										
6/8/1995		168.14	21.18		146.96										
8/22/1995		168.14	22.76		145.38										
10/27/1995		168.14	23.61		144.53										
1/25/1996		168.14	15.95		152.19										
4/19/1996		168.14	17.33		150.81										
7/23/1996		168.14	21.25		146.89										
11/11/1996		168.14	22.27		145.87										
1/21/1997		168.14	15.19		152.95										
4/29/1997		168.14	20.22		147.92										
4/30/1997		168.14				130,000	4,600	15,000	6,000	37,000	<5000	5			
8/21/1997		168.14	21.74		146.40	110,000	6,000	16,000	4,700	28,000	<500	4.6			
11/5/1997		168.14	21.61		146.53	120,000	7,800	18,000	4,900	28,100	<2500	4.6			
2/3/1998		168.14	11.51		156.63	75,000	590	1,500	1,800	12,800	<2500	4.5			
5/28/1998		168.14	16.51		151.63	79,000	3,900	3,100	3,100	18,000	900	4.3			
12/30/1998		168.14	17.70		150.44	95,000	4,700	3,500	3,700	21,000	<250				
2/2/1999		168.14	15.46		152.68	170,000	3,500	1,500	5,200	34,000	<500				
5/10/1999		168.14	16.52		151.62	84,000	3,200	3,200	3,700	20,000	75				
8/24/1999		168.14	20.73		147.41	130,000	9,100	9,200	4,700	27,000	<250				
11/3/1999		168.14	20.93		147.21	120,000	10,000	21,000	4,700	30,200	2,200				
3/1/2000		168.14	13.37		154.77	39,000	1,400	1,500	1,700	8,100	44				
4/21/2000		168.14	16.59		151.55	68,000	3,300	2,500	3,100	20,000	260				
7/31/2000		168.14	16.37		151.77	99,000	5,600	1,400	4,300	22,000	490				
11/20/2000		168.14	19.71		148.43	37,000	5,100	1,500	1,300	4,800	2,800				
2/18/2001		168.14	15.29		152.85	54,000	5,020	3,880	2,850	15,400	1,010				
6/7/2001		168.14	19.43		148.71	110,000	7,240	4,380	4,160	22,100	567				
9/5/2001		168.14	22.44		145.70	69,000	5,750	5,790	2,770	14,200	1,510				
11/30/2001		168.14	19.58		148.56	120,000	7,270	6,540	4,590	23,000	794				
2/20/2002		168.14	16.39		151.75	56,000	2,410	2,270	2,910	14,300	160				
6/20/2002		168.14	19.77		148.37	86,000	7,310	6,490	3,080	14,600	659				
9/11/2002		168.14	21.60		146.54	130,000	7,600	13,000	5,400	30,000	<5000				

		тос	Depth to	Product	Water Level			Concentra	ations in (µ	g/L)					
Well and Sample Date	P/NP	Elevation (feet msl)	Water (feet bgs)	Thickness (feet)	Elevation (feet msl)	GRO/ TPHg	Benzene	Toluene	Ethyl- Benzene	Total Xylenes	MTBE	DO (mg/L)	Lab	pН	Comments
MW-2 Cont.														-	
11/12/2002		168.14	21.34		146.80	46,000	4,100	4,300	1,900	10,000	1,900				t
1/29/2003		168.14	16.80		151.34	77,000	4,700	2,600	2,800	13,000	820				n,t
5/22/2003		168.14	17.15		150.99	52,000	6,400	2,600	1,800	7,400	1,000				t
7/28/2003		168.14	21.47		146.67	31,000	6,900	5,500	2,200	12,000	1,700				р
11/18/2003	Р	168.14	20.50		147.64	23,000	3,300	800	500	2,000	500		SEQM	6.6	-
02/23/2004	Р	168.14	14.77		153.37	84,000	14,000	6,200	3,100	14,000	790		SEQM	6.6	t
05/04/2004	Р	168.14	20.09		148.05	120,000	15,000	17,000	4,900	24,000	780		SEQM	6.6	t
08/04/2004	Р	168.14	21.39		146.75	38,000	9,100	3,300	1,900	5,800	430		SEQM	6.69	t
11/10/2004	Р	168.14	18.98		149.16	22,000	4,400	2,000	940	3,600	310		SEQM	7.5	
02/15/2005	Р	168.14	15.62		152.52	67,000	11,000	4,200	3,000	11,000	690		SEQM	7.1	t
05/16/2005	Р	168.14	14.71		153.43	94,000	11,000	7,600	4,100	17,000	560		SEQM	6.5	
08/17/2005	Р	168.14	20.00		148.14	110,000	13,000	8,000	4,300	18,000	480		SEQM	6.6	
11/18/2005	Р	168.14	20.89		147.25	37,000	11,000	2,400	1,500	4,600	340		SEQM	6.6	
02/07/2006	Р	168.14	13.31		154.83	74,000	8,900	5,800	3,600	14,000	440		SEQM	6.7	
5/19/2006	Р	168.14	16.30		151.84	78,000	11,000	3,700	4,500	14,000	430		SEQM	6.6	t
8/23/2006	Р	168.14	20.83		147.31	100,000	12,000	9,100	5,800	25,000	480		TAMC	6.6	
11/15/2006		168.14	20.80		147.34	46,000	8,800	3,600	2,300	8,500	400	0.70	TAMC	6.73	
2/14/2007	Р	168.14	15.96	SHEEN	152.18	100,000	13,000	3,600	6,200	26,000	810	1.43	TAMC	6.97	t
5/22/2007	Р	168.14	18.20		149.94	91,000	15,000	8,700	4,700	20,000	1,000	0.08	TAMC	6.90	
8/15/2007	Р	168.14	21.23	SHEEN	146.91	14,000	7,300	130	280	600	260	4.24	TAMC	6.78	
11/8/2007	Р	168.14	20.32		147.82	22,000	7,400	420	640	1,700	240	1.21	TAMC	7.03	
2/20/2008		168.14	15.20	0.06	152.99										b, j
5/7/2008		168.14	19.80	0.04	148.37										b, j
MW-3															
7/9/1990		167.17				140	5.3	4.6	2	3.8					
12/21/1990		167.17				0.19	100	6	0.9	27					
3/7/1991		167.17	17.40		149.77	0.4	69	22	6.1	57					
4/1/1991		167.17	13.69		153.48										
6/27/1991		167.17				380	28	26	13	46					
9/27/1991		167.17				0.07	7.9		0.4	1.1					

		тос	Depth to	Product	Water Level		-	Concentra	ations in (µ	g/L)					
Well and	D/MD	Elevation	Water	Thickness	Elevation	GRO/	D	<b>T</b> - h	Ethyl-	Total V-l	MTDE	DO (mm/II)	Tab		Commente
Sample Date	<b>F</b> /IN <b>F</b>	(leet liist)	(leet bgs)	(leet)	(leet list)	Irng	Delizene	Toluelle	Belizelle	Aylenes	WIDE	(IIIg/L)	Lau	рп	Comments
MW-3 Cont.															
12/18/1991		167.17				0.26	34	24	0.8	28					
7/3/1992		167.17	19.59		147.58	71	9.4	0.9	5	13					
10/5/1992		167.17				<50	2.2	< 0.5	1.5	2.8					с
10/5/1992		167.17	21.22		145.95	67	5.1	1.1	6.1	8.1					
1/13/1993		167.17	13.63		153.54	830	50	34	42	89					i
4/23/1993		167.17	15.02		152.15	<50	< 0.5	< 0.5	< 0.5	< 0.5					i
4/23/1993		167.17				<50	< 0.5	< 0.5	< 0.5	< 0.5					c,i
7/12/1993		167.17	19.16		148.01	250	12	4.2	12	16	<5.0				i
10/21/1993		167.17				65	7.4	1	6.9	4.2					с
10/21/1993		167.17	21.81		145.36	52	4.4	1.4	4.7	3.3	<5.0				i
1/21/1994		167.17	19.94		147.23	57	3	3.4	3.6	9	<5.0				i
4/20/1994		167.17	20.24		146.93	600	26	23	33	88	28.7	1.8			i
8/1/1994		167.17				120	7.7	1.6	5.9	6.7	5.43				c,i
8/1/1994		167.17	20.74		146.43	99	6.2	1.1	4.5	5.2	<5.0	1.4			i
12/23/1994		167.17	14.70		152.47	<50	< 0.5	0.78	< 0.5	< 0.5	9.8	1.7			i
12/23/1994		167.17				<50	< 0.5	< 0.5	< 0.5	< 0.5					с
1/26/1995		167.17	12.89		154.28	190	16	0.5	35	24		6.6			d
6/8/1995		167.17	19.95		147.22	330	21	4	34	32		7			
8/22/1995		167.17	21.41		145.76	150	14	< 0.50	< 0.50	1.6	<5.0	6.6			d
10/27/1995		167.17	22.43		144.74										
10/30/1995		167.17				51	2.4	< 0.50	< 0.50	<1.0	<5.0	6.9			
1/25/1996		167.17	14.03		153.14	<50	< 0.50	< 0.50	< 0.50	<1.0	5.1				
4/19/1996		167.17	15.26		151.91	460	55	4	33	63	<10	9.4			
7/23/1996		167.17	19.19		147.98	<50	< 0.5	< 0.5	< 0.5	< 0.5	<10	9.2			
11/11/1996		167.17	20.24		146.93	<250	<2.5	<5.0	<5.0	<5.0	<50	8.4			
1/21/1997		167.17	13.09		154.08	<50	< 0.5	<1.0	<1.0	<1.0	<10	5.4			
4/29/1997		167.17	18.14		149.03	<50	< 0.5	<1.0	<1.0	<1.0	<10	4.3			
8/21/1997		167.17	19.64		147.53	<50	<0.5	<1.0	<1.0	<1.0	<10	4.9			
11/5/1997		167.17	19.95		147.22	<250	<2.5	<5.0	<5.0	<5.0	<50	4.5			
2/3/1998		167.17	10.57		156.60	<50	< 0.50	<1.0	<1.0	<1.0	<10	4.7			
5/28/1998		167.17	14.65		152.52	330	<2.5	<5.0	<5.0	<5.0	<50	4.2			

		тос	Depth to	Product	Water Level			Concentra	ntions in (µ	g/L)					
Well and	DAD	Elevation	Water	Thickness	Elevation	GRO/	D	<b>T</b> 1	Ethyl-	Total		DO			
Sample Date	P/NP	(feet msl)	(feet bgs)	(feet)	(feet msl)	TPHg	Benzene	Toluene	Benzene	Xylenes	MTBE	(mg/L)	Lab	рН	Comments
MW-3 Cont.															
12/30/1998		167.17	16.63		150.54										
2/2/1999		167.17	13.12		154.05	<250	<5.0	<5.0	<5.0	<5.0	<5.0				
5/10/1999		167.17	14.21		152.96										
8/24/1999		167.17	14.36		152.81										
11/3/1999		167.17	19.21		147.96										
3/1/2000		167.17	15.17		152.00	<50	< 0.5	0.57	< 0.5	0.62	<0.5				
4/21/2000		167.17	14.88		152.29										
7/31/2000		167.17	15.29		151.88										
11/20/2000		167.17	17.31		149.86										
2/18/2001		167.17	12.85		154.32	160	1.95	1.31	10.2	9.09	1				
6/7/2001		167.17	18.00		149.17										
9/5/2001		167.17	20.32		146.85										
11/30/2001		167.17	16.94		150.23										
2/20/2002		167.17	14.84		152.33	86	< 0.5	0.845	6.58	5.75	<0.5				
6/20/2002		167.17	18.40		148.77										
9/11/2002		167.17	20.06		147.11										
11/12/2002		167.17	19.84		147.33										
1/27/2003		167.17	14.83		152.34	850	20	9.7	24	45	0.76				n
5/22/2003		167.17	15.60		151.57										
7/28/2003		167.17	20.12		147.05										р
11/18/2003		167.17	19.15		148.02										
02/23/2004		167.17	13.53		153.64	160	< 0.50	1.1	9.6	12	< 0.50		SEQM	6.7	
05/04/2004		167.17	18.61		148.56										
08/04/2004		167.17	19.21		147.96										
11/10/2004		167.17	17.48		149.69										
02/15/2005	Р	167.17	14.31		152.86	500	7.8	1.8	9.2	9.6	1.7		SEQM	7.5	
05/16/2005		167.17	13.11		154.06										
08/17/2005		167.17	18.53		148.64										
11/18/2005		167.17	19.34		147.83										
02/07/2006	Р	167.17	11.64		155.53	65	< 0.50	< 0.50	1.4	2.3	< 0.50		SEQM	7.1	
5/19/2006		167.17	14.88		152.29										

		тос	Depth to	Product	Water Level			Concentra	ntions in (µ	g/L)					
Well and		Elevation	Water	Thickness	Elevation	GRO/			Ethyl-	Total		DO			
Sample Date	P/NP	(feet msl)	(feet bgs)	(feet)	(feet msl)	TPHg	Benzene	Toluene	Benzene	Xylenes	MTBE	(mg/L)	Lab	pН	Comments
MW-3 Cont.															
8/23/2006		167.17	19.43		147.74										
11/15/2006		167.17	19.22		147.95										
2/14/2007	Р	167.17	13.80		153.37	200	1.1	< 0.50	5.9	3.2	3.8	0.68	TAMC	7.52	
5/22/2007		167.17	16.80		150.37										
8/15/2007		167.17	19.87		147.30										
11/8/2007		167.17	19.27		147.90										
2/20/2008	Р	167.17	13.58		153.59	240	1.1	< 0.50	0.99	0.79	2.3	2.58	CEL	7.06	
5/7/2008		167.17	18.32		148.85										
MW-4															
7/9/1990		170.36													
12/21/1990		170.36								0.8					
3/7/1991		170.36	20.72		149.64		2.2	3.8	1.5	2.8					
4/1/1991		170.36	17.49		152.87										
6/27/1991		170.36					6.3	1.8	0.4	1					
9/27/1991		170.36													
12/18/1991		170.36													
7/3/1992		170.36	22.16		148.20	<50	<0.5	< 0.5	< 0.5	< 0.5					
10/5/1992		170.36	23.38		146.98	<50	<0.5	< 0.5	< 0.5	< 0.5					
1/13/1993		170.36	17.58		152.78	<50	< 0.5	< 0.5	< 0.5	< 0.5					i
4/23/1993		170.36	15.72		154.64	<50	< 0.5	< 0.5	< 0.5	< 0.5					i
7/12/1993		170.36	21.74		148.62	<50	< 0.5	< 0.5	< 0.5	< 0.5	<5.0				i
10/21/1993		170.36	23.84		146.52	<50	< 0.5	< 0.5	< 0.5	< 0.5	<5.0				i
1/21/1994		170.36	22.42		147.94	<50	<0.5	< 0.5	< 0.5	< 0.5	<5.0				i
4/20/1994		170.36	22.66		147.70	<50	< 0.5	< 0.5	< 0.5	< 0.5	<5.0	2.2			i
8/1/1994		170.36	23.01		147.35	<50	<0.5	< 0.5	< 0.5	< 0.5	<5.0	1.9			i
12/23/1994		170.36	17.03		153.33										
1/26/1995		170.36	17.42		152.94	<50	<0.5	< 0.5	< 0.5	<1		7.5			
6/8/1995		170.36	21.55		148.81										
8/22/1995		170.36	23.47		146.89	<50	< 0.50	<0.50	< 0.50	<1.0	<5.0	6.4			d
10/27/1995		170.36	24.50		145.86										

		тос	Depth to	Product	Water Level			Concentra	ntions in (µ	g/L)					
Well and	DAD	Elevation	Water	Thickness	Elevation	GRO/	D	<b>T</b> 1	Ethyl-	Total	MTDE	DO	<b>T</b> . 1		
Sample Date	P/NP	(feet msl)	(feet bgs)	(feet)	(feet msl)	TPHg	Benzene	Toluene	Benzene	Xylenes	MTBE	(mg/L)	Lab	рН	Comments
MW-4 Cont.															
1/25/1996		170.36	18.74		151.62	<50	< 0.50	< 0.50	< 0.50	<1.0	58				
4/19/1996		170.36	18.63		151.73										
7/23/1996		170.36	22.56		147.80										
11/11/1996		170.36	23.63		146.73	<50	<1.0	<1.0	<1.0	<1.0	34	8.2			
1/21/1997		170.36	16.59		153.77										
4/29/1997		170.36	21.43		148.93	<50	< 0.5	<1.0	<1.0	<1.0	<10	4.7			
8/21/1997		170.36	22.91		147.45										
11/5/1997		170.36	22.34		148.02	60	< 0.5	<1.0	<1.0	<1.0	76	4.9			
2/3/1998		170.36	12.26		158.10										
5/28/1998		170.36	18.50		151.86	70	< 0.5	<1.0	<1.0	<1.0	160	4.2			
12/30/1998		170.36	19.69		150.67										
2/2/1999		170.36	18.26		152.10	70	<1.0	<1.0	<1.0	<1.0	130				
5/10/1999		170.36	17.86		152.50										
8/24/1999		170.36	17.93		152.43										
11/3/1999		170.36	22.78		147.58										
3/1/2000		170.36	18.04		152.32	<50	< 0.5	0.67	< 0.5	0.7	110				
4/21/2000		170.36	17.36		153.00										
7/31/2000		170.36	17.83		152.53										
11/20/2000		170.36	18.91		151.45										
2/18/2001		170.36	17.72		152.64	88	< 0.5	< 0.5	< 0.5	< 0.5	97.3				
6/7/2001		170.36	20.23		150.13										
9/5/2001		170.36	22.76		147.60										
11/30/2001		170.36	21.30		149.06										
2/20/2002		170.36	19.32		151.04	76	<0.5	< 0.5	< 0.5	<1.0	81				
6/20/2002		170.36	20.71		149.65										
9/11/2002		170.36	22.22		148.14										
11/12/2002		170.36	22.22		148.14										
1/29/2003		170.36	19.80		150.56	100	<0.5	< 0.5	< 0.5	< 0.5	66				n
5/22/2003		170.36	19.35		151.01										
7/28/2003		170.36	22.18		148.18										р
11/18/2003		170.36	21.65		148.71										

		тос	Depth to	Product	Water Level			Concentra	ations in (µ	g/L)					
Well and	D/ND	Elevation	Water	Thickness	Elevation	GRO/	D	T.I	Ethyl-	Total V-1	MTDE	DO	Tab		Gammanta
Sample Date	P/NP	(leet msi)	(leet bgs)	(leet)	(leet msi)	IPHg	вепzепе	1 oluene	Benzene	Aylenes	MIBE	(mg/L)	Lab	рн	Comments
MW-4 Cont.															
02/23/2004	Р	170.36	17.53		152.83	75	< 0.50	< 0.50	< 0.50	< 0.50	65		SEQM	6.8	
05/04/2004		170.36	20.62		149.74										
08/04/2004		170.36	21.30		149.06										
11/10/2004		170.36	20.65		149.71										
02/15/2005	Р	170.36	18.91		151.45	<50	< 0.50	< 0.50	< 0.50	< 0.50	62		SEQM	7.6	
05/16/2005		170.36	17.34		153.02										
08/17/2005		170.36	21.31		149.05										
11/18/2005		170.36	21.67		148.69										
02/07/2006	Р	170.36	16.74		153.62	100	< 0.50	< 0.50	1.0	3.0	29		SEQM	6.8	
5/19/2006		170.36	18.22		152.14										
8/23/2006		170.36	20.95		149.41										
11/15/2006		170.36	22.21		148.15										
2/14/2007	Р	170.36	18.25		152.11	<50	< 0.50	< 0.50	< 0.50	< 0.50	61	0.95	TAMC	7.34	
5/22/2007		170.36	20.16		150.20										
8/15/2007		170.36	22.34		148.02										
11/8/2007		170.36	21.86		148.50										
2/20/2008	Р	170.36	17.74		152.62	<50	< 0.50	< 0.50	< 0.50	< 0.50	36	2.13	CEL	6.93	
5/7/2008		170.36	21.38		148.98										
MW-5															
7/9/1990		165.14				280	200	210	46	290					
12/21/1990		165.14				0.69	300	34	8.4	39					
3/7/1991		165.14	16.60		148.54		17	0.9	0.7	1.6					
4/1/1991		165.14	11.99		153.15	800	250	54	11	60					
6/27/1991		165.14				330	120	10	12	8					
9/27/1991		165.14				0.73	230	16	20	22					
12/18/1991		165.14													
7/3/1992		165.14	18.65		146.49	150	36	< 0.5	< 0.5	1.1					
10/5/1992		165.14	20.32		144.82	270	79	4	1.7	2.9					
1/13/1993		165.14	13.03		152.11	180	59	6	1.8	7.6					i
4/23/1993		165.14	13.51		151.63	8,700	440	96	35	136					i

		тос	Depth to	Product	Water Level		I	Concentra	tions in (µ	g/L)	1				
Well and Sample Date	P/NP	Elevation (feet msl)	Water (feet bgs)	Thickness (feet)	Elevation (feet msl)	GRO/ TPHa	Renzene	Toluono	Ethyl- Benzene	Total Xylenes	MTRF	DO (mg/L)	Lah	nH	Comments
	1/111	(reet list)	(Itel bgs)	(itet)	(reet mar)	11 llg	Delizene	Tolucite	Delizene	Ayienes	MIDL	(ing/L)	Lab	рп	Comments
MW-5 Cont.															
7/12/1993		165.14	18.06		147.08	250	57	2.9	2.1	6	<5.0				i
10/21/1993		165.14	20.41		144.73	210	82	1.5	< 0.5	1.4					i
1/21/1994		165.14	18.86		146.28	110	36	1.2	< 0.5	0.7	<5.0				i
4/20/1994		165.14	17.30		147.84	690	230	4.5	1.6	11	21.2	1.3			i
8/1/1994		165.14	17.53		147.61	170	44	1.6	0.9	2.7	<5.0	0.9			i
12/23/1994		165.14	11.63		153.51	630	180	1.9	0.66	1.9	7.81	1.4			i
1/26/1995		165.14	11.25		153.89	160	68	< 0.5	< 0.5	22		5.9			
6/8/1995		165.14				1,700	560	51	55	170					с
6/8/1995		165.14	16.80		148.34	2,000	630	58	61	180		6.5			
8/22/1995		165.14	19.02		146.12	3,700	1,100	18	27	59	<130	7.3			d
10/27/1995		165.14	20.94		144.20										
10/30/1995		165.14				6,500	2,200	55	180	270	<250	7.5			
1/25/1996		165.14				540	37	0.66	< 0.50	<1.0	<5.0				с
1/25/1996		165.14	13.30		151.84	590	37	0.7	< 0.50	<1.0	<5.0				
4/19/1996		165.14	13.63		151.51	1,500	470	38	49	210	<50	8.1			
7/23/1996		165.14	17.61		147.53	140	4.6	< 0.5	< 0.5	< 0.5	<10	8			
11/11/1996		165.14	18.70		146.44	140	40	<1.0	<1.0	<1.0	<10	7.9			
1/21/1997		165.14	11.63		153.51	730	300	<5.0	7.8	26	<50	5			
4/29/1997		165.14	16.74		148.40	340	530	<5.0	<5.0	<5.0	<50	4.8			
8/21/1997		165.14	18.26		146.88	<50	< 0.5	<1.0	<1.0	<1.0	<10	4.9			
11/5/1997		165.14	18.84		146.30	120	13	<1.0	<1.0	<1.0	<10	4.4			
2/3/1998		165.14	9.49		155.65	<50	< 0.50	<1.0	<1.0	<1.0	<10	4.3			
5/28/1998		165.14	13.57		151.57	4,900	1,500	34	180	311	<10	4.1			
12/30/1998		165.14	14.65		150.49										
2/2/1999		165.14	12.56		152.58	100	<1.0	<1.0	<1.0	<1.0	9.1				
5/10/1999		165.14	13.36		151.78										
8/24/1999		165.14	13.50		151.64										
11/3/1999		165.14	18.48		146.66										
3/1/2000		165.14	9.59		155.55	<50	< 0.5	0.58	< 0.5	0.54	2.9				
4/21/2000		165.14	13.52		151.62										
7/31/2000		165.14	14.04		151.10										

		тос	Depth to	Product	Water Level			Concentra	ntions in (µ	g/L)					
Well and		Elevation	Water	Thickness	Elevation	GRO/			Ethyl-	Total		DO			
Sample Date	P/NP	(feet msl)	(feet bgs)	(feet)	(feet msl)	TPHg	Benzene	Toluene	Benzene	Xylenes	MTBE	(mg/L)	Lab	pН	Comments
MW-5 Cont.															
11/20/2000		165.14	15.89		149.25										
2/18/2001		165.14	11.88		153.26	560	161	2.38	6.11	13	5.67				
6/7/2001		165.14	15.30		149.84										
9/5/2001		165.14	19.32		145.82										
11/30/2001		165.14	17.44		147.70										
2/20/2002		165.14	13.88		151.26	4,200	940	18.7	98.2	176	55.6				
6/20/2002		165.14	16.20		148.94										
9/11/2002		165.14	19.15		145.99										
11/12/2002		165.14	19.01		146.13	390	55	0.89	3.4	3.5	210				
1/29/2003		165.14	16.33		148.81	7,900	1,400	34	220	350	82				n
5/22/2003		165.14	14.35		150.79	9,900	2,300	91	400	690	<50				
7/28/2003		165.14	18.90		146.24	3,200	690	14	81	100	120				р
11/18/2003		165.14													Well inaccessible e, q
02/23/2004	Р	165.14	12.21		152.93	7,500	1,500	100	190	350	100		SEQM	6.7	
05/04/2004	Р	165.14	17.12		148.02	5,900	1,500	57	200	280	42		SEQM	6.6	
08/04/2004	Р	165.14	19.05		146.09	<2,500	<25	<25	<25	<25	390		SEQM	6.69	
11/10/2004	Р	165.14	16.95		148.19	870	80	<5.0	<5.0	<5.0	530		SEQM	7.5	
02/15/2005	Р	165.14	12.75		152.39	1,600	330	8.0	37	67	260		SEQM	7.2	
05/16/2005	Р	165.14	15.46		149.68	<500	<5.0	<5.0	<5.0	<5.0	370		SEQM	6.7	
08/17/2005	Р	165.14	17.00		148.14	7,000	1,000	17	110	130	51		SEQM	6.6	
11/18/2005	Р	165.14	18.33		146.81	1,900	91	<5.0	33	29	340		SEQM	7.3	
02/07/2006	Р	165.14	10.27		154.87	2,100	590	9.6	86	110	200		SEQM	6.7	
5/19/2006	Р	165.14	13.08		152.06	3,200	720	9.7	150	170	44		SEQM	6.8	
8/23/2006	Р	165.14	17.02		148.12	1,400	69	<5.0	20	24	230		TAMC	7.11	
11/15/2006	Р	165.14	18.30		146.84	1,100	24	<2.5	10	8.6	490	0.85	TAMC	6.82	
2/14/2007	Р	165.14	13.16		151.98	680	110	<2.5	16	11	420	2.54	TAMC	7.24	
5/22/2007	Р	165.14	15.42		149.72	2,800	660	8.8	74	100	26	1.41	TAMC	7.03	
8/15/2007	Р	165.14	18.80		146.34	2,800	50	<10	26	29	280	3.81	TAMC	7.14	
11/8/2007	Р	165.14	18.55	SHEEN	146.59	3,800	77	<2.5	46	35	270	1.08	TAMC	7.23	t
2/20/2008	Р	165.14	12.21		152.93	2,500	530	<5.0	75	62	43	2.01	CEL	6.84	
5/7/2008	Р	165.14	16.91		148.23	6,700	1,800	29	270	360	30	2.45	CEL	6.87	t

		тос	Depth to	Product	Water Level		1	Concentra	tions in (µ	g/L)					
Well and Sample Date	P/NP	Elevation (feet msl)	Water (feet bgs)	Thickness (feet)	Elevation (feet msl)	GRO/ TPHg	Benzene	Toluene	Ethyl- Benzene	Total Xylenes	MTBE	DO (mg/L)	Lab	pН	Comments
MW-5														-	
MW-6															
7/9/1990		165.40													
12/21/1990		165.40				0.17	2.6	7	4.9	26					
3/7/1991		165.40													e
4/1/1991		165.40	11.79		153.61										
6/27/1991		165.40													e
9/27/1991		165.40													e
12/18/1991		165.40					1.3	22		2.7					
7/3/1992		165.40	17.77		147.63	<50	< 0.5	<0.5	< 0.5	<0.5					
10/5/1992		165.40	19.46		145.94	<50	< 0.5	< 0.5	< 0.5	< 0.5					
1/13/1993		165.40	11.34		154.06	<50	< 0.5	<0.5	< 0.5	<0.5					i
4/23/1993		165.40	12.92		152.48	<50	< 0.5	< 0.5	< 0.5	< 0.5					i
7/12/1993		165.40	17.36		148.04	<50	< 0.5	< 0.5	< 0.5	0.7	<5.0				i
10/21/1993		165.40	19.98		145.42	<50	< 0.5	< 0.5	< 0.5	< 0.5					i
1/21/1994		165.40	18.10		147.30	<50	< 0.5	<0.5	< 0.5	<0.5	<5.0				i
4/20/1994		165.40	18.68		146.72	<50	< 0.5	< 0.5	< 0.5	< 0.5	17.4	2			i
8/1/1994		165.40	18.90		146.50	<50	< 0.5	< 0.5	< 0.5	<0.5	8.66	1.5			i
12/23/1994		165.40	12.94		152.46										
1/26/1995		165.40	10.46		154.94	<50	< 0.5	< 0.5	< 0.5	<1		7.3			
6/8/1995		165.40	16.84		148.56										
8/22/1995		165.40	19.48		145.92	<50	< 0.50	< 0.50	< 0.50	<1.0	< 5.0	6.7			d
10/27/1995		165.40	20.39		145.01										
1/25/1996		165.40	12.24		153.16	<50	< 0.50	<0.50	< 0.50	<1.0	9.9				
4/19/1996		165.40	13.90		151.50										
7/23/1996		165.40	17.83		147.57										
11/11/1996		165.40	18.90		146.50	<50	< 0.5	<1.0	<1.0	<1.0	<10	7.7			
1/21/1997		165.40	11.97		153.43										
4/29/1997		165.40	17.04		148.36	<50	< 0.5	<1.0	<1.0	<1.0	<10	4.5			
8/21/1997		165.40	18.58		146.82										
11/5/1997		165.40	19.17		146.23	70	< 0.5	<1.0	<1.0	<1.0	85	4.3			

		тос	Depth to	Product	Water Level			Concentra	ations in (µ	g/L)					
Well and		Elevation	Water	Thickness	Elevation	GRO/			Ethyl-	Total		DO			
Sample Date	P/NP	(feet msl)	(feet bgs)	(feet)	(feet msl)	TPHg	Benzene	Toluene	Benzene	Xylenes	MTBE	(mg/L)	Lab	pН	Comments
MW-6 Cont.															
2/3/1998		165.40	9.87		155.53										
5/28/1998		165.40	13.38		152.02	<50	< 0.5	<1.0	<1.0	<1.0	<10	3.7			
12/30/1998		165.40	14.45		150.95										
2/2/1999		165.40	18.29		147.11										
5/10/1999		165.40	17.49		147.91										
8/24/1999		165.40	17.61		147.79										
11/3/1999		165.40	16.26		149.14										
3/1/2000		165.40	17.43		147.97										
4/21/2000		165.40	13.32		152.08										
7/31/2000		165.40	13.46		151.94										
11/20/2000		165.40	14.78		150.62										
2/18/2001		165.40	11.33		154.07										
6/7/2001		165.40	16.36		149.04										
9/5/2001		165.40	18.61		146.79										
11/30/2001		165.40	15.20		150.20										
2/20/2002		165.40	12.74		152.66										
6/20/2002		165.40	16.68		148.72										
9/11/2002		165.40	18.38		147.02										
11/12/2002		165.40	18.78		146.62										
1/29/2003		165.40	14.45		150.95										n
5/22/2003		165.40	14.36		151.04										
7/28/2003		165.40	18.43		146.97										р
11/18/2003		165.40	17.48		147.92										
02/23/2004		165.40	11.54		153.86										
05/04/2004		165.40	16.58		148.82										
08/04/2004		165.40	18.12		147.28										
11/10/2004		165.40	15.75		149.65										
02/15/2005		165.40	12.50		152.90										
05/16/2005	Р	165.40	11.51		153.89	<50	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50		SEQM	7.0	
08/17/2005		165.40	16.85		148.55										
11/18/2005		165.40													e

		тос	Depth to	Product	Water Level			Concentra	ations in (µ	g/L)					
Well and		Elevation	Water	Thickness	Elevation	GRO/	_		Ethyl-	Total		DO			_
Sample Date	P/NP	(feet msl)	(feet bgs)	(feet)	(feet msl)	TPHg	Benzene	Toluene	Benzene	Xylenes	MTBE	(mg/L)	Lab	рН	Comments
MW-6 Cont.															
02/07/2006	Р	165.40	9.93		155.47	<50	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50		SEQM	7.1	
5/19/2006		165.40													е
8/23/2006		165.40	16.35		149.05										
11/15/2006		165.40	17.42		147.98										
2/14/2007	Р	165.40	12.03		153.37	<50	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50	1.07	TAMC	7.73	
5/22/2007		165.40	15.11		150.29										
8/15/2007		165.40	18.08		147.32										
11/8/2007		165.40	17.79		147.61										
2/20/2008	Р	165.40	11.81		153.59	<50	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50	1.29	CEL	7.10	
5/7/2008		165.40	16.75		148.65										
MW-7															
7/9/1990		167.61													
12/21/1990		167.61													
3/7/1991		167.61	19.04		148.57			0.4	0.3	2.4					
4/1/1991		167.61	15.18		152.43										
6/27/1991		167.61				70	17	4	0.8	2.2					
9/27/1991		167.61					0.4			0.4					
12/18/1991		167.61					0.7	2.9	0.8	3.3					
7/3/1992		167.61	20.28		147.33	<50	< 0.5	< 0.5	< 0.5	< 0.5					
10/5/1992		167.61	21.56		146.05	<50	< 0.5	< 0.5	< 0.5	1.5					
1/13/1993		167.61	15.41		152.20	<50	< 0.5	< 0.5	< 0.5	< 0.5					i
4/23/1993		167.61	15.84		151.77	<50	< 0.5	< 0.5	< 0.5	< 0.5					i
7/12/1993		167.61	19.84		147.77	<50	< 0.5	< 0.5	< 0.5	< 0.5	<5.0				i
10/21/1993		167.61	21.61		146.00	<50	< 0.5	< 0.5	< 0.5	< 0.5					i
1/21/1994		167.61				<50	< 0.5	< 0.5	< 0.5	< 0.5					с
1/21/1994		167.61	20.49		147.12	<50	< 0.5	< 0.5	< 0.5	< 0.5	<5.0				i
4/20/1994		167.61	20.54		147.07	<50	<0.5	<0.5	<0.5	<0.5	<5.0	1.5			i
8/1/1994		167.61	20.99		146.62	<50	0.7	< 0.5	< 0.5	< 0.5	<5.0	1.9			i
12/23/1994		167.61	15.00		152.61										
1/26/1995		167.61	14.69		152.92	<50	< 0.5	< 0.5	< 0.5	<1		7			

		тос	Depth to	Product	Water Level			Concentra	ations in (µ						
Well and		Elevation	Water	Thickness	Elevation	GRO/			Ethyl-	Total		DO			
Sample Date	P/NP	(feet msl)	(feet bgs)	(feet)	(feet msl)	TPHg	Benzene	Toluene	Benzene	Xylenes	MTBE	(mg/L)	Lab	pН	Comments
MW-7 Cont.															
6/8/1995		167.61	19.87		147.74										
8/22/1995		167.61	21.49		146.12	<50	< 0.50	< 0.50	< 0.50	<1.0	<5.0	6.4			d
10/27/1995		167.61	22.53		145.08										
1/25/1996		167.61	17.21		150.40	<50	< 0.50	< 0.50	< 0.50	<1.0	<5.0				
4/19/1996		167.61	17.09		150.52										
7/23/1996		167.61	21.02		146.59										
11/11/1996		167.61	22.03		145.58	<50	< 0.5	<1.0	<1.0	<1.0	<10	7.8			
1/21/1997		167.61	15.06		152.55										
4/29/1997		167.61	20.11		147.50	<50	< 0.5	<1.0	<1.0	<1.0	<10	4.4			
8/21/1997		167.61	21.59		146.02										
11/5/1997		167.61	20.05		147.56	<50	< 0.5	<1.0	<1.0	<1.0	<10	4.4			
2/3/1998		167.61	9.97		157.64										
5/28/1998		167.61	13.52		154.09	<50	< 0.5	<1.0	<1.0	<1.0	<10	4.3			
12/30/1998		167.61	18.33		149.28										
2/2/1999		167.61	12.33		155.28										
5/10/1999		167.61	13.52		154.09										
8/24/1999		167.61	14.01		153.60										
11/3/1999		167.61	19.91		147.70										
3/1/2000		167.61	19.89		147.72										
4/21/2000		167.61	17.94		149.67										
7/31/2000		167.61	17.33		150.28										
11/20/2000		167.61	18.41		149.20										
2/18/2001		167.61	15.13		152.48										
6/7/2001		167.61	18.75		148.86										
9/5/2001		167.61	20.48		147.13										
11/30/2001		167.61	20.11		147.50										
2/20/2002		167.61	18.40		149.21										
6/20/2002		167.61	18.62		148.99										
9/11/2002		167.61	20.05		147.56										
11/12/2002		167.61	21.13		146.48										n
1/29/2003		167.61	19.10		148.51										

		тос	Depth to	Product	Water Level			Concentra	ntions in (µ	g/L)					
Well and		Elevation	Water	Thickness	Elevation	GRO/			Ethyl-	Total		DO			
Sample Date	P/NP	(feet msl)	(feet bgs)	(feet)	(feet msl)	TPHg	Benzene	Toluene	Benzene	Xylenes	MTBE	(mg/L)	Lab	pН	Comments
MW-7 Cont.															
5/22/2003		167.61	18.83		148.78										
7/28/2003		167.61	19.88		147.73										р
11/18/2003		168.08	20.50		147.58										
11/18/2003		167.61	20.50		147.11										S
02/23/2004		168.08	15.92		152.16										
05/04/2004		168.08	18.86		149.22										
08/04/2004		168.08	19.10		148.98										
11/10/2004		168.08	20.25		147.83										
02/15/2005		168.08	16.37		151.71										
05/16/2005		168.08													е
08/17/2005		168.08	19.74		148.34										
11/18/2005		168.08	20.82		147.26										
02/07/2006	Р	168.08	14.26		153.82	<500	<5.0	<5.0	<5.0	<5.0	270		SEQM	7.3	
5/19/2006		168.08	16.51		151.57										
8/23/2006		168.08	20.30		147.78										
11/15/2006		168.08	20.85		147.23										
2/14/2007	Р	168.08	16.57		151.51	520	<5.0	<5.0	<5.0	<5.0	740	3.08	TAMC	7.30	v
5/22/2007		168.08	18.40		149.68										
8/15/2007		168.08	20.85		147.23										
11/8/2007		168.08	20.41		147.67										
2/20/2008	Р	168.08	15.90		152.18	<50	< 0.50	< 0.50	< 0.50	< 0.50	700	4.34	CEL	7.09	
5/7/2008		168.08	19.41		148.67										
MW-8															
3/7/1991		165.74	16.72		149.02	2.7	780	450	64	310					
4/1/1991		165.74	12.54		153.20	15,000	3,600	2,600	410	1,900					
6/27/1991		165.74				12,000	3,400	1,100	240	750					
9/27/1991		165.74				41	5,700	5,200	1,100	4,300					
12/18/1991		165.74				3.2	990	150	120	250					
7/3/1992		165.74	18.78		146.96	72,000	19,000	32,000	3,000	15,000					
10/5/1992		165.74	20.48		145.26										

		тос	Depth to	Product	Water Level Concentrations in (µg/L)										
Well and Sample Date	P/NP	Elevation (feet msl)	Water (feet bgs)	Thickness (feet)	Elevation (feet msl)	GRO/ TPHg	Benzene	Toluene	Ethyl- Benzene	Total Xylenes	MTBE	DO (mg/L)	Lab	pН	Comments
MW-8 Cont.		~ /	× 87	~ /	· · · ·	0				•				•	
1/13/1993		165.74	12.87		152.87										
4/23/1993		165.74	13.90		151.84										t
7/12/1993		165.74	18.30		147.44										t
10/21/1993		165.74	21.91		142.88										
10/2/93-12/9/98		165.74		0.12											
1/21/1994		165.74	19.12		146.62										
4/20/1994		165.74	19.28		146.46	26,000	1,700	4,100	960	4,000	632	1.1			i
8/1/1994		165.74													
12/23/1994		165.74	13.81		151.93										
1/26/1995		165.74													
6/8/1995		165.74	17.82		147.92										
8/22/1995		165.74	19.41		146.33										
10/27/1995		165.74	20.47		145.27										
1/25/1996		165.74	13.35		152.39										
4/19/1996		165.74	14.40		151.34										
7/23/1996		165.74	18.35		147.39										
11/11/1996		165.74	19.41		146.33										
1/21/1997		165.74	12.29		153.45										
4/29/1997		165.74													e
8/21/1997		165.74	19.61		146.13	240,000	1,100	9,300	4,100	31,100	<1000	5.2			
11/5/1997		165.74	19.45		146.29	57,000	790	2,700	2,300	15,200	<1000	5			
2/3/1998		165.74	9.33		156.41										
2/4/1998		165.74				94,000	570	1,500	2,100	15,200	<2500	5.5			
5/28/1998		165.74													е
12/30/1998		165.74	15.48		150.26	120,000	460	2,300	2,200	15,000	150				
2/2/1999		165.74	18.29		147.45	82,000	450	2,200	3,700	26,000	<500				
5/10/1999		165.74	15.62		150.12	28,000	740	1,800	1,100	5,800	<25				
8/24/1999		165.74	18.41		147.33	75,000	530	1,400	3,300	21,000	150				
11/3/1999		165.74	18.71		147.03	70,000	600	1,300	3,600	20,500	750				
3/1/2000		165.74	19.37		146.37	27,000	1,600	1,200	2,600	6,600	120				
4/21/2000		165.74													e

		тос	Depth to	Product     Water Level     Concentrations in (µg/L)											
Well and	D/ND	Elevation	Water	Thickness	Elevation	GRO/	Dongono	Toluono	Ethyl-	Total Vulence	MTDE	DO (mg/L)	Lah	~II	Commonta
Sample Date	<b>F</b> /IN <b>F</b>	(leet liist)	(leet bgs)	(leet)	(leet liisi)	IFng	Benzene	Toluelle	Belizelle	Aylenes	MIDE	(Ing/L)	LaD	рп	Comments
MW-8 Cont.															
7/31/2000		165.74													е
11/20/2000		165.74	17.42		148.32	1,300,000	1,400	1,700	20,000	16,000	5,700				
2/18/2001		165.74													e
6/7/2001		165.74													e
9/5/2001		165.74	21.45	0.04	144.25										j
11/30/2001		165.74	18.31		147.43										h
12/6/2001		165.74													е
2/20/2002		165.74	14.02		151.72	20,000	163	114	403	3,810	80.4				
6/20/2002		165.74	17.56		148.18	28,000	466	141	962	5,850	2,520				
9/11/2002		165.74	19.45		146.29	190,000	1,500	670	4,500	23,000	1,200				
11/12/2002		165.74	19.15		146.59	420	6.4	2.9	16	110	31				t
1/29/2003		165.74	15.02		150.72	200,000	810	<500	2,000	11,000	<500				n
5/22/2003		165.74	15.07		150.67										t
6/24/2003		165.74	17.95		147.79	43,000	860	300	2,100	9,600	46				
7/28/2003		165.74	19.45		146.29	62,000	690	230	1,800	15,000	2,100				
8/12/2003		165.74	19.40	< 0.01	146.34										o,t
9/12/2003		165.74	19.34		146.40										0
10/3/2003		165.74		< 0.01											
11/18/2003	Р	165.74	18.80	< 0.01	146.94	8,800	500	37	530	930	1,700		SEQM		o,p
12/31/2003		165.74		< 0.01											
2/2/2004		165.74		< 0.01											
02/23/2004	Р	165.74	12.82	< 0.01	152.92	32,000	840	360	1,000	7,100	110		SEQM	6.6	t
3/18/2004		165.74		< 0.01											
4/13/2004		165.74		< 0.01											
05/04/2004	Р	165.74	18.87	< 0.01	146.87	42,000	570	230	1,700	8,400	2,000		SEQM	7.0	t
6/2/2004		165.74		< 0.01											
08/04/2004		165.74	19.37	0.05	146.41										
09/22/2004	NP	165.74	19.60		146.14										
11/10/2004	Р	165.74	16.58		149.16	11,000	790	61	1,000	830	74		SEQM	7.3	t
02/15/2005	Р	165.74	12.85		152.89	38,000	1,300	390	2,300	7,900	<50		SEQM	7.2	
05/16/2005	Р	165.74	12.22		153.52	31,000	1,000	360	2,500	7,500	<50		SEQM	6.5	

		тос	Depth to	Product	duct Water Level Concentrations in (µg/L)										
Well and Sample Date	P/NP	Elevation (feet msl)	Water (feet bgs)	Thickness (feet)	Elevation (feet msl)	GRO/ TPHg	Ronzono	Toluene	Ethyl- Benzene	Total Xylenes	MTRF	DO (mg/L)	Lah	nH	Comments
	1/111	(reet hist)	(Itel bgs)	(itet)	(reet msi)	IIIg	Delizene	Totuche	Delizene	Ayienes	MIDE	(Ing/L)	Lab	рп	Comments
MW-8 Cont.															
08/17/2005	Р	165.74	17.80		147.94	60,000	540	240	2,500	8,600	<50		SEQM	6.7	
11/18/2005	Р	165.74	21.02		144.72	33,000	340	120	1,400	4,900	140		SEQM	6.9	
02/07/2006	Р	165.74	10.73		155.01	5,700	94	27	260	820	7.5		SEQM	6.6	
5/19/2006	Р	165.74	13.89		151.85	40,000	1,100	320	2,900	6,000	<25		SEQM	6.6	t
8/23/2006	Р	165.74	18.85		146.89	21,000	520	150	1,800	6,300	82		TAMC	7.35	
11/15/2006	Р	165.74	18.75		146.99	3,300	81	<25	130	430	110	0.81	TAMC	6.91	
2/14/2007	Р	165.74	13.45	SHEEN	152.29	9,300	320	<25	360	710	82	1.89	TAMC	7.13	t
5/22/2007	Р	165.74	15.92	SHEEN	149.82	17,000	370	51	760	1,600	11	1.05	TAMC	6.99	t
8/15/2007	Р	165.74	19.11	SHEEN	146.63	17,000	170	44	1,000	2,700	28	3.93	TAMC	7.08	
11/8/2007	Р	165.74	18.46	SHEEN	147.28	24,000	150	43	1,100	3,200	27	1.29	TAMC	7.14	t
2/20/2008															e
5/7/2008															е
MW-9															
3/7/1991		166.20	16.79		149.41	7.1	220	4	2.4	2,400					
4/1/1991		166.20	12.89		153.31	12,000	2,000	2,600	360	1,600					
6/27/1991		166.20				3,600	520	400	85	310					
9/27/1991		166.20				3.2	720	150	50	180					
12/18/1991		166.20					2.5	1.1	0.3	5.8					
7/3/1992		166.20	18.89		147.31	5,700	17,000	840	230	800					
10/5/1992		166.20	20.52		145.68	1,400	440	17	14	100					
1/13/1993		166.20				11,000	1,200	1,600	330	1,300					c,i
1/13/1993		166.20	12.92		153.28	11,000	1,200	1,700	340	1,400					i
4/23/1993		166.20	14.08		152.12	24,000	2,800	4,500	730	3,400					i
7/12/1993		166.20				10,000	1,200	900	310	1,200					с
7/12/1993		166.20	18.44		147.76	13,000	1,400	1,100	360	1,400	20.8				i
10/21/1993		166.20	21.81		143.50										
11/2/93-4/29/97		166.20		0.10											
1/21/1994		166.20	19.28		146.92										
4/20/1994		166.20	19.72		146.48	43,000	2,800	6,800	1,300	7,900	768	1.7			i
4/20/1994		166.20				45,000	2,700	6,800	1,200	8,200	740				c,d

		тос	Depth to	Product	Water Level	Vater Level Concentrations in (μg/L)									
Well and		Elevation	Water	Thickness	Elevation	GRO/			Ethyl-	Total		DO			<i>a</i>
Sample Date	P/NP	(feet msl)	(feet bgs)	(feet)	(feet msl)	TPHg	Benzene	Toluene	Benzene	Xylenes	MTBE	(mg/L)	Lab	рН	Comments
MW-9 Cont.															
8/1/1994		166.20	20.18		146.02										
12/23/1994		166.20	14.22		151.98										
1/26/1995		166.20	11.85		154.35										
6/8/1995		166.20	18.33		147.87										
8/22/1995		166.20	19.95		146.25										
10/27/1995		166.20	20.88		145.32										
1/25/1996		166.20	13.84		152.36										
4/19/1996		166.20													e
7/23/1996		166.20	18.84		147.36										
11/11/1996		166.20	19.91		146.29										
1/21/1997		166.20	12.93		153.27										
4/29/1997		166.20	18.03	0.1	148.17										t
4/30/1997		166.20				78,000	1,900	3,600	3,100	20,600	<5000	5.5			
8/21/1997		166.20	19.56		146.64	110,000	2,100	3,400	2,300	18,800	<500	5.1			
11/5/1997		166.20	20.59	0.01	145.60	59,000	1,400	1,700	2,200	17,000	<500	4.5			
2/3/1998		166.20	10.56		155.64	55,000	490	1,200	1,400	10,200	<1000	4.9			
5/28/1998		166.20	14.21		151.99	41,000	250	1,200	1,500	11,400	<250	3.8			
5/28/1998		166.20				53,000	290	830	1,400	10,500	<500				с
12/30/1998		166.20	15.61		150.59	83,000	860	1,300	2,400	21,000	180				
2/2/1999		166.20	12.33		153.87	75,000	530	960	1,900	17,000	<50				
5/10/1999		166.20	15.67		150.53	22,000	600	1,500	1,100	4,400	72				
8/24/1999		166.20	19.10		147.10	85,000	850	1,300	1,700	20,000	<250				
11/3/1999		166.20	19.58		146.62	72,000	700	780	1,900	19,000	<5.0				
3/1/2000		166.20	13.19		153.01	34,000	78	490	1,100	8,200	63				
4/21/2000		166.20	14.29		151.91	55,000	260	920	1,500	16,000	<5.0				
7/31/2000		166.20	15.01		151.19	1,200,000	1,500	6,300	15,000	120,000	1,600				
11/20/2000		166.20	18.23		147.97	320,000	3,500	19,000	5,000	40,000	3,900				
2/18/2001		166.20	13.14		153.06	32,000	290	417	1,180	10,400	121				
6/7/2001		166.20	17.41		148.79	96,000	421	704	2,330	17,300	223				
9/5/2001		166.20	20.56		145.64	39,000	445	323	1,240	8,940	310				
11/30/2001		166.20	17.42		148.78	60,000	310	586	1,890	14,200	285				

		тос	Depth to	Product	Water Level Concentrations in (µg/L)   File_time File_time										
Well and Sample Date	P/NP	Elevation (feet msl)	Water (feet bgs)	Thickness (feet)	Elevation (feet msl)	GRO/ TPHg	Benzene	Toluene	Ethyl- Benzene	Total Xvlenes	MTBE	DO (mg/L)	Lab	рH	Comments
MW-9 Cont		()	(8-)	()	()	8						(8,)		<b>F</b>	
Wiw-9 Cont.															
2/20/2002		166.20	13.87		152.33	14,000	64	122	897	2,650	293				
6/20/2002		166.20	18.22		147.98	29,000	307	168	1,100	5,670	208				
9/11/2002		166.20	20.27		145.93	230,000	1,400	680	3,600	23,000	<2500				
11/12/2002		166.20	19.40		146.80	840	5.8	3.6	28	160	21				t
1/29/2003		166.20	14.30	0.1	151.80										j,n
5/22/2003		166.20	15.16		151.04	23,000	260	<50	1,000	2,900	<50				t
6/24/2003		166.20													e
7/28/2003		166.20	19.55	< 0.01	146.65	1,500,000	<500	<500	9,800	79,000	<500				
8/12/2003		166.20	19.60	< 0.01	146.60										o,t
9/12/2003		166.20	19.60	< 0.01	146.60										o,t
11/18/2003	Р	166.20	18.98	< 0.01	147.22	19,000	250	18	690	2,400	45		SEQM	6.8	o,p
12/31/2003		166.20		< 0.01											
2/2/2004		166.20		< 0.01											
02/23/2004	Р	166.20	13.91	< 0.01	152.29	91,000	<250	440	2,200	13,000	<250		SEQM	6.8	t
3/18/2004		166.20		< 0.01											
4/13/2004		166.20		< 0.01											
05/04/2004	Р	166.20	18.11	< 0.01	148.09	39,000	230	44	1,100	4,200	<25		SEQM	6.9	t
6/2/2004		166.20		< 0.01											
08/04/2004		166.20	18.90	0.03	147.32										
09/22/2004	NP	166.20	19.69		146.51										
11/10/2004	NP	166.20	16.95		149.25	31,000	300	<50	1,100	3,800	<50		SEQM	7.3	t
02/15/2005	Р	166.20	12.95		153.25	19,000	200	<50	720	2,000	<50		SEQM	7.3	t
05/16/2005	Р	166.20	12.53		153.67	17,000	99	15	770	2,500	<10		SEQM	6.7	
08/17/2005	Р	166.20	18.03		148.17	28,000	160	26	1,000	2,700	<12		SEQM	6.8	
11/18/2005	Р	166.20	19.04		147.16	12,000	98	<5.0	410	510	19		SEQM	7.1	
02/07/2006	Р	166.20	10.95	SHEEN	155.25	18,000	110	8.7	770	1,500	<5.0		SEQM	6.9	t
5/19/2006		166.20													e
8/23/2006	Р	166.20	18.91		147.29	28,000	84	<50	1,600	6,200	<50		TAMC	7.3	
11/15/2006	Р	166.20	18.60		147.60	8,200	44	<25	190	370	26	0.92	TAMC	6.88	
2/14/2007	Р	166.20	13.30		152.90	20,000	64	<25	720	2,000	<25	0.87	TAMC	7.17	t
5/22/2007	Р	166.20	16.14	SHEEN	150.06	16,000	80	<25	460	1,200	<25	0.81	TAMC	7.08	t

		тос	Depth to	Product	Water Level			Concentra	ntions in (µ	g/L)					
Well and Sample Date	P/NP	Elevation (feet msl)	Water (feet bgs)	Thickness (feet)	Elevation (feet msl)	GRO/ TPHg	Benzene	Toluene	Ethyl- Benzene	Total Xvlenes	MTBE	DO (mg/L)	Lab	рН	Comments
MW-9 Cont.		~ /	× 87		× ,	0									
in the second															
8/15/2007	Р	166.20	19.31	SHEEN	146.89	5,900	27	<2.5	59	170	27	2.57	TAMC	6.98	
11/8/2007	Р	166.20	18.70		147.50	6,100	29	<5.0	98	250	52	1.24	TAMC	7.47	
2/20/2008		166.20	12.79	0.03	153.43										b, j
5/7/2008		166.20	17.68	0.03	148.54										b, j
<b>MW-10</b>															
3/7/1991		167.01	18.09		148.92	1.6	120	190	32	230					
4/1/1991		167.01	13.92		153.09										
6/27/1991		167.01				12,000	7,300	500	150	300					
9/27/1991		167.01				57	12,000	7,200	1,400	4,600					
12/18/1991		167.01				5.3	2,500	120	36	79					
7/3/1992		167.01	19.92		147.09	8,600	5,100	1,300	180	690					
10/5/1992		167.01	21.92		145.09										
1/13/1993		167.01	14.43		152.58										
4/23/1993		167.01	15.26		151.75										
7/12/1993		167.01	19.78		147.23										
10/21/1993		167.01	22.90		144.11										
1/21/1994		167.01	20.25		146.76										
4/20/1994		167.01	20.74		146.27	100,000	12,000	24,000	2,400	14,000	1,577	1			d,i
8/1/1994		167.01	22.00		145.01										
12/23/1994		167.01	16.08		150.93										
1/26/1995		167.01	13.68		153.33										
6/8/1995		167.01	19.08		147.93										
8/22/1995		167.01	20.73		146.28										
10/27/1995		167.01	21.69		145.32										
1/25/1996		167.01	15.05		151.96										
4/19/1996		167.01	16.26		150.75										
7/23/1996		167.01	20.18		146.83										
9/4/1996		167.01		0.76											
11/11/1996		167.01	21.20		145.81										
1/21/1997		167.01	13.66		153.35										

		тос	Depth to	Product	Water Level	Concentrations in (µg/L)									
Well and		Elevation	Water	Thickness	Elevation	GRO/			Ethyl-	Total		DO			
Sample Date	P/NP	(feet msl)	(feet bgs)	(feet)	(feet msl)	TPHg	Benzene	Toluene	Benzene	Xylenes	MTBE	(mg/L)	Lab	pН	Comments
MW-10 Cont.															
4/29/1997		167.01	18.71		148.30										
4/30/1997		167.01				170,000	9,700	38,000	4,700	30,500	<5000	5.6			
8/21/1997		167.01	20.19		146.82	170,000	9,500	35,000	4,300	27,100	<5000	5.3			
11/5/1997		167.01	20.52		146.49	80,000	3,800	12,000	2,700	15,700	<500	4.4			
12/2/1997		167.01		0.03											
2/3/1998		167.01	10.62		156.39										
2/4/1998		167.01				72,000	500	1,300	1,700	12,000	<1000	5.1			
5/28/1998		167.01	15.46		151.55	220,000	3,200	24,000	5,200	43,000	<1000	4.8			
12/30/1998		167.01	16.65		150.36	110,000	3,500	14,000	5,800	50,000	<50				
2/2/1999		167.01	14.58		152.43	74,000	1,000	2,800	1,000	26,000	860				
5/10/1999		167.01	15.72		151.29	81,000	2,800	2,800	3,000	17,000	220				
8/24/1999		167.01	19.85		147.16	54,000	3,500	3,800	1,500	9,100	<250				
11/3/1999		167.01	20.00		147.01	30,000	3,000	3,500	1,200	5,000	31				
3/1/2000		167.01	14.62		152.39	62,000	320	1,200	1,100	26,000	4,400				
4/21/2000		167.01	15.46		151.55	88,000	2,700	7,400	3,700	35,000	2,400				
7/31/2000		167.01													e
11/20/2000		167.01	18.74		148.27	78,000	3,800	5,500	2,800	13,000	450				
2/18/2001		167.01	14.10		152.91	39,000	1,050	1,160	1,550	14,700	4,180				
6/7/2001		167.01	18.78		148.23	76,000	2,460	2,840	3,330	20,700	635				
9/5/2001		167.01	21.40	0.01	145.60	25,000	2,510	2,070	1,090	4,540	189				
11/30/2001		167.01	18.50		148.51	100,000	2,480	5,720	3,890	22,800	325				
2/20/2002		167.01	14.39		152.62	49,000	2,170	3,070	1,960	12,300	1,090				
6/20/2002		167.01	18.80		148.21	44,000	2,040	3,050	1,690	8,430	224				
9/11/2002		167.01	20.52		146.49	28,000	1,200	2,700	1,400	6,800	<250				
11/12/2002		167.01	20.37	0.07	146.57										j
1/29/2003		167.01	16.33	0.03	150.65										j,n
5/22/2003		167.01	16.32		150.69	13,000	2,100	850	630	1,600	300				t
6/24/2003		167.01	18.73	0.04	148.24										0
7/28/2003		167.01	20.39	0.04	146.58										j
8/12/2003		167.01	20.43	< 0.01	146.58										o,t
9/12/2003		167.01	20.41		146.60										0

		тос	Depth to	Product	Water Level	cl Concentrations in (μg/L)									
Well and		Elevation	Water	Thickness	Elevation	GRO/			Ethyl-	Total		DO			
Sample Date	P/NP	(feet msl)	(feet bgs)	(feet)	(feet msl)	TPHg	Benzene	Toluene	Benzene	Xylenes	MTBE	(mg/L)	Lab	pН	Comments
MW-10 Cont.															
10/3/2003		167.01		< 0.01											
11/18/2003	Р	167.01	19.55	< 0.01	147.46	9,900	2,200	530	320	860	<50		SEQM	6.8	o,p
12/31/2003		167.01		< 0.01											
2/2/2004		167.01		< 0.01											
02/23/2004	Р	167.01	15.45	< 0.01	151.56	46,000	1,900	2,000	1,800	9,000	180		SEQM	6.7	t
3/18/2004		167.01		< 0.01											
4/13/2004		167.01		< 0.01											
05/04/2004	Р	167.01	18.81	< 0.01	148.20	35,000	3,100	3,600	1,400	5,600	<25		SEQM	7.1	t
6/2/2004		167.01		< 0.01											
7/2/2004		167.01		< 0.01											
08/04/2004		167.01	18.90		148.11										
09/22/2004	NP	167.01	20.60		146.41										
11/10/2004	Р	167.01	17.95		149.06	9,800	470	91	450	1,700	230		SEQM	7.3	t
01/13/2005		167.01	12.21		154.80										
02/15/2005	Р	167.01	14.19		152.82	30,000	510	330	1,800	7,200	77		SEQM	7.2	
05/16/2005	Р	167.01	13.85		153.16	37,000	540	730	2,100	9,200	<50		SEQM	6.7	
08/17/2005	Р	167.01	19.01		148.00	15,000	1,100	420	1,200	4,100	<50		SEQM	6.7	
11/18/2005	Р	167.01	19.95		147.06	12,000	1,200	240	550	1,300	16		SEQM	6.8	
02/07/2006	Р	167.01	12.28	SHEEN	154.73	22,000	340	580	1,300	4,500	73		SEQM	6.8	t
5/19/2006	Р	167.01	15.12		151.89	40,000	690	430	2,600	4,900	<25		SEQM	6.9	t
8/23/2006	Р	167.01	20.00		147.01	13,000	1,500	540	1,200	3,000	<10		TAMC	6.97	
11/15/2006	Р	167.01	19.84		147.17	3,800	700	22	67	160	54	0.65	TAMC	6.78	
2/14/2007	Р	167.01	14.94	SHEEN	152.07	37,000	350	120	2,400	8,100	120	2.12	TAMC	7.05	t
5/22/2007	Р	167.01	17.17	SHEEN	149.84	13,000	810	130	750	2,200	15	0.06	TAMC	7.10	t
8/15/2007	Р	167.01	20.30	SHEEN	146.71	4,400	550	38	160	310	<10	3.09	TAMC	7.09	
11/8/2007	Р	167.01	19.58	SHEEN	147.43	13,000	970	130	480	1,600	6.0	1.47	TAMC	7.95	t
2/20/2008		167.01	14.27	0.05	152.78										b, j
5/7/2008	Р	167.01	18.61		148.40	16,000	970	150	770	2,000	<20	2.18	CEL	6.98	t
QC-2															
10/5/1992		168.01				<50	< 0.5	< 0.5	< 0.5	< 0.5					f

		тос	Depth to	Product	Water Level	Concentrations in (µg/L)									
Well and Sample Date	P/NP	Elevation (feet msl)	Water (feet bgs)	Thickness (feet)	Elevation (feet msl)	GRO/ TPHg	Benzene	Toluene	Ethyl- Benzene	Total Xvlenes	MTBE	DO (mg/L)	Lab	рH	Comments
OC-2 Cont		()	(	()	()	8						(8,)		<b>F</b>	
QC 2 Conta															
1/13/1993		168.01				<50	<0.5	<0.5	<0.5	<0.5					f,i
4/23/1993		168.01				<50	< 0.5	<0.5	< 0.5	< 0.5					f,i
7/12/1993		168.01				<50	<0.5	< 0.5	<0.5	<0.5					f
10/21/1993		168.01				<50	< 0.5	< 0.5	< 0.5	< 0.5					f
1/21/1994		168.01				<50	< 0.5	2.1	< 0.5	2.1					f
4/20/1994		168.01				<50	< 0.5	< 0.5	< 0.5	< 0.5					f
12/23/1994		168.01				<50	<0.5	< 0.5	< 0.5	< 0.5					f
1/26/1995		168.01				<50	< 0.5	< 0.5	< 0.5	<1					f
6/8/1995		168.01				<50	< 0.50	< 0.50	< 0.50	<1.0					f
8/22/1995		168.01				<50	< 0.50	< 0.50	< 0.50	<1.0	<5.0				d,f
10/30/1995		168.01				<50	< 0.50	< 0.50	< 0.50	<1.0	<5.0				f
1/25/1996		168.01				<50	< 0.50	< 0.50	< 0.50	<1.0	<5.0				f
4/19/1996		168.01				<50	< 0.5	<1	<1	<1	<10				f
RW-1															
7/0/1000		1.00.01													
//9/1990		168.01													
12/21/1990		168.01													
3/7/1991		168.01	17.62		150.39										t
4/1/1991		168.01	14.40		153.61										
6/27/1991		168.01													
9/27/1991		168.01													
12/18/1991		168.01													
7/3/1992		168.01	20.66		147.35										t
10/5/1992		168.01	23.34		144.67										
1/13/1993		168.01	16.59		151.42										
4/23/1993		168.01	16.17		151.84										
7/12/1993		168.01	20.18		147.83										
10/21/1993		168.01	25.70		142.31										
1/21/1994		168.01	21.24		146.77										
4/20/1994		168.01	32.20		135.81										
8/1/1994		168.01	21.70		146.31	29,000	580	950	300	7,800	1,200	1.1			d

		тос	Depth to	Product	Water Level	Concentrations in (µg/L)									
Well and Sample Date	P/NP	Elevation (feet msl)	Water (feet bgs)	Thickness (feet)	Elevation (feet msl)	GRO/ TPHg	Benzene	Toluene	Ethyl- Benzene	Total Xylenes	MTBE	DO (mg/L)	Lab	рH	Comments
RW-1 Cont		( ,	(		(	8				<b>J</b>		( <del>,</del> ,		r	
Kii I Conu															
12/23/1994		168.01	16.02		151.99	1,300	25	8.6	1.4	69	616	1.8			i
1/26/1995		168.01	13.78		154.23	<50	<0.5	< 0.5	<0.5	<1					
1/26/1995		168.01				<50	<0.5	<0.5	< 0.5	<1					с
6/8/1995		168.01	20.05		147.96	1,300	130	<1.0	<1.0	36					
8/22/1995		168.01	21.74		146.27	3,300	230	13	4.9	280	<25	6.6			d
8/22/1995		168.01				2,800	210	9.3	4.3	250	<25				с
10/27/1995		168.01	32.00		136.01										
10/30/1995		168.01				240	1.6	<1.0	<1.0	<2.0	630				с
10/30/1995		168.01				230	1.4	<1.0	<1.0	<2.0	650	6.9			
1/25/1996		168.01	15.41		152.60	15,000	3,400	930	330	2,500	5,300				
4/19/1996		168.01				33,000	5,600	3,200	1,700	8,800	15,000				с
4/19/1996		168.01	16.83		151.18	35,000	5,500	3,300	1,700	9,400	14,000	7.6			
7/23/1996		168.01				47,000	3,700	2,500	930	5,300	35,000				с
7/23/1996		168.01	20.76		147.25	46,000	3,600	2,300	900	5,100	36,000	7.4			
11/11/1996		168.01				31,000	2,900	1,000	860	4,600	22,000				с
11/11/1996		168.01	21.73		146.28	34,000	3,000	1,200	880	4,600	22,000	8.3			
1/21/1997		168.01	14.20		153.81	260	40	16	2.7	34	1,500	6.1			
1/21/1997		168.01				270	42	17	2.7	36	1,500				с
4/29/1997		168.01	19.15		148.86	32,000	3,100	590	1,300	6,000	46,000	5.3			
8/21/1997		168.01	20.67		147.34	7,600	730	58	370	1,780	9,500	4.7			
11/5/1997		168.01	21.01		147.00	39,000	2,300	86	1,300	3,840	56,000	4.5			
2/3/1998		168.01	10.68		157.33	3,400	31	11	29	161	3,200	5.1			
5/28/1998		168.01	15.55		152.46	2,000	90	15	60	305	2,700	4.3			
12/30/1998		168.01	17.35		150.66										
2/2/1999		168.01	14.58		153.43	82,000	2,300	120	2,000	3,200	51000/78000				g
5/10/1999		168.01	16.00		152.01	15,000	620	88	340	660	61,000				
8/24/1999		168.01	20.00		148.01	52,000	1,400	170	2,200	2,900	37,000				
11/3/1999		168.01	20.39		147.62	17,000	2,500	86	1,500	970	54,000				
3/1/2000		168.01	12.97		155.04	17,000	580	78	790	1,100	13,000				
4/21/2000		168.01	16.02		151.99	31,000	2,100	100	1,400	1,100	39,000				
7/31/2000		168.01	21.89		146.12	47,000	1,300	170	2,700	2,300	30,000				

		тос	Depth to	Product	Water Level	Concentrations in (µg/L)									
Well and		Elevation	Water	Thickness	Elevation	GRO/			Ethyl-	Total		DO			
Sample Date	P/NP	(feet msl)	(feet bgs)	(feet)	(feet msl)	TPHg	Benzene	Toluene	Benzene	Xylenes	MTBE	(mg/L)	Lab	pН	Comments
RW-1 Cont.															
11/20/2000		168.01	19.15		148.86										h
2/18/2001		168.01	15.35		152.66	14,000	589	89	600	712	13,000				
6/7/2001		168.01	19.09		148.92	28,000	1,140	68.2	504	530	19,100				
9/5/2001		168.01	22.06	0.02	145.93										j
11/30/2001		168.01	19.53		148.48	20,000	405	39.4	545	740	8,260				
2/20/2002		168.01	15.99		152.02	13,000	469	29	434	655	7,240				
6/20/2002		168.01	19.31		148.70										j,1
9/11/2002		168.01	21.07	0.03	146.91										j
11/12/2002		168.01	20.92	0.02	147.07										j
1/29/2003		168.01	16.31	0.04	151.66										j,n
5/22/2003		168.01	16.68		151.33										j,t
6/24/2003		168.01	19.76	0.07	148.18										0
7/28/2003		168.01	21.04	0.04	146.93										j
8/12/2003		168.01	21.41	< 0.01	146.60										o,t
9/12/2003		168.01	21.10	0.07	146.84										0
10/3/2003		168.01		0.03											
11/18/2003	Р	168.01	20.10	< 0.01	147.91	12,000	770	<50	320	250	6,100		SEQM	6.6	o,p
12/31/2003		168.01		< 0.01											
02/23/2004		168.01	14.35	0.01	153.67										
3/18/2004		168.01		0.09											
4/13/2004		168.01		0.02											
05/04/2004		168.01	19.58	0.02	148.45										
6/2/2004		168.01		0.05											
7/2/2004		168.01		0.11											
08/04/2004		168.01	22.05	0.05	146.00										
09/22/2004	NP	168.01	21.28	0.06	146.78										
10/26/2004		168.01		0.01											
11/10/2004		168.01	18.56	0.02	149.47										
12/27/2004		168.01		0.03											
01/13/2005		168.01	12.51	0.01	155.51										
02/15/2005		168.01	15.24	0.03	152.79										

		тос	Depth to	Product	Water Level		Concentra								
Well and		Elevation	Water	Thickness	Elevation	GRO/			Ethyl-	Total		DO			
Sample Date	P/NP	(feet msl)	(feet bgs)	(feet)	(feet msl)	TPHg	Benzene	Toluene	Benzene	Xylenes	MTBE	(mg/L)	Lab	pН	Comments
RW-1 Cont.															
03/07/2005		168.01	11.90	0.02	156.13										
4/29/2005		168.01		0.03											
05/16/2005		168.01	14.39	0.02	153.64										j
6/21/2005		168.01		0.03											
7/7/2005		168.01		0.06											
08/17/2005		168.01	19.91	0.03	148.12										j
9/6/2005		168.01		0.03											
10/4/2005		168.01		0.07											
11/18/2005		168.01	20.36	0.07	147.71										b, j
12/30/2005		168.01		0.04											
1/24/2006		168.01		0.01											
02/07/2006		168.01	12.87	0.01	155.15										j
3/30/2006		168.01		0.02											
5/19/2006		168.01	15.87	0.04	152.17										b
8/23/2006		168.01	20.50	0.07	147.56										b, j
11/15/2006		168.01	20.52	0.07	147.54										b, j
2/14/2007		168.01	15.44	0.04	152.60										b, j
5/22/2007		168.01	17.78	SHEEN	150.23										j, l
8/15/2007		168.01	20.80	0.02	147.23										b, j
11/8/2007		168.01	20.32	0.01	147.70										b, j
2/20/2008		168.01	14.55	0.02	153.48										b, j
5/7/2008		168.01													e

#### SYMBOLS AND ABBREVIATIONS:

- -- = Not analyzed/applicable/measured/available
- < = Not detected at or above specified laboratory reporting limit
- DO = Dissolved oxygen
- DTW = Depth to water in ft bgs
- ft bgs = Feet below ground surface
- ft MSL = Feet above mean sea level
- GRO = Gasoline range organics
- GWE = Groundwater elevation measured in ft MSL
- mg/L = Milligrams per liter
- MTBE = Methyl tert-butyl ether
- NP = Well not purged prior to sampling
- P = Well purged prior to sampling
- TOC = Top of casing measured in ft MSL
- TPH-g = Total petroleum hydrocarbons as gasoline
- $\mu g/L = Micrograms \ per \ liter$
- SEQ/SEQM= Sequoia Analytical/Sequoia Analytical Morgan Hill (Laboratories)
- SPH = Separate phase hydrocarbons

#### FOOTNOTES:

- a = Casing elevations surveyed to the nearest 0.01 ft MSL.
- b = GWE adjusted assuming a specific gravity of 0.75 for free product (FP).
- c = Blind duplicate.
- d = A copy of the documentation for this data is included in Appendix C of Alisto report 10-024-10-001.
- e = Well inaccessible.
- f = Travel blank.
- g = EPA Methods 8020/8260 used.
- h = Unable to sample.

i = A copy of the documentation for this data can be found in Blaine Tech Services report 010607-M-3. MTBE data for the January 13, 1993 and April 23, 1993 sampling events has been destroyed. No chromatograms could be located for MTBE data from wells MW-5, MW-6, and MW-7, sampled on October 21, 1993.

- j = Well not sampled due to presence of SPH and nature of the product.
- $\mathbf{k} = \mathbf{Could}$  not purge and sample; waste drum full.
- l = Value represents the depth to product. Unable to determine depth to water, product disabled the interface probe.
- m = Discrete p[ak @ C6-7.
- n = TPH-g, BTEX, and MTBE analyzed by EPA method 8260 B beginning on 1st quarter 2003 aampling event (1/29/03).
- o = Groundwater samples are not collected during FP bailing event.
- p = Well not included in the monthly FP bailing program.
- q = Well not sampled in November 2003 due to the presence of a pile of gravel dumped over the well box.
- r = This sample was analyzed beyond the EPA recommended holding time. The results may still be useful for their intended purpose.
- s = MW-7 TOC elevation raised +0.47 ft during well repair on January 20, 2004.
- t = Sheen in well.
- $\boldsymbol{u}=\boldsymbol{C}ali\boldsymbol{b}.$  verif. is within method limits but outside contract limits.
- v = GRO result partly due to individual peak(s) in quantitation range.

#### NOTES:

Beginning in the fourth quarter 2003, the laboratory modified the reported analyte list. TPH-g was changed to GRO. The resulting data may be impacted by the potential of non-TPH-g analytes within the requested fuel range resulting in a higher concentration being reported.

Beginning in the second quarter 2004, the carbon range for GRO was changed from C6-C10 to C4-C12.

Values for DO and pH were obtained through field measurements.

Note: The data within this table collected prior to April 2006 was provided to Broadbent & Associates, Inc. by Atlantic Richfield Company and their previous consultants. Broadbent & Associates, Inc. has not verified the accuracy of this information.

Well and				Concentrati	ions in (µg/L)				
Sample Date	Ethanol	TBA	MTBE	DIPE	ETBE	TAME	1,2-DCA	EDB	Comments
<b>MW-1</b>									
5/19/2006	<6,000	<400	86	<10	<10	<10	<10	<10	
MW-2									
1/29/2003	<4000	<2000	820	<50	<50	<50	<50	<50	
5/22/2003	<10000	<2000	1,000	<50	<50	<50			
7/28/2003	<20000	<4000	1,700	<100	<100	<100	<100	<100	a
11/18/2003	<5,000	<1,000	500	<25	<25	<25			
02/23/2004	<25,000	<5,000	790	<120	<120	<120	<120	<120	
05/04/2004	<50,000	<10,000	780	<250	<250	<250	<250	<250	
08/04/2004	<50,000	<10,000	430	<250	<250	<250	<250	<250	
11/10/2004	<5,000	<1,000	310	<25	<25	<25	<25	<25	
02/15/2005	<20,000	<4,000	690	<100	<100	<100	<100	<100	
05/16/2005	<50,000	<10,000	560	<250	<250	<250	<250	<250	
08/17/2005	<20,000	<4,000	480	<100	<100	<100	<100	<100	
11/18/2005	<20,000	<4,000	340	<100	<100	<100	<100	<100	b
02/07/2006	<60,000	<4,000	440	<100	<100	<100	160	<100	
5/19/2006	<60,000	<4,000	430	<100	<100	<100	<100	<100	b
8/23/2006	<60,000	<4,000	480	<100	<100	<100	<100	<100	
11/15/2006	<60,000	<4,000	400	<100	<100	<100	<100	<100	
2/14/2007	<60,000	<4,000	810	<100	<100	<100	<100	<100	
5/22/2007	<150,000	<10,000	1,000	<250	<250	<250	<250	<250	
8/15/2007	<30,000	2,400	260	<50	<50	<50	<50	<50	b
11/8/2007	<30,000	2,800	240	<50	<50	<50	<50	<50	
MW-3									
1/29/2003	<40	<20	0.76	<50	<50	<50	<50	<50	
02/23/2004	<100	<20	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50	
02/15/2005	<100	<20	1.7	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50	
02/07/2006	<300	<20	< 0.50	< 0.50	< 0.50	<0.50	<0.50	< 0.50	
2/14/2007	<300	<20	3.8	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50	u
2/20/2008	<100	<10	2.3	< 0.50	< 0.50	< 0.50	<0.50	< 0.50	
MW-4									

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Well and				Concentratio	ons in (µg/L)				
Sample Date	Ethanol	TBA	MTBE	DIPE	ETBE	TAME	1,2-DCA	EDB	Comments
MW-4 Cont.									
1/29/2003	<40	<20	66	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50	
02/23/2004	<100	<20	65	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50	
02/15/2005	<100	<20	62	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50	
02/07/2006	<300	<20	29	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50	
2/14/2007	<300	<20	61	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50	
2/20/2008	<100	<10	36	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50	
MW-5									
1/29/2003	<400	<200	82	<5.0	<5.0	<5.0	<5.0	<5.0	
5/22/2003	<10000	<2000	<50	<50	<50	<50			
7/28/2003	<2000	<400	120	<10	<10	<10	<10	<10	
11/18/2003									Well inaccessible
02/23/2004	<5,000	<1,000	100	<25	<25	<25	38	<25	
05/04/2004	<5,000	<1,000	42	<25	<25	<25	<25	<25	
08/04/2004	<5,000	<1,000	390	<25	<25	<25	<25	<25	
11/10/2004	<1,000	<200	530	<5.0	<5.0	5.5	<5.0	<5.0	
02/15/2005	<1,000	<200	260	<5.0	<5.0	<5.0	<5.0	<5.0	
05/16/2005	<1,000	<200	370	<5.0	<5.0	<5.0	<5.0	<5.0	
08/17/2005	<1,000	<200	51	<5.0	<5.0	<5.0	<5.0	<5.0	
11/18/2005	<1,000	<200	340	<5.0	<5.0	<5.0	<5.0	<5.0	b
02/07/2006	<3,000	<200	200	<5.0	<5.0	<5.0	<5.0	<5.0	
5/19/2006	<3,000	<200	44	<5.0	<5.0	<5.0	<5.0	<5.0	ь
8/23/2006	<3,000	<200	230	<5.0	<5.0	<5.0	<5.0	<5.0	
11/15/2006	<1,500	<100	490	<2.5	<2.5	4.2	<2.5	<2.5	
2/14/2007	<1,500	<100	420	<2.5	<2.5	3.6	<2.5	<2.5	
5/22/2007	<1,500	<100	26	<2.5	<2.5	<2.5	<2.5	<2.5	
8/15/2007	<6,000	<400	280	<10	<10	<10	<10	<10	
11/8/2007	<1,500	310	270	<2.5	<2.5	<2.5	<2.5	<2.5	
2/20/2008	<1,000	<100	43	<5.0	<5.0	<5.0	<5.0	<5.0	
5/7/2008	<6,000	<200	30	<10	<10	<10	<10	<10	
MW-6									

Station #11132,	3201 35tl	Ave,	Oakland.	CA
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Well and				Concentratio	ons in (µg/L)				
Sample Date	Ethanol	TBA	MTBE	DIPE	ETBE	TAME	1,2-DCA	EDB	Comments
MW-6 Cont.									
05/16/2005	<100	<20	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50	
02/07/2006	<300	<20	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50	
2/14/2007	<300	<20	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50	
2/20/2008	<100	<10	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50	< 0.50	
MW-7									
02/07/2006	<3,000	<200	270	<5.0	<5.0	<5.0	<5.0	<5.0	
2/14/2007	<3,000	<200	740	<5.0	<5.0	9.6	<5.0	<5.0	
2/20/2008	<100	13	700	< 0.50	< 0.50	12	0.60	< 0.50	
MW-8									
1/29/2003	<4000	<2000	<500	<50	<50	<50	<50	<50	
5/22/2003	<5000	<1000		<25	<25	<25			
7/28/2003	<20000	<4000	2,100	<100	<100	<100	<100	<100	
11/18/2003	<2,000	<400	1,700	<10	<10	20			a,b
02/23/2004	<10,000	<2,000	110	<50	<50	<50	<50	<50	
05/04/2004	<5,000	<1,000	2,000	<25	<25	33	<25	<25	
11/10/2004	<5,000	<1,000	74	<25	<25	<25	<25	<25	
02/15/2005	<10,000	<2,000	<50	<50	<50	<50	<50	<50	
05/16/2005	<10,000	<2,000	<50	<50	<50	<50	<50	<50	
08/17/2005	<10,000	<2,000	<50	<50	<50	<50	<50	<50	
11/18/2005	<10,000	<2,000	140	<50	<50	<50	<50	<50	b
02/07/2006	<3,000	<200	7.5	<5.0	<5.0	<5.0	<5.0	<5.0	
5/19/2006	<15,000	<1,000	<25	<25	<25	<25	<25	<25	b
8/23/2006	<15,000	<1,000	82	<25	<25	<25	<25	<25	
11/15/2006	<15,000	<1,000	110	<25	<25	<25	<25	<25	
2/14/2007	<15,000	<1,000	82	<25	<25	<25	<25	<25	
5/22/2007	<6,000	<400	11	<10	<10	<10	<10	<10	
8/15/2007	<6,000	<400	28	<10	<10	<10	<10	<10	
11/8/2007	<15,000	<1,000	27	<25	<25	<25	<25	<25	
MW-9									
5/22/2003	<10000	<2000	<50	<50	<50	<50			

	Station	#11132,	3201	35th Ave,	Oakland,	CA
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Well and	Concentrations in (µg/L)								
Sample Date	Ethanol	TBA	MTBE	DIPE	ETBE	TAME	1,2-DCA	EDB	Comments
MW-9 Cont.									
7/28/2003	<100000	<20000	<500	<500	<500	<500	<500	<500	
11/18/2003	<2,000	<400	45	<10	<10	<10			a,b
02/23/2004	<50,000	<10,000	<250	<250	<250	<250	<250	<250	
05/04/2004	<5,000	<1,000	<25	<25	<25	<25	<25	<25	
11/10/2004	<10,000	<2,000	<50	<50	<50	<50	<50	<50	
02/15/2005	<10,000	<2,000	<50	<50	<50	<50	<50	<50	
05/16/2005	<2,000	<400	<10	<10	<10	<10	<10	<10	
08/17/2005	<2,500	<500	<12	<12	<12	<12	<12	<12	
11/18/2005	<1,000	<200	19	<5.0	<5.0	<5.0	<5.0	<5.0	b
02/07/2006	<3,000	<200	<5.0	<5.0	<5.0	5.4	<5.0	<5.0	
8/23/2006	<30,000	<2,000	<50	<50	<50	<50	<50	<50	
11/15/2006	<15,000	<1,000	26	<25	<25	<25	<25	<25	
2/14/2007	<15,000	<1,000	<25	<25	<25	<25	<25	<25	
5/22/2007	<15,000	<1,000	<25	<25	<25	<25	<25	<25	
8/15/2007	<1,500	<100	27	<2.5	<2.5	<2.5	<2.5	<2.5	b
11/8/2007	<3,000	<200	52	<5.0	<5.0	<5.0	<5.0	<5.0	
MW-10									
5/22/2003	<10000	<2000	300	<50	<50	<50			
11/18/2003	<10,000	<2,000	<50	<50	<50	<50			b
02/23/2004	<20,000	<4,000	180	<100	<100	<100	<100	<100	
05/04/2004	<5,000	<1,000	<25	<25	<25	<25	<25	<25	
11/10/2004	<5,000	<1,000	230	<25	<25	<25	<25	<25	b
02/15/2005	<10,000	<2,000	77	<50	<50	<50	<50	<50	
05/16/2005	<10,000	<2,000	<50	<50	<50	<50	<50	<50	
08/17/2005	<10,000	<2,000	<50	<50	<50	<50	<50	<50	
11/18/2005	<2,500	<500	16	<12	<12	<12	<12	<12	b
02/07/2006	<15,000	<1,000	73	<25	<25	<25	<25	<25	
5/19/2006	<15,000	<1,000	<25	<25	<25	<25	<25	<25	b
8/23/2006	<6,000	<400	<10	<10	<10	<10	<10	<10	
11/15/2006	<6,000	<400	54	<10	<10	<10	<10	<10	
2/14/2007	<6,000	<400	120	<10	<10	<10	<10	<25	
#### Table 2. Summary of Fuel Additives Analytical Data

Well and		Concentrations in (µg/L)							
Sample Date	Ethanol	TBA	MTBE	DIPE	ETBE	TAME	1,2-DCA	EDB	Comments
MW-10 Cont.									
5/22/2007	<6,000	<400	15	<10	<10	<10	<10	<10	
8/15/2007	<6,000	<400	<10	<10	<10	<10	<10	<10	
11/8/2007	<3,000	<200	6.0	<5.0	<5.0	<5.0	<5.0	<5.0	
5/7/2008	<12,000	<400	<20	<20	<20	<20	<20	<20	
RW-1									
11/18/2003	<10,000	11,000	6,100	<50	<50	160			a,b

#### Station #11132, 3201 35th Ave, Oakland, CA

#### SYMBOLS AND ABBREVIATIONS:

-- = Not analyzed/applicable/measured/available
 < = Not detected at or above specified laboratory reporting limit</li>
 1,2-DCA = 1,2-Dichloroethane
 DIPE = Di-isopropyl ether
 EDB = 1,2-Dibromoethane
 ETBE = Ethyl tert-butyl ether
 MTBE = Methyl tert-butyl ether
 TAME = tert-Amyl methyl ether
 TBA = tert-Butyl alcohol
 µg/L = Micrograms per Liter

#### FOOTNOTES:

a = The result for TBA was reported with a possible high bias due to the continuing calibration verification falling outside acceptance criteria

b = The continuing calibration verification for ethanol was outside of client contractual acceptance limits. However, it was within method acceptance limits. The data should still be useful for its intended purpose.

#### NOTES:

All volatile organic compounds analyzed using EPA Method 8260B.

Note: The data within this table collected prior to April 2006 was provided to Broadbent & Associates, Inc. by Atlantic Richfield Company and their previous consultants. Broadbent & Associates, Inc. has not verified the accuracy of this information.

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Date Sampled	<b>Approximate Flow Direction</b>	Approximate Hydraulic Gradient
5/19/2006	South	0.003 to 0.005
8/23/2006	Southwest	0.01
11/15/2006	South	0.004
2/14/2007	Southeast	0.01
5/22/2007	South	0.005
8/15/2007	South-Southwest	0.008
11/8/2007	Southwest	0.006
2/20/2008	Southeast	0.008
5/7/2008	South-Southwest	0.003

## Table 3. Historical Ground-Water Flow Direction and GradientStation #11132, 3201 35th Ave, Oakland, CA

Note: The data within this table collected prior to April 2006 was provided to Broadbent & Associates, Inc. by Atlantic Richfield Company and their previous consultants. Broadbent & Associates, Inc. has not verified the accuracy of this information.

WELL ID	DATE OF MONITORING	PRODUCT THICKNESS (feet)	PRODUCT REMOVED (gallons)	CUMULATIVE PRODUCT REMOVED (gallons)
MW-1	7/9/1990	0.22	2.000	2.000
MW-1	12/21/1990	0.58	2.000	4.000
MW-1	3/7/1991	0.00		4.000
MW-1	6/27/1991	0.18	2.000	6.000
MW-1	9/27/1991	0.27	2.000	8.000
MW-1	12/18/1991	0.28	2.000	10.000
MW-1	4/1/1991	0.15	2.000	12.000
MW-1	7/3/1992	0.27	2.000	14.000
MW-1	10/5/1992	0.24	2.000	16.000
MW-1	1/13/1993	0.24	2.000	18.000
MW-1	4/23/1993	0.42	2.000	20.000
MW-1	7/12/1993	0.49		20.000
MW-1	10/21/1993	1.09	2.000	22.000
MW-1	1/21/1994	0.76		22.000
MW-1	4/20/1994	1.80	2.000	24.000
MW-1	8/1/1994	0.35		24.000
MW-1	1/26/1995	1.10	3.000	27.000
MW-1	6/8/95-6/28/95	1.25	0.700	27.700
MW-1	8/22/1995	0.85	0.150	27.850
MW-1	10/30/95-12/23/95	0.69	0.110	27.960
MW-1	1/25/96-2/16/95	1.40	1.080	29.040
MW-1	4/19/1996	1.22	0.750	29.790
MW-1	7/23/1996	0.89	0.000	29.790
MW-1	9/4/1996		0.350	30.140
MW-1	11/11/1996	0.89	0.980	31.120
MW-1	1/21/1997	0.90	0.200	31.320
MW-1	4/29/1997	0.85	0.250	31.570
MW-1	8/21/1997		0.150	31.720
MW-1	11/2/97-12/9/97	0.87	2.030	33.750
MW-1	2/3/1998	0.32	0.250	34.000
MW-1	2/4/1998			34.000
MW-1	5/28/1998	0.17		34.000
MW-1	12/30/1998	0.08	0.020	34.020
MW-1	2/2/1999	0.03	0.010	34.030
MW-1	5/10/1999	0.03	0.010	34.040
MW-1	8/24/1999	0.06	0.010	34.050
MW-1	11/3/1999	0.36	0.050	34.100
MW-1	3/1/2000	0.23	*	34.100
MW-1	4/21/2000	0.33	0.070	34.170
MW-1	//31/2000	0.53	0.130	34.300
MW-1	2/18/2001	0.37	0.500	34.800
MW-1	2/18/2001	0.13	0.050	34.850
MW-1	2/26/2001	0.15	0.150	35.000
IVI VV - 1 MIX7 1	0/7/2001	0.00		35,000
MW 1	11/30/2001	0.35	0.260	35.000
MXX/ 1	12/6/2001	0.41	0.200	35.200
MW 1	2/20/2001	0.27	0.040	35 320
MW 1	6/20/2002	0.15	0.020	35.320
MW-1	9/11/2002	0.34	0.070	35.450
MW_1	11/12/2002	0.37	0.000	35 510
MW-1	1/29/2003	0.30	0.320	35,830

WELL ID	DATE OF MONITORING	PRODUCT THICKNESS (feet)	PRODUCT REMOVED (gallons)	CUMULATIVE PRODUCT REMOVED (gallons)
MW-1	5/22/2003	0.20	0.140	35.970
MW-1	6/24/2003	0.35	0.070	36.040
MW-1	7/28/2003	0.35	0.080	36.050
MW-1	8/12/2003	0.23	0.040	36.090
MW-1	9/12/2003	0.24	0.040	36.130
MW-1	10/3/2003	0.23	0.040	36.170
MW-1	11/18/2003	0.25	0.040	36.210
MW-1	12/31/2003	0.15	0.020	36.230
MW-1	2/2/2004	0.15	0.020	36,250
MW-1	2/23/2004	0.09	0.030	36,280
MW-1	3/18/2004	0.09	0.010	36.290
MW-1	4/13/2004	0.24	0.040	36.330
MW-1	5/4/2004	0.16	0.030	36,360
MW-1	6/2/2004	0.08	0.010	36.370
MW-1	7/2/2004	0.28	0.040	36.410
MW-1	8/4/2004	0.10	0.080	36 490
MW-1	9/22/2004	0.20	0.030	36.520
MW-1	10/26/2004	0.12	0.020	36.540
MW-1	11/10/2004	0.14	0.020	36,560
MW-1	12/27/2004	0.08	0.010	36.570
MW-1	1/13/2005	0.03	0.005	36 575
MW-1	2/15/2005	0.03	0.005	36 581
MW-1	3/7/2005	0.04	0.000	36 588
MW-1	4/29/2005	0.01	0.007	36 589
MW-1	5/16/2005	0.01	0.002	36 592
MW-1	6/21/2005	0.02	0.003	36.594
MW 1	7/7/2005	0.01	0.002	36.623
MW 1	8/17/2005	0.18	0.029	36.636
MW 1	9/6/2005	0.03	0.013	36,630
MW 1	9/0/2005	0.02	0.003	36.650
MW 1	0/6/2005	0.12	0.020	36.660
MW 1	9/0/2005	0.06	0.010	30.009
IVI VV - I	1/24/2005	0.03	0.003	30.074
NIW-1	1/24/2006	0.00	0.000	30.074
MW-1	2/7/2006	0.01	0.002	36.676
MW-1	3/30/2006	0.00	0.000	36.676
MW-1	4/21/2006	0.00	0.000	36.676
MW-1	5/19/2006	<0.01 (SHEEN)	0.000	36.676
MW-1	6/22/2006	0.04	0.006	36.682
MW-1	7/31/2006	0.04	0.006	36.688
MW-1	8/23/2006	0.14	0.022	36.710
MW-1	9/28/2006	0.35	0.056	36.766
MW-1	11/15/2006	0.18		36.766
MW-1	2/14/2007	0.17	*	36.766
MW-1	3/14/2007	0.04	****	36.766
MW-1	4/10/2007	0.15	****	36.766
MW-1	5/22/2007	0.01	****	36.766
MW-1	6/26/2007	0.05	****	36.766
MW-1	7/19/2007	0.00		36.766
MW-1	8/15/2007	0.01	2.0	38.766
MW-1	9/18/2007	0.10	2.0	40.766
MW-1	10/17/2007	0.01	4.0	44.766
MW-1	11/8/2007	0.01	3.0	47.766

WELL ID	DATE OF MONITORING	PRODUCT THICKNESS (feet)	PRODUCT REMOVED (gallons)	CUMULATIVE PRODUCT REMOVED (gallons)
MW-1	12/12/2007	0.01	1.5	49,266
MW-1	1/14/2008	0.01	3.0	52.266
MW-1	2/27/2008		2.0	54.266
MW-1	4/1/2008	0.01	5.0	59.266
MW-1	5/7/2008	0.02	*	59.266
MW-1	5/20/2008	0.00	10	60 266
MW-1	6/18/2008	0.00	4.5	64.766
MW-2	4/1/2008	0.01	1.5	1.500
MW-2	5/7/2008	0.04	*	1.500
MW-2	5/20/2008	0.00	1.0	2.500
MW-2	6/18/2008	0.00	2.5	5.000
MW	11/02/02 12/00/08	0.12	1 (20	1 (20
MW-8	0/5/2001	0.12	1.620	1.620
MW-8	9/5/2001	0.04		1.660
MW-8	8/12/2003	<0.01 (SHEEN)		1.660
MW-8	10/3/2003	<0.01 (SHEEN)		1.660
MW-8	11/18/2003	<0.01 (SHEEN)		1.660
MW-8	12/31/2003	<0.01 (SHEEN)		1.660
MW-8	2/2/2004	<0.01 (SHEEN)		1.660
MW-8	2/23/2004	<0.01 (SHEEN)		1.660
MW-8	3/18/2004	<0.01 (SHEEN)		1.660
MW-8	4/13/2004	<0.01 (SHEEN)		1.660
MW-8	5/4/2004	<0.01 (SHEEN)		1.660
MW-8	6/2/2004	<0.01 (SHEEN)		1.660
MW-8	7/2/2004			1.660
MW-8	8/4/2004	0.05	0.110	1.770
MW-8	9/22/2004			1.770
MW-8	10/26/2004			1.770
MW-8	11/10/2004			1.770
MW-8	12/26/2004			1.770
MW-8	1/13/2005			1.770
MW-8	2/15/2005			1.770
MW-8	3/7/2005			1.770
MW-8	4/29/2005			1.770
MW-8	5/16/2005			1.770
MW-8	6/21/2005			1.770
MW-8	7/7/2005			1.770
MW-8	8/17/2005			1.770
MW-8	9/6/2005			1.770
MW-8	1/24/2006			1.770
MW-8	2/7/2006			1.770
MW-8	3/30/2006			1.770
MW-8	4/21/2006			1.770
MW-8	5/19/2006	<0.01 (Sheen)		1.770
MW-8	6/22/2006			1.770
MW-8	7/31/2006			1.770
MW-8	8/23/2006			1.770
MW-8	9/28/2006			1.770
MW-8	11/15/2006	<0.01 (Sheen)		1.770
MW-8	2/14/2007	<0.01 (Sheen)		1.770
MW-8	5/22/2007	<0.01 (Sheen)		1.770
MW-8	6/26/2007			1.770

## Table 4 Free Product Removal

Former BP Service Station #11132 3201 35th Avenue, Oakland, CA

WELL ID	DATE OF MONITORING	PRODUCT THICKNESS (feet)	PRODUCT REMOVED (gallons)	CUMULATIVE PRODUCT REMOVED (gallons)
MW-8	7/19/2007			1.770
MW-8	8/15/2007	<0.01 (Sheen)		1.770
MW-8	9/18/2007			1.770
MW-8	10/17/2007			1.770
MW-8	11/8/2007			1.770
MW-8	12/12/2007			1.770
MW-8	1/14/2008	NM	NM	1.770
MW-8	2/27/2008	NM	NM	1.770
MW-8	4/1/2008	NM	NM	1.770
<b>MW-8</b>	5/7/2008	NM	NM	1.770
MW-8	5/20/2008	0.00	0.000	1.770
MW-8	6/18/2008	0.00	0.000	1.770
MW-9	11/2/93-4/29/97	0.10	<0.1	0.880
MW-9	11/5/1997	0.01	< 0.1	0.880
MW-9	1/29/2003	0.10	0.190	1.070
MW-9	6/24/2003	NM	NM	1.070
MW-9	7/28/2003	<0.01 (SHEEN)		1.070
MW-9	8/12/2003	<0.01 (SHEEN)		1.070
MW-9	9/12/2003	<0.01 (SHEEN)		1.070
MW-9	10/3/2003	0.01	0.002	1.072
MW-9	11/18/2003	<0.01 (SHEEN)		1.072
MW-9	12/31/2003	<0.01 (SHEEN)		1.072
MW-9	2/2/2004	<0.01 (SHEEN)		1.072
MW-9	2/23/2004	<0.01 (SHEEN)		1.072
MW-9	3/18/2004	<0.01 (SHEEN)		1.072
MW-9	4/13/2004	<0.01 (SHEEN)		1.072
MW-9	5/4/2004	<0.01 (SHEEN)		1.072
MW-9	6/2/2004	<0.01 (SHEEN)		1.072
MW-9	7/2/2004			1.072
MW-9	8/4/2004	0.03	0.053	1.125
MW-9	9/22/2004			1.125
MW-9	10/26/2004			1.125
MW-9	11/10/2004			1.125
MW-9	12/27/2004			1.125
MW-9	1/13/2005			1.125
MW-9	2/15/2005			1.125
MW-9	3/7/2005			1.125
MW-9	4/29/2005			1.125
MW-9	5/16/2005			1.125
MW-9	6/21/2005			1.125
MW-9	7/7/2005			1.125
MW-9	8/17/2005			1.125
MW-9	9/6/2005			1.125
MW-9	1/24/2006			1.125
MW-9	2/7/2006	SHEEN		1.125
MW-9	3/30/2006			1.125
MW-9	4/21/2006			1.125
MW-9	5/19/2006	NM		1.125
MW-9	6/22/2006			1.125
MW-9	7/31/2006			1.120
MW-9	8/23/2006			1.120

WELL ID	DATE OF MONITORING	PRODUCT THICKNESS (feet)	PRODUCT REMOVED (gallons)	CUMULATIVE PRODUCT REMOVED (gallons)
MW-9	9/28/2006			1.120
MW-9	11/15/2006	<0.01 (Sheen)		1.120
MW-9	2/14/2007	<0.01 (Sheen)		1.120
MW-9	5/22/2007	<0.01 (Sheen)		1.120
MW-9	6/26/2007			1.120
MW-9	7/19/2007			1.120
MW-9	8/15/2007	<0.01 (Sheen)		1.120
MW-9	9/18/2007			1.120
MW-9	10/17/2007			1.120
MW-9	11/8/2007			1.120
MW-9	12/12/2007			1.120
MW-9	1/14/2008			1.120
MW-9	2/27/2008			1.120
MW-9	4/1/2008	0.00	0.000	1.120
MW-9	5/7/2008	0.03	*	1.120
MW-9	5/20/2008	0.00	0.000	1.120
MW-9	6/18/2008	0.00	0.000	1.120
MW-10	9/7/93-7/23/96		10.520	10.520
MW-10	9/4/1996	0.76	0.100	10.620
MW-10	11/11/1996		0.200	10.820
MW-10	1/21/1997		< 0.03	10.850
MW-10	4/29/1997		0.040	10.890
MW-10	4/29/1997		0.040	10.930
MW-10	12/2/1997	0.03	<0.1	10.930
MW-10	2/3/1998		<0.1	10.930
MW-10	9/5/2001	0.01		10.930
MW-10	11/12/2002	0.07	0.010	10.940
MW-10	1/29/2003	0.03	0.030	10.970
MW-10	6/24/2003	0.04	0.010	10.980
MW-10	7/28/2003	0.04	0.020	11.000
MW-10	8/12/2003	<0.01 (SHEEN)		11.000
MW-10	10/3/2003	<0.01 (SHEEN)		11.000
MW-10	11/18/2003	<0.01 (SHEEN)		11.000
MW-10	12/31/2003	<0.01 (SHEEN)		11.000
MW-10	2/2/2004	<0.01 (SHEEN)		11.000
MW-10	2/23/2004	<0.01 (SHEEN)		11.000
MW-10	3/18/2004	<0.01 (SHEEN)		11.000
MW-10	4/13/2004	<0.01 (SHEEN)		11.000
MW-10	5/4/2004	<0.01 (SHEEN)		11.000
MW-10	6/2/2004	<0.01 (SHEEN)		11.000
MW-10	7/2/2004	<0.01 (SHEEN)		11.000
MW-10	8/4/2004	0.08	0.110	11.110
MW-10	9/22/2004			11.110
MW-10	10/26/2004			11.110
MW-10	11/10/2004			11.110
MW-10	12/27/2004			11.110
MW-10	1/13/2005	<0.01 (SHEEN)		11.110
MW-10	2/15/2005			11.110
MW-10	3/7/2005			11.110
MW-10	4/29/2005			11.110
MW-10	5/16/2005			11.110
MW-10	6/21/2005			11.110

WELL ID	DATE OF MONITORING	PRODUCT THICKNESS (feet)	PRODUCT REMOVED (gallons)	CUMULATIVE PRODUCT REMOVED (gallons)
MW-10	7/7/2005			11.110
MW-10	8/17/2005			11.110
MW-10	9/6/2005			11.110
MW-10	1/24/2006			11.110
MW-10	2/7/2006	SHEEN		11.110
MW-10	3/30/2006			11.110
MW-10	4/21/2006			11.110
MW-10	5/19/2006	<0.01 (SHEEN)		11.110
MW-10	6/22/2006			11.110
MW-10	7/31/2006			11.110
MW-10	8/23/2006			11.110
MW-10	9/28/2006			11.110
MW-10	11/15/2006	<0.01 (Sheen)		11.110
MW-10	2/14/2007	<0.01 (Sheen)		11.110
MW-10	5/22/2007	<0.01 (Sheen)		11.110
MW-10	6/26/2007	<0.01 (Sheen)		11.110
MW-10	7/19/2007			11.110
MW-10	8/15/2007	<0.01 (Sheen)		11.110
MW-10	9/18/2007			11.110
MW-10	10/17/2007			11.110
MW-10	11/8/2007			11.110
MW-10	12/12/2007			11.110
MW-10	1/14/2008			11,110
MW-10	2/27/2008			11.110
MW-10	4/1/2008	0.00	0.000	11.110
MW-10	5/7/2008	0.00	0.000	11.110
MW-10	5/20/2008	0.00	0.000	11.110
MW-10	6/18/2008	0.00	0.000	11.110
DW 1	0/5/2001	0.02		0.000
KW-I	9/5/2001	0.02		0.000
KW-I	6/20/2002	0.02		0.000
KW-I	9/11/2002	0.03	0.040	0.040
KW-I	1/20/2002	0.02	0.030	0.070
KW-I	1/29/2003	0.04	0.070	0.140
KW-I	6/24/2003	0.07	0.040	0.180
KW-I	7/28/2003	0.04	0.020	0.200
KW-I	8/12/2003	<0.01 (SHEEN)		0.200
KW-I	9/12/2003	0.07	0.100	0.300
KW-I	10/3/2003	0.03	0.040	0.340
KW-I	11/18/2003	<0.01 (SHEEN)		0.340
KW-I	12/31/2003	<0.01 (SHEEN)		0.340
KW-I	2/23/2004	0.01	0.005	0.345
RW-I	3/18/2004	0.09	0.120	0.465
KW-I	4/13/2004	0.02	0.030	0.495
KW-I	5/4/2004	0.02	0.030	0.525
KW-I	6/2/2004	0.05	0.020	0.545
KW-1	7/2/2004	0.11	0.162	0.707
KW-I	8/4/2004	0.05	0.159	0.865
RW-1	9/22/2004	0.06	0.088	0.953
RW-1	10/26/2004	0.01	0.010	0.963
KW-1	11/10/2004	0.02	0.030	0.993
RW-1	12/27/2004	0.03	0.010	1.003
RW-1	1/13/2005	0.01	0.004	1.007

## Table 4 Free Product Removal Former BP Service Station #11132

3201 35th Avenue, Oakland, CA

WELL ID	DATE OF MONITORING	PRODUCT THICKNESS (feet)	PRODUCT REMOVED (gallons)	CUMULATIVE PRODUCT REMOVED (gallons)	
RW-1	2/15/2005	0.03	0.044	1.051	
RW-1	3/7/2005	0.02	0.029	1.080	
RW-1	4/29/2005	0.03	0.044	1.124	
RW-1	5/16/2005	0.02	0.029	1.154	
RW-1	6/21/2005	0.03	0.013	1.167	
RW-1	7/7/2005	0.06	0.092	1.259	
RW-1	8/17/2005	0.03	0.044	1.304	
RW-1	9/6/2005	0.03	0.044	1.348	
RW-1	10/4/2005	0.07	0.100	1.448	
RW-1	11/18/2005	0.07	0.010	1.458	
RW-1	12/30/2005	0.04	0.006	1.464	
RW-1	1/24/2006	0.01	0.015	1.479	
RW-1	2/7/2006	0.01	0.015	1.494	
RW-1	3/30/2006	0.02	0.030	1.524	
RW-1	4/21/2006	0.00	0.000	1.524	
RW-1	5/19/2006	0.04	0.058	1.582	
RW-1	6/22/2006	0.03	0.044	1.626	
RW-1	7/31/2006	0.12	0.176	1.802	
RW-1	8/23/2006	0.07	0.103	1.905	
RW-1	9/28/2006	0.07	0.103	2.008	
RW-1	11/15/2006	0.07		2.008	
RW-1	2/14/2007	0.04	*	2.008	
RW-1	3/14/2007	0.05	****	2.008	
RW-1	4/10/2007	0.10	****	2.008	
RW-1	5/22/2007	**	****	2.008	
RW-1	6/26/2007	0.05	****	2.008	
RW-1	7/19/2007	<0.01 (Sheen)		2.008	
RW-1	8/15/2007	0.02	2.0	4.008	
RW-1	9/18/2007	0.03	2.0	6.008	
RW-1	10/17/2007	0.01	4.0	10.008	
RW-1	11/8/2007	0.01	2.5	12.508	
RW-1	12/12/2007	0.01	2.5	15.008	
RW-1	1/14/2008	0.01	4.0	19.008	
RW-1	2/27/2008		1.0	20.008	
RW-1	4/1/2008	0.01	1.5	21.508	
<b>RW-1</b>	5/7/2008	NM	NM	21.508	
RW-1	5/20/2008	0.00	2.0	23.508	
RW-1	6/18/2008	0.00	3.0	26.508	
Free Product Removed this Quarter = 22.000					

Total Free Product =

110.274

NM = Unable to gauge free product thickness or remove product because the well was inaccessible.

\* No hazardous waste drum on-site or drum was full, therefore no product was removed.

\*\* Indeterminate thickness of product. The nature of product is unknown, very viscous.

\*\*\* Data prior to 1998 is incomplete, and amounts removed are estimates based on quarter reports from the previous consultants.

\*\*\*\* Absorbent socks used to collect product. Unknown amount of product recovered.

The data within this table collected prior to June 2006 was provided to BAI by RM and their previous consultants. BAI has not verified the accuracy of this information.

#### APPENDIX A

Historical Soil and Ground-Water Data



- MW (HCNITORING WELL)

Source: KEI, September 10, 1986

Figure C-1

## ENVIRONMENTAL RESEARCH GROUP, INC.

11/ N. First Ann Arbor, Michigan 48104 (313) 662-3104



April 7, 1986

KEI Engineers 535 Main Street Martinez, CA 94553

Attention: Mardo Kapriliean

Report #7535

P.O. #Contract

Site Location: Mobil, Oakland, 35th

RE: Seven (7) soil samples submitted on April 2, 1986, for rush total hydrocarbon response analysis.

Procedure: The samples are analyzed for total hydrocarbon response (gasoline) by following the method described in Attachment 2, Analytical Procedures for Fuel Leak Investigations. The samples are concentrated on a Tekmar LSC-2 automatic sample concentrator prior to injection into a gas chromatograph fitted with a flame ionization detector. Quantitation is performed, as total hydrocarbon response, against known concentrations of heptane-isooctane (55/45). The limit of detection for this method of analysis is one part per million (mg/kg), unless indicated.

The results are displayed in the table below.

ERG #	CLIENT ID#	CONCENTRATION (mg/kg)
75 35 - 1	1	8
75 35 - 2	1A	16
75 35 - 3	2	3.1
75 35 - 4	3	210
75 35 - 5	4	ND (1)
75 35 - 6	5	ND (5)
75 35 - 7	6	5.7

ND = None Detected. The limits of detection are in ( ).

Submitted by:

Molust D. Flay

Robert B. Flay Manager, Organics Department

RBF:clp 040886t

Ann Arbor

Chicago

Cleveland

KEI-86-045 September 10, 1986

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#### TABLE - 1

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### Results of Groundwater Analysis

Parameter	<u>MW #1</u>	<u>MW #2</u>	<u>MW #3</u>
Total Fuel Hydrocarbons (ppm)	4.4	26.0	<0.05
Benzene (ppm)	0.8	3.8	<0.001
Toluene (ppm)	0,52	1.0	<0.001
Xylene (ppm)	0.35	1.7	<0.001
Depth (feet)	22.0	20.0	21.2
Free Product (inches)	0.0	0.0	0.0
Odor	ND	ND	ND
Sheen	ND	ND	ND

### Results of Soil Analysis

Odor	N	ND	ND	ND
Depth (feet)		26.0	16.0/26.0	16.0
Total Fuel Hydrocarbons (ppm)	)	12.0	5.7/2.0	<1.0

#### ND = None Detected

)

KEI-P86-045A-1 February 5, 1987

#### TABLE 1

## Results of the Groundwater Analyses

In Parts Per Million (ppm)

Date	Parameter	<u>Well_#1</u>	<u>Well #2</u>	Well #3
8/18/86	Total Dissolved Hydrocarbons	4.4	26.0	<0.05
	Benzene	0.8	3.8	<0.001
	Toluene	0.52	1.0	<0.001
	Xylene	0.35	1.7	<0.001
12/23/86	Total Dissolved Hydrocarbons	85.0	6.2	0.25
	Benzene	28.0	3.6	0.0087
	Toluene	30.0	1.3	0.007
	Xylene	11.0	0.39	0.023

## Monitoring Wells

<u>Date</u>	<u>Well #</u>	DTW (feet)	<u>PT</u> (inches)	<u>Odor</u>	<u>Sheen</u>
10/28/86	1 2 3	23.0 21.0 20.0	<0.25 0.0 0.0	Yes Yes Yes	No No
11/26/86	1 2 3	22.92 21.58 20.25	<0.1 0.0 0.0	Yes Yes Yes	No No
12/23/86	1 2 3	21.83 20.5 19.25	0.0 0.0 0.0	Yes No No	Yes No No

DTW

Depth to Water
Product Thickness  $\mathbf{PT}$ 

Source: KEI, February 5, 1987

KEI-P86-045A-2 May 20, 1987 Page 4

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#### TABLE 1

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#### GROUNDWATER MONITORING DATA

<u>Date</u>	<u>Well No.</u>	<u>DTW</u> (ft)	<u>Odor</u>	<u>Sheen</u>	Gallons <u>Pumped</u>
4/25/87	MW-1	20.813	Moderate	No	35
	MW-2	19.375	Slight	No	35
	MW-3	17.760	No	No	40
3/17/87	MW-1	18.0	Moderate	No	30
	MW-2	16.583	Slight	No	30
	MW-3	15.563	No	No	30
2/11/87	MW-1	19.750	Moderate	Yes	31
	MW-2	17.542	Slight	No	30
	MW-3	16.167	No	No	31

DTW = Depth to water

Source: KEI, May 20, 1987

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Table C-3 Page 2 of 5 .

KEI-P86-045A-3 September 28, 1987 Page 4

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#### TABLE 1

#### GROUNDWATER MONITORING DATA

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Date	<u>Well No.</u>	<u>DTW</u> (ft)	I Odor 1	Product Thickness	<u>Sheen</u>	Gallons <u>Pumped</u>
6/20/87	MW-1	22.33	Slight	0	Yes	40
	MW-2	21.60	Slight	0	No	35
	MW-3	19.708	No	0	No	35
7/20/87	MW-1	22.875	Strong	0.25		40
•••	MW-2	21.583	Moderate	e 0	No	35
	MW-3	20.270	No	0	No	35
11107	MW-1	23.333	Strong	1.25		40
110121	MW-2	21.917	Slight	0	No	35
	MW-3	20.667	No	õ	No	35
	4'4TT *** 🖬	EU+007	110	v	10	في د

DTW = Depth to water

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Source: KEI, September 28, 1987

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Table C-3 Page 3 of 5

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KEI-P86-045B-2 January 8, 1988 Page 4

#### TABLE 1

## GROUNDWATER MONITORING DATA

<u>Date</u>	<u>Well No.</u>	<u>DTW</u> (ft)	Product <u>Thickness</u>	<u>Odor</u>	<u>Sheen</u>	Gallons Pumped
10/17/87	MW-1	23.583	0.25	Strong	Yes	80
	MW-2	22.688	0	Faint	No	65
	MW-3	21.33	0	None	No	65
11/18/87	MW-1	23.250	0	Strong	Yes	45
	MW-2	21.438	0	Faint	No	35
	MW-3	20.50	0	None	No	30
12/19/87	MW-1	19.729	0	Strong	Yes	45
	MW-2	16.833	0	Faint	No	35
	MW-3	16.750	0	None	No	30

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Source: KEI, January 8, 1988

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Table C-3 Page 4 of 5 .

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KEI-P86-0405.QR5 March 16, 1989

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#### TABLE 1

#### SUMMARY OF MONITORING DATA

Date	Well No.	Water Depth (feet)	Product <u>Thickness</u>	Sheen	Water Bailed <u>(gallons)</u>
2/15/89	MW-1	19.60	<b>,</b> 5*	taga apite titar	45
	MW-2	18.16	.5*		30
	MW-3	16.54	0	Trace	30
1/17/89	MW-1	19.71	1.25*	<b>(**</b> 49 <b>**</b>	22
	MW-2	18.20	Trace	100 gli 410	14
	MW-3	16,79	0	None	0
12/21/88	3 MW-1	22.15	(3=)		25
	MW-2	22.38	0/38#		15
	MW-3	19.05	Õ	None	0

Source: KEI, March 16, 1989

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Table C-3 Page 5 of 5

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#### RESULTS OF GROUNDWATER ANALYSES (Concentrations are in Parts Per Million)

Date	<u>Parameter</u>	<u>MW-1</u>	<u>MW-2</u>	<u>MW-3</u>
12/22/87	TPH	69.00	9.50	<0.050
	Benzene	28.00	0.360	0.00085
	Toluene	27.00	0.990	0.0016
	Xylene	12.00	6.00	0.0058
9/10/87	трн	210.00	13.00	<0.050
and	Benzene	6.80	0.170	<0.0005
9/22/87	Toluene	11.00	0.065	<0.0005
	Xylene	12.00	0.740	<0.0005
4/25/87	трн	13.00	1.50	<0.050
• •	Benzene	1.80	0.120	<0.0005
	Toluene	0.730	0.0078	<0.0005
	Xylene	1.300	0.150	<0.0005
12/23/86	TPH	86.00	6.2	0.25
• •	Benzene	28.00	3.6	0.0087
	Toluene	30.00	1.3	0.007
	Xylene	11.00	0.39	0.023
8/18/86	TPH	4.4	26.0	<0.050
	Benzene	0.8	3.8	<0.001
	Toluene	0.52	1.0	<0.001
	Xylene	0.35	1.7	<0.001

Table C-4 Page 1 of 2

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KEI-P86-0405.QR5 March 16, 1989

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#### TABLE 2

## SUMMARY OF LABORATORY ANALYSES

### (All results in ppb)

Date	Sample <u>Well #</u>	Depth (feet)	TPH <b>as</b> <u>Gasoline</u>	<u>Benzene</u>	Toluene	<u>Xylenes</u>	Ethyl- benzene
2/15/89	MW-1	20.00	Not samp]	led due to	presence	of free pro	duct
	MW-2	18.33	9,200	110	290	1,400	8.5
	MW-3	18.00	<50	<0.5	<0.5	<0.5	<0.5

Source: KEI, March 16, 1986

Table C-4 Page 2 of 2

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Figure C-2



#### RESULTS OF ANALYSIS GROUND WATER SAMPLES

Well	TPH (ppm)	Benzene (ppb)	Toluene (ppb)	Ethyl- benzene (ppb)	Total Xylenes (ppb)
MW-1	FD				
MW-2	14	580	1300	460	2300
MW-3	0.5	20	30	24	35
TW-1	7.4	230	180	690	1200
TW-2	FP				
TW-3	22	2400	2800	530	4000
TW-4	ND <0.1	ND <0.3	ND <0.3	ND <0.3	0.7
TW-5	240	1100	5100	5600	28000
ти-б	20	56	910	590	3700
TW-7	ND <0.1	ND <0.3	0.4	0.7	4.3
<b>TW-8</b>	ND <0.1	0.3	0.6	1.1	7.9
TW-9	41	2100	5700	120	6900
TW-10	50	1900	7300	1400	8000

ND = Non-Detected FP = Free Product ppm = parts per million ppb = parts per billion MW = Monitoring Well TW = Temporary Well

Source: Alton, February 28, 1990



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#### Source: Alton, September 4, 1990

Figure C-3

Boring	Sample Depth (ft)	TPH-G (Concer	B ntrations	T in Parts	E Per Mill	X ion)
			June 199	<u>0</u>		
MW-4	5.0	ND	ND	ND	ND	ND
MW-4	10.0	ND	ND	ND	ND	ND
MW-4	15.0	ND	ND	ND	ND	ND
MW-4	20.0	ND	ND	ND	ND	ND
MW-4	25.0	ND	ND	ND	ND	ND
RW-1	5.0	ND	ND	ND	ND	
RW-1	10.0	ND	ND	ND	ND	ND
RW-1	15.0	22	0.72	1.6	0.58	2.2
RW-1	20.0	41	ND	18.0	8.0	40.0
RW-1	25.0	50	1.4	3.3	1.0	5.4
			<u>July 199</u>	Q		
MW5	5.0	ND	ND	ND	ND	ND
MW-5	10.0	9.3	ND	0.019	ND	0.11
MW5	15.0	14	0.16	0.037	0.29	0.42
MW-5	20.0	190	1.8	11	2.5	17
MW-5	25.0	770	4.8	44	13	94
MW-6	15.0	ND	ND	ND	ND	רוא
MW-6	20.0	ND	ND	ND	ND	ND
MW-7	15.0	ND	ND	ND	ND	ND

#### RESULTS OF LABORATORY ANALYSIS OF SOIL SAMPLES June - July 1990

#### Notes:

.

TPH-G	=	Total Petroleum Hydrocarbons as Gasoline
B	Ħ	Benzene
T .	=	Toluene
Е	=	Ethylbenzene
X	=	Total Xylenes
ND	a	Not Detected at Method Detection Limit (refer to Appendix D, Official Laboratory Reports)

Source: Alton, September 4, 1990

Table C-6

11132

Monitoring Well	TPH-G (Conce	B ntrations	T in Parts	E per Bill	X ion)
MW-1		یور افغا			
MW-2		4946 dawa			
MW-3	140	5.3	4.6	2.0	3.8
MW-4	ND	ND	ND .	ND	ND
MW-5	280	200	210	46	290
MW-6	ND	ND	ND	ND	ND
MW-7	ND	ND	ND	ND	ND

#### RESULTS OF LABORATORY ANALYSIS OF GROUND WATER SAMPLES July 1990

Notes:

TPH-G = Total Petroleum Hydrocarbons as Gasoline
B = Benzene
T = Toluene
E = Ethylbenzene
X = Total Xylenes
ND = Not Detected at Method Detection Limit
 (refer to Appendix D, Official Laboratory Reports)
-- = No sample collected due to the presence of free
 floating product

Source: Alton, September 4, 1990



#### LEGEND

\* Sample Point Location

	<b>D</b> 30	60
Figure	Approx. scale BP Service Station 3201 35th Avenue Oakland, CA C-4	feel

#### SUMMARY OF LABORATORY ANALYSES SOIL

#### (Collected on August 21 & 24, 1990)

<u>Sample</u>	Depth (feet)	TPH as <u>Gasoline</u>	<u>Benzene</u>	Toluene	<u>Xylenes</u>	Ethyl- <u>benzene</u>	Organic <u>Lead</u>
Dl	4.5	ND	ND	ND	ND	ND	ND
D2	3.0	ND	ND	ND	ND	ND	ND
D3	7.0	ND	ND	ND	ND	ND	ND
PT-1	3.0	ND	ND	ND	ND	ND	0.55
PT-2	3.0	ND	ND	ND	ND	ND	ND
PT-3	4.0	21	0.0099	0.062	0.038	0.060	ND
PT-4	3.0	ND	ND	ND	ND	ND	ND
Detect	ion	1.0	0.0050	0.0050	0.0050	0.0050	0.050

ND = Non-detectable.

Results in parts per million (ppm), unless otherwise indicated.

Source: KEI, October 11, 1990a

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Table C-8

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\* Sample Point Location

U 30	
Approx. scale	teel
<b>BP</b> Service Station	
3201 35th Avenue	
Oakland, CA	

U



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Figure C-6

Source: KEI, October 11, 1990b

KEI-J90-0804.R1 October 11, 1990

#### TABLE 1

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### SUMMARY OF LABORATORY ANALYSES

(Collected on August 21 & 31, 1990)

<u>Sample</u>	TPH as <u>Gasoline</u>	Benzene	Toluene	<u>Xylenes</u>	Ethylbenzene
Comp A*	8.0	ND	0.019	0.14	0.014
Comp B	240	0.060	0.70	9.5	0.68
Comp 1	6.1	ND	ND	0.019	0.0060
Detectior Limits	1 1.0	0.0050	0.0050	0.0050	0.0050

\* Organic lead was non-detectable.

ND = Non-detectable.

Results in parts per million (ppm), unless otherwise indicated.

Source: KEI, October 11, 1990b

	RESULTS	OF		
LABORATORY	ANALYSIS	OF	SOIL	SAMPLES
	March 1	991		

Boring	Sample Depth (ft)	TPH-G (Conce	B ntrations i	T In Parts	E Per Milli	X .on)
SB-8	10.5-11.0	ND<1	ND<0.003	0.004	ND<0.003	ND<0.003
	20.5-21.0	390	1.8	16	6.7	37
	25.5-26.0	ND<1	0.013	0.028	0.009	0.05
SB-9	10.5-11.0	ND<1	ND<0.003	0.004	ND<0.003	0.006
	20.5-21.0	120	1.7	7.1	1.7	11
	25.5-26.0	130	0.47	3.9	1.6	12
SB-10	10.5-11.0	ND<1	ND<0.003	0.007	ND<0.003	0.017
	20.5-21.0	73	0.49	3.3	1.3	6.9
	25.5-26.0	1	0.41	0.009	0.007	0.019

#### Notes:

TPH-G = Total Petroleum Hydrocarbons as Gasoline
B = Benzene
T = Toluene
E = Ethylbenzene
X = Total Xylenes
ND = Not Detected at Method Detection Limit shown

Source: Alton, AUgust 21, 1991

Monitoring Well	TPH-G (Concer	B itrations i	T .n Parts	E per Bill.	X ion)
MW-1	*	*	*	*	*
MW-2	*	*	*	*	*
MW-3	400	69	22	6.1	57
MW-4	ND<50	2.2	3.8	1.5	2.8
MW-5	ND<50	17	0.9	0.7	1.6
MW-6	**	**	**	**	**
MW-7	ND<50	ND<0.3	0.4	0.3	2.4
MW-8	2700	780	450	64	310
MW-9	7100	220	4	2.4	2400
MW-10	1600	120	190	32	230
RW-1	***	***	***	***	***

#### RESULTS OF LABORATORY ANALYSIS OF GROUND WATER SAMPLES April 1990

#### Notes:

TPH-G = Total Petroleum Hydrocarbons as Gasoline

- B = Benzene
- T = Toluene
- E = Ethylbenzene
- X = Total Xylenes
- ND = Not Detected at Method Detection Limit
- \* = No sample collected due to the presence of free product
- \*\* = No sample collected due to the presence of an abandoned vehicle located over the well
- \*\*\* = The recovery well was not sampled due to the presence
   of an oily substance

Source: Alton, August 21, 1991

#### TABLE 2 - PRODUCT REMOVAL STATUS

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## BP OIL COMPANY SERVICE BTATION NO. 11132 3201 35TH STREET, OAKLAND, CAUFORNIA

#### ALISTO PROJECT NO. 10-024

WELL ID	DATE	PRCOUCT REMOVED {Guilonia}	PRODUCT REMOVED CUMULATIVE (Galione)
₩₩-2	09/29/93 10/05/93 10/14/93 10/20/93 11/02/93 12/07/93 12/17/93 12/23/93 01/12/94 02/02/94 02/02/94 02/11/94	0.10 0.10 0.25 0.10 0.25 0.01 0.3 0.05 0.01 0.01 0.01	0.10 0.20 0.55 0.65 0.70 0.70 0.70 1.00 1.05 1.05 1.07 1.07
м₩-8 	11/02/93 11/10/93 11/10/93 11/10/93 11/10/93 11/10/93 12/17/93 12/17/93 12/17/94 02/02/94 02/12/94 02/18/94 04/27/94 11/10/93 11/10/94 11/10/93 11/10/94 11/10/93 11/10/94 11/10/	025 010 010 010 010 000 000 000 000 000 00	0.25 0.35 0.45 0.55 0.65 0.65 0.65 0.65 0.77 0.79 0.00 0.79 0.79 0.00 0.79 0.00 0.00
₩₩-10 	09/07/93 09/14/93 09/26/93 10/05/93 10/20/93 10/20/93 10/20/93 11/10/93 11/10/93 11/20/93 11/20/93 12/07/93 12/07/93 12/20/94 01/02/94 01/20/94 01/20/94 01/20/94 02/18/94	0.10 0.10 0.10 1.20 2.10 1.00 1.00 0.20	0.10, 0.20 0.30 1.90 4.00 6.00 6.30 6.30 6.30 6.30 7.20 7.20 7.20 7.20 7.20 7.20 7.20 7.2

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Source: Alisto, May 25, 1994



#### Table A-1

#### Site Number 11132 3201 - 35th Avenue, Oakland, California

## Soil Sample Results of Analyses (ppm)

			California DHS LUFT Method TPH-G	California Method Hydr	DHS LUFT ocarbon Scan	BTEX EPA Method 5030/802			
Sample Number	Depth (feet)	Date Collected	TPH-G	TPH-D	TPH-O	Benzene	Toluene	Ethylbenzene	Total Xylenes
THP1-S-4-4.5*	4-4.5	11/22/94	nd	nd	120	nd	nd	nd	nd
NOTE:       TPH-G = Total petroleum hydrocarbons as gasoline.       TW = Tosco well.         TPH-D = Total petroleum hydrocarbons as diesel.       TB = Tosco boring.         TPH-O = Total petroleum hydrocarbons as oil.       TD = Tosco dispenser soil sample.         nd = Not detected at or above method reporting limit.       THP = Tosco HydroPunch.         n/a = Not applicable.       SGP = Soil gas probe.         - = Not analyzed.       * = THP1 is referred to as HP1 on the lab report (see Attachment D).									

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### Table 1 Soil Analytical Results

### Former BP Service Station #11132 3201 35th Avenue Oakland, California

Sample ID	Sample Depth (feet bgs)	Date Sampled	GRO (mg/kg)	Benzene (mg/kg)	Toluene (mg/kg)	Ethyl- benzene (mg/kg)	Total Xylenes (mg/kg)	MTBE (mg/kg)	Ethanol (mg/kg)	TBA (mg/kg)	DIPE (mg/kg)	ETBE (mg/kg)	TAME (mg/kg)	I,2-DCA (mg/kg)	EDB (mg/kg)	Lead (mg/kg)
UB-1-32.0	30.0	7/22/04	ND<0.10	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.10	ND<0.020	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	NA
UB-1-32.5	30.5	7/22/04	ND<0.10	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.10	ND<0.020	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	NA
UB-3-30.0	30.0	7/22/04	ND<0.10	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.10	ND<0.020	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	NA
UB-3-30.5	30.5	7/22/04	ND<0.10	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.10	ND<0.020	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	NA
UB-4-30.0	30.0	7/21/04	ND<0.10	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	0.0056	ND<0.10	ND<0.020	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	NA
UB-4-30.5	30.5	7/21/04	ND<0.10	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	0.018	ND<0.10	ND<0.020	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	NA
UB-6-30.0	30.0	7/21/04	ND<0.10	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.10	ND<0.020	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	NA
UB-6-30.5	30.5	7/21/04	ND<0.10	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.10	ND<0.020	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	NA
UB-7-5	5	04/19/04	ND<1.0	ND<0.0050	ND<0.0050	ND<0.0050	0.0055	0.0075	ND<0.20	ND<0.10	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	NA
UB-7-15	15	04/19/04	6.9	ND<0.025	ND<0.025	0.067	0.62	ND<0.025	ND<0.20	ND<0.10	ND<0.025	ND<0.025	ND<0.025	ND<0.025	ND<0.025	NA
UB-7-25	25	04/19/04	19	ND<2.0	ND<2.0	ND<2.0	4.2	ND<2.0	ND<80	ND<40	ND<2.0	ND<2.0	ND<2.0	ND<2.0	ND<2.0	NA
UB-7-35	35	04/19/04	ND<1.0	ND<0.025	ND<0.025	ND<0.025	ND<0.025	0.036	ND<1.0	0.76	ND<0.025	ND<0.025	ND<0.025	ND<0.025	ND<0.025	NA
UB-7-41	41	04/19/04	ND<1.0	0.0093	ND<0.0050	ND<0.0050	0.013	0.20	ND<0.20	0.56	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	NA
UB-9-5	5	04/19/04	ND<1.0	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.20	ND<0.10	ND<0 0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	NA
UB-9-15	15	04/19/04	ND<1.0	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0 0050	ND<0.20	ND<0.10	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	NA
UB-9-25	25	04/19/04	22	ND<5.0	ND<5.0	ND<5.0	20	ND<5.0	ND<200	ND<100	ND<5.0	ND<5.0	ND<5.0	ND<5.0	ND<5.0	NA
UB-9-35	35	04/19/04	ND<1.0	0.17	0.014	0.031	0.020	<b>0.061</b>	ND<0.20	<b>0.14</b>	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	NA
UB-9-42	42	04/19/04	ND<1.0	ND<0.0050	ND<0.0050	ND<0.0050	0.011	ND<0.0050	ND<0.20	ND<0.10	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	NA
UB-10-5	5	04/20/04	ND<1.0	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	0.0058	ND<0.20	ND<0.10	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	NA
UB-10-15	15	04/20/04	72	ND<2.0	ND<2.0	ND<2.0	3.0	ND<2.0	ND<80	ND<40	ND<2.0	ND<2.0	ND<2.0	ND<2.0	ND<2.0	NA
UB-10-25	25	04/20/04	820	ND<5.0	ND<5.0	5.7	37	ND<5.0	ND<200	ND<100	ND<5.0	ND<5.0	ND<5.0	ND<5.0	ND<5.0	7.9
UB-10-35	35	04/20/04	ND<1.0	ND<0.0050	ND<0.0050	ND<0.0050	0.0061	0.016	ND<0.20	0.85	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	NA
UB-10-37	37	04/20/04	ND<1.0	ND<0.0050	ND<0.0050	ND<0.0050	0.0099	0.0062	ND<0.20	0.24	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	NA
UB-11-5 UB-11-15 UB-11-25	5 15 25	04/20/04 04/20/04 04/20/04	ND<1.0 64 ND<1.0	ND<0.0050 ND<2.0 ND<0.0050	ND<0.0050 ND<2.0 ND<0.0050	ND<0.0050 <b>2.6</b> ND<0.0050	ND<0.0050 13 ND<0.0050	0.0083 ND<2.0 0.0093	ND<0.20 ND<80 ND<0.20	ND<0.10 ND<40 ND<0.10	ND<0.0050 ND<2.0 ND<0.0050	ND<0.0050 ND<2.0	ND<0.0050 ND<2.0	ND<0.0050 ND<2.0	ND<0.0050 ND<2.0	NA NA
UB-11-35	35	04/20/04	ND<1.0	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	0.054	ND<0.20	ND<0.10	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	NA
UB-11-37	37	04/20/04	ND<1.0	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	9.034	ND<0.20	ND<0.10	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	NA
UB-12-5	5	04/19/04	ND<1.0	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.20	ND<0.10	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	NA
UB-12-10	10	04/19/04	ND<1.0	ND<0.0050	ND<0.0050	ND<0.0050	0.0072	ND<0.0050	ND<0.20	ND<0.10	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	NA
UB-12-15	15	04/19/04	ND<1.0	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.20	ND<0.10	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	NA
UB-12-24.5	24.5	04/19/04	ND<1.0	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.20	ND<010	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	ND<0.0050	NA

# Table 1Soil Analytical Results

#### Former BP Service Station #11132 3201 35th Avenue Oakland, California

Notes

- GRO = Gasoline Range Organics (C4-C12) analyzed by EPA Method 8015B
- BTEX = Benzene, toluene, ethylbenzene, and total xylenes, EPA Method 8260B
- MTBE = Methyl tent-butyl ether by EPA Method 8260B
- TBA = Tert butyl alcohol, by EPA Method 8260B
- DIPE = Di-isopropyl ether, by EPA Method 8260B
- ETBE = Ethyl tert-butyl ether, by EPA Method 8260B
- TAME = Tert-Amyl methyl ether, by EPA Method \$260B
- 1,2-DCA = 1,2-Dichloroethane, by EPA Method 8260B
- EDB = 1,2-Dibromoethane, by EPA Method 8260B
- ND< = Not detected at or above laboratory reporting limits
- NA = Not analyzed
- bgs = Below ground surface
- mg/kg = milligrams per kilogram

						Former	BP Service S	Station #11132	2					
							3201 35th A	venue						
							Oakland, Cal	ifornia						
Sample ID	Date Sampled	GRO (µg/L)	Benzene (µg/L)	Toluene (µg/L)	Ethyl- benzene (µg/L)	Total Xylenes (µg/L)	MTBE (µg/L)	Ethanol (µg/L)	TBA (μg/L)	DIPE (µg/L)	ETBE (µg/L)	TAME (µg/L)	1,2-DCA (μg/L)	EDB (µg/L)
UB-1-48	07/23/04	ND<50	ND<0.50	ND<0.50	ND<0.50	0.81	ND<0.50	ND<100	ND<20	ND<0.50	ND<0.50	ND<0.50	ND<0.50	ND<0.50
UB-2-48	07/22/04	ND<50	ND<0.50	ND<0.50	ND<0.50	ND<0.50	ND<0.50	ND<100	ND<20	ND<0.50	ND<0.50	ND<0.50	ND<0.50	ND<0.50
UB-3-48	07/22/04	ND<50	ND<0.50	ND<0.50	ND<0.50	1.0	ND<0.50	ND<100	ND<20	ND<0.50	ND<0.50	ND<0.50	ND<0.50	ND<0.50
UB-4	07/21/04	ND<50	ND<0.50	ND<0.50	ND<0.50	ND<0.50	ND<0.50	ND<100	ND<20	ND<0.50	ND<0.50	ND<0.50	ND<0.50	ND<0 50
UB-5	07/21/04	190	9.5	ND<0.50	6.7	8.1	75	ND<100	ND<20	ND<0.50	ND<0.50	ND<0.50	ND<0.50	ND<0.50
UB-6	07/21/04	260	9.1	1.2	21	8.3	1.2	ND<100	ND<20	ND<0.50	ND<0.50	ND<0.50	ND<0.50	ND<0.50
UB-7	04/19/04	32,000	7,300	960	1,300	4,000	28,000	ND<100,000	ND<20,000	ND<1,000	ND<1,000	ND<1,000	ND<500	ND<500
UB-9	04/19/04	25,000	11,000	1,500	1,200	2,400	2,700	ND<100,000	ND<20,000	ND<1,000	ND<1,000	ND<1,000	ND<500	ND<500
UB-10	04/20/04	31,000	3,700	2,400	1,000	4,000	35,000	ND<200,000	ND<40,000	ND<2,000	ND<2,000	ND<2,000	ND<1,000	ND<1,000
UB-11	04/20/04	1,200	ND<50	ND<50	ND<50	51	2,400	ND<10,000	ND<2,000	ND<100	ND<100	ND<100	ND<50	ND<50
UB-12	04/19/04	120	5.9	ND<0.50	0.99	2.1	0.77	ND<100	ND<20	ND<1.0	ND<1.0	ND<1.0	ND<0.50	ND<0.50

 Table 2

 Boring Groundwater Grab Sample Analytical Results

Table 2
Boring Groundwater Grab Sample Analytical Results

Former BP Service Station #11132 3201 35th Avenue Oakland, California

Notes
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- GRO = Gasoline Range Organics (C4-C12) analyzed by EPA Method 8260B (samples UB-1 through UB-6) and by EPA Method 8015B (samples UB-7 through UB-12)
- BTEX = Benzene, toluene, ethylbenzene, and total xylenes, EPA Method 8260B
- MTBE = Methyl tert-butyl ether by EPA Method 8260B
- TBA = Tert butyl alcohol, by EPA Method 8260B
- DIPE = Di-isopropyl ether, by EPA Method 8260B
- ETBE = Ethyl tert-butyl ether, by EPA Method 8260B
- TAME = Tert-Amyl methyl ether, by EPA Method 8260B
- 1,2-DCA = 1,2-Dichloroethane, by EPA Method 8260B
- EDB = 1,2-Dibromoethane, by EPA Method 8260B
- ND< = Not detected at or above specified laboratory reporting limit
- $\mu g/L$  = micrograms per liter

### APPENDIX B

Soil Boring and Well Construction Logs

DAILLRIG Hollow Stem	SURFAC	E ELEVATION		LOGGED BY JCW					
DEPTH TO GROUNDWATER AS Noted	BORING	DIAMETER	811			DATE OF	ULLED	7/30/	/86
DESCRIPTION AND CLASSIFIC	ATION			DEPTH	LER	SSIVE GTH	۲ (%) ۲	<u>ک</u> لار	TION NCE (FT.)
DESCRIPTION AND REMARKS	COLO	CONSIST.	SOIL TYPE	(FEET)	SAMP	UNCONF COMPRE STREN	WATI	DENSI	PENETRA RESISTA
ASPHALT AND BASE ROCK									
SILTY CLAY (FILL)	dark brow	firm	CL	-					
SILTY SAND (old trench backfill)	gray to tan	loose	SM·						
SILTY CLAY with rock fragments	tan to ligh brow	fine to tstiff	CL						
Large angular cobbles SANDY CLAY, grading to clayey sand and gravel No product odor	tan to. ligh brow	very stiff	CL- SC						
		1		20 -					
		EXPL	TORY	BC	RING	LOG			
		M( 35	OIL C AVENUE	OR	PORAT	CION ND	*		
	e H	ROJEGT NO. 182-20	-	DATE 8/86		80	BORING NO. MW-1		

DRILLRIG Hollow Stem	SURFACE	ELEVATION		•	L	LOGGED BY JCW				
DEPTH TO GROUNDWATER As Noted	BORING	IAMETER	811		D,	ATE DF	ILLED	7/30	/86	
DESCRIPTION AND CLASSIFIC	CATION		<del></del>	DEPTH	PLER	RESSIVE RESSIVE NGTH SF)	ter NT (%)	AY SITY CFJ	RATION TANCE (S/FT.)	
DESCRIPTION AND REMARKS	COLOR	CONSIST.	SOIL TYPE	(FEET)	SAM	COMPF STRE (K	CONTE	O N O	PENET RESIS (BLOW	
SANDY CLAY, grading to clayey sand and gravel (contd)			CL- SC							
SILTY CLAY, with some occasional sand and fine gravel No product odor			CL							
	<u> </u>	EXPI	LORA		BO	RING		<u> </u>		
•		M 3	OBIL 5TH	OIL ( AVENUE	IORI	PORATION OAKLAND				
	P	182-20		DATE 8/86	5	- 80	DRING NO.	MW-1		

DRILLRIG Hollow Stem	SURFACE	ELEVATION	** **		T	LOGGE	DBY	JCW	
DEPTH TO GROUNDWATER AS Noted	BORING		8''			DATE DRILLED		7/30/	/86
DESCRIPTION AND CLASSIFIC	CATION			DEPTH	LER	FINED SSIVE GTH	ER T (%)	کتار ال	VTION VNCE /FT.)
DESCRIPTION AND REMARKS	COLOR	CONSIST.	SOIL TYPE	(FEET)	dmbs	UNCONF COMPRE STREN	WATI	DENS	PENETRA RESISTA
SILTY CLAY, with some occasional sand and fine gravel (Contd)			CL						
TOTAL DEPTH = 45.0 feet				45					
		EXPI	ORA	TORY	B	ORING	G LOG	ì	
•		M 3	OBIL 5TH	AVENU	COI E,	APORA OAKL	TION AND	*	
	P H	PROJECT NO.         DATE           H182-20         8/86					BORING NO. MW-1		

## MOBIL OIL CORPORATION OAKLAND, CALIFORNIA

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#### MW-1

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Well completed to 45.0 feet in depth with 2-inch Class 160 PVC casing, flush-threaded joints. Screen (.020inch slot) set from 10.0 to 45.0 feet. 6 X 12 Monterey sand placed from 4.5 to 45.0 feet and concrete seal placed from 0 to 4.5 feet.

DRILL RIG Hollow Stem	SURFACE ELEVATION					T	LOGGED BY JCW				
DEPTH TO GROUNDWATER As Noted	во	RING DI	AMETER	811			DATE	DRILLED	7/31	./86	
DESCRIPTION AND CLASSIFI	CAT	ION			DEPTH	LER	FINED	F) FER 4T (%)	۲ 117 17	ATION ANCE S/FT.)	
DESCRIPTION AND REMARKS	С	OLOR	CONSIST	SOIL TYPE	(FEET)	SAME	UNCON COMPRI	(KS WAT CONTER	DENS PENS	PENETR RESIST (BLOW!	
ASPHALT AND BASE ROCK											
SILTY CLAY with rock frag- ments, dry	d g	ark ray	stiff	CL							
Decreasing rock fragments (very faint"old" product odor)	b: g:	lue- reen									
, Large angùlar gravel, damp No product odor SILTY CLAY; damp	t.t.1 b	an o ight rown	stiff	GL- GC							
	MOBIL OLL CODDODATION					à 					
			м 3	MOBIL O 35TH AV			OAK	AKLAND +			
	٠	PA H1	0JECT NO. 82-20	DATE 8/86.				BORING NO. )	MW-2		

DRILLRIG Hollow Stem	ຣບຄ	RFACE	ELEVATION				LOGGED BY JCW				
DEPTH TO GROUNDWATER As Noted	во	RING DI	AMETER	8''			DATE D	RILLED	7/31/	/86	
DESCRIPTION AND CLASSIFIC	CATI	ON			DEPTH	LER	FINED ESSIVE VGTH	ER 11 (%)	۲ التر ا	ATION ANCE S/FT.)	
DESCRIPTION AND REMARKS	c	OLOR	CONSIST.	SOIL TYPE	(FEET)	SAMF	UNCON COMPRI STREN (KS	WA1 CONTER	DENG	PENETR RESIST (BLOW:	
SILTY CLAY (CONTD)	t: t: 1: b:	an o ight rown	stiff	CL							
SILTY CLAY with some fine sand and gravel (faint odor in sample above water table) ,	m b g t b	otld lue- ray o rown	stiff	CL- SC							
TOTAL DEPTH = 35.0 feet					- 35						
		<b>h</b>	EXPL	.ORA	TORY	B	ORING	LOG	<i>-</i>		
•		MC 3 5			OIL C AVENUE	OF	ORPORATION , OAKLAND .				
		PAC H18	DJECT NO.	. DA1 8			80	DRING NO.	MW-2		

## MOBIL OIL CORPORATION OAKLAND, CALIFORNIA

*i*.

#### MW-2

Well completed to 35.0 feet in depth with 2-inch Class 160 PVC casing, flush-threaded joints. Screen (.020inch slot) set from 10.0 to 35.0 feet. No. 3 Monterey sand placed from 4.5 to 35.0 feet, bentonite pellets placed from 4.0 to 4.5 feet, and concrete seal placed from 0 to 4.5 feet.

DRILL RIG Hollow Stem	SUR	RFACE ELEVATION					LOGGED BY JCW					
DEPTH TO GROUNDWATER As Noted	воя	ING DI	AMETER	8''			DATE DRILLED 7/3			'86		
DESCRIPTION AND CLASSIF		DN		·	DEPTH	IPLER	NFINED	57) TER NT (%)	RY ISITY CF)	RATION TANCE (S/FT.)		
DESCRIPTION AND REMARKS		OLOR	CONSIST	SOIL TYPE	(FEET)	SAN	UNCOI COMPE STRE	CONTE	0 Å 0	PENET RESIS (BLOV		
ASPHALT AND BASE ROCK												
SILTY CLAY with rock fragments	te	in	stiff	CL								
Large angular cobbles			dense	CL- GC	 5 							
SILTY CLAY, damp	ta	an C	stiff	CL								
Trace of gravel; moisture in fissures (No product odor)		ight rown	EXP	CL GC		ľ B	ORIN	G LOO				
	-		M	MOBIL OIL			RPOR	ATION	*			
		PR	OJECT NO.		DAT	E		BORING				
		Hl	8.2-20		8/86			NO.	MW-3			

DRILLRIG Hollow Stem	SURFACE ELEVATION -						LOGGED BY JCI			
DEPTH TO GROUNDWATER As Noted	BOR	ING DI	AMETER	8"			DATE DF	HLLED	7/31/	/86
DESCRIPTION AND CLASSIFIC	CATIC	)N			DEPTH	PLER	LFINED ESSIVE NGTH SF)	TER NT (%)	۲ ک تع	RATION FANCE S/FT.)
DESCRIPTION AND REMARKS	cc	LOR	CONSIST	SOIL TYPE	(FEET)	SAM	UNCON COMPR STRE	WA-CONTE	DEN DI	PENETP RESIST (BLOW
SILTY CLAY (CONTD) with a trace of gravel	ta to li br	n ght own	stiff	CL						
No product odor					   -25			<u> </u>		
Increasing gravel			medium dense	CL- GC						
Decreasing gravel	-		hard	CL		• •				
Gravelly, increasing toward total depth				CL- GC						
TOTAL DEPTH = 35.0 feet					- 35   					
	 				   					```
	ŀ		EXPI	DBIL	ATORY	B COF	ORING	LOG	à	
·	·		35	TH AVENUE			, OAKLAND -			
	ŀ	PR H1	0JECT NO. .82-20	DATE			<sup>B</sup>	(W - 3		

# MOBIL OIL CORPORATION OAKLAND, CALIFORNIA

### MW-3

Well completed to 35.0 feet in depth with 2-inch Class 160 PVC casing, flush-threaded joints. Screen (.020inch slot) set from 10.0 to 35.0 feet. No. 3 Monterey sand placed from 5.5 to 35.0 feet, bentonite perfets placed from 5.0 to 5.5 feet, and concrete seal placed from 0 to 5.0 feet.

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AL LO BO	tor g c Rin	I G		SCIENCE, In LORATORY	с.		<b>)</b>	PROJECT NO. CLIENT <u>BP</u> LOCATION <u>LOGGED BY</u>	<u>30-0</u> Oil Co 3201 3 M. Ta	81-01 Mpany 5th Ave vior	DATE_DRILLED_2/26/91 Oakland APPROVED BY M. Hopwood	BORING NO. SB-9 WELL NO. MW-9
FIELC	SKE	TC	I OF	BORING LOCATI	ON							Page 2 of 2
TOP	DF C	ASIN	ig Ei	EVATION <u>166</u>	.20'			DRILLING MET SAMPLER TYP CASING DATA DRILLER <u>Soll</u>	HOD <u>See v</u> 	Hollow odifled well co loration	stem auger HOLE DI split spoon nstruction detail s Services, Inc.	AM. <u>8"</u>
Ę.	5		Ŧ	P CLO			<u>W</u>	ATER LEVEL				
E Lo	(PPI	튁	<b>F</b>	<b>漢운 문</b>	4	ц.		ATE				
<b>H</b> X	Sal	3		CONSCIENT.	nec	£₽			l		DESCRIPTION	
6,12,17		Ţ	- 36		CL		SI	LTY CLAY: reddish	n brown	, satura	ted to wet, very stiff, medium	plasticity
							B	ORING TERMINATI	EDATS	36.5 FEE	T BELOW GRADE	
			. 30									
			- 40									
			- 42									
		·	44									
			- 46									
			48									
			- 50									
			- 52 -									
			- 54									
			- 56									
			- 58									
			- - 60									ŕ
	ļ			l								
						XXX 1555	н 23 1 1 1	<sup>3</sup> ortland Cement Sand #3 Lonestar 3entonite Pellets		₽ U	Sample Driven interval Water level encountered dur	ing drilling



ALTON GEOSCIENCE, Inc. LOG OF EXPLORATORY BORING       PROJECT NO30-081-01 DATE DRILL CLIENT _BP OIL Company LOCATION _3201 35th Ave., Oakland LOGGED BY _M. Taylor APPROVED BY         FIELD SKETCH OF BORING LOCATION       DRILLING METHOD _Hollow stem auger SAMPLER TYPEModified split spoon CASING DATA _See well construction deta DRILLER _Solls Exiplorations Services, Inc         TOP OF CASING ELEVATION167.01'       WATER LEVEL DATE	ED <u>2/27/91</u>	BORING NO.
FIELD SKETCH OF BORING LOCATION         DRILLING METHOD Hollow stem auger         SAMPLER TYPE         SAMPLER TYPE         Modified split spoon         CASING DATA         See well construction deta         DRILLER         Solis         E         E         E         E         E         E         E         E         E         E         E         E         E         E         E         E         E         E         E         E         E         E         E         E         E         E         E         E         E         E         E         E         E         E         E         E         E         E         E         E         E         E         E	M. Hopwood	WELL NO. MW-10
TOP OF CASING ELEVATION		Page 2 of 2
SAMPLER TYPEModified split spoon CASING DATA _See well construction deta DRILLER _Soils Exiptorations Services, Inc         U       U       E       U       U       E       U       U       E       U       U       E       U       U       E       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       U       <	HOLE DIAN	A8"
TOP OF CASING ELEVATION 167.01'       CASING DATA See well construction deta DRILLER Soils Exiplorations Services, Inc         Image: Second Service		
Image: Second and the second and t	<u>I</u>	
H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H     H <th></th> <th></th>		
Image: Second		
Image: Second		
Total     Total     Total       7,8,11     -36     CL     SILTY CLAY: brown, wet, very stiff, medium plasticit       -38     -38     BORING TERMINATED AT 36.5 FEET BELOW GRAD       -40     -42     -42		
BORING TERMINATED AT 36.5 FEET BELOW GRAD		
- 38 - 40 - 42	/, with some tin	le sand
- 40 - 42 -	E	
42		
· - 44	··· ··	
- 46		
- 50		
- 52		
54		į
- 58		
Portland Cement Sample		
Sand #3 Lonestar Driven interval		
Bentonite Pellets Set Water level enc		

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ALT LOC BOI	roi g C Rin	n G )F E IG	ieo Exp		)E, Ind ORY	с. 8		PROJECT NO. <u>30-081</u> DATE DRILLED <u>1/29/90</u> CLIENT <u>BP OIL COMPANY</u> LOCATION <u>3201 35TH AVENUE, OAKLAND, CA</u>	BORING NO, WELL NO.
FIELD	SKE	TCI	HOF	BORING L	OCATIO	ON		LOGGED BY <u>M. TAYLOR</u> APPROVED BY	RW-1
TOP C	)F C,	ASII	NG E	LEVATION	168.	01		DRILLING METHOD HOLLOW-STEM AUGER HOLE DIA SAMPLER TYPE CASING DATA SEE MONITORING WELL CONSTRUCTIO DRILLER WEST HAZMAT	N DETAIL
	Ŵ		H	CTON 6			4	WATER LEVEL 27.93	
ows ot(n	1 (PP	MPLE			22	8	렸는	TIME	
<b>a</b> 2	ទ	SAI		HEL CON ORE	ลั ช	ğ	*	DESCRIPTION	
			-0	Christy Bo	X			ASPHALT	
			-2	Portland				SILTY CLAY; gravels, brown, damp, backfill	
9,19, 33	0		- 4 - 6	Cement Bentonite	33 E8	a		SILTY CLAY; gravelly, greenish brown, dry to damp, low plat present	sticity, odor
16,33, 40	0		-8 -10 -12	6" sch		a		SILTY CLAY; gravely, greenish brown, dry to damp, mediun odor present	n plasticity,
15,36, 43	0		- 14 - 16	6"		a		SILTY CLAY; gravelly, brown, damp, medium odor present	
.11,16, 25	0	T	- 18 - 20 - 22	PVC ,020 Slot		a		SILTY CLAY; gravelly, brown, damp, medium plasticity, odo present	r
6,7, 16	0	H	- 24 - 26 - 28	Sand #3 Lonestar		a		SILTY CLAY; sandy gravelly, greenish brown, medium plasticity	
6,13, 17	0		- - 30			a	// s	SILTY CLAY; gravelly, sandy (fine) brown, saturated very stift	
			- 32 - 34						

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			L	.OG OF	= B	ORI	NG	ì
	1333 Broadway,	Suite 800	Borehol	e ID: UB	-1			
	Oakland, Californ	nia 94612	Total De	epth: 48 f	ft. bį	gs		
PROJI	ECT INFORMATION		DF	RILLING I	NFC	RMAT	ION	3
Project: BP #11132	Soil and Water Investigation	Drilling	Company	Gregg Dril	ling	& Testi	ng	
Site Location: 320	1 35th Avenue, Oakland, CA	Driller:	Dustin Tidy	well				······································
Project Manager: Leonard Niles Type of Drilling Rig: CPT								
RG: Leonard Niles	RG: Leonard Niles Drilling Method: Direct Push							
Geologist: Kevin U	no	Sampl	ing Method	: Groundwa	ter G	irab		<u></u>
Job Number: 3848	6822.0013001	Date(s)	) Drilled: 7/2	2/04				,,,,,,
	BC	RING INFORMA	TION					
Groundwater Dept	h (ft bgs): Unknown, <48 ft. bgs.	Boring	Location:	78 ft S of SV	V cor	mer of N	Aang	els Ave. and 35th Ave.
Air Knlfe or Hand Auger Depth: 5.0 feet bgs Boring Diameter: 2-i				2-inch				
Coordinates: Latitude Longtitude Boring Type: Exploratory								
Depth (ft bgs) Symbol	Lithologic Descri	ption		Blow Count	USCS	PiD (ppm)	Recovery	Sample ID/ Comments
2 4 4 6 10 12 14 16 18 20 22 24 24 26 28 10 10 12 14 16 18 20 12 14 20 21 22 24 24 26 28 28 20	Air knife to 5 ft. bgs Boring not lithologically logged. Pur depth discrete soil samples and gro boring UB-2 for lithology.	pose of boring was to undwater grab sample	collect . See					Borehole grouted to grade with Portland neat cement.



				1	LOGC	FE	BORI	NG	ì
	~	1333 Broadway, Suite 8	00	Boreho	le ID: U	B-2			
		Oakland, California 946	12	Total D	epth: 48	Sft. b	gs		
PI	ROJE	ECT INFORMATION		D	RILLING	INF	ORMA	TION	4
Project: BP #	11132	Soil and Water Investigation	Drillin	g Company	: Gregg Di	rilling	, & Testi	ng	Malastan ana ang Malamatan ang panganan ang pang ang pang pang p
Site Location: 3201 35th Avenue, Oakland, CA Drille					lwell				
Project Manager: Leonard Niles Type of Drilling Rig: CPT									
RG: Leonard N	liles		Drillin	g Method:	Direct Push	1			
Geologist: Ke	vin Uı	no	Sampl	ing Metho	<b>d:</b> Groundv	vater (	Grab		
Job Number:	38480	5822.0013001	Date(s	) Drilled: 7/	22/04				
	· · · · · · · · · · · · · · · · · · ·	BORING IN	FORMA	TION					
Groundwater	Dept	h (ft bgs): Unknown, <48 ft. bgs	Boring	Location:	155 ft S of	SW (	corner of	f Mar	igels Ave. and 35th Ave.
Air Knife or H	and A	Auger Depth: 5.0 feet bgs	Boring	Diameter:	2-inch				
Coordinates:	La	atitude Longtitude	Boring	Type: Exp	loratory				
Depth (ft bgs)	Symbol	Lithologic Description			Blow Count	nscs	PID (ppm)	Recovery	Sample ID/ Comments
4 4 6		Note: Lithology is interpreted from CPT logs. S observed. Air knife to 5 ft. bgs CLAYEY SILT SILT CLAYEY SILT	oll not visu	ially		ML			Borehole grouted to grade with Portland neat cement
- 8 	AA AA	STIFF FINE GRAINED: -undifferentiated SILTY CLAY CLAYEY SILT				CL			
- 12		SILTY CLAY SILT CLAYEY SILT				CL ML			
URS C	corp	oration Page	1 of 3				Boreho	ole l	D: UB-2

UR		LOG OF BORING	ł	Bor	ehole	ID:	UB-2
Depth (ft bgs)	Symbol	Lithologic Description	Blow Count	nscs	(mqq) Olq	Recovery	Sample ID
- 16		STIFF FINE GRAINED					
- 18		SILTY CLAY		CL			
20		CLAY STIFF FINE GRAINED					
- 22		SILTY CLAY					
24		CLAYEY SILT SILTY CLAY CLAY CLAYEY SILT		ML CL ML			
- 26	, , , , , ,	STIFF FINE GRAINED CLAYEY SILT CLAY		CL			
28		CLAYEY SILT SILT CLAYEY SILT SILTY CLAY		ML CL			
- 30		STIFF FINE GRAINED CLAY					
32	<i>XA</i>	SILTY CLAY CLAYEY SILT		ML			
- 34		SANDY EU T		SM			
36		STIFF FINE GRAINED			Boroh		

UR		LOG OF BORING		Bore	ehole	ID:	UB-2
Depth (ft bgs)	Symbol	Lithologic Description	Blow Count	uscs	(mqq) Olq	Recovery	Sample ID
		SILTY CLAY CLAYEY SILT STIFF FINE GRAINED SILTY CLAY		CL ML CL			
40 		CLAYEY SILT SILT		ML			
- <b>44</b>		CLAYEY SILT STIFF FINE GRAINED CLAYEY SILT STIFF FINE GRAINED					
46		SILTY CLAY STIFF FINE GRAINED SAND: Cemented. CLAYEY SILT SILT: Bottom of boring: 48 ft.bgs		CL SM ML			UB-2-48: Groundwater grab sample at 48 ft, bgs.

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	26	1333 Br	adway. Suite 80							
UI	K,		California 0464	12	Boreho		<u>в-3</u>			
			, camornia 940°	<b>Control Depth:</b> 48 ft. bgs						
PF	<b>SOJE</b>	CT INFORMATION	N		D	RILLING	INFO	ORMAT	TION	1
Project: BP #1	1132	Soil and Water Investig	gation	Drilling	) Company	y: Gregg Di	rilling	& Testu	ng	
Site Location:	3201	35th Avenue, Oakland	, CA	Driller: Dustin Tidwell						
Project Manag	jer: L	eonard Niles		Туре о	f Drilling F	Rig: CPT				
RG: Leonard N	liles			Drilling	3 Method:	Direct Push	h			
Geologist: Ke	vin Un	10		Sampl	ing Metho	d: Groundv	water (	Grab		
Job Number:	38486	822.0013001		Date(s	) Drilled: 7/	/22/04				
			BORING IN	FORMA	TION					
Groundwater	Depti	Depth (ft bgs): Unknown, <48 ft. bgsBoring Location: 182 ft S of SW corner of Mangels and 35th Ave.				gels and 35th Ave.				
Air Knife or Hand Auger Depth: 5.0 feet bgs Boring Diameter: 2-inch										
Coordinates:	La	ititude Lon	gtitude	Boring	Type: Exp	loratory				
ŝ						t		î.		
(ft bg	Į	E IALAN	Madic Description			Cou	SCS	(ppr	over	Sample ID/ Comments
ŧ	Ущt	հառ				3low	15	ПЧ	Rec	Completing
De	٥,					Ľ				
E 0										
Ē										Borehole grouted to grade with Portland
										neat cement
Ę		Air knife to 5 ft. bgs								
E 4		۱				}				
Ē		Boring not lithological	ly logged. Purpose of born nples and groundwater or	ing was to ab sample	collect					
Ē		boring UB-2 for litholo	gy.	•				ļ		Į
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E 30						<u> </u>		-	L-estade	
	:orn	oration	Pade	1 of 2				Boreh	ole I	D: UB-3
	vorp		1 690						-	

<b>URD</b>	URS
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# LOG OF BORING

### Borehole ID: UB-3

Depth (ft bgs) Svmhof	Lithologic Description	Blow Count	nscs	PID (ppm)	Recovery	Sample ID
32 34 36 38 40 42 44 46 48			CL			UB-3-30.5 UB-3-48: Groundwater grab sample at 50 ft. bgs,

				LOG C	)FE	BORI	NG				
	1333 Broadway, Suite 8	00	Boreho	le ID: U	<b>B-4</b>			/ Li ,			
	Oakland, California 946 <sup>°</sup>	12	Total D	epth: 5	) ft. t	ogs					
PROJECT IN	FORMATION		D	RILLING	INF	ORMA	TIO	V			
Project: BP #11132 Soil an	d Water Investigation	Drilling	Company	y: Gregg D	rilling	& Testi	ng	· · · · · · · · · · · · · · · · · · ·			
Site Location: 3201 35th A	venue, Oakland, CA	Driller:	Dustin Tic	iwell							
Project Manager: Leonard	Niles	Type o	f Drilling F	Rig: CPT							
RG: Leonard Niles		Drilling Method: Direct Push									
Geologist: Kevin Uno		Sampli	ing Method	<b>d:</b> Groundv	vater	Grab					
Job Number: 38486822.00	13001	Date(s	) Drilled: 7/	21/04							
	BORING IN	FORMA	ΓΙΟΝ								
Groundwater Depth (ft bg	<b>js):</b> Unknown, < 50ft. bgs	Boring	Location:	135 ft E of	f E co	rner of S	choo	l St. and 35th Ave.			
Air Knife or Hand Auger I	Depth: 5.0 feet bgs	Boring	Diameter:	2-inch	<b></b>						
Coordinates: Latitude	Longtitude	Boring Type: Exploratory									
Depth (ft bgs) Symbol	Lithologic Description			Blow Count	USCS	(mqq) Olq	Recovery	Sample ID/ Comments			
Air kni 2 Air kni 6 Boring depth boring 10 11 12 14 14 16 18 20 16 18 20 10 22 14 26 28 30	ife to 5 ft. bgs not lithologically logged. Purpose of bori discrete soll samples and groundwater groundwa	ing was to ab sample.	collect See					Borehole grouted to grade with Portland neat cement			
URS Corporation	on Page 1	of 2			E	Boreho	ole II	D: UB-4			
UR		5	LOG	OF BORIN	IG	Borehole ID: UB-4					
--------------------------------------------------------------------	--------	---------	----------------	-------------	----	-------------------	------	-----------	----------	------------------------------------------------------------------------------	--
Depth (ft bgs)	Symbol	Lith	ologic Descrip	tion		Blow Count	USCS	PID (ppm)	Recovery	Sample ID	
132 134 136 138 140 142 144 146 148 150							CL			UB-4-30.0 UB-4-30.5 UB-4: Groundwater grab sample at 50 ft. bgs.	
URS C	orpo	pration		Page 2 of 2			E	Boreho	le IC	D: UB-4	

TTD	C 1333 Broadway Suite 8	00	L	.060	1- E	SOR	INC	5	
UR	Oakland, California 946	12	Borehol	e ID: UI	<u>B-5</u>				
		12.	Total De	epth: 50	ft. b	gs			
PROJ		ļ	DR	RILLING	INF	ORMA	TIO	<u>N</u>	
Project: BP #1113	2 Soil and Water Investigation	Drilling Company: Gregg Drilling & Testing							
Site Location: 320	01 35th Avenue, Oakland, CA	Driller: Dustm Tidwell							
Project Manager:	Leonard Niles	Турео	of Drilling Ri	Ig: CPT				······································	
RG: Leonard Niles	· · · · · · · · · · · · · · · · · · ·	Drilling	g Method: D	virect Push					
Geologist: Kevin U		Sampl	ing Method	: Cone Pen	trom	eter Tes	ting		
JOD NUMBER: 3848	86822.0013001	Date(s	) United: //2	.2/04					
Groundwater Den	th (ft has). Unknown < 50 ft has	Boring	Location: /	Approx 60	θF	ofFcor	maro	f School St and 25th A-	
Air Knife or Hand	Auger Denth: 5.0 feet bas	Boring	Diameter:	-inch					
Coordinates: 1	atitude	Boring	Type: Explo	oratory					
			- Jpo: 2npic	1			1		
Depth (ft bgs) Symbol	Lithologic Description			Blow Count	nscs	PID (ppm)	Recovery	Sample ID/ Comments	
	Air knife to five feet bgs. Note: Lithology is interpreted from CPT logs. Sobserved.	oil not visu	ally		SM			Borehole grouted to grade with Portland neat cement	
URS Corp	l Page 1	l of 3	I		E	Boreho	l le ll	D: UB-5	

UF	2	LOG OF BORING	_	Borehole ID: UB-5						
Depth (ft bgs)	Symbol	Lithologic Description	Blow Count	USCS	PID (ppm)	Recovery	Sample ID			
E E										
⊢ 16 ⊑										
F										
E										
E 18	CENT.	SILTY CLAY		]						
	14.7	STIFF FINE GRAINED								
Ē										
- 20		SILTY CLAY								
F		CLAY								
		CLAYEY SILT		ML						
- 22		SILT								
2	H.	SILTY CLAY								
Ē		CLAYEY SILT		ML						
					-					
- 24				CL						
È		CLAY				1				
Ē				L						
E			1	) ML		Ì				
- 26	<u>، ،</u>					Į				
E		SILT								
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- 28	Ļ			ļ						
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<u>k</u>	1 ·			{						
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F 30	[·	•		}		}				
	STAT					İ				
È.		SILIY CLAY								
Ē	H									
- 32						1				
E		SAND: Compared		GN4						
F					}	1				
Ę				IVIL.						
- 34										
F	157159	SILTY CLAY			ł		)			
E	12				{					
F					ļ	ļ				
- 36										
URS	Corp	oration Page 2 of 3		i	Boreho	ole li	D: UB-5			

Image: Second	UR		LOG OF BORING		Bor	ehole	ID:	UB-5
40     STIFF FINE GRAINED       33     SILT       40     SULT       41     STIFF FINE GRAINED       42     STIFF FINE GRAINED       44     CLAYEY SILT       51     SILT	Depth (ft bgs)	Symbol	Lithologic Description	Blow Count	nscs	(mqq) Olq	Recovery	Sample ID
40     SILTY CLAY       STIFF FINE GRAINED       CLAYEY SILT       STIFF FINE GRAINED       44       CLAYEY SILT       SILT       46       CLAYEY SILT       SILT       48       SILT       CLAYEY SILT       SILT       50	38		CLAYEY SILT STIFF FINE GRAINED SILT					
44       CLAYEY SILT         SILT         46       CLAYEY SILT         48       SILT         CLAYEY SILT         STIFF FINE GRAINED         CLAYEY SILT: Bottom of boring: 50 ft. bgs	40 ×		SILTY CLAY STIFF FINE GRAINED CLAYEY SILT STIFF FINE GRAINED		CL ML			
46       CLAYEY SILT         48       SILT         CLAYEY SILT         STIFF FINE GRAINED         GLAYEY SILT: Bottom of boring: 50 ft. bgs         50	<b>44</b>		CLAYEY SILT SILT					
Grad sample at 50 ft.       S1       CLAYEY SILT: Bottom of boring: 50 ft. bgs       50	46		CLAYEY SILT SILT CLAYEY SILT STIFF FINE GRAINED					UB-5: Ground water
	50		CLAYEY SILT: Bottom of boring: 50 ft. bgs					grab sample at 50 ft. bgs.

TTDC 1333 Broadway Suite 800						SORI	NG			
	Oakland California 9464		Boreho	ble ID: UB-6						
		Z	Total D	epth: 5(	) ft. b	ogs				
PROJ	ECT INFORMATION		D	RILLING	INF	ORMA	TION	١		
Project: BP #1113:	2 Soil and Water Investigation	Drilling	Company	ompany: Gregg Drilling & Testing						
Site Location: 320	11 35th Avenue, Oakland, CA	Driller:	Dustin Tid	well						
Project Manager:	Leonard Niles	Type o	f Drilling R	lig: CPT		. <u> </u>				
RG: Leonard Niles		Drilling	Method: I	Direct Push	1					
Geologist: Kevin U	Jno	Sampli	ng Method	i: Groundy	vater (	Grab				
Job Number: 3848	36822.0013001	Date(s)	Drilled: 7/	21/04						
BORING INFORMATION										
Groundwater Depth (ft bgs): Unknown, < 50 ft. bgs. Boring Location: 20 ft. E of E corner of School St. and 35th										
Air Knife or Hand	Auger Depth: 5.0 feet bgs	Boring	Diameter:	2-inch						
Coordinates: L	atitude Longtitude	Boring	Type: Expl	oratory						
Depth (ft bgs) Symbol	Lithologic Description			Blow Count	nscs	PID (ppm)	Recovery	Sample ID/ Comments		
and a second sec	Air knife to 5 ft. bgs Boring not lithologically logged. Purpose of borin depth discrete soil samples and groundwater gra boring UB-5 for lithology.	ng was to d	collect See					Borehole grouted to grade with Portland neat cement		
URS Corr	poration Page 1	of 2				Boreho	ole II	D: UB-6		



Depth (ft bgs)	Symbol	Lithologic Description	Blow Count	nscs	(mqq) Olq	Recovery	Sample ID
32 34 36 38 40 42 44 44 50		SILTY CLAY: Light brown with 5-10% fine sand. Moist, Stiff. Low o medium plasticity.		CL			UB-6-30.5 UB-6-30.5 UB-6: Groundwater grab sample at 50 ft. bgs.

	l	<u>_OG 0</u>	FE	BORI	NG			
	1333 Broadway, Suite 80	10	Boreho	le ID: U	<b>B-7</b>			
	Oakland, California 946	12	Total D	epth: 41	.5 fe	et bgs		
PROJECT	NFORMATION		DI	RILLING	INF	ORMA'	TION	1
Project: BP #11132 Soil a	and Water Investigation	Drilling Company: Gregg Drilling & Testing						
Site Location: 3201 35th	Avenue, Oakland, CA	Driller: Paul Rodgers						
Project Manager: Leonar	rd Niles	Туре о	of Drilling R	Rig: Geopro	be			
RG: Leonard Niles Drilling Method: Direct Push								
Geologist: Joe Gonzales		Sampl	ing Method	d: Continuc	ous co	ore with	acetat	te sleeve.
Job Number: 38486822.0	0013001	1/19/04		· ···		··· -		
	BORING IN	FORMA	TION					
Groundwater Depth (ft b	bgs): 36 feet bgs	Location:	10 feet sou	th of	RW-1			
Air Knife or Hand Auger	r Depth: 5.0 feet bgs	Boring	Diameter:	2-inch				
Coordinates: Latitud	le Longtitude	Boring	Type: Expl	loratory				
Depth (ft bgs) Symbol	Blow Count	nscs	(mqq) CII	Recovery	Sample ID/ Comments			
Air k Air k Med stiff 10 SAN sand odor V.X. sand SAN SAN SAN SAN SAN SAN SAN SAN	AVELLY SANDY SILT: orangish brown, 50% flum to coarse sand, 20% fine subangular g to stiff, damp, increasing gravel with depth NDY GRAVELLY SILT: brown, 50% silt, 15% d, 35% fine to coarse subangular gravel, sti ngish brown, decreasing gravel and sand, so r des to clay NDY GRAVELLY CLAY: brown, 50% clay, 2 d, 30% fine to coarse subangular to subrour , damp, slight odor te as above, mostly fine gravel, odor	% silt, 30% rravel, mec 6 fine to co ff, damp ome clay, s 00% fine to nded gave	dum barse slight coarse l, very		ML CL	0.8		Borehole grouted to grade with Portland neat cement UB-7-5 UB-7-15
28	tion	1 of 2				Boreh		D: 1/B-7



1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Deput (R. ngs)	Symbol	Lithologic Description	Blow Count	nscs	PID (ppm)	Recovery	Sample ID	
	32 34 36 38 40		SANDY GRAVELLY CLAY: brown, 50% clay, 15% fine to coarse sand, 35% fine gravel, very stiff, damp decreasing gravel Increasing gravel and coarse sand SANDY GRAVELLY SILT: dark brown, 50% silt, 15% sand, 35% gravel, stiff to very stiff, wet Increasing coarse sand with depth decreasing gravel, medium stiff, saturated, geoprobe refusal at 41.5 feet bgs		CL ML	70 17 12		UB-7-35 UB-7 (hydropunch) <sup>SZ</sup> UB-7-41	r -

						LOG C	) <u>F</u> [	<b>30</b> RI	NG						
			1333	Broadw	ay, Suite 80	00	Borehole ID: UB-8								
			Oaki	and, Call	fornia 946'	12	Totai E	tal Depth: 3.5 feet bgs							
P	ROJ	ECT IN	FORM/	ATION			DRILLING INFORMATION								
Project: BP	411132	Soil and	d Water I	nvestigation		Drilling Company: Gregg Drilling & Testing									
Site Location	n: 3201	35th Av	venue, O	akland, CA		Driller: Paul Rodgers									
Project Mana	iger: I	Leonard ]	Niles		·····	Туре о	f Drilling I	Rig: Vacma	sters	4000					
RG: Leonard	Niles					Drilling	Method:	Air knife							
Geologist: Joe Gonzales Sampling Method: NA															
Job Number: 38486822.0013001         Date(s) Drilled: 04/19/04															
					BORING IN	FORMA	TION			·					
Groundwater	Dept	h (ft bgs	s): Unkn	iown		Boring	Location:	Near UST	pad						
Air Knife or I	Hand /	Auger D	Septh: 3.	5 feet bgs		Boring	Diameter:	<u>6"</u>		·····					
Coordinates: Latitude Longtitude				Boring	iype: Exp	ioratory									
Depth (ft bgs)	Symbol			Lithologic D	escription			Blow Count	nscs	(mqq) Ol9	Recovery	Sample ID/ Comments			
ն ամացել	02020	GRAVE clear h	EL: Air kr ole to five	nife to 3.5feet b a feet. Abando	ogs: Gravel with conned boring.	obbles. C	ould not					No samples taken Borehole grouted to grade with Portland neat cement			

TTDC 1333 Broadway, Suite 800						LOGC	)F I	BORI	NG	)		
			Oakland, California 946	12	Boreho	Depth: 42.5 foot has						
					I otal L	Deptn: 42.5 feet bgs						
P	ROJE			Deillie	D	DRILLING INFORMATION						
Project: BP #	11132	Soil and	water Investigation	Drilling	g Company	Company: Gregg Drilling & Testing						
Project Mana	aer: 1	conard N	iles	Type o	f Drilling F	ia. Geopre	he	·				
RG: Leonard I	Viles			Drillin	a Method:	Direct Push	1 1			······································		
Geologist: Joe Gonzales         Sampling Method: Continuous core								ore with	aceta	te sleeve.		
Job Number:	38480	5822.0013	001	Date(s	) Drilled: 0	4/19/04				The Phone Public		
BORING INFORMATION												
Groundwater	Dept	h (ft bgs)	): 40 feet bgs	Boring	Location:	Near west	side o	of station	buil	ding		
Air Knife or H	land A	Auger De	pth: 5.0 feet bgs	Boring	Diameter:	2-inch	<u> </u>					
Coordinates:	La	atitude	Longtitude	Boring	Type: Exp	loratory						
Depth (ft bgs)	Symbol		Lithologic Description			Blow Count	nscs	(mqq) Cl <sup>q</sup>	Recovery	Sample ID/ Comments		
Air knife to five feet bgs										Borehole grouted to grade with Portland neat cement		
aniuuluu luuluu 8		SANDY sand, 30	GRAVELLY SILT: brown, 50% slit, 20% % fine subangular gravel, very stiff, da	6 fine to co mp	Darse		ML	0		UB-9-5		
10 12 12 14		same as increasir	above, with more gravel Ig clay with depth					0				
16 18 18		SANDY to coarse varying a slight od	GRAVELLY CLAY: orangish brown, 50 e sand, 35% fine to coarse sand, stiff to amounts of sand and gravel or	% clay, 15 o very stiff,	5% fine damp,		CL	0.5		UB-9-15		
22 1 1 1 1 22		same as	above, dark brown, decreasing graver arse gravel (4 cm dlameter)					23				
26 28 4 28 4 30		SILTY C sliff, dar	LAY: orangish brown, 60% clay, 40% s np to moist, slight odor, some orange n	silt, mediur nottling	n stiff to		CL	275		UB-9-25		
URS C	corp	oratior	<b>1</b> Page 1	1 of 2			l	Boreho	ole II	D: UB-9		



Depth (ft bgs)	Symbol	Lithologic Description	Blow Count	nscs	PID (ppm)	Recovery	Sample ID
32 100 100 100 100 100 100 100 100 100 10		orangish brown, 50% clay, 30% silt, 10% cs sand, 10% fine sub rounded gravel, stilf, damp to moist some coarse gravel (3 cm diameter) SANDY GRAVELLY CLAY: orangish brown, 50% clay, 15% fine to coarse sand, 35% fine to coarse sand, stiff to very stiff, damp SANDY GRAVELLY SILT: orangish brown, 50% silt, 15% medium to coarse sand, 35% fine to coarse subangular gravel, medium stiff, moist to wet, geoprobe refusal at 42.5 feet bgs		CL	172 24 1.7		UB-9-35 UB-9 :groundwater grab with bailer at 42.5 ft. bgs. UB-9-42

	10	LOG OF BORING								
URD	Oakland California 946	12	Borehole ID: UB-10							
	Culland, Cullionna 540		I otal Depth: 37.5 feet bgs							
PROJECT IN	FORMATION		DRILLING INFORMATION							
Project: BP #11132 Soil and	Water Investigation	Drilling Company: Gregg Drilling & Testing								
Site Location: 3201 35th Av	venue, Oakland, CA	Driller:	Paul Rodg	l Rodgers						
Project manager: Leonard I	dig: Geopre	be								
Goologist: Jos Gonzales	Direct Push			4 - 4						
Job Number: 38486822 001			se with		le sieeve.					
BORING INFORMATION										
Groundwater Depth (ft bg	12 ft. SW o	of sou	ithern di	spens	er					
Air Knife or Hand Auger D	Diameter:	2-inch		<u></u>	-					
Coordinates: Latitude	Boring	Type: Expl	loratory							
Depth (ft bgs) Symbol	<u> </u>		Blow Count	nscs	PID (ppm)	Recovery	Sample ID/ Comments			
Air knif 2 4 6 5 5 6 7 6 7 7 7 7 7 7 7 7 7 7 7 7 7	Y GRAVELLY CLAY: brown to light brown coarse sand, 30% fine to coarse subanguamp, decreasing gravel with depth ing gravel own, very stiff h brown, 55% clay, 20% sand, 25% grave sing gravel ing gravel own, increasing gravel, odor amounts of sand and gravel	n, 50% cla Jar gravel	y, 20% very dor,		CL	0 0 9.0 63 177		Borehole grouted to grade with Portland neat cement. UB-10-5 UB-10-15 UB-10-15		
URS Corporatio	<b>n</b> Page 1	of 2				Boreho	ole IC	D: UB-10		



Depth (ft bgs)	Symbol	Lithologic Description	Blow Count	uscs	PiD (ppm)	Recovery	Sample ID
ահավ 32 34		SILTY CLAY: reddish brown, 60% clay, 40% silt, trace fine to coarse sand and fine gravel, very stiff, damp		CL	0		
սես 36 հուլ		SANDY GRAVELLY CLAY: reddish brown, 50% clay, 15% fine to coarse sand, 35% fine gravel, stiff, damp		CL	0		UB-10-35 UB-10-37 (soil); UB-10 (groundwater grab with bailer)

TTDC 1333 Broadway Suito 800							LOG OF BORING						
	K,		a 04612	Borehole ID: UB-11									
				a 37012	Total	Depth: 3	7.5 f	eet bgs					
PF	ROJE		RMATION		DRILLING INFORMATION								
Project: BP #1	11132	Soil and Wa	ater Investigation	Dril	Drilling Company: Gregg Drilling & Testing								
Site Location:				Dril	er: Paul Roc	lgers		TAPAL (		• • · · · · · · · · · · · · · · · · · ·			
Project Manag	jer: L	eonard Nile	S	Тур	e of Drilling	Rig: Geop	obe						
RG: Leonard N	iles			Dril	ing Method	: Direct Pus	h						
Geologist: Joe	Gonz	ales	-	Sar	pling Meth	od: Continu	ious c	ore with	aceta	te sleeve.			
Job Number:	38480	822.001300	BOE		e(s) Drilled:	04/20/04				······			
Groundwater	Depti	h (ft bgs): 3	36	Bori	ng Location	: Near plan	ter on	35th Av	enue				
Air Knife or H	and A	Auger Depl	<b>h:</b> 5.0 ft. bgs	Bori	ng Diameter	: 2-inch				<u> </u>			
Coordinates:	La	atitude	Longtitude	Bori	n <b>g Type:</b> Ex	ploratory		•••••					
Depth (ft bgs)	Symbol		Lithologic Descript	ion		Blow Count	NSCS	(mqq) CIA	Recovery	Sample ID/ Comments			
0         10         10         11         12         13         14         16         18         20         22         24         26         28		Air knife to SANDY GF sand, 30% slight green same as at increasing e greenish cc SANDY GF silt, 15% fir size is up to SANDY GF sand, 30% decreasing coarse grav SILTY CLA fine gravel,	RAVELLY CLAY: brown, 50 fine to coarse subrounded n color in soil bove gravel, with some coarse gu lor. RAVELLY SILT: reddish bro to coarse sand, 35% fine to coarse sand, 35% fine to 3 cm in diameter, stiff, da RAVELLY CLAY: brown, 50 fine to coarse subrounded gravel with depth vel (4cm diameter) Y: reddish brown, 60% clay very stiff, damp	9% clay, 20% find gravel, very stiff ravel (4 cm diam own to orangish l a to coarse grave imp, slight odor 1% clay, 20% find gravel, very stiff y, 40% slit, trace	eter). No rown, 50% I, gravel to coarse damp, sand and		CL CL CL	0		Borehole grouted to grade with Portland neat coment. UB-11-5 UB-11-15			
	×-/-/	oration		Page 1 of 9				Boreh		D: TIR_11			



Depth (ft bgs) Symbol	Lithologic Description	Blow Count	nscs	PID (ppm)	Recovery	Sample ID
32 34 36	continued increase of sand and gravel SANDY GRAVELLY CLAY: reddish brown, 50% clay, 15% fine to coarse sand, 35% fine to coarse subrounded gravel, moderately stiff, moist to wet, geoprobe refusal at 37.5 feet bgs		CL	1.3 0		UB-11-35 UB-11 (groundwater <sup>-SZ</sup> grab with bailer); UB-11-37 (soil).

LAND C 1222 Broodway Suito 800							<u>) - t</u>	SURI	NG		
	κ.		10	Boreho	le ID: U	<u>B-12</u>					
		Uaki	and, Camornia 540		Total D	epth: 26	5 feet	bgs			
PF	ROJE	CT INFORMA	TION	DRILLING INFORMATION							
Project: BP #1	11132	Soil and Water I	nvestigation	Drilling Company: Gregg Drilling & Testing							
Site Location:	3201	35th Avenue, O	akland, CA	Driller: Paul Rodgers							
Project Manag	ger: L	eonard Niles		Type o	f Drilling F	Rig: Geopro	obe	<u></u>			
RG: Leonard N			<u></u>	Drilling	j Methou:	Direct Pusi	1 	ro with r		e doove	
Geologist: Joc		ales		Date/s	) Drilled 04	4/19/04				C SIECVE.	
JOD NUITBAL	38480		BORING IN	FORMA	TION		···				
Groundwater	Denti	h (ft bas): 25		Boring	Location:	Behind sta	tion b	uilding	near f	ormer dispenser island	
Air Knife or H	and A	Auger Depth: 5.	0	Boring	Diameter:	2-inch			<u> </u>		
Coordinates:	La	titude	Longtitude	Boring	Type: Exp	loratory		···· <u>·</u> ····			
							1				
Depth (ft bgs)	Symbol		Lithologic Description			Blow Count	nscs	PID (ppm)	Recovery	Sample ID/ Comments	
2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		Air knife to five	feet bgs						Borehole grouted to grade with Portland neat cement.		
սհայհում 6 8		SANDY GRAVI sand, 30% fine damp increasing grave	ELLY SILT: brown, 50% silt, 20% subangular gravel, medium stiff al with depth	oarse ff,		ML	0		UB-12-5		
10 12 14		dark brown, 509 subrounded to s	% slit, 15% fine to coarse sand, ubangular gravel, trace clay, ve	35% fine to ery stiff, da	o coarse mp			0		UB-12-10	
14 16 18		SANDY GRAV to coarse sand damp decreasing grav	ELLY CLAY: orangish brown, 50 35% fine to coarse subangular rel and stiffness with depth	)% clay, 18 gravel, ve	5% fine ry stiff,		CL	0		UB-12-15	
20 11 22		brown increasing gravel									
<ul> <li>24</li> <li>ark brown</li> <li>increased coarse sands and gravels</li> <li>SANDY GRAVELLY SILT: light brown, 50% silt, 15% medium to coarse sand, 35% fine to coarse subangular to subrounded cravel medium stiff wat generative at 26 feet bras</li> </ul>							ML	0		UB-12 (groundwater grab with bailer); UB-12-25 (soil).	
	orn	oration	Page	1 of 1				Boreho	ole I	D: UB-12	

PROJECT No. 0152-044.02 DATE 1/22/94 BORING No. FIELD LOG OF CLIENT TOSCO 11132 HP-1 LOCATION 3201 35th St., Oakland, CA **EXPLORATORY BORING** Sheet 1 of Z LOGGED BY D. Galasso 6.51 Drilling Co. Precision N Field location of boring: - HP-1 7 Drill rig model XD1 8' -Drilling method \_\_\_\_\_CPT TEL \_Hole dla. \_2 3/ 9 " Servicesti Ge dispansir lands Boring completion data Grouted hole to surface ST. adding asphalt patch to top on boring Ave, Datum Ground Elev. Depth to ablaDepth to 🔻 Sample Number and Container Type Depth Sampled interval Penetrometer (TSF) Blows/6 in. and/or Pressure (PSI)  $\mathcal{O}$ Graphic Log Well Detall Soll/Rock Symbol Recovery (ft/ft) Type of Sampler Time Time V Date Date m DESCRIPTION As Asphalt - Y" GF 0. durk gray (2,54, N4/0) Gravel (GP) 0.5/3 ., 40% coorse (grave)) size sand, 60% . · o Fre gravel, damp, no od or (very title to look at) 0 ' .0 ۵ 0.0 0.5/3 44,5 0.3 Go Sandy Gravel (GP) olive bon (2.54.4/4) ..... 69 5% low -plasticity fines, 35% fine to ο · coarse sand [1:2:3], 60% time . 0 ο. gravel, damp, no odor *o*<sub>0</sub> very little to look at 0 -3/3 1:14 olv. brn (2.54, 5/4) 0 ' 59. low-plesticity fines, 40% five . 0 to coarse send (1:2:3), 55% ٥ fine to coarse gravely mineral ٠, break-up, dump, no odor ्ण 9.5-0.6 10 • 11 1/3 sm Sand light olu, brn \$2,54,54 11.5-0.6 12 17 minarals 13 3/3 @ 20-257 med. Fina.3 60-65% five to coarse sand (1:2:3) 15% five to coarse gravel (1:2) damp, no odar 15 15-5 0.3 16 @ 25-30% low -med fine? 3/2 70-75% five to course send (1: 2:4 17 damp, no odor 18 • 17 15-20% low-med fines, 70-80% fine 3/3 to coarge soud (1:2:4), 5-10% fine graved damp , no odor 

									-							
Em	<b>S</b> Son	E>	F (PL)			OG RY	i O B(	F DR	IN	G	PROJECT No. $0952 - 044.02$ DATE $11/22/94$ BORING NO.CLIENT TOSCO 11132HP-1LOCATION 3201 35Th St., Oakland, CASheet 2LOGGED BY D. Galassoof 2					
Field location of boring:											Drilling Co.     Precision       Drill rig model     XD I       Drilling method     CPT       Hole dia.     23/8					
Groun	d Elev.		se	وم م	).   Datu	m					Boring completion data Grouted hole to surface adding asphalt paten to top of boring					
072	Pocket Penetrometer (TSF)	Blows/6 in. and/or Pressure (PSI)	Type of Sampler	Recovery (ft/ft)	Sample Number and Container Type	Depth	Samp <del>le</del> d Interval	Weil Detail	Soll/Rock Symbol	Graphic Log	Depth to      □       Depth to      □       Time     □       Date     □					
						21-			800 571 CL		DESCRIPTION Silty Sand (SM) continued Clay (CL) olive (54, 513) 95 % high-plast. Anos, 5% fine 3 and orange nothing, iron-staining, gray verining, damp, Refusal at 23.0' ador Boring terminoted					

Reviewed by: \_\_\_

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j

\_\_\_\_ Date: \_\_\_\_\_

### APPENDIX C

Geologic Cross-Sections



Residential

#### EXPLANATION



Existing monitoring well location Proposed monitoring well location Groundwater recovery well location Soil boring location, drilled May and July 2004 Groundwater flow direction and graduent (ft/ft) for May4, 2004 Soil bonng location, drilled 1994 F Hydrgeologic Cross-section location

#### SITE MAP WITH BORING WELL AND **CROSS-SECTION LOCATIONS**

F GURE 2



X-SOLIMTBEDIC18mp kg I SOIL SAMPLE ANANYTICAL PESULTS IN

WATER MIBE 75 Mg L. WATER SAMPLE ANANYTICAL RESULTS IN VICROGRAMS PER LITER

HYDROGEOLOGIC CROSS-SECTION A-A'

3201 35th Avenue Oakland, California 3



#### **EXPLANATION**



- NOT LOGGED EXCEPT FOR SINGLE SOIL SAMPLE AT 30-31 ft bgs
- LITHOLOGY INTERPRETED FROM CONE PENETROMETER LOG AND DATA

GP= GF4/EL GH= GPAVEL } - OH PERMEABLITY SP= SAND

SM=SILTY SAND GM=SI. TY GPA.EL GC=GPA ELY CLAY HODEPATE PERVEAS (14 SC=CLAYEY SAND

\fr =\$!! <sup>--</sup> 10 =JUAM 01. PH-18-48, 177 C~=CL∸Y



LITHOLOGY CONTACT, INFERRED WHERE

UST EXCAVATION; BACKFILLED WITH GRAVEL

30



Oakland, California

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• 1

#### HYDROGEOLOGIC CROSS-SECTION B-B'



#### APPENDIX D

Sensitive Receptors Survey

## SENSITIVE RECEPTORS SURVEY SITE SURVEY AND LITERATURE SEARCH

Client: <u>Bŕ</u>	Dil Con	npany		Project No.:	<u> 30-081-01</u>
Station No.:	11132				
Location:	3201 357	H AVe.	0x	antenin antenin d'	
City/State:	Ockland	C4			

I. Provide answers to the following questions:

	Α.	Is there a public water supply well within 2500 feet?	Y/N
		If Yes, Distance	ft.
	в.	Is there a private water supply well within 1000 feet?	Y/N N
		If Yes, Distance	ft.
	c.	Is there a subway within 1000 feet? If Yes, Distance	Y/N <u>N</u> ft.
	D.	Is there a basement within 1000 feet If Yes, Distance	? Y/N <u>V</u> ft.
	E.	Is there a school within 1000 feet? If Yes, Distance	$\frac{Y/N}{1000} \frac{7e5}{\text{ft.}}$
	F.	Is there a surface body of water within 1000 feet?	Y/N Yes
		If Yes, Distance Name	500 ft. PeralTA Creek
II.	Des	cribe type of local water supply.	
	Pub	olic: X	alayan ay an
	- S	Suppliers Name: East Bay Municipa	1 Water District Pardee Dam
	- S - D	Distance to Site:	
	Pri	vate:	

#### SENSITIVE RECEPTORS SURVEY SITE SURVEY AND LITERATURE SEARCH

#### Page 2

III. Distance to Nearest Adjacent Properties:

Residential50 ft.Commercial00 ft.Industrial1000 ft.Hospital11,000 ft.School (Allandale School)1000 ft.NameName

IV. Aquifer Classification, if available.

Class	I	- Special Ground Waters - Irreplaceable Drinking Water	
		- Ecologically Vital	
		- ECOLOGICALLY VICAL	
Class	II	- Current and Potential	
		Drinking Water Sources	
<b>01</b>		- Not Dotantial Source of	
CIASS	111	- NOC FOCENCIAL BOALCE OF	$\sim$
		Drinking Water	
		<del>.</del>	

V. Describe observation wells, if any.

Number Free Product?

// Y/N <u>ye</u>s

- VI. Signature of Preparer:  $M_alther A. Taylow$ Date: 2-20-91
- VII. Sketch of Site